SENSITIZED FLUORESCENCE IN A MIXTURE OF MERCURY AND CADMIUM VAPORS

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INTRODUCTION

When a mixture of two different vapors is illuminated by radiation that can be absorbed by only one of the vapors, the atoms of the non-absorbing vapor can be observed to fluoresce. This luminescence is termed sensitized fluorescence.

To better understand this phenomena, consider a hypothetical mixture of two different vapors, A and B. Let the atoms of vapor A have an energy level E_a as the first excited level above their normal state, while the atoms of B have as their corresponding level an energy state designated E_b . Assume that E_a is greater than E_b , and further, that the incident frequency, f_a , times Flanck's constant is equal to E_a . Then, as atom A absorbs the incident radiation, it will change to an excited state, A^a . If the half life of the excited state of A^a is of like order of magnitude as the time between collisions between atoms A and B, it will be probable, by collisions of the second kind, for the energy of A^a to be transferred to atom B. The energy difference, $E_a - E_b$, will be divided between the colliding atoms in the form of kinetic energy. The atom B^a can then emit energy of a new frequency, f_b .

It is also possible for kinetic energy to combine with the energy of an excited atom to excite a second atom to a higher energy level. If, for example, vapor B in the above mentioned mixture were replaced by a vapor C, that has an atomic energy level, E_0 , which is greater than E_a , it would be possible for the quantum, hf_a , to combine with thermal energy to excite the atom C to E_0 , its lowest excited state. The energy difference here, E_0 - E_a , would have to be obtained from the relative kinetic energy of the two atoms. This emission frequency, f_0 , from atom C* would be

different from either fa or fh.

Cario and Franck (1) sought to verify these hypotheses experimentally in 1924. They reported evidence which substantiated both predictions. The purpose of this research was to confirm their results and to obtain more quantitative information with the aid of improved techniques and equipment.

THEORY

Cario and Franck performed their first experiments using mercury and thallium vapors. Their experimental arrangement consisted of two reservoirs connected to an absorption vessel. In one reservoir a sample of mercury was deposited. The other held thallium. These reservoirs were in separate ovens, to enable the experimenter to control the temperature, and hence, the vapor pressure of the materials. The absorption vessel was placed in a third oven which was capable of supplying the thermal energy necessary to excite the atoms to the states lying higher than the quantum energy of incident radiation. The mixture of the two vapors in the absorption vessel was irradiated by light from a water cooled mercury are lamp. The principal irradiating line was the 2537 A resonant line arising from the mercury $6^1S_0 - 6^5P_1$ transition. It was essential that this line be unreversed. The reradiated light was dispersed and detected with the aid of a quarts spectrograph.

Sensitized fluorescence was observed from thallium levels lying both above and below the 4.86 volt level of the mercury resonant line. However, the intensity ratios for some of the lines were not as had been expected. This was attributed to the fact that metastable states which

EXPLANATION OF PLATE I

Fig. 1. Energy level diagram of mercury. Pig. 2. Energy level diagram of cadmium.

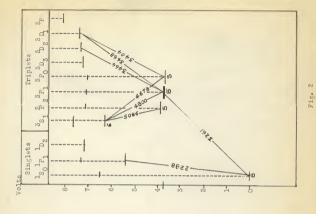
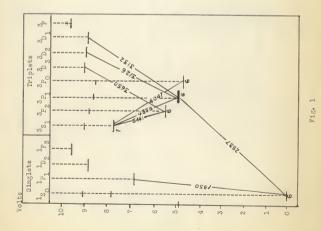


PLATE I



could be excited thermally were present in thallium. The next step was to replace the thallium by eadmium since it has no such low lying metastable states. With the main oven at 400°C, they observed only the cadmium 3261 A resonant line from the $5^{13}_{0} - 5^{5}P_{1}$ transition. At 800°C, the triplet emanating from the $6^{5}3_{1}$ level of cadmium as well as the 5261 A line was observed on the spectrograms. The possibility of exciting this level by stepwise absorption was ruled out, as the same results were obtained when a monochromator was used to pass only the mercury resonant line as the exciting radiation. Referring to Plate I (Mitchell and Zemansky, 2), it can be seen that the $6^{5}3_{1}$ level of cadmium lies at 6.5 electron volts. This means that 1.4 electron volts of thermal energy was supplied by the main oven to excite the atom to this level. This was cited as evidence supporting the contention that thermal and quantum energy can cooperate in exciting higher levels.

The main improvement in performing the experiment again as described in this paper was the substitution of a photomultiplier for photographic film as the detecting device. This has the obvious advantage of observing the results while performing the experiment as well as saving time in focusing. An additional objective was to obtain temperature versus intensity graphs for the triplet of cadmium.

APPARATUS AND TECHNIQUE

The source of the 2537 A radiation used in this research was a Sylvania U-shaped germicidal lamp. The 2537 A resonant line was predominant, although the mercury triplet consisting of the 4047, 4358, and 5461 A lines was present in measurable intensity. A complete spectrum

is listed with the results. This radiation was focused on the absorption vessel by a fused quartz lens of focal length 16.5 cm. The lens was supported by a horizontally mounted rod. The distance from a reference point on the rod to the point of focus for the 2557 A line was determined by focusing the same on a fluorescent screen while the visible light was filtered out. This simplified the focusing procedure in the research. The combined optical system is shown in the center of the photograph on Plate II.

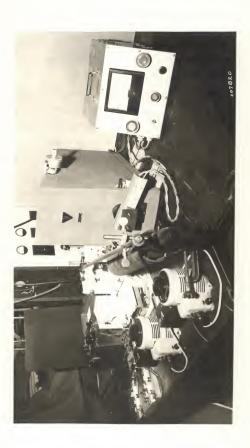
The construction of the ovens was the most time consuming part of preparing the experimental equipment, hence considerable attention has been given to this item. The heater coils were of Chromel-A wire, closely would around a 1.5 mm. rod which was mounted in the lathe. After being removed from the lathe, the coil was elongated to approximately four times its original length. The coil was first wrapped around an alundum core, which was helically grooved, then tied in place with a string. The coil was then carefully washed with alcohol to remove any contamination which might cause corrosion upon heating, and inserted into a hollow cylindrical form which had been poured from refractory concrete. This sheath served to hold the coil in position after the string had burned away as well as to separate the coils from asbestos. The sheath, core, and coil were supported between two plates of transite which were bolted together. The bolts also served as electrodes. The system was further insulated thermally by a mixture of asbestos paste which when dried, lent support to the oven.

Plate III shows the ovens. The two smaller ones were built as described above. The one on the left contains a quartz observation window in the end as a means of determining the amount of material in the oven

EXPLANATION OF PLATE II

Apparatus used in experiment.

The following are shown in the photograph:
Variable transformers, ammeters, light
source and shielded lens, ovens, monochrometor,
photowolt, and temperature measuring potentioneter.



PLA L II

EXPLANATION OF PLATE III

Fig. 1. Photograph of front view of ovens and Cd reservoir.

Fig. 2. Photograph of diagonal view of ovens and Hg reservoir.

PLATT III

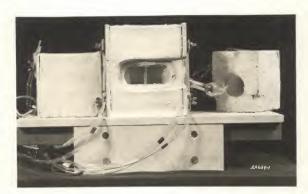


Fig. 1



Fig. 2

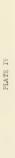
without removing the oven. The main oven in the center has two quarts windows in the side through which the incident and the sensitized fluorescence radiations passed. To help compensate for the heat losses through the window area, the heating coil was compressed by a factor of three at the ends and center of the aperture. Fig. 2 of Flate III shows how the thermocouples were rigidly mounted to facilitate measurement of the temperature at the same point on the reservoirs. Since the auxiliary ovens could not always be in the same position relative to the reservoirs, this was necessary for reproducible temperature results.

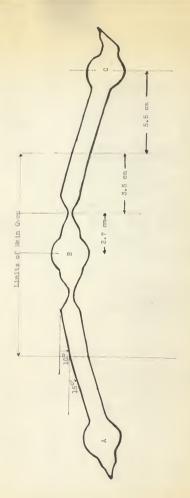
The quartz cell is shown in Plate IV. The bulb in the center is the absorption vessel. At the left end is the mercury reservoir; at the right is the reservoir containing cadmium. The constrictions serve to decrease the rate of diffusion through the tube. They are located within the limits of the main oven. Since the main oven is maintained at the highest temperature, this minimizes the possibility of condensation occurring at the constriction and hence clossing the vessel.

The tube connecting the vessel to the reservoir is bent downward to cause the mercury to flow into the reservoir where it can be more readily observed. After the quartz vessel had been blown to the proper shape, it was attached to a vacuum system and evacuated. The vacuum system consisted of a Welch Duo-seal fore pump and a Wisconsin type mercury diffusion pump. A Bayard-Alpert ionization guage was used to measure the pressure. One liquid nitrogen trap separated the guage from the diffusion pump. Another trap was placed between the guage and the container being evacuated. Phosphorous pentoxide in the system absorbed water vapor which might have been present. The cell was outgassed under vacuum at 800°C for 24 hours.

EXPLANATION OF PLATE IV

Sketch of the quarts absorption vessel and reservoirs.





After 0.7 $\,\mathrm{cm}^3$ of both mercury and cadmium were distilled into the system, it was evacuated down to approximately 2 x 10^{-6} mm. of mercury, outgassed again, and sealed under vacuum.

The light emerging from this vessel was dispersed and its wavelength measured with a Bausch and Lomb, 500mm, grating-type monochromator.

Light traps were used to prevent light from the source reaching the monochromator directly. A model 1P28 photomultiplier tube was used as the light detecting device. This tube was mounted in the receptor of a Photovolt multiplier photometer which is essentially a D.C. amplifier. The temperatures were measured with chromel-alumel thermocouples in conjunction with a Leeds and Northrup potentiometer indicator. The items mentioned above are shown in Plate II.

One of the more difficult problems in the techniques was the focusing of the system. The method found best was to first position the optical system the premeasured distance from the reference mark to the absorption vessel. The monochromator was then moved until a maximum 2537 A intensity was observed. The optical system and monochromator were then alternately moved until the 2537 A line could no longer be intensified. The monochromator was then set on the 3261 A line of cadmium and the procedure repeated until the cadmium resonant line could not be made more intense. The system was then assumed to be in focus.

To ascertain that the triplet was not excited by stepwise absorption, a black wire screen which diminished the intensity by a factor of one-half was to have been used. If stepwise absorption were the responsible excitation mechanism, the intensity would be reduced by one half when the screen was placed between the monochromator and the absorption cell and

by one fourth when interposed between the ultra-violet source and the absorption cell.

The second order ghost from the 2537 A line was so intense that it masked the 5086 A line from the cadmium triplet. This ghost was eliminated, when scanning for this line, by blocking the 2537 A line from the monochromator with a pyrex glass plate.

EXPERIMENTAL RESULTS

Tables 1 and 2 show a typical source spectrum and the thermal background from the main oven at 800°C. It was not necessary to correct the mercury lines in the following data for this background, since the mercury lines in the region where this background was significant were reflected lines. However, the cadmium line intensities listed are corrected for this background.

In Tables 3 through 8, $T_{\rm m}$ represents the average temperature of the main oven as determined by two thermocouples, one on either side of the absorption cell. $T_{\rm cd}$ and $T_{\rm hg}$ are the temperatures of the reservoirs for cadmium and meroury, as determined by a thermocouple in contact with each reservoir. These temperatures can be correlated to equilibrium vapor pressures with the aid of the graph on Plate V. (3) The subscripts after the current symbol, I, refer to the cadmium, meroury and main ovens.

The two parts of Table 3 were intensity measurements made when the constriction between the mercury reservoir and the absorption cell was about 2 mm. in diameter. The top set was taken with the monochromator slits opened to approximately 0.80 mm., and the bottom set when the slits were opened to 0.40 mm. The data in Tables 4 through 8 were taken with

the constriction mentioned above closed down to approximately 0.5 mm. in diameter. Since the 0.40 mm. slit widths were optimum for both intensity and resolution, the data on the pages following Table 3 were taken with these apertures.

In the earlier work, an attempt to find the 5086 A line of the cadmium triplet was not always made, since it would have been masked by the second order appearance of the 2537 A line of moroury. Later, the previously mentioned technique with the pyrex plate was used to eliminate this obstacle.

Table 1. Irradiating spectrum.

Table 2. Background at 800°C.

Wavelength	: Relative	were a rave ave	: Relative
in angstroms	: intensity	in angstroms	: intensity
2537	23,000	3500	0
		3600	0
2752	32	3700	0
		3800	0
2894	62	3900	0
2967	33	4000	0
		4100	0
3132	1,100	4200	0
		4300	0.2
3341	110	4400	0.4
3650	150	4500	1.0
		4600	1.2
4047	3,300	4700	1.8
		4800	3.0
4358	5,300	4900	4.0
4916	24	5000	5.8
		5100	7.6
5074		5200	10
		5300	13
5461	2,000	5400	16
		5500	19
		5600	22.5
	pearing at 5074	5700	25.2
	ond order appear-	5800	28
ance of the	2537 resonant	5900	28

Table 3. Variation of line intensities with time and temperature.

ours of	Tem!	Temperature					Re	Relative		intensity			**	Oven	Oven current	rent
time	tof	ovens in	in oc		7	Mercury lines	lines			20 2	Sadmium lines	lines		in a	in amperes	80
interval	Tm	Tod	: Thg		2557 : 3132 : 3650 : 4047 : 4358 : 5461 : 3261 : 4678 : 4800 :	3650	4047 :	4358	5461	3261:	4678	4800	5086	Lod	Ing 'Im	H.F
1	795	125	107	770	13	80	84	230	220	6/3	0	0	0	0	0	7.0
23	811	152	16							2	0	0	*	0	0	7.0
10	826	172	95	575	13	30	84	230	275	22	0	0		0	0	7.0
4	831	175	135							26	0	0		0	0	6.8
2	823	182	102	490	12	29	90	220	240	18	0	0		0	0	6.8
9	818	182	100							7	0	0		0	0	6.8
4	820	196	127	420	12	29	88	230	250	d	0	0		-1	0	6.8
00	821	202	122							6.5	0	0		٦	0	6.8
0	821	209	110	410	12	28	85	225	245	7.5	0	0		7	0	6.8
10	824	250	114							70	0	0		62	0	6.8
11	829	280	120	200	21	42	120	300	200	46	0	0		cs.	0	6.8
12	830	293	103							3.5	0	0		63	0	6.8
13	833	313	140	200	23	47	130	520	200	1.0	0	0		2.5	0	6.8
14	824	338	93							2.0	0	0		200	0	6.8
Н	851	204	82	170	5.8	13	65.5	172	96	0.4	0	0	0	0	0	
63	850	210	88							3.0	0	0	*	0	0	6.6
60	840	219	87	212	6.3	13	64	165	36	11.5	0	0		0	0	
4	837	223	88							14.0	0	0		0	0	
LO.	837	228	88	222	6.6	15	65	160	98	14.0	0	0		0	0	
8	834	240	93							22	0	0		0	1.0	
7	834	265	16	220	6.8	20	68	175	93	19.5	0	0		0	1.0	
80	834	266	86							15.5	0	0		0	1.0	
09	834	295	16	210	6.7	20	88	170	93	16.0	0	0		0	1.5	
10	834	311	89							5.0	0	0		0	1.5	
11	839	881	20							<		•		•		

* Not measured below here.

Table 4. Variation of line intensities with time and temperature.

15 min.	: Tem	rembers cure		**				Kelative		intensity				Ueao	onr	current
time	30 :	ovens	in oc			Mercury	lines				Cadmium	lines		1 1n e	in amperes	8 8
interval	e F	Tod :	. The	\$ 2537	00	3132: 3650	: 4047	: 4358	4358 : 5461	: 3261	: 467B:	4800	: 5086	Lod	The	H
1	788			510	16	28	99	160	64	0	0	0	0	0	0	6.1
23	808			460	15	28	65	170	7.1	0	0	0	0	-	0	6.5
63	812			370	16	28	67	170	74	0.1	0	0	0	٦	0	6.2
4	813			540	16	28	88	170	75	0.1	0	0	0	٦	0	6.2
ເລ	816			330	16	28	99	170	75	13	0	0	0	1.5	0	6.2
9	818			\$20	16	29	67	170	74	58	0	0	0	1.5	0	6.2
1.4	820			250	14	28	7.1	200	86	45	0	0	0	1.5	0	6.2
00	819			250	15	30	75	210	83	45	0	0	0	1.5	0	6.1
O)	819			260	14	58	73	200	86	42	0	0	0	1.5	0	6.1
10	816			250	15	29	75	200	87	40	0	0	0	1.5	0	6.1
11	815			250	14	29	74	200	87	36	0	0	0	1.5	0	6.1
12	816		-	270	15	28	74	200	86	555	0	0	0	1.5	0	6.1
18	816			250	14	29	74	190	87	51	0	0	0	2.0	0	6.1
14	818		-	230	14	28	73	200	88	7.1	0	0	0	2.0	0	6.1
15	820		-	220	14	28	73	200	88	75	0	0	0	2.0	0	6.1
16	820			220	14	28	72	200	88	75	0	0	0	2.0	0	6.1
17	820		_	230	14	28	73	190	88	75	0	0	0	2.0	0	6.1
18	821			250	14	28	73	190	20	73	0	0	0	2.0	0	6.1
19	821		-	250	14	28	72	190	83	41	0	0	0	2.0	0	6.1
20	823		_	260	14	28	22	190	88	18	0	0	0	2.0	0	6.1
21	823	-		250	14	28	72	190	89	45	0	0	0	200	0	6.1
22	824		-	260	14	28	72	190	06	18	0	0	0	200	0	6.1
23	823			260	14	27	72	190	88	9	0	0	0	20.01	0	6.1
24	818		_	270	15	53	73	200	85	N	0	0	0	2.3	0	6.1
25	810		_	280	14	28	73	190	84	1	0	0	0	200	Ç	6.0
26	817	-	-	270	14	28	72	190	86	7	0	0	0	2.5	0	6.1
27	822			280	14	27	72	190	98	0.5	0	0	0	2.5	0	6.1
28	821	437	00	280	14	27	73	200	88	0.5	0	0	0	2,5	0	6.1
29	823	-		230	14	27	73	200	83	0.7	0	0	0	2.5	0	6.1

* System was refocused preceeding this reading.

Table 5. Variation of line intensities with time and temperature.

15 min.	a Temp	Temperature		**			24	Relative		intensity				Over	Oven curren	rent
time	tor o	ovens i	oc ut		-	Mercury					Cadmium			in s	in amperes	80
interval	I I	Tod &	Thg	: 2537	: 5132	\$ 3650	4047	: 4358	4358 : 5461	: 2261 :	4678	. 4800	\$ 5086 s	Tod.	* Ing	S Im
1	789	108	81	099	20	45	120	210	94	0		0	0	0	0	6.8
~	791	130	81	900	12	53	85	220	92	0		0	0	m	0	6.8
63	797	177	83	430	12	32	87	220	85	0		0	0	m	0	6.8
41	199	202	85	340	13	53	87	230	87	0.2		0	0	1	0	6.8
ເລ	800	220	86	310	12	32	87	230	82	0.4		0	0	-	0	6.8
89	802	230	83	310	13	33	80	220	86	1.5		0	0	-	0	6.8
2	802	261	86	450	20	40	100	250	84	88		0	0	1.5	0	6.8
89	803	270	89	400	19	40	100	240	80	81		0	0	1.5	0	6.8
00	803	280	89	470	20	48	120	290	97	88		0	0	1.5	0	6.8
10	802	289	88	480	20	47	120	290	26	20		0	0	1.5	0	8.8
11	800	290	88	490	24	47	120	290	96	25	0	0	0	1.5	0	6.8
12	800	290	88	490	200	47	120	280	96	28		0	0	1.5	0	6.8
13	800	290	88	490	83	46	120	280	96	31		0	0	1.5	0	6.8
14	800	292	88	490	24	46	120	280	96	36		0	0	1.5	0	6.8
15	800	252	88	490	23	46	120	280	98	40		0	0	1.5	0	6.8
18	800	200	88	-	25	46	120	270	94	42	0	0	0	1.5	0	8,00
19	800	326	88	490	24	46	120	260 -	88	64	0	0	0	2.0	0	6.8
20	800	345	88		25	45	110	260	92	98	0	0	0	2.0	0	6.7
21	800	353	83	4.	24	44	110	260	92	92	0	0	0	2.0	0	6.7
22	718	260	80	4.	CS PS	48	120	330	120	100	0	0	0	2.0	0	6.7
28	808	267	83	-	23	20	130	340	120	20	0	0	0	2.0	0	6.8
24	810	268	81	-	20	20	130	330	330	25	0	0	0	2.0	0	6.8
25	683	265	76	4.	23	49	140	340	120	60	0	0	0	2.0	0	3.4
26	689	898	117	-	12	37	87	230	90	15	0	0	0	2.5	0	4.0
27	686	415	120	-	12	30	88	230	92	14	0	0	0	2.5	0	4.0
28	687	417	81		11	30	88	230	16	4	0	0	0	2.4	0	4.0
29	684	419	101		11	85	00	240	50	c	0	0	0	0	(4

Table 6. Variation of line intensities with time and temperature.

1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	15 min.	: Tem:	Temperature	-	**				Re	slativ	Relative intensity					Ze Ode	Owen current	rent
1	time	1 of	t sueve	-	100		M	ercury	lines			2	admium	lines		do or	mper	80
602 72 81 400 9 19 50 180 67 0 0 0 0 1.0 0 181 142 85 560 9 19 40 180 68 0.1 0 0 0 1.0 0 181 142 85 560 9 19 40 180 68 0.1 0 0 0 0 1.0 0 182 181 142 82 224 94 220 8 19 49 120 70 0.2 0 0 0 0 1.0 0 1.0 0 182 224 94 220 8 19 49 120 70 0.2 0 0 0 0 1.0 0 1.0 0 182 225 224 94 280 9 180 68 110 63 19 0.1 0 0 0 1.	interval			P	. 4		5132	3650	4047		5461	: 3261	: 4678	4800	5086	Lod	00	H
\$\text{811} 142 \text{85} \text{85} \text{550} \text{9} \text{150} \text{150} \text{65} \text{150}	-	802	72	w	12	400	6	13	20	130	67	0	0	0	0	0	-	6.2
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	0	811	142	00	22	250	O	19	20	130	68	0	0	0	0	1.0	_	6.2
\$22.2.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.	1/3	818	180	Ψ	88	270	0	19	49	130	69	0.1	0	0	0	1.0		6.2
852 224 994 220 8 19 45 120 70 0.2 0 0 0 1.0 0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	4	821	202	00	8	240	00	18	48	120	69	0.1	_	0	0	1.0		6.2
\$\text{8.5} 22\$ \$\text{9.4} 260 \$\text{8.18} 46 \$\text{110}\$ \$\text{6.11}\$ \$6.11	ın	828	224	0,0	34	220	00	19	49	120	20	0.0	_	0	0	1.0		6.1
\$\text{Sign 256} \text{ \$97 \text{ \$260} \$9 \text{ \$18 26} \$97 \text{ \$260} \$9 \text{ \$18 273} \$97 \text{ \$260} \$9 \text{ \$18 280} \$18 \$280 13 24 61 150 74 57 67 0 \te	60	823	229	- 00	34	260	00	18	45	110	63	0.2	_	0	0	1.0		6.1
1, 2, 77 27 25 25 61 150 74 57 0 0 0 1, 5 0 0 1, 5 0 1, 5 0 1, 5 0 0 1, 5 0 0 1, 5 0 0 1, 5 0 0 0 1, 5 0 0 0 0 0 0 0 0 0	7	818	256	00	26	260	6	18	45	110	61	19		0	0	1.5		6.1
15 277 250 15 24 61 150 75 54 0 0 0 1-5	89	816	273	0,	26	250	6	25	61	150	74	57		0	0	1.5	0	6.1
15 280 28 230 13 25 61 150 74 42 0 0 0 1.5 0 15 286 282 230 13 25 61 150 77 42 0 0 0 1.5 0 15 285 280 13 25 60 150 77 26 0 0 0 1.5 0 15 285 280 12 24 60 150 77 26 0 0 0 1.5 0 15 285 310 220 12 24 60 140 76 45 0 0 0 2.0 0 15 285 310 320 32 24 59 150 76 45 0 0 0 2.0 0 15 285 341 342 24 59 140 76 54 0 0 0 2.0 0 15 285 340 32 24 59 140 76 54 0 0 0 2.0 0 15 285 340 32 22 58 140 76 54 0 0 0 2.0 0 15 285 390 39 220 12 23 56 140 76 54 0 0 0 2.3 0 16 285 340 340 75 34 0 75 34 0 0 0 0 17 285 340 340 340 76 54 0 0 0 0 18 285 340 340 340 76 340	0	816	277	00	26	250	13	24	61	150	75	34		0	0	1.5	0	6.1
15 285 95 230 13 25 61 150 74 42 0 0 0 1.5 0 17 286 98 220 13 25 61 150 77 26 0 0 0 1.5 0 18 25 235 100 220 12 24 60 150 77 26 0 0 0 1.5 0 18 235 103 200 12 24 59 140 76 45 0 0 0 2.0 18 241 103 200 13 24 59 140 75 55 0 0 0 2.0 18 25 350 350 35 24 59 140 76 54 0 0 0 2.0 18 25 350 350 35 24 59 140 76 54 0 0 0 2.0 18 25 350 35 35 35 340 76 54 0 0 0 2.0 18 25 350 35 25 35 340 75 35 0 0 0 2.0 18 25 350 35 25 35 340 75 35 0 0 0 2.0 18 25 350 35 25 35 340 75 35 35 18 25 350 35 25 35 340 74 1 0 0 0 0 18 25 350 35 35 35 340 74 1 0 0 0 18 25 35 35 35 35 35 35 35	10	815	280		88	230	13	25	61	150	75	47		0	0	1.5	0	6.1
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025 226 100 150 77 19 0 1.6 025 235 107 200 12 24 59 150 76 36 0 0 2.0 025 354 103 200 13 24 59 140 75 50 0 0 2.0 026 354 103 200 13 24 59 140 75 50 0 0 2.0 026 356 100 200 13 24 59 140 76 54 0 0 2.0 026 350 36 20 10 76 54 0 0 0 2.0 026 350 36 20 10 76 54 0 0 0 2.0 0 2.0 0 2.0 0 0 2.0 0 2.0 0 0 2.0 0	12	617	286	00	93	220	13	25	90	150	22	26	0	0	0	1.5	0	6.1
S25 255 100 220 12 24 60 150 77 13 0 0 0 1.5 U25 353 103 200 13 24 59 150 76 38 0 0 0 2.0 U25 353 103 200 13 24 59 140 76 58 0 0 0 2.0 U25 355 103 200 13 24 59 140 75 50 0 0 0 2.0 U25 355 103 200 13 24 59 140 76 54 0 0 0 2.0 U25 355 360 36 210 13 24 59 140 76 54 0 0 0 0 U25 357 36 36 210 13 24 59 140 76 54 0 0 0 U25 377 390 39 220 12 23 55 140 75 46 0 0 0 U25 357 400 100 220 12 23 55 140 74 4 0 0 0 U25 356 400 39 220 12 22 54 140 74 0 0 0 U25 366 402 39 220 12 22 54 140 74 0 0 0 U25 366 402 30 20 22 25 340 75 0 0 0 U25 366 402 30 31 22 25 340 75 0 0 0 U25 366 402 31 32 32 34 32 30 0 0 0 U25 366 402 30 31 32 35 340 75 0 0 0 U25 25 36 36 36 36 36 36 36 3																		
UPS SIS LOY ZOO 12 24 59 LSO 76 58 0 0 2.0 0255 5.85 1.03 20.0 13 24 60 140 76 46 0 0 2.0 0256 5.85 1.03 20.0 13 24 60 140 76 56 0 0 2.0 0256 5.85 1.03 20.0 12 23 58 140 76 54 0 0 2.0 0256 5.85 1.00 76 54 0 0 0 2.0 055 5.90 1.40 76 54 0 0 0 2.0 055 5.90 1.40 76 54 0 0 0 2.2 055 5.90 1.40 76 55 0 0 0 2.2 056 5.90 1.40 77 <td>15</td> <td>825</td> <td></td> <td>10</td> <td>00</td> <td>220</td> <td>12</td> <td>24</td> <td>60</td> <td>150</td> <td>77</td> <td>19</td> <td>0</td> <td>0</td> <td>0</td> <td>1.5</td> <td>0</td> <td>6.1</td>	15	825		10	00	220	12	24	60	150	77	19	0	0	0	1.5	0	6.1
925 335 1103 200 13 24 60 140 76 45 0 0 2.0 926 341 103 200 13 24 59 140 75 56 0 0 2.0 926 356 100 20 140 76 56 0 0 2.0 926 356 100 76 56 0 0 2.0 0 2.0 825 376 36 20 13 24 59 140 76 56 0 0 2.0 825 376 36 140 76 56 0 0 2.0 2.0 826 377 40 75 46 0 0 2.2 2.0 826 397 30 75 46 0 0 2.2 2.0 0 0 2.2 2.0 0 0 2.2	16	325		H	24	200	12	24	59	150	26	88		0	0	2.0	0	6.1
126 55.41 10.3 20.0 13 2.4 59 14.0 75 50 0 0 2.0 126 55.0 10.3 20.0 12 2.5 59 140 76 54 0 0 2.0 126 55.0 10.0 20.0 12 2.5 59 140 76 54 0 0 2.0 2.0 125 57.0 140 76 54 0 0 2.0	17	325		ĭ	53	200	13	24	9	140	76	45		0	0	2.0		6.1
126 350 103 200 13 24 59 140 76 54 0 0 2.0 126 356 100 22 58 140 76 55 0 0 2.0 126 356 30 22 58 140 76 55 0 0 2.0 125 376 36 23 140 76 55 0 0 2.2 126 376 36 140 76 55 0 0 2.3 126 377 34 76 19 0 0 2.3 126 377 34 76 10 0 0 2.3 126 377 36 140 76 4 0 0 2.3 127 23 55 140 74 4 0 0 2.3 128 402 96 20	18	325		J	200	200	13	24	59	140	75	50		0	0	2.0	_	6.1
126 356 100 200 12 25 58 140 76 55 0 0 2.0 125 356 376 13 22 58 140 76 55 0 0 2.0 2.0 825 376 39 20 13 23 56 140 75 46 0 0 2.2 3 825 390 89 220 12 23 55 140 75 46 0 0 2.2 3 826 400 100 220 12 23 55 140 74 4 0 0 2.2 3 826 400 10 22 25 140 74 4 0 0 2.2 3 826 400 96 220 12 22 54 140 74 0.7 0 0 2.2 3	19	825		7	53	200	13	24	59	140	76	54		0	0	2.0	_	6.1
125 360 96 210 13 24 59 140 76 54 0 0 2.0 825 376 96 210 13 23 56 140 76 58 0 0 2.5 825 377 64 220 12 23 56 140 75 19 0 0 2.5 826 400 10 22 25 55 140 74 4 0 0 2.5 826 402 96 220 12 22 55 140 74 4 0 0 2.5 826 402 96 220 12 22 55 140 74 0.7 0 0 2.5 826 402 96 220 12 22 55 140 75 0 0 0 2.5 826 405 97 20	20	825		1	8	200	12	23	58	140	75	53		0	0	2.0		6.1
825 376 96 210 13 23 58 140 75 55 0 0 0 2.3 8 8 8 8 8 9 8 20 12 23 58 140 75 46 0 0 2 2.3 8 8 8 8 9 8 20 12 23 55 140 75 46 0 0 0 2.3 8 8 8 8 9 9 8 20 12 23 55 140 77 4 4 0 0 0 2 2.3 8 8 8 9 9 8 20 12 22 55 140 77 1 0 0 0 2.3 8 8 8 9 9 9 20 12 22 55 140 77 1 0 0 0 2.3 8 8 8 9 9 20 12 22 55 140 77 1 0 0 0 2.3 8 8 8 9 9 20 12 22 55 140 77 1 0 0 0 2.3 8 8 8 9 9 20 12 22 55 140 77 0.7 0 0 0 2.3 8 8 9 9 0 0 12 22 55 140 77 0.5 0 0 0 2.3 8 8 9 9 0 0 12 22 55 140 77 0.5 0 0 0 2.3 8 9 9 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	21	825		0.	96	210	13	24	59	140	76	54		0	0	2.0		6.1
826 590 89 220 12 23 56 140 75 46 0 0 0 2.3 826 537 84 220 12 23 55 140 74 4 0 0 0 2.3 82 826 400 100 220 12 22 55 140 74 4 0 0 0 2.3 82 826 400 96 220 12 22 55 140 74 4 0 0 0 2.3 82 826 400 96 220 12 22 56 140 74 1 0 0 0 2.3 82 826 400 96 210 12 22 54 140 74 0.7 0 0 0 2.5 82 826 400 97 20 12 22 54 140 77 0.5 0 0 0 2.5 82 826 405 97 20 12 22 55 140 77 0.5 0 0 0 2.5	22	825		-	96	210	13	23	58	140	76	53		0	0	2.8		6.1
826 837 84 820 12 23 55 140 75 19 0 0 0 2.3 826 400 100 220 12 22 55 140 74 4 0 0 0 2.3 826 400 86 820 12 22 55 140 74 1 0 0 0 2.3 826 402 96 220 12 22 55 140 74 0.7 0 0 0 2.3 826 402 97 230 12 22 55 140 73 0.5 0 0 0 2.3 826 405 97 230 12 22 55 140 73 0.5 0 0 0 2.3	23	825			88	220	12	23	56	140	75	46		0	0	2.5		6.1
825 400 100 220 12 22 55 140 74 4 0 0 0 2.8 58 6 140 74 1 0 0 0 2.8 58 6 402 96 220 12 22 55 140 74 0.7 0 0 0 2.8 58 6 402 96 220 12 22 55 140 77 0.7 0 0 0 2.8 58 6 402 97 230 12 22 55 140 77 0.5 0 0 0 2.8 58 6 405 97 230 12 22 55 140 77 0.5 0 0 0 2.8 58 6 405 405 40 12 22 55 140 77 0.5 0 0 0 2.8 58 6 405 405 405 40 12 22 55 140 77 0.5 0 0 0 2.8 58 6 405 405 405 405 405 405 405 405 405 405	24	825		-	34	220	12	23	55	140	75	13		0	0	2.3		6.1
826 400 96 820 12 22 55 140 74 1 0 0 0 2.8 826 402 98 220 12 22 54 140 74 0.7 0 0 0 2.8 826 405 98 210 12 22 55 140 75 0.5 0 0 0 2.8 826 405 97 280 12 22 55 140 77 0.5 0 0 0 2.8	25	825		H	90	220	12	23	55	140	74	4		0	0	200		6.1
826 402 96 220 12 22 54 140 74 0.7 0 0 0 2.5 826 400 97 20.0 12 2.5 826 400 73 0.5 0 0 0 2.5 826 405 405 12 22 55 140 73 0.5 0 0 0 2.5	26	826		0.	96	220	12	22	55	140	74	7		0	0	2.8		6.1
826 400 98 210 12 22 55 140 73 0.5 0 0 0 826 405 97 230 12 22 55 140 73 0.5 0 0 0	27	826			98	220	12	22	54	140	74	0.7		0	0	20.01		6.1
826 405 97 230 12 22 55 140 73 0.5 0 0 0	28	826			98	210	12	22	55	140	73	0.5		0	0	200	0	6.1
	29	826			26	230	12	22	55	140	73	0.5	0	0	0	20	0	6.1

Table 7. Variation of line intensities with time and temperature.

F-f-ma							4	ATOTOL	ATTOTION TO TRADITOR	SOTOT				CAGE	mo I	OVER CULTBILL
OTHER DESIGNATION OF THE PERSON OF THE PERSO	: of	of ovens in	tn oc			Serenty	line		**		Sadmium lines	lines		in a	In amperes	80
nterval	. Ta	a Tod	a Thg	: 2537	: 3132	: 3650	: 4047	1 4358 :	5461:	3261	4678	4678 : 4800 :	: 5088 :	I od	Ing	I S
-1	843	386	53	370	14	8	7.5	190	500	-	0	0	0	63	0	6.
63	851	396	124	530	13	27	7.1	180	16	1.1	0	0	0	2.0	0	6.1
100	829	402	124	230	13	27	72	180	83	1.6	0	0	0		0	6.3
4	828	402	123	230	14	27	7.1	180	89	1.5	0	0	0		0	6.1
1O	828	419	169	300	13	26	70	180	88	1.5	0	0	0	2.5	0	6.1
9	828	426	180	290	13	26	20	180	88	1.8	0	0	0		0	6.1
7	828	428	189	280	13	26	70	170	87	1.7	0	0	0		0	6.1
00	831	435	224	220	7.5	26	68	180	88	0.5	0	0	0	2.5	0	6.3
6	836	438	242	200	13	26	68	170	88	0.4	0	0	0		0	6.1
10	836	443	259	130	13	26	68	170	86	9.0	0	0	0	2.5	0	6.0
11	834	440	263	180	13	25	99	170	86		0	0	0		0	6.0
75	834	440	270	290	18	28	9	120	99	1.0	0	0	0	20	0	6.0
-4	783	370	73	520	18	28	9	130	56	0.5	0	0	0	53	0	6.0
03	800	588	78	490	18	27	58	130	59	0.8	0	0	0	3	0	6.3
8/3	812	398	78	480	13	27	59	130	09	6.0	0	0	0	2.4	0	6.1
ela ela	818	412	85	480	18	26	57	130	64	0.6	0	0	0	2.4	0	6.1
es es	822	414	117	470	18	56	56	130	64	9.0	0	0	0	2.4	0	6.1
9	822	416	116	470	16	22	99	130	63	0.5	0	0	0	2.4	0	6.3
-	823	417	122	470	16	26	56	130	63	0.5	0	0	0	2.4	0	6.1
00	817	419	165	470	16	26	57	130	62	0.9	0	0	0	2.4	0	6.0
0	817	417	174	470	17	26	57	130	09	1.0	0	0	0	2.4	0	0.9
10	814	419	182	460	17	26	56	130	19	1.0	0	0	0	2.4	0	6.0
11	817	419	204	420	17	25	56	130	61	0.6	0	0	0	2.4	0	6.0
12	821	421	236	230	17	25	55	130	62	0.3	0	0	0	2.4	0	6.0
13	823	424	249	360	17	25	55	130	62	0.5	0	0	0	2.4	0	6.0
* *																

Table 8. Variation of line intensities with time and temperature.

time				-			75	יום דם מד מון		intensity				CAGE	l our	Gven current
aterva]	to:	10	in oc			Mercury	lines			3	Cadmium	lines		i in a	In amperes	82 69
-	L . Tu	Tod 3	Thg	1 2537 1		3132; 3650;		4047 : 4358	: 5461	: 5261 : 4678:	46781	4800:	5086	Lod	t Ing	니티
1	822	402	79	230	11	21	55	130	72	0.0	0	0	0	63	0	6.1
N	825	230	107	230	11	21	52	130	7.1	0.3	0	0	0	200	0	6.1
19	825	400	112	220	11	21	51	130	7.1	0.4	0	0	0		0	6.1
41	825	407	143	210	11	21	51	130	70	0.5	0	0	0	2.4	0	6.1
10	825	412	145	210	10	20	51	130	20	0.5	0	0	0		0	6.1
9	825	412	189	200	10	20	20	120	69	0.8	0	0	0	200	0	6.1
2*	823	410	130	160	0	19	49	130	73	0.5	0	0	0		0	6.1
00	837	419	249	230	12	13	49	150	75	0.3	0	0	0		0.5	
0	837	421	266	220	11	18	48	130	78	0.5	0	0	0	2.5	0.5	
10	835	424	293	210	11	13	44	100	61	7	0	0	0	63	1.0	6.0
11	830	424	305	200	11	19	43	100	61	2	0	0	0	2.3	1.0	
12	830	417	217	220	11	18	40	100	26	9	0	0	0	63	1.0	6.0
ri	810	412	83	230	10	17	40	100	54	0.8	0	0	0	2.4	0	6.0
os.	810	409	100	230	10	17	40	100	10	0.7	0	0	0	2.4	0	
6/3	807	410	110	230	10	18	41	100	53	0.5	0	0	0	2.4	0	
4	807	407	167	230	10	17	40	100	50	0.7	0	0	0	2.4	0	
LO	810	407	192	210	10	17	40	100	53	0.5	0	0	0	2.4	0	6.0
9	810	404	235	200	10	17	40	100	53		0	0	0	2.4	0.5	
4	813	410	274	130	10	17	39	100	53	0.5	0	0	0	2.4	0.5	
න	813	412	264	180	10	17	619	100	553	0.9	0	0	0	2.4	0.5	
o	812	412	285	180	10	17	40	100	54	ເລ	0	0	0	2.4	1.0	
10	817	413	302	170	10	17	40	100	55	8	0	0	0	2.4	1.0	
11	820	412	513	170	10	17	39	100	55	ıs	0	0	0	2.4	1.0	
12	820	412	317	170	10	17	39	100	55	4	0	0	0	2.4	1.0	
13	820	412	317	170	10	17	00	100	55	60	0	0	0	2.4	1.0	6.0
14	820	412	210	170	10	17	39	100	55	₁	0	0	0	2.4	1.0	

* Ovens were moved during adjustment.

DISCUSSION OF RESULTS

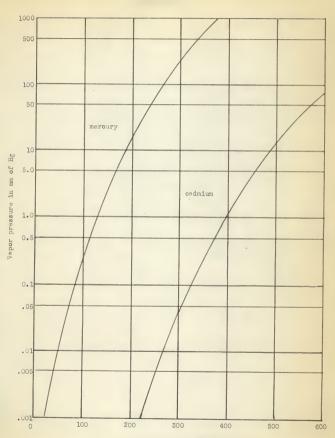
The lines of principal interest for this problem were those of cadmium. The 3261 A line of cadmium was observed to be moderately intense at times. It was found that the optimum initial conditions for its observation were when the mercury and cadmium were together in the reservoir which was to be heated. The runs in Tables 4, 5, and 6 were started by having both cadmium and mercury in the cadmium reservoir. The mercury reservoir was left in the open air. As the mixture in the cadmium reservoir was heated, both the mercury and cadmium vapor began to move out. At a temperature of 250°C, the cadmium vapor pressure was sufficient for the 3261 A line of cadmium to be observed. The results show that the line normally appeared more intense during a rapid temperature increase, which followed an abrupt increase in the current. After the temperature was reasonably stable, the intensity would decrease. No positive explanation is given for this action. However, it may be that the mercury, which has a high vapor pressure at these temperatures as indicated by the graph on Plate V, carried small particles of cadmium into the abscrption cell as it rushed from the cadmium reservoir. These small cadmium particles would then be vaporized and furnish sufficient concentrations of cadmium vapor for the resonant line to be observed. As the cadmium reservoir temperature was further increased, this intensity pulsing was observed again. At 400°C, the intensity of the 3261 A line had diminished to near zero, and remained there even though cadmium remained in the heated cell and a relatively high mercury vapor pressure was present.

According to the literature, the optimum temperatures for sensitized fluorescence of mercury and cadmium are 400°C for the cadmium and 100°C for the mercury. Further literature research disclosed that the behavior

EXPLANATION OF PLATE V

Pressure vs. temperature curves for mercury and cadmium.

PLATE V



Temperature in degrees centigrade

just described had been observed before by Mitchell, (4) when studying the polarization of sensitized fluorescence in mercury and cadmium vapors. His explanation was that the cadmium vapor carried the mercury vapor from the absorption cell with it, as it migrated to a colder reservoir. Due to the high vapor pressure of mercury at 400°C, it is reasonable to assume that little mercury would be left at equilibrium in the cadmium reservoir. The mercury vapor pressure would then be controlled by the reservoir whose temperature was between 80 and 100°C, where its equilibrium vapor pressure would be of the order of 1 mm. of mercury, as would be the vapor pressure of cadmium at 400°C. The non-equilibrium condition of the cadmium would cause streaming and a degree of pumping. Mitchell's explanation seems

The constriction between the mercury reservoir and the absorption cell was reduced to one-fourth of its original diameter in an effort to decrease this pumping rate. The data in Tables 4 through 8 are typical of data taken after the smaller opening was in use. Still, at the optimum temperatures, the intensity of the cadmium resonant line was negligible. Some moderate intensities were obtained during the transient stages of heating. These intensities might possibly be exceeded if the optimum concentrations of the two vapors could be attained under equilibrium conditions.

Tables 7 and 8 are illustrative of data obtained while trying to find a mercury temperature which would neutralize this pumping action after the cadmium vapor had transported the mercury vapor out of the absorption cell. Only when the mercury temperature was near 500°C was the cadmium resonant line observed again, even then the intensity was low. In view of this low

intensity and the fact that several mishaps had occurred near this mercury temperature, it was felt that it would be neither safe nor fruitful to continue at these temperatures.

The primary objective of this experiment was to obtain some quantitative measurements of the cadmium triplet. The intensities involved were so low that they were not discernible above the random fluctuations of the measuring device, which were less than one tenth of one unit. Considering the intensities of the observed cadmium resonant line, this is not altogether surprising. Franck and Cario calculated that only one part in 3 x 10⁵ of all collisions have sufficient relative kinetic energy to supply the 1.4 evenergy difference necessary to excite the cadmium atom to the 6⁵S₁ level. Since it is energetically possible for all collisions between excited mercury atoms and cadmium atoms to result in an excited cadmium atom, one would expect this ratio or a lower one for the intensities of the resonant line and the triplet.

The results also indicate some variation in the intensities of the mercury lines. These variations were not in general correlated to the results for cadmium. The intensity of the 2537 A line was due not only to resonance radiation, but also to scattering. The contribution of each of these phenomena to the total intensity is not known. The 3132 and 3650 A lines are attributable to scattering. The intensities of the 5416, 4558, and 4047 A lines from the source were moderately high. It is possible that these lines could be absorbed by excited mercury atoms in the 6⁵P levels, to raise the atom to the 7⁵S₁ level. Resonance radiation would result. The test for stepwise absorption was made. After correcting for the thermal background, the resultant intensities were the same

whether the screen was placed in the incident or outgoing beam. The conclusion was that these were also scattered lines. The variation in the intensity of these lines can be attributed to two factors. First, the mercury source does not maintain a constant intensity output. Secondly, the geometry of the system changed slightly due to thermal expansion of the ovens and the quartz cell.

CONCLUSIONS

Two conclusions can be drawn from this experiment. Since the optimum conditions for sensitized fluorescence are to have equal vapor pressures, this experiment should be performed with the mercury at 100°C and the cadmium at 400°C. Due to the pumping action of the cadmium, this is not feasible with the present arrangement. The solution of the problem by Mitchell indicates that helium equal in pressure to 2 mm. of mercury should be added to the cell in future experiments of this nature. Secondly, the problem of insufficient intensities must be overcome. The present system is clearly inadequate in this respect. If a stronger mercury light source cannot be obtained, perhaps more than one source could be used to irradiate the absorption cell.

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SENSITIZED FLUORESCENCE IN A MIXTURE OF MERCURY AND CADMIUM VAPORS

by

JOSEPH SHARON WELLS

B. S., Kansas State College of Agriculture and Applied Science, 1956

AN ABSTRACT OF A THESIS

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requirements for the degree

MASTER OF SCIENCE

Department of Physics

KANSAS STATE COLLEGE
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energy levels through a cooperative effort between quantum and kinetic energies during a collision of the second kind. They cited evidence, which was obtained through studies of sensitized fluorescence of servoury and cadmium vapors, to substantiate their hypothesis. The major portion of their evidence was dependent upon the intensity of a triplet emanating from the $6^{3}S_{1}$ level of cadmium. This level could be excited only when 1.4 ev of energy was available in the form of relative kinetic energy between the mercury and cadmium atoms. The purpose of this research was to confirm their results and obtain some temperature versus intensity relations with the aid of improved techniques and equipment.

In the original work, the sensitized fluorescence was analyzed with the aid of a quartz spectrograph. The intensities on the spectrogram were weak and only a two point correlation was obtained between the temperatures and the intensities of the cadmium in question. One of these values of intensity was zero. In the present research, temperatures were controllable to a greater degree. The desired lines were selected for measurement by a Fausch and Lomb monochromator. A photo multiplier and D.C. amplifier system of high sensitivity were used to measure the relative intensities. This system had the advantages of speed in focusing, continuous monitoring of intensities, and a relative scale for the value of the intensities.

The problem of weak intensities again prevented the desired quantitative information from being obtained. The intensities of the triplet were less than the random fluctuations of the measuring device. Possibly this low intensity was partially due to the behavior of the materials in the absorption well. The recommended concentrations of the mercury and cadmium vapors could not be obtained under equilibrium conditions due to the pumping action of the cadmium at the optimum temperature. The addition of 2 mm. of mercury pressure of helium to the absorption cell to prevent pumping and the acquisition of a stronger mercury light source were concluded to be necessary for future experiments of this nature.