

EXPERIMENTAL AND THEORETICAL INVESTIGATION
OF THE DIFFUSION LENGTH OF THERMAL
NEUTRONS IN GRAPHITE

by

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LIST OF SYMBOLS

a	extrapolated x dimension of pile.
b	extrapolated y dimension of pile.
B_m^2	material buckling of loaded pile.
B_G^2	geometric buckling of pile.
c	extrapolated z dimension of pile, measured from source.
d	extrapolated z dimension of multiplying lattice.
D	diffusion coefficient.
f_i	fraction of source neutrons in ith energy group.
f	thermal utilization.
J	neutron current, neutrons per cm^2 - second.
k_∞	multiplication factor in an infinite reactor.
k_{eff}	effective multiplication factor in a finite reactor.
L	diffusion length of thermal neutrons.
L_t	lattice diffusion length.
L_r	reflector diffusion length.
q	slowing down density, neutrons per cm^3 per second.
r_i	Gaussian range of neutrons in the ith energy group.

Greek Letters

γ_{mn}	reciprocal relaxation length of the mnth mode of the flux.
δ	reflector savings.
ϵ	fast fission factor.
η	fast neutrons produced per thermal fission.

LIST OF SYMBOLS (concl.)

κ	ratio of absorption cross section to diffusion coefficient.
λ_{tr}	transport mean free path.
Σ_a	macroscopic absorption cross section.
τ	Fermi age.
ϕ	thermal neutron flux, neutrons per cm^2 - second.
ϕ_{corr}	thermal neutron flux corrected for harmonics and end effects.

INTRODUCTION

The diffusion length of thermal neutrons in a moderating medium is a necessary parameter in most reactor calculations. The determination of this constant is, however, subject to the assumption of a particular mathematical model. The types of solutions most widely used can be classified in two broad categories: 1) One-group diffusion, in which all source neutrons are considered born at thermal energy. In this case the source is treated as a boundary condition on the thermal diffusion equation. 2) Age-diffusion, in which Fermi age theory is used to describe the source term in the thermal diffusion equation as the slowing down density from a source of high energy neutrons.

Discussions of one-group diffusion theory using specific thermal source boundary conditions can be found in several references (1, 10, 13, 25). Descriptions of age-diffusion can be found in references (5, 17, 18). A paper written by Wallace and LeCaine (31) presents mathematical solutions to the neutron diffusion problem in several geometries and subject to several different source considerations. Lee (15), of Hanford, discusses techniques designed to correct for the effect of various inhomogenieties in the moderating medium.

The most elementary technique used in the determination of diffusion length is to use the negative reciprocal of the slope of a plot of $\ln \phi$ vs. z for data taken in an exponential, or sigma pile. This simple analysis is described by Hoag (13) and assumes an infinite moderating medium and thereby avoids consideration of the higher harmonics

of the flux function. Glasstone and Edlund (11) describe a harmonic analysis procedure whereby the higher harmonics may be taken into account.

Methods used in this work include two different assumed thermal source boundary conditions; a method whereby consideration of the source condition is avoided completely, and a method which calculates a series of constants which would result from a fictitious thermal source equivalent to the existing fast source. Two approaches based on age-diffusion were used; 1) the assumption of a monoenergetic fast point source, and 2) the use of an empirically determined Gaussian range source which gives a closer approximation to the Pu-Be spectrum than a monoenergetic source. Results of each method are compared, and the extent of validity of the approximations discussed.

Previous work at Kansas State University leading to this work has been the determination of the Fermi age of Pu-Be neutrons both from theory and experiment by Steichen (26) and the empirical fit of a sum of exponential terms to the slowing down density in the KSU pile by Foulke (9).

THEORY

One-Group Diffusion Model

The theory of thermal neutron diffusion has been studied by many investigators (1, 10, 11, 16). The following paragraphs will serve to outline the basic theory with particular attention to the assumptions involved.

The change in neutron density in a volume element of a moderating medium is the result of (a) the net flow of neutrons through the boundary of the element, (b) the number of neutrons absorbed by the medium per unit time, and (c) the production of neutrons by sources within the element. Assuming Fick's law to be valid, the neutron current, defined as the number of neutrons per second flowing through a unit area normal to the direction of flow, can be expressed as

$$J = -D \text{ grad } \phi. \quad (1)$$

The net flow of neutrons into a volume element can be written in terms of the current as

$$- \text{div } J = \text{div } (D \text{ grad } \phi).$$

Assuming D , the diffusion coefficient, to be independent of position, it can be factored out of the above expression. Thus the leakage term can be written $D\nabla^2\phi$ and the equation of continuity becomes

$$D\nabla^2\phi - \sum_a \phi + S = \frac{\partial n}{\partial t} \quad (2)$$

For the purpose of this work, only steady state diffusion will be considered. The neutron source will be treated as a boundary condition in thermal source theory so that Eq. (2) becomes

$$D\nabla^2\phi - \sum_a \phi = 0. \quad (3)$$

Dividing both terms of (3) by D and defining $\frac{\Sigma_a}{D}$ as κ^2 results in the equation

$$\nabla^2 \phi - \kappa^2 \phi = 0 \quad (4)$$

where

$$\kappa^2 = \frac{\Sigma_a}{D} = \frac{1}{L^2}.$$

Conditions not previously mentioned which are necessary to the validity of elementary diffusion theory include the following:

1. There are no collisions between neutrons, which means that each neutron diffuses independently of all others. Weinberg and Wigner (32), and Hughes (14) point out the importance of this property due to the resulting simplification of the mathematics involved.

2. The neutrons diffuse with a constant (average) energy and no energy is gained or lost (on the average) in a collision with a nucleus. This assumption is supported by Hughes (14) who states that experimental evidence indicates that the Maxwellian distribution is maintained reasonably well throughout the diffusion process.

3. The flux is a slowly varying function throughout the pile, with no sharp dips or spikes. This assumption is essential to the validity of Fick's law, and means that diffusion theory is not applicable in close proximity to concentrated sources, absorbers, or the boundaries of the diffusing medium. It is also necessary that the medium be only slightly absorbing, since a high absorption cross

section would cause the neutron density to vary substantially within one mean-free path.

4. The neutron scattering is spherically symmetric or isotropic, allowing the velocity vector to be treated as a scalar in the equation of continuity. Since scattering is not isotropic near sources, boundaries, and absorbers, this assumption necessitates restrictions similar to those stated in condition (3).

The solution of Eq. (4) in rectangular geometry, with the origin at the source location, is derived in Appendix A, and given here as

$$\phi(x, y, z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} A_{mn} \cos \frac{m \pi x}{a} \cos \frac{n \pi y}{b} \sinh \gamma_{mn} (c - z) \quad (5)$$

where m and n are odd, and where a , b , and c are the extrapolated x , y , and z dimensions of the pile. The auxiliary separation constants equation is

$$-\alpha_m^2 - \beta_n^2 + \gamma_{mn}^2 = \kappa^2 \quad (6)$$

where

$$\alpha_m = \frac{m \pi}{a}$$

$$\beta_n = \frac{n \pi}{b}.$$

Equation (5) is derived with the origin at the center of the source plane. The constants A_{mn} may be determined analytically, through the use of a particular source boundary condition, or experimentally.

Point Thermal Source. Numerous investigators (5, 6, 22, 23) have used the assumption of a point source of thermal neutrons at the location of the physical source in diffusion length experiments. Other investigators (3, 7) have used several point sources superimposed upon one another to describe the thermal flux in a diffusing medium.

The application of the point thermal source condition involves the use of the Dirac delta function (11). By expanding the source in a series of orthogonal functions which satisfy the boundary conditions, $S \delta(x, y)$ at $z = 0$ can be written

$$S \delta(x, y) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} S_{mn} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \quad (7)$$

where m and n are odd. The S_{mn} 's may be regarded as sources for each mode of the flux. To obtain the values of the S_{mn} 's, each side of Eq. (7) should be multiplied by $\cos \frac{p\pi x}{a} \cos \frac{q\pi y}{b}$ and integrated over the interval of orthogonality, from $-\frac{a}{2}$ to $\frac{a}{2}$ and $-\frac{b}{2}$ to $\frac{b}{2}$. By virtue of the Dirac delta function, the left-hand side of Eq. (7) will reduce to S . Due to the principles of orthogonal functions the right side will become S_{mn} times one-half the orthogonality interval in each of the x and y directions, giving

$$S_{mn} = \frac{4S}{ab}. \quad (8)$$

Since only positive values of z will be used in this work, the current density in any one mode will be equal to one-half the total number of neutrons produced in that mode. The current

density in the mn mode can be found by using Fick's law, Eq. (1), and the expression for the thermal flux, Eq. (5), to give

$$J_{mn} = -D \left(\frac{\partial \phi_{mn}}{\partial z} \right)_{z=0} = D \gamma_{mn} A_{mn} \cos \frac{m \pi x}{a} \cos \frac{n \pi y}{b} \cosh \gamma_{mn} (c-z) \quad (9)$$

$m, n \text{ odd}$

Setting this expression equal to half the number of neutrons emitted by the source in the mn mode,

$$\frac{2S}{ab} \cos \frac{m \pi x}{a} \cos \frac{n \pi y}{b},$$

results in an expression for A_{mn} ,

$$A_{mn} = \frac{2S}{ab D \gamma_{mn} \cosh \gamma_{mn} c} \quad (10)$$

Substituting Eq. (10) into Eq. (5) will give an expression for the flux due to a point source of thermal neutrons located at the origin of the co-ordinate system

$$\phi(x, y, z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{2S}{ab D \gamma_{mn}} \cos \frac{m \pi x}{a} \cos \frac{n \pi y}{b} \frac{\sinh \gamma_{mn} (c-z)}{\cosh \gamma_{mn} c} \quad (11)$$

where m and n are odd.

If a single point source is located at some arbitrary position $(x_i, y_i, 0)$ in the xy plane, then the integration of

$$S \int_{-a/2}^{a/2} \int_{-b/2}^{b/2} \delta(x_i, y_i) \cos \frac{m \pi x}{a} \cos \frac{n \pi y}{b} dx dy$$

would result in $S \cos \frac{m \pi x_i}{a} \cos \frac{n \pi y_i}{b}$. Since x_i and y_i are

constants, these cosine terms would carry through the analysis so that

$$A_{mn} = \frac{2 S \cos \frac{m \pi x_i}{a} \cos \frac{n \pi y_i}{b}}{ab D \gamma_{mn} \cosh \gamma_{mn} c} .$$

For N sources located at various positions throughout the xy plane, superposition of fluxes yields

$$A_{mn} = \sum_{i=1}^N \frac{2 S \cos \frac{m \pi x_i}{a} \cos \frac{n \pi y_i}{b}}{ab D \gamma_{mn} \cosh \gamma_{mn} c} . \quad (12)$$

An equation describing the flux due to N point thermal sources located in the xy plane is then

$$\phi(x, y, z) = \sum_{i=1}^N \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{2 S}{ab D \gamma_{mn}} \cos \frac{m \pi x_i}{a} \cos \frac{n \pi y_i}{b} \cos \frac{m \pi x}{a} \cos \frac{n \pi y}{b} \frac{\sinh \gamma_{mn}(c-z)}{\cosh \gamma_{mn} c} \quad (13)$$

where m and n are odd.

To determine κ from Eq. (5) it is necessary to determine γ_{11} (or any other of the γ_{mn} 's). In order to accomplish this purpose the hyperbolic functions in Eq. (11) can be rewritten as

$$\phi(x, y, z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{2 S}{ab D \gamma_{mn}} \cos \frac{m \pi x}{a} \cos \frac{n \pi y}{b} e^{-\gamma_{mn} z} \left[\frac{1 - e^{-2\gamma_{mn}(c-z)}}{1 + e^{-2\gamma_{mn} c}} \right], \quad (14)$$

where m and n are odd.

It is desired to express the flux simply in the form

$$\phi(x, y, z) = C_H C_E e^{-\gamma_{11} z} \quad (15)$$

so that a linear least squares fit of $\ln \phi$ vs. z will have a slope equal to minus γ_{11} . In order to write Eq. (14) in the form of Eq. (15) it is necessary to factor the fundamental mode, $m = n = 1$, out of the summation. Defining

$$C_E = \left[\frac{1 - e^{-2\gamma_{11}(c-z)}}{1 - e^{-2\gamma_{11}c}} \right], \quad (16)$$

Eq. (14) can be written

$$\phi(x, y, z) = \frac{2S}{abD\gamma_{11}} \cos \frac{\pi x}{a} \cos \frac{\pi y}{b} e^{-\gamma_{11} z} C_E \left\{ 1 + \frac{\sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{\gamma_{11}}{\gamma_{mn}} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} e^{-\gamma_{mn} z} \left[\frac{1 - e^{-2\gamma_{mn}(c-z)}}{1 + e^{-2\gamma_{mn}c}} \right]}{C_E \cos \frac{\pi x}{a} \cos \frac{\pi y}{b}} \right\} \quad (17)$$

where m and n are odd, but not simultaneously equal to one.

Thus, C_H for a point thermal source is defined by

$$C_H = 1 + \frac{\sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \gamma_{11} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} e^{-\gamma_{mn} z} \left[\frac{1 - e^{-2\gamma_{mn}(c-z)}}{1 + e^{-2\gamma_{mn}c}} \right]}{\gamma_{mn} C_E \cos \frac{\pi x}{a} \cos \frac{\pi y}{b}} \quad (18)$$

where m and n are odd, but not simultaneously equal to one.

The fundamental mode end correction factor, C_E , and the composite end and harmonic correction factor, C_H , for the point

thermal source boundary condition are listed in Table 1, along with the corresponding correction factors for all other boundary conditions discussed in this paper.

The correction factors derived above are used in an iteration procedure for determination of an accurate value of γ_{11} starting from an initial estimate of γ_{11} . The initial value can be determined from a semi-log plot of neutron count rates vs. z . The steps in the iteration procedure are:

1. Using the initial estimate, $(\gamma_{11})_1$, C_E and C_H are calculated for each data point in a series of measurements along any vertical axis in the pile.

2. A series of corrected count rates is calculated according to

$$\phi_{\text{corr}} = \frac{\phi}{C_E C_H} .$$

3. The corrected count rates are used to obtain a new value, $(\gamma_{11})_2$, as the least squares slope of $\ln \phi_{\text{corr}}$ vs. z .

4. The new value, $(\gamma_{11})_2$, is compared with $(\gamma_{11})_1$, the value used to calculate the correction factors C_E and C_H . If the difference is not within a previously determined precision, $(\gamma_{11})_2$ replaces $(\gamma_{11})_1$ in step one and new correction factors are calculated leading to a third value, $(\gamma_{11})_3$. The precision is again checked until two successive values of γ_{11} are within the desired precision.

5. When a final value of γ_{11} has been obtained, it is used in Eq. (6) to calculate the diffusion length.

SOURCE BOUNDARY CONDITION	C_n^*	Ce
POINT THERMAL	$1 + \frac{\sum \frac{\sum}{m} \frac{\sum}{n} \frac{\sum}{p} \frac{\sum}{q} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \cos \frac{p\pi z}{c}}{C_e \cos \frac{\pi x}{a} \cos \frac{\pi y}{b} e^{-\gamma z}}$	$\left\{ \frac{1 - e^{-2\gamma c} (c-z)}{1 + e^{-2\gamma c}} \right\}$
CONSTANT THERMAL	$1 + \frac{\sum \frac{\sum}{m} \frac{\sum}{n} \frac{\sum}{p} \frac{\sum}{q} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \cos \frac{p\pi z}{c}}{C_e \cos \frac{\pi x}{a} \cos \frac{\pi y}{b} e^{-\gamma z}}$	$\left\{ \frac{1 - e^{-2\gamma c} (c-z)}{1 + e^{-2\gamma c}} \right\}$
DOUBLE ITERATION	$1 + \frac{\sum \frac{\sum}{m} \frac{\sum}{n} \frac{\sum}{p} \frac{\sum}{q} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \cos \frac{p\pi z}{c}}{C_e \cos \frac{\pi x}{a} \cos \frac{\pi y}{b} e^{-\gamma z}}$	$\left\{ \frac{1 - e^{-2\gamma c} (c-z)}{1 + e^{-2\gamma c}} \right\}$
MONOENERGETIC FAST SOURCE	$1 + \frac{\sum \frac{\sum}{m} \frac{\sum}{n} \frac{\sum}{p} \frac{\sum}{q} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \cos \frac{p\pi z}{c} \left\{ e^{-\gamma z} \left[1 + \operatorname{erf} \left(\frac{\sqrt{2}}{2} \frac{\gamma m n c}{\sqrt{a^2 + b^2}} \right) \right] + e^{-\gamma z} \left[1 - \operatorname{erf} \left(\frac{\sqrt{2}}{2} \frac{\gamma m n c}{\sqrt{a^2 + b^2}} \right) \right] \right\}}{C_e e^{-\gamma z} \cos \frac{\pi x}{a} \cos \frac{\pi y}{b} \left\{ e^{-\gamma z} \left[1 + \operatorname{erf} \left(\frac{\sqrt{2}}{2} \frac{\gamma m n c}{\sqrt{a^2 + b^2}} \right) \right] + e^{-\gamma z} \left[1 - \operatorname{erf} \left(\frac{\sqrt{2}}{2} \frac{\gamma m n c}{\sqrt{a^2 + b^2}} \right) \right] \right\}}$	$\left\{ \frac{1 - e^{-2\gamma c} (c-z)}{1 + e^{-2\gamma c}} \right\}$
GAUSSIAN RANGE EMPIRICAL SOURCE	$1 + \frac{\sum \frac{\sum}{m} \frac{\sum}{n} \frac{\sum}{p} \frac{\sum}{q} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \cos \frac{p\pi z}{c} \left\{ e^{-\gamma z} \left[1 + \operatorname{erf} \left(\frac{\sqrt{2}}{2} \frac{\gamma m n c}{\sqrt{a^2 + b^2}} \right) \right] + e^{-\gamma z} \left[1 - \operatorname{erf} \left(\frac{\sqrt{2}}{2} \frac{\gamma m n c}{\sqrt{a^2 + b^2}} \right) \right] \right\}}{C_e \sum \frac{\sum}{m} \frac{\sum}{n} \frac{\sum}{p} \frac{\sum}{q} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \cos \frac{p\pi z}{c} \left\{ e^{-\gamma z} \left[1 + \operatorname{erf} \left(\frac{\sqrt{2}}{2} \frac{\gamma m n c}{\sqrt{a^2 + b^2}} \right) \right] + e^{-\gamma z} \left[1 - \operatorname{erf} \left(\frac{\sqrt{2}}{2} \frac{\gamma m n c}{\sqrt{a^2 + b^2}} \right) \right] \right\}}$	$\left\{ \frac{1 - e^{-2\gamma c} (c-z)}{1 + e^{-2\gamma c}} \right\}$

* a , b AND c ARE ODD, AND NOT SIMULTANEOUSLY EQUAL TO ONE.

Table 1. Harmonic and end correction factors for methods studied.

An IBM 650 program for the determination of the diffusion length by the above method is described in Appendix C.

Constant Thermal Source. The assumption of a constant source of thermal neutrons in the xy plane at $z = 0$ is not often used since it is an obviously poor geometric assumption in most cases. It is included here primarily for purposes of comparison.

To determine an expression for A_{mn} based on a constant source of thermal neutrons let $z = 0$ in Eq. (5), and let $\phi(x, y, 0) = \phi_0$.

Thus,

$$\phi_0 = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} A_{mn} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \sinh \gamma_{mn} c \quad (19)$$

where m and n are odd. As for the point thermal source, multiplying both sides of the equation by $\cos \frac{p\pi x}{a} \cos \frac{q\pi y}{b}$ and integrating over the interval of orthogonality yields

$$\frac{4 \phi_0 ab}{mn \pi^2} (-1)^{\frac{m+n+2}{2}} = A_{mn} \sinh \gamma_{mn} c \left(\frac{ab}{4}\right).$$

The resulting expression for A_{mn} is

$$A_{mn} = \frac{16 \phi_0 (-1)^{\frac{m+n+2}{2}}}{mn \pi^2 \sinh \gamma_{mn} c} \quad (20)$$

Substituting Eq. (20) into Eq. (5) gives an expression for the flux due to a constant thermal source as

$$\phi(x, y, z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{16 \phi_0 (-1)^{\frac{m+n+2}{2}}}{mn \pi^2 \sinh \gamma_{mn} c} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \sinh \gamma_{mn} (c-z) \quad (21)$$

where m and n are odd.

Using the same procedure outlined in the section dealing with the point thermal source boundary condition, correction factors C_E and C_H can be derived from Eq. (21), and the flux expressed in the form of Eq. (15). These correction factors may then be used in an iteration procedure identical to that described previously to determine the diffusion length based upon the assumption of a constant thermal source. The correction factors C_E and C_H for this case are listed in Table I.

An IBM 650 program for the determination of diffusion length by the above method is described in Appendix D.

Ratio Method. In the use of the ratio method, no source boundary condition need be assumed. This method was originally presented by Uhrig (29) in 1959.

The procedure involves the application of orthogonality conditions to Eq. (5). Multiplying both sides of Eq. (5) by $\cos \frac{\pi x}{a} \cos \frac{\pi y}{b}$ and integrating over the interval of orthogonality yields

$$\int_{-a/2}^{a/2} \int_{-b/2}^{b/2} \phi(x, y, z_1) \cos \frac{\pi x}{a} \cos \frac{\pi y}{b} dx dy = A_{11} \frac{ab}{4} \sinh \gamma_{11}(c - z_1) \quad (22)$$

where z_1 is held constant. If the left side of Eq. (22) is defined as $F_{11}(z_1)$, then

$$F_{11}(z_1) \equiv \int_{-a/2}^{a/2} \int_{-b/2}^{b/2} \phi(x, y, z_1) \cos \frac{\pi x}{a} \cos \frac{\pi y}{b} dx dy. \quad (23)$$

$F(z_1)$ can be evaluated by using numerical integration techniques such as Simpson's rule. If this integration is performed at two different levels z_1 and z_2 the ratio of $F_{11}(z_1)$ to $F_{11}(z_2)$ can be written

$$\frac{F_{11}(z_1)}{F_{11}(z_2)} = \frac{\sinh \gamma_{11} (c - z_1)}{\sinh \gamma_{11} (c - z_2)} .$$

By expanding the hyperbolic functions in terms of exponentials the above equation becomes

$$\frac{F_{11}(z_1)}{F_{11}(z_2)} = e^{-\gamma_{11}(z_1 - z_2)} \left[\frac{1 - e^{-2\gamma_{11}(c - z_1)}}{1 - e^{-2\gamma_{11}(c - z_2)}} \right] . \quad (24)$$

Assuming the bracketed term in Eq. (24) to be equal to one, a first approximation of γ_{11} is

$$\gamma_{11} = \frac{1}{z_2 - z_1} \ell n \left[\frac{F_{11}(z_1)}{F_{11}(z_2)} \right] \quad (25)$$

Using an initial estimate provided by Eq. (25) an iterative procedure based upon Eq. (24) can be set up to solve for γ_{11} . IBM 650 programs for the evaluation of $F_{11}(z)$ and for the iterative solution for γ_{11} are described in Appendix E.

Double Iteration Method. Previous methods described have used assumed source boundary conditions to evaluate the constants A_{mn} in Eq. (5). In the ratio method described here, the evaluation of these constants was avoided completely. The double iteration method evaluates the constants A_{mn} experimentally.

To express each of the constants A_{mn} in a form in which they may be readily calculated both sides of Eq. (5) should be multiplied by $\cos \frac{p\pi x}{a} \cos \frac{q\pi y}{b}$, and integrated over the interval of orthogonality. Thus,

$$\int_{-a/2}^{a/2} \int_{-b/2}^{b/2} \phi(x, y, z) \cos \frac{p\pi x}{a} \cos \frac{q\pi y}{b} dx dy = A_{pq} \frac{ab}{4} \sinh \gamma_{pq} (c-z). \quad (26)$$

Defining F_{pq} as

$$F_{pq} = \int_{-a/2}^{a/2} \int_{-b/2}^{b/2} \phi(x, y, z) \cos \frac{p\pi x}{a} \cos \frac{q\pi y}{b} dx dy,$$

the constant A_{pq} can be written

$$A_{pq} = \frac{4F_{pq}}{ab \sinh \gamma_{pq} (c-z)}. \quad (27)$$

F_{pq} can be evaluated, using numerical integration techniques, from data taken at several points at a given elevation in the pile. Hence, it is possible to evaluate any constant A_{pq} subject to an initial assumption of γ_{11} .

The double iteration process may be described as follows:

1. The values of the constants A_{pq} are calculated using an initial estimate of γ_{11} .
2. Using these values of A_{pq} , correction factors C_E and C_H , derived in the same manner as those for the point thermal source and listed in Table 1, can be calculated. Thus

a correction factor iteration identical to that described previously can be used to determine a more accurate value of γ_{11} .

3. The value of γ_{11} obtained from the correction factor iteration process is then compared with the value used to calculate the constants A_{pq} . If the two values are not within a specified precision, the new value of γ_{11} resulting from the correction factor iteration process is used to calculate another set of A_{pq} 's.

4. The new set of A_{pq} 's is used in another correction factor iteration process to obtain a third value of γ_{11} .

5. The comparison described in step (3) is again made, and the process is repeated until the precision check is satisfied.

An IBM 650 program written to perform the double iteration analysis is described in Appendix F.

Experimental Pile Size. An experimental method of determining the effective x and y dimensions of a sub-critical assembly is outlined by Babb, et. al. (3). This method involves a trial and error solution for the effective pile size.

The variation of the thermal flux along the x axis where $y = 0$ and $z = \text{constant}$, is described by

$$\phi(x) = \sum_{n=1}^{\infty} A_n \cos \frac{n \pi x}{a}, \quad (28)$$

where n is odd, and where a represents the effective x dimension of the pile. Assuming a value of a , least squares values of the constants A_n can be calculated,

along with the error squared of the least squares fit. The best value of a is found by changing the initial estimate by an increment Δa until a minimum is found in the curve of error squared versus a . An IBM 650 program written to perform this analysis using a variable number of harmonics is described in Appendix G.

Age-Diffusion Model

In all of the previously described methods, the source neutrons were assumed to be of thermal energy. In actual practice, however, sources are used which produce neutrons of much higher energies. To account for this discrepancy, a combination of Fermi age theory and thermal diffusion theory is used. Fermi (18) used age - diffusion theory to describe the thermal flux due to a plane source of fast neutrons in a semi-infinite medium. Discussions of the application of age-diffusion theory to the determination of diffusion length can be found in several references (5, 7, 17).

The continuity equation for steady state thermal neutron diffusion is

$$\nabla^2 \phi - \kappa^2 \phi + \frac{S}{D} = 0. \quad (29)$$

Assuming a point source of fast neutrons, the source term in Eq. (29) can be described in terms of the thermal slowing down density, $q_{th}(r, \tau)$. The slowing down density is defined as the number of neutrons being slowed to thermal energy per unit volume per second, and is a function of the distance from the source and the age to thermal of the source neutrons.

Substituting this quantity into Eq. (29) gives

$$\nabla^2 \phi - \kappa^2 \phi + \frac{q_{th}(x, \tau)}{D} = 0 \quad (30)$$

The slowing down density, q_{th} , is described by the Fermi age equation

$$\nabla^2 q(x, \tau) = \frac{\partial q(x, \tau)}{\partial \tau} \quad (31)$$

The solution of Eqs. (30) and (31) for an infinitely tall rectangular parallelepiped is derived in Appendix B and stated here as

$$\begin{aligned} \phi(x, y, z) = & \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{Q_0}{\gamma_{mn}^{ab} D} e^{\kappa^2 \tau} \cos \frac{m \pi x}{a} \cos \frac{n \pi y}{b} \left[e^{-\gamma_{mn} z} \left\{ 1 + \right. \right. \\ & \left. \left. \operatorname{erf} \left(\frac{z}{2\sqrt{\tau}} - \gamma_{mn} \sqrt{\tau} \right) \right\} + e^{\gamma_{mn} z} \left\{ 1 - \operatorname{erf} \left(\frac{z}{2\sqrt{\tau}} + \gamma_{mn} \sqrt{\tau} \right) \right\} \right] \quad (32) \end{aligned}$$

where m and n are odd. Q_0 is the source strength in neutrons per second and τ is the age to thermal of the source neutrons.

Monoenergetic Fast Source. Equation (32) describes the thermal flux due to a point source of monoenergetic neutrons. This relationship can be used in two different ways to determine the diffusion length (7, 17). First, corrections to the original C_E and C_H for the point thermal source may be derived.

Second, Eq. (32) may itself be written in the form of Eq. (15)

$$\phi = C_E C_H e^{-\gamma_{11} z} \quad (15)$$

The second and more direct method will be used in this work.

On the basis of Eq. (32) the harmonic correction factor, C_H , can be derived by a procedure analogous to that outlined for the point thermal source. Since Eq. (32) is based upon an infinitely tall pile, C_E cannot be derived in the usual manner. Davenport, et. al. (7) state that an appropriate end correction would be the same as that used in thermal source theory. It was therefore decided to include the terms

$$(1 - e^{-2 \gamma_{mn}(c-z)})$$

in Eq. (32). This provides an end correction for each mode of the flux such as would result from replacing an exponential function (which approaches zero as z approaches infinity) by an hyperbolic function (which can be made equal to zero at a finite value of z). Thus the boundary condition that the flux go to zero at a finite value of z can be met intuitively. The correction factors C_E and C_H for the monoenergetic fast source condition are listed in Table I. An IBM 650 program, written to determine the diffusion length using these correction factors, is included in Appendix H.

Gaussian Range Empirical Source. The energy spectrum of Pu-Be sources, shown in Fig. 1, indicates that these sources are definitely not monoenergetic. This fact introduces a difference in the slowing down density from that expected from a monoenergetic fast source.

The one dimensional solution to the Fermi age equation for a monoenergetic point source of fast neutrons at the origin of an infinite column of rectangular sides a and b is derived in Appendix B and given here as

$$q(z, \tau) = \frac{4 Q_0}{ab \sqrt{4 \pi \tau}} \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} e^{-\pi^2 \tau \left(\frac{m^2}{a^2} + \frac{n^2}{b^2} \right)} e^{-\frac{z^2}{4 \tau}}$$

where m and n are odd. Defining

$$c = \frac{4}{ab \sqrt{4 \pi \tau}} \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} e^{-\pi^2 \tau \left(\frac{m^2}{a^2} + \frac{n^2}{b^2} \right)},$$

the expression for slowing down density becomes

$$q(z, \tau) = Q_0 c e^{-\frac{z^2}{4 \tau}} \quad (33)$$

for a monoenergetic fast source.

The $\sqrt{\tau}$ is often referred to as the slowing down length. The quantity $2 \sqrt{\tau}$ will be referred to as the Gaussian range denoted by

$$r = 2 \sqrt{\tau} \quad (34)$$

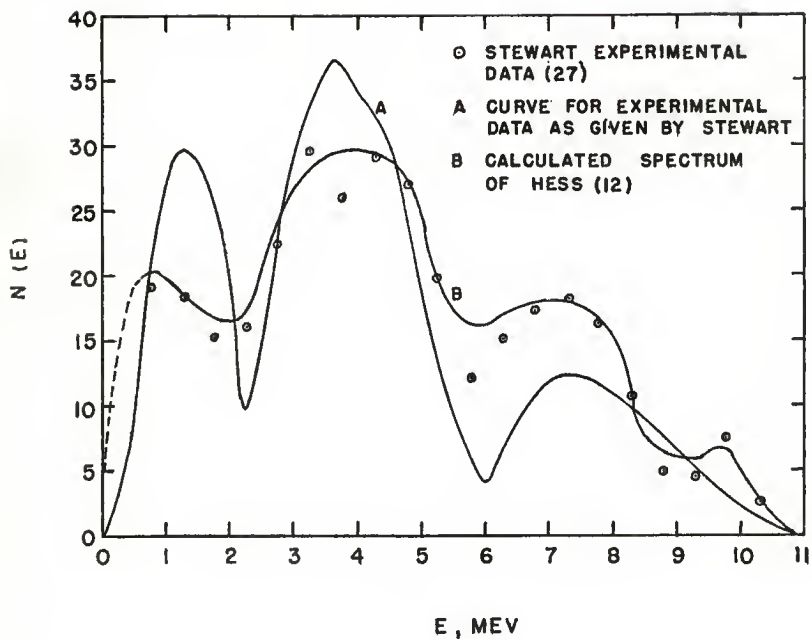


Fig. 1. Calculated and measured neutron energy spectrum for a Pu-Be neutron source.

Thus Eq. (33) can be written in terms of the Gaussian range as

$$q(z, \tau) = Q_0 c e^{-z^2/r^2} \quad (35)$$

A plot of the natural logarithm of the slowing down density vs. z^2 for a monoenergetic source would be expected to give a straight line of slope $-1/r^2$. However, in an experiment performed by Foulke (9) a plot of the natural logarithm of the activity of cadmium covered indium foils (proportional to the slowing down density to indium resonance) vs. z^2 was shown to be curved, due to the broad energy spectrum of the Pu-Be sources. This curve could be considered to be due to the superposition of an infinite number of monoenergetic sources. Hence the slowing down density should be expressed as

$$q(z, \tau) = Q_0 \sum_{i=1}^{\infty} f_i c_i e^{-z^2/r_i^2} \quad (36)$$

where f_i represents the fraction of the source neutrons in the i th energy group, and r_i represents the Gaussian range of the i th energy group. Foulke made a series of empirical fits of Eq. (36) to a plot of the natural logarithm of the activity of the cadmium covered indium foils vs. z^2 for the KSU Pu-Be sources.

If the Gaussian ranges used are defined from source energy to thermal energy, then Eq. (36) may be used as the source term in the thermal diffusion equation. The resulting expression for the thermal flux would be

$$\phi(x, y, z) = \sum_{i=1}^n \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{Q_0}{\gamma_{mn} ab D} e^{\kappa^2 r_i^2 / 4} \cos \frac{m \pi x}{a} \cos \frac{n \pi y}{b} \left[e^{-\gamma_{mn} z} \left\{ 1 + \operatorname{erf} \left(\frac{z}{r_i} - \frac{\gamma_{mn} r_i}{2} \right) \right\} + e^{\gamma_{mn} z} \left\{ 1 - \operatorname{erf} \left(-\frac{z}{r_i} + \frac{\gamma_{mn} r_i}{2} \right) \right\} \right] \quad (37)$$

where m and n are odd. In order to express the flux in the form of Eq. (15), the above equation must be treated similarly to Eq. (32) to derive the correction factors C_E and C_H . These correction factors for the Gaussian range empirical source are given in Table 1. An IBM 650 program for the determination of diffusion length by this method is described in Appendix I.

Determination of Material Buckling and Effective Multiplication Factor

The continuity equation for neutron diffusion in a multiplying medium differs from the non-multiplying case by the addition of a neutron production term. Thus Eq. (3) for steady state diffusion in a multiplying medium with an external source becomes

$$D \nabla^2 \phi - \Sigma_a \phi + k_{\infty} \Sigma_a \phi = 0 \quad (38)$$

where k_{∞} is the multiplication factor for an infinite reactor (no leakage). Equation (38) can be written in the form

$$\nabla^2 \phi + B_m^2 \phi = 0 \quad (39)$$

where the material buckling, B_m^2 , is defined by

$$B_m^2 = (k_\infty - 1) \frac{\Sigma_a}{D} \quad (40)$$

The solution of Eq. (39) in rectangular geometry and subject to the same boundary conditions as the non-multiplying case is

$$\phi(x, y, z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} A_{mn} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \sinh \gamma_{mn}(c-z) \quad (41)$$

where m and n are odd. The auxiliary separation constants equation is now

$$-\alpha_m^2 - \beta_n^2 + \gamma_{mn}^2 = -B_m^2. \quad (42)$$

If a point source of thermal neutrons is assumed at the origin of the pile co-ordinates, Fig. 3 as the physical source location, the constants A_{mn} are again given by Eq. (10). The material buckling can thus be calculated by the same procedure as was κ^2 in a non-multiplying medium.

If the reactor were critical, with no external source, the boundary conditions impressed on the solution for $\phi(x, y, z)$ would be that the flux be zero at all extrapolated boundaries. Thus, for a critical reactor at steady state (11),

$$\phi(x, y, z) = A \cos \frac{\pi x}{a} \cos \frac{\pi y}{b} \cos \frac{\pi z}{d} \quad (43)$$

where a , b , and d are the extrapolated x , y , and z dimensions of the critical assembly. The reasons that only one mode

is considered here are (a) that criticality can only be achieved in the first mode, and (b) that once criticality is achieved in this mode, the higher modes die out exponentially. The auxiliary separations constants equation for the critical solution is

$$\left(-\frac{\pi}{a}\right)^2 + \left(-\frac{\pi}{b}\right)^2 + \left(\frac{\pi}{d}\right)^2 = B_G^2. \quad (43)$$

Equation (43) also defines the geometric buckling. Hence it can be seen that a condition for criticality is

$$B_m^2 = B_G^2. \quad (44)$$

Glasstone and Edlund (11) define the effective multiplication factor k_{eff} as

$$k_{\text{eff}} = \frac{k_{\infty} e^{-B_G^2 \tau}}{1 + L^2 B_G^2} \quad (45)$$

where the condition for criticality is $k_{\text{eff}} = 1$. Assuming criticality, and simplifying the exponential term gives

$$1 = \frac{k_{\infty}}{(1 + L^2 B^2)(1 + \tau B^2)}.$$

Since B^2 is generally very small, further simplification yields

$$1 = \frac{k_{\infty}}{1 + B^2 (L_t^2 + \tau)}, \quad (47)$$

where L_t represents the diffusion length in the multiplying medium. L_t may be calculated from the diffusion length in the pure moderator by

$$L_t^2 = L^2 (1 - f) \quad (48)$$

where f is the thermal utilization of the lattice.

The infinite multiplication factor, k_{∞} , can be determined from Eq. (47) once B_m^2 , τ , and L_t are known. B_m^2 can be used in this case due to Eq. (44) and the assumption of criticality in deriving Eq. (47). Once k_{∞} has been determined it can be used in Eq. (45) to determine k_{eff} for any size reactor with a constant material buckling by varying B_G^2 . An IBM 650 program for the determination of the material buckling, k_{∞} , and k_{eff} by the methods described above is included as Appendix J.

EXPERIMENTAL FACILITIES

General Pile Description

The Kansas State University graphite pile, shown in Fig. 2, consisted of a rectangular parallelepiped, 68 in. square, and 100 in. high, resting on a concrete foundation. The pile was constructed of machined reactor grade graphite blocks approximately four inches in cross section and of various lengths. In stacking, the long dimension of the blocks was alternated 90° from layer to layer. As can be seen in Fig. 2, certain of the graphite blocks were drilled through their entire length to a diameter of 1.75 in.. The purpose of the holes was to accommodate fuel elements and they were located to provide an 8-in. lattice. For this study, in the effort to make a solid, homogeneous moderator, each of the fuel ports contained three graphite cylinders measuring 1.625 in. in diameter, and 22.68 in. in length. The cylinders were of the same material as the graphite blocks.



Fig. 2. KSU graphite pile.

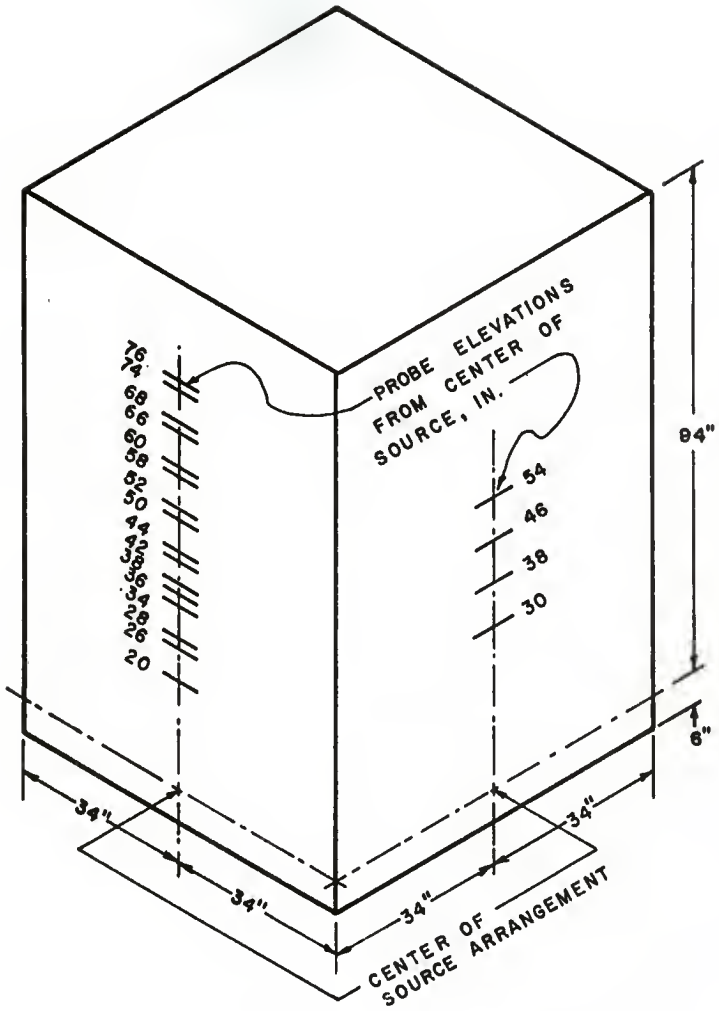


Fig. 3. Schematic diagram of KSU pile.

The graphite used in the construction of this pile was purchased from the Great Lakes Carbon Corporation. The blocks were machined from R - IHLM Nuclear Grade Graphite with a thermal neutron absorption cross section between 3.7 and 4.5 millibarns.

The graphite cylinders, being of smaller diameter than the fuel ports, left crescent-shaped air gaps of 0.125 in. between the tops of the cylinders and the tops of the fuel ports. The blocks along the central vertical axis of the pile contained horizontal foil slots, shown in Fig. 2, with a cross section of 1.281 in. by 0.343 in.. These slots could accommodate foil stringers as well as BF_3 or scintillation probes. The density of the solid graphite blocks was 1.683 g/cc. Steichen (26) calculated the percentage of air voids to be approximately 0.3 per cent. The resulting effective density of the pile was 1.678 g/cc.

A summary of the physical specifications of the one curie Pu-Be neutron sources is given in Table 2.

Non-Multiplying Configuration

For the determination of diffusion length, a solid, homogeneous moderator was needed. To accomplish this, the fuel ports were filled with graphite rods as mentioned above. The source configuration used was a five-source cluster at the center of the source plane (positions 5, 6, 7, 8, and 9 in Fig. 4). In this configuration, one source was located at the exact center of the source plane and the other four were \pm four inches from the center in either x or y direction.

Table 2. Summary of physical specifications of Plutonium-Beryllium neutron sources (4).

Source number	Grams Pu	Grams Be	Neutron emission* rate (n/sec)
365	7.87	15.99	1.54×10^6
366	7.87	16.01	1.73×10^6
367	7.86	15.89	1.82×10^6
368	7.86	15.88	1.69×10^6
369	7.86	16.09	1.71×10^6

* Recalibrated September 1961 at Mound Laboratories during integrity tests and recanning.

The inner container of each source is 0.85 in. in diameter, 0.90 in. in height, and is made of tantalum. The outside container of each source is 1.02 in. in diameter, 1.30 in. in height, and is made of stainless steel. All sources are sealed by welding. The melting point of tantalum is 5,425° F. The melting point of 18-8 stainless steel is 2,600° F.

The sources were calibrated by comparison to within ± 2 per cent of standards calibrated at Los Alamos Scientific Laboratory. The absolute accuracy of the Los Alamos standard is reported as ± 5 per cent, thus giving an absolute accuracy of ± 7 per cent to the sources listed above.

ONE OF 13 POSSIBLE SOURCE LOCATIONS

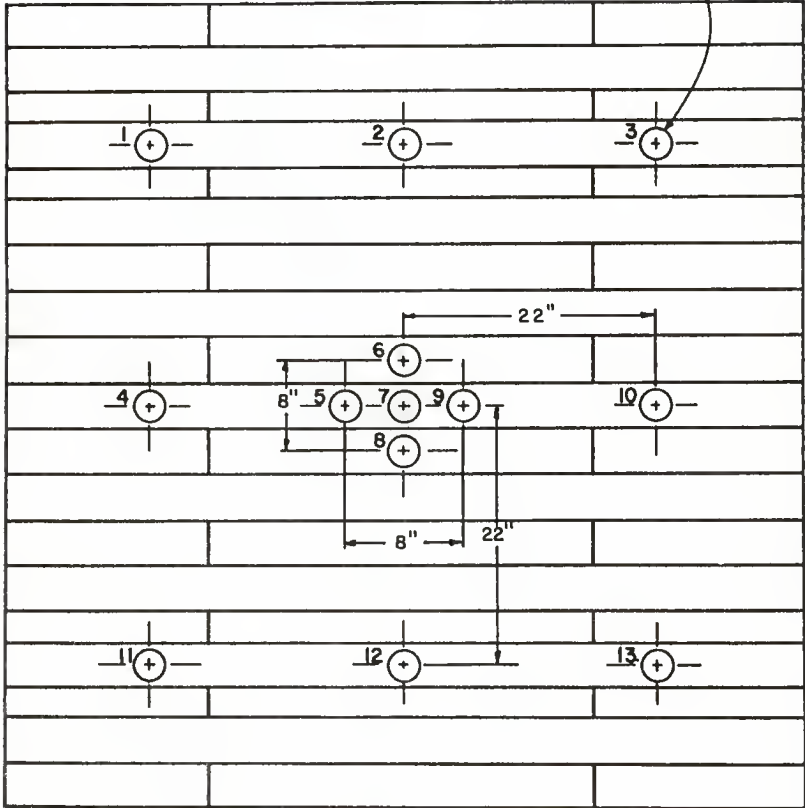


Fig. 4. Source locations in KSU pile.

A schematic diagram of the pile is presented as Fig. 3. The source plane is located six inches above the concrete foundation.

Multiplying Configuration

In this configuration, the fuel holes contain aluminum tubes 68 in. long, and 1.312 in. in outside diameter. Each tube is supported in the fuel port by three aluminum rings, one fixed at the center, and two removable rings at the ends. Eight depleted uranium, Savannah River type MK VII fuel elements, as pictured in Fig. 5, are placed in each tube. Figure 6 illustrates a portion of the loaded pile. The source configuration used with the loaded pile was the five-source cluster described above.

Neutron Detection System

The neutron detection system used throughout this work consisted of a Nuclear Chicago Model NC-202 BF_3 probe, Nuclear Engineering Inventory No. 97; a Nuclear Chicago Model 1062 preamplifier, NEI No. 210; a B. J. Electronics Model DMI-D count rate meter, NEI No. 363; a John Fluke Model 400 BDA high voltage power supply, NEI No. 188; a Baird Atomic Model 132 scaler, NEI No. 144; a Baird Atomic Model 960 timer, NEI No. 147; an Esterline Angus Model A. W. strip chart recorder, NEI No. 360; and a traversing mechanism, NEI No. 568.

The BF_3 probe active volume, with a length of $1/2$ inch and diameter of $3/16$ inch, contained B^{10}F_3 gas at a pressure of



Fig. 5. Fuel elements for KSU pile.



Fig. 6. KSU exponential pile.

70 cm Hg and at an enrichment of 96 per cent. The Model 1062 transistorized preamplifier had a length of 6.25 in. and a diameter of 1.5 in.. The BF₃ probe with the associated counting system is shown in Fig. 7.

The traversing mechanism, illustrated in Fig. 8, was capable of supporting the BF₃ probe in a variety of positions in the pile. This mechanism was designed and built at Kansas State University, and a detailed description of it is provided by L. R. Foulke (9).

In order to accommodate the BF₃ probe in the maximum number of positions and with the minimum amount of created void space, three 1.625 in. diameter graphite cylinders, shown in Fig. 9, were drilled along their central axis to a diameter of 3/8 in.. Their use to accommodate the probe may be seen in Fig. 4.

EXPERIMENTAL PROCEDURE

Cadmium Shutter Technique

The cadmium shutter technique involves the use of a cadmium shutter imposed between source and detector for the purpose of eliminating counts caused by epithermal neutrons. Data is taken without the shutter, and also with the shutter in place. The difference between the two sets of measurements is taken (28) as proportional to the thermal flux.

The cadmium shutter technique is generally used when the detector used is indium foil. The same purpose can be accomplished in this case as when cadmium covers are placed on the individual foils (28).

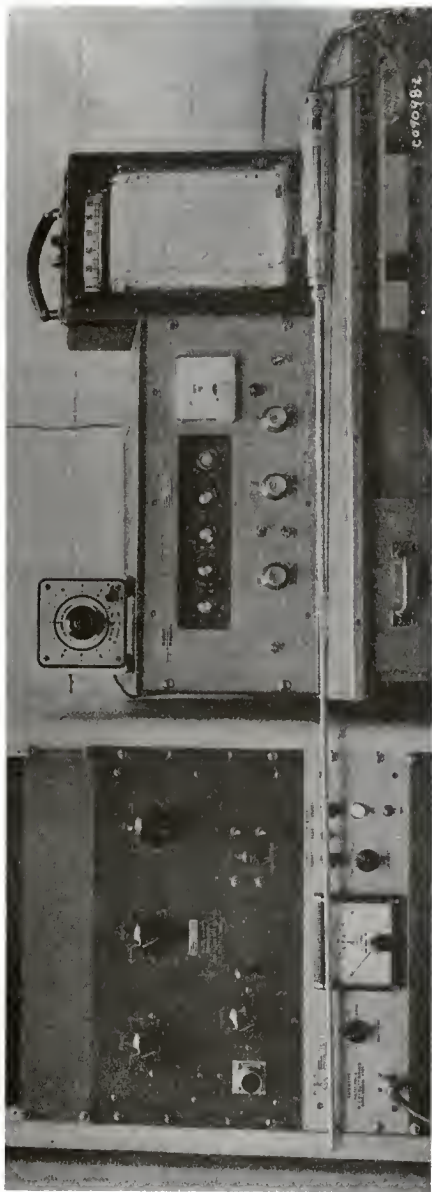


Fig. 7. Neutron probe counting system

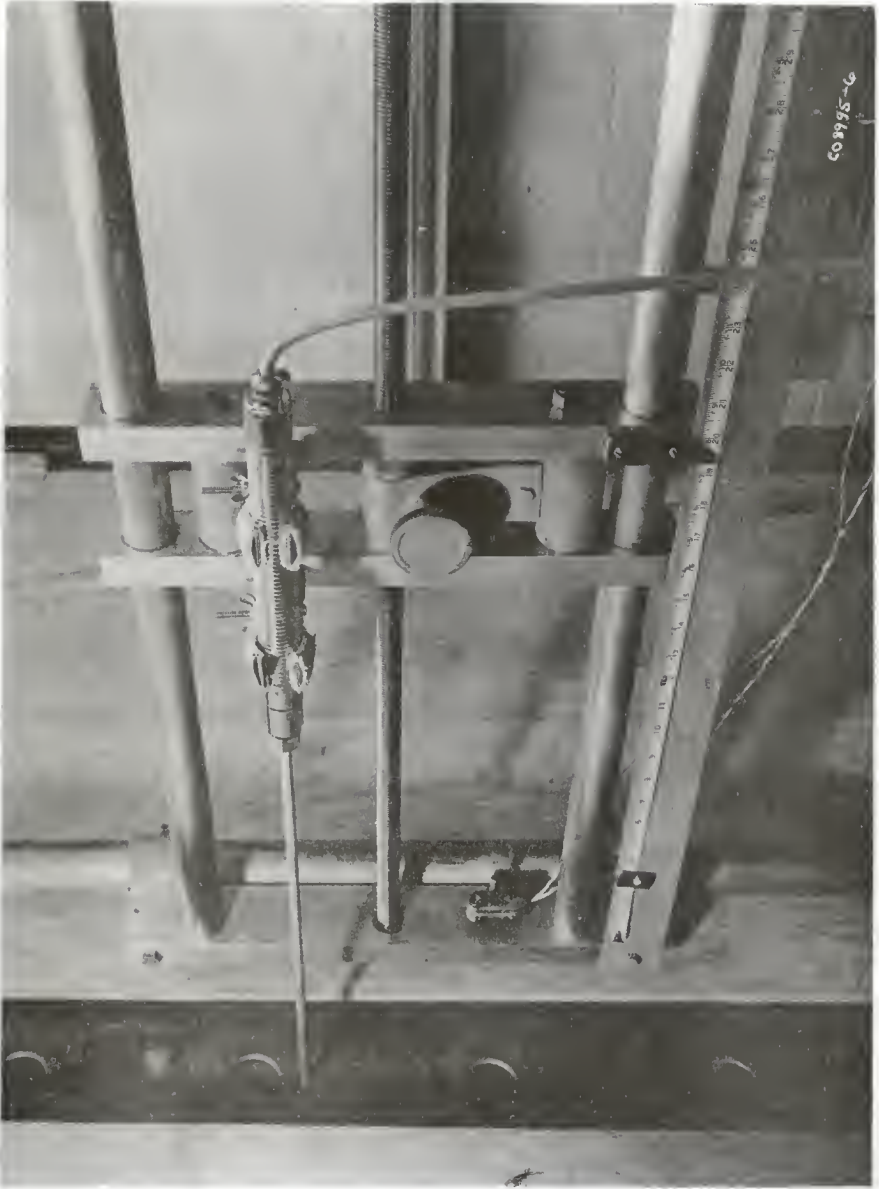


Fig. 8. Sliding assembly of traversing mechanism with scintillation probe



Fig. 9. Special graphite cylinders for accomodation of neutron probes

The cadmium shutter technique is often preferred, however, since it avoids error induced by overlapping of the indium and cadmium resonances.

When individually covered foils are used, the cadmium takes out a certain portion of the indium resonance neutrons before they reach the foil. Thus the covered foil count rates are not as high as they should be. This results in insufficient correction for epithermal neutrons in calculating the cadmium difference.

With the cadmium shutter technique, any neutron which would be at resonance energy at the foil elevation would be at a considerably higher energy at the lower elevation of the shutter. Thus it would be passed by the shutter and absorbed by the foil. In this way the absorption of resonance neutrons by the cadmium does not affect the cadmium difference count rates.

There is another effect, however, which leads one to believe that the use of the cadmium shutter does not produce accurate results. This is due to the fact that some neutrons are thermalized above the shutter but below the elevation of the foils. These neutrons, since they are epithermal at the shutter location, would not be absorbed by the cadmium. They would be highly absorbed by the indium, however. Since the activity of the foil with the cadmium shutter in place is supposed to be proportional to the indium resonance activity induced in the foils without the shutter, one can see that any activity induced by neutrons thermalized above the shutter is in excess of that desired. Thus the cadmium difference flux calculated in this manner will be too low, and not exactly proportional to the actual thermal flux.

Since the BF_3 probe used in this work had been shown (9) to give count rates consistently proportional to the thermal flux, even in close proximity to the source, it was considered adequate for determination of thermal flux. Further discussion of the cadmium shutter technique can be found in references (5) and (6).

Vertical Traverse Measurements

All data were obtained using the previously described BF_3 probe and associated counting system. Measurements were made in the foil stringer slots and in convenient fuel ports using the specially adapted cylinders shown in Fig. 9. All measurements were made with the active volume of the BF_3 probe centered on the vertical, or z axis of the pile by means of the traversing mechanism.

The counter was operated at 1400 volts with a pulse height sensitivity of 0.8. Some tendency toward day to day variation in counter sensitivity was encountered so that normalization counts were taken each day at a position 10 in. above the source plane at the center of the pile. Several short counts were taken in this position and their average used in the normalization.

Two separate vertical traverses were made, one with the non-multiplying configuration, and one with the multiplying configuration. In each case, data were taken such that approximately 10,000 counts were obtained in each position. This was done with 10 series of measurements getting 1,000 counts in each position. Figure 3 is a schematic diagram of the pile showing data locations.

Double Integral Mesh Data

The data used to evaluate the double integral

$$\int_{-a/2}^{a/2} \int_{-b/2}^{b/2} \phi(x, y, z) \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} dx dy$$

for the ratio method and double iteration analyses were obtained by running horizontal traverses in several fuel ports at a given elevation in the pile. Equally spaced measurements were made along the center fuel port from the center of the pile outward. The same procedure was then repeated for each of the remaining four fuel ports on one side of the pile. The space between successive data points was determined by dividing half the extrapolated pile dimension by the number of measurements to be made. The value of zero at the extrapolated boundary was included as an additional data point in evaluating the integral. The data were taken in three sets of 1,000 counts per position, giving a total of 3,000 counts per position.

Due to the symmetry of the pile, it was considered sufficient to evaluate the integral over one-quarter of the pile and multiply the result by four. Figure 10 illustrates the manner in which these data were taken. These data were normalized in the same manner as the vertical traverses.

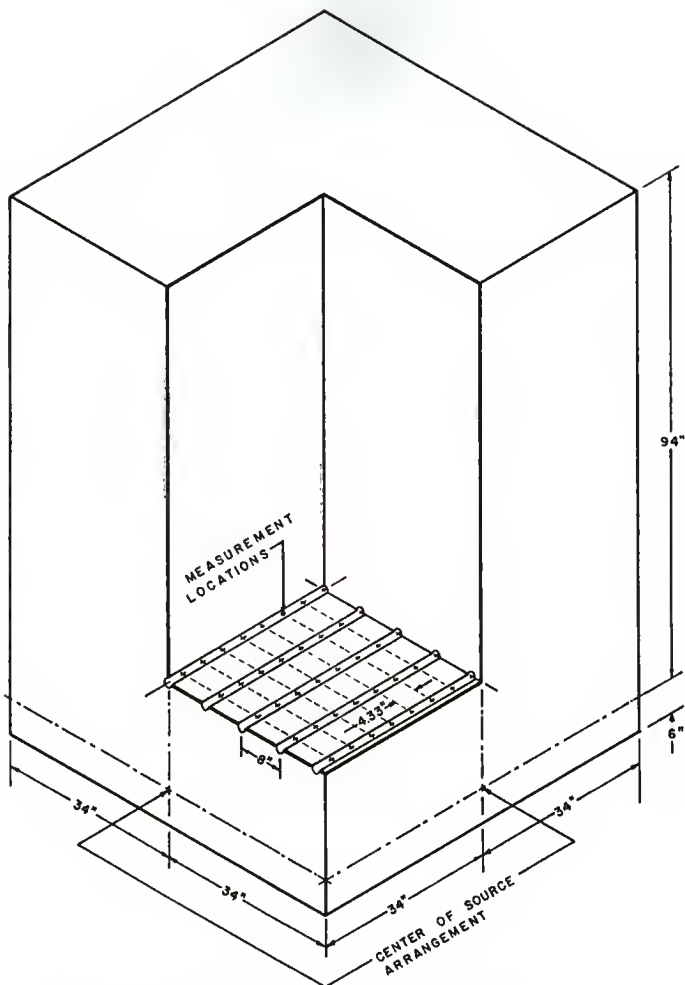


Fig. 10. Schematic diagram of KSU pile illustrating method of obtaining double integral mesh data.

Horizontal Traverses

Horizontal traverses for the experimental determination of the effective pile size were taken such that approximately 5,000 counts were obtained in each of nine positions from the center of the pile outward. This was done with five series of measurements getting 1,000 counts in each position. Certain of the graphite blocks were removed and inverted so that it was possible to make both north-south and east-west traverses at elevations of 38 in., 46 in., and 54 in. above the source. These data were normalized in the same manner as the vertical traverses.

The strip chart recorder was used in conjunction with the count rate meter to monitor the counting during periods of operator absence, thus insuring that no erratic data were recorded.

DATA PRESENTATION AND ANALYSIS

Treatment of Raw Data

The data obtained for each of the vertical traverses were corrected for background and are listed in Table 3 in the form of counts per minute. The deviation reported is the standard deviation of the mean in each case.

The double integral mesh data presented some difficulty due to low count rates and poor statistics near the outside of the pile. An attempt was made to correct this difficulty through a statistical analysis of the data based upon the equation

Table 3. Vertical traverse data sets.

Distance from source plane (Fig. 3)	BF ₃ Count Rates		
	Non-Multiplying configuration		Multiplying configuration
inches	counts per minute		counts per minute
20.000	3009.8	± 20.8	
26.156	1906.2	± 15.8	
28.000	1621.4	± 14.2	
30.156	1400.0	± 12.7	
34.156	998.5	± 9.0	946.0 ± 7.7
36.000	841.1	± 8.1	
38.843	737.3	± 7.7	756.0 ± 4.1
42.156	513.7	± 2.6	597.0 ± 6.3
44.000	434.5	± 2.9	
46.156	367.1	± 3.3	
50.156	262.4	± 3.0	351.3 ± 5.0
52.000	226.5	± 2.3	
54.156	196.1	± 2.1	
58.156	138.8	± 1.7	218.3 ± 2.1
60.000	121.1	± 1.0	
66.156	71.4	± 0.8	136.8 ± 1.4
68.000	62.1	± 0.9	
74.156	36.3	± 0.4	79.4 ± 1.1
76.000	31.2	± 0.4	
82.156	16.0	± 0.2	44.4 ± 2.9
84.000	12.6	± 0.1	

$$\phi(x) = \sum_{m=1}^5 A_m \cos \frac{m \pi x}{a} \quad (49)$$

where m is odd. The constants A_m were determined by a least squares analysis of the data in any one of the five horizontal traverses. Each experimental value was then compared with its least squares value, and if the difference was greater than the calculated 90 per cent confidence limits for that point, the point was rejected. All rejected points were replaced with values calculated from a least squares analysis of the accepted points. An IBM 650 program written to perform this analysis is described in Appendix K. The processed data, corrected for background, appears in Table 4. The deviation reported is the standard deviation of the mean in each case.

Horizontal traverse data, used in the determination of effective pile size, was corrected for background and listed in Table 5. The deviations reported are the standard deviations of the mean.

Analysis of Model Behavior

For reasons stated previously, it is known that elementary diffusion theory is not applicable near sources or boundaries. The amount of error induced in close proximity to the boundary of the diffusing medium is discussed quantitatively by Davison (8), in terms of transport theory. Very little information is available

Table 4b. Thermal neutron count rates at mesh points (FIG. 10)
for evaluation of double integral at $z = 28$ inches.

y co-ord. inches :		BF ₃ Count Rates									
		0	8	16	24	32	b=34.6875				
x co-ord. inches :	counts per min. :	counts per min. :	counts per min. :	counts per min. :	counts per min. :	counts per min. :	counts per min. :	counts per min. :	counts per min. :	counts per min. :	counts per min. :
0	1957.3 ± 29.4	1785.3 ± 33.8	1285.3 ± 23.5	730.7 ± 1.7	188.3 ± 7.2	0					
4.33	1960.7 ± 20.5	1735.8	1248.0 ± 11.7	710.0 ± 6.0	180.0 ± 7.2	0					
8.66	1794.7 ± 34.8	1594.0 ± 24.4	1143.0 ± 14.3	646.0 ± 1.0	164.9 ± 9.2	0					
13.00	1572.8 ± 7.8	1385.3 ± 33.8	1015.0	580.7 ± 4.3	145.3 ± 7.3	0					
17.34	1275.3 ± 15.1	1123.7	795.0 ± 7.0	478.7 ± 1.8	119.0 ± 11.2	0					
21.67	929.3 ± 8.4	839.7 ± 5.4	602.7 ± 9.0	347.7 ± 1.2	95.3 ± 5.5	0					
26.00	613.3 ± 7.2	562.0 ± 7.1	399.1 ± 1.3	239.2 ± 1.3	66.1 ± 2.0	0					
30.35	302.5 ± 4.5	273.3 ± 3.1	198.2 ± 2.0	119.0 ± 0.5	35.7	0					
a=34.687	0	0	0	0	0	0					

Table 4c. Thermal neutron count rates at mesh points (Fig. 10) for evaluation of double integral at $z = 36$ inches.

y co-ord. inches :		BF ₃ Count Rates											
0		8		16		24		32		34.6875			
x co-ord. inches :	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.		
0	1050.0 ± 17.7	942.7 ± 1.5	719.0 ± 22.7	416.4 ± 2.6	109.7 ± 1.1	0							
4.33	993.3 ± 3.8	919.3 ± 5.4	698.6	399.1 ± 13.2	107.3 ± 1.5	0							
8.66	951.3 ± 11.0	862.3 ± 14.4	641.0 ± 7.6	375.6 ± 7.3	98.4 ± 1.4	0							
13.00	815.0 ± 7.0	746.7 ± 18.8	574.0 ± 3.6	329.6 ± 4.6	86.0 ± 2.8	0							
17.34	675.7 ± 3.8	623.7 ± 12.9	476.9 ± 5.2	279.2 ± 5.1	23.3 ± 1.2	0							
21.67	515.1 ± 5.7	476.4 ± 5.1	352.3 ± 1.7	211.9 ± 5.0	57.9 ± 1.6	0							
26.00	337.2 ± 5.4	323.2 ± 6.7	244.1 ± 1.7	141.5 ± 1.9	41.0 ± 0.4	0							
30.35	169.0	166.3 ± 1.6	120.2 ± 1.5	71.7	22.2 ± 1.0	0							
a=34.687	0	0	0	0	0	0							

Table 4d. Thermal neutron count rates at mesh points (Fig. 10) for evaluation of double integral at $z = 44$ inches.

y co-ord: inches :		BF ₃ Count Rates											
0		8		16		24		32		34.6875			
x co-ord: inches :	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.		
0	551.3 ± 11.5	492.0 ± 5.2	379.5 ± 7.3	225.9 ± 4.5	63.3 ± 1.8	0							
4.33	529.3 ± 8.4	476.7 ± 1.0	376.2 ± 2.0	225.3 ± 2.5	58.9 ± 1.3	0							
8.66	496.0 ± 4.2	442.4 ± 11.2	347.5 ± 3.1	210.1 ± 5.2	58.0 ± 1.5	0							
13.00	433.8 ± 3.1	390.0 ± 8.8	310.7 ± 3.7	186.2 ± 3.2	52.6 ± 1.5	0							
17.34	375.8 ± 5.6	328.2 ± 4.6	257.7 ± 5.2	153.6 ± 3.5	43.2 ± 1.9	0							
21.67	280.0 ± 8.9	252.8 ± 3.2	204.3 ± 3.1	118.9 ± 1.8	35.8 ± 0.6	0							
26.00	193.3 ± 2.5	178.8 ± 1.5	136.0 ± 1.6	83.2 ± 2.0	25.8 ± 0.2	0							
30.35	99.9 ± 1.2	90.9	69.5 ± 2.4	41.0	13.2	0							
a=34.687	0	0	0	0	0	0							

Table 5a. Horizontal traverse data in east-west direction at three elevations.

Distance from center of pile inches	BF ₃ Count Rates		
	z = 38 inches counts per min.	z = 46 inches counts per min.	z = 54 inches counts per min.
0	859.9 ± 22.4	394.3 ± 4.0	201.2 ± 1.6
4	808.7 ± 22.2	387.5 ± 6.9	203.0 ± 7.4
8	779.7 ± 21.5	363.5 ± 8.6	187.7 ± 2.4
12	690.6 ± 14.8	333.7 ± 3.2	167.9 ± 3.0
16	594.8 ± 5.2	288.6 ± 6.8	150.7 ± 1.3
20	481.6 ± 7.9	234.9 ± 5.9	119.1 ± 2.0
24	351.1 ± 3.5	174.7 ± 4.2	92.1 ± 1.4
28	223.4 ± 4.0	113.2 ± 3.9	58.5 ± 0.5
32	104.7 ± 4.6	51.8 ± 4.0	26.3 ± 0.3

Table 5b. Horizontal traverse data in north-south direction at three elevations.

Distance from center of pile	BF ₃ Count Rates					
	z = 38 inches		z = 46 inches		z = 54 inches	
inches	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.	counts per min.
0	723.6	± 4.2	373.5	± 5.2	202.1	± 1.6
4	710.3	± 9.4	365.9	± 6.4	191.3	± 3.5
8	666.6	± 10.2	339.0	± 8.2	185.3	± 2.9
12	605.4	± 11.5	308.9	± 8.0	168.5	± 2.0
16	526.4	± 5.7	269.2	± 5.9	144.6	± 2.4
20	408.0	± 4.9	218.0	± 5.3	118.7	± 1.0
24	308.6	± 3.5	166.7	± 2.6	90.7	± 0.8
28	195.1	± 2.9	103.6	± 2.2	58.1	± 1.0
32	79.9	± 0.4	47.6	± 1.0	26.4	± 0.2

regarding the amount of error induced by using data points in close proximity to the source in a diffusion length analysis.

In attempting to determine the effect of using measurements made near the source to determine diffusion length two sources of error must be examined: (1) The possibility that a given assumed source boundary condition might lead to errors near the source, and (2) the possibility that the thermal diffusion model itself may be invalid.

A preliminary problem which was expected was inconsistency in results obtained using points too far from the source. The primary reason for such inconsistency being poor counting statistics near the top of the pile. For this reason, a series of determinations of L was made in which the point at the highest elevation was dropped from the data set for each determination. Consistency in the values obtained was used as a criterion for judging the highest level in the pile at which useable data could be obtained. The lowest data point used in this analysis was at least two diffusion lengths above the source. At this elevation the harmonic content is negligible (11), so that the one-group model and a given boundary condition could be assumed to be valid. When an effective upper limit had been established, the behavior of the model close to the source could be studied.

To examine a given assumed boundary condition based on either the one-group diffusion model or the age-diffusion model, a procedure was used whereby the effect of adding additional points near the source could be observed. Successive determinations of diffusion length were

made, each using one additional data point closer to the source. It is logical to assume that as long as all points used were far enough from the source, neither the assumed boundary condition nor the model would cause any deviation in the values obtained. Hence the apparent deviations of these values of L should be random about the average of the series of determinations.

The appearance of a decisive trend in several determinations of L , either increasing or decreasing, was taken as evidence of error induced by one of the two causes listed above.

RESULTS AND CONCLUSIONS

Experimental Effective Pile Size

The experimental determination of effective pile size described previously was attempted in the KSU pile. For this purpose, several horizontal traverses were made and these data were processed using the IBM 650 code described in Appendix G.

The effective size in each of the horizontal directions was determined at three elevations; 38, 46, and 54 in. above the source. Since it was expected that the harmonic content would not be the same at all elevations, provision was made in the IBM 650 code so that successive analyses could be performed with different assumed harmonic content.

Table 6a lists the results obtained in the east-west direction (parallel to pile void channels) with various assumed harmonic contents. Table 6b lists the corresponding results in the north-south

Table 6a. Results of determination of experimental pile size in the x direction, actual size 68 in. (theoretical value $a = 69.375$ in.).

Elevation inches	Effective Pile Size "a" in inches			
	Assumed Harmonic Content			
	1, 3	1, 3, 5	1, 3, 5, 7	1, 3, 5, 7, 9
38	68.9 ± 3.71	69.5 ± 3.71	68.9 ± 3.71	68.8 ± 3.71
46	69.1 ± 0.73	69.5 ± 0.73	69.9 ± 0.73	69.7 ± 0.73
54	71.0 ± 2.96	70.1 ± 2.96	71.3 ± 2.96	70.1 ± 2.96

Table 6b. Results of determination of experimental pile size in the y direction, actual size 68 in. (theoretical value $b = 69.375$).

Elevation inches	Effective Pile Size "b" in inches			
	Assumed Harmonic Content			
	1, 3	1, 3, 5	1, 3, 5, 7	1, 3, 5, 7, 9
38	69.8 ± 0.72	69.5 ± 0.72	68.7 ± 0.72	68.3 ± 0.72
46	69.9 ± 1.34	70.0 ± 1.34	70.5 ± 1.34	68.9 ± 1.34
54	70.5 ± 3.64	70.7 ± 3.64	72.0 ± 3.64	70.3 ± 3.64

direction. Deviations reported in these tables were calculated from the experimental data. Eight values of pile size were calculated

from the equation

$$a = \frac{\pi x}{\cos^{-1} \frac{\phi}{A_1}}$$

which was derived from Eq. (28) by assuming that all higher modes were insignificant. The value of ϕ at the center of the pile was used as A_1 . The standard deviation of the mean of the eight values of a is reported as the expected deviation of the calculated value of pile size. Since these deviations were determined directly from the raw data using only the fundamental mode, no difference in confidence limits appears with variation of assumed harmonic content.

The data in Tables 6a and 6b are much too random in nature to accurately define the effective pile size. The only noticeable trend is the increase of experimental pile size with increase in the elevation at which it was determined. This would indicate that the pile was shaped similar to an inverted pyramid, expanding toward the top. However, the confidence limits placed on these values indicate that a more extensive analysis should be performed before any valid conclusions may be drawn.

Since definite values of a and b could not be determined experimentally due to the difficulties mentioned above, the theoretical extrapolation distance was used in the remainder of this work. This quantity is described from transport theory as $0.71 \lambda_{tr}$, where λ_{tr} represents the transport mean free path in the medium. The value of λ_{tr} used was 2.58 ± 0.09 centimeters, the same value used by Foulke (9) in the standardization of the KSU pile. The value of the

effective pile size obtained in this manner was 69.375 in. in both horizontal directions.

Diffusion Length Results

Point Thermal Source. The results obtained by assuming a point thermal source are listed in Table 7. The first four determinations do not show any definite tendency to increase or decrease, but as points were considered closer to the source than 38 in., a definite increasing trend became apparent.

Table 7. Results obtained for the diffusion length based on assuming a point thermal source.

Elevation of Lowest Data Point	Number of Data Points Used	Diffusion Length $\rho = 1.678 \text{ g/cc}$
inches		cm
50	8	53.32 ± 0.87
44	9	53.84 ± 0.72
42	10	53.71 ± 0.59
38	11	53.69 ± 0.48
36	12	54.14 ± 0.51
34	13	54.23 ± 0.45
28	14	55.01 ± 0.61
26	15	55.98 ± 0.84

The above values were calculated using the 1, 3, 5, and 7 harmonics with the highest data point 76 inches above the source.

The type of behavior displayed by these calculations was taken as evidence that the point thermal source boundary condition was valid only beyond a distance of approximately 38 in. from the source. Probable causes of this phenomenon are the fact that the assumption disregards the high source energy and that the point source boundary condition exaggerated the harmonic content and would therefore be in error for all elevations low enough for the harmonics to be significant.

Constant Thermal Source. Diffusion length determinations based on an assumed constant thermal source boundary condition are listed in Table 8. Contrary to the case of the assumed point thermal source, no consistent results were obtained using this boundary condition. Instead, a consistent decrease in L was noticed as additional points were included close to the source, and the average value was considerably lower than that obtained using any other method.

Table 8. Results obtained for the diffusion length based on an assumed constant thermal source.

Elevation of : Lowest Data : Point : inches :	Number of Data : Points Used :	Diffusion Length $\rho = 1.678 \text{ g/cc}$: cm
50	8	50.38 \pm 0.58
44	9	50.17 \pm 0.45
42	10	49.62 \pm 0.47
38	11	48.92 \pm 0.52
36	12	48.78 \pm 0.45
34	13	48.37 \pm 0.46
28	14	47.86 \pm 0.47
26	15	47.58 \pm 0.44

The above values were calculated using the 1, 3, 5, and 7 harmonics with the highest data point 76 in. above the source. The conclusion was drawn from these results that since the constant thermal source boundary condition was not at all compatible with actual conditions, and since the results obtained by its use showed none of the desired consistency, that this boundary condition should be considered completely invalid. This was not unexpected in that this particular approximation disregards the high source energy and also uses an incorrect geometric approximation of the source. This boundary condition was used for comparative purposes, and to determine the effect of an erroneous boundary condition on diffusion length calculations.

Ratio Method. Evaluation of the diffusion length by the ratio method was accomplished using integrals evaluated at four different elevations. These integrals were used in six separate pairs, providing six independent determinations of diffusion length. The results of these determinations, at a pile density of 1.678 g/cc, are given in Table 9.

Table 9. Results of the ratio method for determination of diffusion length.

z_1	z_2	Ratio F_1/F_2	Diffusion Length ¹
inches	inches		cm
28	20	0.584	126.52
36	28	0.544	61.69
44	36	0.532	55.36
36	20	0.318	79.19
44	28	0.289	58.29
44	20	0.169	68.48

¹ Confidence limits not calculated due to erratic nature of the results.

It is immediately obvious that the range of these results is exceptionally wide. In fact, the difference between the lowest and highest values is 71.12 cm.

The basic difference between this method and all others is the absence of a vertical traverse. Since the diffusion length is known fundamentally to be strongly related to the attenuation in the z direction, it is logical to assume that a larger number of measurements at different elevations would serve to establish the value of L more firmly. The ratio method uses only two z 's, and the measurements made at these elevations, the integrals, cannot be calculated to the high degree of accuracy necessary because of the poor counting statistics near the edge of the pile.

Whereas the ratio method appeared desirable, since it avoided the necessity of imposing an erroneous boundary condition, the consideration described above and the actual results obtained indicate

that it is not a practical method for the determination of the diffusion length.

Double Iteration. Diffusion length results from the double iteration process, at a pile density of 1.678 g/cc, are listed in Table 10. All of these results were obtained using the 1, 3, and 5 harmonics. Horizontal traverses for the evaluation of the constants A_{mn} were taken at four different levels in the pile. Hence there are four sets of values, each based on constants determined at a different elevation.

It can be seen from Table 10 that the results obtained using constants evaluated at the higher elevations do not display the same consistency as those obtained using constants evaluated at the lower elevations. This can be explained as follows: The value of γ_{11} , and hence the value of L , obtained from this process is the direct result of a least squares analysis of a plot of $\ln \phi_{\text{corr}}$ vs. z . ϕ_{corr} is determined as explained previously by essentially removing the higher harmonics from consideration by means of the correction factor, C_H , derived previously. In order to do this accurately, it is generally advisable to include as many harmonics in the analysis as is feasible. This is particularly true when deriving C_H for a point close to the source where the harmonics are known to be of significance.

However, in determining A_{mn} for the higher harmonics at $z = 44$ in., for example, one is attempting to evaluate a quantity which is numerically insignificant. This is known to be the case because at

Table 10. Diffusion length results from the double iteration technique using the 1, 3, 5 harmonics.

Elevation of Lowest Point : inches	Diffusion Length, cm			
	Elevation at which Constants were Determined, inches			
	20	28	36	44
50	53.34 ± 1.64	53.35 ± 1.65	53.58 ± 1.68	54.47 ± 1.80
46	53.54 ± 1.26	53.55 ± 1.28	53.83 ± 1.29	54.88 ± 1.40
44	53.96 ± 1.06	53.98 ± 1.05	54.31 ± 1.09	55.52 ± 1.21
42	53.67 ± 0.88	53.68 ± 0.88	54.05 ± 0.90	55.37 ± 0.99
38	53.37 ± 0.72	53.38 ± 0.72	53.81 ± 0.74	55.34 ± 0.82
36	53.75 ± 0.67	53.76 ± 0.67	54.27 ± 0.70	56.05 ± 0.83
34	53.65 ± 0.58	53.65 ± 0.58	54.23 ± 0.60	56.20 ± 0.73
30	53.63 ± 0.49	53.63 ± 0.50	54.33 ± 0.52	56.62 ± 0.68
28	54.23 ± 0.59	54.28 ± 0.59	55.14 ± 0.67	-----
26	54.71 ± 0.60	54.70 ± 0.58	55.73 ± 0.71	-----

such distances from the source the harmonic content is negligible (11). The numerical integration process used in this analysis was found to be overestimating the magnitude of these harmonics at higher elevations. This was believed to have been caused by the efforts of the numerical integration process to give credence to the statistical noise inherent in the data. At lower elevations, however, where the harmonic content was appreciable, the estimate was considerably better. This statement is supported by Fig. 11, which illustrates the predicted relative contribution of the 13 and 31 harmonics as a function of distance from the source. Analytical curves based on the point thermal source and constant thermal source boundary conditions are included.

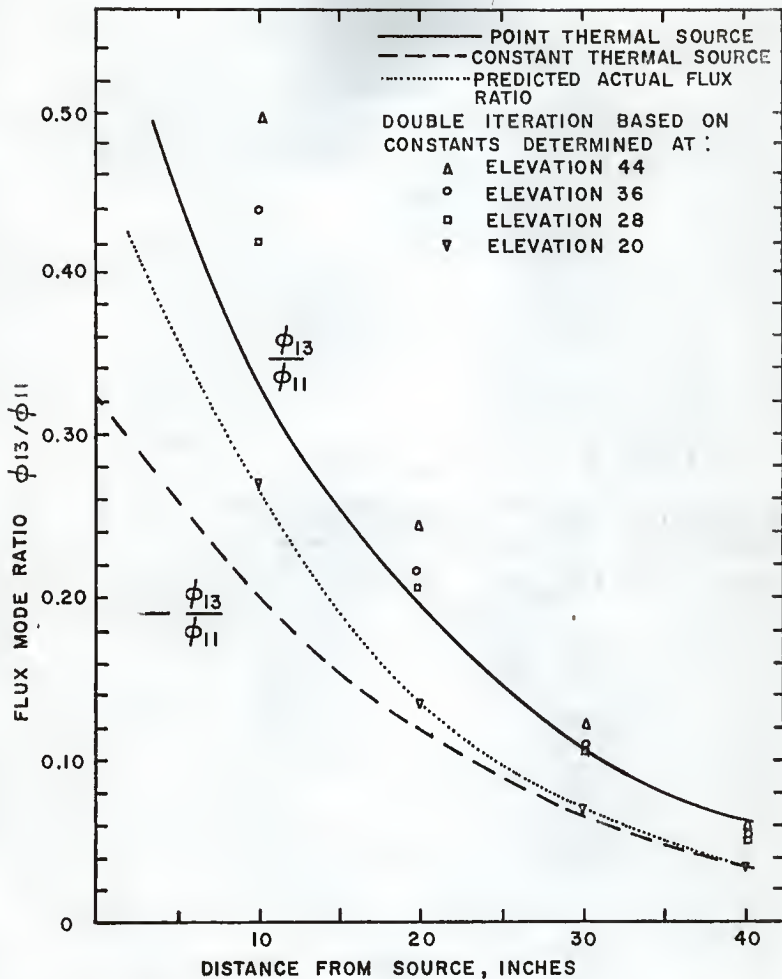


FIG. II. RELATIVE CONTRIBUTIONS OF ϕ_{13} HARMONICS AS A FUNCTION OF DISTANCE FROM SOURCE.

The fast source used can presumably be represented by an equivalent thermal source which will be neither a point nor constant, but some intermediate configuration. It is therefore logical to assume that the actual harmonic content of the flux function would be something in between these two specific thermal boundary conditions. It can be seen from Fig. 11 that as lower elevations are used to determine the constants A_{mn} , the predicted harmonic content is bounded by the point thermal and constant thermal source predictions.

Further evidence of the effect of harmonic content on the behavior of the double iteration technique is presented in Figs. 12, 13 and 14. Figure 12 is a plot of the data given in Table 10, and shows the behavior of this technique for all four elevations when the 1, 3, and 5 harmonics are used. Figure 13 shows the effect of neglecting the 5th harmonic with constants determined at elevation $z = 44$. Figure 14 shows this same effect plus the effect of taking the 7th harmonic into consideration. The data used in these plots are presented in Table 11. It is interesting to note that the effect of using additional harmonics in the analysis is much more pronounced at the higher elevation.

The conclusions to be reached from the observations mentioned above are that the double iteration technique gives valid results only when the constants A_{mn} are determined from data taken at a level in the pile where the harmonics contribute significantly to the total thermal flux.

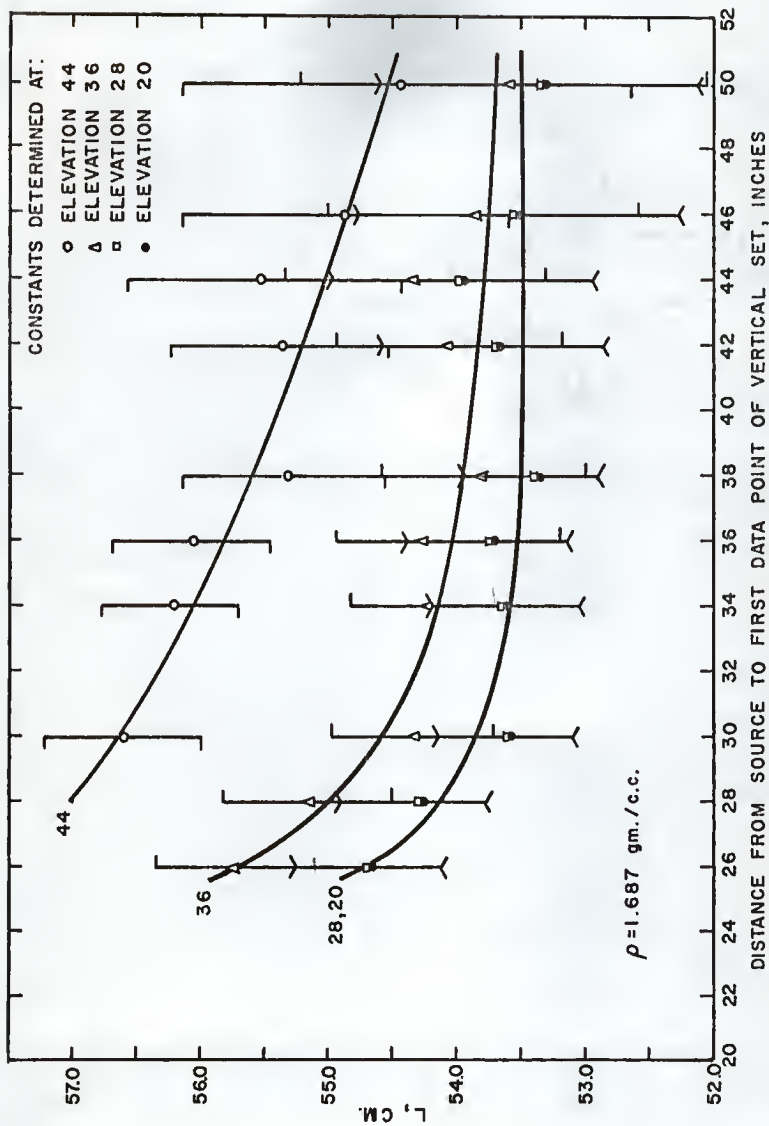


FIG. 12. BEHAVIOR OF DOUBLE ITERATION ANALYSIS AS POINTS ARE INCLUDED CLOSER TO THE SOURCE.

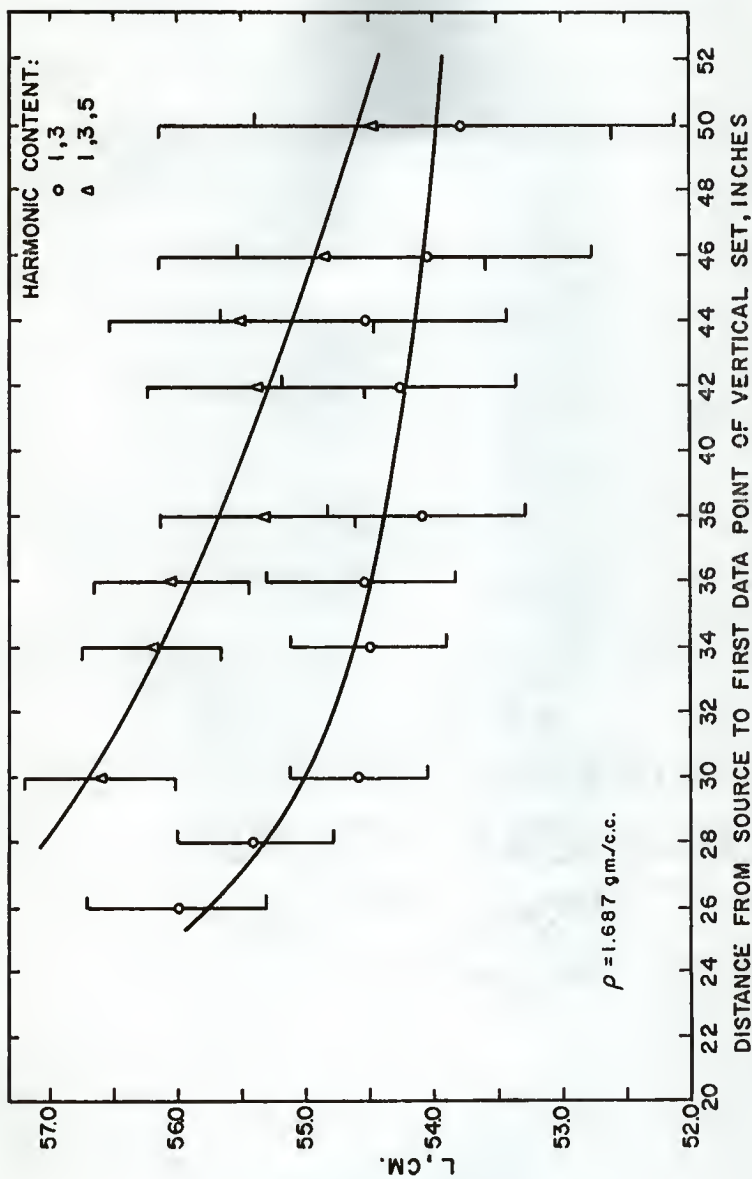


FIG. 13. EFFECT OF ASSUMPTION OF DIFFERENT HARMONIC CONTENT ON BEHAVIOR OF DOUBLE ITERATION METHOD USING CONSTANTS DETERMINED AT $Z=44$

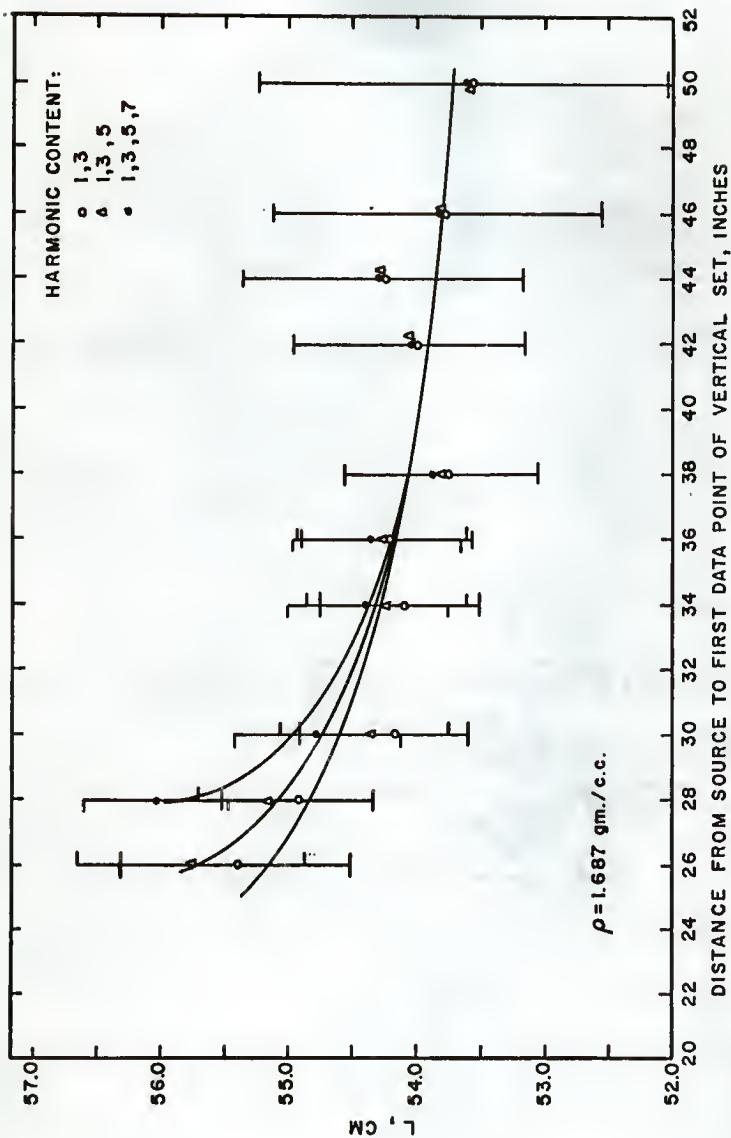


FIG.14. EFFECT OF ASSUMPTION OF DIFFERENT HARMONIC CONTENT ON BEHAVIOR OF DOUBLE ITERATION METHOD USING CONSTANTS DETERMINED AT $Z = 36$

Table 11. Diffusion length results obtained from the double iteration method with different harmonic contents.

Constants evaluation: elevation, inches :		44		:		36	
Harmonics used :		1, 3		1, 3, 5		1, 3, 5	
Elevation of lowest data point :		Diffusion : length :		Diffusion : length :		Diffusion : length :	
inches :		cm :		cm :		cm :	
50	53.76 ± 1.70	54.47 ± 1.80	53.58 ± 1.52	53.58 ± 1.68	53.57 ± 1.68		
46	54.03 ± 1.31	54.88 ± 1.40	53.82 ± 1.29	53.83 ± 1.29	53.82 ± 1.29		
44	54.53 ± 1.11	55.52 ± 1.21	54.29 ± 1.09	54.31 ± 1.09	54.29 ± 1.09		
42	54.27 ± 0.92	55.37 ± 0.99	54.01 ± 0.91	54.05 ± 0.90	54.04 ± 0.91		
38	54.04 ± 0.76	55.34 ± 0.82	53.75 ± 0.74	53.81 ± 0.74	53.84 ± 0.74		
36	54.53 ± 0.71	56.05 ± 0.83	54.19 ± 0.69	54.27 ± 0.70	54.35 ± 0.71		
34	54.49 ± 0.62	56.20 ± 0.73	54.13 ± 0.60	54.23 ± 0.60	54.38 ± 0.62		
30	54.59 ± 0.53	56.62 ± 0.68	54.17 ± 0.52	54.33 ± 0.52	54.76 ± 0.58		
28	55.40 ± 0.68	-----	54.91 ± 0.65	55.14 ± 0.67	56.03 ± 0.94		
26	55.98 ± 0.72	-----	55.41 ± 0.87	55.73 ± 0.71	-----		

Using the values of A_{mn} determined at elevation $z = 20$ in., the magnitude of the fundamental and the higher harmonics at the source plane could be calculated. Thus an equivalent thermal source condition can be described based upon the actual flux distribution in the pile. The constants A_{mn} used to calculate this equivalent source are listed in Table 12. The equivalent source, with calculated flux plots at distances of 10, 20, 30, and 40 in. above the source, is plotted in Fig. 15. A similar plot is made for the point thermal source boundary condition in Fig. 16. The double iteration equivalent boundary condition was plotted using the 11, 13, 31, and 33 harmonics. As indicated on the plot, these curves fit the normalized data accurately. It is believed that this equivalent thermal source condition could be duplicated within limits of experimental error using constants determined at elevation $z = 28$ in. and possibly also using constants evaluated at $z = 36$ in.

Table 12. Values of the constants A_{mn} evaluated by the double iteration technique at elevation $z = 20$ inches.

m :	n :	A_{mn}	
1	1	15.70	0.040
1	3	7.59	0.002×10^{-2}
3	1	7.59	0.002×10^{-2}
3	3	3.28	0.004×10^{-6}

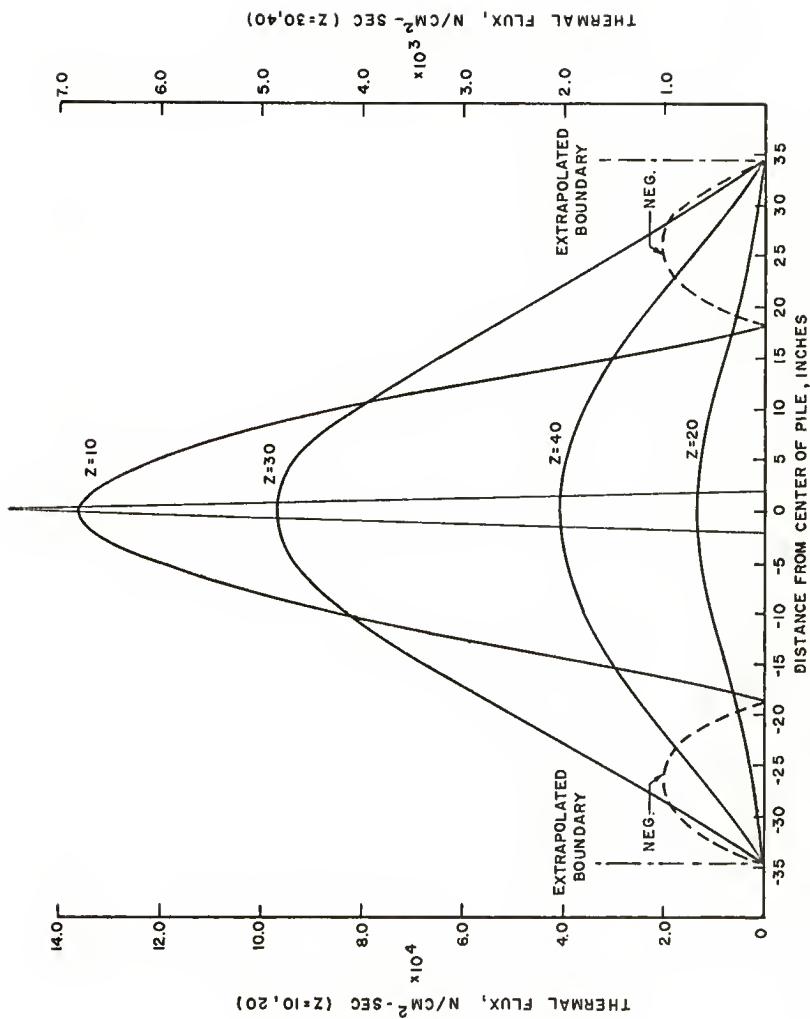


FIG. 15. HORIZONTAL BEHAVIOR OF FLUX FROM POINT THERMAL SOURCE AT $Z=0$, ELEVATIONS $Z=10, 20, 30$ AND 40 INCHES

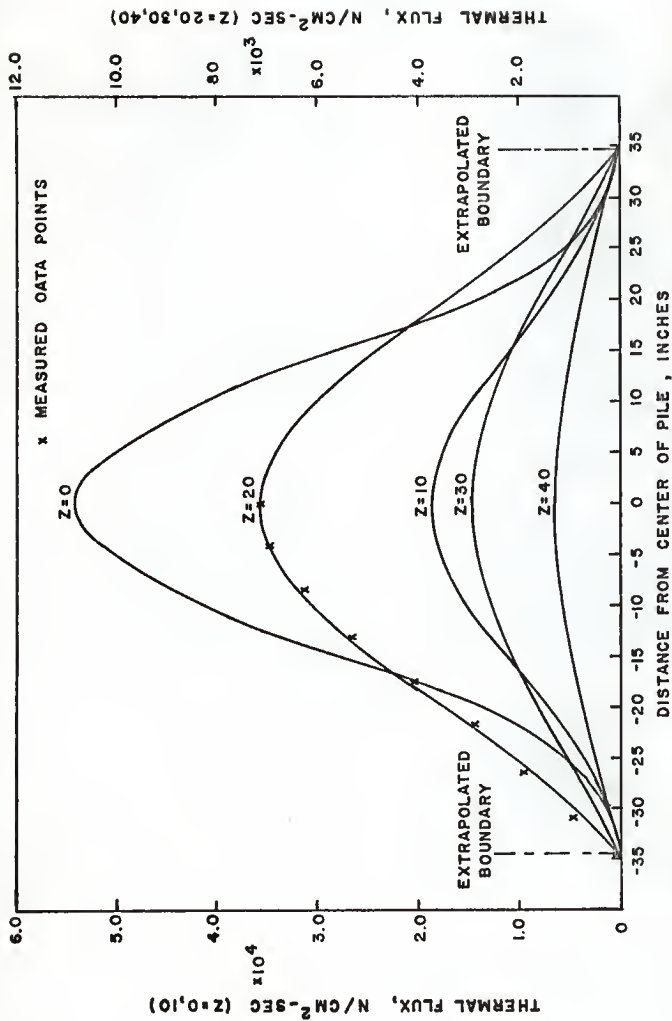


FIG. 15. HORIZONTAL BEHAVIOR OF FLUX FROM EQUIVALENT THERMAL SOURCE AT Z=0, ELEVATIONS Z=10, 20, 30, AND 40 INCHES.

Monoenergetic Fast Source. Diffusion length results based on age-diffusion theory assuming a monoenergetic fast source at a pile density of 1.678 g/cc are listed in Table 13. These results show a fair degree of consistency, but have a slight increasing trend not noticed in the double iteration results based on constants evaluated at elevation $z = 20$ inches.

Table 13. Diffusion length results based on a monoenergetic point source of fast neutrons.

Elevation of Lowest Data Point inches	Number of Data Points Used	Diffusion Length cm
46	10	53.09 ± 0.81
44	11	53.52 ± 0.74
42	12	53.50 ± 0.64
38	13	53.45 ± 0.55
36	14	53.79 ± 0.53
34	15	53.76 ± 0.47
30	16	53.64 ± 0.42
28	17	53.90 ± 0.40
26	18	53.92 ± 0.37

Examination of the results listed in Table 13 indicate that the assumption of a monoenergetic fast source for the determination of diffusion length is reasonably good over the region studied. In order to more firmly establish the validity of this assumption, the effect of variation of the age of Pu-Be neutrons should be studied. The value used in this work was 426 cm² as reported by Steichen (26). Table 14

lists diffusion length results for several values of age.

Table 14. Effect of variation of age on determinations of L assuming a monoenergetic fast source.

Number of Data Points	Fermi Age of Pu-Be Neutrons	Diffusion Length
	cm ²	cm
10	446	53.08 ± 0.81
10	436	53.09 ± 0.81
10	426	53.09 ± 0.81
10	416	53.09 ± 0.81
10	406	53.10 ± 0.81
10	396	53.10 ± 0.81
10	386	53.11 ± 0.81
10	376	53.11 ± 0.81

The obvious conclusion to be drawn from Table 14 is that the results obtained by assuming a monoenergetic fast point source are almost completely insensitive to normal uncertainty in the value of the Fermi age.

Gaussian Range Empirical Source. The results of the determination of diffusion length based on an empirically determined fast source described by Gaussian ranges and range fractions, at a pile density of 1.678 g/cc, are given in Table 15. The uniformity of the results is quite good, however, the average is slightly lower than that of the point thermal source, double iteration, and monoenergetic fast source methods.

Table 15. Diffusion length results from Gaussian range empirical source.

Elevation of lowest data point	Number of data points used	Diffusion length
inches		cm
50	7	52.82 ± 1.56
46	8	52.96 ± 1.19
44	9	53.33 ± 0.92
42	10	53.01 ± 0.83
38	11	52.66 ± 0.70
36	12	52.99 ± 0.63
34	13	52.85 ± 0.55
30	14	52.76 ± 0.47

Table 16. Effect on diffusion length of using varying Gaussian range sets.

Set number	No. of terms	Error squared of fit to slowing down density	Equivalent Agg $\Sigma f_1 r_1^2/4$, cm ²	Diffusion length, cm
1	3	7.94×10^3	378.1	53.53 ± 1.58
2	3	8.17×10^3	379.6	53.56 ± 1.58
3	3	9.08×10^3	397.2	53.56 ± 1.58
4	3	9.17×10^3	396.5	53.12 ± 1.57
5	3	1.51×10^4	411.9	52.82 ± 1.56

Foulke (9) determined several sets of ranges from one set of indium foil data. Each set was determined by an exponential stripping method. The differences between the several sets of ranges was in the treatment of the raw indium foil count rates. Table 16 lists diffusion length results obtained using several of these sets with nine data points. The elevation of the lowest point was 50 in.

Set number five was used in the calculations for this work because it appeared to be the best fit of the experimental slowing down data (9). The empirical curve based on this set passed within the experimental deviations of the slowing down data for a greater portion of the points than did any of the other curves. Details on the data treatment and analysis may be found in reference (9). This evidence is presented here to point out the fact that the determination of diffusion length in this manner requires a very precise knowledge of the Gaussian ranges and range fractions. The small variations in the age and the equivalent age for the two methods indicate that neither can be said to be highly sensitive to determinations of these quantities.

General Comparison. The behavior of each of the methods studied is illustrated in Fig. 17. For clarity, confidence limits have been eliminated from this plot. However, the confidence limits for each value are listed in the respective tables of results for each method. It is apparent from this figure that all of the methods, with the exception of the constant thermal source, give results of essentially the same magnitude when considered only in the region where consistent results were obtained. Table 17 lists the value of diffusion length obtained

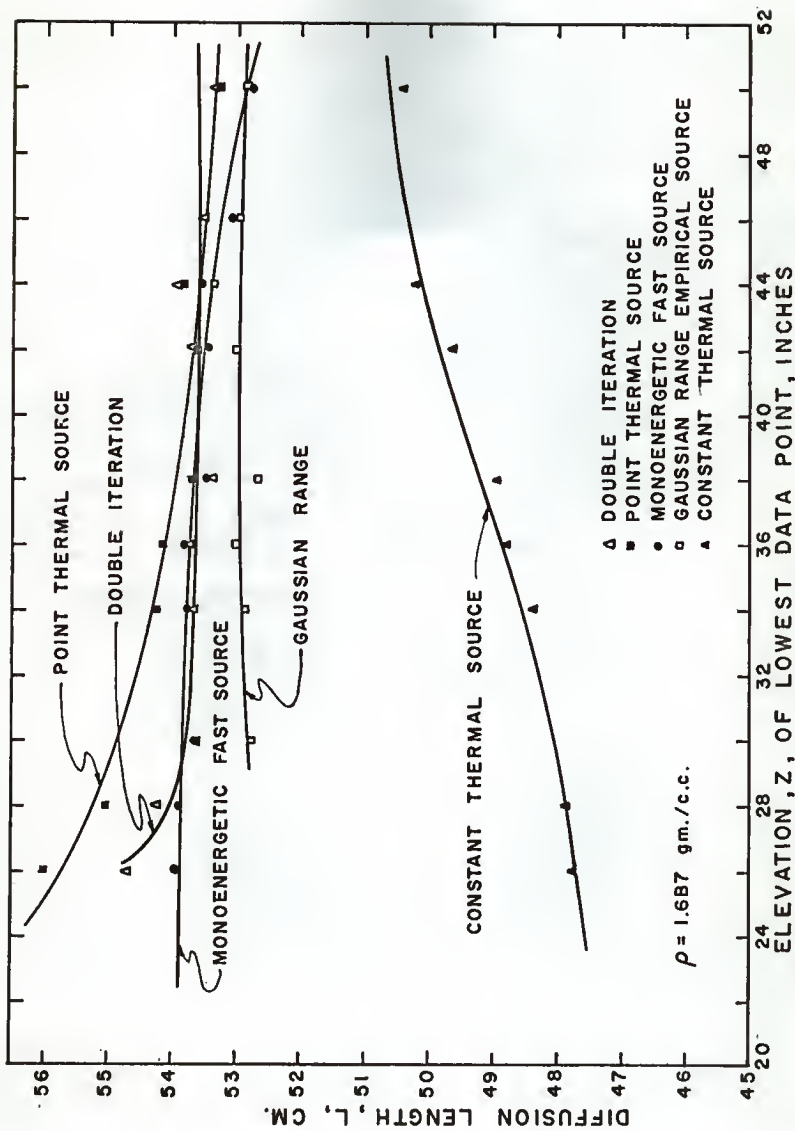


FIG. 17. VARIATION OF DIFFUSION LENGTH CAUSED BY INCLUDING DATA CLOSER TO THE SOURCE.

Table 17. Results of the determination of diffusion length for all methods considered.

		Diffusion length, centimeters				
		One-group model		Age-diffusion model		
Graphite Density g/cc	Point thermal source*	Constant thermal source	Ratio method	Double iteration**	Monenergetic fast source	Gaussian Range empirical source
1.678	53.64 ± 0.48	48.96 ± 0.58	74.92 ± 10.80	53.61 ± 0.60	53.53 ± 0.37	52.92 ± 0.47
1.600	56.25 ± 0.48	51.35 ± 0.58	78.57 ± 11.33	56.22 ± 0.60	56.14 ± 0.37	55.50 ± 0.47

* Average of first four determinations listed in Table 7.

** Average of first eight determinations listed in Table 10, constants determined at elevation $z = 20$ inches.

from each method. These values were obtained by taking the average of all determinations which exhibited only an apparent random distribution about the average. The confidence limits quoted with these values are the confidence limits obtained using all points in the region of consistent results. Values are reported at the KSU pile density and at a density of 1.6 g/cc as is commonly quoted in the literature.

Using as criteria for judgment; (1) the degree of consistency of results as data are included closer to the source, (2) the number of determinations for which this consistency is observed, and (3) the extent to which the average value, reported in Table 17, of a given method conformed to the averages of the other methods, after rejecting the ratio and constant thermal source methods, the best method appeared to be the double iteration procedure, based on one-group diffusion.

It can be seen from Fig. 17 that age-diffusion results did not exhibit the erratic behavior, as points were included near the source, that was displayed in the results obtained using the thermal diffusion model. This leads to the conclusion that age-diffusion may be the more reliable method for determination of diffusion length. However, the slight increasing trend noticed in the monoenergetic fast source results as data were included closer to the source cast some doubt on the reliability of this method. The Gaussian range method has been shown to be sensitive to determination of ranges and range fractions, and gives an average value somewhat lower than would be expected after examining the results of the other methods.

The point thermal source gave consistent results only at a considerably greater distance from the source than the other methods and

was ruled out for this reason. The constant thermal source method and the ratio method failed to produce satisfactory results. The double iteration method gave highly consistent results to within 30 in. of the source, and its average value was within 0.08 cm of the average values of the point thermal and monoenergetic fast source methods.

Based on the double iteration method, the value of L reported here will be 53.61 ± 0.60 cm, at a graphite density of 1.678 g/cc. At a density of 1.60 g/cc, this value becomes 56.22 ± 0.60 cm. Table 18 lists this value of L along with several other values obtained from the literature.

Table 18. Comparison of measurements of the diffusion length of thermal neutrons in graphite.

Diffusion Length L , cm	Graphite Density ρ , gr/cc	References
50.0	1.62	(10)
50.2	1.62	(11), (32)
52.39	1.60	(3)
53.39 - 55.21	1.60	(23)
54.40 ± 0.5	1.60	(7)
56.22 ± 0.6	1.60	this work

The range of diffusion lengths quoted from reference (23) include several values obtained in several different piles. The fact that the diffusion length measured in the KSU pile is higher than the literature values is attributed to the purity of the graphite (described in "EXPERIMENTAL FACILITIES").

Confidence Limits. Unless otherwise specified, all confidence limits placed on determinations of diffusion length in this work were calculated in the following manner: First, the standard deviation of γ_{11} was calculated from a linear regression analysis based on the corrected count rates from which that value of γ_{11} had been determined. The standard deviation of L was then calculated by means of propagation of errors. An IBM 650 program written to perform this analysis is described in Appendix L.

Material Buckling and Effective Multiplication Factor

The material buckling of the fully loaded KSU pile was determined experimentally using Eqs. (41) and (42) of the Theory. Equations (45) and (47) were used to evaluate the effective multiplication factor and the infinite multiplication factor respectively. The calculation of the material buckling was based on a point thermal source, so the data used was restricted to that which was within the previously determined region of validity of this boundary condition. The value of B_m^2 used in the remainder of the calculations was $7.755 \pm 0.41 \times 10^{-4}$ in. $^{-2}$. This value is the average of five separate determinations and the confidence limits are the standard deviation of the mean. The infinite multiplication factor, k_∞ , was calculated to be 1.104 ± 0.05 . This result was then used to extrapolate the KSU pile to critical size by varying B_G^2 . This was done by writing B_G^2 as a function of the extrapolated dimension a only. Thus by increasing a , the pile was expanded proportionally. Table 19 lists the extrapolated values of geometric

buckling and k_{eff} . These values of k_{eff} are plotted vs. pile size in Fig. 18.

Comparison of the values of material buckling calculated in the KSU pile compare favorably with values calculated by Richey (21) of Hanford in an eight-inch lattice with natural uranium as fuel.

Effective Size. Certain problems were encountered in determining the effective size of the multiplying lattice in the KSU pile. Whereas the top and side boundaries could be defined by adding the extrapolation distance of $0.71 \lambda_{\text{tr}}$, the bottom boundary required more detailed considerations.

It was decided to treat the unfueled pedestal of the pile as a reflector, so that the reflector savings δ could be approximately calculated from

$$\delta \approx L_t \tanh \frac{T}{L_r}$$

where T is the reflector thickness, and L_r the reflector diffusion length. The above equation is based on a slab reactor, and will thus overestimate the reflector savings. The error thus induced will not seriously affect the results of this analysis, however. The reflector was considered to be present throughout the entire analysis, although in a critical experiment it may be desirable not to have the reflector entering into the analysis.

The result of the reflector savings calculations was used to define an equivalent bare reactor, so that the extrapolation distance $0.71 \lambda_{\text{tr}}$ was also included in defining the lower boundary of the equivalent multiplying medium.

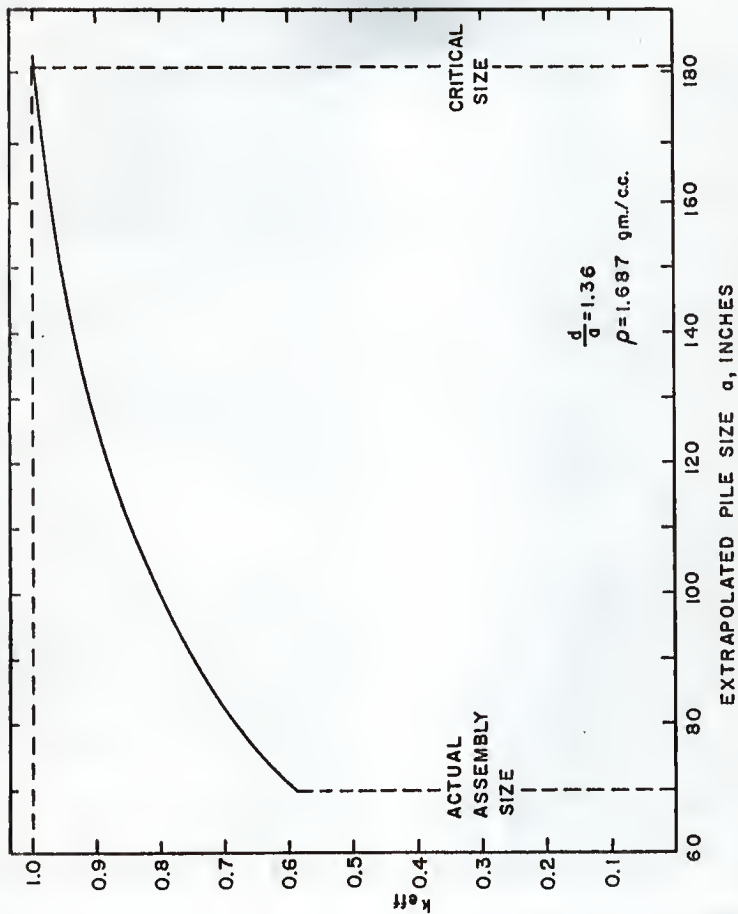
FIG. 18. MULTIPLICATION FACTOR, k_{eff} , vs. PILE SIZE, a .

Table 19. Extrapolation values of k_{eff} for the KSU pile (8-in. lattice, $\rho_{\text{graph}} = 1.689 \text{ g/cc}$).

Extrapolated Pile Dimension a	Geometric Buckling	k_{eff}
inches	in^{-2}	
69.375	5216×10^{-6}	0.58
86.375	3365×10^{-6}	0.72
101.375	2443×10^{-6}	0.81
116.375	1853×10^{-6}	0.87
131.375	1454×10^{-6}	0.91
146.375	1172×10^{-6}	0.95
161.375	964×10^{-6}	0.97
171.375	855×10^{-6}	0.98
180.895	767×10^{-6}	0.99

Lattice Diffusion Length. In the calculation of k_{∞} from Eq. (47) the value of L used should be that for the multiplying lattice. This value may be found from the diffusion length in the pure moderator by the equation

$$L_t^2 = L^2 (1 - f),$$

where L_t is the lattice diffusion length and f is the thermal utilization.

Thermal utilization was calculated as shown in Appendix M, from equations presented in ANL 5800 (20) which were based on integral transport theory in cylindrical geometry. These equations considered the case of a rod of fissionable material surrounded by an annular cooling gap and an annular moderator region. The value of f obtained in this manner was 0.820. Glasstone (10) uses a value of 1.308 for η ,

the number of neutrons produced per fission, in natural uranium. If the product of the fast fission factor ϵ , and the resonance escape probability p is assumed to be one which will be high (10), the four factor formula for k_{∞} yields $k_{\infty} = 1.073$. This value is slightly lower than the value obtained in this paper. The reason for this discrepancy is believed to be in the calculation of thermal utilization. Other methods of calculation of f were tried, but proved less satisfactory than that referred to above.

Since the thermal neutron flux in the uranium core of a heterogeneous cell is greatly depressed, the absorption of neutrons in the fuel is less for a heterogeneous cell than for a homogeneous cell. Hence the value of f for a homogeneous cell, calculated as 0.910, could be regarded as an upper limit of the actual value of the thermal utilization.

Fermi Age. The value of the Fermi age to thermal used in the calculations of material buckling and effective multiplication factor was 350 cm^2 . This value is reported by Weinberg and Wigner (32) and Glasstone and Edlund (11).

Suggestions for Further Work

The basic problem encountered in determination of diffusion length is in obtaining an accurate mathematical description of the thermal flux. Because of the nature of a sigma pile, the flux attenuation in the z direction will always be very nearly exponential. Determination of the fundamental mode attenuation coefficient, γ_{11} , should

always lead to knowledge of the diffusion length, L .

One possible model for further research in diffusion analysis is the use of a first collision density function as a boundary condition for age-diffusion theory. Instead of describing all neutrons as starting the slowing down process at the location of the physical point source, they should be considered as starting from the location of their first collisions. This would constitute a further refinement of the age-diffusion model.

Another such possibility is the use of two group methods to determine L . In a moderating medium (no multiplication) the fast flux would be independent of the thermal flux and could be solved for separately. The boundary condition of a point source, applied to the fast group, would be necessary to completely define the fast flux. The fast flux would then be used as a source term for the thermal flux equation, depending upon the knowledge of an appropriate slowing down cross section. This method would be subject to the same complications arising in most two-group calculations, that of determining constants for the fast group.

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APPENDICES

APPENDIX A

Solution to the Thermal
Diffusion Equation

The geometry for the solution to the thermal diffusion equation is shown in Fig. 19.

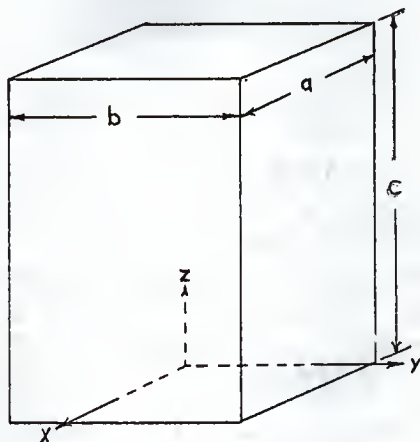


Fig. 19. Pile geometry for solution to thermal diffusion equation.

The equation to be solved is

$$\nabla^2 \phi - \kappa^2 \phi = 0 \quad (\text{A-1})$$

The solution is subject to the boundary conditions that the flux, ϕ , be zero at all extrapolated boundaries. This may be stated mathematically as

$$\phi \left(\pm \frac{a}{2}, y, z \right) = 0$$

$$\phi \left(x, \pm \frac{b}{2}, z \right) = 0$$

$$\phi \left(x, y, c \right) = 0$$

where a, b, and c are the extrapolated x, y, and z dimensions of the pile.

Equation (4) may be written in the form

$$\frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} + \frac{\partial^2 \phi}{\partial z^2} - \kappa^2 \phi = 0 \quad (A-2)$$

Assuming a solution of the form

$$\phi \left(x, y, z \right) = X(x) Y(y) Z(z) \quad (A-3)$$

equation (A-2) becomes

$$X''YZ + XY''Z + XYZ'' - \kappa^2 XYZ = 0$$

Dividing both sides of this equation by XYZ gives

$$\frac{X''}{X} + \frac{Y''}{Y} + \frac{Z''}{Z} - \kappa^2 = 0 \quad (A-4)$$

In order to meet the boundary conditions let each term of equation (A-4) be equal to a constant as follows:

$$\frac{X''}{X} = -\alpha^2 \quad (A-5a)$$

$$\frac{Y''}{Y} = -\beta^2 \quad (A-5b)$$

$$\frac{Z''}{Z} = +\gamma^2 \quad (A-5c)$$

Rewriting equation (A-5a) gives

$$X'' + \alpha_m^2 X = 0$$

A solution of this equation is

$$X(x) = A_m \cos \alpha_m x$$

To meet the boundary conditions that $X(a/2) = 0$,

$$\alpha_m = \frac{m\pi}{a}, m = 1, 3, 5, \dots$$

so that the solution for $X(x)$ is

$$X(x) = A_m \cos \frac{m\pi x}{a}, m = 1, 3, 5, \dots \quad (\text{A-6})$$

Similarly for $Y(y)$,

$$Y(y) = A_n \cos \frac{n\pi y}{b}, n = 1, 3, 5, \dots \quad (\text{A-7})$$

Rewriting equation (A-5c) gives

$$Z'' - \gamma_{mn}^2 Z = 0,$$

which has as a solution

$$Z(z) = C_{mn} \sinh \gamma_{mn} z$$

This function may be made to fit the boundary condition by altering the argument to give

$$Z(z) = C_{mn} \sinh \gamma_{mn} (c - z). \quad (\text{A-8})$$

Combining the solutions for $X(x)$, $Y(y)$ and $Z(z)$ in the manner indicated previously and combining coefficients yields

$$\phi(x, y, z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} A_{mn} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \sinh \gamma_{mn} (c-z) \quad (\text{A-9})$$

where m and n are summed over odd integers. Substituting (A-5a), (A-5b) and (A-5c) into equation (A-4) yields

$$-\alpha_m^2 - \beta_n^2 + \gamma_{mn}^2 = \kappa^2 \quad (\text{A-10})$$

which shall be referred to as the auxiliary separation constants equation in this work. Substituting in the expressions for α_m and β_n the above equation becomes

$$-\left(\frac{m\pi}{a}\right)^2 - \left(\frac{n\pi}{b}\right)^2 + \gamma_{mn}^2 = \kappa^2$$

where a and b are the effective lateral dimensions of the pile and κ is the reciprocal of the diffusion length.

Discussion of this solution can be found in Glasstone and Edlund (11) and many other Nuclear Engineering texts.

When considering a Multiplying medium, equation (A-1) becomes

$$\nabla^2 \phi + B^2 \phi = 0 \quad (\text{A-11})$$

By a completely analogous procedure, the solution to this equation is

$$\phi(x, y, z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} A_{mn} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \sinh \gamma_{mn} (c-z) \quad (\text{A-12})$$

where m and n are odd and the auxiliary separation constants equation becomes

$$+\alpha_m^2 + \beta_n^2 - \gamma_{mn}^2 = B^2 \quad (\text{A-13})$$

APPENDIX B

Solution to the Fermi Age Equation and
the Thermal Diffusion Equation

The geometry for this solution is shown in Fig. 20 .

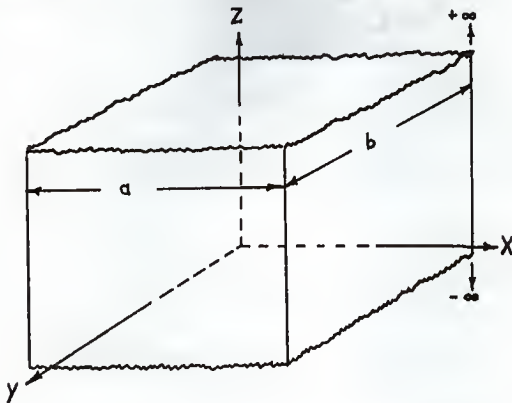


Fig. 20. Pile geometry for solution to the age-diffusion problem.

The equations involved were the Fermi age equation

$$\nabla^2 q = \frac{\partial q}{\partial \tau} \quad (\text{B-1})$$

and the thermal diffusion equation

$$D \nabla^2 \phi - \Sigma_a \phi + S = 0 \quad (\text{B-2})$$

The Fermi age equation was subjected to the boundary conditions that $q = 0$ at $x = \pm a/2$, $y = \pm b/2$, and $q \rightarrow 0$ as $|z| \rightarrow \infty$. The source condition was that all source neutrons entered the system at $x = y = z = 0$, at an age $\tau = 0$.

This condition was written into the Fermi age equation in the form

$$\nabla^2 q = \frac{\partial q}{\partial \tau} - Q_0 \delta(\tau) \delta(x) \delta(y) \delta(z). \quad (\text{B-3})$$

The boundary conditions to the thermal diffusion equation were that $\phi = 0$ at $x = \pm a/2$, $y = \pm b/2$, and $\phi \rightarrow 0$ as $|z| \rightarrow \infty$. The source condition was that $S = q(x, y, z, \tau_{th})$.

Q_0 , q and ϕ were expressed as double Fourier series satisfying the boundary conditions

$$\phi = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \phi_{mn}(z) \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \quad (\text{B-4})$$

$$q = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} q_{mn}(z) \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \quad (\text{B-5})$$

and

$$Q_0 \delta(\tau) \delta(x) \delta(y) \delta(z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} Q_{mn}(z) \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \quad (\text{B-6})$$

where m and n are summed over odd integers. Each side of Eq. B-6 was multiplied by orthogonal functions and then was integrated over the range of orthogonality which resulted in

$$Q_0 \delta(\tau) \delta(x) \delta(y) \delta(z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{4 Q_0}{ab} \delta(\tau) \delta(z) \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \quad (\text{B-7})$$

Substitution of Eqs. B-5 and B-7 into the age equation, Eq. B-3 gave

$$\sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \left[-\frac{\partial q_{mn}}{\partial \tau} + \frac{\partial^2 q_{mn}}{\partial z^2} - \left(\frac{m^2 \pi^2}{a^2} + \frac{n^2 \pi^2}{b^2} \right) q_{mn} + \frac{4 Q_0}{ab} \delta(\tau) \delta(z) \right] = 0 \quad (\text{B-8})$$

Taking the Fourier transform of the equation for a particular m and n and letting

$$\alpha_m = \frac{m\pi}{a} \quad (\text{B-9})$$

and

$$\beta_n = \frac{n\pi}{b} \quad (\text{B-10})$$

led to

$$-\frac{\partial \bar{q}}{\partial \tau} + (\alpha_m^2 + \beta_n^2 + \omega^2) \bar{q} = \frac{4 Q_0}{ab} \delta(\tau), \quad (\text{B-11})$$

where $\bar{q}(\omega)$ represents the Fourier transform of $q_{mn}(z)$.

The solution to this differential equation was

$$\bar{q}(\omega) = \frac{4 Q_0}{ab} e^{-(\alpha_m^2 + \beta_n^2 + \omega^2) \tau} \quad (\text{B-12})$$

Taking the inverse transform of Eq. B-12 and substituting it into Eq. B-5 gave the slowing down density along the z axis as

$$q(z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{4 Q_0 e^{-(\alpha_m^2 + \beta_n^2) \tau}}{ab \sqrt{4 \pi \tau}} e^{-z^2/4\tau}. \quad (\text{B-13})$$

Substitution of Eqs. B-4 and B-5 into the thermal diffusion equation. Equation A-2, and designating Σ_a/D as κ^2 gave

$$\sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \left[\frac{\partial^2 \phi_{mn}}{\partial z^2} - (\alpha_m^2 + \beta_n^2 + \kappa^2) \phi_{mn} + \frac{q_{mn}}{D} \right] = 0. \quad (\text{B-14})$$

Taking the Fourier transform of Eq. B-14 for a particular m and n and designating the Fourier transforms of ϕ_{mn} and q_{mn} by $\bar{\phi}(\omega)$ and $\bar{q}(\omega)$, respectively, gave

$$\bar{\phi}(\omega) = \frac{\bar{q}(\omega)}{D(\alpha_m^2 + \beta_n^2 + \omega^2)}. \quad (\text{B-15})$$

Taking the inverse transform of Eq. B-15 by means of the convolution theorem (30), after Eq. B-12 had been used to express $\bar{q}(\omega)$ gave

$$\phi_{mn} = \frac{2Q_0 e^{-(\alpha_m^2 + \beta_n^2)\tau}}{D_{ab} \gamma_{mn} \sqrt{4\pi\tau}} \int_{-\infty}^{\infty} e^{-z^2/4\tau} e^{-|z-z'|} \gamma_{mn} dz' \quad (\text{B-16})$$

where

$$\gamma_{mn} = \sqrt{\alpha_m^2 + \beta_n^2 + \kappa^2} \quad (\text{B-17})$$

Glasstone and Edlund (11), on pages 185 to 187, give the development showing how the integral in Eq. B-16 may be expressed in terms of the error function

$$\text{erf}(t) = \frac{2}{\sqrt{\pi}} \int_0^t e^{-u^2} du. \quad (\text{B-18})$$

Writing Eq. B-16 in terms of the error function and substituting it into Eq. B-4 gave the thermal flux along the z axis as

$$\phi(z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{Q_0}{D_{ab} \gamma_{mn}} e^{-\gamma_{mn} z} \left[e^{-\gamma_{mn} z} \left[1 + \operatorname{erf} \left(\frac{z}{2\sqrt{\tau}} - \gamma_{mn} \sqrt{\tau} \right) \right] + e^{\gamma_{mn} z} \left[1 - \operatorname{erf} \left(\frac{z}{2\sqrt{\tau}} + \gamma_{mn} \sqrt{\tau} \right) \right] \right] \quad (\text{B-19})$$

To describe the thermal flux due to an empirical r_i source which is defined by a set of Gaussian ranges, the quantity $\frac{r_i^2}{4}$ should be substituted into Eq. B-19 for the age τ . The flux must then be multiplied by the appropriate f_i and summed over the number of terms in the empirical source, which gave

$$\phi(z) = \sum_{i=1}^N \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{Q_0}{D_{ab} \gamma_{mn}} e^{-\frac{\kappa^2 r_i^2}{4}} \left[e^{-\gamma_{mn} z} \left[1 + \operatorname{erf} \left(\frac{z}{r_i} - \frac{\gamma_{mn} r_i}{2} \right) \right] + e^{\gamma_{mn} z} \left[1 - \operatorname{erf} \left(\frac{z}{r_i} + \frac{\gamma_{mn} r_i}{2} \right) \right] \right] \quad (\text{B-20})$$

The above derivation is identical to that presented by L. R. Foulke (9).

APPENDIX C

IBM 650 Program for Diffusion Length,
Point Thermal Source

This code was written to determine an experimental value of diffusion length based on the assumption of a point source of thermal neutrons. The program was written in SOAP II and floating point form. The object program and a logic diagram are given in this section.

The method of calculation was an iteration procedure based upon the equation

$$\phi(x, y, z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{2S}{abD} \cos \frac{m\pi x}{a} \cos \frac{n\pi y}{b} \frac{\sinh \gamma_{mn}(c-z)}{\cosh \gamma_{mn}C} .$$

Values of the correction factors C_E and C_H , were calculated using an initial estimate of γ_{11} , the data was corrected according to these factors, and a new value of γ_{11} was obtained by a least squares analysis of the corrected data. The new value of γ_{11} was then used to calculate a second set of correction factors. This procedure was repeated until the least squares value of γ_{11} obtained at the end of one trial was within a specified precision of the value obtained from the previous trial. At this point the last value of γ_{11} obtained was used to calculate the diffusion length according to

$$\frac{1}{L^2} = -\alpha_1^2 - \beta_1^2 + \gamma_{11}^2$$

where

$$\alpha_1 = \frac{\pi}{a}, \beta_1 = \frac{\pi}{b}$$

a and b being the extrapolated pile dimensions.

Input for this code consisted of the data and accompanying position co-ordinates as well as certain parameters listed in Table 20. Table 21 gives the form of the two types of output of this program.

Table 20. Input data for IBM 650 program for diffusion length based on a point thermal source.

Symbol :	Explanation	: Drum Storage : Location
FIRST	Initial value of γ_{11}	0100
POINT	No. of data points, in form 00 0000 00xx	0101
DATPT	No. of data points, in floating point form	0102
A	Extrapolated x-dimension	0103
B	Extrapolated y-dimension	0104
C	Extrapolated z-dimension	0105
X	x co-ordinate of data	0106
Y	y co-ordinate of data	0107
Z	z co-ordinate of data, to be stored consecutively starting at	0301
N	neutron count rates, to be stored consecutively starting at	0501

The input parameters and data listed in Table 19 should be punched on one-word load cards and fed into the machine with the object program. Point Stripping may be accomplished by listing the data, N and z, with the points to be dropped last and varying the parameters POINT and DATPT.

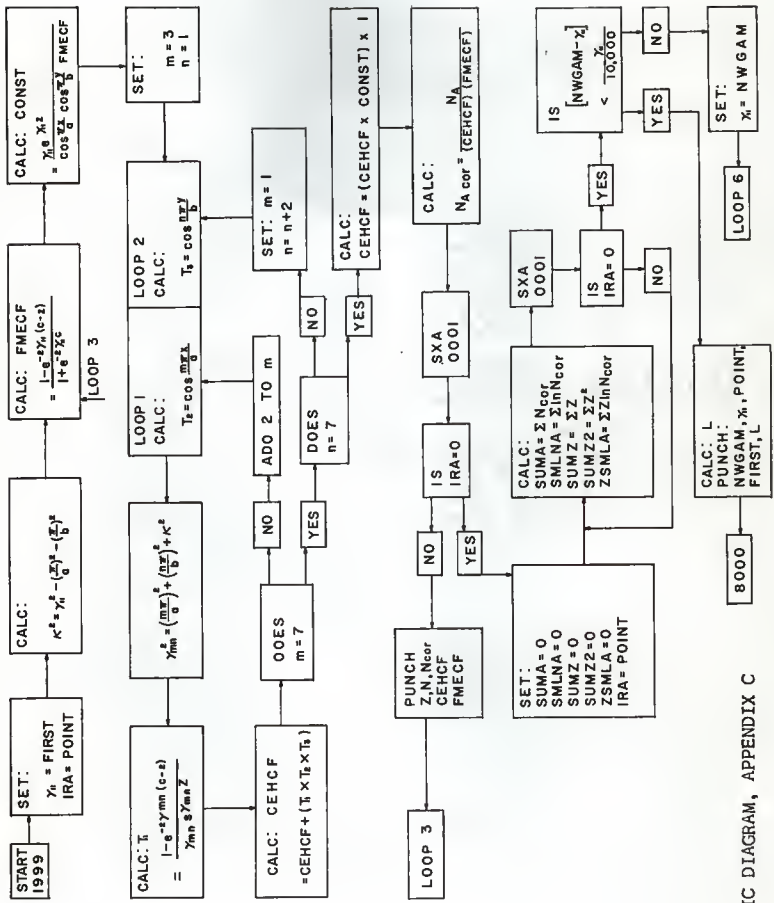
The form one output is punched after the calculation of each corrected data point. One card of this form will be obtained for each data point during a given trial. When the desired precision is reached, the final calculations are made and one card of form two is punched.

Table 21. Output forms for IBM 650 program for diffusion length based on a point thermal source.

Word No. 1	2	3	4	5
Form One:				
z co-ordinate	data	corrected data	Harmonic Correction	End Correction
Form Two:				
γ_{11} , Last value	γ_{11} Next to Last value	POINT	γ_{11} , Initial value	Diffusion Length

The operating time necessary to calculate the correction factor for one data point using four harmonics is approximately 45 seconds. The capacity of the program is 200 data points.

LOGIC DIAGRAM FOR IBM 650 PROGRAM FOR POINT THERMAL SOURCE METHOD



LOGIC DIAGRAM, APPENDIX C

OBJECT PROGRAM - APPENDIX C

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	BLH	1951	1958		1	0000	00	0000	0000	
	BLH	1977	1984		2	0000	00	0000	0000	
	WLM	0300	0900		3	0000	00	0000	0000	
	SYN	FIRST	0100		4	0000	00	0000	0000	
	SYN	POINT	0101	INDEX FORM	5	0000	00	0000	0000	
	SYN	QATPT	0102	DATA FORM	6	0000	00	0000	0000	
	SYN	A	0103	X OIMEN	7	0000	00	0000	0000	
	SYN	U	0104	Y OIMEN	8	0000	00	0000	0000	
	SYN	C	0105	Z OIMEN	9	0000	00	0000	0000	
	SYN	X	0106	DATA	10	0000	00	0000	0000	
	SYN	Y	0107	COORDINATE	11	0000	00	0000	0000	
	SYN	Z	0300		12	0000	00	0000	0000	
	SYN	N	0500		13	0000	00	0000	0000	
	SYN	NCOH	0700		14	0000	00	0000	0000	
	SYN	START	1999		15	0000	00	0000	0000	
ZERO	00	0000	0000		16	0000	00	0000	0000	
ONE	10	0000	0051		17	0050	10	0000	0051	
TWO	20	0000	0051		18	0150	00	0000	0051	
THREE	30	0000	0051		19	0200	00	0000	0051	
FOUR	40	0000	0051		20	0250	30	0000	0051	
FIVE	50	0000	0051		21	0300	31	4100	0051	
SIX	60	0000	0051		22	1000	70	0000	0051	
SEVEN	70	0000	0051		23	1050	25	3600	0051	
EIGHT	80	0000	0051		24	1100	10	0000	0055	
NINE	90	0000	0055		25	1150	24	0003	0006	
LNX01	STU	LNX08			26	0006	45	0010	0011	
	RHE	LNX14	LNX14		27	0010	46	0011	0014	
	STU	LNX09			28	0014	21	0018	0021	
	RSL	FPONE			29	0021	66	0024	0029	
	STU	LNX10			30	0029	24	0032	0033	
	STL	LNX02			31	0035	20	0039	0042	
	RAU	LNX09			32	0042	60	0018	0023	
	STL	LNX05			33	0043	20	0043	0043	
	STL	LNX11			34	0050	20	0085	0038	
	SLT	0008			35	0058	35	0008	0007	
	SUP	FIFTY			36	0057	11	0060	0058	
	NZE		LNX04		37	0015	45	0068	0019	
	BH1		LNX03		38	0068	46	0071	0022	
	R80	0003			39	0071	61	0003	0079	
	LOD	FPONE			40	0079	69	0024	0077	
	STU	LNX02	LNX03		41	0077	24	0039	0022	
	SCY	0008			42	0022	30	0008	0041	
	SCT	0000			43	0041	36	0000	0013	
	ADP	FIFTY			44	0013	10	0016	0121	
	SOP	H002			45	0121	11	0021	0121	
	RAU	H003			46	0129	60	0003	0037	
	FMP	LNX02			47	0037	39	0039	0039	
	FMP	LNTEN			48	0039	30	0032	0143	
	STU	LNX05	LNX04		49	0142	21	0027	0019	
	RAL	LNX09			50	0019	65	0018	0073	
	SRT	0002			51	0073	30	0002	0179	
	RAU	H004			52	0179	60	0002	0087	
	ALO	FIFTY			53	0087	15	0060	0065	
	SLT	0002			54	0065	35	0026	0177	
	FAD	FPONE			55	0171	32	0024	0001	
	STU	LNX09			56	0001	21	0018	0221	
	F88	FTWO			57	0221	33	0074	0051	
	F8V	LNX09			58	0051	34	0018	0118	
	STU	LNX13			59	0118	21	0072	0025	
	STU	LNX16			60	0025	84	0028	0031	
	STU	LNX11			61	0031	24	0085	0088	
	FMP	R001			62	0088	39	0001	0091	
	STU	FACTR	LNX06		63	0091	81	0046	0049	
	RAU	LNX10			64	0049	60	0032	0137	
	FAO	FTWO			65	0137	32	0004	0151	
	STU	LNX10			66	0151	21	0032	0137	
	RAU	LNX13			67	0135	60	0072	0127	
	FMP	FACTR			68	0127	39	0046	0096	
	F8V	LNX10			69	0096	34	0026	0081	
	STU	LNX13			70	0082	21	0072	0075	
	FAO	LNX12			71	0075	32	0028	0005	
	STU	LNX14			72	0005	32	0005	0028	
	F8H	LNX11			73	0081	33	0085	0061	
	F0V	LNX11			74	0061	34	0085	0185	
	RAU	R003			75	0185	67	0005	0053	
	RAU	H002			76	0043	60	0002	0201	
	F88	SIZE7			77	0201	33	0004	0131	
	F8H	LNX07			78	0131	46	0034	0086	
	LOD	LNX12			79	0235	69	0028	0181	
	STU	LNX11			80	0181	24	0085	0138	
	RAU	LNX13			81	0138	60	0078	0177	
	FMP	LNX10			82	0177	39	0032	0132	
	STU	LNX13	LNX06		83	0152	21	0072	0049	
	RAU	LNX16			84	0034	60	0028	0033	
	FMP	FTWO			85	0033	39	0074	0124	
	F8H	LNX05	LNX08		86	0124	53	0027	0003	
	FPONE	0000			87	0004	10	0000	0051	
	FPTWO	20	0000		88	0074	20	0000	0051	
	SIZE7	10	0000		89	0004	10	0000	0043	
	LNTEN	23	0000		90	0023	31	0239	0151	
	FIFTY	50	0000		91	0060	50	0000	0000	
	SIXTY	00	0000		92	0016	00	0000	0000	
	LNX14	01	2345		93	0001	01	2345	0789	
	E00A0	STU	SEXT		1	94	1200	24	0053	0056
		BH	SERR		2	95	0056	46	0056	0056
		NZE		BEXT	3	96	0110	45	0064	0053
		STU	8A		4	97	0084	21	0168	0271
		FAO	8SD		5	98	0271	0252	0455	0151
		FMP	8HAF	8B	6	99	0851	39	0004	0154
		STU	8SAV	8AH	7	100	0154	21	0008	0111
8B		RAU	8A	8	101	0111	60	0111	0000	0000
8AB		FDV	8SAV	8	102	0123	34	0008	0058	
		FAO	88AF		10	103	0058	39	0008	0285
		FMP	88AF		11	104	0285	39	0054	0204

	FSH	SSAV		12	1U5	0204	33	0008	U935
	NZU		BR	13	1U6	0935	44	0139	0040
	HMI			14	1U7	0139	0139	0070	0040
	FAU	SSAV		15	1U8	0192	32	0008	4985
	STU	SSAV	SAH	16	1U9	0985	21	0008	4111
BR	RAI	SSAV	SEXT	17	11T	0040	60	0040	4053
SERR	HLT	0000	SEXT	18	11J	0009	01	0000	4053
BHAF	SU	0000	0050	19	11J	0034	50	0000	4050
S10	0000	0051	0000	20	11J	0074	50	0000	4051
EUDEA	STU	AAA1		114	1450		24	0101	0114
	STL	AAA2		115	0156		20	0161	0114
	RAU	AAA2		116	0144		39	0069	4076
	STL	AAA3		117	0115		60	0069	4122
	RAU	AAA3		118	0122		60	0069	4173
	FMP	AAA3		119	0173		39	0069	4173
	FAU	AAA15		120	0076		32	0229	4055
	FMP	AAA3		121	0055		39	0069	4119
	FAU	AAA14		122	0119		32	0172	4099
	FMP	AAA3		123	0099		39	0069	4169
	FAU	AAA13		124	0169		32	0288	4149
	RAU	AAA3		125	0269		32	0288	4249
	FAD	AAA12		126	0219		32	0272	4199
	FMP	AAA3		127	0199		39	0069	4269
	FAU	AAA11		128	0269		32	0288	4249
	FMP	AAA3		129	0249		39	0069	4919
	FAU	AAA10		130	0919		32	0972	4299
	STU	AAA4		131	0599		21	0284	4057
	FMP	AAA4		132	0057		39	0254	4904
	STU	AAA4		133	0904		21	0284	4157
	FMP	AAA4		134	0157		39	0254	4914
	STU	AAA4		135	0954		21	0284	4207
	RAU	AAA2		136	0207		60	0161	4165
	HMI	AAA5	AAAA	137	0165		46	0218	4969
	RAU	AAA10		138	0218		60	0972	4227
AAA5	FDV	AAA4		139	0227		34	0284	4104
	STU	AAA4		140	1004		21	0284	4914
	RAL	AAA4	AAAA	141	0969		65	0284	4153
AAA6	IU	0000	0051	142	0972		10	0000	4051
AAA10	24	0998	0850	143	0922		24	0922	4922
AAA11	31	2575	0349	144	0272		31	2575	0349
AAA12	25	9137	1248	145	0222		25	9137	1248
AAA13	25	9137	1248	146	0172		17	0172	1248
AAA14	54	3020	0045	147	0229		54	3020	4045
AAA15	69	0600	0044	148	0026		69	0600	4044
EDOCH	STU	0002		149	1300		24	1300	4044
	RAU	0002		150	0206		60	8002	0215
	HMI	NEGAT	HEBUC	151	0215		46	0268	1019
	FAU	NEGAT		152	0268		46	0268	1019
NEGAT	FMI	NEGAT		153	0047		46	0268	4901
	FSR	UNEPI	COBUU	154	0901		33	1034	4923
	FTU	TWOP		155	0119		33	1034	4923
RFBUC	HMI		REUCU	156	0097		46	1350	1019
	FAD	UNEPI		157	1350		32	1034	4923
	RAU	NEGAT		158	0311		31	0284	4923
COBUU	RBV	FPONE		159	0189		61	0084	4279
	STU	TERMM		160	0479		21	0084	4979
	STU	FUNKT		161	0187		21	0242	4045
	STL	ENNN	NEGST	162	0445		20	0949	4002
EUOSH	STU	FXIT		163	1400		24	0203	4256
	RAU	0002	REOUU	164	0256		60	8002	4265
	HMI	NEGAT		165	0263		46	0918	4099
NEGAV	FAU	TWOP		166	0918		32	0921	4147
	HMI	NEGAT		167	0147		46	0918	4951
	FSR	UNEPI	SINET	168	0951		33	1034	4281
REOUU	FSR	TWOP		169	1069		33	0921	4197
	HMI		HEUHU	170	0197		46	1450	1069
	FAU	UNEPI	SINET	171	1450		32	0354	4281
SINET	STU	TRETA		172	0281		21	0036	4239
	RBV	0003		173	0239		61	8003	4247
	STU	TERMM		174	0247		21	0242	4095
	STU	FUNKT		175	0337		21	0242	4095
	LOU	FPONE		176	0935		69	0242	4095
	STU	ENNN	NEGST	177	0277		24	0949	4008
NEGST	RAU	ENNN		178	0003		60	0949	4253
	FAD	FPONE		179	0283		32	0949	4253
	STU	FPONE		180	1001		21	0906	4059
	FAD	FPONE		181	0059		32	0024	1051
	STU	ENNN		182	1051		21	0949	4059
	RBV	TERMM		183	0052		61	0084	4229
	FMP	TRETA		184	0489		39	0036	4086
	FMP	TRETA		185	0266		39	0036	4136
	FOV	FPONE		186	0166		34	0906	4086
	FUV	ENNN		187	0956		14	0949	4999
	STU	TERMM		188	0999		21	0084	4287
	STU	FUNKT		189	0287		21	0242	4095
	OTL	FNAC		190	0297		20	1101	1104
	RAU	TERMM		191	1104		67	0044	4939
	RAU	0002		192	0239		60	0008	4997
	FOV	FNAC		193	0947		34	1101	1151
	RAU	TERMM		194	1151		31	1151	4939
	HMI	ENUFF		195	0931		46	0134	4035
	RAU	FUNKT		196	1035		60	0242	4997
	FAD	TERMM		197	0977		32	0949	4253
	STU	FUNKT	NEGST	198	0211		21	0242	4002
ENUFF	RAL	FUNKT	EXIT	199	0134		65	0242	4203
S1ZEB	62	0043		200	1544		10	1544	4002
TWOP	62	0318	5351	201	0921		62	0318	5351
ONEPI	31	4159	8751	202	1054		31	4159	2751
FPUNE	62	0000	0051	203	0044		10	0044	4002
START	LOD	FIRST		204	1999		69	0100	4903
	STO	GAM11	LOOPb	205	0903		24	1006	4109
	LOD	FIRST		206	0109		69	0100	4903
LOOPb	RAA	0001		207	1204		60	8001	4160

LUU ZERO		208	0160	69	0000	U953
STU ALPHA		209	0953	24	1056	U159
STD BETA		210	0158	24	0018	U955
RAU GAM11		211	0915	60	1006	U261
FMP GAM11		212	0261	39	1006	1106
STU GAM80		213	1106	21	0106	U063
STU TEMP1		214	0063	21	0960	U711
RAU PI		215	0971	60	0950	U155
FUV A		216	0135	34	0108	1003
STU TEMP2		217	1003	34	0108	U711
FMP TEMP2		218	0911	39	0108	U158
STU TEMP2		219	0158	21	0108	U961
RAU PI		220	0964	60	0950	U205
FUV H		221	0205	34	0104	1254
STU TEMP3		222	1254	21	0208	1011
FMP TEMP3		223	1011	39	0208	U258
STU TEMP3		224	0258	21	0208	1061
RAU TEMP1		225	1061	60	0968	U223
F88 TEMP2		226	0223	33	0108	1085
F88 TEMP3		227	1085	33	0208	1135
STU KWPS0		228	1135	21	0090	0093
LDD ZERO		229	0093	69	0000	U953
STU CEMCF		230	1053	24	1156	U209
RAU C		231	0209	60	0105	U259
FBR Z		232	0259	33	0300	U927
FMP GAM11		233	0927	39	1006	1206
FMP MTR0		234	1206	39	0200	U050
RAL 8003		235	1300	65	0003	0257
LUU		236	0257	69	0260	1250
STL TEMP1		237	0260	80	0968	1021
RAU OR		238	1021	60	0950	U255
FBR TEMP1		239	0255	33	0968	0145
STU TEMP1		240	0145	21	0968	1071
RAU C		241	1071	09	0108	0909
FMP GAM11		242	0909	39	1006	1256
FMP MTR0		243	1256	39	0200	1550
RAL 8003		244	1550	69	0108	0907
LDD		245	0907	69	0910	1250
STL TEMP2		246	0910	80	0108	1111
RAU OR		247	1111	80	0108	1185
FBR TEMP2		248	0905	33	0108	1185
STU TEMP2		249	1185	21	0108	1161
RAU TEMP1		250	1161	02	0108	0233
FUV TEMP2		251	0233	34	0108	U908
STU FMECF		252	0908	21	0062	U965
RAU PI		253	0965	90	0965	0965
FMP X		254	0955	39	0106	1306
FUV A		255	1306	34	0103	1103
RAL 8003		256	1103	69	0108	1251
LDD		257	1211	69	0164	1300
STL TEMP1		258	0164	20	0968	1121
RAU PI		259	1121	60	1150	1005
FUV B		260	1005	34	0104	1304
FMP Y		261	1304	39	0107	U957
RAL 8003		262	0957	65	0903	1016
LDD		263	1016	69	1018	1300
STL TEMP2		264	1018	20	0108	1261
RAU GAM11		265	1261	60	1006	1311
FMP Z		266	1311	39	2300	1600
RAL 8003		267	1600	65	8003	1007
LUU		268	1007	69	0960	0350
RAU H002		269	0960	60	8002	1119
FMP GAM11		270	1119	39	1006	1356
FUV TEMP1		271	1356	34	0968	1068
FUV TEMP2		272	1068	34	0108	U958
FUV FMECF		273	0958	34	0062	U122
STU CONST		274	0112	21	0066	1169
LDD THREE		275	1169	69	0250	1153
STO M		276	1153	24	1406	U959
LDD ONE		277	0959	69	0250	1233
STO N		278	1203	24	0500	1253
RAU N		279	1253	60	0500	1055
FMP PI		280	1055	39	1055	1600
FMP Y		281	1600	39	0107	1057
FUV B		282	1057	34	0104	1354
RAL 8003		283	1354	69	0108	1561
LDD		284	1361	69	0214	1300
STL TEMP3		285	0214	20	0200	1411
RAU TEMP1		286	1411	60	1406	1461
FMP PI		287	1461	39	0950	1700
FMP X		288	1700	39	0106	1456
FUV A		289	1456	34	0108	1303
RAL 8003		290	1303	69	0003	1111
LDD		291	1511	69	0264	1300
STL TEMP2		292	0264	20	0108	1561
RAU M		293	1561	80	0108	1611
FMP PI		294	1611	39	0950	1750
FUV A		295	1750	34	0103	1353
STU TEMP4		296	1353	21	1008	1661
FMP TEMP2		297	1661	39	1008	1058
STU ALPH2		298	1058	21	0108	1056
RAU N		299	1065	60	0500	1105
FMP PI		300	1105	39	0950	1800
FUV B		301	1800	34	0104	1700
STU TEMP4		302	1404	21	1008	1711
FMP TEMP4		303	1711	39	1008	1108
STU FTI2		304	1108	21	0212	1154
FAD ALPH2		305	1115	32	0162	U989
FAD KAPPO		306	0949	32	0090	U017
LDD		307	0017	29	0200	1200
STU GAMHA		308	0020	21	0224	U977
RAU C		309	0977	60	0105	1005
FBR Z		310	1009	33	2300	1027

FMP GAMMA		311	1027	39	0224	4274
FMP MTHO		312	1027	39	0270	1850
RAL 8003		313	1050	65	8003	1107
LDD		314	1107	69	1010	1250
STL TEMP5	EODEA	315	1010	20	1165	1218
RAU C		316	1118	60	0105	1059
FMP GAMMA		317	1059	39	0224	0924
FMP MTHO		318	0924	39	0224	1900
RAL 8003		319	1900	65	8003	1157
LDD		320	1157	69	1060	1250
STL TEMP7	EODEA	321	1060	20	0115	1168
RAU OME		322	1168	60	0105	1155
FBR TEMP7		323	1155	35	1215	0141
STO TEMP7		324	0141	18	215	1218
RAU GAMMA		325	1218	60	0214	0929
FMP Z	A	326	0929	39	2300	1950
RAL 8003		327	1950	65	8003	1207
LDD		328	1207	69	1110	2550
STL TEMP6	EODEA	329	1110	20	1265	1268
RAU ONE		330	1268	60	0050	1205
FBR TEMP5		331	1205	33	1165	0191
FDV TEMP6		332	0191	34	1265	1315
FVJ TEMP7		333	1315	34	1215	1365
FDV GAMMA		334	1365	34	0224	0974
FHP TEMP3		335	0974	39	0208	1158
FMP TEMP2		336	1158	39	1108	1208
FAD CENCF		337	1208	34	1126	0483
STO CENCF		338	0483	21	1156	1109
RAU SEVEN		339	1109	60	1050	1255
FBR H		340	1255	34	1406	0133
NZ CONT1	CUNT4	341	0133	45	0186	0937
RAU M		342	0186	60	1406	1761
FAU TNO		343	1761	32	0150	1077
STU		344	1077	41	1406	1411
RAU N		345	0937	60	0500	1303
FBR SEVEN		346	1303	33	1905	1149
NZ CONT2	CUNT4	347	1127	45	0080	0981
LDD ONE		348	0080	69	0050	1403
STO M		349	1403	34	1403	1403
RAU N		350	1159	60	0500	1355
FAU TNO		351	1355	32	0150	1177
STU		352	1177	21	1177	1353
STO CENCF		353	0981	60	1156	1811
FMP CONST		354	1811	39	0066	0116
FAD ONE		355	0116	38	0116	1209
STU CFHCF		356	1209	21	1156	1209
RAU N	A	357	1209	60	2500	1405
FVJ CFHCF		358	1405	34	1405	358
FDV FNECF		359	1306	34	0022	0262
STH NCOR	A	360	0262	21	2700	1453
LDD Z	A	361	1453	69	1310	1533
STU 1977	A	362	1503	24	1977	0130
LDD N	A	363	0130	69	2500	1553
STU 1976	A	364	1553	24	1978	1031
LDD NCOR	A	365	1031	69	2700	1603
STO 1979	A	366	1603	24	1979	0182
LDD CFHCF		367	0182	69	1156	1259
STU 1980		368	1259	24	1980	0183
LDD FNECF		369	0183	69	0062	1415
STO 1981		370	1415	24	1981	0184
MCH 1977		371	0184	71	0977	1377
SXA 0001		372	1277	11	0001	0233
NZA LDDP3		373	0233	40	0093	0989
LDD POINT		374	0989	39	0101	1454
RAA 8005		375	1454	80	8001	1160
LDD ZERU		376	1160	69	0000	1653
STU 80MA		377	1653	24	1536	1309
STU 8MLNA		378	1309	24	0912	1465
STU 80MZ		379	1465	24	1314	1171
STU 8UMZ2		380	1171	24	0180	0283
STU Z8MLA		381	1387	24	0180	0283
LDD OATPT		382	0283	69	0102	1455
STU P		383	1455	34	1458	1359
RAU NCOR	A	384	1861	60	2700	1505
FAO 80MA		385	1505	32	1536	0959
STU 80MA		386	0959	32	0912	1515
RAU NCOR	A	387	1359	60	2700	1555
LDD		388	1555	69	1308	1139
FAO 8MLNA	A	389	1139	21	0912	1515
STU 8MLNA		390	1039	21	0912	1515
RAU Z	A	391	1515	60	2300	1605
STU 80MZ		392	1605	32	1318	0195
RAU Z	A	393	0195	21	1318	1221
FMP Z	A	394	1221	60	2300	1605
FAO 80MZ2		395	1605	39	0000	1201
STU 8UMZ2		396	1201	32	1024	1251
RAU NCOR	A	397	1251	21	1024	1377
LDD		398	1377	60	2700	1705
RAU NCOR	A	399	1705	69	1358	1150
FMP Z	A	400	1150	39	2300	1351
FAO Z8MLA		401	1351	32	0180	1257
STU Z8MLA		402	1257	21	0180	0983
SXA 0001		403	0983	31	0001	1089
NZA LDDP5		404	1089	40	1861	0143
RAO 8MLNA		405	0143	60	0912	0067
FMP 80MZ		406	0067	39	1358	1271
STU TEMP1		407	1271	21	1358	1368
RAU P		408	1271	60	1258	0113
FMP Z8MLA		409	0113	21	0108	0113
STO TEMP2		410	0113	21	0108	1911
RAU P		411	1911	60	1258	0163
FMP 8UMZ2		412	0163	39	1024	1074

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END
CORRECTION

STU TEMP3	413	1074	21	0208	1961
RAU SUMZ	414	1961	60	1318	0923
FMP SUMZ	415	0923	39	1318	1418
STU TEMP4	416	1418	21	1008	0968
RAU TEMP3	417	0968	60	0208	0213
FBS TEMP4	418	0213	33	1008	1633
STU TEMP3	419	1635	21	0208	1012
RAU TEMP1	420	1018	60	0968	0973
FBS TEMP3	421	0973	33	0108	1285
FOV TEMP3	422	1285	14	0208	1408
STU NWGAM	423	1408	21	1062	1565
FOV IOUO0	424	1565	34	1100	1351
STU PREC	425	1351	21	1606	1409
RAU GAM11	426	1409	60	1006	1112
FBS NWGAM	427	1112	33	1062	1139
FAM B003	428	1139	67	8003	1047
RAU B002	429	1047	60	8002	1755
FBS REG	430	1755	33	1606	1033
SHI COMTB	431	1033	46	0236	1037
RAU NWGAM	432	1037	60	1062	0117
STU GAM11	433	0117	21	1086	0109
RAU PI	434	0236	60	0950	1605
FOV A	435	1805	34	0103	1703
STU ALPH2	436	1703	21	0162	1615
FMP ALPH2	437	1615	39	0162	1162
STU ALPH2	438	1162	21	0162	1665
RAU PI	439	1665	60	0950	1855
FOV B	440	1855	34	0104	1504
STU BETA2	441	1504	21	0212	1715
FMP BETA2	442	1715	39	0212	1232
STU BETA2	443	1232	21	0212	1765
RAU NWGAM	444	1765	60	1062	0167
FMP NWGAM	445	0167	39	1062	1262
FBS BETA2	446	1262	33	0212	1189
FBB ALPH2	447	1189	33	0162	1239
LQU	448	1239	69	0292	1200
STU TEMP1	449	0292	21	0968	1321
RAU UNE	450	1321	60	0050	1905
FOV TEMP1	451	1905	34	0968	1468
FMP CONVT	452	1468	39	1050	1401
STU DL	453	1401	21	1656	1459
LDD NWGAM	454	1459	69	1062	1815
STD 1977	455	1815	24	1977	0280
LDD GAM11	456	0280	69	1006	1509
STD 1978	457	1509	24	1978	1081
LDD POLWT	458	1081	69	0101	1554
STD 1979	459	1554	24	1979	0232
LDD FIRRT	460	0232	69	0100	1753
STD 1980	461	1753	24	1980	0083
LDD DL	462	1083	69	1656	1559
STD 1981	463	1559	24	1981	0234
PCH 1977	464	0234	71	1977	8000

CONT9

LOOPS-----

E00A0

B000

GONT9

CONTR

APPENDIX D

IBM 650 Program for Diffusion Length
Constant Thermal Source

The purpose of this program was to determine an experimental value of the diffusion length based on the assumption of a constant source of thermal neutrons. The program was written in SOAP II and floating point form. The object program and a logic diagram are given in this section.

The calculations in this program are based on the equation

$$\phi(x, y, z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{16 \phi_0 (-1)^{\frac{m+n+2}{2}}}{m n \pi^2 \sinh \gamma_{mn} c} \cos \frac{m \pi x}{a} \cos \frac{n \pi y}{b} \sinh \gamma_{mn} (c-z)$$

The same iterative procedure is used in this program as was used in the point thermal source program described in Appendix C.

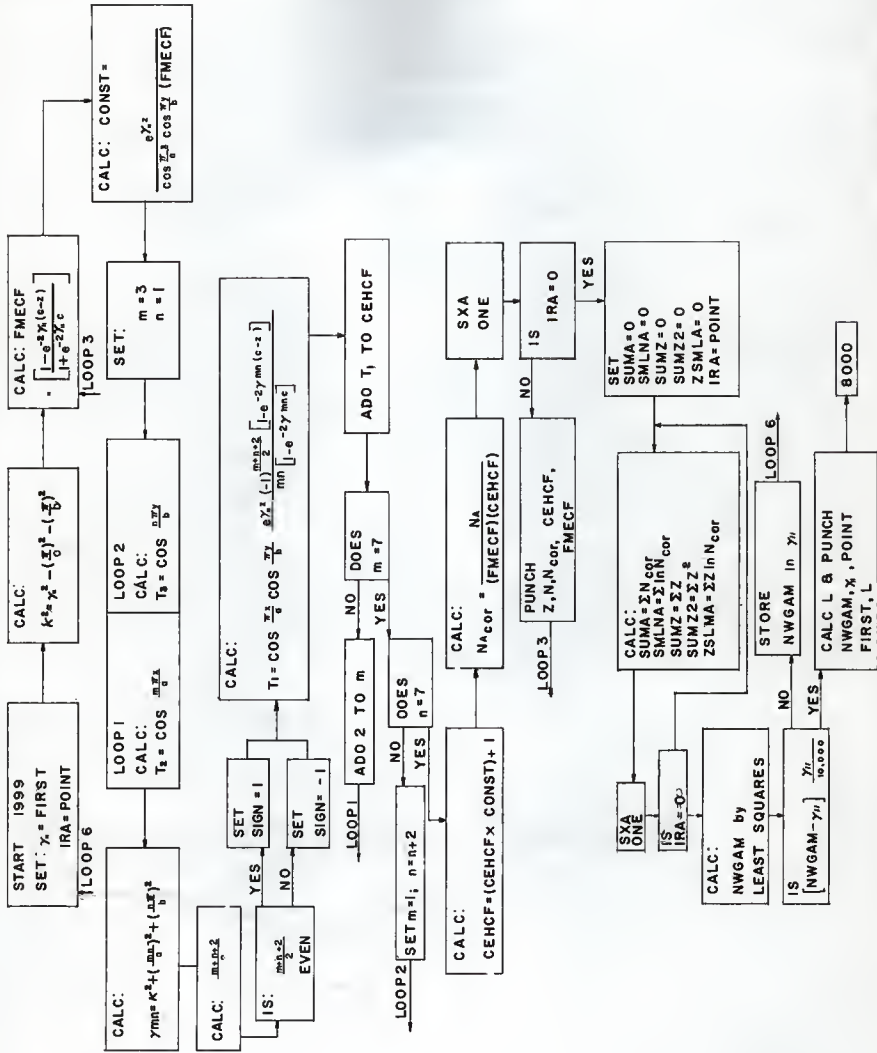
Input parameters and data are identical to those used in the point thermal source program and are listed in Table 20. Output is similar, and is described in Table 22.

Table 22. Output forms for IBM 650 program for diffusion length based on a constant thermal source.

Word No. 1	2	3	4	5
Form One:				
z co-ordinate	data	corrected data	Harmonic Correction	End Correction
Form Two:				
γ_{11} , Last value	γ_{11} Next to Last value	γ_{11} Initial value	POINT	Diffusion Length

The output sequence is identical to that for the point thermal source program. The operating time necessary to calculate the correction factor for one data point using four harmonics is about 45 seconds. The capacity of the program is 200 data points.

LOGIC DIAGRAM FOR IBM650 PROGRAM FOR CONSTANT THERMAL SOURCE METHOD



OBJECT PROGRAM - APPENDIX D

111

	SLR	0300	0900		1	0000	00	0000	0000
	BLR	1950	1999		2	0000	00	0000	0000
	SVN	Z	0300		3	0000	00	0000	0000
	SVN	N	0500		4	0000	00	0000	0000
	SVN	FIRST	0100		5	0000	00	0000	0000
	SVN	POINT	0101	INDEX FORM	6	0000	00	0000	0000
	SVN	ORPT	0102	DATA FORM	7	0000	00	0000	0000
	SVN	A	0103	X DIMEN	8	0000	00	0000	0000
	SVN	E	0104	Y DIMEN	9	0000	00	0000	0000
	SVN	C	0105	Z DIMEN	10	0000	00	0000	0000
	SVN	X	0106	DATA	11	0000	00	0000	0000
	SVN	Y	0107	COORDINATE	12	0000	00	0000	0000
	SVN	NCOR	0700		13	0000	00	0000	0000
	SVN	START	1999		14	0000	00	0000	0000
1	SINE	AND	COS	RAJ	25	0000	00	0000	0000
ZERO					26	0000	00	0000	0000
MTWO		20	0000	0051	16	0050	20	0000	0051
PI		31	4160	0051	17	0150	31	4160	0051
ONE		10	0000	0051	18	0200	10	0000	0051
TWO		20	0000	0051	19	0250	20	0000	0051
THREE		30	0000	0051	20	0300	30	0000	0051
SEVEN		70	0000	0051	21	0000	70	0000	0051
10000		10	0000	0055	22	1050	10	0000	0055
PRECN		10	0000	0047	23	1100	10	0000	0047
CONVT		25	1600	0051	24	1150	25	1600	0051
EO09D		STO	813		26	1200	24	0003	0006
		RAU	B002		27	0006	60	0002	0015
		FMP	87	B14	28	0015	39	0016	0008
EO05R		STO	813		29	1250	24	0003	0056
		RAU	B002	B14	30	0056	60	0002	0060
EO00D		STO	813		31	1300	60	0002	0116
		RAU	B002		32	0156	60	0002	0065
EO0CR		FMP	87	B15	33	0065	39	0016	0118
		STO	813		34	1350	60	0002	0066
B14		RAU	B002	B15	35	0206	60	0002	0118
		LDO	89		36	0068	69	0021	0074
		STO	817		37	0094	27	0024	0074
B15		STU	811	B16	38	0030	21	0034	0037
		LDO	810		39	0118	69	0071	0074
		STO	817		40	0074	27	0024	0074
		LDO	81		41	0080	69	0033	0036
B16		STO	812	B16	42	0036	24	0039	0037
		STU	85		43	0037	21	0042	0037
R21		F8B	2P1		44	1400	33	0053	0029
		RAI	B20	B21	45	0029	46	0032	1400
B20		F8B	2P1		46	0032	36	0033	0029
		STU	85		47	0079	21	0042	0045
		LDO	88		48	0095	69	0048	0001
		STO	83		49	0001	39	0042	0092
		FMP	85		50	0007	39	0042	0092
		F0V	83		51	0092	34	0004	0054
B18		STU	84	B18	52	0004	21	0004	0054
		RSU	84		53	0011	61	0000	0013
		STU	84		54	0013	21	0000	0061
		F8U	812		55	0061	33	0039	0115
		STU	812		56	0115	21	0039	0142
		RAU	83		57	0142	60	0004	0009
		F8O	81		58	0009	38	0033	0059
		STU	83		59	0059	21	0004	0057
		RAU	85		60	0057	60	0042	0047
		F0V	83		61	0047	34	0004	0154
		FMP	84		62	0154	39	0008	0058
		BTU	84		63	0058	21	0008	0111
		F8O	811		64	0111	36	0013	0161
		STU	811		65	0161	21	0034	0087
		RAU	83		66	0087	60	0004	0109
		F8O	810		67	0109	39	0033	0159
		STU	83		68	0159	21	0004	0157
		RAU	85		69	0157	60	0042	0097
		F0V	83		70	0097	70	0097	0044
		FMP	84		71	0204	39	0008	0108
		STU	84		72	0108	21	0008	0211
		RAM	84		73	0211	67	0008	0053
		RAU	B002		74	0063	60	0002	0121
		F8O	86		75	0121	32	0124	0051
		RAI	817	B18	76	0051	46	0000	0051
B2		10	0000	0000	77	1450	10	0000	0000
B6		10	0000	0040	78	0124	10	0000	0040
B7		20	0000	2349	79	0040	21	0032	0159
B8		20	0000	0051	80	0048	20	0000	0051
B9		RAL	811	813	81	0021	65	0034	0003
B10		RAI	812	813	82	0048	65	0039	0033
B1		10	0000	0051	83	0033	10	0000	0051
2P1		62	8318	5551	84	0053	62	8318	5551
CO0AU		10	SEIT		1	85	15	000	286
		8W1	SERR		2	86	46	0209	0010
		NZE		SEXT	3	87	45	0014	0153
		ST	SA		4	88	21	0164	0171
		F8O	S10		5	89	38	0174	0151
		FMP	SHAFF	B8	6	90	39	0254	0904
SS		ST	SAV	SAB	7	91	29	0208	0044
SAB		RAU	SA		8	92	39	0254	0023
		F0V	8SAV		9	93	34	0158	0208
		F8O	8SAV		10	94	32	0158	0335
		FMP	SHAFF		11	95	39	0254	0954
		F8B	8SAV		12	96	33	0158	0085
		STU	8	SR	13	97	46	0085	0740
		8W1		SR	14	98	46	0192	0040
		F8O	8SAV	SAB	15	99	32	0158	0135
		ST	SAV	SAB	16	100	21	0158	0041
SR		RAU	SSAV	SEXT	17	101	60	0158	0040
SER		HLT	0000	SEXT	18	102	0209	01	0000
SHAFF		50	0000	0050	19	103	0254	50	0000

'10	10	0000	0051	20	104	0174	10	0000	0051
DOCR	STO	EXIT			105	1350	24	0203	0906
	RAU	8002			106	0906	60	0000	0165
	SMI	NEGAT	REOUO		107	0165	46	0218	0019
NEGAT	FBI	NEGAT			108	0218	32	0221	0147
	SMI	NEGAT			109	0147	46	0147	0001
	F88	ONEPI	COBIO		110	0201	33	1004	0051
EOUC	FBI	TWOPI			111	0019	33	0221	0197
	SMI		REOUO		112	0197	46	1502	0629
	FAD	ONEPI	COBIO		113	1550	32	1004	0031
'0810	STU	THETA			114	0031	21	0086	0139
	RSU	FPONE			115	0139	21	0243	0157
	STU	TERM			116	0247	21	0008	0005
	STU	FUNKT			117	0005	21	0060	0113
'00BR	STL	EXIT	NEOST		118	0113	20	0017	0070
	RAU	EXIT			119	1250	24	0203	0956
	RAU	8002			120	0956	60	8002	0215
	SMI	NEGAV	REOUO		121	0215	46	0243	0069
NEGAV	FAD	TWOPI			122	0268	32	0221	0297
	SMI	NEGAV			123	0297	46	0268	0251
	F88	ONEPI	SINET		124	0251	33	1004	0081
IEOUO	F88	TWOPI			125	0069	33	0221	0947
	SMI		REOUO		126	0947	46	1600	0069
	FAD	ONEPI	SINET		127	0069	32	1004	0081
'1INET	STU	THETA			128	0081	21	0086	0189
	RSU	8003			129	0189	61	8003	0997
	STU	TERM			130	0997	81	0002	0055
	STU	FUNKT			131	0055	81	0060	0163
	LOO	FPONE			132	0163	69	0242	0145
NEGST	STU	ENM	NEOST		133	0145	24	0007	0120
	RAU	ENM			134	0020	60	0017	0271
	FAD	FPONE			135	0271	32	0242	0119
	STU	FPONE			136	0119	81	0222	0070
	FAD	FPONE			137	0077	32	0242	0169
	STU	ENM			138	0169	21	0017	0070
	RSU	TERM			139	0070	61	0002	0057
	FMP	THETA			140	0207	39	0086	0136
	FMP	THETA			141	0136	39	0086	0186
	FOV	HPONE			142	0186	34	0242	0169
	FOV	ENM			143	0274	34	0017	0067
	STU	TERM			144	0067	21	0002	0155
	RAM	FUNKT			145	0155	67	0002	0155
	STL	FMAG			146	0265	20	0219	0022
	RAM	TERM			147	0022	67	0002	0257
	RAU	8002			148	0257	60	0007	0147
	FOV	FMAG			149	0915	34	0219	0269
	F88	SIZES			150	0269	33	0002	0049
	SMI	ENUFF			151	0049	46	0016	0049
	RAU	FUNKT			152	0253	50	0002	0062
	FAD	TERM			153	0965	32	0002	0129
	STU	FUNKT	NEGST		154	0129	21	0002	0129
	RAL	FUNKT	EXIT		155	0052	65	0060	0003
ENUFF	STO	0000	0043		156	0072	10	0000	0043
SIZES	TWOPI	0118	5351		157	0227	62	8318	5311
ONEPI	STU	4159	2751		158	1004	60	4159	2751
FPONE	STO	0000	0051		159	0242	10	0000	0051
LNK01	STU	LNK08			160	1650	24	0903	1006
	NZE		LNK14		161	1006	45	0110	0911
	SMI	LNK14			162	0110	46	0911	0064
	STU	LNK09			163	0064	21	0918	0921
	RBL	FPONE			164	0921	24	1700	0953
	STU	LNK10			165	1047	24	1700	0953
	STL	LNK02			166	0953	20	0907	0160
	RAU	LNK09			167	0160	20	0918	0073
	STL	LNK05			168	0073	20	0127	0130
	STL	LNK11			169	0130	20	0185	0038
	SLT	0008			170	0038	35	0008	0957
	SUP	FIFTY			171	0957	11	0210	1015
	NZE		LNK04		172	1015	45	0964	0919
	SMI		LNK03		173	0968	61	8003	0179
	RSU	8003			174	0971	69	0242	0125
	LOO	FPONE			175	0179	39	0007	0195
	STO	LNK02	LNK03		176	0195	30	0008	0041
LNK03	SRT	0008			177	0122	30	0008	0041
	STO	0000			178	0041	36	0000	0213
	AUP	SIXTY			179	0213	11	8002	0229
	QUP	8002			180	1021	10	8002	0229
	RAU	8003			181	0229	60	8003	0137
	FMP	LNK02			182	0137	39	0260	0910
	FMP	LNK08			183	1007	21	0127	0919
	FMP	LNK08	LNK04		184	0910	21	0127	0919
LNK04	RAL	LNK09			185	0919	55	0918	0062
	SRT	0002			186	0123	30	0002	0279
	RAU	0009			187	0279	60	8002	0187
	ALO	FIFTY			188	0187	15	0210	1065
	SLT	0002			189	1065	35	0002	1071
	FAD	FPONE			190	1071	62	0242	0955
	STU	LNK09			191	0969	31	0918	1121
	F88	FPYWO			192	1121	33	0924	0901
	FOV	LNK09			193	0918	34	0918	1918
	STU	LNK13			194	1018	21	0172	0063
	STU	LNK12			195	0025	24	0028	0131
	STU	LNK13			196	0131	24	0131	0988
	FMP	8001	LNK06		197	0088	39	8001	0003
	STU	FACTR			198	0091	21	0046	0099
LNK06	RAU	LNK10			199	0909	20	1709	0950
	FAD	FPYWO			200	0205	32	0924	0931
	STU	LNK10			201	0951	21	1700	1003
	RAU	LNK13			202	0003	60	0172	0187
	FMP	FACTR			203	0177	39	0046	0096
	FOV	LNK10			204	0096	34	1700	1750
	STU	LNK13			205	1750	25	1750	0205
	FAD	LNK13			206	0075	32	0028	0255

BTU LNX12		207	0255	21	00288	0181
F88 LNX11		208	0181	33	01855	0111
F8V LNX11		209	0235	34	0185	0235
RAW R003		210	0235	67	8003	0043
RAU R008		211	1021	60	8002	1001
F88 BIZE7		212	0241	33	1054	0231
BMI LNX17		213	0231	46	0084	0285
LDO LNX12		214	0285	69	0028	0043
BTU LNX11		215	0285	84	0185	0138
RAU LNX13		216	0138	60	0172	0227
FMP LNX10		217	0227	39	1700	1800
STU LNX13		218	1800	20	0172	0099
FMP LNX10		219	0084	60	0028	0083
STU LNX13		220	0083	39	0924	0044
FMP LNX10		221	0974	33	0277	0903
F88 LNX05	LNX06	222	0242	10	0000	0051
F88 LNX05	LNX08	223	0924	20	0000	0051
F88 LNX05	LNX08	224	1054	10	0000	0040
F88 LNX05	LNX08	225	0260	23	0258	5151
F88 LNX05	LNX08	226	0210	50	0000	0000
F88 LNX05	LNX08	227	0116	00	0000	0060
F88 LNX05	LNX08	228	0911	01	2345	6789
F88 LNX05	LNX08	229	1850	24	1033	1056
F88 LNX05	LNX08	230	1056	20	1011	0114
F88 LNX05	LNX08	231	0114	67	1011	1115
F88 LNX05	LNX08	232	1115	20	1019	0222
F88 LNX05	LNX08	233	0222	60	1019	0173
F88 LNX05	LNX08	234	0173	39	0026	0076
F88 LNX05	LNX08	235	0076	32	0929	0905
F88 LNX05	LNX08	236	0905	39	1019	1069
F88 LNX05	LNX08	237	1069	32	0272	0149
F88 LNX05	LNX08	238	0149	39	1019	1119
F88 LNX05	LNX08	239	1119	32	0026	0199
F88 LNX05	LNX08	240	0199	39	1019	1169
F88 LNX05	LNX08	241	1169	32	0972	0249
F88 LNX05	LNX08	242	0249	39	1019	1219
F88 LNX05	LNX08	243	1219	32	1022	0299
F88 LNX05	LNX08	244	0299	39	1019	1269
F88 LNX05	LNX08	245	1269	32	1022	0349
F88 LNX05	LNX08	246	0349	39	1104	1057
F88 LNX05	LNX08	247	1057	39	1104	1154
F88 LNX05	LNX08	248	1154	21	1104	1107
F88 LNX05	LNX08	249	1107	39	1104	1204
F88 LNX05	LNX08	250	1204	21	1104	1157
F88 LNX05	LNX08	251	1157	60	1011	1165
F88 LNX05	LNX08	252	1165	46	1058	1319
F88 LNX05	LNX08	253	1058	60	1072	0277
F88 LNX05	LNX08	254	0277	34	1104	1254
F88 LNX05	LNX08	255	1254	31	1104	1319
F88 LNX05	LNX08	256	1319	65	1104	1033
F88 LNX05	LNX08	257	1072	10	0000	0051
F88 LNX05	LNX08	258	0051	84	0908	6850
F88 LNX05	LNX08	259	0972	31	2575	8349
F88 LNX05	LNX08	260	0922	25	9137	1248
F88 LNX05	LNX08	261	0572	17	1562	0047
F88 LNX05	LNX08	262	0929	54	3020	0045
F88 LNX05	LNX08	263	0026	69	0600	0044
F88 LNX05	LNX08	264	1999	69	1100	1103
F88 LNX05	LNX08	265	1103	24	1106	0259
F88 LNX05	LNX08	266	0259	69	0101	1304
F88 LNX05	LNX08	267	1304	80	8001	0994
F88 LNX05	LNX08	268	0960	69	0000	1153
F88 LNX05	LNX08	269	1153	24	1156	0909
F88 LNX05	LNX08	270	0909	24	0018	0213
F88 LNX05	LNX08	271	1215	24	1118	1171
F88 LNX05	LNX08	272	1171	24	1106	1061
F88 LNX05	LNX08	273	1061	39	1106	0955
F88 LNX05	LNX08	274	1206	21	1010	0263
F88 LNX05	LNX08	275	0263	60	0150	0955
F88 LNX05	LNX08	276	0955	34	0103	1203
F88 LNX05	LNX08	277	1203	21	0258	1111
F88 LNX05	LNX08	278	1111	39	0258	0908
F88 LNX05	LNX08	279	0908	21	0000	0051
F88 LNX05	LNX08	280	1265	60	0150	1005
F88 LNX05	LNX08	281	1005	34	0104	1354
F88 LNX05	LNX08	282	1354	31	0058	1164
F88 LNX05	LNX08	283	1161	39	0258	0958
F88 LNX05	LNX08	284	0958	21	0112	1315
F88 LNX05	LNX08	285	1315	60	0150	1005
F88 LNX05	LNX08	286	1365	33	0062	0239
F88 LNX05	LNX08	287	0239	33	0112	0285
F88 LNX05	LNX08	288	0239	21	0000	0051
F88 LNX05	LNX08	289	1097	69	0000	1253
F88 LNX05	LNX08	290	1253	84	1156	0955
F88 LNX05	LNX08	291	0955	60	0150	1005
F88 LNX05	LNX08	292	1009	33	2300	0927
F88 LNX05	LNX08	293	0927	39	1106	1254
F88 LNX05	LNX08	294	1256	39	0030	1900
F88 LNX05	LNX08	295	1900	65	8003	1207
F88 LNX05	LNX08	296	1207	69	1060	1850
F88 LNX05	LNX08	297	1060	20	0000	0051
F88 LNX05	LNX08	298	1211	60	0200	1058
F88 LNX05	LNX08	299	1055	33	0258	0935
F88 LNX05	LNX08	300	0935	21	0058	1061
F88 LNX05	LNX08	301	1261	60	0105	1059
F88 LNX05	LNX08	302	1059	39	1106	1306
F88 LNX05	LNX08	303	1306	39	0030	1051
F88 LNX05	LNX08	304	1051	65	8003	1109
F88 LNX05	LNX08	305	1109	69	0162	1050
F88 LNX05	LNX08	306	1050	20	0162	0162
F88 LNX05	LNX08	307	0120	60	0200	1102
F88 LNX05	LNX08	308	1103	33	0117	0133
F88 LNX05	LNX08	309	0093	21	0117	0177

	RAU	TEMP1		MOOE ENO	310	0170	60	0258	0913
	FOV	TEMP3		CORRECTION	311	0913	34	0117	0147
	STU	FWECP		FACTOR	312	0167	21	1122	0125
	RAU	Z	A		313	0125	60	2300	1155
	FMP	GAM11			314	1155	39	1101	3353
	RAL	B003			315	1155	55	8003	0993
	LOO				316	0963	69	0066	1850
	STL	TEMP1	E00EA		317	0666	60	0586	1311
	RAU	X			318	311	60	0150	1361
	FMP	PI			319	1361	39	0150	1101
	FOV	A			320	1101	34	0103	3303
	RAL	B003			321	1303	55	8003	1413
	LDD				322	1411	69	0164	1350
	STL	TEMP2	E00CR		323	0164	60	0117	0220
	RAU	Y			324	0220	60	0107	1461
	FMP	PI			325	1461	39	0150	1151
	FOV	B			326	1151	34	0134	1404
	RAL	B003			327	1404	55	8003	1514
	LDD				328	1511	69	0214	1350
	STL	TEMP3	E00CR		329	0214	60	1369	1172
	RAU	TEMP1		CALCULATE	330	1172	60	0258	1013
	FOV	TEMP2		CONSTANT	331	1013	34	0117	0217
	FMP	TEMP3		TERM FOR	332	0217	34	1369	1419
	FOV	FWECP		GENCF	333	1419	34	1122	0222
	STU	CONST			334	1222	21	0126	0979
	RAU	THREE			335	0979	60	0950	1205
	STU	M			336	1205	21	1110	1063
	RAU	ONE			337	1063	60	0200	1255
	STU	N	LOOP2		338	1255	21	0500	1353
	RAU	N			339	1353	60	0500	1353
	FMP	PI			340	1305	39	0150	1201
	FMP	Y			341	1201	39	0107	1257
	FOV	B			342	1257	34	0104	1464
	RAL	B003			343	1454	65	8003	1561
	LDD				344	1561	69	0264	1350
	STL	TEMP2	E00CR	Y COSINE	345	0264	60	0110	1460
	RAU	M	LOOP1	TERM	346	0270	60	1110	1415
	FMP	PI			347	1415	39	0150	1253
	FMP	PI			348	1253	39	0150	1253
	FOV	A			349	1406	34	0103	1403
	RAL	B003			350	1403	65	8003	1611
	LDD				351	1611	69	0914	1350
	STL	TEMP1	E00CR	X COSINE	352	0914	20	0258	1661
	RAU	M		TERM	353	1661	60	1110	1463
	FMP	PI			354	1463	39	0150	1253
	FOV	A			355	1301	34	0103	1453
	STU	ALW80			356	1453	21	1008	1711
	FMP	ALW80		ALPHA M	357	1711	39	0150	1355
	STU	ALW80		SQUARED	358	1058	21	1008	1761
	RAU	N			359	1761	60	0500	1355
	FMP	PI			360	1355	39	0150	1253
	FOV	B			361	1351	34	0104	1504
	STU	BEN80			362	1504	21	1108	1814
	FMP	BEN80		BETA M	363	1814	39	0150	1355
	STU	BEN80		SQUARED	364	1158	21	1108	1861
	FAD	ALW80			365	1861	32	1008	0985
	FAD	KAP80			366	0985	32	0044	1211
	LDD				367	1221	69	1024	1500
	STU	GAMMN	E00AU	GAMMA MM	368	1024	21	0078	0931
	RAU	M			369	0931	60	1110	1515
	FAD	N			370	1515	32	0500	0977
	FAD	TWO			371	0977	32	0250	1027
	FOV	TWO	LOOP7		372	1027	34	0250	1402
	LDDP7	F8B	TWO		373	1401	33	0250	1077
	NZE		LOOP4		374	1077	45	0180	0981
	EMI		LOOP7		375	0180	46	0133	1401
	RBU	ONE			376	0133	61	0200	1405
	STU	SIGN	LOOPS		377	1405	21	1160	1113
	RAU	ONE			378	0981	60	0500	1453
	STU	SIGN	LDDP5		379	1455	21	1160	1113
	RAU	C			380	1113	60	0105	1155
	F8B	Z	A		381	1159	33	0350	1819
	FMP	GAMMN			382	1127	39	0078	0128
	FMP	MTHO			383	0128	39	0050	1453
	RAL	B003			384	1453	55	0904	1809
	LDD				385	1209	69	0212	1850
	RSU	B002	E00EA		386	0212	61	8002	1271
	FAD	ONE			387	1271	32	0200	1272
	STU	TEMP3			388	1177	21	1369	1272
	RAU	C			389	1272	60	0105	1259
	FMP	GAMMN			390	1259	39	0078	0128
	FMP	MTHO			391	0178	39	0050	1501
	RAL	B003			392	1501	65	8003	1305
	LDD				393	1309	69	0200	1850
	RSU	B002	E00EA		394	0262	61	8002	1321
	FAD	ONE			395	1321	32	0200	1272
	STU	TEMP3			396	1272	21	0143	1036
	RAU	Z	A		397	1035	60	0300	1505
	FMP	GAMMN			398	1505	39	0078	0228
	RAL	B003			399	0228	55	8003	1083
	LDD				400	1085	69	0188	1850
	RTL	TEMP5	E00EA		401	0188	20	0143	0146
	RAU	SIGN			402	0146	60	1160	1113
	FDM	N			403	1555	34	1110	1210
	FOV	N			404	1210	34	0500	0128
	FDM	N			405	1511	34	0143	0193
	FOV	TEMP5			406	0193	39	1369	1469
	FMP	TEMP3			407	1469	34	0069	0178
	STU	TEMP4			408	0132	21	1369	1322
	RAU	TEMP1			409	1322	60	0258	1163
	FMP	TEMP3			410	1163	39	0143	0146
	STU	TEMP3			411	0267	39	1369	1519
	FAD	TEMP3			412	1519	21	1369	1372

	RAU	CENCF		413	1372	60	11556	1911
	FAO	TEMP3		414	1911	32	1378	1245
	STU	CENCF		415	0245	21	1156	1359
	RAU	SEVEN		416	1359	60	1000	1555
	F88	M		417	1555	33	110	1237
	NZE	CONT1	CONT2	418	0237	45	0090	0141
CONT1	RAU	M		419	0090	60	1110	1615
	FAO	TWO		420	1615	21	050	1277
	STU	M	LOOP1	421	1277	31	1110	0270
CONT8	RAU	N		422	0141	60	0500	1605
	FAO	SEVEN		423	1605	32	1000	1337
	NZE	CONT3	CONT4	424	1327	45	0230	1031
CONT3	RAU	ONE		425	0230	60	0200	1655
	FAO	ONE		426	1655	21	110	1213
	RAU	N		427	1213	60	0500	1705
	FAO	TWO		428	1705	32	0250	1377
CONT4	RAU	CENCF	LOOP2	429	1377	21	050	1353
	FMP	CON8T		430	1031	60	1156	0912
	FAO	ONE		431	0912	39	0126	0176
	STU	CENCF		432	0176	32	0200	1427
	RAU	M		433	1427	31	1156	1409
	FOV	FMECF	A	434	1409	60	2500	1755
	FOV	CENCF		435	1755	34	1122	1422
	STU	NCOR	A	436	1422	34	1156	1456
	LDO	Z	A	437	1456	21	2700	1503
	STO	1977	A	438	1503	69	7300	1533
	LOO	N	A	439	1533	24	1977	0280
	STO	1978	A	440	0280	69	2500	1603
	LOO	NCOR	A	441	1603	24	1978	1041
	STO	1979	A	442	1041	69	2700	1641
	LOO	CENCF		443	1633	24	1979	0182
	STO	1980		444	0182	69	1156	1450
	LOO	FMECF		445	1459	24	1980	0183
	STU	1981		446	0183	69	1122	0175
	SCN	1977		447	0175	24	1975	0134
	SXA	0001		448	0134	71	1977	1477
	NZA	LOOP3	CONT5	449	1477	51	0001	0233
CONT5	STU	ZERO		450	0233	40	097	0237
	STO	SUM2		451	0887	69	0000	1703
	STU	SUMZ		452	1703	24	1506	1509
	STO	SMLNA		453	1509	24	1509	1565
	STU	SMLZA		454	1665	24	1148	1371
	STO	SUMZ2		455	1371	24	1074	1527
	LOO	PGANT		456	1527	56	0001	1564
CONT6	RAU	Z	CONT6	457	1554	80	8001	1260
	FAO	SUM2	A	458	1260	60	2300	1805
	STU	SUMZ		459	1805	32	1005	0293
	RAU	Z	A	460	0303	21	1506	1559
	FMP	Z	A	461	1559	60	2300	1855
	FAO	SUMZ2	A	462	1855	69	2300	1601
	STU	SUMZ2		463	1601	32	1074	1651
	RAU	NCOR	A	464	1651	21	1074	1577
	LDO		LNX01	465	1577	60	2700	0205
	FAO	SMLNA		466	1205	69	1208	1650
	STU	SMLNA		467	1808	32	0962	0939
	RAU	NCOR	A	468	0939	21	0962	1715
	LOO		LNX01	469	1715	60	2700	1556
	FMP	Z	A	470	1556	69	1609	1650
	FAO	SMLZA		471	1609	39	2300	1701
	STU	SMLZA		472	1701	32	1148	0295
	RAU	SUM2		473	0295	21	1148	1421
	SXA	0001		474	1421	51	0001	1627
	NZA	CONT6		475	1627	40	260	1131
	RAU	SUM2		476	1131	60	1506	1012
	FMP	SMLNA		477	1012	39	0962	1062
	STU	TEMP1		478	1062	41	0258	0262
	RAU	OATPT		479	1112	60	0102	1307
	FMP	SMLZA		480	1307	39	1168	1216
	STU	TEMP2		481	1216	31	0117	0980
	RAU	DATPT		482	0920	60	0102	1127
	FMP	SUMZ2		483	1127	39	1074	1134
	STU	TEMP3		484	1134	40	1324	1427
	RAU	SUM2		485	1472	60	1506	1162
	STU	TEMP4		486	1162	39	1506	1606
	RAU	TEMP4		487	1606	60	0258	1133
	RAU	TEMP1		488	1135	60	0258	1263
	F88	TEMP2		489	1263	33	0117	0243
	STU	TEMP3		490	0243	31	1324	1323
	RAU	TEMP3		491	1212	60	1369	0223
	F88	TEMP4		492	0223	33	0082	1659
	STU	TEMP5	LEAST	493	1659	31	0117	0970
	RAU	TEMP1	SQUARES	494	0970	60	0258	1313
	FOV	TEMP2	SOLUTION	495	1313	34	0117	0917
	STU	NRGAM	BOR	496	0917	31	1506	1313
	F88	GAM11	GAMMA	497	0225	33	1106	0933
	STU	TEMP1		498	0933	21	0258	1262
	STU	NEG	POS	499	1262	31	1106	1116
NEG	RAU	GEG11		500	1765	60	1106	1312
	FOV	10000		501	1312	34	1050	1751
	STO	TEMP1		502	1751	31	0258	1358
	SMI		CONT7	503	1185	46	0238	0989
	RAU	NRGAM		504	0238	60	1522	1677
	STU	GAM11	LOOP6	505	1677	31	1106	0259
POS	RAU	GAM11		506	0116	60	1106	1362
	FOV	10000		507	1362	34	1050	1801
	F88	TEMP1		508	1801	31	0258	1333
	SMI		CONT7	509	1235	46	0288	0989
	RAU	NRGAM		510	0288	60	1522	1727
	STU	GAM11	LOOP6	511	1727	31	1106	0259
CONT7	RAU	P1		512	0989	60	0150	1656
	FOV	A		513	1656	34	0103	1753
	STU	TEMP1		514	1753	21	0258	1412

FMP	TEMP1	515	1412	39	0258	1355
STU	ALPH2	516	1258	21	0092	1615
RAU	PI	517	1815	60	0150	1706
FOV	B	518	1706	34	0104	1604
STU	TEMP1	519	1604	21	0258	1462
FMP	TEMP1	820	1462	39	0258	1308
STU	ALPH2	521	1308	21	0063	1865
RAU	PI	522	1865	60	0150	1756
FOV	B	523	1756	34	0104	1654
STU	TEMP1	824	1654	21	0258	1512
FMP	TEMP1	525	1512	39	0258	1358
STU	BETA2	526	1358	21	0112	1918
RAU	HWGAM	527	1918	60	1522	1777
FMP	HWGAM	528	1777	39	1522	1572
STU	GAM82	529	1572	21	1010	1363
RAU	ALPH2	530	1363	61	0062	0967
FMP	BETA2	531	0967	33	0112	1039
FAO	GAM82	532	1039	32	1010	0937
LOO		533	0937	69	0140	1500
STU	KAPPA	534	0140	21	0094	1147
RAU	ONE	535	1147	60	0200	1806
FOV	KAPPA	536	1806	34	0094	0144
FMP	CONVT	537	0144	39	1150	1851
STU	OL	538	1851	21	1856	1709
LOO	HWGAM	539	1709	69	1522	0875
STO	1977	540	0875	24	1977	0930
LOO	GAM11	541	0930	69	1106	1759
STO	1978	542	1759	24	1978	1101
LOO	FIRRT	543	1101	69	0100	1803
STO	1979	544	1803	24	1979	0232
LOO	POIHT	545	0232	69	0101	1704
STO	1980	546	1704	24	1980	0928
LOO	OL	547	0928	69	1856	1809
STO	1981	548	1809	24	1981	0184
PGH	1977	549	0184	71	1977	8000

E00AU

CALCULATE
DIFFUSION
LENGTH

8000

APPENDIX E

IBM 650 Programs for Diffusion Length,
Ratio Method

The first of these programs was written to evaluate the double integral function

$$F_{11}(z) = \int_{-a/2}^{a/2} \int_{-b/2}^{b/2} \phi(x, y, z) \cos \frac{\pi x}{a} \cos \frac{\pi y}{b} dx dy$$

The program was written in SOAP II and floating point form. The object program and a logic diagram are listed in this section.

The program was written to accommodate as many data points as were desired. The data was taken in the manner described in the section entitled "EXPERIMENTAL PROCEDURE". An odd number of data points is required in each of the horizontal traverses making up one set of data. This is to accommodate Simpson's rule, which is used for the major portion of the integration. The trapezoidal rule is used to evaluate the integral over the area between the fifth horizontal traverse and the extrapolated boundary.

Input constants and data input forms are listed in Table 23. Flux data should be stored in descending order of traverse, the outermost traverse, the extrapolated boundary, being first. Each traverse should be listed with its outermost point first. One card of form one is needed for each set of data. The output form is listed in Table 24.

The approximate time for evaluation of the integral using 54 data points is three minutes.

The second program was written to determine the diffusion

Table 23. Input forms for double integral evaluation program.

Symbol	Explanation	Drum Storage Location
A	Extrapolated x-dimension	0000
B	Extrapolated z-dimension	0001
BPRIM	Distance from center of pile to outer-most fuel port	0002

Word	1	2	3
Form 1	Number of Data Points (IR Form)	z Elevation of Data	
Form 2	Count Rate	x co-ordinate	y co-ordinate

Table 24. Output forms for double integral evaluation program.

Word	1	2	3
	Integral	Elevation z	Number of Data Points

length by the ratio method. It was written in SOAP II and floating point form. The object program and a logic diagram are included in this section.

An initial trial value of γ_{11} is determined by

$$\gamma_{11} = \frac{1}{(z_2 - z_1)} \ell n \frac{F_1}{F_2}$$

Input constants and data input forms are listed in Table 25.

In the notation used, z_1 should always be greater than z_2 .

Table 25. Input forms for ratio method program.

Symbol	:	Explanation	:	Drum Storage Location
A	:	Extrapolated x-dimension	:	0100
B	:	Extrapolated y-dimension	:	0101
C	:	Extrapolated z-dimension	:	0102

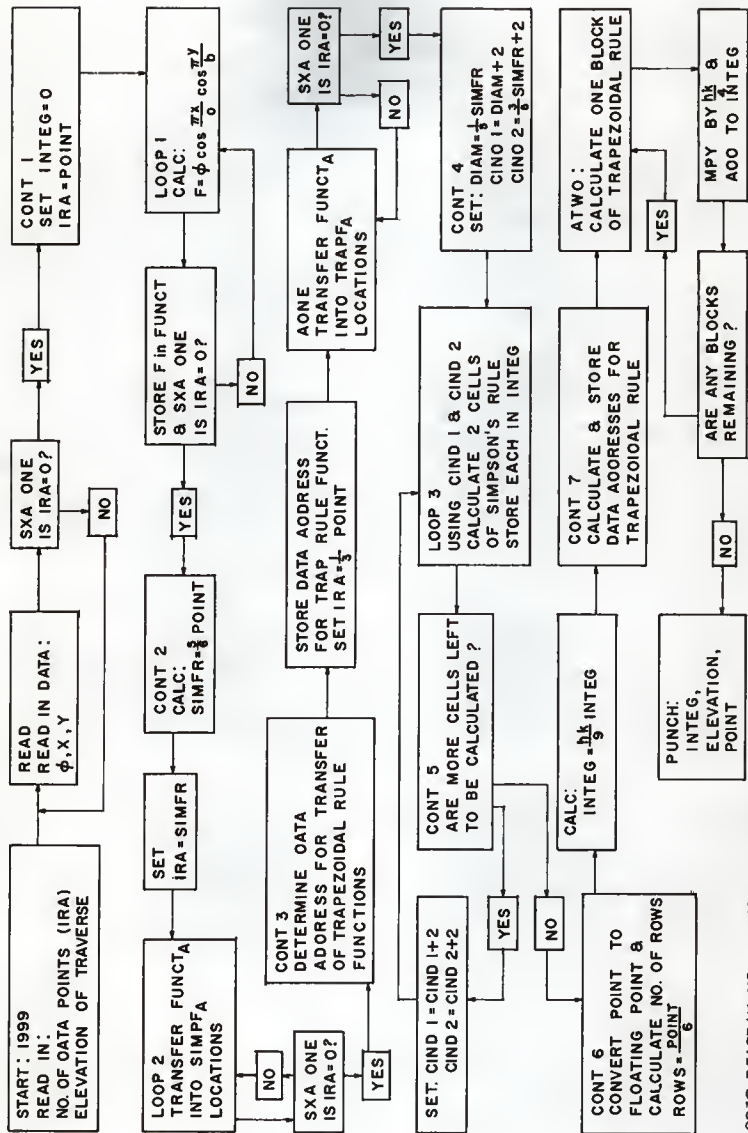
Word	1	2	3	4
Form 1	z_1	z_2	F_1	F_2

The two output forms for the ratio method program are listed in Table 26. One card of form one is punched for each trial. Operating time is between 20 and 30 seconds for one calculation of diffusion length.

Table 26. Output forms for ratio method program.

Word	1	:	2	:	3	:	4	:	5	:	6
Form 1:	Gamma	:	Error	:		:		:		:	
Form 2:	z_1	:	z_2	:	Gamma	:	Diffusion Length	:	Ratio	:	Number of Trials

IBM 650 PROGRAM FOR $\iint \phi \cos \frac{\pi x}{a} \cos \frac{\pi y}{b} dx dy$



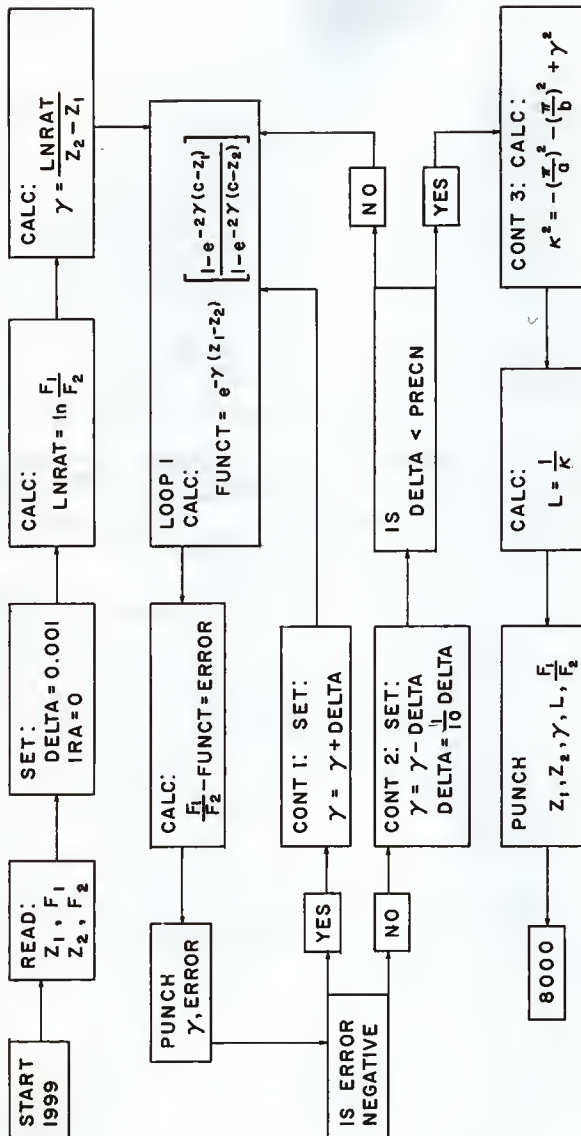
LOGIC DIAGRAM NO. 1, APPENDIX E

	HLR	1951	195H	1	0000	00	0000	0000
	HLR	1977	19H4	2	0000	00	0000	0000
	HLR	0100	0600	3	0000	00	0000	0000
	SYN	FLUX	0100	4	0000	00	0000	0000
	SYN	X	0000	5	0000	00	0000	0000
	SYN	Y	0300	6	0000	00	0000	0000
	SYN	UNCT	0400	7	0000	00	0000	0000
	SYN	HMPF	0500	8	0000	00	0000	0000
	SYN	TRAPP	0600	9	0000	00	0000	0000
	SYN		0800	10	0000	00	0000	0000
	SYN	B	0001	11	0000	00	0000	0000
	SYN	HPRIH	0002	12	0000	00	0000	0000
	SYN	STANT	1999	13	0000	00	0000	0000
ZERO		00	0000	14	0000	00	0000	0000
ONE		00	0000	15	0700	00	0000	0001
TWO		00	0000	16	0750	00	0000	0002
THREE		00	0000	17	0600	00	0000	0003
FOUR		00	0000	18	0850	00	0000	0004
FIVE		00	0000	19	0900	00	0000	0006
SIX		00	0000	20	0950	00	0000	0008
EIGHT		00	0000	21	1000	00	0000	0010
TEN		00	0000	22	1050	00	0000	0012
SIXTY		10	0000	23	1100	10	0000	0051
FP1		20	0000	24	1150	20	0000	0051
FP2		31	4159	25	1200	31	4159	0051
FP4		40	0000	26	1250	40	0000	0051
FP6		60	0000	27	1300	60	0000	0051
FP8		80	0000	28	1350	80	0000	0051
FP9		90	0000	29	1400	90	0000	0051
FP16		16	0000	30	1450	16	0000	0052
INORA		00	4000	31	1500	00	2400	0000
INDA		00	4000	32	1550	00	2600	0000
INOR		00	4000	33	1600	00	4600	0000
EOUCH		BTU	EXIT	34	1650	24	0003	0006
	RAO	W000		35	0006	60	8002	0015
	BHI	NEGAT	HEGUC	36	0015	46	0018	0019
	NEGAT	FWOPI		37	0018	37	0018	0047
	MHI	NEGAT		38	0047	46	0018	0051
	FBR	UNLPI	COSIU	39	0051	33	0004	0051
	FBR	TWOP1		40	0051	40	0001	0077
	MHI		HEHUC	41	0097	46	1700	0019
	FAD	ONEPI	COSIU	42	1700	32	0004	0031
	STH	THETA		43	0031	21	0036	0039
	RSB	PONF		44	0039	61	0042	0697
	STH	TERMH		45	0097	21	0032	0005
	STH	FONKT		46	0051	20	0010	0033
	STL	LNNH	NEGST	47	0013	20	0017	0020
	STH	EXIT		48	1750	24	0003	0056
	R4H	4002		49	0056	00	8002	0045
	MHI	NEGAY	HEBDO	50	0065	46	0058	0069
	FAU	TWOP1		51	0068	32	0021	0747
	FBR	HEAV		52	0068	46	0747	0651
	FBR	ONEPI	SINET	53	0651	33	0004	0081
	FBR	TWOP1		54	0669	33	0021	0797
	MHI		HEOUD	55	0797	46	0010	0059
	FAU	ONEPI	SINLT	56	1800	32	0004	0081
	STO	THETA		57	0081	21	0036	0089
	RSO	8003		58	0089	61	8003	0847
	STU	TERMH		59	0847	21	0052	0055
	BTU	FONKT		60	0055	21	0010	0063
	LDU	FPONE		61	0063	69	0406	0045
	STU	ENNN	NFGST	62	0045	24	0017	0020
	RAO	FNNH		63	0020	60	0017	0071
	FAU	FPONE		64	0071	32	0042	0669
	STU	ONE		65	0669	21	0024	0027
	FAU	FPONE		66	0027	32	0042	0719
	STH	ENNNH		67	0719	61	0017	0070
	RSO	TERMH		68	0070	61	0052	0007
	FMP	THETA		69	0007	39	0036	0086
	FMP	THETA		70	0066	69	0036	0086
	FUY	ENNN		71	0686	34	0024	0074
	STU	TERMH		72	0074	34	0017	0067
	RAW	FONKT		73	0067	67	0010	0665
	STL	FMAG		74	0655	67	0010	0665
	RAM	TERMH		75	0665	20	0769	0022
	RAO	HO02		76	0022	60	8002	0715
	FOY	FHAG		77	0057	60	8002	0715
	FBR	BIZEFF		78	0715	34	0769	0819
	MHI	HMPFF		79	0819	69	0072	0053
	RAU	FONKT		80	0049	46	0652	0033
	FAU	TERMH		81	0033	60	0010	0765
	STU	FONKT		82	0765	60	0010	0765
	RAU	FONKT	NEGST	83	0029	21	0010	0020
	RAU	FONKT	EXIT	84	0652	65	0010	0003
	ENUFF			85	0028	10	0000	0043
	BIZLH	10	0000	86	0000	69	8318	5351
	TWOP1	31	4159	87	0004	31	4159	2751
	ONEPI	10	0000	88	0004	10	0042	0051
	FPONE	10	0000	89	1999	70	1951	0701
	START	LDU	1951	90	0701	69	1951	0034
		STO	POINT	91	0034	64	0052	0029
		LDU	1958	92	0060	69	1952	0705
		STU	ELEV	93	0705	24	0008	0011
		LDU	POINT	94	0011	69	0611	0666
		RAO	PH01	95	0660	80	8001	0016
		RCU	1951	96	0016	70	1951	0751
		LDU	1951	97	0751	69	1951	0051
		RCU	1951	98	0654	24	2100	0653
		LDU	1952	99	0653	69	1952	0751
		LDU	0300	100	0755	24	2855	0703
		LDU	1953	101	0703	69	1953	0656
		LDU	0300	102	0656	24	2300	0753
		RYA	0001	103	0753	51	0001	0009

CUNT1	NZA	HEAO	CUNT1	104	0009	40	0016	066J
	LDD	ZEMO		105	066J	69	005W	0803
	STL	INTEG		106	0803	94	0700	0659
	LJD	POINT		107	0059	69	0657	0710
	RAA	H001	LOOPI	108	0710	80	8001	0066
	RAL	H003		109	0066	60	0066	0803
	FMP	PI	A	110	0805	39	1200	1850
	FUV	A		111	1850	34	000U	1900
	RAL	H003		112	1900	65	0000	0707
	LDD		EODCK	113	0707	69	0760	1650
	STL	TEMP1		114	0760	20	0815	0668
	RAU	Y	A	115	0668	60	0668	0805
	FMP	PI		116	0855	39	1200	1950
	FUV	8		117	1950	34	0001	0801
	RAL	H003		118	0801	65	0003	0659
	LDD		EODCK	119	0659	69	0018	1650
	RAU	H002		120	0012	60	8002	0671
	FMP	TEMP1		121	0671	39	0015	0865
	FMP	FLUX	A	122	0865	39	2100	0851
	STU	FNCT	A	123	0851	21	2400	0853
	SXA	0001		124	0853	31	0001	0709
	NZA	LOOPI	CONT4	125	0709	40	0066	0713
	RAU	POINT		126	0713	60	0657	0061
	MPY	FIVE		127	0061	19	0850	0670
	DIV	SIX		128	0670	14	0900	0810
	UTL	SIMFR		129	0810	20	0915	0718
	LDD	SIMFR		130	0718	69	0915	0768
	RAA	H001	LOOPI	131	0768	80	8001	0674
	LDD	FNCT	A	132	0674	69	2400	0903
	STL	SIMPF	A	133	0903	64	0503	0674
	SXA	0001		134	0953	51	0001	0759
	NZA	LOOPI	CONT3	135	0759	40	0674	0763
	RAU	SIMFR		136	0753	60	0915	0869
	MPY	EIGHT		137	0869	19	0950	0720
	DIV	TEN		138	0720	14	1000	0860
	BLT	0004		139	0860	34	0004	0721
	ALO	INHX		140	0721	15	1500	0905
	LDD	ONE		141	0905	69	0058	0661
	SXA	ADONE		142	0661	22	0038	0711
	RAU	POINT		143	0711	60	0657	0761
	MPY	TWO		144	0761	19	0750	0770
	DIV	SIX		145	0770	14	0700	0930
	LDD	H002		146	0910	69	8002	0667
	RAA	H001	AUNE	147	0667	80	8001	0058
	STU	THAPF	A	148	0058	69	0915	0777
	STU	THAPF		149	0702	24	2600	1003
	SXA	0001		150	1003	51	0001	0809
	NZA	ADONE	CONT4	151	0809	40	0900	0803
	RAL	SIMFR		152	0013	65	0915	0919
	DIV	FIVE		153	0919	14	0850	0960
	STL	OIAM		154	0960	20	0960	0918
	ALO	TWO		155	0918	15	0750	0955
	STL	CIND1		156	0955	20	0059	0662
	RAU	SIMFR	ST INHX	157	0062	60	0915	0969
	MPY	THREE	REGSTERS	158	0969	19	0000	0820
	DIV	FIVE	FOR	159	0820	14	0850	1010
	ALO	TWO	SIMPSONN	160	1010	15	0750	1005
	RAL	POINT	MULL	161	1005	20	0909	0662
	DIV	SIX		162	0662	65	0657	0811
	STL	CIND1		163	0811	14	0900	1060
	STL	CELL4		164	1060	16	0700	1055
	LDD	CIND1	LOOPI	165	1055	20	0959	0718
	RAA	H001		166	0712	69	0859	0764
	RAH	SIMPF	A	167	0762	80	8001	0868
	FMP	FP26		168	0868	60	2500	1105
	FAD	INTEG		169	1105	39	1450	0901
	STU	INTEG		170	0901	32	0706	0033
	STU	INTEG		171	0033	21	0706	1009
	SXA	0001		172	1009	51	0001	1015
	RAU	SIMPF	A	173	1015	60	2500	1155
	AXA	0002		174	1155	50	0002	0861
	FAD	SIMPF	A	175	0861	32	2500	0877
	SXA	0001		176	0077	51	0001	0083
	LOO	OIAM		177	0083	69	0965	0918
	SXA	H001		178	0918	51	0001	0724
	FAO	SIMPF	A	179	0724	32	2500	0677
	LOO	OIAM		180	0677	69	0965	0968
	AXA	H001		181	0968	50	8000	0724
	AXA	0002		182	0774	50	8001	0030
	FAU	SIMPF	A	183	0030	50	2000	0727
	FMP	FP26		184	0727	39	1200	0951
	STU	INTEG		185	0951	32	0706	0683
	STU	INTEG		186	0683	21	0706	1059
	AXA	0001		187	1059	50	0001	1065
	RAU	SIMPF	A	188	1065	60	2500	1205
	SXA	0002		189	1205	50	0002	0911
	FAD	SIMPF	A	190	0911	32	2500	0777
	LOO	OIAM		191	0777	69	0965	1018
	SXA	H001		192	1018	51	8001	0824
	AXA	0002		193	0824	51	8000	0800
	FAO	SIMPF	A	194	0800	32	2500	0827
	AXA	0002		195	0827	50	0002	0733
	FAD	INTEG	A	196	0733	32	2500	0877
	STU	INTEG	4 IMPSDNS	197	0877	32	0706	0783
	LOO	OIAM	MULE	198	0783	21	0706	1109
	SXA	H001		199	1109	39	0900	0668
	LOO	OIAM		200	0668	51	8001	0874
	SXA	0001	CHECK	201	0074	51	0001	0680
			CELLS					

	HMA		CUNT5	REMAINING	202	0680	41	0835	0034
	LOOP		LOOPS		203	0833	69	0909	0762
CONT6	RAL C1N02				204	0034	65	0959	0863
	STL CELL8				205	0863	16	0750	1255
	STL C1N01				206	1255	20	0959	0812
	NZE				207	0912	45	0666	0717
	RAL C1N01		CUNT6		208	0666	65	0159	0913
	ALO TWO				209	0913	15	0750	1305
	STL C1N01			ADJUST TO	210	1305	20	0859	0862
	RAL C1N02			NEXT CELL	211	0862	65	0909	0763
	ALO TWO			SET	212	0963	15	0750	1355
	STL C1N02				213	1355	20	0909	0912
CONT6	LOD C1N01		LOOPS		214	0912	69	0859	0762
	RAU POINT				215	0717	60	0657	0961
	SCT 0000				216	0961	36	0000	0883
	STL TEMP1				217	0883	20	0815	1118
	RAL 8003			CONVERT	218	1118	65	0032	0025
	ALO SIXTY			ROWS TO	219	0025	15	1050	1405
	SLO TEMP1			FLOATING	220	1405	16	0815	1019
	RAU 8003			POINT	221	1019	60	8002	0927
	FOV FP6				222	0927	34	1300	1001
	F8V FP1				223	1001	33	1100	0977
	STU ROWS				224	0977	21	0032	0035
	RAU A				225	0035	60	0000	1455
	FOV FP2				226	1455	34	1150	1051
	FOV ROWS				227	1051	34	0032	0082
	FMP FP0				228	0082	39	1350	1101
	FOV FP9				229	1101	34	1400	1151
	FMP INTEC				230	1151	39	0706	0756
CUNT7	STU INTEC		CUNT7		231	0756	21	0706	1159
	RAL POINT				232	1159	65	0657	1311
	DIV SIX				233	1011	14	0900	1110
	STL INDEK			SET	234	1110	20	1115	1168
	BLT 0004			DATA	235	1168	35	0004	0079
	ALO IN0A			ADDMEMBER	236	0079	15	1550	1505
	LDO ATWO			FOR	237	1505	69	0658	1061
	S0A ATWO			THAP RULE	238	1061	22	0658	1111
	LDD ATREE				239	1111	69	0014	0767
	S0A ATREE				240	0767	22	0014	0817
	RAL INDO				241	0817	65	1600	1555
	LDD BONE				242	1555	69	0708	1161
	S0A BONE				243	1161	22	0708	1211
	LDD BTWO				244	1211	69	0064	0867
	S0A BTWO				245	0867	22	0064	0917
	RAU B				246	0917	60	0001	1605
	FOV FP2				247	1605	34	1150	1201
	F8V WPK1W				248	1201	33	0002	0679
	FMP ROWR				249	0679	39	0032	0682
	FOV FP4				250	0682	34	1250	1251
	STU FACTR				251	1251	21	0006	1209
	LUO INDEK				252	1209	69	1115	1218
	RAA 8001				253	1218	80	8001	0924
	RAN 8001		ATWO		254	0924	82	8001	0658
	RAU 9999		BONE		255	0658	60	9999	0708
	FAI 9999				256	0708	39	9999	0075
	SXA 0001				257	0075	51	0001	0681
	8XB 0001				258	0681	53	0001	0037
	NZA ATREE		CUNT8		259	0037	40	0014	0041
	FAD 9999		BTWO		260	0014	39	9999	0064
	FAD 9999				261	0064	39	9999	0675
	FMP FACTR				262	0675	39	0806	0856
	FAD INTEC				263	0856	34	0706	0933
	STU INTEC				264	0933	21	0706	0658
	LUO INTEC		ATWO		265	0041	69	0706	1259
	8TH 1977				266	1259	24	1977	0740
	LDD ELEV				267	0740	69	0008	1261
	8TD 1978				268	1261	24	1978	0731
	LUO POINT				269	0731	69	0677	1160
	8TO 1979				270	1160	24	1979	0722
	PCH 1977		NO 00	START	271	0732	71	1977	1999

LOGIC DIAGRAM FOR IBM 650 PROGRAM FOR RATIO METHOD



LOGIC DIAGRAM NO. 2, APPENDIX E

OBJECT PROGRAM - APPENDIX E

	HLN	1951	1958	1	0000	00	0000	0000
	HLN	1977	1984	2	0000	00	0000	0000
	SYN	A	0100	3	0000	00	0000	0000
	SYN	B	0101	4	0000	00	0000	0000
	SYN	C	0102	5	0000	00	0000	0000
	SYN	STANT	1999	6	0000	00	0000	0000
UNE		10	0000	7	0000	10	0000	0051
WONE		20	0000	8	0000	20	0000	0051
MTR		30	0000	9	0150	30	0000	0051
PI		40	0000	10	0200	40	0000	0051
CONVT		50	0000	11	0300	50	0000	0052
TEH		60	0000	12	0350	60	0000	0045
PRECN		70	0000	13	0400	70	0000	0048
INCRK		80	0000	14	0450	80	0000	0006
EOGCL		90	0000	15	0006	90	0009	0012
STU	ZZ10			16	0012	24	1977	0030
LPU	ZZ10			17	0030	24	1978	0031
STO	1977			18	0031	24	1979	0032
STO	1978			19	0032	24	1980	0033
STO	1980			20	0033	24	1981	0034
STO	1981			21	0034	24	1982	0035
STO	1982			22	0035	24	1983	0036
STO	1983			23	0036	24	1984	0037
STO	1984			24	0037	00	0000	0000
ZZ10	00	0000	0000	25	0009	00	0000	0000
EOGCU	00	0000	0000	26	0500	24	0103	0056
	STO	NET		27	0056	46	0059	0010
	HMI	SERR		28	0010	45	0014	0103
	MZ	SEAT		29	0014	21	0018	0021
	STU	SA		30	0021	32	0024	0001
	FAO	SS10		31	0001	39	0004	0054
	FMP	SHAF	SS	32	0001	31	0008	0011
	STU	SSAV	SAH	33	0011	60	0018	0023
	RAU	SA	J CAPT A	34	0023	34	0008	0038
	FUV	SSAV		35	0034	31	0008	0043
	FAO	SSAV		36	0034	39	0004	0104
	FMP	SHAF		37	0104	33	0008	0135
	FSH	SSAV		38	0135	48	0039	0040
	MZU		SN	39	0039	46	0042	0040
	b.ii		SM	40	0042	32	0008	0185
	FAO	SSAV	SAH	41	0042	31	0008	0103
	STU	SSAV	SEAT	42	0040	60	0008	0103
	RAU	SSAV		43	0059	01	0000	0103
	NLT	0000	SEAT	44	0044	10	0000	0000
	NWAF	0000	0000	45	0024	10	0000	0051
	R10	10	0000	46	0024	24	0153	0106
	LNK01	STU	LNK08	47	0000	48	0061	0064
	NET		LNK14	48	0000	49	0068	0071
	HMI	LNK14		49	0004	00	0071	0000
	STU	LNK09		50	0004	21	0082	0035
	SL	FGONE		51	0005	20	0089	0092
	STU	LNK10		52	0025	20	0089	0092
	STL	LNK04		53	0027	20	0066	0073
	RAO	LNK09		54	0000	20	0027	0080
	YTL	LNK05		55	0000	20	0085	0038
	STL	LNK11		56	0007	38	0038	0000
	SLT	0000		57	0007	11	0110	0015
	UPP	FIFTY		58	0015	48	0116	0019
	RZE		LNK04	59	0116	46	0121	0022
	RMI		LNK03	60	0021	61	0003	0079
	RSO	8003		61	0079	69	0074	0077
	LPU	FGONE		62	0077	24	0089	0022
	STO	LNK08		63	0022	30	0008	0041
	SHT	0008		64	0041	36	0000	0013
	SCT	0000		65	0013	10	0016	0171
	UPP	SIXTY		66	0171	11	0002	0129
	SUP	8002		67	0129	60	0033	0037
	RAH	8003		68	0037	39	0089	0189
	FMP	LNK04		69	0139	39	0142	0192
	STU	LNK05		70	0192	21	0027	0039
	RAL	LNK00		71	0018	20	0068	0123
	NRT	0002		72	0123	30	0002	0179
	RAO	8002		73	0179	60	0010	0087
	ALO	FIFTY		74	0079	15	0110	0065
	BLT	0002		75	0065	35	0002	0221
	FAD	FGONE		76	0221	32	0204	0051
	STU	LNK09		77	0051	21	0068	0271
	FBR	PFTW0		78	0271	33	0124	0151
	FUV	LNK09		79	0151	31	0066	0168
	STO	LNK13		80	0168	21	0072	0025
	STU	LNK11		81	0025	24	0028	0081
	STO	LNK11		82	0081	24	0285	0088
	FMP	8001		83	0088	60	0078	0077
	STU	FACTN		84	0091	21	0046	0049
	RAU	LNK10		85	0049	60	0088	0137
	STU	LNK10		86	0049	32	0184	0201
	FMP	LNK13		87	0201	21	0082	0335
	FUV	LNK13		88	0335	60	0078	0077
	STU	FACTN		89	0077	39	0046	0096
	RAU	LNK10		90	0096	34	0082	0132
	FMP	LNK13		91	0132	60	0078	0077
	FAO	LNK12		92	0005	32	0028	0005
	STU	LNK12		93	0005	31	0028	0131
	FMP	LNK11		94	0131	32	0285	0141
	FUV	LNK11		95	0005	67	0085	0305
	RAM	8003		96	0305	67	0003	0043
	RAU	8002		97	0043	60	0088	0251
	FMP	SIZE7		98	0251	33	0154	0161
	HMI	LNK07		99	0161	46	0084	0135
	LOD	LNK12		100	0135	69	0043	0031
	STO	LNK11		101	0231	24	0285	0138
	RAO	LNK13		102	0138	60	0072	0177
	FMP	LNK10		103	0177	39	0082	0102

LNK07	STU LNK13	LNK06	104	0182	21	0072	0049
	RAU LNK12		105	0084	60	0028	0083
	FUP FPTW0		106	0083	39	0124	0174
	FUP LNK05		107	0174	21	0167	0133
	LO 0000	LNK08	108	0074	10	0000	0051
FPONE	20 0000		109	0124	20	0000	0051
FPTW0	30 0000		110	0134	20	0000	0051
WIZET	23 0858		111	0148	23	0258	5151
LNTEM	50 0000		112	0110	50	0000	0000
FIFTY	010000		113	0110	00	0100	0050
QIXTY	010000		114	0061	01	2345	6789
LNK14	STO AAA1		115	0600	84	0203	0156
E00EA	STU AAA2		116	0167	21	0167	0133
	RAU AAA2		117	0114	67	0161	M115
	STL AAA3		118	0115	20	0069	0122
	RAU AAA3		119	0122	20	0069	0122
	FMP AAA16		120	0173	39	0026	0076
	FAU AAA15		121	0076	34	0229	0055
	FMP AAA3		122	0033	39	0069	0119
	FAU AAA14		123	0119	32	0172	0099
	FMP AAA3		124	0099	39	0069	0169
	FMP AAA3		125	0169	32	0229	0149
	FMP AAA3		126	0149	39	0069	0219
	FAU AAA12		127	0219	32	0272	0199
	FMP AAA3		128	0199	39	0069	0269
	FAU AAA11		129	0269	32	0322	0249
	FMP AAA3		130	0249	39	0069	0319
	FAU AAA10		131	0319	32	0372	0309
	STU AAA4		132	0299	21	0204	0057
	FMP AAA4		133	0057	39	0204	0254
	STU AAA4		134	0254	21	0204	0347
	FMP AAA4		135	0107	39	0204	0304
	STU AAA4		136	0304	21	0204	0157
	RAU AAA3		137	0157	60	0161	0165
	HMI AAA5		138	0165	46	0218	0369
	FUW AAA4		139	0218	60	0372	0277
AAA5	STU AAA4		140	0277	40	0204	0354
	RAL AAA4	AAA6	141	0354	21	0204	0369
AAA6	RAL AAA4	AAA1	142	0369	65	0000	0051
AAA10	LO 0000	0051	143	0372	21	0000	0051
AAA11	24 9998	6850	144	0322	24	9998	6850
AAA12	31 2575	H349	145	0272	31	2575	6850
AAA13	25 4137	184H	146	0222	25	4137	124H
AAA14	17 1542	0047	147	0172	17	1562	0047
AAA15	54 3050	0045	148	0229	54	3050	0045
AAA16	050000	0044	149	0229	49	0600	0044
RTART	RCD 1951		150	1999	70	1951	0301
	LDD 1951		151	0401	24	0207	0160
	STU ZONE		152	0404	24	0207	0160
	LDD 1958		153	0160	69	1952	0105
	STO FONE		154	0105	24	0108	0211
	OO 1963		155	0211	69	1953	0206
	STU ZTWO		156	0206	24	0109	0062
	LDD 1954		157	0057	69	1952	0277
	RAA 0000		158	0257	24	0210	0063
	LOU INCR7		159	0063	69	0400	0223
	STO RELTA		160	0253	24	0256	0159
	RAU FONE		161	0159	80	0000	0215
	FOY FTW0		162	0215	60	0108	0113
	STU RATIO		163	0113	34	0210	0260
	LDD		164	0260	21	0164	0017
	STU LNRAT	LNK01	165	0017	69	0020	0550
	RAU ZTWO		166	0020	21	0224	0277
	F8H ZONE		167	0277	60	0109	0163
	OTU TEMP1		168	0163	33	0207	0133
	RAU LNRAT		169	0133	21	0108	0141
	F0V TEMP1		170	0141	60	0224	0279
	STU GAMMA	LODP1	171	0279	34	0188	0238
	AXA 0001		172	0238	21	0242	0045
	RAU ZONE		173	0048	50	0001	0351
	F8B ZTWO		174	0351	60	0207	0261
	FMP GAMMA		175	0261	31	0108	0285
	RAL 8003		176	0485	39	0242	0292
	LDD		177	0292	39	0050	0650
	STL TEMP1	E00EA	178	0650	65	8003	0307
	RAU C		179	0310	69	0310	0600
	F8B ZONE		180	0310	20	0188	0191
	FMP GAMMA		181	0191	60	0182	0377
	FMP MTW0		182	0357	33	0207	0183
	RAL 8003		183	0183	39	0242	0342
	LDD		184	0342	39	0340	0700
	ST1 TEMP2	E00EA	185	0700	65	8003	0407
	RAU ONE		186	0407	69	0360	0600
	F0B TEMP2		187	0360	20	0363	0268
	ST1 TEMP2		188	0268	60	0000	0155
	RAU C		189	0155	33	0265	0241
	F8B ZTWO		190	0241	20	0254	0318
	FMP GAMMA		191	0318	60	0102	0457
	RAL 8003		192	0457	33	0109	0555
	LDD		193	0555	39	0343	0392
	ST1 TEMP3		194	0392	39	0130	0750
	RAU ONE		195	0750	65	8003	0307
	F0B TEMP3	E00EA	196	0307	69	0410	0260
	ST1 TEMP3		197	0410	20	0315	0368
	RAU ONE		198	0368	60	0000	0600
	F8B ZONE		199	0600	33	0315	0291
	FMP GAMMA		200	0291	21	0315	0418
	RAL 8003		201	0418	60	0182	0373
	LDD		202	0373	39	0265	0365
	ST1 TEMP3		203	0365	34	0315	0418
	RAU ONE		204	0418	21	0070	0263
	F0V TEMP3		205	0223	60	0164	0419
	STU FUNCT						
	RAU RATIO						

	F8B	FUNCT		CHECK	206	0419	33	0070	8047
	STU	ERROR		ERROR	207	0047	21	0002	0265
	L00		E00CL		208	0255	69	0158	0450
	L00	GAMMA			209	0158	69	0242	0095
	STO	1977			210	0096	24	1977	0130
	L00	ERROR			211	0130	69	0002	0305
	STO	1978		HUNCH	212	0305	24	1978	0281
	WCH	1977		TRIAL	213	0281	71	1977	0357
	RAU	ERROR			214	0327	60	0002	0557
	SMI	CONT1	CUNT#		215	0557	46	0460	0317
CONT1	RAU	GAMMA			216	0460	60	0248	0577
	FAO	DELTA			217	0097	32	0256	0233
CONT2	STU	GAMMA	LOOP1		218	0233	21	0242	0045
	RAU	GAMMA			219	0311	60	0242	0147
	F8B	DELTA			220	0147	33	0256	0283
	STU	GAMMA			221	0243	21	0242	0145
	RAU	DELTA			222	0145	60	0256	0361
	FOV	TEN			223	0361	34	0300	0800
	STU	DELTA			224	0800	21	0256	0209
	F8R	PREC#		CHECK	225	0809	33	0350	0377
CONT3	SMI	CONT3	LOOP1	PRECISION	226	0377	46	0180	0045
	RAU	P1			227	0120	60	0200	0358
	FOV	A			228	0358	34	0100	0850
	STU	ALPH#2			229	0850	21	0454	0607
	FMP	ALPH#2		ALPHA	230	0607	39	0454	0504
	STU	ALPH#2		SQUARE#	231	0504	21	0454	0657
	RAU	P1			232	0657	60	0200	0405
	FOV	B			233	0405	34	0101	0401
	STU	BETA#2			234	0401	21	0306	0259
	FMP	BETA#2		BETA	235	0259	39	0306	0356
	STU	BETA#2		SQUARE#	236	0356	21	0306	0309
	RAU	GAMMA		GAMMA	237	0309	60	0242	0197
	FMP	GAMMA		SQUARE#	238	0197	39	0242	0442
	F8R	ALPH#2			239	0442	33	0454	0331
	F8R	BETA#2			240	0331	33	0306	0333
	L00		E00AU		241	0333	69	0086	0500
	STU	KAPPA		KAPPA	242	0086	21	0090	0143
	RAU	ONE			243	0143	60	0000	0456
	FOV	KAPPA		DIFFUSION	244	0455	34	0090	0140
	FMP	CONVT			245	0140	39	0250	0900
	STU	OL		LENGTH	246	0900	21	0554	0707
	L00	ZONE			247	0707	69	0807	0510
	STU	1977			248	0510	24	1977	0830
	L00	ZI#0			249	0830	69	0109	0112
	STO	1978			250	0112	24	1978	0381
	L00	GAMMA			251	0321	69	0248	0155
	STO	1979			252	0195	24	1979	0232
	L00	OL			253	0232	69	0554	0757
	STO	1980			254	0757	24	1980	0383
	L00	RATIO			255	0383	69	0164	0067
	STO	1981			256	0067	24	1981	0134
	L00	R006			257	0134	69	0008	0341
	STO	1982			258	0341	24	1982	0585
	WCH	1977	B000		259	0585	71	1977	8000

APPENDIX F

IBM 650 Program for Diffusion Length
Double Iteration Method

This program was written to evaluate the diffusion length by the double iteration technique. It was written in SOAP II and floating point form. The object program and a logic diagram are included in this section.

A detailed description of the double iteration process can be found in the THEORY. The constants A_{mn} are determined by the equation

$$A_{mn} = \frac{4 F_{mn}}{ab \sinh \gamma_{mn} (c - z_o)}$$

where z_o is the elevation at which the functions F_{mn} , determined by

$$F_{mn} = \int_{-a/2}^{a/2} \int_{-b/2}^{b/2} \phi(x, y, z) \cos \frac{m \pi x}{a} \cos \frac{n \pi y}{b} dx dy$$

are evaluated. The first portion of this program, which calculates the F_{mn} 's is an adaptation of the double integral evaluation program described in Appendix E. The remainder of the program performs the double iteration analysis. Several determinations may be desired with one set of F_{mn} 's. If this is the case, the data for each additional determination should be followed by a transfer card which sends the machine to the CON11 location. This will avoid unnecessary recalculation of the F_{mn} 's. The correction factors used are listed in Table 1.

Input to this program is partially in the form of one word load cards. Certain parameters, plus the data for the vertical traverse

are of this form. This input, listed in Table 27, should be followed by a transfer card and the data for evaluation of the double integral functions. The data for the evaluation of these functions is exactly the same as the input to the double integral program described in Appendix E, forms one and two.

Table 27. One word load input for double iteration program .

Symbol	Explanation	Drum Storage Location
A	Extrapolated x-dimension	0000
B	Extrapolated y-dimension	0001
BPRIM	Distance from center of pile to outermost fuel port	0002
HARM	Number of highest harmonic, floating point form	0003
FIRST	Initial Estimate of Gamma	0004
POINT	Number of Data Points (vert. traverse) in form 00 0000 00xx	0005
DATPT	Number of Data Points (vert. traverse) in floating point form	0006
C	Extrapolated z-dimension	0007
N	Count Rates for vertical traverse, stored consecutively starting at	0650
z	Co-ordinates of vertical traverse data, stored consecutively starting at	0675

The capacity of the program is 25 data points in the vertical traverse and 100 data points in the horizontal mesh. The program capable of using up to the ninth harmonic.

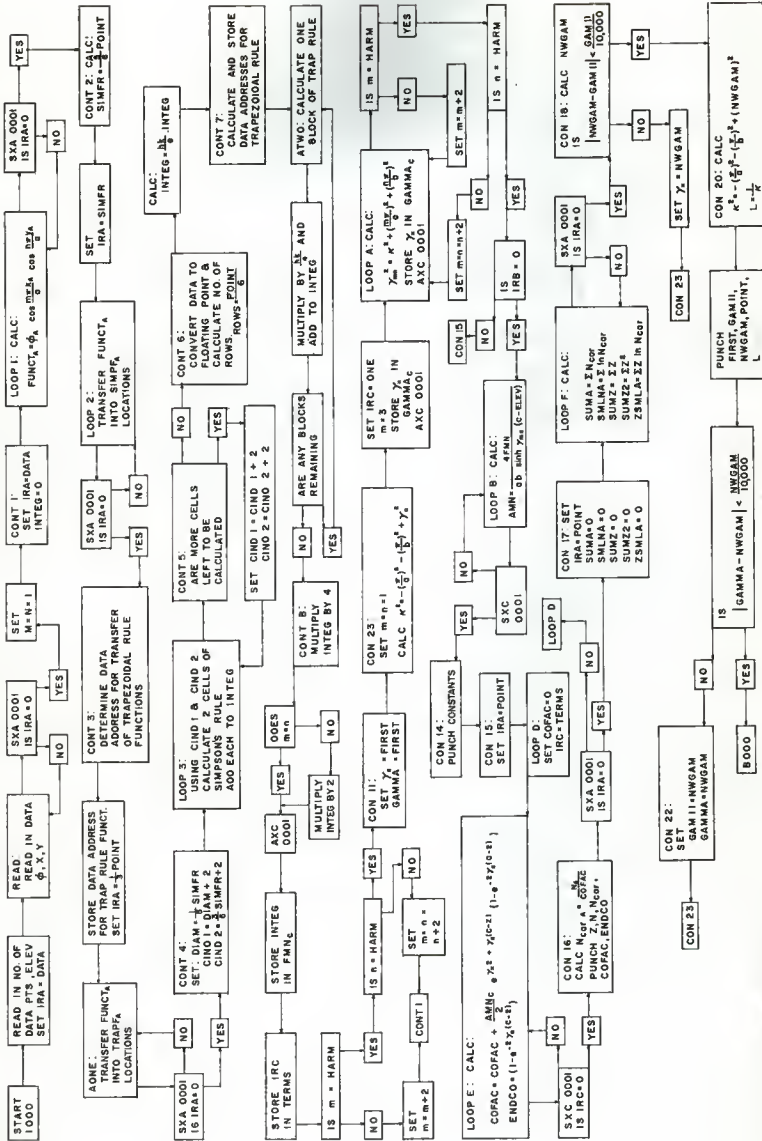
There are three output forms, listed in Table 28. The first lists the constants and may use two cards. The A_{mn} 's are listed in the order A_{11} , $2A_{13}$, $2A_{15}$, ... A_{33} , $2A_{35}$, ... A_{55} , etc.. Where m and n are not equal, the constant is multiplied by two to account for both the mn and nm terms at once. This can be done because of the symmetry of the pile. Form two is the standard correction factor output, and form three is a final output form. Form three is punched after the completion of each correction factor iteration.

Table 28. Output forms for double iteration program.

Word	1	2	3	4	5	6	7	8
Form 1: (3 harmonics)								
	A_{11}	$2A_{13}$	$2A_{15}$	A_{33}	$2A_{35}$	A_{55}	-	-
Form 2:								
	z	N	N_{corr}	C_H	C_E	-	-	-
Form 3:								
	FIRST	Next to last γ	Last γ	Data Points	Diffusion Length	-	-	-

Five to ten minutes are required for complete double iteration analysis using 10 data points. An additional three minutes is required for evaluation of each F_{mn} used.

LOGIC DIAGRAM FOR IBM 450 PROGRAM FOR DOUBLE ITERATION METHOD



LOGIC DIAGRAM, APPENDIX F

	BLR	1951	1960	1	0000	00	0000	0000	0000
	BLR	1977	1984	2	0000	00	0000	0000	0000
	BLR	1900	1999	3	0000	00	0000	0000	0000
	BLR	0100	0790	4	0000	00	0000	0000	0000
	SVN	FLUX	0100	5	0000	00	0000	0000	0000
	SVN	K	0610	6	0000	00	0000	0000	0000
	SVN	Y	0100	7	0000	00	0000	0000	0000
	SVN	FUNCT	0400	8	0000	00	0000	0000	0000
	SVN	SIMPF	0500	9	0000	00	0000	0000	0000
	SVN	TRAPP	0600	10	0000	00	0000	0000	0000
	SVN	Z	0650	11	0000	00	0000	0000	0000
	SVN	AMN	0675	12	0000	00	0000	0000	0000
	SVN	NCOR	0700	13	0000	00	0000	0000	0000
	SVN	GAMMA	0730	14	0000	00	0000	0000	0000
	SVN	AMN	0750	15	0000	00	0000	0000	0000
	SVN	FMM	0770	16	0000	00	0000	0000	0000
	SVN	A	0000	17	0000	00	0000	0000	0000
	SVN	B	0001	18	0000	00	0000	0000	0000
	SVN	8PRIM	0002	19	0000	00	0000	0000	0000
	SVN	HARM	0003	20	0000	00	0000	0000	0000
	SVN	FIRBT	0104	21	0000	00	0000	0000	0000
	SVN	POINT	0005	22	0000	00	0000	0000	0000
	SVN	QATPT	0006	23	0000	00	0000	0000	0000
	SVN	C	0007	24	0000	00	0000	0000	0000
	SVN	START	1000	25	0000	00	0000	0000	0000
ZERO	00	0000	0000	26	0050	00	0000	0000	0000
ONE	00	0000	0001	27	0800	00	0000	0001	0000
TWO	00	0000	0002	28	0850	00	0000	0002	0000
THREE	00	0000	0003	29	0900	00	0000	0003	0000
FIVE	00	0000	0005	30	0950	00	0000	0005	0000
SIX	00	0000	0006	31	1050	00	0000	0006	0000
EIGHT	00	0000	0008	32	1100	00	0000	0008	0000
TEN	00	0000	0010	33	1150	00	0000	0010	0000
SIXTY	00	0000	0060	34	1200	00	0000	0060	0000
FP1	10	0000	0051	35	1250	10	0000	0051	0000
FP8	20	0000	0060	36	1300	20	0000	0060	0000
PI	31	4159	0051	37	1350	31	4159	0051	0000
FP4	40	0000	0051	38	1400	40	0000	0051	0000
FP6	60	0000	0051	39	1450	60	0000	0051	0000
FP8	80	0000	0051	40	1500	80	0000	0051	0000
FP9	90	0000	0051	41	1550	90	0000	0051	0000
FP16	16	0000	0051	42	1600	16	0000	0051	0000
CORXY	25	3600	0051	43	1650	25	3600	0051	0000
10000	10	0000	0055	44	1700	10	0000	0055	0000
INCLX A	00	4000	0000	45	1750	00	4000	0000	0000
INOA	00	2600	0000	46	1800	00	2600	0000	0000
INOB	00	4600	0000	47	1850	00	4600	0000	0000
EODEA	00	4600	0000	48	0051	00	4600	0000	0000
	STL	AAA1		49	0057	20	0011	0014	
	RAU	AAA16		50	0014	60	0017	0021	
	STU	AAA14		51	0021	37	0012	0017	
	STU	AAA2		52	0037	21	0042	0045	
	RAU	AAA3		53	0045	60	0048	0053	
	STU	AAA4		54	0053	21	0042	0047	
	RAU	AAA2		55	0061	60	0042	0047	
AAA8	F88	AAA5	AAA8	56	0047	33	0801	0027	
	SMI	AAA5		57	0027	46	0037	0031	
	STU	AAA2		58	0031	21	0042	0095	
	RAU	AAA4		59	0095	60	0008	0013	
	FMP	AAA7		60	0013	39	0016	0066	
AAA6	STU	AAA4	AAA8	61	0066	21	0008	0061	
	RAU	AAA2		62	0030	60	0042	0097	
	F88	AAA3		63	0097	33	0042	0025	
	SMI	AAA2B		64	0025	46	0028	0029	
	STU	AAA2		65	0029	21	0042	0795	
	RAU	AAA4		66	0795	60	0008	0063	
	FMP	AAA9		67	0063	39	0816	0866	
AAA28	STU	AAA4	AAA6	68	0866	21	0008	0030	
	RAU	AAA2		69	0028	60	0042	0797	
	F88	AAA10		70	0797	33	0851	0077	
	SMI	AAA11		71	0077	46	0880	0881	
	STU	AAA2		72	0881	21	0042	0844	
	RAU	AAA4		73	0845	60	0008	0813	
	FMP	AAA18		74	0813	39	0516	0966	
	STU	AAA2	AAA2R	75	0966	60	0008	0814	
AAA11	RAU	AAA2		76	0080	60	0042	0847	
	LOO	AAA4	AAA17	77	0847	69	0011	0804	
	FMP	AAA4		78	0901	39	0008	0058	
	STU	AAA13		79	0058	21	0012	0015	
	RAU	AAA14		80	0015	60	0011	0052	
	SMI	AAA18		81	0052	46	0012	0119	
AAA15	RAL	AAA13	AAA1	82	0019	65	0012	0054	
	RAU	AAA1		83	0018	60	0048	0803	
	FOW	AAA13		84	0803	34	0042	0062	
	RAL	8003	AAA1	85	0062	65	8003	0054	
AAA17	STU	AAA18		86	0054	60	0042	0804	
	RAU	AAA3		87	0010	60	0048	0833	
	FAC	AAA2		88	0853	32	0042	0069	
	STU	AAA19		89	0069	21	0008	0059	
	RAU	AAA27		90	0827	60	0830	0035	
	STU	AAA20		91	0035	21	0040	0043	
	RAU	AAA21		92	0043	21	0042	0031	
	STU	AAA2		93	0051	60	0042	0897	
	FMP	AAA2		94	0897	39	0042	0092	
	STU	AAA23	AAA22	95	0092	21	0042	0039	
AAA22	FOW	AAA21		96	0049	34	0098	0798	
	STU	AAA24		97	0798	21	0052	0055	
	FOW	AAA19		98	0055	32	0052	0031	
	STU	AAA19		99	1001	21	0024	0877	
	RAU	AAA24		100	0877	60	0052	0857	
	FOW	AAA19		101	0857	34	0097	0034	
	F88	AAA25		102	0074	33	0927	0903	
	SMI	AAA25	AAA26	103	0903	46	0056	0907	
	RAU	AAA19	AAA18	104	0056	60	0024	0007	

AAA26	RAU	AAA20		105	0907	60	0040	0895
	FAD	AAA20		106	0895	32	0040	1078
	STU	AAA20	NEW N	107	0075	21	0040	0093
	FMP	AAA21		108	0093	39	0098	0848
	STU	AAA21	NEW DENOM	109	0848	00	0040	2511
	FMP	AAA23		110	0051	60	0046	1101
	STU	AAA23		111	1101	39	0042	0792
AAA3	FMP	0000	AAA22	112	0792	20	0000	0949
AAA5	STU	0000	0081	113	0081	10	0000	0051
AAA7	FAD	8413	0081	114	0801	80	0000	0051
AAA9	STU	1838	FIVE	115	0813	04	0012	1101
AAA10	FAD	0000	E TO S	116	0813	27	1828	1851
AAA12	STU	2140	0080	117	0851	20	0000	0050
AAA16	FAD	0000	POINT TWO	118	0912	00	0000	0000
AAA20	STU	0000	E TO PT W	119	0912	00	0000	0000
AAA27	FAD	0000	ZERO	120	0927	10	0000	0047
EODCL	STU	0000	CRITERIA	121	0830	20	0000	0051
	LDD	ZZZ10	TWO	122	1153	24	0554	0957
	STU	1977		123	0957	69	0060	0863
	STU	1979		124	0863	24	1977	0880
	STU	1980		125	0880	24	1978	0831
	STU	1981		126	0831	24	1979	0032
	STU	1982		127	0032	84	1980	0033
	STU	1983		128	0033	24	1982	0014
	STU	1983		129	0034	24	1982	0885
	STU	0000	ZZZ1	130	0885	24	1983	0036
	STU	0000	0000	131	0036	24	1984	0854
	STU	0002	0000	132	0060	00	0000	0000
	STU	0002	0000	133	1201	14	0000	1077
	STU	0002	0000	134	1007	60	8002	0815
	STU	0002	0000	135	0818	46	0068	0819
	STU	0002	0000	136	0818	32	0071	0947
	STU	0002	0000	137	0947	46	0068	1251
	STU	0002	0000	138	1251	33	0954	0881
	STU	0002	0000	139	0819	33	0819	0977
	STU	0002	0000	140	0997	46	1301	0819
	STU	0002	0000	141	1301	32	0954	0881
	STU	0002	0000	142	0881	21	0868	0839
	STU	0002	0000	143	0039	61	0842	1047
	STU	0002	0000	144	1047	21	0802	0805
	STU	0002	0000	145	0805	20	0067	0020
	STU	0002	0000	146	0913	20	0067	0020
	STU	0002	0000	147	1351	24	0904	1057
	STU	0002	0000	148	1057	60	1057	0869
	STU	0002	0000	149	0865	46	0818	0869
	STU	0002	0000	150	0818	32	0071	1097
	STU	0002	0000	151	1097	46	1097	1401
	STU	0002	0000	152	1401	33	0954	0931
	STU	0002	0000	153	0869	33	0071	1147
	STU	0002	0000	154	1147	14	147	0849
	STU	0002	0000	155	1451	32	0954	0931
	STU	0002	0000	156	0931	21	0086	0089
	STU	0002	0000	157	0089	61	0086	1577
	STU	0002	0000	158	1197	21	0802	0855
	STU	0002	0000	159	0855	21	0810	0953
	STU	0002	0000	160	0953	69	0953	0845
	STU	0002	0000	161	0945	24	0067	0020
	STU	0002	0000	162	0020	60	0067	0821
	STU	0002	0000	163	0821	32	0842	0919
	STU	0002	0000	164	0919	21	0824	0977
	STU	0002	0000	165	0977	32	0842	0969
	STU	0002	0000	166	0969	21	0067	0070
	STU	0002	0000	167	0070	61	0802	1107
	STU	0002	0000	168	1107	39	0086	0836
	STU	0002	0000	169	0836	39	0086	0866
	STU	0002	0000	170	0886	34	0824	0874
	STU	0002	0000	171	0874	34	0067	0817
	STU	0002	0000	172	0817	21	0802	0905
	STU	0002	0000	173	0905	67	0810	0915
	STU	0002	0000	174	0915	20	1019	0022
	STU	0002	0000	175	0022	67	0022	1577
	STU	0002	0000	176	1157	60	8002	0965
	STU	0002	0000	177	0965	34	1019	1069
	STU	0002	0000	178	1069	33	0072	0099
	STU	0002	0000	179	0099	46	0852	0953
	STU	0002	0000	180	0953	60	0810	1015
	STU	0002	0000	181	1015	10	0819	0909
	STU	0002	0000	182	0079	21	0810	0020
	STU	0002	0000	183	0852	65	0810	0904
	STU	0002	0000	184	0072	10	0072	0043
	STU	0002	0000	185	0071	62	8318	5351
	STU	0002	0000	186	0954	31	1559	2751
	STU	0002	0000	187	0842	10	0042	0051
	STU	0002	0000	188	1501	24	1004	1207
	STU	0002	0000	189	1207	46	0860	0811
	STU	0002	0000	190	0811	31	0842	1044
	STU	0002	0000	191	0064	21	0868	0871
	STU	0002	0000	192	0871	32	0924	1551
	STU	0002	0000	193	1551	39	1054	1044
	STU	0002	0000	194	1104	21	0808	0861
	STU	0002	0000	195	0861	60	0861	0033
	STU	0002	0000	196	0023	34	0808	0858
	STU	0002	0000	197	0858	32	0808	0835
	STU	0002	0000	198	0835	39	1054	1144
	STU	0002	0000	199	1154	33	0808	0885
	STU	0002	0000	200	0885	44	0839	0090
	STU	0002	0000	201	0839	46	0839	0900
	STU	0002	0000	202	0892	32	0808	0936
	STU	0002	0000	203	0935	21	0808	0861
	STU	0002	0000	204	0861	00	0000	1004
	STU	0002	0000	205	0860	01	0000	1004
	STU	0002	0000	206	1054	50	0000	0050
	STU	0002	0000	207	0050	09	024	0051
	STU	0002	0000	208	1601	24	1804	1257

MZE		LMX14	209	1257	45	0910	0911
SMI	LMX14		210	0910	06	0911	0914
STU	LMX09		211	0814	21	0910	0921
RSL	FPONE		212	0921	66	0842	1247
STO	LMX10		213	1247	24	1655	1254
STL	LMX09		214	1874	20	0049	0812
RAU	LMX09		215	0812	60	0915	0073
STL	LMX05		216	0073	20	1027	0930
STL	LMX11		217	017	20	0930	0939
STL	0008		218	0030	33	0008	1307
STP	FIFTY		219	1307	11	0960	1065
MZE		LMX04	220	1065	45	0829	0935
SMI		LMX03	221	0968	46	0971	0822
RSU	8003		222	0971	61	8003	0829
LDO	FPONE		223	0829	69	0042	0922
STO	LMX05	LMX03	224	0095	24	0009	0822
ORT	0008		225	0822	30	0008	0841
ACT	0000		226	0041	36	0000	1013
AUP	81XTY		227	1013	10	1200	0955
STU	8002		228	0955	11	8003	1063
STU	LMX05		229	1063	60	8003	1021
RAU	8003		230	1021	39	0009	0059
FMP	LMX02		231	0059	39	0862	0912
FMP	LMTEM		232	0912	21	1027	1119
STU	LMX05	LMX04	233	0912	65	0918	0823
RAL	LMX09		234	0823	30	0002	0879
ORT	0002		235	0879	60	0002	0087
RAU	8002		236	0087	15	0960	1115
ALO	FIFTY		237	1115	35	0002	1079
STU	0002		238	1079	32	0842	1169
F40	FPONE		239	1169	21	0918	1121
STU	LMX09		240	1121	35	0977	1041
F88	FP TWD		241	1041	34	0718	1018
STU	LMX09		242	1018	21	0872	0825
STO	LMX12		243	0825	24	0078	0811
STO	LMX11		244	0811	34	0985	0088
FMP	0001		245	0088	39	8001	0091
STU	FACTR	LMX06	246	0091	21	0096	0079
RAU	LMX10		247	0799	60	0799	1005
FMP	FACTR		248	1005	32	0974	1751
STU	LMX10		249	1751	21	1651	1314
STU	LMX10		250	1314	60	0304	1077
RAU	LMX10		251	1077	39	0096	0796
FMP	FACTR		252	0796	34	1651	1041
FOV	LMX10		253	1041	21	1802	0875
STU	LMX13		254	0875	32	0078	1055
STU	LMX12		255	1055	21	0078	1055
FOU	LMX11		256	1033	33	0985	0961
F88	LMX11		257	0961	34	0985	1035
F88	LMX11		258	1035	67	8003	0793
RAM	8003		259	0793	60	0793	1851
RAU	8002		260	1851	33	1354	1081
F88	SIZE7		261	1081	46	0084	1085
STU	LMX12		262	0085	69	0078	1122
RAU	LMX11		263	1131	24	0985	0838
STO	LMX12		264	0838	60	0872	1127
STU	LMX13		265	1127	39	1651	0902
FMP	LMX10	LMX06	266	0902	21	0872	0799
RAU	LMX12		267	0084	60	0078	0883
FMP	FACTR		268	0083	39	0974	1024
F88	LMX0	LMX08	269	1024	33	1027	1204
FPONE	10	0000	270	0842	10	0000	0051
FP TWD	20	0000	271	0974	20	0000	0051
SIZE7	20	0000	272	1354	10	0000	0043
LMTEM	23	0258	273	0862	23	0258	5151
FIFTY	50	0000	274	0860	50	0000	0000
STXTV	00	0000	275	1200	00	0000	0060
LMX14	01	2345	276	0911	0	2345	0678
START	RD	951	277	1000	70	1351	0922
	LDO	1951	278	0952	69	1951	1404
	STO	DATA	279	1404	24	240	1105
	STO	DATA	280	1010	69	1952	1105
	STO	ELEV	281	1105	24	0908	1011
	RAC	0000	282	1011	80	0000	0077
	LDO	DATA	283	0867	69	1557	1040
	RAA	8001	284	1060	80	8001	1016
	RCB	1951	285	1016	79	1951	1002
	LDO	1951	286	1002	69	1951	1454
	LDO	0100	287	1454	24	2100	1003
	LDO	1952	288	1003	69	1952	1003
	STO	0200	289	1150	24	2800	1053
	LDO	1953	290	1053	69	1953	0806
	STO	0300	291	0806	24	2800	1103
	STO	0001	292	1103	51	0001	0809
	STO	READ	293	0809	40	1016	1113
	LDO	FP1	294	1113	69	1850	1151
	STU	N	295	1850	24	0066	0859
	STO	N	296	0859	24	0675	0828
	LDO	ZERO	297	1850	69	0675	1203
	LDO	BT EG	298	1850	24	0906	0909
	LDO	DATA	299	0909	69	1357	1110
	RAA	8001	300	1110	80	0675	1066
	RAA	X	301	1066	60	2200	1205
	FMP	M	302	1205	39	0856	0956
	FMP	P	303	0956	39	1350	1058
	FMP	P	304	1058	34	0000	1102
	RAL	8003	305	1102	65	8003	0959
	LDO		306	0959	69	0675	1203
	STL	TEMP1	307	0962	20	0917	0820
	RAU	V	308	0820	60	2300	1255
	FMP	N	309	1255	39	0675	0928
	FMP	P	310	0925	39	1350	1152
	FDV	B	311	1152	34	0001	1208

DATA POINT

FLUX

X

Y

READO

A

A

CONT1

LOOP1

A

EODCR

A

	RAL	8003			312	1202	65	8003	1009
	LDD		EUOCH		313	1009	69	1012	1201
	RAU	8002			314	1012	60	8002	1271
	FMP	TEMP1			315	1171	39	1171	1167
	STU	FUNCT	A		316	0967	39	2100	1252
	STA	0001		CALCULATE	317	1252	21	2400	1253
	NZL	LOOP1	CONTR	FUNCTIONS	318	2053	51	2053	1259
	RAU	DATA			319	1059	40	1066	1163
CONT2	MPY	FIVE			320	1163	60	1357	1061
	STL	SIUFR			321	1061	61	1050	0970
	RTO	SIUFR			322	0870	14	1050	1160
	LDD	FUNCT	LOOP2		323	1160	20	1165	1068
	STA	0001		DISTRIBUTE	324	1068	69	1068	1118
LOOP2	MPY	FIVE	A	SIMPSON	325	1118	80	8001	1074
	RAU	DATA		FUNCTIONS	326	1074	69	2400	1303
	STL	SIUFR			327	1303	24	2500	1353
	RTO	SIUFR			328	1353	51	0001	1109
	LDD	FUNCT	CONTR		329	1109	40	1074	1213
	STA	0001			330	1213	60	1165	1219
CONTR3	MPY	EIGHT			331	1219	19	1100	0920
	OIV	TEM			332	0920	14	1150	1210
	STL	0004			333	1210	35	0004	1221
	ALO	INDXA			334	1221	15	1750	1305
	LDD	AONE			335	1305	69	0958	1111
	STA	AONE			336	1111	22	0958	1161
	RAU	DATA			337	1161	60	1357	1211
	MPY	TWO			338	1211	19	0850	0970
	DIV	SIX			339	0970	14	1050	1260
	LDD	8002			340	1260	69	8002	1017
	RAA	8001	AONE		341	1017	80	8001	0958
	LDD	9999		DISTRIBUTE	342	0958	69	9999	1302
	STU	TRAPF	A	TRAP	343	1302	24	2600	1403
	STA	0001		FUNCTIONS	344	1403	51	0001	1159
	NZA	ADNE	CONTR		345	1159	40	0958	1263
CONTR4	RAL	SIUFR			346	1263	65	1165	1269
	OIV	FIVE			347	1269	14	0950	1310
	STL	OIAM			348	1310	20	1210	1168
	ALO	TWO			349	1168	15	0850	1355
	STL	CIN01			350	1355	20	1209	1062
	RAU	SIUFR		SET INDEX	351	1062	60	1165	1219
	MPY	THREE		REGISTERS	352	1219	19	0900	1020
	OIV	FIVE		FOR	353	1020	14	0950	1360
	ALO	TWO		SIMPSON	354	1360	15	0850	1112
	STL	CIN02		RULE	355	1112	20	1259	1112
	RAL	DATA			356	1112	65	1357	1261
	DIV	81X			357	1261	14	1050	1455
	SLO	ONE			358	1410	16	0800	1455
	STL	CELLS			359	1455	20	1309	1162
	LDD	CIN01	LOOP3		360	1162	69	1209	1212
	RAU	8001			361	1212	80	8001	1212
LOOP3	RAU	SIMPFF	A		362	1218	60	2500	1505
	FMP	FP16			363	1505	39	1600	1556
	FAD	INTFC			364	1352	31	0906	0933
	STU	INTEC			365	0833	21	0906	1359
	STA	0001			366	1359	51	0001	1265
	RAU	SIMPFF	A		367	1265	50	0002	1311
	AXA	0002			368	1555	32	2500	1177
	FAO	SIMPFF	A		369	1311	32	2500	1177
	STA	0001			370	1177	50	0001	0883
	LDD	OIAM			371	0883	69	1215	1268
	STA	8001			372	1268	52	8001	1124
	FAO	SIMPFF	A		373	1124	32	2500	1227
	LDD	OIAM			374	1227	69	1215	1318
	AXA	8001			375	1318	50	8001	1174
	FAO	SIMPFF	A		376	1174	60	0001	0980
	LDD	OIAM			377	0980	32	2500	1277
	FMP	FP4			378	1277	39	1400	1402
	FAD	INTEC			379	1402	69	0906	0933
	STU	INTEC			380	0933	21	0906	1409
	AXA	0001			381	1409	50	0001	1315
	RAU	SIMPFF	A		382	1315	60	2500	1025
	STA	0002			383	1605	51	0002	1361
	FAO	SIMPFF	A		384	1361	32	2500	1327
	LDD	OIAM			385	1327	69	1215	1368
	STA	8001			386	1368	51	8001	1224
	AXA	8001			387	1224	51	8000	1030
	FAO	SIMPFF	A	CELL	388	1030	37	0000	0777
	AXA	0002		CALCULATNB	389	0983	50	0008	0983
	FAO	SIMPFF	A	FOR	390	0983	32	2500	1177
	FAD	INTEC		SIMPSONS	391	1033	69	1215	1033
	STU	INTEC		RULE	392	1033	21	0906	1459
	LDD	OIAM			393	1459	69	1215	1459
	STA	8001		CHECK	394	1418	51	8001	1274
	AXA	0001		CELLS	395	1874	51	0001	1080
	SMA		CONTS	REMAINING	396	1080	41	1080	1212
	LDD	CIN02	LOOP3		397	1083	69	1209	1212
CONTS	RAL	CELLS			398	0834	65	1309	1333
	SLO	TWO			399	1333	69	1209	1363
	STL	CELLS			400	1263	16	1309	1262
	SZZ		CONTR		401	1262	45	1116	1067
	RAL	CIN01			402	1116	69	1209	1363
	ALO	TWO			403	1363	15	0850	1705
	STL	CIN01			404	1705	20	1209	1312
	RAL	CIN02		ADJUST TO	405	1312	61	1253	1333
	ALO	TWO		NEXT CELL	406	1056	15	0850	1755
	TTL	CIN01		SET	407	1755	20	1259	1362
	LDD	DATA	LOOP3		408	1362	69	1209	1411
	RAU	DATA			409	1069	60	1357	1411
CONTR6	SCT	0000			410	1411	36	0000	1133
	STL	TEMP3		CONVERT	411	1070	20	0933	1070
	LDD	TEMP1		ROWS TO	412	1070	65	8003	1477
	SLO	SIXTY		FLOATING	413	1477	15	1200	1805
	RAL	DATA		POINT	414	1805	16	0850	1171
	RAU	8002			415	1271	60	8002	0929

FOV	FP6		416	0929	34	1450	1452
FSB	FP1		417	1452	33	1450	1527
STU	ROWB		418	1527	31	0082	1135
RAU	A		419	1135	60	0000	1855
FOV	FP2		420	1300	34	1300	1502
FOV	ROW8		401	1502	34	0082	0832
FMP	FP8		422	0832	39	1500	1552
FOV	FP9		423	1552	34	1550	1400
FMP	INTEG		424	1602	39	0906	1006
STU	INTEG	CONT7	425	1006	31	0906	1509
RAU	PI		426	1509	34	1500	1461
01Y	81X		427	1461	14	1050	1460
STL	INDEX		428	1460	20	1345	1468
ZLT	0004	SET	429	1468	35	0904	1529
ALO	INDA	DATA	430	0979	15	1800	1056
LOO	ATWO	ADDRESSES	431	1066	69	1559	1412
80A	ATWO	FOR	432	1412	22	1465	1462
LOO	ATREE	TRAP RULE	433	1462	69	1415	1518
8DA	ATREE		434	1518	82	1415	1568
RAL	INOB		435	1568	65	1850	1106
LOO	8ONE		436	1106	69	1609	1512
NOA	8ONE		437	1512	22	1609	1568
LOO	8TWO		438	1562	69	1465	1618
80A	8TWO		439	1618	22	1465	1668
RAU	B		440	1668	60	0001	1156
FOV	FP2		441	1156	34	1300	1652
F88	8PRIM		442	1652	33	0008	1029
FMP	ROW8		443	1029	39	0082	0888
FOV	FP4		444	0882	34	1400	1702
STU	FACTR		445	1702	21	0996	0849
LOO	INDEX		446	0849	69	1345	1718
RAA	8001		447	1718	80	8011	1324
RAB	8001	ATWO	448	1324	82	8001	1559
RAU	9999	8ONE	449	1559	60	9999	1609
STU	9999		450	1609	32	9999	1975
8XA	0001		451	0975	51	0001	1181
8X8	0001	CALCULATE	452	1181	53	0001	0937
RAA	ATREE	TRAP RULE	453	0937	40	1405	1751
FAO	9999	INTEGRAL	454	1415	32	9999	1465
FAO	9999	STWO	455	1465	32	9999	1025
FAO	TR		456	1025	39	0082	0846
FAO	INTEG		457	0846	32	0906	1183
STU	INTEG	ATWO	458	1183	21	0906	1559
STU	INTEG		459	1559	60	0791	1511
FMP	FP4		460	1511	39	1400	1752
STU	INTEG		461	1752	21	0906	1669
RAU	M		462	1669	60	0856	1561
F88	N		463	1561	33	0675	1808
NZE	INTEG	CONT9	464	1808	45	1206	1407
RAU	INTEG		465	1206	60	0266	1611
FMP	FP2		466	1611	39	1300	1852
STU	INTEG	CONT9	467	1852	21	0906	1407
STU	INTEG		468	1407	68	0011	1633
LOO	INTEG		469	1463	69	0906	1709
STO	F8N		470	1709	24	6770	0873
STO	8007	C	471	0873	69	0807	1079
STO	TERM8	COUNT	472	1079	24	0932	1185
RAU	HARM	TERUS	473	1185	60	0003	1457
F88	M		474	1457	33	0856	1233
NZE	M		475	1233	45	0936	0887
RAU	M	CON10	476	0936	60	0856	1661
FAO	FP2		477	1661	32	1300	1577
STU	M	CONT1	478	1577	21	0856	0828
RAU	HARM	ADJUST	479	0887	60	0003	1507
F88	M	M ANU N	480	1507	33	0675	1453
NZE	M		481	1453	45	1256	1557
RAU	N	CON11	482	1556	60	0675	1129
FAO	FP2		483	1129	32	1300	1627
STU	N		484	1627	21	0856	1759
STU	N	CONT1	485	1759	21	0675	0828
LDO	FIRST		486	1557	69	0004	1607
STO	0011		487	1607	84	1510	1513
STO	GAMMA		488	1513	24	0730	1283
LDO	FP1	CON23	489	1283	69	1283	1503
STO	N		490	1503	24	0856	1809
STO	N		491	1809	24	0675	0878
FOV	PI		492	0878	60	0856	1306
FMP	8003		493	1306	34	0000	1553
STU	ALPH2		494	1553	39	8003	1657
RAU	PI		495	1657	21	1612	1815
FOV	B		496	1815	60	1350	1356
STU	8003		497	1356	34	0001	1603
STU	BETA2		498	1603	39	8003	1707
RAU	GAM11		499	1707	21	1662	1565
FMP	8003		500	1565	60	1510	1615
F88	ALPH2		501	1615	39	8003	1599
F88	BETA2	CALCULATE	502	1599	33	1612	0889
STU	KAPPA	KAPPA	503	0889	33	1662	0939
STO	8001	SQUARED	504	0939	21	0044	1627
LOO	GAM11		505	1627	88	0001	1653
STO	8004		506	1653	69	1310	1563
STO	8004		507	1563	24	6730	1333
AKC	0001	C	508	1333	33	0001	1677
RAU	M		509	1677	58	0001	0989
STU	FP2		510	0989	60	0856	1711
FMP	PI	LOOPA	511	1711	32	1300	1677
FOV	A		512	1677	39	1350	1703
STU	8003		513	1703	34	0000	1753
STU	ALPH2		514	1753	39	8003	1757
RAU	N		515	1757	21	1612	1665
FMP	PI		516	1665	60	0675	1179
FOV	8		517	1179	39	1350	1803
FMP	8003		518	1803	34	0001	1853
			519	1853	39	8003	1807

FAD	KAP30			519	1807	32	0044	1321
FAD	ALPH2			520	1810	32	0044	1321
LOD		EOOAU	CALCULATE	521	1039	69	0942	1501
STU	GAMMA	C	GAMMA MN	522	0942	21	6730	1383
AXC	0001			523	1544	33	1008	1859
RAU	NARU			524	1089	60	0003	1857
FBB	W			525	1857	33	0856	1433
MZE		CON12		526	1433	25	0836	0937
RAU	W			527	0986	60	0856	1761
FAD	FP2			528	1761	32	1300	1727
STU	W	LODPA		529	1727	32	1566	1277
FBB	NARU			530	0937	60	0003	1008
MZE				531	1008	33	0675	1504
RAU	N	CON13		532	1504	25	1054	1829
FAD	FP2			533	1058	60	0675	1229
STU	W			534	1229	32	1300	1777
STU	W	LOOPA		535	1777	21	0856	1560
NZR	CON15			536	1560	21	0675	1677
LOD	TERMS			537	1859	42	1712	1613
RAC	8001	LOOPB	LOOPB	538	1613	69	0932	1235
RSU	C			539	1235	88	8001	0841
FAD	ELEV			540	0841	61	0007	1811
FMP	GAMMA	C		541	1811	32	0908	1285
RAL	ARG			542	1285	39	6730	1130
LOD		EOOEA		543	1130	31	0884	0987
OTL	TEMP1			544	0987	65	0884	1139
RAM	ARG	EOOEA		545	1139	69	0992	0051
LOD				546	0992	20	0917	1120
RAU	8002			547	1120	67	0884	1189
F88	TEMP1			548	1189	69	1042	0051
FMP	B			549	1048	60	8002	1554
STU	TEMP1	C		550	1554	33	0954	0843
FMP	B			551	0843	39	0000	1604
STU	TEMP1			552	1604	39	0001	1654
RAU	FPB			553	1654	61	0917	1170
FMP	FNN	C		554	1170	60	1500	1406
STU	TEMP1			555	1406	39	6770	1220
FWD	TEMP1	C	CALCULATE	556	1220	34	0920	1277
STU	AMN		AMN	557	1117	21	6750	1704
SXC	0001	CON14		558	1704	59	0001	1610
NZC	LOOPB			559	1610	48	0610	0864
RHP	0008			560	0864	88	0008	1870
LOD	LOOPC	EOOCL		561	1270	69	0923	1151
LOD	AMN	C		562	0923	69	0923	1364
STD	1976			563	1754	24	7976	1879
SXC	0001	C		564	1279	59	0001	1335
NZC	LOOPC			565	1335	48	0535	1489
PCH	1977		PUNCH	566	1239	71	1977	1827
RAL	TERMS		CONSTANTS	567	1827	65	0932	1037
8LO	EIGHT			568	1103	16	1103	1666
8HL	CON15			569	1456	46	1712	1660
LOD	TERMS			570	1460	69	0932	1385
RAC	8001	CON25		571	1385	88	8001	0921
LOD	AMN	C		572	0891	69	6750	1804
STD	1968	C		573	1804	24	7968	1371
8XC	0009			574	1371	89	0009	1377
NZC	CON24			575	1877	48	1180	1231
PCN	1977	CON15		576	1231	71	1977	1712
AXC	0008	CON25		577	1180	58	0008	0891
LOD	POINT			578	1712	69	0005	1108
RAA	8001			579	1108	80	8001	0914
RAB	0001	LOOPD		580	0914	82	0001	1320
LOD	TERMS			581	1320	69	0932	1435
RAC	8001			582	1435	88	8001	0941
LOD	ZERO	LOOPE		583	0941	69	0050	1854
STO	COFAC			584	1854	24	1158	1861
RAU	GAM11			585	1861	60	1510	1715
FMP	Z	A		586	1715	39	2650	1066
STU	TEMP1			587	1506	21	0917	1370
RAU	C			588	1370	60	0007	1762
FBB	Z			589	1762	33	2650	0988
FMP	GAMMA	C		590	0928	39	6730	1230
FAD	TEMP1			591	1230	32	0917	0893
RAL	8003			592	0893	65	8003	1566
LOD		EOOEA		593	1556	69	1710	0051
RAU	8002			594	1710	60	8002	1449
FMP	AMN	C		595	1449	39	6750	1606
STU	TEMP1			596	1606	34	1300	1656
RBU	C			597	1656	21	0917	1420
FAD	Z	A		598	1420	61	0907	1812
FMP	GAMMA	C		599	1812	32	2650	0978
FMP	FPB			600	0978	39	6730	1280
RAL	8003			601	1280	39	1300	1706
LOD		EOOEA		602	1706	65	8003	1663
RSU	8002			603	1663	69	1166	0051
FAD	FP1			604	0051	61	8066	1475
STU	ENOCO		CALCULATE	605	1075	32	1250	1028
FMP	TEMP1		END AND	606	1028	21	0982	1485
FAD	COFAC		HARMONIC	607	1485	39	0485	1877
STU	COFAC		FACTOR	608	1167	32	1158	1535
SXC	0001			609	1535	21	1158	1862
NZC	0002			610	1862	59	0062	5988
RAU	N	CON16		611	1768	48	1861	0922
FAD	COFAC	A	CALCULATE	612	0922	60	2675	1328
STU	NFOR		CORRECTO	613	1328	34	1158	1078
LOD	Z	A	DATA	614	1808	21	2700	1756
LOD	Z	A	EOOCL	615	1756	69	1760	1151
STD	1977			616	1151	89	2675	1078
LOD	N	A		617	1806	24	1977	1330
STD	1978		PUNCH DATA	618	1330	69	2675	1078
LOD	NFOR	A	AND	619	1078	61	1978	1281
STD	1979	A	CORRECTION	620	1281	69	2700	1856
				621	1856	24	1979	1032

	LOB	C8FAC		FACTOR	622	1038	69	1158	1713
	8TO	1980			623	1713	24	1980	1483
	LOB	ENR88			624	1483	69	1088	1588
	8TO	1981			625	1588	24	1981	0934
	PCN	8001			626	8933	71	1977	1128
	STA	0001			627	1128	84	1088	0840
CON17	NZA	LO8P8	C8N17		628	09884	40	1320	0888
	LOB	POINT			629	08888	69	80885	1258
	8TO	R001			630	1258	84	1088	0840
	LOB	IERS			631	0964	69	0050	1308
	8TO	SUMA			632	1308	24	1763	1308
	WTO	SMLNA			633	1216	24	1088	0932
	8TO	SUM2			634	0978	24	1125	1178
	8TO	SUM28			635	1178	24	1331	1034
	8TO	Z8MLA			636	1034	24	1088	0840
LOBPF	WAU	NCOR	A	LOBPF	637	0840	68	2708	1358
	F88	WUMA			638	1358	32	1763	1289
	8TO	SUMA			639	1889	81	1763	1266
	RAU	NCOR	A		640	1266	60	2700	1488
	LOB	SMLNA		LNK01	641	1813	69	1813	1601
	8TO	SMLNA			642	1413	32	1469	1045
	8TO	SMLNA			643	1045	21	1469	1822
	WAU	Z	A		644	1028	68	2458	1458
	F88	SUM2		FORM SUMS	645	1458	32	1125	1228
	8TO	SUM2		FBR LEAST	646	1508	21	1125	1228
	RAU	Z	A	SQUARES	647	1228	68	2458	1508
	FMP	Z	A	ANALYSIS	648	1538	39	2650	1608
	FAD	SUM22			649	1688	32	1331	1458
	8TO	SUM28			650	1658	28	1331	1084
	RAU	NCOR	A		651	1658	60	1038	1084
	LOB	Z	A	LNK01	652	1708	69	1863	1681
	FMP	Z	A		653	1863	39	2650	1758
	8TO	Z8MLA			654	1758	32	1758	1644
	8TO	Z8MLA			655	1814	21	1887	0890
	8XA	0001			656	0890	32	8888	0896
	NZA	LOBPF		CON18	657	0896	40	1088	0932
	RAU	SMLNA			658	1888	68	1469	8973
	FMP	SUM2			659	0978	39	1428	1475
	WAU	TEMP1			660	1173	21	1173	1178
	WAU	SATPT			661	1478	60	00886	1864
	8TO	Z8MLA			662	1064	39	1088	1337
	8TO	TEMP2			663	1177	23	1198	1095
	RAU	QATPT			664	1095	40	00066	1114
	FMP	SUM22			665	1114	39	1331	3588
	8TO	TEMP3			666	1381	21	1381	1339
	RAU	SUM2			667	1339	60	1125	1379
	FMP	SUM2			668	1379	39	1388	1223
	8TO	TEMP4			669	1225	21	1388	0991
	8TO	TEMP3			670	1533	68	1036	0991
	F88	TEMP4			671	8988	33	1388	1388
	8TO	TEMP3			672	1038	21	1038	1388
	8TO	TEMP1			673	1389	60	8917	1421
	F88	TEMP2			674	1421	33	1098	1119
	F88	TEMP3			675	1421	34	1836	1086
	8TO	NWCAM			676	1886	21	0940	8943
	F88	10000			677	8943	34	17943	1340
	F88	PREC			678	1810	21	1164	1217
	RAU	CAM13			679	1217	60	1510	1765
	F88	NWCAM			680	1765	33	0940	1267
	RAU	8003			681	1267	67	8883	1583
	F88	8002			682	1275	60	8088	1583
	SMI	C8N00		CON19	683	1583	33	1164	1841
	RAU	NWCAM			684	1041	46	0094	1145
	8TO	CAM11		CON23	685	1145	60	0940	1195
	WTO	CAM11			686	1195	21	1510	1283
	WAU	NWCAM			687	0894	68	0940	1245
	FMP	NWCAM		CAMMA	688	1245	39	0940	0998
	8TO	CAM59		SQUARES	689	0990	21	0794	1347
	WAU	PI			690	1347	60	1350	1860
	F88	8003		ALPHA	691	1860	34	0080	1214
	8TO	ALPN2		SQUARES	692	1317	39	0214	3577
	RAU	PI			693	1815	21	0618	1815
	F88	8003		BETA	694	1815	60	1350	1264
	F88	8003		SQUARES	695	8645	60	0080	1344
	WTO	BETA2			696	1314	39	8003	1367
	RAU	CAM80			697	1367	21	1662	1865
	F88	ALPN2		KAPPA	698	1865	21	1662	1865
	F88	BETA2		SQUARES	699	0899	33	1612	1439
	8TO	KAPPA			700	1439	33	1662	1489
	8TO	KAPPA		EOOAU	701	1489	69	1489	1601
	RAU	FP1			702	1148	21	0946	0949
	F88	KAPPA			703	0949	60	1250	1364
	FMP	CONVT		DIFFUSION	704	1364	34	1364	0933
	8TO	OL		LENGTH	705	1414	21	1818	1471
	8TO	0000			706	1471	81	1977	1378
	LOB	FIRST		EO8CL	707	1278	69	1431	1151
	8TO	1977			708	1431	69	0004	1464
	8TO	CAM11			709	1464	84	1977	1481
	8TO	1978			710	1430	69	1510	1514
	LOB	NWCAM			711	1514	24	1978	1481
	8TO	1979			712	1344	69	1440	0993
	8TO	POINT			713	0993	24	1979	1082
	8TO	1980			714	1082	69	0005	1564
	LOB	OL			715	1564	24	1564	1614
	8TO	1981			716	1633	69	1818	1521
	PCN	1977		CON21	717	1521	24	1981	1134
	WAU	NWCAM			718	1134	84	1977	1481
	F88	10000			719	1388	84	1789	1614
	8TO	CAMMA			720	1417	34	11614	1614
	8TO	NWCAM			721	1417	60	0730	1635
	F88	NWCAM			722	1635	33	0940	1467

	RAM	0003		725	1467	67	8003	1328
	RAU	0009		726	1328	60	8009	1683
	F08	PREC		727	1683	33	1164	1091
CON22	0M1	0000	CON22	728	1091	46	8000	1345
	LOC	HWGAM		729	1345	69	0940	1043
	STO	GAM11		730	1043	24	1510	1664
	STO	GAMNA	CON23	731	1664	24	0730	1883

APPENDIX G

IBM 650 Program for Experimental
Determination of Effective Pile Size

This program was written to determine the effective pile size by an experimental analysis of data taken in a horizontal traverse. The program was written in SOAP II and floating point form. The object program and a logic diagram are included in this section.

The program is based upon the equation

$$\phi(x) = \sum_{m=1}^{\infty} A_m \cos \frac{m \pi x}{a} \quad (G-1)$$

and proceeds as follows:

1. Using an assumed initial value for the effective pile size, a , the constants A_m are evaluated using a least squares analysis.

2. The least squares error is calculated using the equation

$$E^2 = \sum_{i=1}^N \left[A_1 \cos \frac{\pi x_i}{a} + A_3 \cos \frac{3 \pi x_i}{a} + \dots - N_i \right]^2.$$

3. The value of a is increased by an increment Δa and a new set of A_m 's is calculated.

4. A new E^2 is calculated and compared with the old E^2 . If E^2 is found to be decreasing, a is increased again by Δa .

5. If E^2 is increasing, a is decreased by Δa and Δa is divided by two. This process is repeated until Δa is less than a specified precision. The last value of a is then the desired value of extrapolated pile size.

The criterion for determination of a is that E^2 , described above, should be minimized. Input to this program is entirely on one-word load cards and is listed in Table 29.

Table 29. Input to IBM 650 code for determination of effective size.

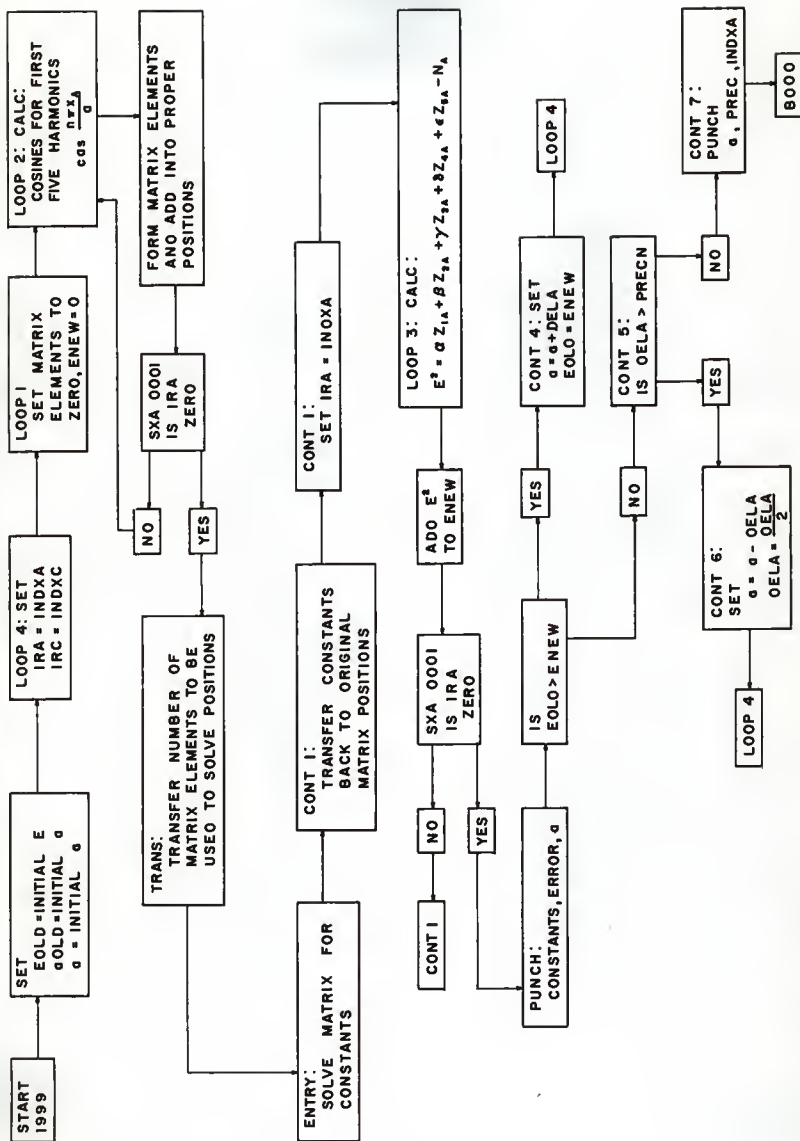
Symbol	Explanation	Drum Storage Location
AINIT	Initial value of a	1000
DELA	Increment Δa	1001
INDXA	Number of Data Points form - 00 0000 00xx	1002
ENN	Number of Harmonics form - 00 0000 000x (2, 3, 4, or 5)	1003
N	BF ₃ Count Rates - to be stored consecutively starting with location	0301
X	Co-ordinates of count rates, to be stored consecutively in location	0201

The capacity of this program is 100 data points. It will perform the analysis using from two to five terms of Eq. (G-1). Output forms for this program are listed in Table 30. Form one is punched after each trial and form two is the final output.

Table 30. Output forms for IBM 650 program
for effective pile size.

Word 1	:	2	:	3	:	4	:	5	:	6	:	7	
Form 1:													
		A_1		A_3		A_5		A_7		A_9		E^2	
Form 2:													
		a		Precision		Number of		Data Points					

The initial estimate of a should always be less than the final answer or the program will not converge. Therefore, the actual size is recommended as an initial estimate since this will always be less than the extrapolated size. Approximately 45 seconds is required for one trial using nine data points.



OBJECT PROGRAM - APPENDIX G

RLR	0000	0030	1	0000	00	0000	0000
HLR	0101	0141	2	0000	00	0000	0000
HLR	0200	0900	3	0000	00	0000	0000
HLR	1951	1960	4	0000	00	0000	0000
HLR	1977	1986	5	0000	00	0000	0000
SYN	Y11	0101	6	0000	00	0000	0000
SYN	Y12	0102	7	0000	00	0000	0000
SYN	Y13	0103	8	0000	00	0000	0000
SYN	Y14	0104	9	0000	00	0000	0000
SYN	Y15	0105	10	0000	00	0000	0000
SYN	Y21	0106	11	0000	00	0000	0000
SYN	Y22	0107	12	0000	00	0000	0000
SYN	Y23	0108	13	0000	00	0000	0000
SYN	Y24	0109	14	0000	00	0000	0000
SYN	Y25	0110	15	0000	00	0000	0000
SYN	Y31	0111	16	0000	00	0000	0000
SYN	Y32	0112	17	0000	00	0000	0000
SYN	Y33	0113	18	0000	00	0000	0000
SYN	Y34	0114	19	0000	00	0000	0000
SYN	Y35	0115	20	0000	00	0000	0000
SYN	Y41	0116	21	0000	00	0000	0000
SYN	Y42	0117	22	0000	00	0000	0000
SYN	Y43	0118	23	0000	00	0000	0000
SYN	Y44	0119	24	0000	00	0000	0000
SYN	Y45	0120	25	0000	00	0000	0000
SYN	Y51	0121	26	0000	00	0000	0000
SYN	Y52	0122	27	0000	00	0000	0000
SYN	Y53	0123	28	0000	00	0000	0000
SYN	Y54	0124	29	0000	00	0000	0000
SYN	Y55	0125	30	0000	00	0000	0000
SYN	Z1	0126	31	0000	00	0000	0000
SYN	Z2	0127	32	0000	00	0000	0000
SYN	Z3	0128	33	0000	00	0000	0000
SYN	Z4	0129	34	0000	00	0000	0000
SYN	Z5	0130	35	0000	00	0000	0000
SYN	ALPHA	0400	36	0000	00	0000	0000
SYN	BETA	0500	37	0000	00	0000	0000
SYN	GAMMA	0600	38	0000	00	0000	0000
SYN	DELTA	0700	39	0000	00	0000	0000
SYN	EPSI	0800	40	0000	00	0000	0000
SYN	H	0300	41	0000	00	0000	0000
SYN	X	0200	42	0000	00	0000	0000
SYN	ALPHA	1000	43	0000	00	0000	0000
SYN	BETA	1001	44	0000	00	0000	0000
SYN	DELTA	1002	45	0000	00	0000	0000
SYN	EPSI	1003	46	0000	00	0000	0000
SYN	ZETA	1999	47	0000	00	0000	0000
ZERO	0000	0000	48	0000	00	0000	0000
TWO	20	0000	49	0100	20	0000	0051
THREE	30	0000	50	0150	30	0000	0051
PI	31	159	51	0930	31	4159	0051
FIVE	50	0000	52	1050	50	0000	0051
SEVEN	70	0000	53	1100	70	0000	0051
NINE	90	0000	54	1150	90	0000	0051
FINIT	10	0000	55	1200	10	0000	0075
PREC	10	0000	56	1250	10	0000	0048
INUXC	100	0000	57	1300	00	0000	0030
FOUCH	ST	EXIT	58	1350	24	0053	0056
	RD	HOOD	59	0056	60	8002	0065
	HI	REGAT	60	0065	46	0068	0069
NEGAT	FAO	TROP	61	0068	32	0071	0047
	HI	NEGAT	62	0047	46	0068	0051
REDUC	FSR	ONEPI	63	0051	33	0154	0031
	FSR	TROP	64	0068	33	0071	0097
	HI	ONEPI	65	0097	46	1400	0069
COSID	ST	THETA	66	1400	32	0154	0031
	RSU	FPONE	67	0031	61	0042	0147
	STU	TERMN	68	0039	61	0042	0147
	STU	FUNKT	69	0147	21	0052	0053
	STL	ENNN	70	0053	20	0067	0070
	STL	ENNN	71	0063	20	0067	0070
EOUSR	STU	EXIT	72	1450	24	0053	0156
	RD	HOOD	73	0156	60	8002	0065
NEGAV	FAO	TROP	74	0165	46	0168	0169
	HI	NEGAV	75	0168	32	0071	0197
	HI	NEGAV	76	0197	46	0168	0151
REDUP	FSR	ONEPI	77	0151	33	0154	0081
	FSR	TROP	78	0169	33	0071	0047
	HI	ONEPI	79	0047	46	0168	0169
SINET	FAO	ONEPI	80	1500	32	0154	0081
	STU	THETA	81	0081	21	0052	0089
	STU	HOOD	82	0089	61	0042	0147
	STU	TERMN	83	0097	21	0052	0153
	STU	FUNKT	84	0153	21	0060	0163
	LOU	FPONE	85	0163	59	0163	0051
	STU	ENNN	86	0045	24	0067	0070
NEGST	RD	ENNN	87	0070	60	8002	0171
	FAO	ONEPI	88	0171	32	0042	0069
	STU	NPONE	89	0042	21	0074	0077
	FAO	FPONE	90	0077	32	0042	0069
	STU	ENNN	91	0069	61	0042	0147
	RSU	TERMN	92	0170	61	0052	0087
	FMP	THETA	93	0057	39	0056	0086
	FOV	NPONE	94	0066	34	0074	0174
	FOV	NPONE	95	0136	34	0074	0174
	FOV	ENNN	96	0174	24	0067	0167
	STU	TERMN	97	0167	21	0052	0089
	RAM	FUNKT	98	0905	67	0060	0915
	STL	FMAG	99	0095	20	0915	0051
	RAM	TERMN	100	0072	67	0052	0157
	RAO	HOOD	101	0157	60	8002	0065
	FOV	FMAG	102	0965	34	1019	1069

FSH	NIZEB		103	1069	33	0172	0049
BMI	ENUFF		104	0049	46	0152	4153
RAU	FUNKT		105	0153	60	0060	1015
FAU	FERMM		106	1015	37	0052	0079
STU	FUNKT		107	0079	21	0060	1070
RAL	FUNKT	EXIT	108	0158	65	0050	0053
ERUFF	10	0000	109	0172	10	0000	0043
NIZEM	10	0000	110	0071	14	0158	0151
TRUMI	31	4159	111	0154	31	4159	0751
UNEMI	10	0000	112	0042	10	0000	0051
FPONL	10	0000	113	1500	24	0050	0066
EGUCL	ZZZ1	0051	114	0906	69	0059	0068
STU	ZZZ10		115	0062	24	1977	0080
STU	1977		116	0080	24	1978	0181
STU	1978		117	0181	24	1979	0032
STU	1980		118	0032	24	1980	0033
STU	1981		119	0033	24	1981	6034
STU	1982		120	0034	24	1982	0035
STU	1983		121	0035	24	1983	0166
STU	1984		122	0146	24	1984	0903
ZZZ10	00	0000	123	0059	60	0000	0000
START	LDU	AINIT	124	1999	69	1000	0953
STU	ACLO		125	0953	24	0056	0159
LDU	FINIT	SET UP	126	0159	69	1200	1053
STU	FULO	CONDITION	127	1053	24	1006	0909
LDU	AINIT		128	0909	69	1000	1103
STU	A		129	1103	24	1036	0959
LOUP4	LDU	INOXA	130	0959	69	1102	0955
RAU	H001	SET	131	0955	40	0001	0061
LDU	INDXC	INOFX	132	0061	69	1300	1153
RAC	H001	REGISTER	133	1153	88	8001	1009
LDU	ZERO		134	0009	69	0000	0000
STU	0100	C	135	1403	24	6100	1253
STU	0000	C	136	1553	24	6000	1303
STU	0001	C	137	1001	59	0001	1059
NZC	LOUP1	CUNTH	138	1059	48	1203	0913
STU	KNEW	LOUPH	139	0913	24	0066	1119
CUNTH	R		140	1119	60	0950	1005
LOUP2	FHP	X	141	1005	39	2200	1600
FVU	TEMP1	A	142	1600	34	1056	1106
STU	TEMP1		143	1106	21	0100	1000
FHP	THREF		144	0963	39	0150	1650
STU	TEMP4	3	145	1650	21	0904	0907
RAU	TEMP1		146	0907	60	0160	1055
FHP	FIVE		147	1065	39	1050	1700
STU	TEMP5	5	148	1700	21	0954	0957
RAU	TEMP1		149	0957	60	0160	1155
FHP	SEVEN		150	1115	39	1100	1750
STU	TEMP4	7	151	1750	21	1004	1007
RAU	TEMP1		152	1007	60	0160	1365
FHP	NINE		153	1165	39	1150	1800
STU	TEMP5	9	154	1800	21	1054	1037
RAL	TEMP1		155	1037	65	0160	1215
LDU		EDUCH	156	1215	69	0918	1350
STL	ALPHA	A	157	0918	20	2400	1353
RAL	TEMP2		158	1353	65	0904	1309
LDL		EDUCH	159	1109	69	0162	1350
STL	BETA	A	160	0162	20	2500	1403
RAL	TEMP3		161	1403	65	0954	1159
LDL		EDUCH	162	1159	69	0912	1350
STL	GAMMA	A	163	0912	20	2600	1453
RAL	TEMP4		164	1453	65	1004	1209
LDL		EDUCH	165	1209	69	0962	1350
STL	DELTA	A	166	0962	20	2700	1503
RAL	TEMP5		167	1503	65	1054	1259
LDU		EDUCH	168	1259	69	1012	1350
STL	EPSIL	A	169	1012	20	2800	1553
RAU	ALPHA	A	170	1553	60	2400	1055
FHP	ALPHA	A	171	1055	39	2400	1850
FAU	Y11		172	1050	32	0101	0177
STU	Y11		173	0177	21	0101	1104
RAU	ALPHA	A	174	1104	30	2400	1050
FHP	BETA	A	175	1105	39	2500	1900
FAD	Y12		176	1900	32	0102	0179
STU	Y12	12	177	0179	21	0179	0955
STU	Y21	21	178	1155	21	0106	1309
RAU	ALPHA	A	179	1309	60	2400	1805
FHP	GAMMA	A	180	1805	39	2500	1950
FAO	Y13		181	1950	32	0103	0929
STU	Y13	13	182	0929	21	0103	1156
STU	Y31	31	183	1156	21	1156	0644
RAU	ALPHA	A	184	0064	60	2400	1255
FHP	DELTA	A	185	1255	39	2700	0901
FAD	Y14		186	0901	32	0101	0177
STU	Y14	14	187	0931	21	0104	1107
STU	Y41	41	188	1107	21	0116	1169
RAU	ALPHA	A	189	1169	30	2600	1305
FHP	EPSIL	A	190	1305	39	2800	0951
FAD	Y15		191	0951	32	0105	0981
STU	Y15	15	192	0981	21	0108	1051
STU	Y51	51	193	1051	21	0121	0924
RAU	BETA	A	194	0924	60	2500	1355
FHP	BETA	A	195	1355	39	2500	1950
FAD	Y22		196	1051	32	0107	0083
STU	Y22	22	197	0083	21	0107	0920
RAU	BETA	A	198	0920	60	2500	1025
FHP	GAMMA	A	199	1405	39	2600	1101
FAD	Y23		200	1101	32	0108	0085
STU	Y23	23	201	0085	21	0108	1021
STU	Y38	32	202	0161	21	0112	1265
RAU	BETA	A	203	1265	60	2500	1453
FHP	DELTA	A	204	1453	39	2700	0151
FAO	Y24		205	1151	32	0109	0135

STU Y#4		24	206	0135	21	0109	1062
STU Y#2		42	207	1062	21	0117	4920
RAU BETA	A		208	0920	60	2800	1805
FNP EPBIL	A		209	1505	39	2800	1201
FAO Y#5			210	1201	32	0110	8037
STU Y#5		25	211	0037	21	0114	8013
STU Y#2		52	212	1013	21	0122	0075
RAU GAMMA	A		213	0075	60	2600	1555
FNP GAMMA	A		214	1555	39	2600	1031
FAO Y33			215	1851	32	0113	4139
STU Y33		33	216	0139	21	0113	4166
RAU GAMMA	A		217	0166	60	2600	1605
FNP OELTA	A		218	1605	39	2700	1301
FAD Y34			219	1301	32	0114	8041
STU Y44		34	220	0041	21	0114	8078
STU Y43		43	221	0917	21	0088	0921
RAU GAMMA	A		222	0921	60	2600	1655
FNP EPBIL	A		223	1655	39	2800	1351
FAU Y35			224	1351	32	0115	0051
STU Y35		38	225	0091	21	0115	4968
STU Y53		53	226	0968	21	0123	0076
RAU OELTA	A		227	0076	60	2700	1705
FNP OELTA	A		228	1705	39	2700	1401
FAU Y44			229	1401	32	0119	0095
STU Y44		44	230	0095	21	0119	0922
RAU OELTA	A		231	0922	60	2700	1755
FNP EPBIL	A		232	1755	39	2800	1451
FAD Y45			233	1451	32	0120	0047
STU Y45		4b	234	1047	21	0120	0073
STU Y54		54	235	0073	21	0124	4927
RAU EPBIL	A		236	0927	60	2800	1805
FNP P#SIL	A		237	1805	39	2800	1501
STU Y55			238	1501	32	0125	1551
RAU ALPHA	A	5b	239	1551	21	0125	0978
FNP N	A		240	0078	60	2400	1855
FAU Z1			241	1855	39	2300	1601
STU Z1		Z1	242	1601	32	0126	1303
RAU BETA	A		243	1303	21	0126	4979
FNP N	A		244	4979	60	2500	1905
FAO Z#			245	1905	39	2300	1451
STU Z#			246	1451	32	0127	1653
RAU GAMMA	A	22	247	1653	21	0127	4180
FNP N	A		248	0180	60	2400	606
FAU Z3			249	1206	39	2300	1701
STU Z3			250	1701	32	0128	1256
RAU OELTA	A	23	251	1256	21	0128	1031
FNP N	A		252	1031	60	2700	1306
FAU Z4			253	1306	39	2300	1751
STU Z4		24	254	1751	32	0129	1366
RAU P#BIL	A		255	1366	21	0129	0082
FNP N	A		256	0082	60	2600	1406
FAD Z5			257	1406	39	2300	1311
STU Z5		25	258	1011	32	0130	1157
SXA 0001			259	1157	21	0130	4133
NZA LOOP#		TRANS	260	0033	60	0133	599
RAA 0001			261	1019	40	1119	0043
RAH 0001			262	0043	80	0001	0099
RAC 0001			263	0099	82	0001	1456
LDO ENN			264	1456	88	0001	1112
STO ENNO		LUOPX	265	1112	69	1003	1506
LH 0100	A		266	1506	24	1359	1162
STO 0000	C		267	1162	69	2100	1703
LDO ENNO			268	1703	24	6000	1753
SXC 8001			269	1753	69	1359	1212
NZC 8001		CUNTY	270	1212	59	8001	1018
AXA 0001			271	1018	48	0971	0972
AXC 0001			272	0971	58	8001	4977
AXD 0001			273	0977	50	0001	4183
RAU 8001		LOOPX	274	0183	58	0001	1162
SUP ENN			275	0977	58	8001	4977
NZU ENN		BFC2	276	0178	60	8001	4185
SUP ENN			277	0185	11	1003	1207
NZU ENN		SFC3	278	0207	44	1003	1207
SUP ENN		BFC4	279	0911	11	1003	1257
NZU ENN			280	1257	44	0961	1132
SUP ENN		BFC5	281	0961	11	1003	1307
NZU ENN			282	1307	44	1011	1362
SUP ENN			283	1011	11	1003	1357
NZU ENN			284	1357	44	1003	1412
SXR 8001		CULZ	285	1262	69	1003	1366
AXB 8001			286	1556	53	8001	1462
AXR 0001			287	1462	42	1355	1061
RAA 0006			288	1315	58	8001	1021
LDO ENN			289	1021	52	0001	1027
RAC 8001			290	1027	80	0001	8033
AXC 0001			291	0933	69	1003	1606
RAU ENN			292	1606	88	8001	1512
SUP ENN			293	1512	58	0001	1068
NZU ENN		LOOPX	294	1068	60	1003	1407
SXR 8001			295	1407	10	1003	1457
AXR 8001			296	1457	21	1357	1162
RAA 0011			297	1357	69	1003	1656
LDO ENNO			298	1656	53	8001	1562
RAC 8001			299	1562	42	1356	1061
AXR 8001		CULZ	300	1365	58	8001	1071
AXR 0001			301	1071	52	0001	1077
RAA 0011			302	1077	80	0001	8033
LDO ENNO			303	0983	69	1359	1612
RAO 8001			304	1612	88	8001	1118
AXC 0001			305	1118	58	0001	8074
RAU ENND			306	0974	60	0559	1063
SUP ENN			307	1063	10	1003	1507
STU ENN		INDV	308	1507	10	1003	1507

	SKR	H001		310	1706	53	8001	1662
	NZ8		COLZ	311	1662	42	1415	1061
	AX8	H001		312	1415	62	8001	1121
	AX8	0001		313	1121	52	0001	1127
	RAA	0016		314	1127	80	0001	1033
	LDU	ENND		315	1033	69	1359	1712
	RAC	H001		316	1712	88	8001	1158
	AKC	0001		317	1158	58	0001	1029
	RAU	ENND		318	1029	60	1359	1113
	AUP	ENN		319	1113	10	1003	1557
	STU	ENND	LOOPX	320	1557	21	1359	1168
BFC5	LDU	ENND		321	1412	69	1003	1756
	GXR	H001		322	1756	53	8001	1762
	NZ8		COLZ	323	1762	48	1465	1061
	RAA	0021		324	1465	80	0021	1171
	LUU	LNND		325	1171	69	1359	1812
	RAC	H001		326	1812	88	8001	1218
	AKC	0001		327	1218	58	0001	1074
	RAU	ENND		328	1074	60	1359	1163
	AUP	ENN		329	1163	10	1003	1607
	STU	ENND	LOOPX	330	1607	81	1359	1162
COLZ	LDU	ENND		331	1061	69	1359	1862
	RAC	H001		332	1862	48	8001	1268
	AKC	0001		333	1268	58	0001	1124
	RAA	0001		334	1124	80	0001	0930
LOUPZ	LDU	0125	LUOPZ	335	0930	69	2185	0928
	STO	0000	A	336	0928	24	6000	1803
	LDU	ENN	C	337	1803	89	1003	1806
	SXA	H001		338	1806	61	8001	1522
	NZA	R001	CONT1	339	1912	40	1515	0916
	AXA	0001		340	1515	50	8001	1221
	AXC	0001		341	1221	50	0001	1177
CONT1	LDU		LODPZ	342	1177	58	0001	0930
	RAU	ENN	ENTHY	343	0916	69	1219	1022
	MPY	ENN		344	1219	10	1003	1637
	ALO	UMITY		345	1637	19	1003	1744
	STL	LNND		346	1174	15	1227	1081
	RAA	0001		347	1081	20	0535	0038
	LDU	ENND		348	0038	80	0001	1663
	RAC	H001	LOOPY	349	0044	69	0935	0088
	AKC	0001		350	0088	88	8001	1094
LOOPY	LDU	0000	C	351	0094	69	6000	1833
	STO	0125	A	352	1833	24	2125	0978
	SXA	0005		353	0978	51	0003	0084
	NZA		CON1	354	0084	40	0084	4138
	AXC	0006		355	0087	50	0006	0093
	AKC	0001	LOOPY	356	0093	58	0001	0994
CON1	LDU	INDXA		357	0138	69	1038	1266
	RAA	H001	LOOP3	358	1856	80	8001	1962
	RAU	Z4		359	1962	60	0126	1131
LOOP3	FMP	ALPHA	A	360	1131	39	2581	0911
	STU	TEMP1		361	1051	21	0160	1213
	RAU	Z4		362	1213	60	1277	1881
	FMP	HFTA	A	363	1581	39	2581	0911
	STU	TEMP2		364	1901	21	0904	1707
	RAU	Z3		365	1707	60	0128	1083
	FMP	GAMMA	A	366	1083	39	2600	0962
	STU	TEMP3		367	0908	21	0954	1757
	RAU	Z4		368	1757	60	0129	1133
	FMP	DELTA	A	369	1133	39	2700	0952
	STU	TEMP4		370	0952	21	1004	1007
	RAU	Z5		371	1807	60	0130	0985
	FMP	EBIL	A	372	0985	39	2800	1052
	FAD	TEMP1		373	1052	32	0160	0137
	FAD	TEMP2		374	0137	32	0904	1231
	FAU	TEMP3		375	1231	32	0954	1281
	FAD	TEMP4		376	1281	32	1004	1331
	ESB	N	A	377	1331	33	2300	1877
	STU	TEMP1		378	1877	21	0160	1263
	FMP	TEMP1		379	1263	39	2800	1409
	FAD	ENEW		380	0960	32	0066	0143
	STU	ENEW		381	0143	21	0066	1269
	SXA	0001		382	1269	81	1004	1381
	NZ8	LODP3	CONT3	383	0175	40	1962	1029
	LDU		EUOCL	384	1029	69	0132	1550
	LDU	Z1		385	0132	64	1978	1075
	LDU	Z2		386	1075	24	1977	0980
	STD	1978		387	0980	69	0127	1030
	LDU	Z3		388	1030	34	1981	1381
	STD	1979		389	1381	69	0128	1431
	LDU	Z4		390	1431	24	1979	0182
	STD	1980		391	0182	60	0129	0932
	LDU	Z5		392	0932	24	1980	1103
	STU	ENEW		393	1103	69	0130	1233
	LDU	1982		394	1233	24	1981	0134
	STU	ENEW		395	0134	89	0086	1319
	LDU	A		396	1319	24	1982	1035
	STO	1983		397	1035	60	1056	1409
	PCW	1977		398	1409	24	1983	0938
	RAU	EOLD		399	0938	71	1977	1327
	F88	ENND		400	1327	60	1007	1111
	F88	CONT5	CONT4	401	1111	33	0064	0193
	RAU	A		402	0193	46	0044	1097
CONT4	RAU	DELA		403	1097	80	1057	1161
	FAD	DELA		404	1161	32	1001	1377
	STU	A		405	1377	21	1056	1459
	LDU	ENEW		406	1459	89	0086	1369
	STO	EOLD		407	1369	24	1066	1509
	LDU	ZERD		408	1509	69	0050	1903
	STO	ENEW	LOOP4	409	1903	60	1007	0959
CONT5	RAU	DELA		410	0046	60	1001	1906
	F88	CONT7		411	1906	33	1250	1427
	BMI	CONT7	CONT6	412	1427	60	1001	1857
CONT6	RAU	DELA		413	1481	60	1001	1857

CALCULATE
ERROR
BOJAREU

	FOV TWO		414	1857	34	0100	1106
	STU OELA		415	1102	41	1001	1154
	RAU A		416	1154	60	1058	1211
	FSB OELA		417	1211	33	1001	1477
	STU A		418	1477	31	1053	8935
CUNTY	LDU		419	1080	69	1283	1550
	LOD A		420	1283	69	1056	1556
	STO 1977		421	1519	69	1977	1130
	LDU PHEC		422	1130	69	1250	1204
	STO 1978		423	1204	24	1978	1537
	LDU INDXA		424	1531	69	1009	1907
	STU 1979		425	1907	24	1907	0982
	STO 1977		426	0982	71	1977	8000
ENTRY	STU EXIT	0000	427	1028	24	0053	8158
	RAU ENN		428	0908	60	1003	0908
	SUP UNITY		429	0908	11	1227	1581
	STU UNLES		430	1388	21	0986	0935
	RAU ENN		431	0939	60	1003	0958
	AUP UNITY		432	0958	10	1227	1631
	STU ENPLU		433	1631	21	1036	0985
	MPY ENN		434	0989	19	1003	1224
	STL NSPEN		435	1224	20	1129	1032
	BLT ODD4		436	1032	35	0004	0973
	ALD INDA		437	0943	15	0096	1152
	LDU AONE		438	1152	69	1008	1261
	SUA ADME		439	1261	22	1008	1311
	LDU LOOPB		440	1311	69	0164	0967
	SUA LOOPB		441	0967	22	0164	1017
	LDU ATWO		442	1017	69	0270	0930
	SUA ATWO		443	0173	22	0270	0930
	LDU ATHEE		444	0923	69	0176	1175
	SUA ATHEE		445	1179	22	0176	1175
	LDU AFOUR		446	1229	69	1082	1085
	SUA AFOUR		447	1085	22	1082	1135
	LDU LOOPF		448	1135	69	0144	1147
	SUA LOOPF		449	0141	22	0188	0191
	LDU LOADC		450	0191	69	0144	1147
	SUA LOADC		451	1147	22	0188	0191
	LDU AFIVE		452	1197	69	1202	1058
	SUA AFIVE		453	1058	22	1202	1109
	ALD INDB		454	1108	22	1108	1543
	LDU CONE		455	1565	69	1318	1271
	SUA CONE		456	1271	22	1318	1321
	LDU CTWO		457	1321	69	1129	1433
	SUA CTWO		458	1527	22	1274	1577
	LDU CTREE		459	1577	69	1180	1333
	SUA CTREE		460	1333	22	1180	1383
	LDU CFOUR		461	1383	69	1086	1035
	SUA CFOUR		462	1039	22	1086	1084
	LDU CFIVE		463	1089	69	0099	813
	SUA CFIVE		464	0145	22	0092	8925
	RAC ODD0		465	0195	88	0000	1252
	STL NSPEN		466	1252	69	8007	1156
	STU CTEMP		467	1156	24	1158	0914
	RSL NSPEN		468	0914	66	1129	1433
	RAA ODD2		469	1433	80	8002	0941
	STL ATEMP		470	0941	38	0943	0948
	RSL UNLES		471	0048	66	0986	0991
	RAH ODD2		472	0991	82	8002	0145
	STL BTEMP		473	0145	38	1254	1008
	RAH ODD2		474	1008	65	9999	1304
	RAH ODD2		475	1304	45	1200	1609
	RAH ODD2		476	1609	20	1313	8164
	RAH ODD2		477	0164	60	9999	1354
	RAH ODD2		478	1354	34	1313	8970
	RAH ODD2		479	0970	21	9999	1302
	RAH ODD2		480	1302	65	1003	1258
	RAH ODD2		481	1258	50	8002	1067
	RAH ODD2		482	1067	13	0001	1137
	RAH ODD2		483	1371	65	0945	0199
	RAH ODD2		484	0199	80	8002	1308
	RAH ODD2		485	1308	48	1308	1413
	RAH ODD2		486	1461	65	8007	1419
	RAH ODD2		487	1419	15	8005	1627
	RAH ODD2		488	1627	88	1027	1318
	RAH ODD2		489	1318	61	9999	1404
	RAH ODD2		490	1404	45	1358	1659
	RAH ODD2		491	1659	52	0001	8046
	RAH ODD2		492	0966	60	1413	8176
	RAH ODD2		493	0176	39	9999	1274
	RAH ODD2		494	1274	13	9999	1180
	RAH ODD2		495	1180	21	9999	1352
	RAH ODD2		496	1352	65	1003	1408
	RAH ODD2		497	1408	50	8008	1137
	RAH ODD2		498	1137	58	8002	8925
	RAH ODD2		499	0925	41	0966	1659
	RAH ODD2		500	1659	52	0001	8143
	RAH ODD2		501	1615	42	1368	1469
	RAH ODD2		502	1469	69	1411	0964
	RAH ODD2		503	0964	88	0945	1020
	RAH ODD2		504	1020	88	0945	0990
	RAH ODD2		505	0990	80	8001	1454
	RAH ODD2		506	1454	69	1054	8139
	RAH ODD2		507	1139	50	8001	8925
	RAH ODD2		508	0925	69	8005	1407
	RAH ODD2		509	1407	24	0909	8148
	RAH ODD2		510	0148	41	1452	0953
	RAH ODD2		511	1452	59	0001	1458
	RAH ODD2		512	1458	69	8001	1124
	RAH ODD2		513	1014	24	1411	1064
	RAH ODD2		514	1064	24	1167	0948
	RAH ODD2		515	0948	69	0945	8158
	RAH ODD2		516	0198	80	8001	1504

	LUD KTEMP			517	1504	69	1167	1070
	RAC 0001	SHKIP		519	1070	69	8001	1363
SHKIP	AXC 0001			520	1363	58	0001	1519
	LUD 0007			521	1519	69	8007	0975
	YTD KTEMP	LUDPC		522	0975	24	1177	1306
NEPLA	LUD UNLES			523	1609	59	0986	1189
	AXC 0001	LOOPE		523	1189	58	8001	1045
LUUPE	AXC 0001			524	1045	58	0001	1502
	BXC 0001	AFUUN		525	1502	39	0001	1082
AFUUN	RAL 9999			526	1082	65	9999	1584
	NZE	ZEERO		527	1584	45	1508	1709
	RSL UNLES			528	1309	66	0986	1041
	AXC 0002			529	1041	58	8002	0949
	RAL 0007			530	0949	65	8007	1558
	ALO 0002			531	1558	15	8005	1665
	RAC 0002	LOOPF		532	1665	88	8002	0188
	RAL 9999	CFUUN		533	0188	65	9999	1086
LOUPF	LUD 9999	AFIVE		534	1086	69	9999	1202
CFUUN	GTU 9999	CFIVE		535	1202	24	9999	0092
AFIVE	BTU 9999			536	0092	20	9999	1552
CFIVE	LUD ENN			537	1552	69	1003	1608
	AXC 0001			538	1608	58	8001	1114
	AXA 0001			539	1114	50	8001	1120
	MMI LOOPF			540	1120	46	0188	1324
	LUD ATEMP			541	1324	69	0948	0948
	RAA 0001			542	0948	60	8001	1604
	LUD CTEMP			543	1604	69	1411	1164
	RAC 0001	NORMA		544	1164	88	8001	1208
ZEERO	NZC LOOPF	STOPP		545	1709	48	1045	1463
PUNCN	LUD ENN			546	1602	69	1003	1658
	RSA 0001			547	1658	81	8001	1214
	RRC 0008	LUUUC		548	1814	89	0008	0144
LUUUC	LUD 9999			549	0144	69	9999	1652
	STD 19H5			550	1652	24	7965	0938
	AXC 0001			551	0938	58	0001	0194
	NZC INCKA			552	0194	48	1247	0998
	PCM 1977			553	0998	71	1977	1677
	RSC 0008	INCKA		554	1677	89	0008	1847
INCKA	AXA 0001			555	1247	50	0001	1654
	NZA LOAOC			556	1654	40	0144	1708
	PCM 1977			557	1708	71	1977	1727
	RAU NSPEN			558	1727	60	1129	1483
	RBR 0001			559	1483	83	0001	1239
	RAA 0008	ZEERE		560	1239	80	0000	1095
ZEERE	NZB	N000		561	1095	42	1048	0000
	AXN 0001			562	1048	58	0001	1704
	STL 0001			563	1704	20	2001	1754
	AXA 0001	ZEENC		564	1754	50	0001	1095
UNITY	OO 0000	DU01		565	1227	80	0000	0501
	INDA	0000		566	0096	00	2001	0000
INDA	OO 4000	0000		567	1361	00	4000	0000
INDR	OO 4000	0000		568	1463	01	5555	5555
STOPP	01 5555	5593						

APPENDIX H

IBM 650 Program for Diffusion Length,
Monoenergetic Fast Source

This code was written to determine an experimental value of diffusion length based upon the assumption of a monoenergetic source of fast neutrons. The program was written in SOAP II and floating point form. The object program and a logic diagram are given in this section.

The solution to this problem is based upon the equation

$$\phi = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{Q_0}{ab D \gamma_{mn}} e^{-k^2 \tau} \left[e^{-\gamma_{mn} z} \left[1 + \operatorname{erf} \left(\frac{z}{2\sqrt{\tau}} - \gamma_{mn} \sqrt{\tau} \right) \right] + e^{\gamma_{mn} z} \left[1 - \operatorname{erf} \left(-\frac{z}{2\sqrt{\tau}} + \gamma_{mn} \sqrt{\tau} \right) \right] \right] (1 - e^{-2\gamma_{mn}(c-z)}).$$

An iteration procedure similar to that used in the point thermal and constant thermal source programs was used.

Input parameters and data are listed in Table 31. All input should be punched on one word load cards and read into the machine with the object deck.

Output from this program is in two forms, as shown in Table 32. Form one is punched after the calculation of each individual correction factor. Form two is the final result and gives the last value of γ_{11} as well as the diffusion length.

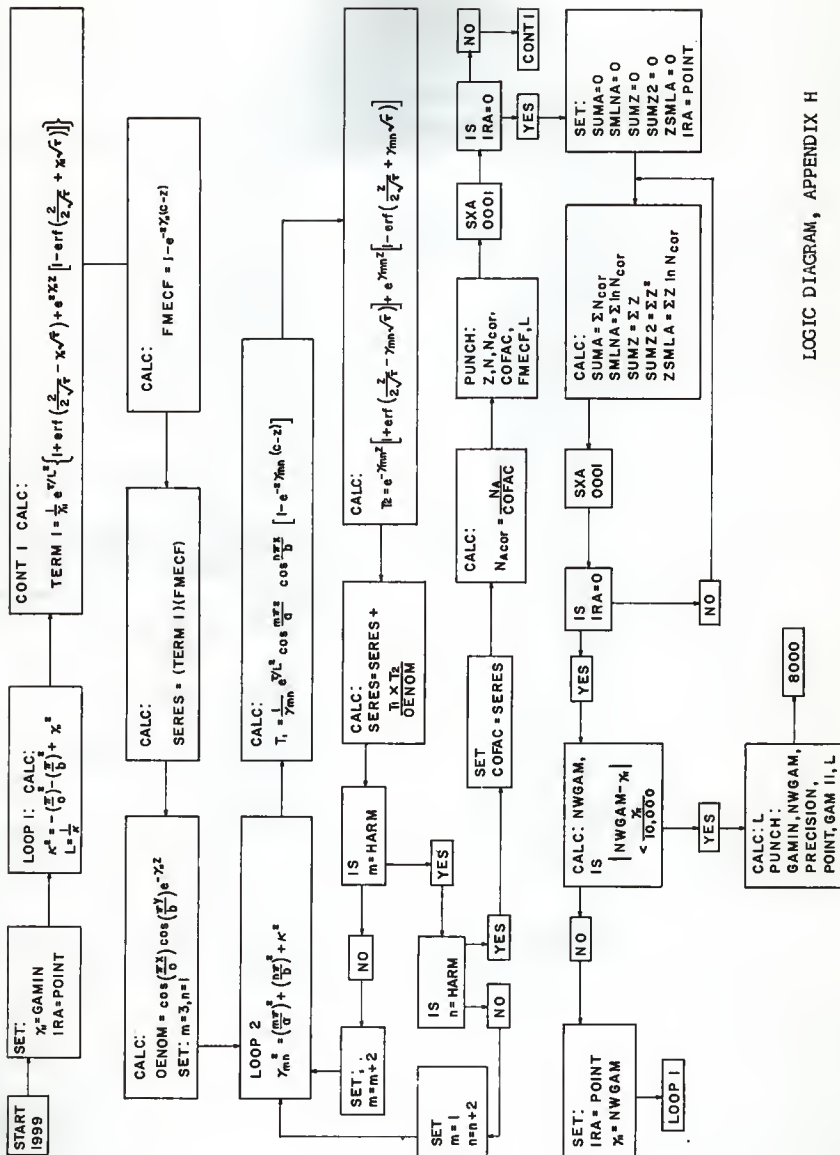
The operating time for the calculation of one correction factor using four harmonics is approximately 40 seconds. The capacity of the program is 200 data points.

Table 31. Input to IBM 650 program for diffusion length, monoenergetic fast source.

Symbol	Explanation	Drum Storage Location
FIRST	Initial estimate of γ_{11}	0100
POINT	Number of Data Points, in form 00 0000 00xx	0101
DATPT	Number of Data Points, in floating point form	0102
A	Extrapolated x-dimension	0103
B	Extrapolated y-dimension	0104
C	Extrapolated z-dimension	0105
X	X co-ordinate of data	0106
Y	y co-ordinate of data	0107
TAU	Fermi age of source neutrons	0108
HARM	Magnitude of highest harmonic used.	0109

Table 32. Output forms for IBM 650 program for diffusion length, monoenergetic fast source.

Word No.	1	2	3	4	5	6
Form One:						
z co-ordinate	data	corrected data	Harmonic correction	End correction	Diffusion Length	
Form Two:						
γ_{11} , initial value	γ_{11} last value	Precision	POINT	γ_{11} , next to last value	Diffusion Length	



LOGIC DIAGRAM, APPENDIX H

OBJECT PROGRAM - APPENDIX H

	BLR	1951	1958	1	0000	00	0000	0000
	BLR	1977	1984	2	0000	00	0000	0000
	BLR	0300	0900	3	0000	00	0000	0000
	BYN	Z	0300	4	0000	00	0000	0000
	BYN	N	0500	5	0000	00	0000	0000
	BYN	NCOR	0700	6	0000	00	0000	0000
	BYN	GAMIN	0100	7	0000	00	0000	0000
	BYN	POINT	0101	8	0000	00	0000	0000
	BYN	QAPPT	0102	9	0000	00	0000	0000
	BYN	A	0103	10	0000	00	0000	0000
	BYN	B	0104	11	0000	00	0000	0000
	BYN	C	0105	12	0000	00	0000	0000
	BYN	X	0106	13	0000	00	0000	0000
	BYN	Y	0107	14	0000	00	0000	0000
	BYN	TAU	0108	15	0000	00	0000	0000
	BYN	HARM	0109	16	0000	00	0000	0000
	BYN	START	1999	17	0000	00	0000	0000
ZERO	00	0000	0000	18	0000	00	0000	0000
ONE	01	0000	0001	19	0000	10	0000	0001
THREE	30	0000	0051	20	0150	30	0000	0051
PI	31	4159	0051	21	0200	31	4159	0051
CDNVT	25	3600	0051	22	0250	25	3600	0051
10000	10	0000	0055	23	0950	10	0000	0055
TWO	20	0000	0051	24	1000	20	0000	0051
EOERF	BT0	OUT		25	1030	24	0003	0006
	SMI	NGTVE	PSTVE	26	0006	46	0009	0010
NGTVE	STU	TEW1		27	0009	21	0014	0017
	RAM	TEW1		28	0017	67	0014	0019
	RAU	8002		29	0019	60	8002	0027
	STU	ARGG		30	0027	21	0032	0035
	LOO	MUNIT		31	0035	69	0038	0041
	BT0	COEFF	APPRO	32	0041	24	0044	0047
PBTVE	BTU	ARGG		33	0010	21	0032	0085
	LOO	UNIT		34	0008	69	0085	0091
	BT0	COEFF	APPRO	35	0091	24	0044	0047
APPRO	RAU	ARGG		36	0047	60	0032	0037
	FAD	A4AA		37	0047	39	0047	0070
	FAO	A5AA		38	0090	32	0043	0069
	FMP	ARGG		39	0069	39	0032	0082
	FAD	A4AA		40	0092	32	0092	0091
	FMP	ARGG		41	0011	39	0032	0132
	FAD	A3AA		42	0132	32	0185	0061
	FMP	ARGG		43	0061	39	0032	0232
	FAO	A2AA		44	0182	32	0235	0111
	FMP	ARGG		45	0111	39	0032	0232
	FAD	A1AA		46	0232	32	0232	0261
	FMP	ARGG		47	0161	39	0032	0282
	FAD	UNIT		48	0282	32	0088	0015
	FMP	8003		49	0015	39	0015	0019
	FMP	8003		50	0019	39	8003	0023
	FMP	8003		51	0023	39	8003	0077
	FMP	8003		52	0077	39	8003	0021
	STU	TEW1		53	0031	21	0014	0067
	RAU	UNIT		54	0067	60	0088	0093
	FAD	TEW1		55	0093	34	0014	0064
	STU	TEW1		56	0064	21	0014	0117
	RAU	UNIT		57	0117	60	0088	0143
	FOS	TEW1		58	0143	33	0014	0141
	FMP	COEFF	OUT	59	0141	39	0044	0003
A1AA	70	5230	7849	60	0285	70	5230	7849
A2AA	42	2829	3249	61	0285	42	2829	3249
A3AA	92	7052	7249	62	0185	92	7052	7248
A4AA	15	2014	3047	63	0135	15	2014	3047
A5AA	47	5677	8047	64	0047	27	0677	8047
A6AA	43	0638	0046	65	0040	43	0638	0046
UNIT	10	0000	0051	66	0088	10	0000	0051
MUNIT	10	0000	0051	67	0038	10	0000	0051
LNK01	BT0	LNK08		68	1100	24	0053	0056
	NZE		LNK14	69	0056	46	0211	0114
	BTU	LNK14		70	0060	46	0211	0114
	STU	LNK09		71	0114	21	0018	0021
	R9L	FPONE		72	0024	66	0024	0029
	STU	LNK10		73	0029	24	0932	0935
	BTU	LNK02		74	0935	20	0039	0042
	RAU	LNK09		75	0042	60	0042	0073
	STL	LNK05		76	0073	20	0127	0030
	STL	LNK11		77	0030	20	0985	0138
	BLT	0008		78	0138	35	0038	0077
	SUP	FIFTY		79	0007	11	0110	0065
	NZE		LNK04	80	0065	45	0068	0169
	RM1		LNK03	81	0068	45	0068	0242
	RAU	8003		82	0071	61	8003	0079
	LOO	FPONE		83	0079	69	0024	0177
	BTU	LNK02	LNK03	84	0177	24	0039	0022
LNK03	BTU	0008		85	0022	30	0008	0191
	SC7	0000		86	0191	36	0000	0013
	AUP	81FTY		87	0013	10	0013	0013
	SUP	8002		88	0121	11	8002	0129
	RAU	8003		89	0029	60	8003	0087
	FMP	LNK02		90	0087	39	0087	0089
	FMP	LNK02		91	0089	39	0092	0142
	STU	LNK05	LNK04	92	0142	21	0127	0169
	RAL	LNK09		93	0169	65	0169	0223
LNK04	STU	0002		94	0123	30	0002	0179
	RAU	8002		95	0179	60	8002	0137
	ALO	FIFTY		96	0137	15	0137	0155
	SLT	0002		97	0115	35	0002	0171
	FAD	FPONE		98	0171	32	0024	0001
	STU	LNK09		99	0001	21	0018	0021
	FBO	FPONE		100	0221	33	0074	0051
	F0Y	LNK09		101	0051	34	0018	0118
	BTU	LNK13		102	0118	21	0118	0025
	BTU	LNK12		103	0025	24	0028	0081

	STP	LNK11	104	0081	24	0985	0188
	FMP	8001	105	0188	39	8001	0241
	STU	FACT8	106	0241	21	0046	0159
LNK06	RAU	LNK10	107	0049	60	0932	0187
	FAO	FPY10	108	0187	32	0074	0151
	STU	LNK10	109	0151	21	0051	0185
	8AU	LNK13	110	1035	60	0072	0227
	FMP	FACT8	111	0527	39	0046	0096
	FOV	LNK10	112	0096	34	0096	0128
	STU	LNK13	113	0982	21	0072	0075
	FAO	LNK12	114	0075	32	0088	0065
	STU	LNK12	115	0005	21	0028	0151
	F08	LNK11	116	0131	33	0985	0261
	FOV	LNK11	117	0261	34	0985	1085
	RAM	8003	118	1085	67	8003	0193
	8AU	8002	119	0193	60	8002	0201
	F8R	81ZE7	120	0201	33	0004	0181
	SMI	LNK07	121	0181	46	0034	1135
	LOO	LNK12	122	1135	69	0028	0231
	STO	LNK11	123	0231	24	0985	0838
	8AU	LNK13	124	0238	60	0072	0277
	FMP	LNK10	125	0277	39	0932	1032
	STU	LNK13	126	1032	21	0072	0049
LNK07	RAU	LNK12	127	0034	60	0028	0033
	FMP	FPY10	128	0033	39	0074	0184
	F8R	LNK05	129	0124	33	0127	0053
	10	0070	130	0084	10	0000	0051
FPONE	20	0000	131	0074	20	0000	0051
FPY10	10	0000	132	0004	10	0000	0043
81ZE7	20	0000	133	0096	23	0028	0151
LNTEW	50	0000	134	0110	50	0000	0000
FIFTY	50	0000	135	0016	00	0000	0060
SIXTY	00	0000	136	0145	01	0345	6789
LNK14	STU	EXIT	137	1150	24	0153	0156
E0CR	RAU	8002	138	0156	60	8002	0165
	SMI	NEGAT	139	0165	46	0168	0199
NEGAT	FAO	TROP1	140	0168	32	0271	0097
	MI	NEGAT	141	0097	46	0168	0251
	FMP	ONEPI	142	0251	33	0254	0211
REUC	F8R	TROP1	143	0219	33	0271	0147
	MI		144	0147	46	1300	0219
	MI	ONEPI	145	1200	32	0054	0211
COS10	STU	THETA	146	0281	21	0036	0139
	R8U	FPONE	147	0139	61	0024	0229
	STU	TERMH	148	0239	21	0039	0477
	STU	FUNKT	149	0237	21	0198	0045
	STL	ENNN	150	0045	20	0099	0002
E0BR	SMI	EXIT	151	1250	24	0153	0166
	8AU	80D2	152	0206	60	8002	0215
	MI	HEGAV	153	0215	46	0218	0269
NEGAV	FMP	TROP1	154	0218	38	0271	0177
	MI	NEGAV	155	0197	46	0218	0901
	F8R	ONEPI	156	0901	33	0054	0931
REOHU	FMP	TROP1	157	0269	33	0279	0177
	MI		158	0247	46	1300	0269
	FAO	ONEPI	159	1300	32	0054	0931
8INET	STU	THETA	160	0931	21	0036	0189
	89U	80D3	161	0189	61	8003	0297
	STU	TERMH	162	0297	21	0084	0287
	STU	FUNKT	163	0287	21	0192	0055
	LOO	FPONE	164	0095	69	0024	0927
	STO	ENNN	165	0927	24	0099	0002
NEG5T	RAU	ENNN	166	0002	60	0099	0203
	FAU	FPONE	167	0203	32	0024	0951
	STU	FPONE	168	0951	21	0256	0059
	FAU	FPONE	169	0059	32	0024	1001
	STU	ENNN	170	1001	21	0099	0052
	89U	TERMH	171	0052	61	0084	0239
	FMP	THETA	172	0239	39	0036	0166
	FMP	THETA	173	0086	39	0036	0136
	FOV	NPONE	174	0136	34	0256	0906
	FOV	ENNN	175	0906	34	0096	0149
	RAU	FUNKT	176	0149	21	0084	0937
	STL	FWAG	177	0937	67	0192	0947
	RAU	TERMH	178	0947	20	0151	0164
	RAU	80D2	179	0154	67	0084	0289
	FOV	FAA1	180	0889	60	8002	0997
	F08	FAA1	181	0997	34	0151	1111
	F8R	81ZEB	182	1101	33	0204	0981
	MI	EMUFF	183	0981	46	0134	1185
	RAU	FUNKT	184	1185	60	0192	1047
	FOV	FUNKT	185	1047	32	0084	0911
	STU	FUNKT	186	0911	21	0192	0002
ENUFF	RAU	EXIT	187	0192	65	0192	0153
81ZE7	10	0000	188	0204	10	0000	0043
TROP1	62	8318	189	0271	62	8318	5351
ONEPI	30	1159	190	0204	31	4159	2011
FPONE	10	0000	191	0024	10	0000	0051
E0DEA	STO	AAA1	192	1350	24	0253	0956
	STL	AAA2	193	0956	20	0961	0164
	RAM	AAA2	194	0164	67	0961	0265
	STL	AAA3	195	0265	20	0919	0122
	8AU	AAA3	196	0122	60	0919	0133
	FMP	AAA16	197	0173	39	0026	0076
	FAO	AAA15	198	0076	32	0279	0055
	FMP	AAA14	199	0055	39	0099	0199
	FAO	AAA14	200	0969	32	0172	0199
	FMP	AAA3	201	0199	39	0919	1069
	FAO	AAA13	202	1019	32	0228	0249
	FMP	AAA3	203	0249	39	0919	1069
	FAO	AAA12	204	1069	32	0272	0299
	FMP	AAA7	205	0299	39	0919	1199
	FAO	AAA11	206	1119	32	0922	0949

	FMP AAA3		207	0749	39	0919	1169
	FAD AAA10		208	1169	34	0972	0999
	STU AAA4		209	0994	21	0994	0999
	FMP AAA4		210	0057	39	0254	0904
	STU AAA4		211	0904	21	0254	0157
	FMP AAA4		212	0157	39	0254	0054
	STU AAA4		213	0954	21	0254	0207
	RAU AAA2		214	0207	60	0961	0915
	RAU AAA5	AAA6	215	0915	46	0268	1219
AAA5	RAU AAA10		216	0057	60	0972	0977
	FOV AAA4		217	0977	34	0254	1004
	STU AAA4	AAA6	218	1004	21	0254	1219
	RAU AAA4	AAA1	219	0119	65	0254	0253
AAA6	RAU AAA4		220	0972	10	0000	0051
AAA10	10 0000	0051	221	0972	24	9998	6850
AAA11	24 9998	6850	222	0928	31	2575	8349
AAA12	31 2575	8349	223	0228	25	9137	1248
AAA13	25 9137	1248	224	0172	17	1562	0047
AAA14	17 1562	0047	225	0279	54	1020	0045
AAA15	54 1020	0045	226	0026	69	0600	0044
AAA16	69 0600	0044	1 227	1400	24	0903	1006
E00AU	STU NEXT		2 228	1006	46	0159	0160
	HMI REHF		3 229	0160	45	0214	0903
	NZE	NEXT	4 230	0921	21	0918	0921
	STU RA		5 231	0921	32	0174	1151
	FAD RO		6 232	1151	39	1054	1104
	FMP RHAF	RB	7 233	1104	21	0008	1011
RB	STU RBAV	BAH	8 234	1011	60	0918	0223
BAH	RAU RBAV		9 235	0223	34	0008	0058
	FOV SBAV		10 236	0058	32	0008	1235
	FAD SBAV		11 237	1235	39	1054	1154
	FMP SHAF		12 238	1154	33	0008	1285
	FMR SBAV		13 239	1285	44	0939	0140
	HZH	SR	14 240	0939	66	0949	0240
	RAU		15 241	0242	32	0008	1335
	FAU SBAV	SAH	16 242	1335	21	0008	1011
BR	STU SBAV	SEH	17 243	0140	60	0008	0903
SERR	RAU SBAV	SEH	18 244	0159	01	0000	0050
RHAF	HLT 0000	NEXT	19 245	1054	50	0000	0050
SID	50 0000	0050	20	0214	0	0000	0051
START	STU 0000	0051	247	1999	69	0100	0953
	LHO GAVIN		248	0953	24	1056	0209
LOOP1	STU GAVIN	LOOP1	249	0209	60	0209	0209
	LHO GAVIN		250	0155	34	0103	1003
	FOV A		251	1003	21	0158	1061
	STU TEMP1		252	1061	39	0158	1111
	FMP TEMP1		253	0208	21	0158	1111
	STU TEMP1		254	1111	60	0900	0205
	RAU H		255	0205	34	0104	1204
	FOV H		256	1204	21	0258	1161
	STU TEMP2		257	1161	39	0258	0908
	FMP TEMP2		258	0908	21	0258	1111
	STU TEMP2		259	1211	60	1056	1261
	RAU GAVIN		260	1261	39	1056	1106
	FMP GAVIN		261	1106	33	1106	1311
	STU TEMP2		262	1311	33	0258	1435
	FMR TEMP2	CALCULATE	263	1435	21	0190	0243
	STU KAPPA	KAPPA	264	0243	69	0146	1053
	LHO	SQUAREH	265	0146	21	1450	1053
	STU KAPPA		266	1053	60	0050	0255
	RAU ONE	CALCULATE	267	0255	34	1450	1504
	FOV KAPPA	DIFFUSION	268	1504	21	1254	0257
	STU DL	LENGTH	269	0257	69	0101	1304
	LDR POINT		270	1304	80	8001	0210
	RAA 0001	RIGHT	271	0210	60	0108	0063
CONT1	RAU TAN		272	0063	34	1254	1354
	FOV DL		273	1354	34	1254	1404
	FVY DL		274	1404	65	8003	1311
	RAL RO03		275	1311	69	0264	1350
LOD	RAU RO03	E00EA	276	0264	60	8003	0273
	FOV CAM11		277	0273	34	1056	1156
	STU TEMP1		278	1156	21	0158	1361
	RAU TEMP1	A	279	1361	60	0258	0905
	FMP CAM11		280	0905	39	1056	1206
	FMP TPO		281	1206	39	1000	1550
	RAL RO03		282	1550	65	8003	0207
LOD	STU TEMP2	E00EA	283	0207	69	0260	1350
	BITL TEMP2		284	0260	20	0258	1411
	RAU TAU		285	1411	60	0108	0033
	LOD	E00AU	286	0113	69	0066	1400
	STU HTAU		287	0066	21	0020	0923
	RAU Z		288	0923	60	0263	0958
	FOV TPO	A	289	0958	34	1000	1600
	STU HTAU		290	1600	34	0020	0070
	RAU PART1		291	0070	21	0020	0917
	RAU RTAU		292	0917	60	0020	0125
	FMP CAM11		293	0125	39	1056	1256
	STU PART2		294	1256	21	0020	0233
	RAU PART2		295	0163	60	0224	0929
	FMR PART2		296	0929	33	0910	0987
	DOO	E00RF	297	0987	69	1000	1500
	FAD ONE		298	0240	32	0050	1077
	STU TEMP3		299	1077	21	1092	1485
	RAU PART1		300	1485	60	0148	0919
	FAO PART2		301	0919	32	0910	1037
LOD	STU TEMP4	E00RF	302	1037	69	0290	1050
	RAU ONE		303	0290	21	0020	0137
	FMR TEMP4		304	1097	60	0050	1005
	FMP TEMP4		305	1005	33	0094	0971
	STU TEMP2		306	0971	39	0258	0958
	BTU TEMP2		307	0958	21	0258	1461
	FAD TEMP3		308	1461	32	1082	0859
	FMP TEMP1		309	0259	39	0158	1008

STU	TERM1			310	1008	21	0012	0965
RAU	Z	A		311	0965	60	2300	1055
F8B	C			312	1055	33	0105	1031
FMP	GAM11			311	1031	39	1056	1306
FMP	TFO			314	1016	39	1000	1650
RAL	8003			315	1650	65	8003	0957
LOO				316	0957	69	0900	1350
STL	TEMP1	EOOEA		317	0900	20	0158	1511
RBU	C			318	1511	61	0105	0909
FMP	GAM11			319	0909	39	1050	1306
FMP	TFO			320	1350	39	0000	1700
RAL	8003			321	1700	65	8003	1007
LOO				322	1007	69	1010	1350
RAU	8002	EOOEA		323	1010	60	8002	1269
FAO	ONE			324	1269	32	0050	1187
STU	TEMP2			325	1187	21	0258	1561
RAU	ONE			326	1561	60	0050	1105
F8B	TEMP1			327	1105	33	0158	1535
FOV	TEMP2			328	1535	34	0258	1058
STU	FUECF			329	1058	21	0062	1015
FMP	TERM1		CALCULATE	330	1015	39	0012	0112
STU	SEREB		TERM ONE	331	0112	21	0116	1319
RAU	PI		OF SERIEB	332	1319	60	0200	1155
FDP	A			333	1155	34	0103	1103
FMP	X			334	1103	39	0106	1406
RAL	8003			335	1406	65	8003	0213
LOO				336	0213	69	0166	1150
STL	TEMP1	EOOCH		337	0166	80	0158	1611
RAU	PI			338	1611	60	0200	1205
FOV	S			339	1205	34	0104	1454
FMP	Y			340	1454	39	0107	1057
RAU	8003			341	1057	65	8003	1065
LDO				342	1065	69	0968	1150
STL	TEMP2	EOOCH		343	0968	20	0258	1661
RBU	Z	A		344	1661	21	3000	1855
FMP	GAM11			345	1855	39	1056	1456
RAL	8003		CALCULATE	346	1456	65	8003	0263
LDO			OENOMINATR	347	0263	69	0200	1350
RAU	8002		FOR	348	0216	60	8002	0175
FMP	TEMP1		SUCCEEDING	349	0175	39	0158	1108
FMP	TEMP2		SERIEB	350	1108	39	0108	1358
STU	OENOM		TERMS	351	1150	21	0162	1115
RAU	HARM			352	1115	60	0109	0913
RAU	THREE		SET M N	353	0913	60	0103	1105
STU	M		FOR BECOND	354	1305	21	1060	0963
RAU	ONE		SERIEB	355	0963	60	0050	1355
STU	N		TERM	356	1355	21	0355	1105
RAU	M	LOOP2		357	1153	60	0200	1165
FMP	PI			358	1165	39	1060	1750
FOV	A			359	1750	34	0103	1803
STU	TEMP1			360	1803	21	0158	1711
FMP	TEMP1			361	1711	39	0158	1208
STU	TEMP1			362	1208	21	0208	1761
RAM	N			363	1761	60	0500	1405
FMP	PI			364	1405	39	0200	1800
FOV	A			365	1800	34	0104	1504
STU	TEMP2			366	1504	21	0258	1811
FMP	TEMP2			367	1811	39	0258	1258
STM	TEMP2			368	1258	21	0258	1861
RAU	KAP90			369	1861	60	0190	0145
FAO	TEMP1			370	0145	32	0158	1585
FAO	TEMP2			371	1585	32	0258	1635
LOO				372	1635	69	0288	1400
STU	GAMMA	EOOAU	CALCULATE	373	0988	21	0288	0195
RAU	TAU		GAMMA MN	374	0195	60	0108	1013
FOV	OL			375	1013	34	1254	1554
FOV	OL			376	1554	34	1254	1604
RAL	8003			377	1604	65	8003	1911
LOO				378	1911	69	0914	1350
RAM	8002	EOOEA		379	0914	60	8002	0973
FOV	GAMMA			380	0973	34	0973	0942
STU	TEMP1			381	0942	21	0158	1961
RAM	M			382	1961	60	1060	1215
FMP	PI			383	1215	39	0200	1850
FDP	A			384	1850	34	0103	1253
FMP	X			385	1253	39	0106	1506
RAL	8003			386	1506	65	8003	1063
LOO				387	1063	69	0266	1150
STL	TEMP2	EOOCH		388	0266	20	0258	0219
RAU	N			389	0219	60	0200	1455
RAM	PI			390	1455	39	0200	1900
FMP	PI		CALCULATE	391	1900	34	0104	1654
FOV	X		TERM	392	1654	39	0200	1850
FMP	X		OF	393	1850	65	8003	1113
LOO			SERIEB	394	1113	69	0916	1150
STL	TEMP3	EOOCH		395	0916	20	0106	1585
RAU	Z	A		396	1585	60	2300	1505
F8B	C			397	1505	33	0105	1081
FMP	GAMMA			398	1081	39	0200	1902
FMP	TFO			399	0992	39	1000	1950
RAL	8003	EOOEA		400	1950	65	8003	1107
LOO				401	1107	69	1100	1350
STL	TEMP4	EOOEA		402	1110	20	0094	1147
RBU	C			403	1147	61	0105	0959
FMP	GAMMA			404	0959	39	0200	1404
FMP	TFO			405	1404	39	1000	1201
RAL	8003	EOOEA		406	1201	65	8003	1009
LOO				407	1009	69	0200	1350
RAU	8002			408	0262	60	8002	1021
FAO	ONE			409	1021	32	0050	1177
STU	TEMP5			410	1177	21	0116	1735
RAU	ONE			411	1735	60	0050	1585
F8B	TEMP4			412	1585	33	0094	1071

	F DV	TEMP5		413	1071	34	1132	1182
	F MP	TEMP1		414	1182	39	0158	1308
	F MP	TEMP2		415	1308	39	0288	1338
	F MP	TEMP3		416	1358	39	1038	1368
	STU	TEMP1		417	1232	21	0158	0912
	RAU	RT TAU		418	0912	60	0050	0282
	F MP	GAMMA		419	0225	33	0925	1029
	STU	PART2		420	1092	21	0920	1163
	RAU	PART1		421	1163	60	0284	1029
	F SR	PART2		422	1029	33	0920	1029
	L DD		E OERF	423	1087	69	0940	1050
	F AO	ONE		424	0940	32	0050	1227
	STU	TEMP3		425	1227	21	0858	1605
	RAU	PART1		426	0962	60	0284	1079
	F AO	PART2		427	1079	32	0920	1137
	L DD		E OERF	428	1137	69	0990	1050
	STU	TEMP3		429	0990	21	1082	1785
	RAU	ONE		430	1785	60	0050	1605
	F SR	TEMP3		431	1605	33	1082	1059
	STU	TEMP3		432	1059	21	1082	1835
	RAU	GAMMA		433	1835	60	0282	1197
	F MP	Z		434	1197	39	2300	1251
	R AL	BOO3	A	435	1251	65	8003	1109
	L DD		E ODEA	436	1109	69	1012	1350
	RAU	BOO2		437	1012	60	8002	1121
	F MP	TEMP3		438	1121	39	1082	1282
	STU	TEMP3		439	1282	21	1082	1885
	R BU	GAMMA		440	1885	61	0282	1247
	F MP	Z	A	441	1247	69	3300	1301
	R AL	BOO3	A	442	1301	65	8003	1159
	L DD		E ODEA	443	1159	69	1012	1350
	RAU	BOO2		444	1022	60	8002	1171
	F MP	TEMP3		445	1171	39	0288	1408
	F AD	TEMP3		446	1408	32	1040	1282
	F MP	TEMP1		447	1209	39	0158	1458
	F DV	ONOW		448	1458	34	0162	1112
	F AO	SERES	ADD TERM	449	1112	32	0282	1282
	STU	SERES	SERIES	450	0293	21	0116	1369
	RAU	HARM		451	1369	60	0109	1213
	F SR	H		452	1213	33	1043	1282
	N Z	CONT3	CONT2	453	1187	45	1040	0291
CONT2	RAU	ONE	ADJUST	454	0291	60	0050	1655
	STU	M	W AND N	455	1655	21	1060	1121
	RAU	HARM	FOR	456	363	60	1040	1313
	F BB	N	NEXT TERM	457	1313	33	0500	1277
	N ZE			458	1277	45	0282	1282
	RAU	N	CONT4	459	0090	60	0500	1705
	F AO	TWO		460	1705	32	1000	1327
	STU	N	LOOP2	461	1327	21	0500	1153
CONT3	RAU	TWO		462	1040	60	1040	1282
	F AO	TWO		463	1265	32	1000	1377
	STU	M	LOOP2	464	1377	21	1060	1153
CONT4	RAU	SERES		465	1153	60	1116	0929
	STU	COFAC		466	0989	21	0144	1297
	RAU	N	A	468	1297	60	2500	1755
	COV	COFAC	A	469	1755	34	0144	0194
	STU	NCOR	A	470	0194	21	2700	1303
	L DD	Z	A	471	1303	69	2300	1353
	STO	1977	A	472	1353	24	1977	0130
	L DD	N	A	473	0130	69	2500	1403
	STO	1978	A	474	1403	24	1978	1181
	L DD	NCOR	A	475	1181	69	2700	1453
	STO	1979	A	476	1453	24	1979	1332
	L DD	COFAC		477	1332	69	0144	1347
	STO	1980		478	1347	24	1980	0083
	L DD	FNECF		479	0083	69	0062	1315
	STO	1981		480	1315	24	1981	0184
	L DD	DI		481	0184	69	1162	1137
	STO	1982		482	1137	24	1982	1935
	PCM	1977		483	1935	71	1977	1427
	EXA	OOO1		484	0027	60	0027	0131
CONT5	NZA	CONT1	CONT5	485	0133	40	0210	1237
	L DD	POINH7		486	1237	69	0101	1704
	RAU	BOO1		487	1704	60	1040	1377
	L DD	ZERO		488	1160	69	0000	1503
	STO	SUMA		489	1503	24	1606	1259
	STO	SMLNA		490	1259	34	1162	1365
	STD	SUMZ		491	1365	24	1018	1271
	STO	SUMZ2		492	1271	24	0274	1477
	STO	SMLNA		493	1477	60	1160	0133
LOOP3	RAU	NCOR	A	494	0183	60	2700	1805
	F AD	SUMA	LOOP3	495	1805	32	1606	0233
	STU	SUMA		496	0233	21	1606	1349
	RAU	NCOR	A	497	1309	60	2700	1855
	L DD		A	498	1855	69	1508	1000
	F AO	SMLNA	A	499	1000	32	1082	1039
	STU	SMLNA		500	1039	21	1162	1415
	RAU	Z	A	501	1415	60	2300	1356
	F AD	SUMZ	FORM BUMS	502	0028	32	0118	0245
	STU	SUMZ	FOR LEABT	503	0245	21	1018	1321
	RAU	Z	BOUAREB	504	1321	60	2300	1356
	F MP	Z	ANALYSIS	505	1356	39	2300	1351
	RAU	SUMZ2		506	1351	32	0274	1401
	STU	SUMZ2		507	1401	21	0274	1401
	RAU	NCOR	A	508	1377	60	2700	1706
	L DD		A	509	1706	69	1359	1100
	F MP	Z	A	510	1359	39	2300	1401
	F AD	ZSMLA		511	1401	32	0180	1207
	STU	ZSMLA		512	1207	21	0180	0883
	EXA	OOO1		513	0883	51	0283	1089
	RAU	SMLNA	CONT6	514	1089	40	0183	0943
CONT6	RAU	SMLNA		515	0943	60	1162	0167
	F MP	SUMZ		516	0167	39	1018	1068

STU TEMP1	517	1068	81	01598	1218
RAU OATPT	518	1212	60	01028	1257
FMP ZOMLA	519	1257	39	01860	09330
STU TEMP2	520	0830	81	02558	1862
RAU OATPT	521	1268	60	01028	1307
FMP SUMZ2	522	1307	39	02774	0924
STU TEMP3	523	0924	21	10882	1985
RAU BUMZ	524	1988	60	1018	1023
FMP SUMZ	525	1023	39	1018	1118
STU TEMP4	526	1118	21	00994	1397
RAU TEMP3	527	1397	60	1082	1287
F88 TEMP4	528	1287	33	00994	1371
STU TEMP3	529	1371	21	10882	0186
RAU TEMP1	530	0186	60	0158	1363
F88 TEMP2	531	1363	33	0258	0236
FOY TEMP3	532	0236	34	10882	1388
STU NWCAM	533	1388	21	0286	1139
FOY 10000	534	1139	34	0950	1501
STU PREC	535	1501	21	1756	1409
RAU GAM11	536	1409	60	1056	1312
F88 NWCAM	537	1312	33	0286	1413
RAW S003	538	1413	67	8003	1421
RAU S002	539	1421	60	0002	1129
F88 PREC	540	1129	33	1756	0933
SMI CONT8	541	0933	46	0936	1337
RAU NWCAM	542	1337	60	0286	0941
STU GAM11	543	0941	21	1056	1459
LOO ZERO	544	1459	69	0000	1553
STO SERE8	545	1553	24	0116	0209
RAU NWCAM	546	0936	60	0286	0991
FMP NWCAM	547	0991	39	0286	0986
STU GAM80	548	0986	21	1090	0993
RAU PI	549	0993	60	0200	1806
FOY A	550	1806	34	0103	1603
STU ALPH2	551	1603	21	1558	1362
FMP ALPH2	552	1362	39	1558	1608
STU ALPH2	553	1608	21	1558	1412
RAU PI	554	1412	60	0300	1856
FOY 8	555	1856	34	0104	1754
STU BETA2	556	1754	21	1658	1462
FMP BETA2	557	1462	39	1658	1708
STU BETA2	558	1708	21	1658	1512
RAU GAM88	559	1512	60	1090	0295
F88 ALPH2	560	0295	33	1558	1036
F88 BETA2	561	1036	33	1658	1086
LOO	562	1086	69	1189	1400
STU KAPPA	563	1189	21	1450	1653
RAU ONE	564	1653	60	0050	1906
FOY KAPPA	565	1906	34	1450	1551
FMP CORVT	566	1551	39	0250	1601
STU OL	567	1601	21	1284	1357
LOO GAM11	568	1357	69	0100	1703
STO 1977	569	1703	24	1977	0280
LOO NWCAM	570	0280	69	0286	1239
STO 1978	571	1239	24	1978	1231
LOO PREC	572	1231	69	1251	0918
STO 1979	573	1509	24	1979	1432
LOO POINT	574	1432	69	0101	1804
STO 1980	575	1804	24	1980	0918
LOO GAM11	576	0918	69	1056	1559
STO 1981	577	1559	24	1981	0834
LOO OL	578	0834	69	1254	1467
STO 1982	579	1407	24	1982	1136
PCN 1977	580	1136	71	1977	8000

CONT7

CONT7

CONT8

LOOP1

GAMMA
SQUAREALPHA
SQUAREBETA
SQUAREKAPPA
SQUARE

E00AU

DIFFUSION
LENGTH

8000

APPENDIX I

IBM 650 Program for Diffusion Length,
Gaussian Range Empirical Source

This program was written to determine the diffusion length based upon an empirically determined source of high energy neutrons. The program was written in SOAP II and floating point form. The object program and a logic diagram are included in this section.

The solution to this problem is based upon the equation

$$\phi(x, y, z) = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \frac{f_i Q_0}{abD \gamma_{mn}} e^{-\frac{\kappa^2 r_i^2}{4}} \left[e^{-\gamma_{mn} z} \left[1 + \operatorname{erf} \left(\frac{z}{r_i} - \frac{\gamma_{mn} r_i}{2} \right) \right] \right. \\ \left. + e^{+\gamma_{mn} z} \left[1 - \operatorname{erf} \left(\frac{z}{r_i} + \frac{\gamma_{mn} r_i}{2} \right) \right] \right] (1 - e^{-2\gamma_{mn}(c-z)})$$

Correction factors C_E and C_H derived from this equation are listed in Table 1. A correction factor iteration, such as has been described previously, is used to obtain an accurate value of γ_{11} and hence the diffusion length.

Input parameters and data are listed in Table 33. All input should be punched on one word load cards and read into the machine with the object deck.

Output forms are listed in Table 34. Form one is punched after calculation of each individual correction factor. Form two gives the end result of the analysis.

The operating time for the calculation of one correction factor using four harmonics is approximately one minute and 30 seconds. The data

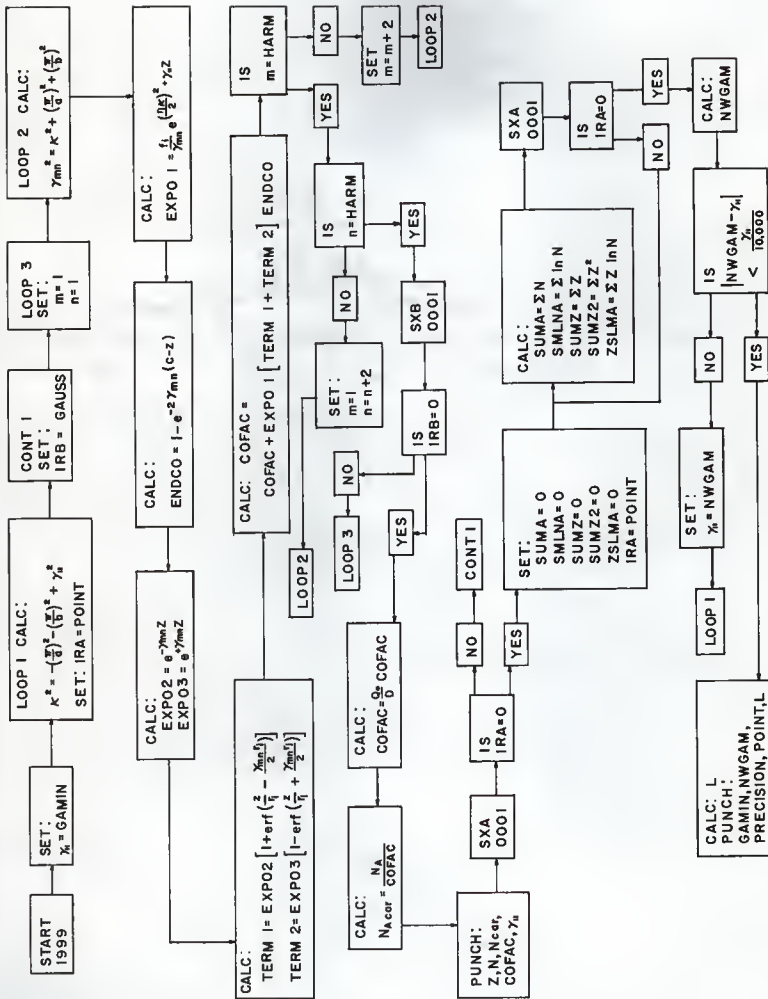
capacity of the program is 200 data points. As many as five sets of Gaussian ranges and fractions may be used.

Table 33. Input parameters and data for IBM 650 program for diffusion length, empirical source method.

Symbol:	Explanation	Drum Storage Location
GAMIN	Initial Estimate of γ_{11}	0100
POINT	No. of Data Points, form 00 0000 00xx	0101
DATPT	No. of Data Points, floating point form	0102
A	Extrapolated x-dimension	0103
B	Extrapolated y-dimension	0104
C	Extrapolated z-dimension	0105
HARM	No. of highest harmonic, floating point form	0106
GAUSS	No. of Gaussian Ranges used, form 00 0000 000x	0107
QO	Source strength	0108
DIFCO	Diffusion Coefficient	0109
RI	Gaussian Range, stored consecutively starting at	0901
FI	Range Fractions, stored consecutively starting at	0906
N	Count Rates, stored consecutively starting at	0501
z	Data co-ordinates, stored consecutively starting at	0301

Table 34. Output forms for IBM 650 program for determination of diffusion length, empirical source method.

WORD 1	2	3	4	5
Form 1:				
z	N	N (corrected)	Combined correction	γ_{11}
Form 2:			No. of Data Points	Diffusion Length
Gamin	γ_{11} , last value	Precision		



LOGIC DIAGRAM, APPENDIX I

	BLR	1951	1961	1	0000				
	BLR	1977	1984	2	0000				
	SLR	0300	0910	3	0000				
	SYN	Z	0300	4	0000				
	SYN	N	0500	5	0000				
	SYN	WFOR	0700	6	0000				
	SYN	RI	0900	7	0000				
	SYN	F1	0905	8	0000				
	SYN	CLMIN	0100	9	0000				
	SYN	POINT	0101	10	0000				
	SYN	OATPT	0102	11	0000				
	SYN	A	0103	12	0000				
	SYN	B	0104	13	0000				
	SYN	C	0105	14	0000				
	SYN	HARM	0106	15	0000				
	SYN	CAUS	0107	16	0000				
	SYN	00	0108	17	0000				
	SYN	DIFFCO	0109	18	0000				
	SYN	START	1999	19	0000				
		00	0000	20	0000				
ZERO	ONE	10	0000	0051	10	0000	0051		
TWO		20	0000	0052	20	0000	0052		
THREE		30	0000	0053	30	0000	0053		
PI		31	4159	0054	31	4159	0054		
CONVT		35	3600	0055	35	3600	0055		
10000		10	0000	0055	10	0000	0055		
EOOEA				26	1050	24	0003	0066	
	STO	AAA1		88	0066	30	0011	0064	
	RAM	AAA2		29	0014	67	0011	0015	
	STL	AAA3		30	0015	80	0019	0028	
	RAA	AAA3		31	0022	60	0019	0023	
	FMP	AAA16		32	0023	39	0026	0076	
	FAO	AAA15		33	0076	32	0029	0005	
	FMP	AAA3		34	0005	39	0019	0009	
	FAO	AAA14		35	0009	32	0072	0049	
	FMP	AAA3		36	0049	39	0019	0119	
	FAO	AAA3		37	0119	32	0129	0099	
	FMP	AAA3		38	0099	39	0019	0169	
	FAO	AAA19		39	0169	32	0172	0149	
	FMP	AAA3		40	0149	39	0019	0219	
	FAO	AAA11		41	0219	32	0222	0199	
	FMP	AAA3		42	0199	39	0019	0269	
	FAO	AAA10		43	0269	32	0272	0249	
	STU	AAA4		44	0249	81	0004	0007	
	FMP	AAA4		45	0007	39	0004	0054	
	STU	AAA4		46	0054	81	0004	0057	
	FMP	AAA4		47	0057	39	0004	0154	
	STU	AAA4		48	0154	21	0004	0157	
	RAU	AAA2		49	0157	60	0004	0204	
	RAM	AAA5		50	0065	46	0018	0919	
AAA5	RAU	AAA10	AAA6	51	0018	60	0272	0027	
	FOV	AAA4		52	0027	34	0004	0204	
	STU	AAA4		53	0204	21	0004	0919	
AAA6	RAL	AAA4	AAA6	54	0919	65	0004	0003	
AAA10		10	0000	0051	55	0272	10	0000	0051
AAA11		22	0909	0650	56	0272	34	9998	6850
AAA12		31	2575	8349	57	0172	11	2575	8349
AAA13		25	9137	1248	58	0122	25	9137	1248
AAA14		17	1562	0047	59	0072	17	1568	0047
AAA15		54	3020	0045	60	0029	54	3020	0045
AAA16		69	0600	0044	61	0036	69	0600	0044
LNX01	STO	LNX08		62	1100	24	0003	0056	
	HZE		LNX14	63	0056	43	0010	0061	
	BHI	LNX14		64	0010	46	0061	0064	
	STU	LNX09		65	0064	21	0068	0021	
	RSL	FPONE		66	0024	66	0024	0079	
	STO	LNX10		67	0079	24	0032	0035	
	FMP	LNX02		68	0035	60	0035	0042	
	RAU	LNX09		69	0042	60	0068	0073	
	STL	LNX05		70	0073	80	0077	0030	
	STL	LNX12		71	0030	20	0085	0068	
	SLT	0008		72	0038	35	0008	0207	
	SUP	FIFTY		73	0207	11	0060	0115	
	HZE		LNX04	74	0115	45	0071	0649	
	BMI		LNX03	75	0118	46	0071	0922	
	RSU	8003		76	0071	61	8003	0129	
	LOO	FPONE		77	0129	69	0024	0127	
	STO	LNX02		78	0024	24	0039	0922	
LNX03	BCT	0008		79	0922	30	0008	0041	
	BCT	0000		80	0041	26	0000	0013	
	AUT	LKT7		81	0013	10	0016	0021	
	SUP	8002		82	0121	11	8008	0179	
	RAU	8003		83	0179	60	8003	0037	
	FMP	LNX02		84	0037	39	0039	0089	
	FMP	LXTEN		85	0089	39	0092	0142	
LNX04	STU	LNX05	LNX04	86	0142	21	0077	0969	
	RAU	LNX02		87	0969	30	0069	0123	
	BRT	0002		88	0123	30	0002	0229	
	RAU	8002		89	0229	60	8002	0087	
	STU	FIFTY		90	0087	15	0060	0165	
	SLT	0002		91	0165	35	0002	0171	
	FAO	FPONE		92	0171	22	0024	0001	
	STU	LNX09		93	0001	93	0001	0921	
	F8B	FPTW0		94	0221	33	0074	0051	
	FOY	LNX09		95	0051	34	0068	0168	
	STU	LNX13		96	0168	24	0068	0023	
	STO	LNX12		97	0023	24	0028	0031	
	STO	LNX11		98	0031	24	0085	0088	
	FMP	8001		99	0088	30	0081	0099	
	STU	FACTR	LNX06	100	0091	21	0046	0299	
LNX06	RAU	LNX10		101	0299	60	0032	0137	
	STU	TWO		102	0137	32	0114	0137	
	STU	LNX10		103	0151	21	0032	0135	

RAU	LNX13		104	0135	60	0978	0177	
FMP	FACT		105	0177	39	0046	0435	
FOV	LNX10		106	0096	34	0032	0088	
FTU	LNX13		107	0088	21	0972	0078	
FTU	LNX12		108	0075	32	0078	0085	
GTU	LNX12		109	0055	21	0088	0081	
F88	LNX11		110	0081	33	0085	0111	
FOV	LNX11		111	0111	24	0085	0185	
RAW	8003		112	0133	33	0085	0133	
RAU	8002		113	0043	60	8002	0201	
F88	81ZE7		114	0201	33	0854	0133	
BMI	LNX07		115	0133	33	0085	0133	
L00	LNX12		116	0235	69	0028	0181	
STU	LNX11		117	0181	84	0085	0138	
RAU	LNX13		118	0138	60	0972	0287	
FMP	LNX10		119	0287	39	0032	0138	
STU	LNX13	LNX06	120	0138	81	0972	0299	
RAU	LNX12		121	0034	60	0086	0033	
FMP	FPTW0		122	0033	39	0074	0124	
F88	LNX05	LNX08	123	0124	33	0077	0053	
IO	T0000	0051	124	0059	10	0004	0087	
FPTW0	20	0000	0051	125	0074	20	0000	0051
81ZE7	10	0000	0043	126	0854	10	0000	0043
LWTEM	23	0288	5151	127	0052	23	0288	5151
FIFTV	50	0000	0000	128	0060	50	0000	0000
8IXTV	00	0000	0060	129	0016			60
LWX14	01	2345	6789	130	0061	1	2345	6789
E00CR	STO	EXIT	131	1150	84	0153	0156	
RAU	8002		132	0156	60	8002	0215	
NEGAT	FAO	THOP1	133	0215	46	0215	0215	
NEGAT	FAO	THOP1	134	0218	32	0271	0047	
BMI	NEGAT		135	0047	46	0218	0251	
REUC	F8R	THOP1	136	0251	33	0972	0133	
REUC	F8R	THOP1	137	1019	33	0271	0097	
BMI	ONEPI	REUC	138	0097	46	1200	1019	
COBIO	STU	THETA	139	1200	32	0972	0133	
COBIO	RSU	FPHONE	140	0231	21	0036	0139	
STU	TERMUM		141	0139	61	0024	0279	
STU	FUNKT		142	0279	21	0004	0087	
STU	FUNKT		143	0187	21	0192	0045	
STL	ENNN	NEGBT	144	0045	20	0949	0002	
E00BR	STO	ENNT	145	0250	24	0150	0150	
RAU	8002		146	0206	60	8002	0265	
BMI	NEGAV	REUCO	147	0265	46	0268	1069	
NEGAV	FAO	THOP1	148	0268	32	0271	0097	
NEGAV	BMI	NEGAV	149	047	46	0268	0951	
REUCO	F88	ONEPI	150	0951	33	0954	0281	
REUCO	F88	THOP1	151	1069	32	0024	0279	
BMI	ONEPI	REUCO	152	0197	46	1500	1069	
FAO	ONEPI	REUCO	153	1300	32	0954	0281	
STU	THETA		154	0281	21	0036	0189	
RSU	8003		155	0199	61	8003	0247	
STU	TERMUM		156	0247	21	0084	0237	
STU	FUNKT		157	0237	21	0192	0095	
L00	FPHONE		158	0095	69	0954	0281	
STO	ENNN	NEGBT	159	0277	24	0949	0002	
RAU	ENNN		160	0002	60	0949	0203	
STU	NPOME		161	0203	32	0024	1001	
FAO	FPHONE		162	1001	21	0256	0009	
FAO	FPHONE		163	0009	32	0024	1051	
STU	ENNN		164	1051	21	0949	0052	
RSU	TERMUM		165	0052	61	0084	0239	
FMP	THETA		166	0239	39	0036	0086	
FMP	THETA		167	0086	39	0036	0136	
FOV	NPOME		168	0136	34	0256	0956	
FOV	ENNN		169	0956	34	0949	0999	
STU	TERMUM		170	0999	21	0084	0287	
RAM	FUNKT		171	0287	67	0192	0297	
STL	FMAG		172	0297	20	1101	1004	
STU	TERMUM		173	1004	67	1004	0289	
RAU	8002		174	0289	60	8002	0947	
FOV	FMAG		175	0947	34	1101	1151	
F88	81ZE7		176	1151	34	1101	0281	
FM	ENNT		177	0931	46	0134	0285	
RAU	FUNKT		178	0285	60	0192	0997	
FAO	TERMUM		179	0997	34	0084	0287	
STU	FUNKT	NEGBT	180	0161	21	0129	0002	
RAL	FUNKT	EXIT	181	0134	65	0192	0153	
81ZE7	10	0000	0043	182	1054	10	0000	0043
THOP1	6	0000	5351	183	0271	52	0192	0151
ONEPI	31	4159	2751	184	0954	31	4159	2751
FPHONE	6	10	0000	185	0024	10	0000	0024
E00AU	STO	ENNT	1	186	46	0134	0285	
BMI	SERR		2	187	1006	46	0059	0110
NZE	SA	SEXT	3	188	0110	25	0114	0283
STL	SA		4	189	0114	32	0174	0221
FAO	810		5	190	0921	32	0174	1201
FMP	8HAF	SB	6	191	1101	39	1104	1244
FAO	8BAV	SAS	7	192	1154	21	0008	0211
RAU	BA	B CAPT A	8	193	0211	60	0918	0173
FOV	8BAV		9	194	0173	34	0098	0258
FAO	8BAV		10	195	0058	32	0008	0935
FMP	8HAF		11	196	0935	39	1104	1204
F88	8BAV		12	197	1204	33	0004	0935
NZU	8BAV		13	198	0995	44	0939	0040
BMI		SR	14	199	0939	46	0242	0040
FAO	8BAV	SAB	15	200	0242	32	0028	0235
FAO	8BAV	SAB	16	201	1035	21	0008	0211
RAU	8BAV	SEXT	17	202	0040	60	0008	0253
SERR	HLT	SEXT	18	203	0059	10	0000	0285
8HAF	10	0000	0050	19	004	50	0000	0050
810	10	0000	0051	20	205	10	0000	0051
E00RF	STO	OUT		206	1400	24	0953	1056

	BMI	NGTVE	PBTVE	807	1056	46	0159	0160
NGTVE	STU	TEW1		2008	0159	21	0164	0017
	RAU	TEW1		2010	0177	67	0164	0177
	RAU	8002		210	1119	60	8002	0927
	STU	ARGG		211	0927	21	0182	1085
	LOO	MUNIT		212	1085	39	0185	0141
	STU	COEFF	APPRO	213	0141	24	0044	1047
	STU	ARGG		214	0160	21	0182	1135
PBTVE	LOO	MUNIT		215	1135	69	0238	0191
	STU	COEFF	APPRO	216	0191	84	0044	1047
	RAU	ARGG		217	1047	60	0182	0937
	FMP	A6AA		218	0937	39	0185	0140
APPRO	FAO	A3AA		219	0140	32	0093	1169
	FMP	ARGG		220	1169	39	0182	0232
	FAD	A4AA		221	0232	32	1185	0261
	FMP	ARGG		222	0261	39	0185	0883
	FAO	A3AA		223	0282	32	1235	0911
	FMP	ARGG		224	0911	39	0188	0932
	FAD	A2AA		225	0932	32	1285	0961
	FMP	ARGG		226	0961	39	0182	0982
	FAD	A3AA		227	0982	32	1335	1011
	FMP	ARGG		228	1011	39	0182	1032
	FAO	UNIT		229	1032	32	0238	0915
	FMP	8003		230	0915	39	8003	1219
	FMP	8003		231	1219	39	8003	0223
	FMP	8003		232	0223	39	8003	0977
	FMP	8003		233	0977	39	8003	0981
	STU	TEW1		234	0981	21	0164	0067
	RAU	UNIT		235	0067	60	0238	0143
	FOV	TEW1		236	0143	34	0164	0214
	STU	TEW1		237	0214	67	0164	0177
	RAU	UNIT		238	0117	60	0238	0193
	FBB	TEW1		239	0193	33	0164	0241
	FMP	COEFF	OUT	240	0241	39	0085	0183
	FMP	COEFF		241	1335	70	5230	7849
A1AA	7D		7849	242	1285	42	2820	1249
A2AA	42	2820	1249	243	1235	72	7052	7248
A3AA	92	7052	7248	244	844	15	2014	3047
A4AA	15	2014	3047	245	185	15	2014	3047
A5AA	27	6567	2047	245	0093	27	6567	2047
A6AA	43	0638	0046	246	0090	43	0638	0046
UNIT	10	0000	0051	247	0238	10	0000	0051
MUNIT	10	0000	0051	248	0188	10	0000	0051
START	LOO	GAMM		249	1999	69	0100	1003
	STU	GAMM	LOOP1	250	1003	84	0100	0250
LOOP1	RAU	P1		251	0250	60	0250	0155
	FOV	A		252	0155	34	0103	1053
	STU	8003		253	1053	39	8003	0257
	STU	TEMP1		254	0257	21	0012	0965
	RAU	P1		255	0965	60	0250	0205
	FOV	B		256	0205	34	0205	1254
	FMP	8003		257	1254	39	8003	0957
	STU	TEMP2		258	0957	21	0062	1015
	RAU	GAMM		259	1015	69	1015	1061
	FMP	8003		260	1061	39	8003	1065
	FBB	TEMP1	CALCULATE	261	1065	33	0012	0989
	FBB	TEMP2	KAPPA	262	0989	103	0062	1047
	STU	KAP80	ROUAREO	263	1039	21	0094	1097
	LOO	POINT		264	1097	69	0101	1304
CONT1	RAA	8002	CONT1	265	1304	80	8001	0210
	LOO	GAMM		266	0210	69	0107	0260
	RAB	8001		267	0260	82	8001	0066
LOOP3	LOO	ONE	LOOP3	268	0066	69	0050	1103
	STO	M		269	1103	84	1156	0259
	STO	N		270	0259	24	0500	1153
LOOP2	RAU	M	LOOP2	271	1153	60	1156	1111
	FMP	P1		272	1111	39	0280	0750
	FOV	A		273	1450	34	0103	1203
	FMP	8003		274	1203	39	8003	1007
	STU	ALPH2		275	1007	21	0111	1115
	RAU	M		276	1115	60	0500	0255
	FMP	P1		277	0255	39	0250	1500
	FOV	B		278	1500	34	0104	1354
	FMP	8003		279	1354	39	8003	1057
	STU	BETA2		280	1057	21	0162	1165
	FAD	ALPH2		281	1165	32	0162	1389
	FAD	KAP80		282	1089	32	0094	0971
	LOO			283	0971	69	0224	1350
	STU	GAMM	EOGAU	284	0224	21	0078	1014
	RAU	R1	CALCULATE	285	1031	60	4900	0958
	FOV	TWO	GAMMA MN	286	0958	34	0150	1550
	FMP	8003		287	1550	60	8003	1263
	FMP	KAP80		288	1263	39	0094	0144
	STU	TEMP1		289	0144	21	0012	1215
	RAU	Z		290	1215	80	0300	0066
	FAO	AH11	A	291	1005	39	1106	1206
	FAD	TEMP1		292	1208	32	0012	1139
	FAL	8003		293	1139	65	8001	0147
	LOO	R		294	1147	69	1600	1050
	RAU	F	EOOE A	295	1800	60	8008	0959
	FMP	GAMM		296	0959	39	4900	1053
	STU	EXPOL	B	297	1053	34	0078	0128
	RAU	Z		298	0128	21	1082	1385
	FBB	C	A	299	1385	60	2385	1095
	FMP	TWO		300	1105	33	0105	1081
	FMP	GAMM		301	1081	39	0150	1450
	FAL	8003		302	1450	60	0078	0178
	LOO		EOOE A	303	0178	65	8003	1435
	RBO	ONE		304	1435	69	0288	1050
	FAO	8002		305	0288	61	8008	1597
	STU	TEMP1		306	1197	32	0050	1027
	RBO	C		307	1027	21	0012	1265
	FMP	TWO		308	1265	81	0100	1009
	FMP	GAMM		309	1009	39	0150	1700
	FMP	GAMM		310	1700	39	0078	0228

	RAU	8003			311	0228	65	8003	1485
	LOO	8002	EOEEA		312	1485	69	0938	1050
	RAU	8002			313	0938	60	8002	1247
	FAO	ONE			314	1247	32	0050	1077
	STU	TEMP2			315	1077	21	0062	1315
	RAU	TEMP1		END	316	1315	60	1312	1037
	FDV	TEMP2		CORRECTION	317	0167	34	0062	0812
	STU	ENOCO		FACTOR	318	0212	21	0116	1269
	RSU	Z	A		319	1269	61	1269	1545
	FMP	GAMMN			320	1155	39	0078	0278
	STU	ARG			321	0278	21	1132	1535
	RAU	ARG			322	1535	65	1535	0927
	LOO		EOEEA		323	0927	69	0190	1050
	STL	EXP02			324	0190	20	0145	0048
	RAM	ARG			325	0048	67	1132	1205
	LOO		EOEEA		326	1037	69	0240	1050
	STL	EXP03			327	0240	20	0195	0098
	RAU	Z	A		328	0098	60	4900	1255
	FOV	NI	B		329	1205	34	4900	1750
	STU	TEMP1			330	1750	21	0012	1365
	RAU	RI	B		331	1365	60	4900	1255
	FMP	GAMMN			332	1255	39	0078	0920
	FOV	TWO			333	0928	34	0150	1800
	STU	TEMP2			334	1800	21	0062	1415
	RAU	TEMP1			335	1415	60	0012	0237
	FSR	TEMP2			336	0217	33	0062	1189
	LOO		EOERF		337	1189	69	0246	1400
	FAO	ONE			338	0292	32	0050	1127
	FMP	EXP02			339	1127	39	0145	0245
	STU	TERM1			340	0245	21	1850	1503
	RAU	TEMP1			341	1339	60	0012	0267
	FAD	TEMP2			342	0267	32	0062	1239
	LOO		EOERF		343	1239	69	0942	1400
	STU	TEMP1			344	0942	21	0042	1464
	RAU	ONE			345	1465	60	0050	1305
	FSR	TEMP1			346	1305	33	0012	1289
	FMP	ENOCO			347	1289	39	1289	0295
	FAD	TERM1			348	0295	32	1850	1177
	FMP	EXP02			349	1177	39	1082	1182
	FMP	ENOCO			350	1182	39	0102	1131
	FAO	COFAC		CORRECTION	351	0166	32	1319	0945
	STU	COFAC		FACTOR	352	0945	21	1319	1022
	RAU	HARM			353	1022	60	0102	1131
	FSR	M			354	1161	33	1156	0083
	NZE		CONT2		355	0083	45	0186	1087
	RAU	M			356	0186	60	1156	1531
	FAO	TWO			357	1211	32	0150	1227
	STU	M	LOOP2		358	1227	21	1156	1153
	RAU	HARM			359	1087	60	1087	0261
	FSR	N			360	1261	33	0500	1277
	NZE		CONT3		361	1277	45	0080	1131
	RAU	N			362	0080	60	0062	1562
	FAO	TWO			363	1355	32	0150	1327
	STU	N	LOOP2		364	1357	21	0500	1153
	SKX	0001			365	1131	15	0001	1337
	NZB	LOOP3			366	1137	42	0062	0291
	RAU	00			367	0291	60	0108	0063
	FOV	DIFCO			368	0063	34	0109	1059
	FOV	A			369	1059	34	0103	1353
	FOV	B			370	1353	34	0104	1404
	FMP	COFAC			371	1404	39	1311	1369
	STU	COFAC			372	1369	21	1319	1072
	RAU	N	A	CALCULATE	373	1072	60	2500	1405
	FOV	COFAC		CORRECTED	374	1405	34	1319	1419
	STU	NCOR	A	DATA	375	1419	21	2700	1403
	LOO	Z	A		376	1403	69	2300	1453
	STO	1977			377	1453	24	1977	0130
	LOO	N	A		378	0130	69	2500	1503
	STO	1978			379	1503	24	1978	1181
	LOO	NCOR	A		380	1181	29	2700	1553
	STO	1979			381	1553	24	1979	1452
	LOO	COFAC			382	1232	69	1319	1122
	STO	1980			383	1122	24	1980	0133
	LOO	GAM11			384	0133	69	0106	1049
	STO	1981			385	1109	24	1981	0184
	PCH	1977			386	0184	71	1977	1377
	LOO	ZERO			387	1377	69	0001	1603
	STO	COFAC			388	1603	24	1319	1172
	SKX	0001	CONT5		389	1172	51	0000	0978
	LOO	CONT1			390	0978	40	0500	1653
	LOO	POINT			391	1282	69	0101	1454
	RAA	8001			392	1454	80	8001	0960
	STO	SUM1			393	0960	69	0001	1653
	STO	SUMA			394	1653	24	1256	1159
	STO	BMLNA			395	1159	24	0262	1515
	STO	SUMZ			396	1515	24	0262	1422
	STO	SUMZ2			397	1021	24	0274	1227
	STO	ZSMLA	LOOP4		398	1427	24	0180	0183
	STO	SUMZ			399	0183	60	2700	1503
	FAO	SUMA	A		400	1455	32	1256	0233
	STU	SUMA			401	0233	21	1256	1209
	RAU	NCOR			402	1209	60	2700	1503
	LOO		LNxD1		403	1505	69	0119	1030
	FAD	BMLNA			404	0158	32	0262	1339
	STU	BMLNA			405	1339	21	0262	1525
	RAU	Z	A	FORM SUMS	406	1525	60	3300	0555
	FAD	SUM2		FOR LEAST	407	1555	32	0262	0995
	STU	SUM2		SQUARES	408	0995	21	0995	1081
	RAU	Z	A	ANALYSIS	409	1071	60	2300	1605
	FMP	Z	A		410	1605	39	2300	1900
	FAO	SUM12			411	1900	32	0274	1231
	STU	SUM12			412	1251	21	0274	1477

RAU	NCOR	A		413	1477	60	2700	1655
LOD			LNK01	414	1555	69	0208	1100
FMP	Z	A		415	0208	39	0208	1950
FAO	Z8MLA			418	1950	30	0180	1107
STU	Z8MLA			417	1107	01	0180	0283
874	OD D1			418	0083	51	001	1389
NZA	LOOP4		CONT6	419	1389	40	0183	0243
RAU	S8LNA			480	0043	60	0262	0917
FMP	SUM1			401	0917	39	0968	1058
STU	TEMP1			422	1018	01	0012	1615
RAU	DATPT			423	1615	60	0100	1157
FMP	Z8MLA			424	1157	39	0180	0230
STU	TEMP0			425	0230	21	0052	1665
RAU	DATPT			426	1665	60	0102	1807
FMP	SUM22			407	1007	39	0074	0924
STU	TEMP3			428	0924	21	1028	1831
RAU	SUM2			429	1031	60	0968	0073
FMP	SUM2			430	0973	39	0968	1068
STU	TEMP4			431	1068	01	1022	0113
RAU	TEMP3			432	0125	60	1028	0933
F88	TEMP4			433	0933	33	1228	1049
STU	TEMP3			434	1049	31	1028	1881
RAU	TEMP1			435	1081	60	0012	0967
F88	TEMP2			436	0967	33	0060	1439
FOV	TEMP3			437	1439	34	0228	1078
STU	NWGAM			438	1078	21	1332	1585
FOV	10000			439	1585	34	1000	1301
STU	PREC			440	1301	21	1306	1259
RAU	GAM11			441	1859	60	1106	1311
F88	NWGAM			442	1311	33	1332	1309
RAU	S003			443	1309	67	8003	1017
RAU	S002			444	0175	60	8002	0175
F88	PREC		CONT7	445	0983	36	0036	1187
SM1	CONT8			446	0983	46	0036	1187
RAU	NWGAM		LOOP1	447	1187	60	1332	1037
STU	GAM11			448	1237	21	1106	0209
RAU	NWGAM			449	0236	60	1332	1287
FMP	NWGAM		CAMMA	450	1287	39	1332	1382
STU	GAM30		SQUARE0	451	1380	01	0286	1489
RAU	PI			452	1489	60	0250	1703
FOV	A			453	1703	34	0103	1703
STU	ALPH2		ALPHA	454	1715	39	0112	1715
FMP	ALPH2		SQUARE0	455	1715	39	0118	0910
STU	ALPH0			456	0912	21	0112	1765
RAU	PI			457	1765	60	0250	1755
FOV	B			458	1755	34	0104	1504
STU	SETA0			459	1504	01	0162	1815
FMP	SETA2		BETA	460	1815	39	0162	0968
STU	SETA0		SQUARE0	461	0962	21	0162	1865
RAU	GAM30			462	1865	60	0086	0941
F88	ALPH0		KAPPA	463	0941	33	0112	1539
F88	SETA2		SQUARE0	464	1539	33	0160	1589
LOD			E00AU	465	1589	39	0922	1350
STU	KAPPA			466	0990	01	0146	1099
RAU	ONE			467	1099	60	0050	1805
FOV	KAPPA			468	1803	34	0146	0136
FMP	CONVT		DIFFUSION	469	0196	39	0950	1361
STU	OL		LENGTH	470	1351	21	1356	1339
LOD	GAMIN			471	1359	69	0100	1753
STO	1977			472	1753	24	1977	0280
LOD	NWGAM			473	0080	69	1328	1635
STO	1978			474	1635	24	1978	1331
LOD	PREC			475	1331	69	1306	1409
STO	1979			476	1409	24	1979	1432
LOD	POINT			477	1430	49	0101	1534
STO	1980			478	1534	04	1980	1033
LOD	OL			479	1033	69	1356	1459
STO	1981			480	1459	24	1981	0040
PCM	1977		8000	481	0034	71	1977	8000

APPENDIX J

IBM 650 Program for Determination of Material Buckling and Effective Multiplication Factor

This code was written to determine the material buckling, B_m^2 , and the effective multiplication factor, k_{eff} , in the KSU exponential pile. The program was written in SOAP II and floating point form. The object program and a logic diagram are included in this section.

The program is based upon the point thermal source solution to the thermal diffusion equation. An accurate value of γ_{11} is determined by the iteration procedure outlined previously using the correction factors listed in Table 1. B_m^2 is calculated from the equation

$$B_m^2 = \left(\frac{\pi}{a}\right)^2 + \left(\frac{\pi}{b}\right)^2 - \gamma_{11}^2.$$

The program then calculates the infinite multiplication factor, k_∞ , from

$$k_\infty = 1 + B_m^2 (L_t^2 + \tau).$$

The effective multiplication factor, k_{eff} , can then be calculated from

$$k_{eff} = \frac{k_\infty e^{-B_G^2 \tau}}{1 + B_G^2 L_t^2}$$

where B_G^2 is the geometric buckling. By increasing the effective dimensions of the multiplying medium, k_{eff} can be extrapolated to critical pile size. This is done by reading in new values for a , b , and d and starting the program over at CON11 by means of a transfer card.

Input forms for this program are given in Table 35. All input should be in the form of one word load cards.

Table 35. Input forms for IBM 650 program for material buckling and effective multiplication factor.

Symbol	Explanation	Drum Storage Location
FIRST	Initial estimate of γ_{11}	0100
POINT	Number of Data Points, form 00 0000 00xx	0101
DATPT	Number of Data Points, floating point form	0102
A	Extrapolated x-dimension	0103
B	Extrapolated y-dimension	0104
C	Extrapolated z-dimension	0105
X	x co-ord of data	0106
Y	y co-ord of data	0107
L	Lattice diffusion length	0108
TAU	Fermi age	0109
D	z dimension of active lattice	0110
N	Count Rates, to be stored consecutively, starting at	0501
z	Data co-ordinates, to be stored consecutively, starting at	0301

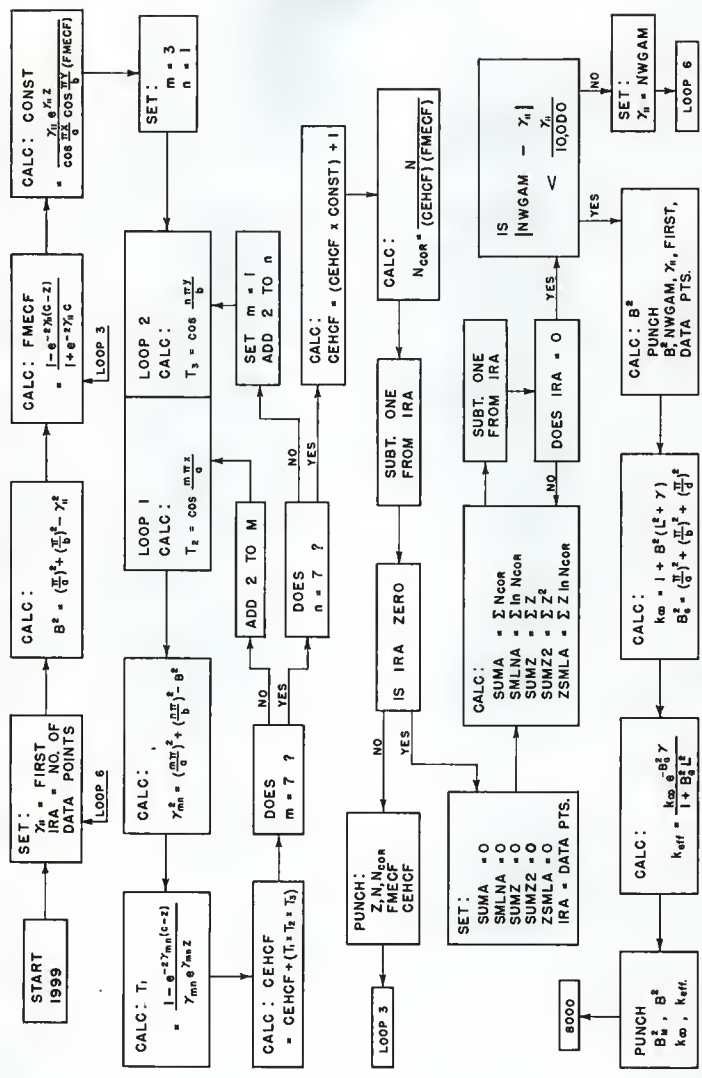
Output from this program is in three forms. Form one is punched after calculation of each correction factor. Form two is the results of the buckling calculation. Form three gives the buckling and the multiplication factors. Table 36 lists the output forms.

Table 36. Output forms for IBM 650 program for material buckling and effective multiplication factor.

WORD	1	2	3	4	5
Form 1:					
z		N	N (corrected)	C_H	C_E
Form 2:					
B_m^2		γ_{11} , last value	γ_{11} , next to last value	γ_{11} , initial value	No. of Data Points
Form 3:					
B_m^2		B_G^2	k_∞	k_{eff}	--

The operating time necessary to calculate the correction factor for one data point using four harmonics is approximately 45 seconds. The capacity of the program is 200 data points.

Logic Diagram for I.B.M. 650 Program for Material Buckling, B_m^2 , and Multiplication Factor, k_{eff} .



LOGIC DIAGRAM, APPENDIX J

OBJECT PROGRAM - APPENDIX J

	HLR 1951	1958	1	8000	00	0000	0000
	HLR 1977	1984	8	0000	00	0000	0000
	BLN 0300	0900	J	0000	00	0000	0000
	SYN FIRST	0100	4	0000	00	0000	0000
	SYN POINT	0101	INDEX FORM	0000	00	0000	0000
	SYN OATPT	0102	DATA FORM	6	0000	00	0000
	SYN A	0103	X DIMEN	7	0000	00	0000
	BYN B	0104	Y DIMEN	8	0000	00	0000
	SYN C	0105	Z DIMEN	9	0000	00	0000
	SYN Y	0106	DATA	10	0000	00	0000
	SYN V	0107	COORDINATE	11	0000	00	0000
	SYN L	0108	DIFFUSION	12	0000	00	0000
	SYN TAU	0109	FERMI ARE	13	0000	00	0000
	SYN O	0110		14	0000	00	0000
	SYN Z	0208		15	0000	00	0000
	SYN N	0508		16	0000	00	0000
	SYN NCOR	0700		17	0000	00	0000
	SYN START	1999		18	0000	00	0000
ZERO	00	0000		19	0000	00	0000
ONE	10	0000		20	0000	00	0000
TWO	20	0000		21	0150	20	0000
THREE	30	0000		22	0200	20	0000
FOUR	40	0000		23	0250	30	0000
FIVE	50	0000		24	0300	30	0000
SIX	60	0000		25	0350	31	4160
SEVEN	70	0000		26	0400	70	0000
EIGHT	80	0000		27	1050	25	3600
NINE	90	0000		28	1100	10	0000
TEN	100	0000		29	1150	24	0000
ELEVEN	110	0000		30	0000	64	0000
TWELVE	120	0000		31	0012	24	1977
THIRTEEN	130	0000		32	0018	24	1978
FOURTEEN	140	0000		33	0022	24	1979
FIFTEEN	150	0000		34	0023	24	1980
SIXTEEN	160	0000		35	0024	24	1981
SEVENTEEN	170	0000		36	0025	24	1982
EIGHTEEN	180	0000		37	0026	24	1983
NINETEEN	190	0000		38	0027	24	1984
TWENTY	200	0000		39	0028	24	1985
ONE AND ONE TENTH	210	0000		40	0029	24	1986
TWO AND ONE TENTH	220	0000		41	0030	24	1987
THREE AND ONE TENTH	230	0000		42	0031	24	1988
FOUR AND ONE TENTH	240	0000		43	0032	24	1989
FIVE AND ONE TENTH	250	0000		44	0033	24	1990
SIX AND ONE TENTH	260	0000		45	0034	24	1991
SEVEN AND ONE TENTH	270	0000		46	0035	24	1992
EIGHT AND ONE TENTH	280	0000		47	0036	24	1993
NINE AND ONE TENTH	290	0000		48	0037	24	1994
TEN AND ONE TENTH	300	0000		49	0038	35	0008
ONE AND TWO TENTH	310	0000		50	0039	11	0006
TWO AND TWO TENTH	320	0000		51	0040	45	0068
THREE AND TWO TENTH	330	0000		52	0041	46	0071
FOUR AND TWO TENTH	340	0000		53	0042	61	0074
FIVE AND TWO TENTH	350	0000		54	0043	69	0024
SIX AND TWO TENTH	360	0000		55	0044	24	0039
SEVEN AND TWO TENTH	370	0000		56	0045	20	0039
EIGHT AND TWO TENTH	380	0000		57	0046	60	0018
NINE AND TWO TENTH	390	0000		58	0047	20	0023
TEN AND TWO TENTH	400	0000		59	0048	20	0035
ONE AND THREE TENTH	410	0000		60	0049	20	0035
TWO AND THREE TENTH	420	0000		61	0050	35	0008
THREE AND THREE TENTH	430	0000		62	0051	11	0007
FOUR AND THREE TENTH	440	0000		63	0052	45	0068
FIVE AND THREE TENTH	450	0000		64	0053	46	0071
SIX AND THREE TENTH	460	0000		65	0054	61	0074
SEVEN AND THREE TENTH	470	0000		66	0055	69	0024
EIGHT AND THREE TENTH	480	0000		67	0056	24	0039
NINE AND THREE TENTH	490	0000		68	0057	20	0039
TEN AND THREE TENTH	500	0000		69	0058	60	0018
ONE AND FOUR TENTH	510	0000		70	0059	20	0023
TWO AND FOUR TENTH	520	0000		71	0060	20	0035
THREE AND FOUR TENTH	530	0000		72	0061	35	0008
FOUR AND FOUR TENTH	540	0000		73	0062	11	0007
FIVE AND FOUR TENTH	550	0000		74	0063	45	0068
SIX AND FOUR TENTH	560	0000		75	0064	46	0071
SEVEN AND FOUR TENTH	570	0000		76	0065	61	0074
EIGHT AND FOUR TENTH	580	0000		77	0066	69	0024
NINE AND FOUR TENTH	590	0000		78	0067	24	0039
TEN AND FOUR TENTH	600	0000		79	0068	20	0039
ONE AND FIVE TENTH	610	0000		80	0069	60	0018
TWO AND FIVE TENTH	620	0000		81	0070	20	0023
THREE AND FIVE TENTH	630	0000		82	0071	20	0035
FOUR AND FIVE TENTH	640	0000		83	0072	35	0008
FIVE AND FIVE TENTH	650	0000		84	0073	46	0071
SIX AND FIVE TENTH	660	0000		85	0074	61	0074
SEVEN AND FIVE TENTH	670	0000		86	0075	69	0024
EIGHT AND FIVE TENTH	680	0000		87	0076	24	0039
NINE AND FIVE TENTH	690	0000		88	0077	20	0039
TEN AND FIVE TENTH	700	0000		89	0078	60	0018
ONE AND SIX TENTH	710	0000		90	0079	20	0023
TWO AND SIX TENTH	720	0000		91	0080	20	0035
THREE AND SIX TENTH	730	0000		92	0081	35	0008
FOUR AND SIX TENTH	740	0000		93	0082	11	0007
FIVE AND SIX TENTH	750	0000		94	0083	45	0068
SIX AND SIX TENTH	760	0000		95	0084	46	0071
SEVEN AND SIX TENTH	770	0000		96	0085	61	0074
EIGHT AND SIX TENTH	780	0000		97	0086	69	0024
NINE AND SIX TENTH	790	0000		98	0087	24	0039
TEN AND SIX TENTH	800	0000		99	0088	20	0039
ONE AND SEVEN TENTH	810	0000		100	0089	60	0018
TWO AND SEVEN TENTH	820	0000		101	0090	20	0023
THREE AND SEVEN TENTH	830	0000		102	0091	20	0035
FOUR AND SEVEN TENTH	840	0000		103	0092	35	0008
FIVE AND SEVEN TENTH	850	0000		104	0093	46	0071
SIX AND SEVEN TENTH	860	0000				61	0074
SEVEN AND SEVEN TENTH	870	0000				69	0024
EIGHT AND SEVEN TENTH	880	0000				24	0039
NINE AND SEVEN TENTH	890	0000				20	0039
TEN AND SEVEN TENTH	900	0000				60	0018
ONE AND EIGHT TENTH	910	0000				20	0023
TWO AND EIGHT TENTH	920	0000				20	0035
THREE AND EIGHT TENTH	930	0000				35	0008
FOUR AND EIGHT TENTH	940	0000				46	0071
FIVE AND EIGHT TENTH	950	0000				61	0074
SIX AND EIGHT TENTH	960	0000				69	0024
SEVEN AND EIGHT TENTH	970	0000				24	0039
EIGHT AND EIGHT TENTH	980	0000				20	0039
NINE AND EIGHT TENTH	990	0000				60	0018
TEN AND EIGHT TENTH	1000	0000				20	0023
ONE AND NINE TENTH	1010	0000				20	0035
TWO AND NINE TENTH	1020	0000				35	0008
THREE AND NINE TENTH	1030	0000				46	0071
FOUR AND NINE TENTH	1040	0000				61	0074
FIVE AND NINE TENTH	1050	0000				69	0024
SIX AND NINE TENTH	1060	0000				24	0039
SEVEN AND NINE TENTH	1070	0000				20	0039
EIGHT AND NINE TENTH	1080	0000				60	0018
NINE AND NINE TENTH	1090	0000				20	0023
TEN AND NINE TENTH	1100	0000				20	0035

FIFTY	SO	0000	0000	105	0060	50	0000	U000	
SIXTY	SO	0000	0060	106	0016	60	0000	0060	
LNX14	01	2345	6789	107	0011	01	2345	6789	
E00CR	STO	EXIT		108	1250	24	0153	0156	
	RAM	8002		109	0016	24	0153	0156	
	BMI	NEGAT	REUC	110	0115	46	0160	0069	
NEGAT	FAO	TWOP1		111	0168	32	0271	0047	
	RAM	ONEPI		112	0047	46	0168	0051	
	FBR	UNEP1	COS10	113	0251	33	0054	0201	
REDUC	FBR	TWOP1		114	0069	33	0271	0097	
	BMI	REUC	REUC	115	0097	46	1300	0069	
	FAD	ONEPI	COS1U	116	1300	32	0054	0201	
COS10	STU	THETA		117	0281	21	0086	0139	
	STU	FPONE		118	0139	61	0024	0229	
	STU	TERHM		119	0229	21	0134	0187	
	STU	FUNKT		120	0187	21	0192	0045	
	STL	ENNN	NEGST	121	0045	20	0099	0002	
E00SR	STO			122	1350	24	0153	0066	
	RAU	8002		123	0206	60	8002	0165	
	BMI	NEGAV	REOU	124	0165	46	0218	0119	
NEGAV	FAD	TWOP1		125	0218	32	0271	0147	
	BMI	NEGAV		126	0147	46	0218	0901	
	FBR	ONEPI	GINET	127	0901	33	0054	0931	
REDIU	FBR	TWOP1		128	0119	33	0271	0197	
	BMI	REOU	REOU	129	0197	46	1400	0119	
	FAD	ONEPI	GINET	130	1400	32	0054	0931	
GINET	STU	THETA		131	0931	21	0086	0189	
	RBU	8003		132	0189	61	8003	0347	
	STU	TERHM		133	0247	21	0134	0377	
	STU	FUNKT		134	0237	21	0192	0095	
	LDD	FPONE		135	0095	69	0024	0227	
	STL	ENNN	NEGST	136	0227	24	0099	0002	
NEGBT	RAM	NN		137	0002	60	0099	0203	
	FAO	FPONE		138	0203	32	0024	0951	
	STU	FPONE		139	0951	21	0251	0959	
	STU	ENNN		140	0059	32	0024	1001	
	RSU	TERHM		141	1001	21	0099	0052	
	FAD	THETA		142	0052	61	0134	0959	
	FMP	THETA		143	0239	39	0086	0136	
	FDV	WPONE		144	0136	39	0086	0186	
	FDV	ENNN		145	0186	34	0256	0966	
	STU	TERHM		146	0906	34	0099	0149	
	RAM	FUNKT		147	0149	21	0134	0287	
	STL	FWAC		148	0287	67	0287	0077	
	RAM	TERMM		149	0997	20	1051	0154	
	RAU	8002		150	0154	67	0134	0289	
	FDV	FWAC		151	0289	60	0289	0517	
	FBR	SIZEB		152	0947	34	1051	1101	
	BMI	ENUFF		153	1101	33	0204	0981	
	RAU	FUNKT		154	0981	46	0184	0485	
	FAD	TERHM		155	0935	60	0192	0997	
	STU	FUNKT	NEGST	156	0997	32	0134	0111	
	STU	FUNKT	EXIT	157	0111	21	0192	0128	
ENUFF	RAL	EXIT		158	0184	65	0192	0153	
RIZEB	1Q	0U0U	004J	159	0204	10	0000	0043	
TWOP1	G2	H318	S351	160	0271	62	8118	5351	
ONEPI	J1	4159	2731	161	0054	31	4159	2751	
FPONE	10	0000	0051	162	0284	10	0000	0051	
E00CA	STL	AAA1		163	1450	24	0253	0956	
	STL	AAA2	EXIT INSTR	164	0956	20	0161	0064	
	RAM	AAA2	BTORC X	165	0064	67	0161	0215	
	STL	AAA3		166	0215	20	0169	0122	
	RAU	AAA3	X FOR CALC	167	0122	60	0169	0123	
	FMP	AAA16		168	0123	39	0026	0076	
	FAD	AAA15		169	0076	32	0279	0055	
	FMP	AAA3		170	0055	39	0169	0219	
	FAD	AAA14		171	0219	32	0172	0199	
	FMP	AAA3		172	0199	39	0169	0259	
	FAD	AAA3		173	0269	32	0282	0249	
	FMP	AAA3		174	0249	39	0169	0919	
	FAD	AAA12		175	0919	32	0279	0969	
	FMP	AAA3		176	0299	39	0169	0969	
	FAD	AAA11		177	0969	32	0928	0949	
	FMP	AAA3		178	0949	39	0169	1019	
	FAD	AAA10		179	1019	32	0972	0999	
	STU	AAA4		180	0999	21	0234	0057	
	FMP	AAA4		181	0057	39	0234	0157	
	STU	AAA4		182	0904	21	0234	0157	
	FMP	AAA4		183	0157	39	0234	0954	
	STU	AAA4		184	0954	21	0234	0207	
	FMP	AAA4		185	0207	60	0161	0265	
	STU	AAA4	AAA6	186	0265	46	0268	1069	
AAA5	RAU	AAA10		187	0268	60	0972	0277	
	FMP	AAA4		188	0277	34	0254	1004	
	STU	AAA4	AAA6	189	1004	21	0254	1069	
AAA6	RAL	AAA4	AAA1	190	1069	65	0164	0253	
AAA10	10	0000	0051	191	0972	10	0000	0051	
AAA11	24	9998	6850	192	0922	24	9998	6850	
AAA12	31	2575	8349	193	0272	31	2575	8349	
AAA13	17	1337	1248	194	0222	25	9137	1248	
AAA14	17	1562	0047	195	0172	17	1562	0047	
AAA15	54	3020	0045	196	0279	54	3020	0948	
AAA16	07	0600	0044	197	0026	69	0600	0044	
E00AU	STD	SEXT		1	198	1500	24	0903	1006
	BMI	SERR		2	199	1006	46	0154	0960
	STU	SA	SEXT	3	200	0160	45	0114	0903
	STU	SA		4	201	0114	21	0918	0921
	FAD	B10		5	202	93	0211	0214	1351
	FMP	SHAIF	SB	6	203	1151	39	1054	1104
S8	STU	SBAY	SBAB	7	204	1104	21	0008	0201
SB	FAD	SA		8	205	0211	60	0911	0604
	FMP	SBAY	8 CAPT A	9	206	0173	34	0008	0058
	FAD	SBAY		10	207	0058	32	0008	0985

	FMP SHAF		11	208	0985	39	1054	1154
	FSS SBAV		12	209	1154	33	0908	1035
	MZU SBAV	SS	13	210	1053	44	0935	1059
	BMI	SS	14	211	0939	45	0242	0040
	FAD SBAV		15	212	0242	32	0008	1085
	FAU SBAV	SAH	16	213	1045	21	0008	0131
	ROU SBAV	SENT	17	214	0040	60	0008	0903
SR	NLT 0000	SEXT	18	215	0159	01	0000	0903
SHAF	SD 0000	OS0	19	216	1054	50	0000	0050
B10	SO 0000	00S1	20	217	0174	10	0000	0051
START	LDB FRRT	INITIAL	21R	1999	69	0100	0953	3
	LUD ZERO	GAMMA	21Q	0953	24	1056	0209	
LOOP6	LDO POINT	DATA POINT	220	0209	69	0101	1204	
	RAA BOO1		221	1204	80	8001	0210	
	STD ZERO		222	0210	69	0000	1003	
	STD ALPHA		223	1003	24	1106	0259	
	STO BETA		224	0259	24	0052	0915	
	RAH GAM11		225	0915	60	1056	0261	
	FMP GAM11		226	0261	39	1056	1156	
	STH GAMSQ	GAMMA SWU	227	1156	21	0260	0063	
	STH TEMP1		228	0063	21	0968	0971	
	RAU PI		229	0971	60	0950	0155	
	FDV A		230	0155	34	0103	1053	
	STU TEMP2		231	1053	21	0158	0911	
	FMP TEMP2	ALPHA	232	0911	39	0188	0208	
	STU TEMP2	BOU	233	0208	21	0158	0961	
	RAU PI		234	0961	60	0950	0205	
	FDV H		235	0205	34	0104	1254	
	STU TEMP3		236	1254	21	0258	1011	
	FMP TEMP3	BETA	237	1011	39	0258	0927	
	STU TEMP3	SOU	238	0908	21	0258	1061	
	RSU TEMP1		239	1061	61	0968	0223	
	FAO TEMP2		240	0223	32	0258	1132	
	FAO TEMP3	R	241	1135	32	0258	1185	
	STU HSQO	BOU	242	1185	21	0090	0093	
LOOP3	LUD ZERO		243	0093	69	0000	1101	
	STD CENCF		244	1103	24	1206	0909	
	RAU C	CORRECTION	245	0909	60	0105	0959	
	FSS H	FOR	246	0959	33	2300	0927	
	FMP GAM11	ENH	247	0927	39	0200	1456	
	FMP HTWO	EFFECT	248	1256	39	0200	1550	
	RAL SOO3		249	1550	65	8003	0257	
	LDO	EOGEA	250	0257	69	0910	1450	
	STL TEMP1		251	0910	20	0968	1021	
	RAU ONE	FIND MODE	252	1021	60	0050	0255	
	FSS TEMP1	CORRECTION	253	0255	33	0968	0152	
	STU FMECF	FACTOR	254	0145	21	1600	1153	
	RAU PI	CALCULATE	255	1153	60	950	0950	
	FMP X	CONSTANT	256	0905	39	0106	1302	
	FOV A	FACTOR	257	1306	34	0103	1203	
	RAL BOO3	FOR CENCF	258	1203	65	8003	1111	
	LDO		259	1111	69	0164	1240	
	STL TEMP1		260	0164	20	0968	1071	
	RAU PI		261	1071	60	0950	0955	
	FOV B		262	0955	34	0104	1304	
	FMP Y		263	1304	39	0107	0907	
	RAL BOO3		264	0907	65	8003	0965	
	LDO	EOOCH	265	0965	69	1018	1250	
	STL TEMP2		266	1018	20	0158	1161	
	RAL GAM11		267	1161	60	1056	1211	
	FMP Z		268	1211	39	2300	1600	
	RAL BOO3		269	1600	65	8003	0957	
	LDO	EOGEA	270	0957	69	0960	1450	
	RAU ROO2		271	0960	60	8002	1719	
	FMP GAM11		272	1119	39	1056	1356	
	FDV TEMP1		273	1356	34	0968	1058	
	FOV TEMP2		274	1058	34	1538	0958	
	FOV FMECF		275	0958	34	1600	1700	
	STD CENCF		276	1700	21	1354	1007	
	LDO THREE	CONSTANT	277	1007	69	0250	1253	
	STD ONE		278	1253	24	1406	1009	
	LDO N		279	1009	69	0050	1303	
LOOP2	RAU N		280	1303	64	0000	0333	
	FMP PI		281	1333	60	0500	1005	
	FMP Y		282	1005	39	0950	1750	
	FOV S		283	1750	39	1078	1057	
	RAL BOO3		284	1057	34	0104	1404	
	LDO	EOOCH	285	1404	65	8003	1261	
	STL TEMP3	LOOP1	286	1261	69	0214	1250	
LOOP1	RAU M		287	0214	20	0258	1311	
	FMP X		288	1311	60	1406	1351	
	FDV TEMP2		289	1351	39	0950	1800	
	FMP X		290	1800	39	0106	1456	
	FOV BOO3		291	1456	24	0103	1403	
	LDO	EOOCH	292	1403	65	8003	1251	
	STL TEMP2		293	1411	69	0264	1250	
	FOV A		294	0264	20	0158	1461	
	RAU U		295	1461	60	1406	1311	
	FMP PI		296	1311	39	0950	1850	
	STU TEMP4		297	1850	24	0103	1453	
	FMP TEMP4		298	1453	21	1008	1351	
	STH ALPH2		299	1351	39	1008	1058	
	RAU N		300	1058	21	0112	1015	
	FMP PI		301	1015	60	0500	1003	
	FOV S		302	1055	39	0950	1900	
	STU TEMP4		303	1900	34	0104	1454	
	FMP TEMP4		304	1454	21	1008	1611	
	STH BETA2		305	1611	39	1008	1108	
	FAD ALPH2		306	1108	21	0162	1056	
	FSS BOO0		307	1056	32	0112	0989	
	LDO	EOOAU	308	0989	33	0090	0017	
	STU AMMA		309	0017	69	0010	1000	
	RAU C		310	0020	21	0224	0977	
			311	0977	60	0105	1059	

	RAU C		311	0977	60	0105	1059
	FBR Z	A	312	1059	33	2300	1027
	FMP GAMMA		313	1027	39	0224	0274
	FAL N1W0		314	0274	39	0274	1100
	L00 8003		315	1950	65	8003	1107
	STL	EOOEA	316	1107	69	1010	1450
	STL TEMP5		317	1118	60	1118	1178
	RAU GAMMA		318	1118	60	0224	0929
	FMP Z	A	319	0929	39	2300	1201
	RAU 8003		320	1201	65	8003	1099
	L00	EOOEA	321	1109	69	0212	1450
	STL TEMP6		322	0212	60	0667	0070
	STL ONE		323	0070	60	0050	1165
	FBR TEMP5		324	1105	33	1115	0141
	FVU TEMP5		325	0141	34	0067	0117
	FVU GAMMA		326	0117	34	0224	0924
	FMP TEMP3		327	0924	39	0258	1158
	FMP TEMP2		328	1158	39	0158	1208
	FAU CEHCF		329	1208	32	1206	0133
	STU CENCF		330	0133	21	1206	1159
	RAU SEVEN		331	1159	60	1000	1155
	FBR N		332	1155	33	1406	0183
CONT1	NZE CONT1	CUNT4	333	0183	45	0236	0937
	RAU N		334	0236	60	1406	1661
	FAO TWO		335	1661	32	0150	1077
CONT2	STU N	LOOP1	336	1077	21	1406	1311
	RAU N		337	0937	60	0500	1205
	FBR SEVEN		338	1205	33	1000	1127
CONT3	NZE CONT3	CUNT4	339	1127	45	0130	1031
	STU ONE		340	1031	69	0050	1503
	RAU N		341	1503	61	1503	1399
	FAO TWO		342	1209	60	0500	1255
CONT4	STU N	LOOP2	343	1255	32	0150	1177
	RAU CENCF		344	1177	21	1177	1177
	FMP CENCF		345	1031	60	1206	1711
	RAU COMBT	CALC OF	346	1711	39	1354	1504
	FAU ONE	HARMONIC	347	1504	32	0040	1100
	STU CENCF	END	348	1227	21	1206	1859
	RAU N	CORRECTION	349	1859	60	2500	1305
	FVU CEHCF		350	1305	34	1305	1366
	FVU FMECF		351	1506	34	1600	1251
	STU NCDR		352	1251	21	2700	1553
	L00 Z	A	353	1553	69	2353	1303
	STU 1977		354	1603	64	1977	0180
	L00 N	A	355	0180	69	2500	1653
	STU 1978		356	1653	24	1978	0281
	L00 NCDR	A	357	1081	69	2700	1703
	STU 1979		358	1703	24	1979	0232
	L00 CEHCF		359	0232	69	1206	1309
	STU 1980		360	1309	64	1980	0233
	L00 FMECF		361	0233	29	1600	1753
	STU 1981		362	1753	24	1981	0234
	PCH 1977		363	0234	71	1977	1577
	SXA 0001		364	1277	51	0001	0283
	NZA L00P3		365	0283	40	0093	0987
CONT6	L00 POINT	CONTH	366	0987	69	0101	1554
	RAA 8001		367	1554	60	8001	1060
	L00 ZER0		368	1060	69	0000	1603
	STU SUMA		369	1603	24	1556	1359
	STU SMLNA		370	1359	24	0262	1165
	STU SUMZ		371	1165	24	1168	1121
	STU SUMZ2		372	1121	24	0974	1327
	STU ZSMLA		373	1327	24	0230	0933
	L00 DATPT		374	0933	69	0102	1355
LOOPS	STU P	LOOPS	375	1355	24	1558	1761
	RAU NCDR	A	376	1761	60	2700	1405
	FAO SUMA		377	1405	32	1556	0983
	STU SUMA		378	0983	21	1556	1409
	RAU NCDR	A	379	1409	60	2700	1455
	L00	LNXC1	380	1455	69	1308	1200
	FAO SMLNA		381	1200	32	1308	1309
	STU SMLNA		382	1039	21	0262	1215
	RAU Z	A	383	1215	60	2300	1505
	STU SUMZ		384	1505	32	1505	0936
	STU SUMZ		385	0195	81	1168	1171
	RAU Z	A	386	1171	60	2300	1555
	FMP Z	A	387	1555	39	2358	1371
	FAD SUMZ2		388	1301	32	0974	1351
	STU SUMZ2		389	1351	21	0974	1377
	RAU NCDR	A	390	1377	60	2700	1409
	L00	LNXC1	391	1605	69	1358	1200
	FMP Z	A	392	1200	39	2300	1401
	FAO ZSMLA		393	1401	32	0130	1857
	STU ZSMLA		394	1157	21	0230	1033
	SXA 0001		395	1033	51	0001	1089
	NZA L00P5	CONT7	396	1089	60	0101	1443
CONT7	RAU SMLNA		397	0143	60	0262	0167
	FMP SUMZ		398	0167	39	1168	1218
	STU TEMP1		399	1218	21	0968	1281
	RAU P		400	1221	60	1258	0113
	FMP ZBULA		401	0113	39	0230	0280
	STU TEMP2		402	0280	21	0262	0167
	RAU P		403	1811	60	1258	0163
	FMP SUMZ2		404	0163	39	0974	1024
	STU TEMP3		405	1024	21	0262	0167
	RAU SUMZ		406	1861	60	1168	0273
	FMP SUMZ2		407	0273	39	1168	1268
	STU TEMP4		408	1268	21	1068	1261
	RAU TEMP3		409	1911	60	0258	0213
	FMP TEMP4		410	0213	33	1008	1235
	STU TEMP3		411	1235	21	0238	1261
	RAU TEMP1		412	1961	60	0968	0923
	FBS TEMP2		413	0923	33	0158	1285

	FOY TEMP3		414	1285	34	0258	1408
	STU NWGAM		415	1408	31	0912	1265
	FOY 10000		416	1265	34	1100	1451
	STU PREC		417	1451	23	1500	1479
	RAU GAM11		418	1459	60	1056	0962
	FBR NWGAM		419	0962	33	0912	1139
	RAM 8003		420	1139	67	800	1047
	RAU 8008		421	1047	60	8002	1655
	FBR PREC		422	1655	33	1506	1083
	SMI CONTS	CONF9	423	1083	45	0286	1037
CONTR9	RAU NWGAM		424	1037	60	0912	0217
	STU GAM11	LOOP6	425	0217	21	1056	0209
	RAU PI		426	0286	60	0950	1705
	FOY A		427	1705	34	0103	1853
	STU ALPH2		428	1853	21	0112	1315
	FMP ALPH2		429	1315	39	0112	1012
	STU ALPH2		430	1012	21	0112	1365
	RAU PI		431	1365	60	0950	1755
	FOY B		432	1755	34	0104	1504
	STU BETA2		433	1504	21	0162	1415
	FMP BETA2		434	1415	39	0162	1062
	STU BETA2		435	1062	21	0162	1465
	RSU NWGAM		436	1465	61	0912	0267
	FMP NWGAM		437	0267	33	0912	1112
	FAO BETA2		438	1112	32	0112	1189
	FAO ALPH2		439	1189	32	0112	1239
	STU 8800	CALCULATE	440	1239	23	0090	0193
	LOO 8800	MATERIAL	441	0193	62	0090	0243
	BTO 1977	BUCKLING	442	0243	64	1977	0930
	LOO NWGAM		443	0930	25	0912	1515
	STO 1978		444	1515	44	1915	1131
	LOO GAM11		445	1131	69	1056	1509
	STD 1979		446	1509	24	1979	0282
	LOD FIRST		447	0282	29	0282	1903
	STD 1980		448	1903	24	1980	1133
	LDD POINT		449	1133	69	0101	1654
	BTO 1981		450	1654	24	1981	0284
	PCH 1977	CONF9	451	0284	71	1977	1427
CON10	RAU L		452	1427	60	0108	0263
	FMP L		453	0263	39	0108	1458
	FAO TAU		454	1458	32	0109	1335
	FMP 8800	CALCULATE	455	1335	39	0090	0140
	FAO ONE	K INFINITY	456	0140	32	0050	1477
CON11	STU KINF	CON11	457	1477	21	0932	1385
	RAU PI		458	1385	60	0950	1805
	FOY A		459	1805	34	0103	1704
	FMP 8003		460	1704	39	8003	1207
	STU ALPH2		461	1207	21	0112	1565
	RAU PI		462	1565	60	0950	1855
	FOY B		463	1855	34	0104	1754
	FMP 8003		464	1754	39	8003	1257
	STU BETA2		465	1257	21	0162	1615
	RAU PI		466	1615	60	0950	1905
	FOY O		467	1905	34	0110	1110
	FMP 8003		468	1110	39	8003	0913
	FAO ALPH2	CALCULATE	469	0913	32	0112	1289
	FAO BETA2	GEOMETRIC	470	1289	32	0162	1339
	STU 8800	BUCKLING	471	1339	21	0044	1097
	RSU TAU		472	1097	61	0109	0963
	FMP 86800		473	0963	39	0044	0094
	RAL 8003		474	0094	65	8003	1501
LOO	STL TEMP1	EOOEA	475	1501	69	1804	1450
	RAU 86800		476	1804	20	0968	1271
	FMP L		477	1271	80	0044	1049
	FMP L		478	1049	39	0108	1508
	FMP L		479	1508	39	0108	1558
	FAO ONE		480	1558	32	0108	1527
	STU TEMP2		481	1527	21	0158	1163
	RAU KINF	CALCULATE	482	1162	60	0932	1057
	FMP TEMP1		483	1057	39	0968	1318
	FOY TEMP2	EFFECTIVE	484	1318	34	0158	1608
	STU KEFF		485	1608	21	1212	1665
LOO	LOO 8800	EOOGL	486	1665	69	1368	1110
	STO 1977		487	1368	69	0090	0293
	LOO 86800		488	0293	24	1977	0980
	STO 1978		489	0980	89	0044	1049
	LDD KINF		490	1147	24	1978	1181
	STO 1979		491	1181	89	0932	1435
	LOD KEFF		492	1435	24	1978	1452
	STO 1980		493	0982	69	1212	1715
	PCH 1977	8000	494	1715	24	1980	1183
			495	1183	71	1977	8000

APPENDIX K

IBM 650 Program for Statistical Analysis
of Horizontal Traverse Data

The purpose of this program was to analyze data taken in a horizontal traverse of the KSU pile and to determine the reliability of each data point based on predicted statistical variations. The program was written in SOAP II and floating point. The object program and a logic diagram are given in this section.

The analysis performed by this program is based on the equation

$$\phi(x, y, z) = \sum_{m=1}^{\infty} A_m \cos \frac{m \pi x}{a}$$

where m is odd, and y and z are held constant. Care should be taken that too many harmonics are not used, as this will cause errors in the least squares calculation due to statistical noise. The 1, 3, and 5 harmonics were found sufficient in this work. In performing the analysis, the program first determines the values of A_m , for as many harmonics as are specified, by a least squares technique. It then proceeds to calculate the allowable deviation of each point in the traverse according to the formula found in Price (19)

$$DEV = K\sigma = K \left(\frac{r}{t} \right)^{1/2}$$

where r = count rate in counts per minute,

t = total counting time to obtain r ,

K = constant multiplier which may be varied to set the allowable deviation to include any given probability of occurrence.

Having determined the allowable deviations, the program then checks each point to determine whether or not it is within the allowable deviation of the value predicted by the least squares analysis. If not, the point is temporarily discarded. If its deviation is within the allowable limits, the point is stored in the accepted data table, designated in the program as XPRIM and NPRIM.

The accepted data are then used to calculate a new set of least squares coefficients and the same deviation check is repeated for all of the original data points using the new coefficients. The new accepted data table is then compared with the table used in the least squares calculations, previously designated X and N. If the two tables are identical, indicating that the same data points have been rejected in two successive trials, then the rejected values are replaced by least squares values in the original table, and the complete set of corrected data is punched out. If the accepted table and the least squares data do not match, the accepted table replaces the least squares table and a new least squares analysis is performed.

The final output of this program is a complete table of data with statistically invalid points replaced by values calculated from a least squares analysis of the accepted points.

Input constants and data are listed in Table 37. All input to this program should be in the form of one-word load cards.

Output of this program is in three forms as listed in Table 38. Form one contains the least squares coefficients and is punched after each least squares calculation. Form two is punched whenever a data point is rejected, there being no intermediate output of accepted data.

Form three is the final output and gives the accepted or corrected data point and its co-ordinate.

Table 37. Input to IBM 650 program for statistical analysis of horizontal traverse data.

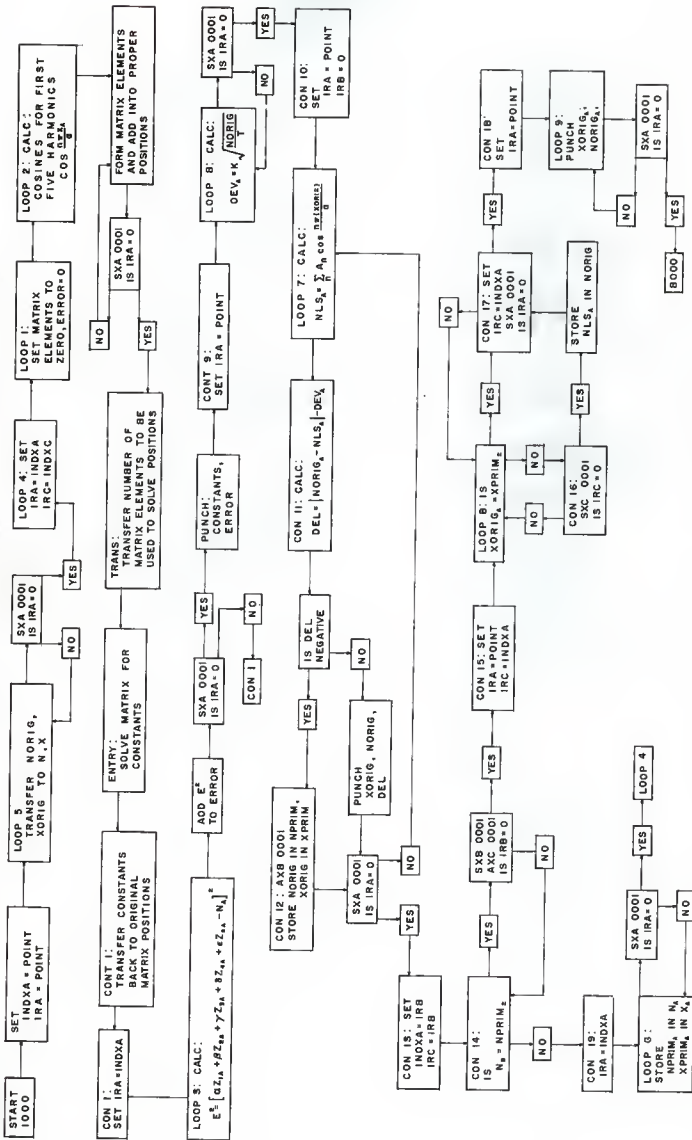
Symbol	Explanation	Drum Storage Location
A	Extrapolated x-dimension	1001
K	Sigma multiplier	1002
POINT	Number of Data Points, in form 00 0000 00xx	1003
HARM	Value of $(2m + 1)$ for highest value of m used	1004
ENN	Number of harmonics used, in form 00 0000 000x	1005
XORIG	Position co-ordinates of data, to be stored consecutively starting at	0251
NORIG	Count rates, to be stored consecutively starting at	0201
T	Total counting times, to be stored consecutively starting at	0651

The operating time for a two-trial analysis of 10 data points is approximately three minutes. The total capacity of the program is 50 data points.

Table 38. Output forms for IBM 650 program for statistical analysis of horizontal data.

Word No.	Form One	Form Two	Form Three
1	A_0		Position co-ordinate
2	A_1		Count Rate
3	A_2		
4	A_3		
5	A_4		
6	Total error squared	Position co-ordinate	
7		Rejected Count Rate	
8		Amount by which point exceeded allow- able deviation	

LOGIC DIAGRAM FOR IBM 650 PROGRAM FOR STATISTICAL ANALYSIS OF HORIZONTAL DATA TRAVERSE



LOGIC DIAGRAM, APPENDIX K

OBJECT PROGRAM - APPENDIX K

BLR	0000	0030	1	0000	00	0000	0000
BLR	0101	0131	2	0000	00	0000	0000
BLR	0200	0900	3	0000	00	0000	0000
BLR	1900	1999	4	0000	00	0000	0000
BYN	Y11	0101	5	0000	00	0000	0000
BYN	Y12	0102	6	0000	00	0000	0000
BYN	Y13	0103	7	0000	00	0000	0000
BYN	Y14	0104	8	0000	00	0000	0000
BYN	Y15	0105	9	0000	00	0000	0000
BYN	Y21	0106	10	0000	00	0000	0000
BYN	Y22	0107	11	0000	00	0000	0000
BYN	Y23	0108	12	0000	00	0000	0000
BYN	Y24	0109	13	0000	00	0000	0000
BYN	Y25	0110	14	0000	00	0000	0000
BYN	Y31	0111	15	0000	00	0000	0000
BYN	Y32	0112	16	0000	00	0000	0000
BYN	Y33	0113	17	0000	00	0000	0000
BYN	Y34	0114	18	0000	00	0000	0000
BYN	Y35	0115	19	0000	00	0000	0000
BYN	Y41	0116	20	0000	00	0000	0000
BYN	Y42	0117	21	0000	00	0000	0000
BYN	Y43	0118	22	0000	00	0000	0000
BYN	Y44	0119	23	0000	00	0000	0000
BYN	Y45	0120	24	0000	00	0000	0000
BYN	Y51	0121	25	0000	00	0000	0000
BYN	Y52	0122	26	0000	00	0000	0000
BYN	Y53	0123	27	0000	00	0000	0000
BYN	Y54	0124	28	0000	00	0000	0000
BYN	Y55	0125	29	0000	00	0000	0000
BYN	Z1	0126	30	0000	00	0000	0000
BYN	Z2	0127	31	0000	00	0000	0000
BYN	Z3	0128	32	0000	00	0000	0000
BYN	Z4	0129	33	0000	00	0000	0000
BYN	Z5	0130	34	0000	00	0000	0000
BYN	Z PHA	0400	35	0000	00	0000	0000
BYN	BETA	0450	36	0000	00	0000	0000
BYN	GAMMA	0500	37	0000	00	0000	0000
BYN	DELTA	0550	38	0000	00	0000	0000
BYN	EPSILON	0600	39	0000	00	0000	0000
BYN	MORIG	0200	40	0000	00	0000	0000
BYN	XORIG	0250	41	0000	00	0000	0000
BYN	N	0300	42	0000	00	0000	0000
BYN	X	0350	43	0000	00	0000	0000
BYN	T	0650	44	0000	00	0000	0000
BYN	NPRIM	0700	45	0000	00	0000	0000
BYN	XRRIM	0750	46	0000	00	0000	0000
BYN	NLS	0800	47	0000	00	0000	0000
BYN	OE	0850	48	0000	00	0000	0000
BYN	A	1001	49	0000	00	0000	0000
BYN	K	1002	50	0000	00	0000	0000
BYN	POINT	1003	51	0000	00	0000	0000
BYN	HARM	1004	52	0000	00	0000	0000
BYN	ENH	1005	53	0000	00	0000	0000
BYN	START	1000	54	0000	00	0000	0000
BYN	START	0000	55	0000	00	0000	0000
ZERO	00	0000	56	0100	10	0000	0051
ONE	10	0000	57	0150	20	0000	0051
TWO	20	0000	58	0950	30	0000	0051
THREE	30	0000	59	1050	31	4159	0051
PI	31	4159	60	1100	50	0000	0051
FIVE	50	0000	61	1150	70	0000	0051
SEVEN	70	0000	62	1200	90	0000	0051
NINE	90	0000	63	1250	00	0000	0030
INOCX	00	0000	64	1300	24	0053	0056
EOOCL	00	0000	65	0056	69	0059	0062
BT0	ZZ10	0000	66	0062	24	1977	0080
LD	T010	0000	67	0080	24	1978	0031
STD	1977	0000	68	0031	24	1979	0032
BT0	1978	0000	69	0032	24	1980	0033
STD	1979	0000	70	0033	24	1981	0034
STD	1980	0000	71	0034	24	1982	0035
STD	1981	0000	72	0035	24	1983	0036
STD	1982	0000	73	0036	24	1984	0037
STD	1983	0000	74	0037	00	0000	0000
STD	1984	ZZ11	75	1350	24	0153	0156
ZZ10	0000	0000	76	0156	60	0068	0065
EOOCL	0000	0000	77	0065	46	0068	0069
NAU	8002	REOUC	78	0068	32	0071	0047
SMI	NEGAT		79	0047	46	0068	0011
FAO	T00P1		80	0051	33	0054	0081
SMI	NEGAT		81	0069	33	0071	0097
FBS	ONEPI	COS10	82	0097	46	1008	0069
FSS	T00P1		83	1400	32	0054	0081
SMI	NEGAT	REOUC	84	0081	21	0086	0039
FAD	ONEPI	COS10	85	0039	61	0052	0147
GTU	THETA		86	0147	21	0052	0055
NSU	FPONE		87	0055	21	0060	0063
GTU	TERMM		88	0060	20	0067	0070
GTU	FUNKT		89	1450	84	0153	0906
STL	ENNN	NEGST	90	0906	60	8002	0165
STD	0002		91	0165	46	0068	0069
NAU	8002	REOUC	92	0168	32	0071	0197
SMI	NEGAT		93	0197	46	0168	0151
FAD	T00P1		94	0151	33	0054	0081
FBS	ONEPI	SINET	95	0169	33	0071	0097
FSS	T00P1		96	0947	46	1500	0161
SMI	NEGAT	REOUC	97	1500	21	0086	0089
FAO	T00P1	SINET	98	0089	21	0086	0089
GTU	THETA		99	0089	61	8003	0997
NSU	8003		100	0997	21	0097	0155
GTU	FUNKT		101	0155	21	0060	0163
STL	ENNN		102	0163	69	0042	0045
LOD	FPONE		103	0045	24	0067	0070
STO	ENNN	NEGST					

DATA IN
HARMONICS
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NEGST	RAU ENNN	104	0070	60	0067	0171		
	FAO FPONE	105	0171	32	0042	0919		
	STU FPONE	106	0119	21	0074	0277		
	FAO FPONE	107	0077	32	0042	0959		
	STU ENNN	108	0969	21	0067	0170		
	STU ENNN	109	0969	61	0052	0077		
	FMP TNETA	110	0057	39	0086	0136		
	FMP TNETA	111	0136	39	0086	0186		
	FOV FPONE	112	0186	1	0074	0124		
	FOV ENNN	113	0174	34	0067	0167		
	STU TERMM	114	0167	21	0052	0905		
	RAU FUNKT	115	0905	67	0060	0915		
	BTL FMAG	116	0915	20	1019	0072		
	RAU TERMM	117	0072	67	0052	0157		
	RAU B002	118	0157	60	8002	0965		
	FOV FMAG	119	0965	34	1019	1069		
	F88 81ZEB	120	1069	53	0172	0049		
	SMI ENUFF	121	0049	46	0152	0903		
	RAU FUNKT	122	0903	60	0060	1015		
	FAO TERMM	123	1015	32	0052	0079		
	STU FUNKT	124	0079	21	0060	0070		
	RAL FUNKT	125	0152	65	0060	0153		
ENUFF	RAL FUNKT	EXIT	125	0172	10	0000	0043	
SIZES	10 0000	0043	126	0049	46	0152	0903	
T80P1	62 8318	5351	127	0054	31	4159	2751	
ONEP1	31 4189	2751	128	0042	10	0000	0051	
FPONE	10 0000	0051	129	1550	24	0953	0956	
COOAU	STO SEKT	HEGST	1	0956	46	0159	0160	
	SMI BERR	SEXT	2	131	132	133	134	
	NZE SA	SEXT	3	132	133	134	135	
	FAO B10	SEXT	4	133	134	135	136	
	FMP SNAF	88	5	134	135	136	137	
88	RAU SBAV	88	6	135	136	137	138	
SAB	RAU SA	SAB	7	136	137	138	139	
	FOV SBAV	8 CAPT A	8	137	138	139	140	
	FMP SNAF	8 CAPT A	9	138	139	140	141	
	F88 SBAV	8 CAPT A	10	139	140	141	142	
	NZU SBAV	8 CAPT A	11	140	141	142	143	
	SMI BR	8 CAPT A	12	141	142	143	144	
	FAO SBAV	8 CAPT A	13	142	143	144	145	
	RAU SBAV	8 CAPT A	14	143	144	145	146	
	NLT 0000	SEXT	15	144	145	146	147	
8R	SNAF	SEXT	16	145	146	147	148	
SERR	10 0000	00S1	17	146	147	148	149	
S10	00 0000	00S1	18	147	148	149	150	
START	LOD POINT	00S1	19	148	149	150	151	
	LOD ORIG A	00S1	20	149	150	151	152	
	STO MORIG A	00S1	150	1000	69	1003	1006	
	STO MORIG A	00S1	151	1000	69	1003	1006	
	STO MORIG A	00S1	152	1006	21	0058	0911	
LOOP5	RAA 8001	LOOP5	152	0162	80	8001	0968	
	LOD MORIG A	PUT DATA	153	0968	69	2200	1053	
	STO MORIG A	IN LEAST	154	0968	24	2053	24	
	STO MORIG A	SQUARES	155	1103	69	2250	1153	
	STO MORIG A	TABLE	156	1153	24	2350	1203	
	SXA 0001	LOOP4	157	1203	51	1059	0911	
	NZC LOOP5	LOOP4	158	0959	40	0968	0913	
LOOP4	LOD INOKX A	SET	159	0913	69	0909	0912	
	RAA 8001	INDEX	160	0912	80	8001	1018	
	LOD INOKX C	REGISTER	161	1018	69	1250	1253	
	RAC 8001	REGISTER	162	1253	88	8001	1009	
	LOD ZERO	REGISTER	163	1009	69	0050	1303	
LOOP1	STO 0100	LOOP1	164	1303	24	6100	1353	
	STO 0000	C	165	1353	24	6000	1403	
	SXC 0001	C	166	1403	59	0001	1059	
	NZC LOOP1	C	167	1059	48	1303	0963	
CONTR	STO ERROR	CONTR	168	0963	24	0066	1119	
LOOP2	RAU PI	CONTR	169	1119	60	1050	0955	
	FMP PI	CONTR	170	0955	39	2350	1600	
	FOY A	CONTR	171	1600	34	1001	0951	
	STU TEMP1	CONTR	172	0951	21	1054	1009	
	FMP THREE	CONTR	1	1109	39	0950	1650	
	STU TEMP2	CONTR	3	1650	21	1054	1009	
	RAU TEMP1	CONTR	1	1750	60	0907	0611	
	FMP FIVE	CONTR	1	0611	39	1100	1700	
	STU TEMP3	CONTR	5	1770	21	1104	0957	
	RAU TEMP2	CONTR	1	1778	0957	60	0911	
	FMP SEVEN	CONTR	1	0911	39	1150	1750	
	STU TEMP4	CONTR	7	1750	21	1154	1007	
	RAU TEMP1	CONTR	1	181	60	1007	60	
	FMP NINE	CONTR	1	0961	39	1200	1900	
	STU TEMP5	CONTR	9	1800	21	1204	1057	
	RAL TEMP1	CONTR	1	184	65	1154	1259	
	LOD ALPHA	EOOCR	1	185	1011	69	0164	1350
	STL ALPHA A	EOOCR	1	186	0164	20	2400	1453
	RAU TEMP2	EOOCR	1	187	65	1453	1559	
	LOD BETA	EOOCR	3	188	1159	69	0952	1350
	STL BETA A	EOOCR	3	189	0962	20	2450	1503
	RAU TEMP3	EOOCR	3	190	65	104	1209	
	LOD GAMMA	EOOCR	5	191	1209	69	1012	1350
	STL GAMMA A	EOOCR	5	192	1012	20	2500	1553
	RAU TEMP4	EOOCR	5	193	65	154	1259	
	LOD DELTA	EOOCR	7	194	1259	69	1062	1350
	STL DELTA A	EOOCR	7	195	1062	20	2380	1603
	RAU TEMP5	EOOCR	7	196	65	1603	1309	
	LOD EPSIL	EOOCR	9	197	1309	69	1112	1350
	STL EPSIL A	EOOCR	9	198	1112	20	2600	1653
	RAU ALPHA	EOOCR	9	199	60	2403	1305	
	FMP ALPHA A	EOOCR	9	200	1055	39	2400	1850
	FAO Y11	EOOCR	11	201	1850	32	0101	0177
	ST Y11	EOOCR	11	202	0177	21	0107	0112
	RAU ALPHA A	EOOCR	11	203	1254	60	2400	1105
	FMP BETA A	EOOCR	11	204	1105	39	2450	1051
	FA Y12	EOOCR	11	205	1051	32	0102	0179
	STU Y12	EOOCR	12	206	0179	21	0102	1155

WTU	Y#1		21	207	1155	21	01006	1359
RAU	ALPHA	A		208	1359	60	24000	12055
FAP	GAMMA	A		209	1205	39	25000	12055
FAO	Y13			210	1101	39	01003	09289
STU	Y13		13	211	09889	21	01003	11006
STU	Y14		31	212	01006	21	01005	09004
RAU	ALPHA	A		213	09114	60	24000	18555
FNP	OELTA	A		214	12555	39	25500	11551
STU	Y14			215	11551	39	01005	09501
STU	Y14		14	216	09331	21	01004	11007
STU	Y41		41	217	11007	21	01116	11669
RAU	ALPHA	A		218	11669	21	01005	09605
FNP	EP8IL	A		219	13005	39	26000	12011
FAO	Y15			220	12001	33	01005	09811
STU	Y15		15	221	09881	21	01005	09008
STU	Y51		51	222	09008	21	01211	09704
RAU	BETA	A		223	09774	60	24500	13555
FNP	BETA	A		224	13555	39	24500	19551
FAO	Y22			225	12551	32	01007	00233
STU	Y22		22	226	00833	21	01007	09100
RAU	BETA	A		227	09100	60	24500	14005
FNP	GAMMA	A		228	14005	39	25000	13011
FAO	Y23			229	13001	32	01002	09355
STU	Y23		23	230	09355	21	01002	10611
STU	Y22		32	231	10611	21	01112	10655
RAU	BETA	A		232	10655	60	24500	14555
FNP	OELTA	A		233	14555	39	25500	13551
FAO	Y24			234	13551	32	01009	09855
STU	Y24		24	235	09855	21	01009	11628
STU	Y42		42	236	11628	21	01110	09200
RAU	BETA	A		237	09200	60	24500	15005
FNP	EP8IL	A		238	15005	39	26000	14011
FAO	Y25			239	14011	39	24000	10377
STU	Y25		25	240	00337	21	01110	10133
STU	Y52		52	241	10133	21	01222	00705
RAU	GAMMA	A		242	00705	21	01110	00401
FNP	GAMMA	A		243	15555	39	25000	14511
FAO	Y33			244	14511	32	01113	01229
STU	Y33		33	245	01229	60	25000	16005
RAU	GAMMA	A		246	01666	60	25000	16005
FNP	OELTA	A		247	16005	39	25500	13011
FAO	Y34			248	15011	38	15011	00401
STU	Y34		34	249	00441	21	01114	09177
STU	Y43		43	250	09177	21	01112	09711
RAU	GAMMA	A		251	09711	60	26000	14855
FNP	EP8IL	A		252	16555	39	26000	18511
FAO	Y35			253	18511	32	01115	00911
STU	Y35		35	254	00911	21	01115	11008
STU	Y53		53	255	10668	21	01223	00706
RAU	OELTA	A		256	00766	60	25500	17005
FNP	OELTA	A		257	17005	60	25500	17005
FAO	Y44			258	16011	32	01119	00955
STU	Y44		44	259	00955	21	01119	09222
RAU	OELTA	A		260	09222	60	25500	18555
FNP	EP8IL	A		261	17555	39	26000	14511
FAO	Y45			262	16551	32	01220	10477
STU	Y45		45	263	10477	21	01200	01733
STU	Y54		54	264	01733	21	01224	09277
RAU	EP8IL	A		265	09277	60	26000	18005
FNP	EP8IL	A		266	18005	39	26000	17011
FAO	Y55			267	17011	32	01225	17511
STU	Y55		55	268	17511	21	01225	00708
RAU	ALPHA	A		269	00708	60	24000	18555
FNP	N			270	12555	39	23000	18011
FAO	Z1		21	271	18011	32	01226	17033
STU	Z1			272	17033	21	01226	09799
RAU	BETA	A		273	09799	60	24500	11556
FNP	N			274	11556	39	23000	18511
FAO	Z2			275	12551	38	01227	17533
STU	Z2		22	276	12533	21	01227	01200
RAU	GAMMA	A		277	01200	60	25000	12006
FNP	N			278	12006	39	23000	09022
FAO	Z3			279	09022	32	01228	13666
STU	Z3		23	280	12556	21	01228	10311
RAU	OELTA	A		281	10311	60	25500	13006
FNP	N			282	13006	39	23000	09022
FAO	Z4			283	09559	39	01229	13556
STU	Z4		24	284	13556	21	01229	00822
RAU	EP8IL	A		285	00822	60	26000	14066
FNP	N			286	14066	39	23000	10522
FAO	Z5			287	10522	32	01330	11537
STU	Z5		25	288	11537	21	01330	01333
SXA	00001			289	01333	51	00001	09399
WZA	LOOP	TRANS		290	09399	40	11119	00433
RAB	0001			291	00433	80	0001	00999
RAC	0001			292	00999	82	0001	14556
LOD	ENH			293	14556	88	0001	18122
STO	ENHND	LOOPX		294	09400	59	10219	09588
LOD	0000			295	09588	24	11111	09664
STO	0000	C		296	09664	29	01000	13033
LOD	ENND			297	13033	84	6000	18533
SXC	8001			298	18533	69	11111	10144
WXC	8001	COMTY		299	10144	89	8001	09700
ACB	8001			300	09700	48	09233	10244
ACD	0001			301	09233	58	8001	10299
ACE	0001	LOOPX		302	10299	50	0001	10355
ACF	8001			303	10355	58	0001	09664
ACG	0001			304	10224	58	8001	09300
ACH	8001			305	09300	60	8001	10577
ACI	0001			306	10577	11	10005	14009
ACJ	FNN			307	00887	44	10633	10664
ACK		SFC2		308	14009	11	10633	14599
ACL	ENH			309	14599	44	11111	11144

	SUP ENN		310	1113	11	1005	1509
	NZU	BFC4	311	1509	44	1163	1164
	SUP ENN		312	1163	11	1005	1509
	NZU COLZ	SFC5	313	1559	44	1213	1214
BFC2	LOD ENN		314	1064	69	1005	1008
	SUP ENN		315	1008	53	1001	1054
	NZB	COLZ	316	1264	42	0967	1213
	AKB 8001		317	0967	52	8001	0973
	AKB 0011		318	0973	52	8001	1079
	RAA 0006		319	1079	60	0006	1085
	LOD ENN		320	1085	69	1005	1058
	RAC 8001		321	1058	88	8001	1129
	AKC 0001		322	1314	58	0001	1020
	RAU ENN		323	1020	60	1005	1020
	AUP ENN		324	1609	10	1005	1659
BFC3	BTU ENND	LOOPX	325	1659	21	1111	0964
	LOD ENN		326	1114	69	1005	1108
	SXB 8001		327	1108	53	8001	1364
	NZB	COLZ	328	1364	42	1017	1213
	AKB 8001		329	1017	52	8001	1033
	AKB 0001		330	1023	52	0001	1129
	RAA 0011		331	1129	60	0011	1135
	LOD ENND		332	1135	69	1111	1414
	RAC 8001		333	1414	88	8001	1070
	AKC 0001		334	1070	58	0001	0176
	RAU ENND		335	0176	60	1111	1115
	AUP ENN		336	1115	10	1005	1709
BFC4	BTU ENND	LOOPX	337	1709	21	1111	0964
	LOD ENN		338	1164	69	1005	1158
	SXB 8001		339	1158	53	8001	1464
	NZB	COLZ	340	1464	42	1067	1213
	AKB 8001		341	1067	52	8001	1073
	AKB 0001		342	1073	52	0001	1179
	RAA 0016		343	1179	60	0016	1185
	LOD ENND		344	1185	69	1111	1514
	RAC 8001		345	1514	88	8001	1129
	AKC 0001		346	1120	58	0001	0926
	RAU ENND		347	0926	60	1111	1165
	AUP ENN		348	1165	10	1005	1759
BFC5	BTU ENND	LOOPX	349	1759	21	1111	0964
	LOD ENN		350	1214	69	1005	1208
	SXB 8001		351	1208	53	8001	1544
	NZB	COLZ	352	1544	42	1117	1213
	RAA 0021		353	1117	60	0021	1123
	LOD ENND		354	1123	69	1111	1544
	RAC 8001		355	1614	88	8001	1170
	AKC 0001		356	1170	58	0001	0976
	RAU ENND		357	0976	60	1111	1155
	AUP ENN		358	1215	10	1005	1809
	STU ENND	LOOPX	359	1809	21	1111	0964
COLZ	LLOD ENND		360	1213	69	1111	1644
	RAC 8001		361	1644	88	8001	1220
	AKC 0001		362	1220	58	0001	1026
	RAA 0011	LOOPZ	363	1026	60	0001	0822
LOOPZ	LOD 0125	A	364	0132	69	2125	0178
	STO 0000	C	365	0178	64	6000	1304
	LOD ENN		366	1304	69	1005	1258
	SXA 8001		367	1258	51	8001	1714
	NZA		368	1714	40	1167	1118
	AKA 8001	CONT1	369	1167	50	8001	1173
	AKA 0001		370	1173	50	0001	1229
CONT1	AKC 0001	LOOPZ	371	1229	58	0001	0132
	LOD	ENTRY	372	1118	69	1021	1074
	RAU ENN		373	1021	60	1005	1859
	MPY ENN		374	1859	19	1005	1076
	ALO UNITY		375	1076	13	1279	0103
	STL ENN2		376	0183	20	0137	0090
	RAA 0001		377	0090	80	0001	0046
	LOD ENN2		378	0046	69	0137	0140
	RAC 8001	LOOPY	379	0140	68	8001	0096
	LOD 0000	C	380	0096	69	6000	1354
	STO 0125	A	381	1354	24	2125	0988
	SXA 0005		382	0928	51	0005	0084
	NZA	CON1	383	0084	40	0185	0038
	AKA 0001	LOOPY	384	0185	40	0186	0033
CON1	AKC 0001		385	0093	58	0001	0096
	LOD INDX		386	0038	60	0009	1262
	RAC 8001	LOOP3	387	1262	80	8001	1168
LOOP3	RAU Z1		388	1168	60	0126	1081
	FMP ALPHA	A	389	1081	39	2480	1102
	STU TEMP1		390	1102	21	1056	0000
	RAU Z2		391	0960	60	0127	1131
	FMP BETA	A	392	1131	39	2480	1158
	STU TEMP2		393	1158	21	1056	0077
	RAU Z3		394	1207	60	0128	0933
	FMP GAMMA	A	395	0933	39	2500	1202
	STU TEMP3		396	1202	21	1104	1257
	RAU Z4		397	1257	60	0129	0983
	FMP DELTA	A	398	0983	39	2550	1286
	STU TEMP4		399	1286	21	1154	1307
	RAU Z5		400	1307	60	0130	1235
	FMP EPSIL	A	401	1235	39	2630	1328
	FAD TEMP1		402	1302	32	1056	1033
	FAD TEMP2		403	1033	32	1054	1181
	FAD TEMP3		404	1181	32	1104	1211
	FAD TEMP4		405	1231	32	1154	1281
	F3B N	A	406	1281	33	2300	0977
	STU TEMP1		407	0977	21	1056	1070
	FMP TEMP1		408	1010	39	1056	1506
	FAD ERROR		409	1506	32	0066	0143
	STU ERROR		410	0143	21	0066	1199
	SXA 0001		411	1219	51	0001	0175
	NZA LOOP3	CONT3	412	0175	40	1168	1329

CONT3	L00		E00CL	413	1329	69	0182	1300
	L00	Z1		414	0182	69	0126	1379
	ST0	1977		415	1379	24	1977	0980
	L00	Z2		416	0980	24	1978	1030
	ST0	1978		417	1030	24	1978	1331
	L00	Z3		418	1331	69	0128	1351
	ST0	1979		419	1351	24	1979	0933
	L00	Z4		420	0932	69	0129	0982
	ST0	1980		421	0982	24	1980	1003
	L00	Z5		422	1003	69	0130	1134
	ST0	1981		423	1133	24	1981	0134
	L00	ERROR		424	0134	69	0066	1269
	ST0	1982		425	1269	24	1982	0933
	PCH	1977	CONT9	426	1285	71	1977	1027
	ST0	EXIT		427	1074	24	0153	1556
ENTRY	RAL	ENH		428	1556	60	1005	1060
	SUP	UNLTY		429	1060	11	1279	1183
	STU	UNLES		430	1183	21	0088	0141
	RAU	ENH		431	0141	60	1005	1110
	AUP	UNTY		432	1110	10	1279	1233
	STU	ENPLU		433	1233	21	0158	0193
	WPY	ENH		434	0191	19	1005	1126
	STL	NSPEN		435	1126	20	1431	0184
	SLT	0004		436	0184	35	0004	0145
	ALO	IN04		437	0145	15	0048	1404
	L00	A0NE		438	1404	69	1357	1160
	S0A	A0NE		439	1160	22	1357	1210
	L00	L00PB		440	1210	69	1263	0916
	S0A	L00PB		441	0916	22	1263	0966
	L00	ATW0		442	0966	69	1319	0972
	L00	ATREE		443	0972	62	1319	1032
	S0A	ATREE		444	1022	69	0925	0978
	L00	AFOUR		445	0978	22	0925	1028
	S0A	AFOUR		446	1028	69	1481	0984
	L00	L00FP		447	0934	22	1481	0984
	S0A	L00FP		448	0984	69	0937	0190
	L00	L0ADC		449	0190	69	0937	0190
	S0A	L0ADC		450	0940	69	0193	0146
	L00	CFIVE		451	0146	22	0193	0196
	S0A	CFIVE		452	0196	69	0196	1332
	L00	AFIVE		453	1352	32	0149	1402
	ALO	IN0B		454	1402	15	1606	1161
	L00	C0NE		455	1161	69	1161	1257
	S0A	C0NE		456	1217	22	1764	1267
	L00	CTW0		457	1267	69	1270	1223
	S0A	CTW0		458	1223	62	1583	1429
	L00	CTREE		459	1273	69	1176	1429
	S0A	CTREE		460	1429	22	1176	1479
	L00	CF0UR		461	1479	69	1032	1315
	S0A	CF0UR		462	1335	22	1032	1385
	L00	CFIVE		463	1385	69	0188	0941
	S0A	CFIVE		464	0941	62	0941	1391
	RAC	0000		465	0991	88	0000	1097
	L00	8007		466	1097	69	8007	1454
	ST0	CTEMP		467	1454	24	1407	1677
	RSL	NSPEN		468	1860	66	1431	1435
	RAA	8002		469	1435	80	8002	0943
	STL	ATEMP	LOOPA	470	0943	30	1147	1458
	RSL	UNLES		471	1452	66	0088	0993
	RAB	8002		472	0993	82	8002	1502
	STL	STEMP	ADNE	473	1502	30	1457	1357
	RAC	9999		474	1357	65	9999	1504
	NZE	NORWA	REPLA	475	1504	45	1308	1310
	RAC	9999	L00PB	476	1308	20	1313	1263
	RAU	9999		477	1263	80	9999	1554
	FQV	0TEMP	ATW0	478	1554	34	1313	1319
	STU	9999		479	1319	81	9999	1552
	RAL	ENH		480	1552	65	1005	1360
	AXA	8002		481	1360	30	8002	1369
	AXA	L00PB		482	1369	41	1263	1333
	RAL	ATEMP		483	1323	65	1147	1602
	RAA	8002	L00PC	484	1602	80	8002	1211
	RZC	8002	SHKIP	485	1211	48	1814	1602
	RAL	8007		486	1814	65	8007	1071
	ALO	8008		487	1071	15	8005	1529
	RAC	8002		488	1529	88	1529	1766
	RBU	9999		489	1764	61	9999	1604
	NZE		NX8BT	490	1604	45	1358	1410
	STU	ATEMP		491	1358	21	1358	1513
	RAU	ATEMP	ATREE	492	1315	60	1312	0925
	FMP	9999	CTW0	493	0925	39	9999	1270
	FXA	9999	CTREE	494	1270	32	9999	1174
	STU	9999		495	1176	21	9999	1652
	RAL	ENH		496	1652	65	1005	1460
	AXA	8002		497	1460	30	8002	1369
	AXC	8002		498	1419	58	8002	1077
	SMA	L00PB	NXSST	499	1077	41	1315	1410
	AXA	8001		500	1410	52	0001	1513
	NZB	NEWTB		501	1016	42	1469	1320
	L00	CTEMP		502	1320	69	1440	1510
	RAC	8001		503	1510	88	8001	1666
	L00	ATEMP		504	1066	69	1147	1702
	RAA	8001		505	1702	80	8001	1408
	L00	ENPLU		506	1408	69	1440	1510
	AXA	8001		507	1041	50	8001	1197
	L00	8005		508	1197	69	8005	1654
	ST0	ATEMP		509	1654	24	1147	1752
	SMA		EXIT	510	1752	41	1656	0153
	AXC	0001		511	0153	59	0001	1362
	L00	8007		512	1362	69	8007	1218
	ST0	CTEMP		513	1218	24	1407	1560
	ST0	CTEMP	LOOPA	514	1560	44	1363	1452
	ST0	XTEMP		515	1459	69	1147	1802
	L00	ATEMP						

	RAA	8001		516	1802	80	8001	145f
	LOD	KTEMP		517	1458	89	1363	111f
	RAA	8001		518	1116	88	8001	126c
	AXC	0001	BHKIP	519	1660	58	0001	1121
BHKIP	STO	8007		520	1121	69	8007	1127
	LOD	KTEMP		521	1127	24	1363	1211
REPLA	STO	UMLES	LOOCP	522	1340	49	0008	1091
	AXC	8001	LOOPE	523	1091	58	8001	1247
LOOPE	AXC	0001		524	1247	58	0001	1704
	STO	8007		525	1704	59	0001	1481
AFOUR	BXC	0001	AFOUR	525	1704	65	9999	1754
	RAL	9999	ZEERO	526	1481	45	1508	1610
	LOD	ENH		527	1754	66	0001	1548
	RSL	UMLES		528	1548	58	8002	1852
	AXC	8002		529	1043	58	0007	1660
	RAL	8007		530	1852	18	8003	1317
	ALO	8005		531	1660	88	8002	0937
	RAC	8002	LOOFP	532	1317	65	9999	1032
LOOFP	RAL	9999	CFOUR	533	0937	69	9999	0149
CFOUR	LOD	9999	AFIVE	534	1032	24	9999	0188
AFIVE	STO	9999	CFIVE	535	0149	20	9999	1804
CFIVE	RTL	9999		536	0189	69	1005	1558
	LOD	ENH		537	1804	58	8001	1864
	AXC	8001		538	1558	50	8001	1370
	AXA	8001		539	1864	46	0937	1124
	BMI	LOOFP		540	1370	69	1147	1854
	LOD	ATEMP		541	1124	80	8001	1710
	RAA	8001		542	1854	69	1407	1760
	LOD	CTEMP		543	1710	88	8001	1308
	RAC	8001	NORMA	544	1760	48	1247	1365
ZEERO	NZC	LOOPE	STOPP	545	1610	69	1706	1608
PUNCH	LOD	ENH		546	1608	81	8001	1415
	RBA	8001		547	1608	89	0008	0193
	RSC	0008	LOADC	548	1415	59	0193	1706
LOADC	RZC	9999		549	1706	24	7985	0938
	STO	1985		550	1756	84	7985	0938
	AXC	0001		551	0938	58	0001	0044
	RZC	INCR A		552	0044	48	0077	0098
	PCN	1977		553	0098	71	1977	1177
	RSC	0008	INCR A	554	1177	89	0008	1297
INCR A	AXA	0001		555	1297	50	1297	1656
	NZA	LOADC		556	1806	40	0193	1810
	PCH	1977		557	1810	71	1977	1227
	RAU	NBFEW		558	1227	58	1427	1585
	R8B	8001		559	1485	83	8001	1141
	RAA	0000	ZEERE	560	1141	80	0000	1347
ZEERE	RZB	0001	BOOD	561	1347	42	1856	8000
	RTL	0001		562	1856	40	2001	1507
	AXC	0001	ZEERE	563	1412	50	2001	1507
	AXA	0001	0001	564	1507	50	0001	1347
UNITY	OO	0000		565	1279	00	0000	0000
INDA	OO	2001	0000	566	0000	00	2001	0000
INDB	OO	4000	0000	567	1606	00	4000	0000
STOSP	OO	5555	0000	568	0135	01	5555	0000
CONTR	LOD	POINT		569	1027	69	1003	1557
	RAA	8001	LOOP6	570	1557	80	8001	1413
LOOP6	RAU	NORIG		571	1413	60	2200	1607
	FOV	T		572	1607	34	2650	1657
	LOD	K	E00AU	573	1657	69	1860	1550
	FMP	OE	ALLOWABLE	574	1860	39	1008	1707
	STU	OE	DEVIATION	575	1707	21	2850	1757
	BXA	0001		576	1757	51	0001	1463
	NZA	LOOPE	CON10	577	1463	40	1413	1367
CON10	LOD	POINT		578	1367	69	1003	1807
	RAA	8001		579	1807	80	8001	1513
	RAB	0000	LOOP7	580	1513	82	0000	1519
LOOP7	RAU	PI		581	1519	60	1050	1857
	FMP	XORIG		582	1857	39	2250	1658
	STU	TEMP1		583	1658	34	1001	1708
	RAL	8003		584	1708	21	1056	1261
	LOD		E00CR	585	1261	65	8003	1569
	RAU	8002		586	1569	69	1078	1350
	FMP	Z1		587	1072	60	8002	1531
	STU	NLB		588	1531	39	0126	1226
	RAU	TEMP1		589	1226	71	2860	1598
	FMP	THREE		590	1758	60	1056	1311
	LOD	8003		591	1311	39	0950	1808
	RAU	8002	E00CR	592	1808	65	8003	1465
	FMP	Z2		593	1465	69	1268	1350
	FAD	NLB		594	1268	60	8002	1277
	STU	NLB		595	1277	39	0127	1427
	RPU	TEMP1		596	1377	32	2800	1377
	FMP	FIVE		597	1377	21	2800	1858
	RAL	8003		598	1858	60	1056	1361
	LOD		E00CR	599	1361	39	1100	1411
	RAU	8002		600	1411	65	8003	1619
	FMP	Z3		601	1619	69	1122	1350
	STU	NLB		602	1122	60	8002	1581
	RPU	TEMP1		603	1581	39	0128	1078
	FMP	SEVEN		604	1078	32	2800	1427
	RAL	8003		605	1427	21	2800	1461
	LOD		E00CR	606	1461	60	1056	1511
	RAU	8002		607	1511	39	1156	1361
	FMP	Z4		608	1361	65	8003	1669
	STU	NLB		609	1669	69	1172	1350
	RPU	TEMP1		610	1172	60	8002	1531
	FMP	NINE		611	1631	39	0129	1579
	RAL	8003		612	1579	32	2800	1477
	LOD		E00CR	613	1477	60	1056	1661
	RAU	8002		614	1661	39	1200	1719
	FMP	Z4		615	1661	65	8003	1669
	STU	NLB		616	1711	69	1222	1350
	RPU	TEMP1		617	1719	69	1222	1350
	FMP	NINE						
	RAL	8003						
	LOD		E00CR					
			CALCULATE					

	RAU 8002		LEAST	618	1222	60 8002	1681
	FMP 25		SQUARES	619	1681	39 0130	1080
	FAD NL8	A	DATA	620	1080	32 2800	1527
	STU NL8	A		621	1527	22 2800	1761
	RAU NORIG	A	CON11	622	1761	60 8002	1811
CON11	F88 NL8	A		623	1811	37 2800	1577
	RAW 8003			624	1577	67 8001	1535
	RAU 8002			625	1535	60 8002	1093
	F88 DEV	A	CHECK	626	1093	33 2850	1627
	STU DEL	A	DEVIATION	627	1627	21 1082	1585
	BMI CON12			628	1585	46 0988	0989
	LDD			629	0989	69 0142	1300
	LDD XORIG	A	E00CL	630	0142	69 2250	1861
	STO 1982			631	1861	24 1982	1635
	LDD NORIG	A	PUNCHED	632	1635	69 2200	1462
	STO 1983		REJECTED	633	1462	24 1983	0936
	LDD OEL		DATA	634	0936	69 1082	1685
	STD 1984		POINT	635	1685	24 1984	0987
	PCH 1977			636	0987	71 1977	1677
	BXA 0001			637	1677	51 0001	1283
	NZA LOOP7	CON13		638	1283	40 1519	1037
CON12	AX8 0001			639	0988	52 0001	0094
	LDD NORIG	A		640	0094	69 2200	1512
	STO NPRIM	B	FORM NEW	641	1512	24 4700	1562
	LDD XORIG	A	LEAST	642	1562	69 2250	1612
	STO XPRIM	B	SQUARES	643	1612	24 4750	1662
	BXA 0001		DATA TABLE	644	1662	51 0001	1318
	NZA LOOP7	CON13		645	1318	40 1519	1037
CON13	LDD XORIG	A		646	1037	69 8006	1143
	STO XPRIM	B		647	1143	24 0909	1712
	RAU 8001	CON14		648	1712	88 8001	1368
CON14	F88 NPRIM	C	COMPARE	649	1368	60 4300	1762
	NZE CON19		NEW OLD	650	1762	33 6700	1727
	F88 0001		DATA	651	1727	45 1130	1731
	BXC 0001		TABLES	652	1731	53 0001	1087
	NZ8 CON14	CON15		653	1087	59 0001	1193
CON19	LDD INDXA			654	1193	42 1368	1397
	RAA 8001	LOOP6		655	1130	69 0909	1812
LOOP6	LDD NPRIM	A	TRANSFER	656	1812	80 8001	1418
	LDD XORIG	A	NEW DATA	657	1418	69 2700	1868
	STO XPRIM	A	TABLE FOR	658	1868	24 2300	1563
	BXA 0001	LOOP4	LEAST	659	1563	69 2750	1613
CON15	LDD POINT		SQUARES	660	1613	24 2350	1663
	RAA 8001		OPERATION	661	1663	51 0001	1769
	LDD INDXA	LOOP8		662	1769	40 1418	0913
	RAC 8001			663	1397	69 1003	1713
LOOP8	RAU XORIG	A	CHECK	664	1713	80 8001	1819
	F88 XPRIM	C	ORIGINAL	665	1819	69 0909	1763
	NZE CON16	CON17	DATA	666	1763	88 8001	1869
CON16	BSC 0001		AND	667	1869	60 2250	1813
	MZC LOOP8		REPLACE	668	1813	33 6750	1777
	LDD NL8	A	REJECTED	669	1777	45 1180	1781
	STO NORIG	A	DATA	670	1180	59 0001	0986
CON17	RAA 8001	CON17		671	0986	48 1869	0990
	LDD INDXA			672	0990	69 2800	1863
	BXA 0001		POINT	673	1863	24 2200	1781
	LDD XORIG	A	WITH	674	1781	51 0001	1137
CON18	NZA LOOP8	CON18	LEAST	675	1137	69 0909	1515
	LDD POINT		SQUARES	676	1515	88 8001	1171
	RAA 8001	E00CL	VALUES	677	1171	40 1869	0975
LDDP9	LDD LOOP9			678	0975	69 1003	1565
	LDD XORIG	A	PUNCHED	679	1565	69 2200	1615
	STO 1977		REJECTED	680	1221	69 1174	1300
	LDD NORIG	A	DATA	681	1174	69 2250	1615
	STD 1978			682	1615	24 1977	1230
	PCH 1977			683	1230	69 2200	1665
	BXA 0001	8000		684	1665	24 1978	1831
	NZA LOOP9			685	1831	71 1977	1677
				686	1827	51 0001	1333
				687	1333	40 1174	8000

APPENDIX L

IBM 650 Program for Determination of
Confidence Limits on Diffusion Length

This code was written to determine the confidence limits on individually determined values of diffusion length based upon the expected standard deviation of the slope of a plot of $\ln \phi_{\text{corr}}$ vs. z from which L was determined. The program was written in SOAP II and floating point form. The object program and a logic diagram are presented in this section.

The method of calculation included a linear regression analysis to determine $\sigma(\gamma_{11})$, the standard deviation of γ_{11} and a propagation of errors analysis to determine $\sigma(L)$ from $\sigma(\gamma_{11})$. A description of the linear regression analysis can be found in Volk (29). The equation used was

$$\sigma^2(\gamma_{11}) = \frac{\sigma^2(\ln \hat{\phi})}{\Sigma^1(z^2)},$$

where

$$\sigma^2(\ln \hat{\phi}) = \frac{\Sigma(\ln \hat{\phi} - \ln \phi)^2}{N - 2}$$

and

$$\Sigma^1(z^2) = \Sigma(z^2) - \frac{(\Sigma z)^2}{N}.$$

In the above equations $\ln \hat{\phi}$, represents the value of $\ln \phi$ predicted by

$$\ln \hat{\phi} = \ln \phi(0) + \gamma z$$

Since $L = 1/\kappa$, the auxiliary separation constants equation could be written

$$\frac{1}{L^2} = \gamma_{11}^2 - \alpha_0^2 - \beta_1^2.$$

By the theory of propagation of errors,

$$\sigma^2(L) = \left(\frac{\partial L}{\partial \gamma_{11}} \sigma(\gamma_{11}) \right)^2.$$

Writing L as a function of γ_{11} ,

$$L = (\gamma_{11}^2 - \alpha_1^2 - \beta_1^2)^{-\frac{1}{2}}$$

Thus,

$$\frac{\partial L}{\partial \gamma_{11}} = -\frac{1}{2} (\gamma_{11}^2 - \alpha_1^2 - \beta_1^2)^{-\frac{3}{2}} (2\gamma_{11}).$$

Since

$$\gamma_{11}^2 - \alpha_1^2 - \beta_1^2 = \kappa^2,$$

$$\frac{\partial L}{\partial \gamma_{11}} = -\frac{\gamma_{11}}{\kappa^3}$$

Thus $\sigma(L)$, the standard deviation of L , can be written in terms of $\sigma(\gamma_{11})$, the standard deviation of γ_{11} , as

$$\sigma(L) = \pm \frac{\gamma_{11} \sigma(\gamma_{11})}{\kappa^3}.$$

Input for this code consisted of the values of z , and ϕ_{corr} obtained from the output of any given diffusion length program as well as certain parameters listed in Table 39. Data to be fed in on one-word load cards are listed first with other load forms following. One card of form two is to be used for each corrected flux value, whereas only one card of form one is required for each set of input data.

The output form is given in Table 40. One output card is produced for each set of input data. Approximately 20 seconds is required to process 12 data points. The capacity of the program is 20 data points.

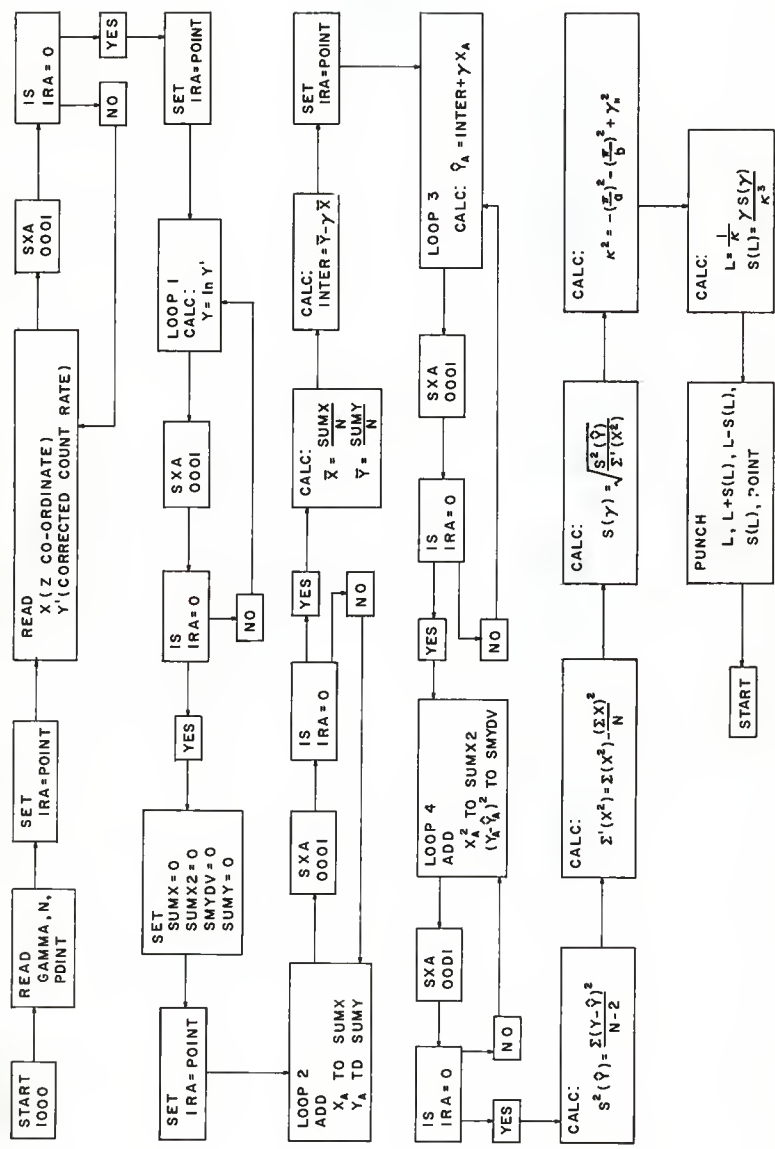
Table 39. Input parameters for IBM 650 program
for determination of confidence limits.

Symbol	Explanation	Drum Storage Location	
A	Extrapolated x-dimension	0100	
B	Extrapolated y-dimension	0101	
Word No.	1	2	
Form 1	Gamma	Number of Data Points, floating point form	Number of Data Points form 00 0000 00xx
Form 2	z-co-ordinate	Corrected count rate	---

Table 40. Output forms for IBM 650 program for
determination of confidence limits.

Word No.	1	2	3	4	5
L	$L + \sigma(L)$	$L - \sigma(L)$	$\sigma(L)$	Number of Data Points	

LOGIC DIAGRAM FOR IBM 650 PROGRAM FOR DETERMINATION OF CONFIDENCE LIMITS



LOGIC DIAGRAM, APPENDIX I

OBJECT PROGRAM - APPENDIX L

	BLR	0000	0003		1	0000	00	000000	0000
	BLR	1951	1961		2	0000	00	000000	0000
	BLR	1977	0004		3	0000	00	000000	0000
	BLR	0200	0280		4	0000	00	000000	0000
	SYN	L	0000		5	0000	00	000000	0000
	SYN	A	0100		6	0000	00	000000	0000
	SYN	S	0101		7	0000	00	000000	0000
	SYN	X	0200		8	0000	00	000000	0000
	SYN	Y	PRIM		9	0000	00	000000	0000
	SYN	Y	0240		10	0000	00	000000	0000
	SYN	YHAT	0260		11	0000	00	000000	0000
	SYN	START	1000		12	0000	00	000000	0000
	CO	0000	0000		13	0050	00	000000	0000
ZERO	ONE	10	0000		14	0150	10	000000	0051
TWO		20	0000		15	0300	20	000000	0051
CONVT		25	3600		16	0350	25	360000	0051
PI		31	415P		17	0400	31	415P00	0051
EOOAU			0051		18	0450	24	005300	0060
	STD	SEXT			19	0006	46	000900	0010
	SMI	SERR			20	0010	45	001400	0053
	NZE		SEXT		21	0014	21	001800	0051
	STU	SA			22	0014	21	001800	0051
	FAD	S10			23	0021	32	002400	0051
	FMP	SHAF	SS		24	0051	39	000400	0054
	STU	SSAV	SAH		25	0054	21	000800	0011
SS	BAU	BA		S CAPT A	26	0011	60	001800	0023
SAB	FOV	SSAV			27	0026	34	000800	0058
	FAD	SSAV			28	0058	32	000400	0035
	FMP	SHAF			29	0035	39	000400	0104
	FBB	SSAV			30	0104	33	000800	0055
	NZU		SR		31	0085	44	000500	0055
	SMI		SR		32	0039	46	004200	0040
	FAO	SSAV			33	0042	32	000800	0135
	STU	SSAV	SAB		34	0045	21	005500	0053
	RAU	SSAV	SEXT		35	0040	60	000800	0053
SR	HLT	0000	SEXT		36	0009	01	000000	0053
SERR	SNAF	50	0000	0050	37	0004	00	000000	0055
S10		10	0000	0051	38	0024	10	000000	0051
LNXX01	STD	LNXX08			39	0500	24	010300	0056
	NZE		LNXX14		40	0506	39	050600	0061
	SMI	LNXX14			41	0050	46	006100	0064
	STU	LNXX09			42	0054	21	006800	0071
	RBL	FPONE			43	0071	46	007400	0028
	STU	LNXX10			44	0025	24	003200	0185
	STL	LNXX02			45	0185	20	008900	0092
	RAU	LNXX09			46	0092	40	006200	0073
	STL	LNXX05			47	0073	20	002700	0030
	STL	LNXX11			48	0030	20	028500	0036
	SLT	0000			49	0036	45	003600	0007
	SUP	FIFTY			50	0007	11	011000	0015
	NZE		LNXX04		51	0015	45	011800	0019
	SMI		LNXX03		52	0118	46	011800	0025
	BBU	0003			53	0121	61	800300	0079
	LOO	FPONE			54	0079	69	007400	0077
	STU	LNXX02		LNXX03	55	0077	54	007900	0025
LNXX03	BR	0000			56	0022	30	000800	0041
	SCT	0000			57	0041	36	000000	0013
	AUP	XACTY			58	0016	10	014600	0171
	SUP	0000			59	0171	11	800000	0122
	RAU	0003			60	0122	50	800300	0122
	FMP	LNXX02			61	0037	39	008900	0139
	FMP	LNTEH			62	0139	39	014200	0102
LNXX04	STU	LNXX05		LNXX04	63	0152	21	002700	0019
	RAL	LNXX09			64	0019	65	006800	0133
	BR	0002			65	0123	30	000200	0179
	RAU	0002			66	0179	60	800200	0087
	ALB	FIFTY			67	0087	15	011000	0065
	ST	0002			68	0065	35	000200	0031
	FAO	FPONE			69	0321	32	007400	0151
	STU	LNXX09			70	0151	21	004600	0031
	SS	FTWO			71	0371	33	012400	0301
	FOV	LNXX09			72	0301	34	006800	0168
	STU	LNXX11			73	0168	24	007200	0025
	STU	LNXX12			74	0025	24	002800	0031
	STD	LNXX11			75	0028	24	028500	0066
	FMP	0001			76	0088	79	002100	0019
	RAU	FACTR		LNXX06	77	0091	21	004600	0040
LNXX06	STU	LNXX10			78	0049	60	003200	0137
	FAD	FTWO			79	0177	32	012400	0351
	STU	LNXX10			80	0351	21	005200	0335
	FMP	FACTR			81	0335	60	007200	0175
	FOV	LNXX10			82	0127	34	003200	0082
	STU	LNXX13			83	0082	21	007200	0075
	FAU	LNXX10			84	0075	21	007200	0075
	STU	LNXX12			85	0005	21	008800	0081
	FBB	LNXX11			86	0081	33	028500	0111
	FOV	LNXX11			87	0111	34	012400	0351
	RAM	0003			88	0355	67	800300	0043
	RAU	0002			89	0043	60	800200	0401
	FBR	SIZE7			90	0401	93	012400	0351
	SMI	LNXX07			91	0131	46	003400	0435
	LOD	LNXX12			92	0435	69	002800	0181
	STU	LNXX11			93	0181	24	003200	0122
	RAU	LNXX13			94	0138	60	007200	0177
	FMP	LNXX10			95	0177	39	003200	0122
	STU	LNXX13		LNXX06	96	0132	21	004600	0040
LNXX07	RAU	LNXX12			97	0034	60	002800	0033
	FMP	FTTWO			98	0034	33	002700	0103
	F8	LNXX05		LNXX08	99	0174	30	008700	0103
	FPONE	0000	0051		100	0074	10	000000	0051
FPTWO		20	0000	0051	101	0074	10	000000	0051
SIZE7		25	0000	0043	102	0154	10	000000	0043
LNTEH		23	0258	S151	103	0142	23	0258	S151

FIFTY	50	0000	0000	104	0110	50	0000	0000
EIKTY	00	0000	0060	105	0016	00	0000	0060
LNX14	01	2345	6789	106	0061	01	2345	6789
START	ACD	1951		107	1000	70	1951	0104
	LDD	1951		108	0451	69	1951	0104
	STD	GAMMA		109	0304	24	0057	0160
	LDD	1952		110	0160	69	1952	0055
	STD	N		111	0588	24	0108	0161
	LDD	1953		112	0161	69	1953	0106
	STD	POINT		113	0106	24	0059	0017
	RAA	8001	CONT1	114	0012	80	8001	0318
	RCD	1951		115	0318	70	1951	0501
	LDD	1951		116	0501	69	1951	0324
	STD	XUMY	A	117	0384	24	2200	0153
	LDD	1952		118	0153	69	1952	0105
	STD	YPRIM	A	119	0105	24	2220	0173
	SXA	0001		120	0173	31	0001	0329
	MZA	CONT1		121	0329	40	0318	0083
	LDD	POINT		122	0083	69	0059	0062
	RAA	8001	LOOP1	123	0062	80	8001	0368
	RAU	YPRIM	A	124	0368	60	2220	0125
	LDD		LNX01	125	0125	69	0078	0300
	STU	Y	A	126	0078	21	2241	0023
	SXA	0001		127	0093	51	0001	0099
	NZA	LODP1		128	0099	40	0368	0303
	LDD	POINT		129	0303	69	0059	0112
	RAA	8001		130	0112	80	8001	0418
	LDD	ZERO		131	0418	69	0050	0353
	STD	BUMX		132	0353	24	0153	0111
	STD	BUMX2		133	0109	24	0162	0115
	STD	8UMY2		134	0115	24	0468	0422
	STD	8UMY	LODP2	135	0468	24	0421	0158
	RAU	X	A	136	0327	60	2200	0155
	FAD	8UMX		137	0155	32	0059	0173
	STU	8UMX		138	0138	31	0108	0451
	RAU	Y	A	139	0159	60	2240	0045
	FAD	8UMY		140	0045	32	0345	0157
	STU	8UMY		141	0551	31	0324	0377
	SXA	0001		142	0377	51	0001	0183
	NZA	LODP2		143	0183	40	0368	0303
	RAA	BUMX		144	0097	60	0156	0111
	FDV	N		145	0311	34	0108	0158
	STU	XBAR		146	0158	61	0368	0379
	RAU	BUMX		147	0165	60	0324	0309
	FOV	N		148	0379	34	0108	0309
	STU	YBAR		149	0309	61	0308	0017
	RDU	XBAR		150	0315	39	0057	0107
	FMP	GAMMA		151	0017	32	0107	0152
	FAD	YBAR		152	0107	32	0107	0152
	STU	INTER		153	0189	21	0044	0047
	LDD	POINT		154	0047	69	0059	0412
	RAA	8001	LOOP3	155	0412	80	0012	0318
	RAU	X	A	156	0518	60	2200	0305
	FMP	GAMMA		157	0305	39	0057	0157
	FAD	INTER		158	0157	32	0059	0451
	STU	YNAT	A	159	0471	21	2260	0063
	SXA	0001		160	0063	51	0001	0065
	NZA	LOOP3		161	0069	40	0518	0323
	LDD	POINT		162	0323	69	0059	0462
	RAA	8001	LOOP4	163	0462	80	8001	0568
	RAU	X	A	164	0568	60	2200	0355
	FMP	8003		165	0355	39	8003	0309
	FAD	8UMX2		166	0309	32	0162	0289
	STU	8UMX2		167	0289	31	0162	0365
	RAU	Y	A	168	0365	60	2200	0095
	FBS	YNAT	A	169	0095	33	2260	0287
	FMP	8003		170	0287	39	0057	0152
	FAD	8UMY2		171	0141	32	0468	0145
	STU	8UMY2		172	0145	21	0468	0521
	SXA	0001		173	0521	61	0057	0152
	NZA	LODP4		174	0427	40	0568	0201
	RAU	N		175	0281	60	0108	0113
	FBS	TWO		176	0113	33	0108	0177
	STU	TEMP1		177	0477	21	0182	0485
	RAU	8UMY2		178	0485	60	0468	0373
	FDV	TEMP1		179	0373	34	0182	0282
	STU	8YHT		180	0282	21	0036	0339
	RDU	8UMX		181	0339	61	0156	0361
	FMP	8UMX		182	0361	39	0162	0389
	FOV	N		183	0306	34	0108	0358
	FAD	8UMX2		184	0358	32	0162	0389
	STU	81PX2		185	0389	31	0094	0097
	RAU	8YHT		186	0097	60	0036	0121
	FDV	81PX2		187	0121	34	0094	0113
	LDD		EO0AU	188	0113	69	0057	0150
	STU	GADEV		189	0147	81	0052	0405
	RAU	PI		190	0405	60	0405	0466
	FDV	A		191	0455	34	0100	0430
	FMP	8003		192	0550	39	8003	0403
	FAD	ALPH2		193	0403	61	0403	0504
	RAU	PI		194	0411	61	0400	0505
	FDV	B		195	0505	34	0101	0601
	FMP	8003		196	0601	39	0057	0150
	FAD	BETA2		197	0555	21	0310	0163
	RAU	GAMMA		198	0163	60	0057	0461
	FMP	GAMMA		199	0461	39	0057	0461
	FBS	ALPH2		200	0307	33	0408	0535
	FBS	BETA2		201	0535	33	0310	0337
	STD		EO0AU	202	0337	69	0057	0150
	STU	KAPPA		203	0050	81	0194	0197
	RAU	GAMMA		204	0197	61	0057	0511
	FMP	GADEV		205	0511	39	0052	0102

FDV	KAPPA		206	0102	34	0194	0294
FDV	KAPPA		207	0394	34	0194	0344
FDV	KAPPA		208	0344	34	0194	0394
FMP	CDMVT	DEVIATION	209	0394	39	0350	0600
STU	LOEV	DF L	210	0600	21	0404	0357
NAU	ONE		211	0357	60	0150	0605
FDV	KAPPA		212	0605	34	0194	0444
FMP	CONVT		213	0444	39	0350	0650
FAD	LDEV		214	0650	32	0404	0331
STU	1970	L PLUS	215	0331	21	1977	0381
F88	LOEV	L	216	0381	33	0404	0431
STU	1977		217	0431	21	1977	0060
F88	LOEV		218	0080	33	0404	0481
STU	1979	L MINUS	219	0481	21	1979	0332
LDC	LDEV		220	0332	69	0404	0407
STD	1980	DEVIATION	221	0407	24	1980	0283
LDD	POINT		222	0283	69	0059	0512
STD	1981	DATA POINT	223	0512	24	1981	0612
PCM	1977	STANT	224	0612	71	1977	1000

APPENDIX M

Calculation of Thermal Utilization

The thermal utilization in the KSU pile was calculated from formulas presented in ANL 5800 (20). The lattice is eight inches square, but was converted to equivalent cylindrical cells of radius 4.52 inches for this calculation. The equation used was

$$\frac{1}{f} - 1 = \frac{b^2 - c^2}{a^2} \frac{\Sigma_{mc}}{\Sigma_{uc}} G + a \Sigma_{uc} \left(1 - \frac{a}{c}\right) + \kappa_m^2 b^2 C + \frac{b^2 - c^2}{c} \Sigma_{mc} \left(\frac{3}{2} \lambda - 1\right)$$

where

$$\begin{aligned} \Sigma_{mt} &= \text{total cross section of moderator} \\ \Sigma_{mc} &= \text{capture cross section of moderator} \\ \Sigma_{uc} &= \text{capture cross section of fissionable material} \\ \Sigma_{ut} &= \text{total cross section of fissionable material} \\ \Sigma_{us} &= \text{scattering cross section of fissionable material} \\ \kappa_m^2 &= 3 \Sigma_{mt} \Sigma_{mc} \end{aligned}$$

$$C = \frac{1}{2} \frac{b^2/c^2}{(b^2/c^2) - 1} \ln \left(\frac{b}{c} \right) - \left(\frac{3}{4} \right) + \frac{1}{4b^2/c^2}$$

$$G = \frac{\phi(a)}{\phi_u} \text{ where } \phi_u \text{ is the average flux in the uranium.}$$

The approximation used for G was

$$G = 1 + \frac{\Sigma_{uc}}{\Sigma_{ut}} A + \alpha \frac{\Sigma_{us}}{\Sigma_{ut}} + \beta \left(\frac{\Sigma_{us}}{\Sigma_{ut}} \right)^2 .$$

Values of A , λ , α , and β were tabulated in ANL 5800. The radii of the fuel cooling gap and moderator region were assigned the symbols

- a - fuel
- b - outer radius of moderator
- c - outer radius of cooling gap.

EXPERIMENTAL AND THEORETICAL INVESTIGATION
OF THE DIFFUSION LENGTH OF THERMAL
NEUTRONS IN GRAPHITE

by

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The effect of the assumption of various mathematical models on the experimental determination of diffusion length was studied, and the diffusion length in the KSU graphite pile determined.

One-group diffusion theory was used in several forms, including an assumed constant thermal source boundary condition and an assumed point thermal source boundary condition. A method whereby the necessity of specifying a source boundary condition could be avoided was studied. A technique for the experimental evaluation of the constants A_{mn} in the thermal flux equation, and hence an equivalent thermal source boundary condition, is also presented.

Age-diffusion theory was studied in two forms, one assuming a point source of monoenergetic fast neutrons, the other an empirical fast source described in terms of Gaussian ranges and range fractions.

Criteria are established for judging the extent of validity of each method in the KSU pile. A final value of L is reported based on the method which best meets the stated criteria.