EFFECT OF ENZYME APPLICATION IN TEMPER WATER ON WHEAT MILLING

by

JUHYUN YOO

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Major Professor Dr. Ekramul Haque

Abstract

The effect of enzyme in temper water on wheat milling performance and flour quality was studied. Five independent variables, enzyme concentration, incubation time, incubation temperature, tempered wheat moisture content, and tempering water pH, were studied. An enzyme cocktail consisting of cellulase, xylanase, and pectinase was used at 5 different concentrations. A single pure variety of hard red winter wheat was tempered under defined conditions following an RSM central composite design which required 33 tests including 7 replicates. Each treatment had 5 levels: high, medium high, medium, medium low, and low. After tempering, the physical characteristics of the wheat kernel were determined by using the Single Kernel Characterization System. An experimental laboratory mill (Ross Mill) was used to mill wheat into flour. Thirteen streams of flour, and additional streams of bran, shorts, red dog, and germ were obtained. Product yield, protein, ash, and flour color were evaluated. The data were analyzed and compared using the software SAS and RSM Plus.

The data showed that incubation time was the only significant factor affecting the tempered wheat hardness (p<0.05). The treatments affected the flour yield from the break rolls more than that from the reduction rolls. However, a maximum point for flour yield was not found. The relationship between treatments and flour yield was established with a prediction model equation. Also, the enzyme effect on the dough properties and bread making were investigated. The treatments did not affect the optimum water absorption for the flours. However, enzyme treated flours showed shorter mixing times. Regardless of the differences in mixing times, the specific loaf volumes were not significantly different for the all treatments.

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Dedication

This dissertation is dedicated to my family.

CHAPTER 1 - Introduction

Milling is a process by which cereals such as wheat are reduced in particle size so as to produce flour. Wheat milling consists of grain cleaning, tempering, grinding (break system and reduction system), and size separation. The ground particle size depends on the end-use and the type of products. Tempering means the addition of water or sometimes removal of water followed by a rest period (Posner and Hibbs, 1997). The unique feature of wheat that makes milling possible is that the three parts of the kernel (bran, germ, and endosperm) differ in relative toughness or friability.

The purpose of tempering is to toughen the bran, so it can resist being broken into small pieces, and to mellow the endosperm and make it easier to grind. One of the main goals in wheat tempering before milling is to distribute water in the kernel as uniformly as possible. Tempering is considered a very important stage for the miller from technical, flour quality, and economic points of view. The amount of water added varies with the original moisture content of the wheat, the relative humidity in the mill, and the desired moisture content for grinding. The resting time between tempering and milling can be determined from the rate of water diffusion throughout the whole kernel. The break system in the mill is very sensitive to variations in tempering moisture in the kernel from the optimum level. Break flour from low-moisture wheat has higher ash values, which is undesirable.

In hard red winter wheat, the starch endosperm (potential flour) amounts to 81.4 to 84.1% (dry matter basis) of the wheat kernel (Hinton, 1959). Despite the complexity of the conventional milling process, the normal commercial extraction rate is 70 to 77% (Jones and Ziegler, 1964). In the last decade or so, research efforts were made in various operations related to the milling process in order to separate bran more easily and effectively. The Satake Company developed a mechanical wheat debranning process, but the reception from the industry for this process was somewhat cold or luke-warm at best, because of its excessive energy need and questionable effectiveness in efficient bran removal.

For a long time, wheat milling has been accomplished by mechanical methods, but they have two disadvantages: 1) the loss of nutritional components which ideally would be recovered

and included in the flour without causing detrimental effects on flour quality, and 2) there is a large portion of endosperm left attached to the wheat bran. Although low moisture content tempered wheat and hard grinding can increase the flour extraction, it results in undesirable quality parameters such as high ash content and dark color. Therefore, as an alternative, the modification in chemical composition or physical structure of wheat can be seriously considered. Recently, enzymes have been introduced to various industries as solutions to many problems and there are many ongoing research projects regarding enzyme applications to maximize the positive effect in the industries. The uses of enzymes during tempering and their effects on the efficacy and efficiency of the milling process have not yet been established. The effort to optimize the condition for the maximum enzyme activity has not yet been published. From the viewpoints of improving the process, enhancing profitability to the cereal miller, human health benefits, and food safety, it is desirable that we research alternative methods for bran separation.

CHAPTER 2 - Literature Review

2.1. Wheat structure and composition

Wheat grain (Figure 2.1) consists of bran, endosperm, and germ. The percentages of each part of grain in the wheat kernel are shown in Table 2.1. Bran consists of pericarp and aleurone.

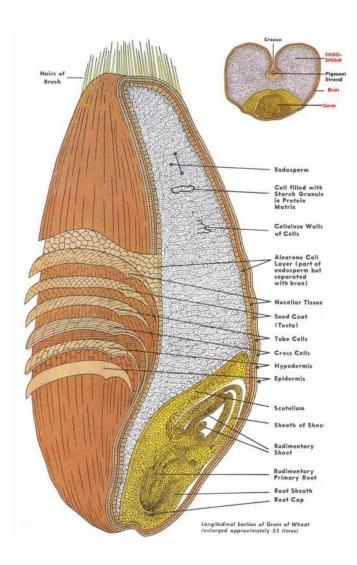


Figure 2.1 Longitudinal and cross sections of wheat kernel (adapted from Hoseney, 1998)

Table 2.1 The parts of grain in wheat kernels

Part of grain	Percentage of kernel weight
Bran	(15.0)
Pericarp	8.0
Aleurone	7.0
Germ	(2.5)
Embryo	1.0
Scutellum	1.5
Starchy endosperm	(82.5)
Outer	12.5
Middle	12.5
Inner	57.5
Whole grain	100
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Adapted from Hinton (1953)

2.1.1. *Aleurone*

As shown in Table 1, aleurone takes up a large portion in the wheat kernel. Aleurone makes up to 7 to 9% (w/w) of the kernel, and 45 to 50% of the bran fraction. The aleurone layer (Figure 2.2) consists of living tissue, generally one cell thick, completely surrounding the kernel, covering both the starchy endosperm and the germ. From the botanical standpoint, it is the outer layer of endosperm (Hoseney, 1998). However, as it is removed during milling, it constitutes the innermost layer of bran. The aleurone layer is presumed to play a significant role in the milling process in that the separation of bran from starchy endosperm occurs near the aleurone layer interface where there is a different structure and biochemical composition from the rest of the endosperm. Aleurone contains most of the nutrients and physiological benefits of whole wheat but in a highly concentrated form. Table 2.2 shows the composition of wheat aleurone. Protein, dietary fiber, & lipid rich components are encased within the living aleurone cells. Aleurone cell walls are very strong, so as a result, they are not normally broken during the conventional milling process. The upper digestive tract also cannot digest the aleurone cells because of their very strong walls. As a result, the nutrients encased in the cells are not available to the body until they reach the large intestine. At that point, high-quality proteins, lipids, and B-vitamins are

released for absorption and digestion (Buri et al. 2004). For this reason, there are many ongoing research projects attempting to add value to the bran, or more precisely to the aleurone.

Greffeuille and coworker (2004) studied the distribution of the aleurone layer during the common wheat milling process by using the biochemical marker identification. Two molecular markers, phytic and para-coumaric (*p*-CA) acids, were used to quantify and describe the fate of the aleurone layer cellular content or cell walls in flour streams and total flour respectively. They found that the aleurone cellular content and the cell walls showed distinct fates in the milling process. The aleurone cell walls were released at the first break stage and found mostly in the break flours, whereas cellular content remained at the same level through the break stages to the reducing stages. Any damage to the aleurone cell walls is followed by release of the cellular content, so the flour after the break stage, therefore, must be enriched in aleurone cellular content, which means that the mode of grain rupture has a significant influence on the flour composition and nutrition.

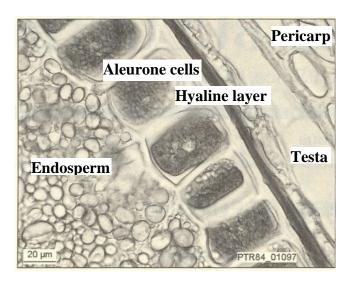


Figure 2.2 Microscopic view of the aleurone layer (adapted from Buri et al. 2004)

Peyron and coworker (2003) focused on the characteristics of the aleurone layer and its association with wheat milling behavior. They suggested that there were two possible factors influencing the milling properties, which were the variability in thickness of the aleurone layer and the irregularity in shape of aleurone cells. Concerning the thickness and irregularity of the aleurone layer, large variations within grains and between grains from the distinct wheat samples

were observed. Consequently, it was found that the thickness of the aleurone layer and the structure of the aleurone did not significantly affect wheat milling behavior. Furthermore, the necessity of an investigation of the tissue adhesion mechanism on the aleurone and subaleurone layer interface was emphasized. They also hypothesized that the concentration and distribution of ferulic acid dehydrodimers in cells could be a factor which controls tissue adhesion.

Table 2.2 Wheat aleurone composition

Constituent	Method	Unit	Content
Crude protein, N×5.70	Leco	g/100g DM ^a	20.8
Crude Fat	Soxhlet	g/100g DM	5.7
Polyunsaturated fatty acids	HPLC fatty acid	% of crude fat	66
Monounsaturated fatty acid	Spectrum	% of crude fat	18
Saturated fatty acid		% of crude fat	16
Total Dietary Fiber	Enzymatic gavimetric method ^b	g/100g DM	47.1
Water insoluble dietary fiber		g/100g DM	43.0
Water soluble dietary fiber		g/100g DM	4.1
Crude Ash	Ashing oven, 590°C	g/100g DM	11.3
Phosphorus		g/kg DM	25.4
Potassium		g/kg DM	22.5
Magnesium	Microwaves-Mineralization+AAS	g/kg DM	10.3
Calcium		mg/kg DM	930
Iron		mg/kg DM	260
Zinc		mg/kg DM	139
Sodium		mg/kg DM	21
Vitamins			
B1 (Thiamin)	Swiss Manual of Food analysis (2002)	$mg/100g\ DM$	1.4
B2 (Riboflavin)		$mg/100g\ DM$	0.2
B6 (Pyridoxine)		mg/100g DM	1.3
Niacin		$mg/100g\ DM$	32.9
Folic Acid		$mg/100g\ DM$	158
Pantothenic Acid		$mg/100g\ DM$	4.9
E (DL-α-Tocopherol-AC)		mg/100g DM	1.2
Phytic Acid (4,5,6-IP)	Egli (2001)	g/100g DM	8.4

^b AOAC method 991.43. ^c Adapted from Buri et al (2004)

2.1.2 Cell Walls of Cereal Grain

The mature cereal grain is composed of the characterized tissues. For example, through the growth period, the cell contents of pericarp-seed coat disappear and only thick cell walls remain. In the case of starchy endosperm, thin cell walls are dead and packed with starchy granules and storage protein. In contrast, the cells of the aleurone, which are alive, have thick bilayered walls (3-5µM) containing the protein and lipid-rich cell contents (Stone, 2006). The cell wall components and composition of various grain tissues are different and have a significant influence on the end uses of grains. According to the composition and structure of grain tissues, the grain show different milling behaviors, such as water uptake during conditioning step and grinding action during break and reduction step. Plant cell walls consist of two different types of cell walls, primary and secondary. Primary and secondary walls contain different proportions of cellulose, hemicellulose, and pectin (Figure 2.3). The cellulose fibrils are embedded in a network of hemicellulose and pectin.

Aleurone cell walls show unique and far less complex structures than any of the other plant cell walls that have been studied, in that such a large percentage of its structural polymer consist of arabinoxylans. McNeil and coworkers (1975) studied the barley aleurone cell wall and found that aleurone cell walls were composed predominantly of two polysaccharides, arabinoxylan and cellulose, and protein, at 85%, 8%, and 6%, respectively. It has been well known that the aleurone layer is a secretory tissue, although the intact aleurone cell walls function as a barrier to the mobilization of secreted enzymes (McNeil, et al. 1975). In 1976, Taiz and Honigman focused on the extensive aleurone cell wall degradation during the tissue's response to gibberellic acid and concluded that three arabinoxylan-degrading enzymes – endoxylanase, arabinosidase, and xylosidase – increased in total activity and were released into the medium, aleurone cell wall, in response to gibberellic acid. Of these enzymes, only endoxylanase would be expected to degrade the intact polymer. Most of the arabinoxylans in the aleurone cell walls consist of a linear xylan backbone substituted with single arabinofuranosyl residues. It is thought that strong noncovalent bonds exist between the arabinoxylan chains themselves, and between arabinoxylan chains and cellulose fiber, which make up the network in the cell walls. The cellulose fibers embedded in this network contribute to the strength of the cell wall, but the protein in the cell walls may not be a structural component.

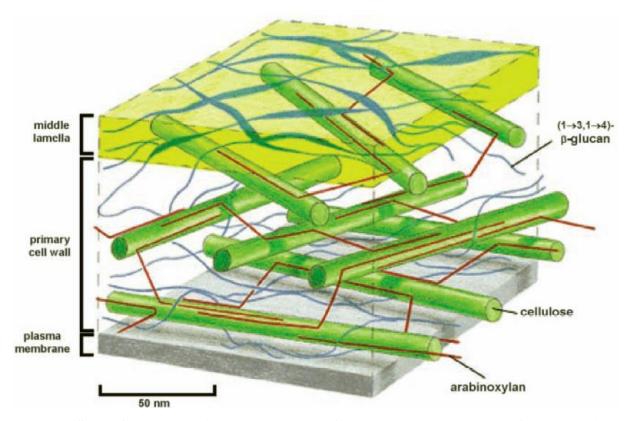


Figure 2.3 Simplified schematic representation of the spatial arrangement of polymers in a primary cereal wall of a cereal, e.g., the wall of starchy endosperm cell.

Primary cell walls are composed of cellulosic microfibrils and non-cellulosic matrix polysaccharides (hemicellulose: arabinoxylan, $(1\rightarrow 3,1\rightarrow 4)$ - β -glucan)or glucomannan). The cellulose fibrils are embedded in a network of hemicellulose and contribute to the strength of cell walls.

2.2. Enzymes

Enzymes have been used in food processes such as beer, wine, bread, and cheese making for centuries, and the history of enzyme uses must be longer than recorded history. In spite of its long history, most advances in enzymology and microbiology have only occurred during the past century, resulting in more progress in enzyme production and application. As the advantages in using enzymes in food processing started to gain attention, the commercial enzyme applications have grown from a relatively insignificant role to one of the most important aspects of food

processing during the past half of a century. How many enzymes may exist is unknown, but it is thought that there are 10,000 or more. (Underkofler, 1972)

2.2.1 Carbohydrases

Cellulases

Cellulases break down cellulose to beta-glucose.

Xylanases

Xylanases degrade the linear polysaccharide beta-1,4-xylan into xylose, thus breaking down hemicellulose, which is a major component of the cell wall of plants.

Pectinases

Pectinases break down the pectin to pectinic acid and finally pectic acid.

2.2.2. Factors affecting enzyme reactions

There are numerous factors affecting the enzyme action, and these factors should be considered for the enzyme applications.

Concentration of enzyme

For most enzymatic reactions the rate of the reaction is directly proportional to the concentration of enzyme, at least during the early stage of the reaction.

Concentration of substrate

The rate of enzyme reaction is proportional to the substrate concentration at very low substrate concentration. With an excess amount of substrate, the extent of enzyme reaction shows a linear relationship between the reaction time and the amount of product formed during the early stage of the reaction. As the enzymatic reactions proceed, the amounts of substrate decrease, which causes the reaction to slow down.

pH

pH has a significant influence on its activity due to the protein nature of enzymes. The optimum pH at which enzymes show the highest activity vary widely with the enzyme. Enzyme activities decrease rapidly above or below the optimum pH until the enzymes are completely

denatured and inactivated. Also, there is a pH range at which enzymes are most stable, which does not always coincide with the optimum pH.

Time

As mentioned above, the reaction rates slow down during the course of the enzymatic reaction due to many factors such as a reduction in the amount of substrate available or the inhibitive action of end products. Therefore, it is important in enzyme applications that sufficient time be allowed for the enzyme reactions to approach completion.

Temperature

Optimum temperature is another important factor affecting enzymatic reactions in two different ways. One effect is inactivation. Enzymes are denatured at high temperatures as well as at extremely low temperatures, losing their ability to catalyze reactions. The other effect is an acceleration of the reaction rate at high temperatures. Like most chemical reactions, the rate of an enzyme reaction increases with increasing temperature, up to a certain point, known as the optimum temperature. Moreover, it should be considered that even for a single enzyme reaction, the optimum temperature changes, depending upon the substrate concentration or incubation time. Also, the inactivation temperature varies, depending upon the particular enzyme.

Moisture content

The moisture content and circumstance in which enzymes are present has a profound effect on enzyme activity. In the presence of sufficient substrate, lack of moisture can inhibit enzyme reactions because all enzyme reactions occur in aqueous systems. There are soluble commercial enzymes which are stable in their dry powder state but start to react as soon as the enzymes are exposed to water.

2.2.3. Enzyme applications in food industry

Using enzymes in the baking industry

Amylases were the first enzymes to be added to bread dough. While initial use was for generating fermentable sugars, current interest centers on their ability to retard crumb firming, the anti-staling effect. During baking, between the gelatinization temperature and the enzyme denature temperature, amylases act on the damaged or gelatinized starch, producing dextrins,

oligosaccharides, and fermentable sugar. As a result, amylases in breadmaking increase gassing power and retard the crumb firming rate. There are three different sources of amylase used in breadmaking, cereal α -amylases, fungal α -amylases, and bacterial α -amylases. These α -amylases show different heat stabilities, which make differences in their functionality in breadmaking.

Proteases hydrolyze the peptide bond in proteins, being sometimes compared with reductants for their functionality in breadmaking. Exo-proteases increase the color and flavor of bread. Endo-proteases reduce the mixing time, fermentation time and elasticity. Especially, protease is used for mellowing strong flours. As a result, increased pan flow, finer grain, and softer texture may be obtained.

Endoxylanases with specificity towards water unextractable arabinoxylan (WU-AX) contribute to increased dough stability in two ways, by increasing the amount of WU-AX in dough on the one hand, and by increasing the amount of soluble arabinoxylan (AX) on the other hand (Figure 2.4). In addition to improvements in loaf volume, crumb structure, and crumb softness, the addition of optimal dosages of endoxylanases during breadmaking results in increased fermentation stability, resistance to mechanical stress, and greater oven rise. At higher enzyme dosages, slack doughs and dough stickiness after mixing become limiting parameters because of a loss in water holding capacity of the WU-AX.

Using enzymes in the milling industry

Enzyme supplementation is practiced both by addition to the flour at the mill and by the baker. It is well known fact that α -amylase preparations are added as a supplement to the flour at the end of milling. In addition to the addition of α -amylase in flour, enzyme application in milling have been studied to increase milling efficiency, i.e. improved quality of flour, higher product yield, and reduced milling steps, etc.

Previous studies (Haros et al 2002) reported that enzyme treated wheat, using such as cellulase, xylanase, and beta-glucanase during tempering, had a positive influence on improving the quality of the final products, especially bread, with respect to volume, crumb, and firming rate of bread. This enzyme pretreatment modified the initial structure of the wheat carbohydrates. The study suggested an alternative method to improve the final bread quality and overcome the enzyme distribution problem caused by nonuniform mixing and overdosage

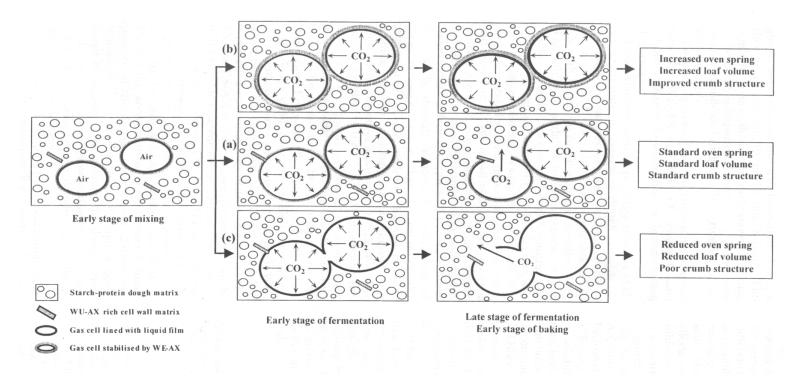


Figure 2.4 The mechanism behind endoxylanase functionality in breadmaking.

Model (a) represents the control situation with no endoxylanase added. There is little stabilization of liquid films by water extractable arabinoxylan (WE-AX) and a negative impact on gas cells of WU-AX. Model (b) represents the situation occurring when an endoxylanase with selectivity for WU-AX is added to the recipe. WU-AX are solubilized and the amount of WE-AX/ES-AX (enzymically solubilized arabinoxylan) increases. Coalescence between two gas cells is delayed. Model (c) represents the situation when an endoxylanase with selectivity for WE-AX is added to the recipe. WE-AX are extensively hydrolyzed, which results in decreased stabilization and increased coalescence of the gas cells compared to the control situation. The detrimental effect of WU-AX remains.

(adapted from Courtin and Delcour, 2002)

problems (slack and sticky dough) which occurred when enzymes were added directly to the flour or dough with other ingredients. However, the enzyme effect on bran separation from endosperm is unknown.

The use of commercial cellulases have been studied and well established. Hirao et al. (1963) studied starch recovery from cellulase enzyme pretreated cereals (rye, milo, corn, and barely) by the disintegration of the aleurone layer. Also, Takahaski et al. (1966) succeed in reducing the steeping time in corn wet milling by using cellulase. Al-Suaidy et al. (1973) studied the effect of cellulase treatment on wheat milling. It was considered that, as hemicellulase and cellulase hydrolyze the bran layer which is rich in cellulose and hemicellulose, the chemical composition of the bran layer might be modified. They could cause a change in the milling behavior and physical properties of the wheat kernel. From this study, it was found that, during cellulase treatment, the aleurone layer cells disintegrated as enzyme concentration increased. However, it was not enough to alter the milling properties. He suggested that it might be possible, through proper strain selection and better culture media, to produce a cellulase enzyme potent enough to cause such modification.

The effect of $(1\rightarrow 4)$ - β -endo-xylanase treatment on wheat bran was studied (Benamrouche et al., 2002). By using UV fluorescence microscopy, this study confirmed the degradation of the aleurone cell wall after $(1\rightarrow 4)$ - β -endo-xylanase treatment. After 24 h incubation, the aleurone layer was completely lost. However, the tissues in the outermost layer of the bran retained their integrity during xylanase treatment. They also reported that 80% and 51.8% of the total carbohydrate was liberated from the hydrolysis of aleurone and inner bran respectively, whereas no carbohydrate was released by $(1\rightarrow 4)$ - β -endo-xylanase treatment. Compared to the xylose/arabinose (X/A) ratios of aleurone layer, inner bran, and outer bran, which were 2.07 ± 0.06 , 2.93 ± 0.03 , and 0.79 ± 0.01 respectively, it was concluded that the degree of arabinose substitution (X/A) is one important factor for the high resistance of these polymers to endoxylanase degradation. For the exogenous enzyme, ferulates were thought to play an important role in modifying the mechanical properties of cell walls as well as in limiting polysaccharide degradation, functioning as a barrier to the hydrolytic enzymes by acting as cross-links between polysaccharides and between polysaccharides and lignin.

Saxena et al. (1993) examined the effect of enzymatic pretreatment on pigeon pea grain milling, and after that Arora et al. (2007) observed the optimum process parameters for the

milling of enzymatically pretreated rice. To obtain a higher quality of finished product (polished white rice), three process parameters (enzyme concentration, incubation time, and incubation temperature) were examined and optimized for developing an efficient milling system. The data was analyzed according to response surface methodology (RSM), showing that with enzymatic pretreatment, the rice bran layer softened up, being removed easily in the mechanical polisher. Cellulase used in the study acted on the bran layer and cell wall, helping break down the bran layer and cell wall structure. A lipase activated along with the cellulase degraded the oily outer bran layer, which functioned as a barrier to water penetration, leading to a reduction in the cooking time.

Synergism

Enzymes have degree of specificity to their substrates, and through various studies it has been found that they often have synergistic effects when used together in a system which is a complex of different kinds of polymers. In 1998, Zheng and Bhatty applied an enzyme cocktail containing cellulase, endo- $(1\rightarrow 3)$, $(1\rightarrow 4)$ - β -D-glucanase and xylanase in the wet separation of starch, extracting a higher yield of starch from hullless barley, as compared with the conventional procedure. In 1991, Steinke and Johnson reported that incorporating multiple enzymes in steeping solutions reduced steeping time and enhanced starch separation during wet-milling of maize. Padmanabhan et al. (1993) reported a significant improvement in starch recovery from cassava by using pectinase and cellulase. Petit-Benvegnen et al. (1998) showed the synergistic enzyme effect of endoxylanase and ferulate esterase on cell wall degradation. As the endoxylanase was used with ferulate esterase, the elimination of some of the ferulic acids improved the accessibility and binding of endoxylanase on the arabinoxylans.

Hille and Schooneveld-Bergmans (2004) examined the synergistic effect of fungal and bacterial endoxylanases in breadmaking. The volume of final products with much less of the combination of these enzymes was similar to those with higher amounts of a single enzyme. Another type of synergy resulted from the addition of cellulase and/or cellobiohydrolyase to the fungal and bacterial endoxylanase. Cellulases open and break down the cellulose which is intertwined with the arabinoxylan polymer, helping the endoxylanase activity. This synergistic effect had a positive influence on bread volume and crumb softness as well.

2.3. Wheat Milling

2.3.1. Processes Affecting the Milling Efficiency

Every step, from planting the seeds to harvesting, and each step of the milling process, represent important factors affecting milling efficiency. Here, conditioning and pretreatments such as debranning, soaking, freezing, and drying of wheat will be considered.

Conditioning (tempering)

Optimum moisture contents for wheat milling vary widely, depending upon whether the wheat is hard or soft, with hard wheat generally conditioned to 15.5 to 17% moisture content and soft wheat to 14 to 15.5% moisture content. To obtain a high yield and high flour quality, tempering (resting) times also range from 12 to 24 hours, depending on the wheat variety and tempered wheat moisture content. Butcher and Stenvert (1973) defined the flour yield related to the resting time and tempered wheat moisture content for various kinds of wheat. After this study, they also reported that a peak in flour yield did not correspond to the moment when the moisture was completely distributed across the wheat kernel. To achieve optimum milling performance, a certain well defined radial moisture gradient across the grain was required, with the periphery being at a higher moisture level than the center of the grain (Butcher and Stenvert, 1973). Lee and Stenvert (1973) pointed out factors affecting the water penetration during the conditioning, such as hydrophilic pentosan content (arabinoxylans), thickness, and physical nature of the bran. They confirmed that the degree of branching (in this study, it was presumed that the ratio of arabinose/xylose reflect differences in branching) in the bran arabinoxylan is of considerable importance in determining the water penetration, in that the rate of water penetration of hard wheat was slower than that for soft wheat.

Pretreatments

There have been various efforts to increase milling efficiency by changing the physical or chemical properties of the wheat kernel before milling. Fisher and Hines (1939) stated that wetting and drying made the wheat swell and created cracks or enlarged preexisting cracks. Similarly, Grosh and Milner (1959) suggested that wetting created stresses due to the moisture difference between the wet and dry portions, which induced the cracks. This cracks served as a

water penetration pathway across the wheat kernel. In 1941, Swanson studied the effects of wetting and drying of mature wheat on the grinding and milling quality. As a result, he observed that kernel test weight and vitreousness were changed but that flour yield and baking quality were not changed. Watson et al. (1967) reported that wheat which underwent weather changes, repeated rain, snow and freezing, during the harvest season showed high milling and baking quality. Adams and Naber (1971) found water soaking improved the nutritive value of wheat for poultry. In 1973, Al-Suaidy et al. reported that softening hard wheat by soaking and drying may be economical, since milling hard wheat required more power and caused more roll repair and sieve replacements than did milling soft wheat (Greenaway, 1962).

From the several studies on the effects of bran on flour quality, it is evident that debranning might improve flour refining, increasing its milling yield in parallel. The Satake Company invented a flour milling pretreatment process which consists of 3 steps of polishing followed by adding water at the last step. They reported that through 3 polishing steps, the pericarp, seed coat, and aleurone layer cell walls were removed and the internal aleurone cell content would be washed out by adding water to raw wheat grains (U.S patent 5,846,591). Pandiella et al. (2004) studied the debranning effect on cereal food quality and reported that the use of debranning technology in flour milling could produce a nutritious flour including the aleurone part, or at the same time the isolated aleurone fraction could be used as a functional ingredient for the production of enhanced value cereal based foods.

Based on the literature review, it appears that the application of enzyme in temper water before wheat milling might have some beneficial effects. This study was planned to determine 1) the parameters which affect enzymatic reactions on probable enhancement of bran separation and 2) the effect of enzyme application in temper water on wheat milling. These parameters were optimized to develop a protocol for the application of enzymes in the temper water, and conditions during tempering. Also, the effects of enzymatic tempering on bran separation during the milling process were studied as compared with the conventional (control) process. A wheat bran fraction was first used to determine if the enzymes work on bran and, if so, to establish the appropriate conditions such as different enzyme concentrations, incubation temperature, and incubation time which enzymes were likely to enhance bran separation during milling if enzymes were used in the tempering water. After milling, test baking using the flour milled from the

enzymatic tempered wheat was conducted in order to see if the enzyme treatment in temper water had the effects on the bread making and bread staling.

CHAPTER 3 - Enzyme Activity on Wheat Bran

Prior to the application of enzymes to intact wheat kernels, enzymes were applied to wheat bran to observe if there was a hydrolyzing effect on wheat bran, and if so, what effects the enzymes have.

3.1 Materials and Methods

Enzymes

Cellulases, xylanases, and pectinases were obtained from Specialty Enzymes and Biochemicals Co. (CA, U.S.). According to the specification sheet provided by the supplier, each of the enzymes showed different optimum conditions for their activity (Table 3.1). Each enzyme and the combination of cellulase and xylanase were applied to wheat bran in the stipulated amount.

Table 3.1 Summary of Commercial Enzyme Characteristics Supplied by the Manufacturer^a

Properties	Cellulase	Xylanase	Pectinase ^b
Appearance	Off white/ light tan powder	Light tan powder	Liquid
Solubility	Soluble in water	Soluble in water	Soluble in water
Activity	5000 CU/gm	5000 units/gm	2335 PGU/ml
Moisture	Not more than 0.7%	-	-
E.Coli	Negative	Negative	-
Salmonella	Negative	Negative	-
TPC	Less than 3000 CFU/gm	Less than 3000 CFU/gm	-
Opt. pH	5.5-6.0	4.0-6.5	3.5-6.0
Opt. Temp.	37-40 °C	55-60 °C	40-55 °C

^a Specialty Enzymes and Biochemicals Co. (2006)

^b In addition to the pectinase enzyme, it contains traces of cellulase, hemicellulase, and protease activities

Wheat bran

A blended hard red winter wheat from a local elevator near Manhattan, KS was milled in the KSU Grain Science and Industry department's in-house pilot flour mill. The resulting bran was obtained and stored in double plastic bags at 4°C until needed. The proximate analysis of wheat bran, on a dry basis, was: starch 19.7%, protein 20.9%, fibrous carbohydrate 45.4% (cellulose and hemicelluloses), lignin 3.5%, fat 3.2%, and ash 7.2%. This wheat bran was used to determine the enzyme activities and optimum conditions prior to application on wheat kernels.

Enzyme treatment of wheat bran

One hundred grams of wheat bran and 16 g of water with enzyme or water without enzyme were blended for 10 minutes in the tempering drum. Enzymes were added at stipulated concentrations (w/w = enzyme weight/tempering water weight). Treated wheat bran samples were transferred to a polyethylene sample bag and kept in an oven or under room conditions for the stipulated temperatures and times. Five g of wheat bran were then blended with 75mL of water, and centrifuged at 3,000 x g for 10 min at room temperature. The decantate was analyzed for carbohydrate reducing ends (monomer and polymer carbohydrates released by enzyme hydrolysis) with the dinitrosalicylic acid (DNS) procedure as described below. Enzyme treated bran was dried and used for scanning electro microscopy (SEM) (Model S-3500N, Hitachi Science Systems, Japan) to compare with the intact wheat bran.

Reducing sugar assay

The effect of enzymes on bran and their activities was related to reducing-end sugar determination for monomers and polysaccharides by the 3,5 dinitrosalicylic acid assay as described by Miller (1959), but volumetrically modified to a total of 1.5 mL reactant. Dextrose was used as a standard.

Experimental design

Response surface methodology is an incomplete block experimental design that fits a second order multiple regression equation to the data. The principle advantages are that it accounts for non-linear effects (most of nature is non-linear) and checks for interactions, and it can predict data for combinations not actually tested, provide three dimensional contour plots, and most importantly it can substantially reduce the number of experimental runs required. Once

the identified "vital few" controllable factors are decided upon, with suitable software or graphical means, it is even possible to find the 'best' combination for all variables in concert (Walker, 2002).

The experiment was conducted according to the requirement of response surface methodology (RSM) for analyzing data regarding the optimum conditions for enzyme activities. A second order Box-Behnken design was conducted with 3 levels, high, medium, and low, for 3 treatments factors, enzyme concentration, incubation time, and incubation temperature (Table 3.2 and 3.3). The results were analyzed and plotted by software, RSM Plus (AEW consulting, version date: 1992) using the model, STD 3_VAR.

Table 3.2 Response Surface Methodology (RSM) design

	Х	У	Z	
1	+1	+1	0	
2	+1	-1	0	
3	-1	+1	0	
3 4 5	-1	-1	0	
5	+1	0	+1	
6	+1	0	-1	
7	-1	0	+1	
8	-1	0	-1	
<u>8</u> 9	0	+1	+1	
10	0	+1	-1	
1 1	0	-1	+1	
12	0	-1	-1	
13	0	0	0	
14	0	0	0	
15	0	0	0	

Random order for center points. Replicates were fixed.

Table 3.3 Variables and levels

		-1	0	+1
Х	enzyme concentration (%) (w/w)	0%	0.75%	1.5%
У	incubation Temp (°C).	25 C	45 C	60 C
Z	incubation time (hr)	1 h	4 h	16 h

3.2 Results and Discussions

Reducing sugar assay results are shown in Figure 3.1, 3.2, 3.3, and 3.4 for cellulase, xylanase, pectinase, and the combination of cellulase and xylanase treatment, respectively. The data were analyzed and plotted by the software, RSM Plus. This graph is made of alphabetical letters; and each letter corresponds to the released reducing sugar concentration in the supernatant. These results show a hydrolysing effect of enzymes on wheat bran. The left side and right side graph presented the released reducing sugar concentration at 0 hour and 16 hours incubation time, respectively. The X-axis is enzyme concentration and Y-axis is incubation temperature.

The coefficients of determination (R²) were 0.9925, 0.9168, 0.9640, and 0.9768 for cellulase, xylanase, pectinase, and the combination enzyme, which means that the model fits the data for enzyme activity very well for all three treatments, enzyme concentration, incubation time, and incubation temperature. From the results, as time and concentration of enzyme increased, the released sugar in the supernatant increased for the three enzymes and the combination of xylanase and cellulase. Within the range of experimental treatments, cellulase, pectinase, and the combination of cellulase and xylanase all show higher activities at the higher temperature and enzyme concentration for longer incubation time. However, although we expected that xylanase would be more active at high temperature, the predicted response surface for the released reducing sugar concentration by xylanase appeared to be a bowl shape with a minimum sugar release at about 0.677% enzyme and 40 °C; and the highest released reducing sugar concentration was observed at two different temperature ranges, high and room temperature, when the same amounts of enzyme were applied on the bran.

Equations (1), (2), (3), and (4) shown below were obtained from the RSM Plus program for the activities of cellulase, xylanase, pectinase, and the combination of xylanase and cellulase respectively, to predict the released sugar concentration. These equations indicated the relation between the individual treatments, and interactions between treatments and released sugar concentration.

Equation (1) for cellulase:

Released sugar, S = 11.4158376 - 1.4923129E - 0.2211565T + 0.7071543t - 0.0608220ET - 0.0019356Tt + 0.0738555Et + 2.8650230E² + 0.0033280T² - 0.0189655t²

Where E = enzyme concentration (%),

t = incubation time (hr), and

T= incubation temperature (°C)

Equation (2) for xylanase:

 $Released \ sugar, \ S = 5.0668739 + 0.4954408E + 0.0860984T + 0.3080767t + 0.0202577ET + 0.0082901Tt - 0.0176452Et - 0.3651399E^2 - 0.0012739T^2 - 0.0222804t^2$

Equation (3) for pectinase:

 $Released \ sugar, \ S = 8.3926584 + 0.1926668E + 0.0285524T + 0.0049771t + 0.0037312ET + 0.0076526Tt + 0.0050051Et + 0.1996072E^2 - 0.0002917T^2 - 0.0112482t^2$

Equation (4) for the combination of xylanase and cellulase:

 $Released \ sugar, \ S = 7.9475436 + 1.4723567E - 0.0917968T + 0.1359924t - 0.0335219ET + 0.0130425Tt + 0.0310216Et + 0.7490712E^2 + 0.0013247T^2 - 0.0227563t^2$

It was found that enzyme concentration and incubation time had the most effect on the released sugar concentration for the cellulase, xylanase, and their enzyme cocktail activities. Unlike cellulase and xylanase, when pectinase was used, the incubation temperature effected the released sugar concentrations slightly more than the incubation time did. When the same amounts of enzyme (1.5% w/w) were used for the bran hydrolysis, the amount of released sugar measured 13.76 mmol for the cellulase, 15.94 mmol for the xylanase, 13.97mmol for the pectinase, and 16.67mmol for the combination of xylanase and cellulase. The combination of two enzymes, cellulase and xylanase, showed a synergistic effect on hydrolyzing the bran fraction slightly, which implies a possible synergistic effect of an enzyme cocktail including all three enzymes, xylanase, cellulase, and pectinase.

Scanning electro microscopy (SEM) showed an interesting picture of the bran fraction (Figure 3.5). The intact bran layer was covered with starch granules and aleurone cell walls.

However, after enzyme treatment, the starch granules might have been washed off and the inner aleurone cell walls were revealed. The aleurone cell contents were released due to the rupture of aleurone cell walls.

It was confirmed that the carbohydrases, xylanase, cellulase, and pectinase, had an effect on hydrolyzing the bran layers, resulting in releasing some of the aleurone cell content. Although higher enzyme concentrations, longer incubation times, and higher incubation temperatures helped the enzyme to act on the bran layer, the usage level of enzyme, incubation time, and temperature should be considered in terms of the economic aspect. It is suggested that the use of an enzyme cocktail consisting of cellulase, xylanase, and pectinase, combined for their synergistic effect, be considered. Also, other conditions influencing enzyme activity which were not tested in this study, such as pH and substrate moisture content, should be examined to optimize the effect of enzyme activities.

====== Response in SUGAR Response in SUGAR (Stepping Variable: TIME = 0) (Stepping Variable: TIME = 16) BBBBBBBBBBB +60.000 | AAAAAAAAAAAAAA +60.000 |II JJJJJJJJJ +59.000 | AAAAAAAAAA REFERENCE CCCCCC +58.000 AAAAAAAAA BBBBBBBBBBB cccccccc +59.000 |III JJJJJJJJJJJ KKKKKKKKKKKKKKKKKKKK +58.000 | IIII JJJJJJJJJJ KKKKKKKKKKKKKKK +57.000 | AAAAAAAAA BBBBBBBBBBB CCCCCCCCC +56.000 | AAAAAAAA BBBBBBBBBBB cccccccccc +57.000 | IIIIII JJJJJJJJJJJ BBBBBBBBBB +56.000 | IIIIIII JJJJJJJJJJJJJ +55.000 | AAAAAAA CCCCCCCCCCCCCC TATATATATATATATATATATA +55.000 | IIIIIIIII +54.000 | AAAAAA BBBBBBBBBB cccccccccccc +53.000 AAAAA +54.000 IIIIIIII BBBBBBBBBBB CCCCCCCCCCCCCCCC +53.000 IIIIIIIII JJJJJJJJJJJJJJJJJJJJJJJJJJJJJJJJJJ +52.000 | AAAAA BBBBBBBBBBB cccccccccccccc +51.000 AAAA BBBBBBBBBB cccccccccccccc +52.000 IIIIIIIIII JJJJJJJJJJJJJJJJJJJJJJJJJJJJJ +51.000 IIIIIIIIIII +50.000 | AAA BBBBBBBBBBB cccccccccccccc +50.000 +49.000 AA BBBBBBBBBBB ccccccccccccccc IIIIIIIIIIII +49.000 IIIIIIIIIIIIII +48.000 A BBBBBBBBBBB ccccccccccccccc IIIIIIIIIIIIIIIIIIIIIIII +48.000 | HHHH +47.000 |A BBBBBBBBBBBB cccccccccccccc +47.000 НННННН +46.000 BBBBBBBBBBB cccccccccccc +46.000 нинининин +45.000 BBBBBBBBBBBB CCCCCCCCCC +45.000 нининининин +44.000 BBBBBBBBBBB IIIIIIIII +43.000 +44.000 нининининин BBBBBBBBBBBB +43.000 нинининининин +42.000 BBBBBBBBBBB +42.000 +41.000 BBBBBBBBBBBB +41.000 нинининининининининининининининининини +40.000 BBBBBBBBBBBB нинининининининининининини +40.000 т Leggeg +39.000 BBBBBBBBBBBB +39.000 GGGGGGGG +38.000 BBBBBBBBBBBBBBB +38.000 GGGGGGGGGGG GGGGGG +37.000 BRRRRRRRRRRRRR +36.000 BBBBBBBBBBBBBBB +37.000 GGGGGGGGGGGGGG GGGGGGGGGGGGG +36.000 +35.000 BBBBBBBBBBBBBBBB +35.000 +34.000 BBBBBBBBBBBBBBBBB GGGGGGGGGGGGGGGGGGGGGG +34.000 +33.000 REFERENCES RRRRRRRRRR +33.000 FFFFFFFF 4444444 +32.000 BRRRRRRRRRRRRR +31.000 +32.000 FFFFFFFFFFFFFFF FFFFFFFFFFFFFFFFFF +31.000 +30.000 +29.000 +30.000 +29.000 EEEEEEE +28 000 REFERENCES DE LA COMPTE DEL COMPTE DE LA COMPTE DEL COMPTE DE LA COMPTE DEL COMPTE DE LA COMPTE DEL COMPTE DE LA COMPTE DEL +28.000 EEEEE EEEEEEEEEEE +27.000 +27.000 EEEEEEEEEEEE EEEEEEEEEEEEEEE +26.000 +26.000 EEEEEEEEEEEEEEEEEEEEEEEE +25.000 REFERENCES DE LA CONTRACTION DEL CONTRACTION DE LA CONTRACTION DE L +25.000 ממממממ +24.000 +24.000 DDDDDDDDDDDDD +23.000 BBBBBBBBBBBB AAAA +22.000 AAAAAA +23.000 ממממ | DDDDDDDDDDDDDDDDDDD +22.000 CCC +21.000 A AAAAAAAAAA +21.000 DDDDDDDDDDDDDDDDDDDDDDDDDDDDDDDDD cccccccc +20.000 | AAA AAAAAAAAAAAA +20.000 CCCCCCCCCCCC +0.333 +0.667 +1.000 +1.333 +1.667 +2.000 +0.000 +0.333 +0.667 +1.000 +1.333 +1.667 +2.000 ENZYME ENZYME Legend: +6.00=A +6.80=B +7.60=C +8.40=D +9.20=E +6 00=A +6.80=B +7.60=C +8.40=D Legend: +10.00=F +10.80=G +11.60=H +12.40=I +13.20=J +10.00=F +10.80=G +11.60=H +12.40=I +13 20=J +14.00=K+14.00=K

020CT06

Figure 3.1 RSM plots for cellulase activity. 0 hour incubation (left) and 16 hours incubation (right)

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-----Response in SUGAR Response in SUGAR (Stepping Variable: TIME = 0) (Stepping Variable: TIME = 16) +60.000 | GGGG 444444444 GGGGG +60.000 JJJJ IIIIIIIIIIIII JJJJJJ KKKKKKKKKK +59.000 FFFFFFF 4444444 GGGGG +59.000 IIIIIIIIIIIIIIII JJJJJJ KKKKKKKKKK +58.000 GG FFFFFFF FFFFFFFF GGGG +58.000 IIIIIIIIIIIIIIIIIIIIII KKKKKKKKKK JJJJJJ +57.000 FFFFFFFF FFFFFFFF GGGGG +57.000 IIIIIIIIIIIIIIIIIIIIIIIIIII JJJJJJ KKKKKKKKKK +56.000 FFFFFFF FFFFFFF GGGGG +56.000 IIIIIIIIIIIIIIIIIIIIIIIIIIIIII JJJJJ KKKKKKKKKK +55.000 9999999 444444 GGGG +55.000 IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII JJJJJ KKKKKKKKK +54.000 EEEE FFFFFFF GGGG +54.000 JJJJJ KKKKKKKKK +53.000 EEEEEEEEE प्रवयवय वयप्रवय GGGG +53.000 JJJJJ KKKKKKKKK +52.000 EEEEEEEEEEEE FFFFFF GGGG +52.000 TTTTTTTTTTTT IIIIIIIIIII JJJJJ KKKKKKKKK +51.000 EEEEEEEEEEEEE FFFFFF GGGG +51.000 IIIIIIIIII IIIIIIIIII JJJJJ KKKKKKKKK +50 000 REFERENCE ERREFERE मयमयमय ययप्रयम्ब GGGG +50.000 TTTTTTTTT TTTTTTTTT JJJJJ KKKKKKKKKK +49.000 EEEEEEEEEEEEEEEE +49.000 | IIIIIIIIII IIIIIIIII JJJJJ KKKKKKKKKK +48.000 REFEREREFEREEREFEER नप्रप्रप्र GGGG +48.000 | IIIIIIII IIIIIIII JJJJJ KKKKKKKKKK +47.000 EEEEEEEEEEEEEEEEE FFFFFF GGGG +47.000 | IIIIIIII JJJJJ IIIIIIII KKKKKKKKKK +46.000 EEEEEEEEEEEEEEEEEE +46.000 IIIIIIII JJJJJ +45.000 EFFEREREFFEREFFEREFFERE GGGG +45.000 İTTTTTT TTTTTTTT JJJJJJ KKKKKKKKKK +44.000 EEEEEEEEEEEEEEEEE GGGG +44.000 | IIIIII IIIIIIII JJJJ KKKKKKKKKKK +43.000 EEEEEEEEEEEEEEEEEE FFFFF GGGG +43.000 ITTTTTT IIIIIIII JJJJJJ KKKKKKKKKKK +42.000 EEEEEEEEEEEEEEEEEE FFFFF GGGG +42.000 IIIII IIIIIIII JJJJJ KKKKKKKKKKK +41.000 EEEEEEEEEEEEEEEEE FFFFF GGGG +41.000 | IIIII IIIIIIII JJJJ +40.000 FFFFFF GGGG +40.000 | IIIII IIIIIIII JJJJJ KKKKKKKKKKKK +39.000 EEEEEEEEEEEEEEEEE +39.000 IIIIIIII JJJJJ KKKKKKKKKKKK +38.000 EEEEEEEEEEEEEEEEE FFFFF GGGG Η +38.000 IIIII IIIIIIII JJJJJ KKKKKKKKKKKKK +37.000 EEEEEEEEEEEEEEEE FFFFFF GGGG НН +37.000 | IIIII IIIIIIIII JJJJJ KKKKKKKKKKKKK +36.000 EEEEEEEEEEEEEEEEE FFFFF GGGG НН +36.000 IIIIII IIIIIIIII JJJJJ KKKKKKKKKKKKKK +35.000 FFFFFF GGGG ннн +35.000 IIIIII IIIIIIIIII JJJJJ KKKKKKKKKKKKKK +34.000 EEEEEEEEEEEEEEEE GGG ннн +34.000 | IIIIIII IIIIIIIIII KKKKKKKKKKKKKKK JJJJJ +33.000 GGGG REFERENCE REFERENCE REFERENCE 97777 нннн JJJJJ +33.000 | IIIIIIIII IIIIIIIIIII KKKKKKKKKKKKKKK +32.000 EEEEEEEEEEEEEEEEE FFFFF GGG HHH +32.000 JJJJJ KKKKKKKKKKKKKKK +31.000 EEEEEEEEEEEEEEE FFFFF GGGG нннн JJJJJ KKKKKKKKKKKKKKKK GGGG +30.000 REFERENCE ERREFERE ннн 999999 +30.000 | IIIIIIIIIIIIIIIIIIIIIIIII JJJJJ KKKKKKKKKKKKKKKK +29.000 EEEEEEEEEEEEEEEE нннн JJJJJ KKKKKKKKKKKKKKKKK +28 000 REFERENCE ERRECTE प्रवयप्रवय GGGG ннн +28.000 JJJJJJ KKKKKKKKKKKKKKKKKK +27.000 EEEEEEEEEEEEE FFFFFFF GGGG HHH +27.000 | IIIIIIIIIIIIIIIIIII JJJJJJ KKKKKKKKKKKKKKKKKK +26.000 EEEEEEEEE 444444 GGGG нннн +26.000 IIIIIIIIIIIIIIIII JJJJJJ +25.000 REFERE FFFFFFF GGGG ннн TT +25.000 IIIIIIIIIIIIII JJJJJJ KKKKKKKKKKKKKKKKKKK +24.000 ННН GGGG ΙI +24.000 IIIIIIIIII JJJJJJJ +23.000 FFFFFFF GGGG нннн III +23 000 JJJJJJJ KKKKKKKKKKKKKKKKKKKKKK +22.000 GGGGG нннн +22.000 JJJJJJJ +21.000 FFF FFFFFFFF GGGGG ннн III +21.000 JJJJJJJJ KKKKKKKKKKKKKKKKKKKKKKKK +20.000 FFFFF FFFFFFFF GGGGG HHH III +20.000 JJJJJJJJ +0.667 +1.667 +0.000 +0.333 +1.000 +1.333 +2.000 +0.000 +0.333 +0.667 +1.000 +1.333 +1.667 +2.000 ENZYME ENZYME Legend: +0.00=A+1.60=B +3.20=C +4.80 = D+6.40=E +4.80=D +0.00 = A+1.60=B +3.20=C +6.40=E Legend: +8.00=F +9.60=G +11.20 = H+12.80=I +14.40=J +8.00=F +12.80=I +14.40=J +9.60=G +11.20 = H+16.00=K

26SEP06I

Figure 3.2 RSM plots for xylanase. 0 hour incubation (left) and 16 hours incubation (right)

26SEP06I

090CT06 090CT06 ====== ====== Response in SUGAR (Stepping Variable: TIME = 0) Response in SUGAR (Stepping Variable: TIME = 16) +60.000 ccccccccccc DDDDDDDDDD EEEEEEE +60.000 JJJJJJ +59.000 CCCCCCCCCCCCCCC DDDDDDDDDDD REFEREE +59.000 JJJJJJJJJJJ +58.000 cccccccccccc DDDDDDDDDD EEEEEEE +58.000 JJJJJJJJJJJJJ +57.000 cccccccccccc DDDDDDDDDD EEEEEEE +57.000 JJJJJJJJJJJJ +56.000 ccccccccccc DDDDDDDDDD EEEEEEE +56 000 JJJJJJJJJJJ KKKKKKKKKKKKKKKKKKKKKK +55.000 cccccccccccc DDDDDDDDDD EEEEEEE +55.000 IIIII JJJJJJJJJJJ +54.000 cccccccccccc ממממממממ +53.000 cccccccccccc DDDDDDDDDD EEEEEE +54 000 TTTTTTTTTTT JJJJJJJJJJJ KKKKKKKKKKKKKKK +53.000 IIIIIIIIIIIII JJJJJJJJJ KKKKKKKKKKKKK +52.000 cccccccccccc DDDDDDDDDD EEEEEE +52.000 IIIIIIIIIIII JJJJJJJJJJ KKKKKKKKK +51.000 cccccccccccc DDDDDDDDDD EEEEEE +51.000 IIIIIIIIIII JJJJJJJJJ KKKKKK +50.000 cccccccccccc DDDDDDDDDD EEEEEE +50.000 ннннн TTTTTTTTT JJJJJJJJJJ KKK +49.000 cccccccccccc DDDDDDDDDD EEEEEE +49.000 нинининини IIIIIIIIII JJJJJJJJ +48.000 cccccccccccc DDDDDDDDDD EEEEEE +48.000 IIIIIIIII +47.000 cccccccccccc DDDDDDDDDD EEEEE +47.000 нининининин IIIIIIIII JJJJJJJ +46.000 ccccccccccccc מממממממממ REFER +46.000 +45.000 cccccccccccc DDDDDDDDDD +45.000 GGGGGGG нинининини IIIIIIII +44.000 EEEEE CCCCCCCCCCCCCCCC DDDDDDDDD +44.000 нинининини +43.000 cccccccccccc ממממממממ +43.000 GGGGGGGGGGGG нинининин IIIIIIII +42.000 ccccccccccccc ממממממממ EEEE +42.000 GGGGGGGGGGGG нининини +41.000 ccccccccccccc DDDDDDDDDD +41.000 GGGGGGGGGG нининини +40.000 REEE CCCCCCCCCCCCCCC DDDDDDDDDD +40.000 FFFFFFFF GGGGGGGGGG нининини +39.000 cccccccccccc +39.000 GGGGGGGGGG +38.000 מממממממממ SEE CCCCCCCCCCCCCCCC +38.000 FFFFFFFFFFFFFF нининини GGGGGGGGG +37.000 cccccccccccc DDDDDDDDDD +37.000 GGGGGGGG +36.000 CCCCCCCCCCCCCCCC מממממממממ +36.000 REFE GGGGGGGG +35.000 cccccccccccc DDDDDDDDDD +35.000 EEEEEEEEEE +34.000 cccccccccccc DDDDDDDDDD E +34.000 EEEEEEEEEEEEE FFFFFFFFF GGGGGGG +33.000 cccccccccccc DDDDDDDDDD +33.000 EEEEEEEEEEE FFFFFFFF GGGGGG +32.000 cccccccccccc DDDDDDDDDD +32.000 EEEEEEEEEE +31.000 DDDDDDDDDDD +31.000 מממממממ REFERENCES 4444444 +30.000 cccccccccccc DDDDDDDDDD +30.000 DDDDDDDDDDDDDD EEEEEEEEE +29.000 cccccccccccc DDDDDDDDDD +29.000 DDDDDDDDDDDDDDDDDD REFERENCE 444444 +28.000 ccccccccccc DDDDDDDDD +28.000 DDDDDDDDDDDDD EEEEEEEE +27.000 ccccccccccc DDDDDDDDDD +27.000 EEEEEEEE DDDDDDDDDDDDD CCCC +26.000 cccccccccccc DDDDDDDDD +26.000 cccccccccc DDDDDDDDDDD EEEEEEE +25.000 cccccccccccc DDDDDDDDDD +25.000 DDDDDDDDDDD +24.000 +24.000 cccccccccccc DDDDDDDDD +23.000 B CCCCCCCCCCCCCC ממממממממ +23.000 cccccccccc +22.000 ВВВ cccccccccccc DDDDDDDDD +22.000 BBBBBBBBBB CCCCCCCCCCC DDDDDDDDD +21.000 BBBB DDDDDDDDDD +21.000 CCCCCCCCCC +20.000 BRRRRR ממממממממ +20 000 מממממ CCCCCCCCCC +0.333 +1.333 +1.000 +0.000 +0.333 +1.000 +1.333 +1.667 +0.667 ENZYME ENZYME Legend: +8.00=A+8.60=B +9.20=C +9.80=D +10.40=E

Figure 3.3 RSM plots for pectinase activity. 0 hour incubation (left) and 16 hours incubation (right)

+13.40=J

+12.80=I

+11.00=F

+14.00=K

+11.60=G

+12.20=H

+8.00=A

+11.00=F

+14.00=K

+8.60=B

+11.60=G

+9.20=C

+12.20=H

+9.80=D

+12.80=I

+10.40=E

+13.40=J

040CT06 040CT06 ====== ====== Response in CON. Response in CON. (Stepping Variable: TIME = 16) (Stepping Variable: TIME = 0) +60.000 | IIIIIIIIIIIII JJJJJJJJJJ KKKKKKKKKKK +60.000 |B CCCCCCC +59.000 JJJJJJJJJ KKKKKKKK +59.000 BBBBBBBBBBBBBBBBB ccccccc +58.000 IIIIIIIIIIIIIIIII KKKKKK JJJJJJJJ +58.000 BRRRRRRRRRRRRRRRRR ccccccc +57.000 TTTTTTTTTTTTT JJJJJJJJ KKK +57.000 BBBBBBBBBBBBBBBB CCCCCCC +56.000 IIIIIIIIII JJJJJJJ +56.000 BBBBBBBBBBBBBBB CCCCCCCC +55.000 ннининининини IIIIIIIII JJJJJJJ +55.000 BBBBBBBBBBBBBB CCCCCCC нининининининининин +54.000 TTTTTTTT JJJJJJJ +54.000 CCCCCC +53.000 нинининининин IIIIIIII JJJJJJ +53.000 BRRRRRRRRRRRR CCCCCC +52.000 нининининини IIIIIII JJJJJ +52.000 BBBBBBBBBBBB cccccc +51.000 нинининин IIIIIII JJJ BBBBBBBBBBRRR CCCCCCC +51 000 +50.000 GGGGGGGGGGGG нининини IIIIII +50.000 BERREBERRER ccccccc +49.000 GGGGGGGGGGGGGGG нининини IIIIII +49.000 BBBBBBBBBBBB cccccc +48.000 GGGGGGGGGGG нининин IIIIII +48.000 AAAAAA BBBBBBBBBBB +47.000 GGGGGGGGGG IIIIII +47.000 | AAAAAAAAA cccccc +46.000 FFFFFFF GGGGGGGGG нининин TTTTT +46.000 AAAAAAAAAA CCCCCCC BRRRRRRRRR +45.000 FFFFFFFFFFFF GGGGGGGGG IIIII +45.000 AAAAAAAAAA BBBBBBBBBB CCCCCC +44.000 FFFFFFFFFFFFFFFFF GGGGGGG нинини TTT +44.000 AAAAAAAAAAAA BBBBBBBBBB CCCCCCC +43.000 FFFFFFFFFFFF GGGGGG +43.000 AAAAAAAAAAAA REFERENCE cccccc +42.000 GGGGGGG нннннн FFFFFFFFFFF +42.000 AAAAAAAAAAAA BBBBBBBBBB cccccc +41.000 FFFFFFFFF GGGGGG ннннн +41.000 BBBBBBBBBB cccccc +40 000 GGGGGG нинини REFERENCE 4444444 +40.000 AAAAAAAAAAAAA BBBBBBBBB cccccc +39.000 EEEEEEEEEEEEE ннннн +39.000 АААААААААААА BBBBBBBBB ccccc +38.000 REFERENCEERE GGGGGG ннннн 444444 +38.000 AAAAAAAAAAAA BBBBBBBBBB CCCCCC +37.000 EEEEEEEEEE нннн +37.000 AAAAAAAAAAA CCCCCC DD +36 000 EFFFFFFFFF GGGGGG प्रवयवयय нн +36 000 Ιαααααααααααα REFERENCE CCCCCCC DD +35.000 DDDDDDD EEEEEEEE +35.000 AAAAAAAAAAA BBBBBBBBBB CCCCCC DDD +34 000 DDDDDDDDDDD EEEEEEEE ਸ਼ਬਸਬਸ਼ GGGGG +34.000 AAAAAAAAAAA BBBBBBBBBB CCCCCCC מממ +33.000 DDDDDDDDDDDDD EEEEEEE GGGGG +33.000 | AAAAAAAAAA BBBBBBBBB CCCCCCC DDDD +32.000 DDDDDDDDDDDDD EEEEEEE FFFFFF +32.000 AAAAAAAAAA BBBBBBBBB CCCCCC DDDDD +31 000 +31.000 DDDDDDDDDD EEEEEEE Ιααααααααα REFERENCE CCCCCCC מממממ +30.000 DDDDDDDDDD EEEEEE FFFFFF GGGGG +30.000 AAAAAAAAA +29.000 CCCCCC DDDDDDDDD EEEEEEE GGGG +29.000 AAAAAAAA BBBBBBBBBB CCCCCC ממממממ +28.000 cccccccc DDDDDDDD EEEEEE FFFFF +28.000 AAAAAAA BBBBBBBBBB cccccc DDDDD +27.000 cccccccccc DDDDDDDD EEEEEE +27.000 AAAAAA BBBBBBBBB cccccc DDDDD ccccccccc DDDDDDD EEEEEE +26.000 +26.000 AAAAAA BBBBBBBBB CCCCCCC DDDDDDD +25.000 AAAAA DDDDDD +25.000 CCCCCCCCCC ממממממ REFER प्रप्रप्रम BBBBBBBBBB +24.000 AAAA +24.000 cccccccc DDDDDDDD BBBBBBBBBB ccccc DDDDDD EEEEE +23.000 | AAA DDDDD +23.000 RRR CCCCCCCCC DDDDDDD EEEEE +22.000 BBBBBBBBBB CCCCCC DDDDD +22.000 BBBBBBB CCCCCCC DDDDDDD EEEEEE +21.000 REFERENCE cccccc DDDDDDD EE +21.000 BRRRRRRRR ccccccc DDDDDDD REFER प्रप्रमुख +20.000 CCCCCC DDDDDD +20.000 CCCCCC DDDDD EEEE +0.000 +0.333 +0.667 +1.000 +1.333 +1.667 +0.000 +0.333 +0.667 +1.000 +1.333 +1.667 ENZYME ENZYME +7.20=B +9.60=D +10.80=E +6.00=A +8.40=C Legend: Legend: +6.00=A +7.20 = B+8.40=C +9.60=D +10.80=E +12.00=F +13.20=G +14.40=H +15.60=I +16.80=J +12.00=F +13.20=G+14.40 = H+15.60=I +16.80=J +18.00=K +18.00=K

Figure 3.4 RSM plots for combination of xylanase and cellulase. 0 hour incubation (left) and 16 hours incubation (right)

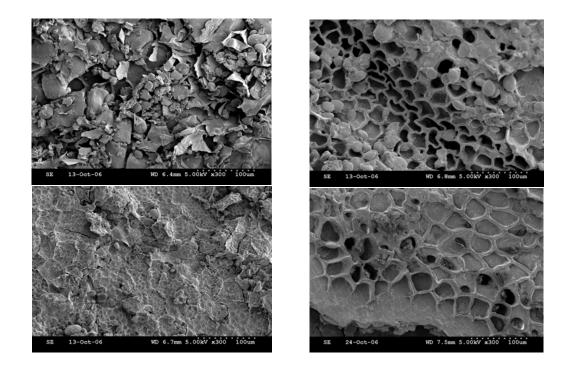


Figure 3.5 Scanning electron microscope (SEM) pictures of inner bran fraction. Intact bran fraction (left) and enzymatically hydrolyzed bran (right). Intact bran fraction is covered with aleurone cell walls whereas the enzymatically hydrolyzed bran fraction exposes the inner aleurone cell wall and aleurone content was released.

CHAPTER 4 - Bran Separation on Enzyme Treated Wheat

Based on results from the preliminary test with wheat bran, an experiment for the enzyme application to intact wheat kernels was designed.

4.1 Materials and Methods

Destarched bran

Prior to running the reducing sugar assay for determining the enzyme activities, destarched bran was prepared as a substrate because, as mentioned previously, the wheat bran contained 19.7% starch. To remove starch from wheat bran and obtain a pure wheat bran fraction, 1 g of α -amylase, SEB® AMYL-XCP (*Aspergillus oryzae*, Specialty Enzymes Co.), and 150 g of wheat bran were incubated at optimum temperature (45°C) for 2 hours in 1200 mL of pH 5 water. The wheat bran was then dried at 65°C, and the α -amylase was inactivated at that temperature.

Enzymes

Cellulases, xylanases, and pectinases were donated by Specialty Enzymes and Biochemicals Co. (CA, U.S.). An enzyme cocktail, comprising a combination of xylanase, cellulase, and pectinase, was prepared in equal ratios based on their activities. These amounts of enzymes were found to produce one locally-defined 'sugar unit' from 1 g of destarched bran substrate when incubated for 2 hours at optimum temperature and pH (40°C, pH 6 for cellulase, 55°C, pH 5 for xylanase, and 45°C, pH 5 for pectinase). After enzyme application on the destarched wheat bran, the mixture was centrifuged at 10,000 x g for 10 min at room temperature, and then the reducing sugar assay was conducted with the supernatant. One unit is defined as the amount of enzyme which can hydrolyze the substrate and releases 15 mmol of reducing sugar in the supernatant in 2 hours incubation time. As a result, 1 unit of the enzymes, cellulase, xylanase, and pectinase, was definded as 31.68 μg, 26.36 μg, and 127.94 μL, respectively (Figure 4.1).

pectinase (micro-liter) 100 150 200 50 250 0 45.0 127.93 40.0 35.0 $y = -0.0022x^2 + 0.5664x + 1.5972$ $R^2 = 0.9997$ reducing sugar conc (mm 30.0 $y = -0.0014x^2 + 0.4558x + 1.9656$ $R^2 = 0.9965$ 25.0 20.0 15.0 $y = -0.0003x^2 + 0.1372x + 2.3573$ $R^2 = 0.9841$ 10.0 31.67 5.0 26.3 0.0 20 60 80 100 0 40 120 cellulase and xylanase (mg) cellulase Xylanase ▲ pectinase

Enzyme activity

Figure 4.1 Enzyme activities for cellulase, xylanase, and pectinase by reducing sugar assay

Wheat kernel

A pure variety sample of hard red winter wheat (2174) was procured from the Agronomy Department, Kansas State University. Test weight was 60.3 lb/Bu. Single kernel weight, diameter, hardness, and moisture were measured by using the Single Kernel Characterization System (SKCS) model 4100 (Perten Instruments North America, Inc., Reno, NV), and were 33.94 mg, 2.72 mm, 63.78 (hardness index), and 12.02%, respectively. By using the oven drying method (AACC 44-15A), moisture content of the wheat was 12.36%; and the required amount of water was determined following the tempering table (AACC 26-95).

Wheat preparation and milling process

Five hundred grams of wheat were tempered to the postulated amount of moisture content following the experimental design (Table 4.4). The required amount of water and enzymes were calculated and added to the wheat. Distilled water was mixed with 37% hydrochloric acid to adjust pH to 3, 4, 5, or 6. For pH 7, distilled water was used for tempering. The enzymes were dissolved completely before adding to the wheat. Wheat samples were shaken with water or enzyme solution in a 2-layer sealed plastic bag for 3 minutes, and then incubated for a stipulated time and temperature in the oven. After the prescribed incubation times, wheat which was tempered above 16%, was spread out on the sieves as a single layer, and dried back to 16% moisture content in a 32°C oven. Prior to milling, the physical properties of the kernel were measured by using the single kernel characterization system (SKCS 4100). For grinding, the experimental laboratory Ross Mill flow, which consisted of four breaks, one sizing, two tailings, and five reductions, was used. The experimental milling flow is shown in Figure 4.2. The amount of flour from each of 13 streams, bran, shorts, red dog, and germ was recorded on the experimental mill data sheet (Appendix A) for later analysis.

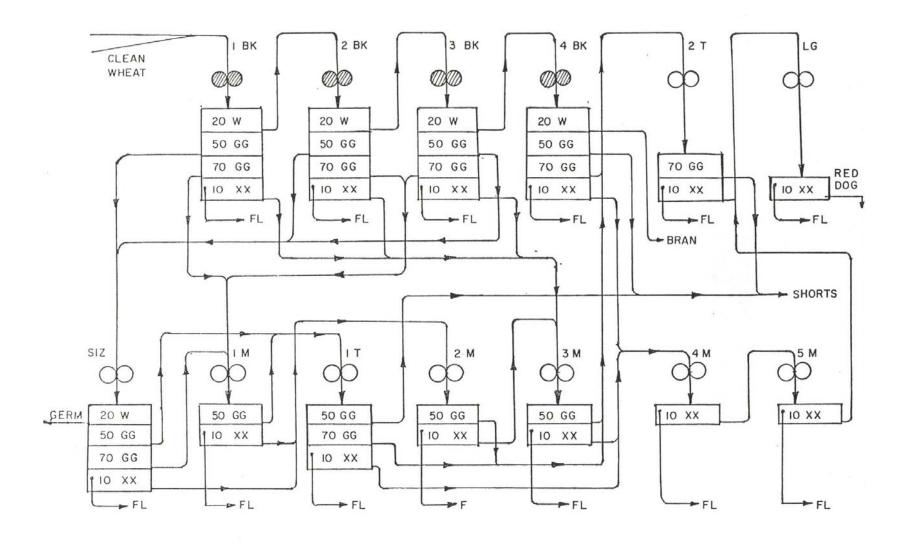


Figure 4.2 Experimental Milling Flow sheet for Ross Rolls Batch Procedure (adapted from Posner et al. 1997)

BK: Break, SIZ: sizing, T: Tailing, M: Middling, LG: Low grade, and FL: Flour

Quality Parameters for Flour and Milling Process

The flour obtained from each grinding was classified into patent and clear flours and then analyzed for flour quality and milling efficiency. To determine the quality and efficiency of the milling process, quality parameters, namely flour yield, flour protein and ash content, flour particle size, and flour color were studied. Protein and ash were measured following AACC 46-30 and AACC 08-01 respectively. For the flour color, the Agtron green light reflectance color meter (Model M-45-D, Agtron Inc. NV) was used. Gillis (1963) reported that the Agtron green light could be used to determine the flour ash content and was more closely related to changes in ash than was the Blue Agtron light. Also, it has been found that the Agtron green light reading was stable during 6 months of storage under ambient condition (Shuey, 1975).

Experimental design

The experiment was conducted according to the requirement of response surface methodology (RSM) for analyzing the data regarding the milling efficiency and flour quality. Central composite designs are economical in terms of experimental units; and enable the estimation of quadratic response equations (Kuehl, 2000). A second order central composite design was conducted with 5 levels, high, medium high, medium, medium low, and low, which were coded by -2, -1, 0, +1, and +2 respectively, with 5 variables, enzyme concentration, incubation time, incubation temperature, tempering water pH, and tempering target moisture content (Table 4.1 and 4.2). The result was analyzed and plotted by SAS (version 9.1, SAS Institute, Inc., Cary, NC, USA) at p < 0.05. Response surface analysis was used to estimate the model coefficient and to perform a response surface regression (RSREG) procedure by SAS. The "ridge min" and "ridge max" options in the RSREG procedure were included to generate the ridge of maximum and minimum response of the dependent variables. The total required number of experiments was 33 for the each treatment, and the levels and required experiment number was balanced (Table 4.3 and 4.4). Actual experimental order was randomized.

Table 4.1 Variables and Levels

			-2	-1	0	+1	+2
X1	Enzyme concentration	Units	0	60	120	180	240
		% (w/w)*	0	0.84	1.70	2.55	3.40
X2	Incubation time	hr	6	9	12	15	18
Х3	Incubation temperature	°C	25	32.5	40	47.5	55
X4	Target moisture content	%	16	18	20	22	24
X5	Tempering water pH	рН	3	4	5	6	7

^{*} Added enzyme concentration based on the dry matter of the wheat kernels

Table 4.2 Balanced Number of Required Experiments

Levels	X1	X2	Х3	X4	X5
-2	1	1	1	1	1
-1	8	8	8	8	8
0	15	15	15	15	15
+1	8	8	8	8	8
+2	1	1	1	1	1
Total runs	33	33	33	33	33

Table 4.3 Response Surface Methodology for Central Composite Design with 5 Variables

-1	X1	X2	Х3	X4	X5
-1	-1	-1	-1	-1	1
1 1 -1 -1 1 -1 -1 -1 -1 -1 1 -1 1 -1 -1 1 -1 1 -1 -1 -1 1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1	1	-1	-1	-1	-1
-1	-1	1	-1	-1	-1
1 -1 1 -1 1 -1 1 1 -1 1 1 1 1 -1 -1 1 -1 -1 -1 -1 -1 -1 -1 1 1 -1 1 -1 -1 1 -1 -1 -1 1 -1	1	1	-1	-1	1
-1	-1	-1	1	-1	-1
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0 0 0 -2 0 0 0 0 2 0 0 0 0 0 -2 0 0 0 0 2	0	0	-2	0	0
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0 0 0 2 0 0 0 0 0 -2 0 0 0 0 2	0	0		-2	0
0 0 0 0 -2 0 0 0 0 2	0	0	0	2	0
0 0 0 0 2	0	0			-2
	0	0			2
	0	0	0	0	0

: 7 replicates

Table 4.4 Randomized Experimental Design Run Order

run	Enzyme Con. X1	Incubation time X2	Incubation Temp X3	Tempered MC X4	Tempering water pH X5
1	120	12	40	0.2	7
2	60	9	47.5	0.22	6
3	120	12	40	0.2	5
4	120	12	25	0.2	5
5	180	15	32.5	0.18	6
6	60	15	47.5	0.18	6
7	60	9	32.5	0.18	6
8	120	6	40	0.2	5
9	120	12	40	0.16	5
10	180	9	32.5	0.22	6
11	120	12	40	0.2	5
12	180	15	47.5	0.18	4
13	120	12	40	0.2	5
14	60	15	47.5	0.22	4
15	60	15	32.5	0.18	4
16	120	18	40	0.2	5
17	0	12	40	0.2	5
18	120	12	40	0.2	5
19	120	12	40	0.2	5
20	120	12	40	0.2	5
21	180	15	32.5	0.22	4
22	180	9	32.5	0.18	4
23	180	9	47.5	0.18	6
24	120	12	40	0.2	3
25	240	12	40	0.2	5
26	180	15	47.5	0.22	6
27	60	9	47.5	0.18	4
28	120	12	40	0.24	5
29	60	9	32.5	0.22	4
30	60	15	32.5	0.22	6
31	120	12	40	0.2	5
32	120	12	55	0.2	5
33	180	9	47.5	0.22	4

: 7 Replicates

4.2 Results and Discussions

4.2.1 Effect on Flour Color

The results that were measured by the Agtron and Minolta were analyzed by SAS software (Appendix D) and the contribution of the independent variables to the response surface for color was investigated. Agtron readings for the various treatments ranged from 72 to 79, 51 to 68, and 70 to 77 for patent, clear, and straight flour, respectively (refer to Appendix C). For both tests (Agtron and Minolta) there were no significant factors affecting the flour color (p<0.05); and the stationary point was at a saddle point. Because the canonical analysis resulted in a saddle point, the estimated surface did not have a unique optimum. Further analysis, ridge analysis with radius 2.0, was required to see the color change pattern for the variables within the given range. In ridge analysis, it was observed that the flour Agtron color index increased slightly as the amount of enzyme and the pH were decreased, and as the incubation time was increased.

4.2.2 Effect on tempered wheat kernel physical characteristics

Significant factors affecting the tempered wheat kernel physical characteristics are summarized in Table 4.5. Time, interactions between time and moisture and between enzyme and pH were the significant factors affecting the single kernel weight after tempering, and resulting RSM equation explained 85.76% of variation in termed kernel weight. Incubation time was the only significant factor affecting the kernel hardness after tempering, and RSM equation accounting for 74.19% of variation in tempered kernel hardness was obtained. There was no significant factor for the tempered wheat diameter, and 73.41% of variation was explained by RSM equation. Only slight changes in physical characteristics were apparently caused by the 5 variables, as observed for the 33 data sets. Since the predicted response surface was a saddle shape, ridge analysis was conducted. For the wheat kernel hardness, the data indicated that kernel hardness increased from 62.47 to 64.10 as the enzyme increased from 120.00 to 120.03 units, incubation time increased from 12 to 12.18 hrs, incubation temperature increased from 40.00 to 40.10 °C, tempering moisture decreased from 20.00 to 18.74%, and tempering pH increased from 5.0 to 5.8.

4.2.3 Effect on the protein and ash content in flour

Significant factors and R-square for flour protein and ash content are shown in Table 4.5. The treatments were not statistically significant for the patent and clear flour ash contents with R² values, 0.43 and 0.54 respectively. Patent flour ash content ranged from 0.382 to 0.532; clear flour ash content ranged from 0.569 to 1.010 for the treatments (refer to Appendix C). For both flours, clear and patent, the result of ridge analysis of the predicted response surface showed that the ash content increased as pH decreased, with a slight change associated with the other treatments. Both the linear and the quadratic terms for tempering moisture content were the significant factors affecting the patent flour protein, whereas incubation time and the interaction between enzyme concentration and pH affected clear flour protein content. Patent flour protein content ranged from 10.37 to 10.92, and clear flour protein content ranged from 10.07 to 12.30 across treatments. Resulting RSM equation explained 79.38% and 61.91% of variation in patent and clear flour protein content, respectively. The correlations between flour ash content and Agtron color reading for patent flour, clear flour, and straight flour are shown in Figure 4.3, 4.4, and 4.5. For all three flours, inverse relations were found between ash and Agtron reading; but only the clear flours showed high correlations between ash content and flour color, with -0.76 for the correlation coefficient.

4.2.4 Effect on the Product Yield

Product yield for the various treatments was shown in Appendix C. The amounts of flour produced from the 13 streams were analyzed individually and then combined as patent, 1st clear, 2nd clear, and straight flour, and analyzed by SAS to observe the effect of treatments on wheat bran separation (Table 4.6). The stationary point for all predicted response surfaces were at the saddle point, which did not show an optimum condition. Most of the flours from break, sizing, and tailing streams were affected by the treatments, whereas none of the flours from the reduction roll were affected by the treatments. The break flours were mostly affected by the treatment. Enzyme by itself, and enzyme interactions with any other factors such as temperature, incubation time, and pH, showed the effect on yield of 1BK, 2BK, 1T, Bran, and 1st Clear flour production. Interactions among incubation time, temperature, moisture content, and pH had a significant influence on the response surface of the break flour yield. The significant factors affecting the response surface of each flour yield are summarized on Table 4.5. From the ridge

analysis, pH change was most obvious as a cause of the production yield change. For the production of shorts, red dog, and germ, all factors but enzyme showed their effect on decreasing or increasing their yield. The yield of 1st clear was well explained by the predictable response surface model with R²=0.9134. Ridge analysis showed that 1st clear flour yield increased from 6.2% to 6.6% when enzyme, time, temperature, moisture, and pH varied from 120.000000 to 120.000109 units, from 12.000000 to 12.745712 hrs, from 40.000000 to 39.887734°C, from 20.000000 to 18.473474%, and from 5.000000 to 3.950702, respectively (refer to Appendix D). Like the 1st clear flour, the pattern of paten flour yield within the range of variables was estimated by ridge analysis and was found to increase with an increase in enzyme, time, and temperature, and a decrease in moisture and pH. Predicted product yield was determined by the model with 21 terms. It was simplified and expressed the product yield with a high R square value (R²>0.75) so that the product yield could be predicted for any treatment conditions, which will be discussed later.

Table 4.5 Analyzed significant factors (at p<0.05) to the response surface of physical characteristics of tempered wheat and flour protein and ash content

	Significant factors	R-square
Kernel weight	b, b*d, a*e	0.8576
Kernel diameter	-	0.7341
Kernel hardness	b	0.7419
Clear flour ash	-	0.5438
Patent flour ash	-	0.4314
Clear flour protein	b, a*e	0.7938
Patent flour protein	d, d*d	0.6191
St. Flour color	-	0.7104

a: enzyme concentration

b: incubation time

c: incubation temperature

d: tempering moisture content

e: tempering water pH

*: interaction between two treatments

Table 4.6 Analyzed significant factors (at p < 0.05) to the response surface of product yield

Yield of milling product	Significant factors	R-square
1BK	e*a, e*e	0.8580
2BK	a, a*c, b*c, c*d, a*e	0.8221
3BK	c*e	0.6461
4BK	-	0.5468
SIZ	С	0.7015
1M	-	0.5558
1T	a*c	0.7100
2M	-	0.6247
3M	-	0.5710
2T	-	0.6810
4M	-	0.6484
5M	-	0.7497
LG	-	0.5767
Shorts, red dog, and germ	b, d, b*b, b*c, d*d, c*e	0.8706
Bran	e*a, e*c	0.7617
Patent flour	b, d*c	0.7880
1 st clear flour	a, b, a*b, a*e, c*e, d*e, e*e	0.9134
2 nd clear flour	-	0.6125
Straight flour	b, a*a, a*c, b*d	0.8658

a: enzyme concentration

b: incubation time

c: incubation temperature

d: tempering moisture content

e: tempering water pH

*: interaction between two treatments

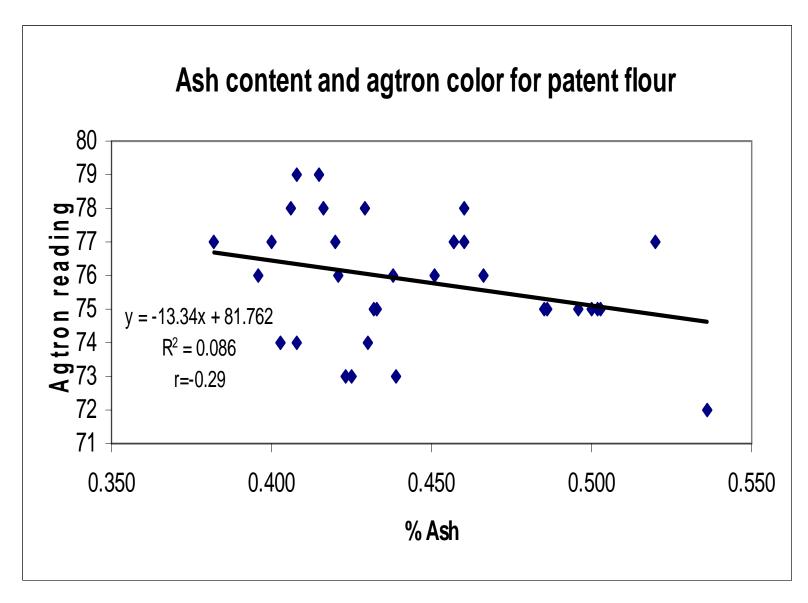


Figure 4.3 Scatter diagram of percent patent flour ash contents vs. Agtron reflectance values

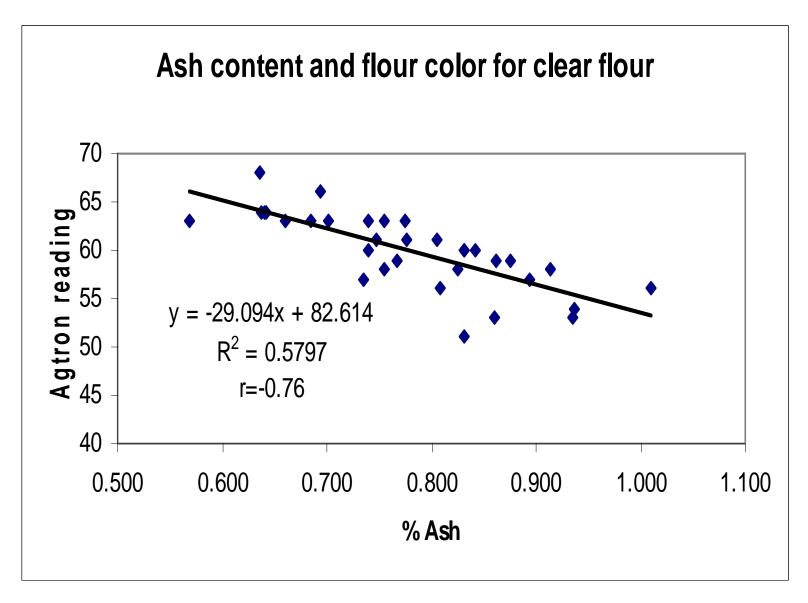


Figure 4.4 Scatter diagram of percent clear flour ash contents vs. Agtron reflectance values

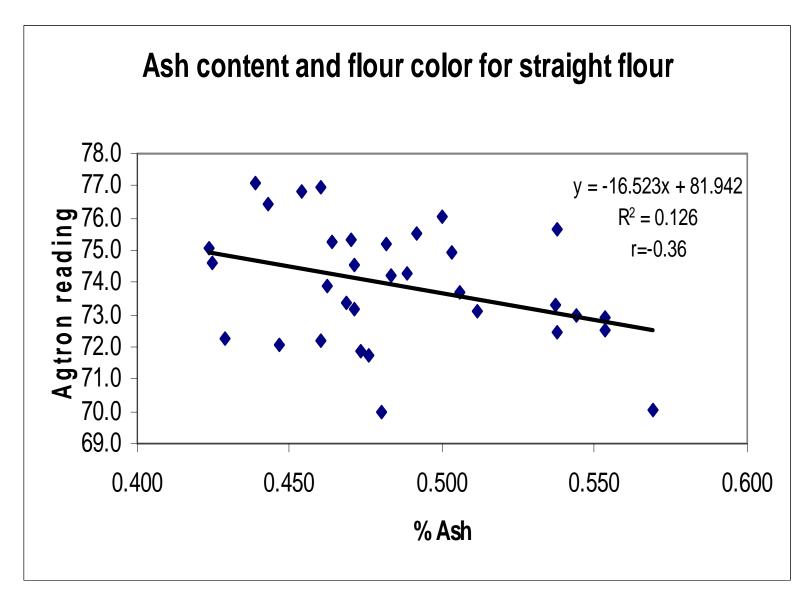


Figure 4.5 Scatter diagram of percent straight grade flour ash contents vs. Agtron reflectance values

4.2.5 Prediction of product yield

From the stepwise regression analysis using SAS software (Appendix D), quadratic models which show the relationship between the product yield and treatment variables were determined based upon 33 data sets. By stepwise regression analysis, quadratic models which can account for more than 75% of the variation in the experimental data, product yield, for the treatment variables were obtained. The selected model consisted of linear terms, quadratic terms, and cross-product terms for five treatment factors. The data for yield of flour from 1BK, 2BK, 1st clear flour, straight flour, patent, and the sum of shorts, red, and germ fit the model reasonably good (R²>0.75); however, the yield data for the others did not fit as well (R²<0.75) (Table 4.6).

The regression model fitted to the experimental results for the yield of 1^{st} break flour showed a good R-square (0.8580). The simplified model after the R-square selection method showed R^2 =0.7513:

 $\label{eq:Yield of 1st} \begin{aligned} \text{Yield of 1}^{\text{st}} \text{ break flour} &= 6.66121\text{--}\ 0.02296E - 0.11778P^2 + 0.00522EP - 0.00191tT \\ &+ 0.01768tP \end{aligned}$

Where E = enzyme concentration (unit), t = incubation time (hr), T = incubation temperature (°C), M = tempering target moisture content (%), and P = tempering water pH.

The regression model for the 2^{nd} break flour showed a good R-square (0.8221). The model after the R-square selection method was obtained with R^2 =0.8161: Yield of 2^{nd} break flour = $9.96279 - 0.03395E - 0.26139M + 0.00018786T^2 - 0.12447P^2 + 0.00028056ET + 0.00517EP - 0.00181tT + 0.00434tM + 0.00041742TM - 0.01191TP + 0.03810MP$

The model for the yield of 1^{st} clear flour was expressed with R^2 =0.9134 and obtained with R^2 =0.7773 after the R-square selection method:

 $\label{eq:Yieldof} \begin{aligned} \text{Yield of } 1^{\text{st}} \text{ clear flour} &= 6.76803 - 0.02379E + 0.00035171T^2 - 0.00436M^2 - 0.12324P^2 + \\ 0.00008433Et + 0.00518EP - 0.01050TP + 0.03459MP \end{aligned}$

The regression model for the yield of patent flour was expressed with R^2 =0.7880 and obtained with R^2 =0.7181 after square selection method:

 $\label{eq:Yield of patent flour} Yield of patent flour = 11.48775 - 0.38040t - 0.38105M - 0.00002769E^2 - 0.00016582T^2 - 0.00073985M^2 - 0.13437P^2 - 0.00008204ET + 0.00268EP - 0.00007337tT + 0.01979tM + 0.03421MP$

The regression model for the yield of straight flour was expressed with R^2 =0.8658 and obtained with R^2 =0.7655 after square selection method:

 $\label{eq:Yieldof} \mbox{Yield of straight flour} = 94.11942 - 2.10556t - 1.10560M - 0.00009795E^2 + 0.00095001ET - 0.00057835EM + 0.10208tM - 0.01708TP$

The regression model for the yield of red dog, germ, and shorts was expressed with R^2 =0.8706 and obtained with R^2 =7515 after square selection method:

Yield of red dog, germ, and shorts = $-59.72917 + 2.55949t + 0.85390T + 4.37230M - 0.06507t^2 - 0.13391M^2 + 0.00310Et + 0.00114ET - 0.00349EM - 0.03333tT - 0.11353TP + 0.24158MP$

CHAPTER 5 - Enzyme Effects on Dough Properties and Bread Making

Dough property tests and baking tests were planned, and the flour for these tests was supposed to be selected based upon the flour protein contents for each of the treatments from the previous experiment. However, the protein and ash contents in flours did not appear to show any differences for the treatments; and it seemed difficult to compare the enzyme effects on the dough and baking quality since there were five treatments (enzyme concentration, incubation time, incubation temperature, tempering moisture, and tempering water pH). To compare the enzymes' effects on dough characteristics and bread making, it was necessary to simplify the experimental design in terms of the number of treatments. Only two factors, incubation temperature and tempering water pH, were controlled and samples compared with the control.

5.1 Materials and Methods

Hard red winter wheat

The same single variety of hard red winter wheat (2174) which was used for the previous experiment was used.

Wheat preparation and tempering

Fifteen hundred grams of wheat were tempered to 16% moisture content under 6 different tempering conditions (Table 5.1).

	Enzyme Concentration*	Incubation temperature	Tempering water
1 (control)	-	Room temperature	Tap water
2	3%	50°C	pH 5
3	3%	Room temperature	Tap water
4	-	50°C	pH 5
5	-	50°C	Tap water

Table 5.1 Tempering condition

Room temperature

pH 5

^{*} w/w% based on the wheat kernel dry matter

Distilled water was mixed with sufficient 37% hydrochloric acid to adjust the pH to 5.0. The cocktail enzyme consisting of xylanase, cellulase, and pectinase with equal ratios of enzyme activity was dissolved completely in tempering water (3% w/w based on the dry matter of wheat) and then added to the wheat in a plastic container. The wheat was shaken in the plastic container for 3 min for uniform water distribution; and then 16 hours were allowed for rest or incubation time. An Isotemp® oven (Model 655F, Fisher Scientific Inc.) was used for 50°C incubation. After tempering, the tempered wheat was characterized by the SKCS.

Milling process

For the grinding, an experimental laboratory Ross Mill procedure consisting of four breaks, one sizing, two tailings, and five reductions, was used (procedure described above in Chapter 4). Product yield, and protein and moisture contents of the flour were determined.

Flour and dough characterization

Protein and moisture methods were based on AACC Approved Methods (AACC 2000) 46-30 and 44-15A, respectively. For the dough test, traditional empirical rheological methods such as the Mixograph (10 g flour bowl, National Manufacturing Division of TMCO, Lincoln, NE) and the Farinograph (50 g flour bowl, Farinograph E, C. W. Brabender, Duisburg, Germany), were conducted prior to the baking test to determine the optimum % water absorption and mixing times following AACC 54-40A and AACC 54-21, respectively.

Test baking

Test loaves (100 g flour) were baked following AACC Approved Method (AACC 2000) 10-10B. The formula was as follows: flour, 14% mb (100%), instant yeast (2.7%), sugar (6%), salt (1.5%), shortening (3%), malt flour (0.2%), and ascorbic acid (50 ppm). Fermentation temperature was 84-88°F, and the relative humidity was 95% in the fermentation cabinet. Optimum water absorption and mixing time was estimated by mixograph and corrected after mixing time pre-test. Mixing time pre-test was conducted with 100 g flour and shortening. Proofing height and baked bread weight and volume were obtained. The loaf volume was measured by rapeseed displacement method (volume meter). For the staling experiment, the Voland Stevens LFRA Texture Analyser (Voland Corp. Hawthrone, NY) was used to measure the staling rate for the treatments, using a 1- inch thick bread slice. Each treatment was baked

twice. Three slices were measured from each loaf, and the average for the 6 slices was taken for comparison purposes. The bread was stored in two layers of plastic bags at room temperature for one, three, and five days. The data obtained from the test baking were analyzed with ANOVA using SAS software at p<0.05.

5.2 Results and Discussions

Physical kernel characteristics

As shown in Figure 5.1, 5.2, 5.3, and 5.4, the results from the SKCS showed obvious effects of enzyme treatment on single kernel weight, diameter, and hardness. Kernels treated with enzymes had significantly higher weight, larger diameter, and greater hardness, irrespective of heat and pH treatments, compared with non-enzyme treated kernels. The increases in weight and diameter of the tempered kernels were not explained solely by their moisture contents. Small but significant differences in the weight of the kernel might be explained for by the weight of the enzyme applied. Three % (w/w) of enzyme was applied, based on the kernel dry matter, during the tempering, and it might account for the difference. For the kernel hardness, enzyme treated kernels were harder than non enzyme treated kernels and were harder than the kernel before tempering, which was against the usual purpose of tempering. Increase in hardness after enzymatic tempering was unexpected result and was in disagreement with well known fact that the larger kernel is softer. Interestingly, although enzymatic tempered wheat kernel was harder, it seemed to be more swollen, as compared with non-enzyme treated kernel.

SINGLE KERNEL WEIGHT

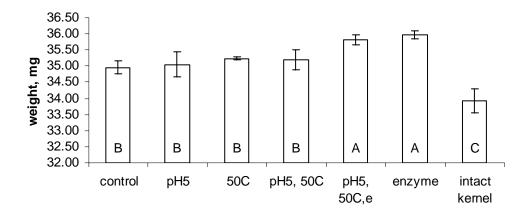


Figure 5.1 Single kernel weight after different tempering conditions

Letters indicate statistical differences at p<0.05 (n=2). The weight of the enzyme treated kernels was significantly higher than that of non-enzyme treated kernels.

SINGLE KERNEL DIAMETER

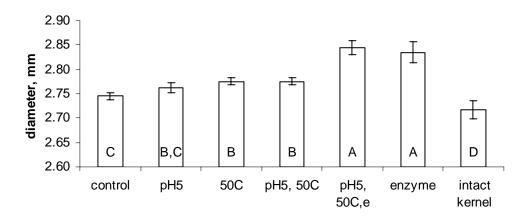


Figure 5.2 Single kernel diameter after different tempering conditions

Letters indicate statistical differences at p<0.05 (n=2). The diameter of the enzyme treated kernels was significantly higher than that of non-enzyme treated kernels.

SINGLE KERNEL HARDNESS

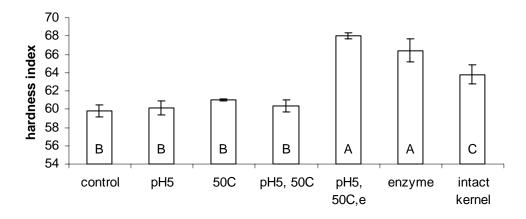


Figure 5.3 Single kernel hardness after different tempering conditions

Letters indicate statistical differences at p<0.05 (n=2). The hardness of enzyme treated kernels was significantly higher than that of non-enzyme treated kernels. After enzyme treatment with or without heat and under pH treatment, the kernel hardness was higher than that of intact kernels.

SINGLE KERNEL MOISTURE

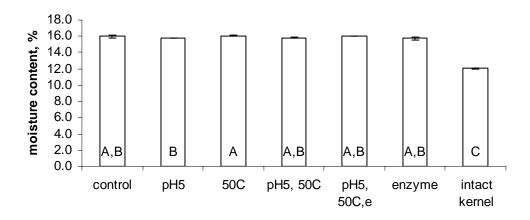


Figure 5.4 Single kernel moisture content for different conditions

Letters indicate statistical differences at p<0.05 (n=2). Moisture of tempered wheat was not significantly different for the treatments. The wheat kernels with 12.02% moisture content (by SKCS) were tempered to 16% moisture content.

Flour yield

Product yields for the patent, clear, straight flour, bran, red dog, germ, and shorts were not significantly different for the treatments, which corresponded to the previous results from the Chapter 4.

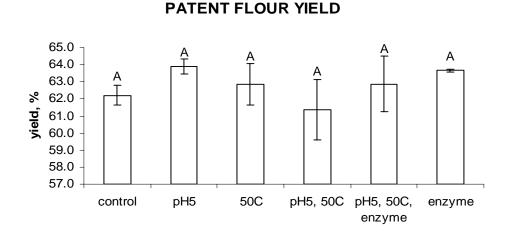


Figure 5.5 Patent flour yield for the treatments

Letters indicate statistical differences at p<0.05 (n=2). Patent flour yield for the treatments was not significantly different.

CLEAR FLOUR YIELD

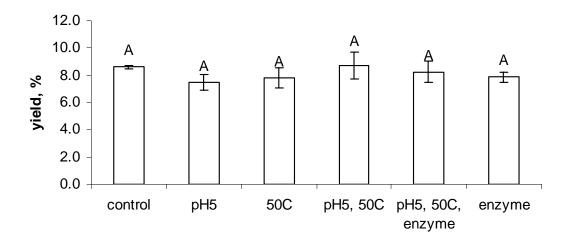


Figure 5.6 Clear flour yield for the treatments

Letters indicate statistical differences at p<0.05 (n=2). Clear flour yield for the treatments was not significantly different.

STRAIGHT FLOUR YIELD

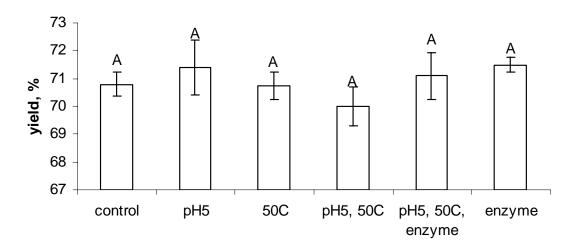


Figure 5.7 Straight flour yield for the treatments

Letters indicate statistical differences at p<0.05 (n=2). Straight flour yield for the treatments was not significantly different.

BRAN YIELD

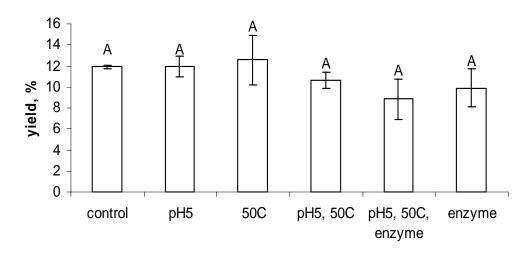


Figure 5.8 Bran yield for the treatments

Letters indicate statistical differences at p<0.05 (n=2). Bran yield for the treatments was not significantly different.

RED DOG, GERM, AND SHORTS YIELD

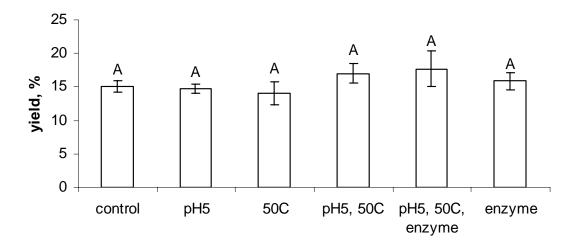


Figure 5.9 Red dog, germ, and shorts yield for the treatments

Letters indicate statistical differences at p<0.05 (n=2). Yield of red dog, germ, and shorts for the treatments was not significantly different.

Flour protein content

The protein contents of the flours for the treatments are shown in Figure 5.10. Significantly higher protein contents of the flours resulted from the enzymatically tempered wheat. Compared with the control, flour protein content was increased 2.18 and 2.94% for the enzyme treatment with heat under the pH treatment and only enzyme treatment, respectively. However, it could not be concluded that the increased protein is functional protein for the bread making because the mixograms did not show any differences in optimum water absorption or mixing time (described later), and also, there were no significant differences in clear flour yields. The applied enzyme amount (3% w/w based on dry matter of wheat kernels) could account for the increase in the protein level of flour from the enzyme treated kernel.

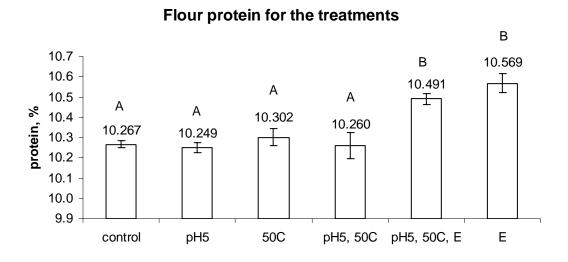


Figure 5.10 Flour protein content for the treatments

Letters indicate statistical differences at p<0.05 (n=2). Protein content in flour containing enzyme treatment was significantly higher, regardless of heat and pH treatment.

Farinograph

Estimates for the absorption ranged from 56 % to 57 %. Control flour and pH treated wheat flour had longer mixing stability. Heat-only treated and heat and pH treated wheat flour showed slightly shorter mixing stability than control and pH-only treated wheat flour. The flour milled from the enzymatic tempered wheat seemed to require slightly higher absorption and broke down more rapidly after the peak time had been reached (Figure 5.11).

Mixograph

Mixograms showed a 64% optimum water absorption for all the treatments (From Figure 5.12 to 5.17). The mixogram prepared with 62% absorption showed a curve with rough edges and wild swings, and the mixogram prepared with 66% absorption appeared slack. After the mixing time pre-test, the optimum absorptions and mixing times were determined and are shown in Table 5.2. Sixty two % absorption, which was lower than that estimated with the mixograph, was used for mixing. The flour with enzyme treatment showed less mixing tolerance, corresponding to the results shown by the farinograph. From the corrected mixing time, it was thought that the increased protein in enzyme treated flour was not functional gluten forming protein.

Table 5.2 Corrected optimum absorption and mixing time by mixing time pre-test

	Treatment	Optimum absorption	Optimum mixing time
1	Control	62%	4 min 15 sec
2	pH5	62%	4 min 15 sec
3	50°C	62%	4 min 15 sec
4	pH5 and 50°C	62%	4 min 15 sec
5	Enzyme, pH5, and 50°C	62%	4 min
6	Enzyme	62%	3 min 30 sec

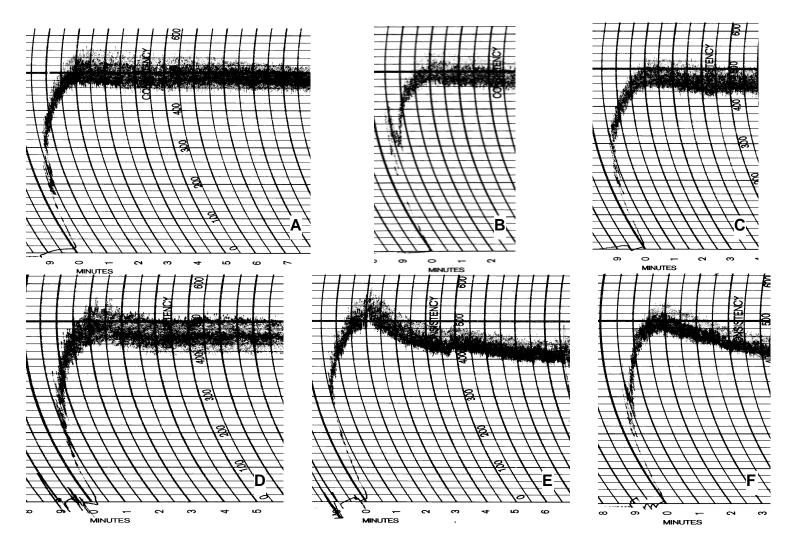


Figure 5.11 Farinograms for the treatments

A) Control (56% absorption); B) pH5 (56%); C) 50°C (56.2%); D) pH5 and 50°C (56%); E) enzyme, pH5, 50°C (56%); F) enzyme (57.2%)

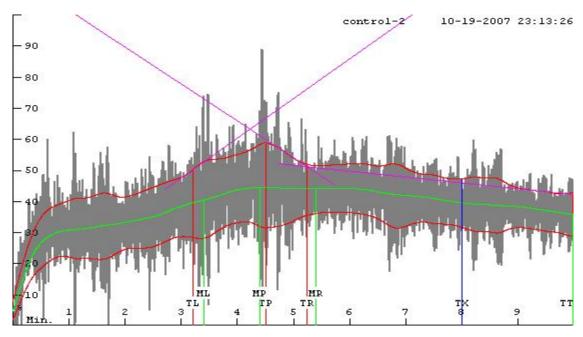


Figure 5.12 Mixogram for the flour from the control wheat (64% absorption)

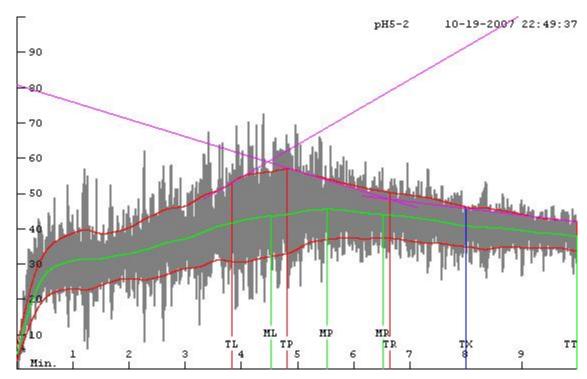


Figure 5.13 Mixogram for the flour from the wheat tempered with pH 5 water (64% absorption)

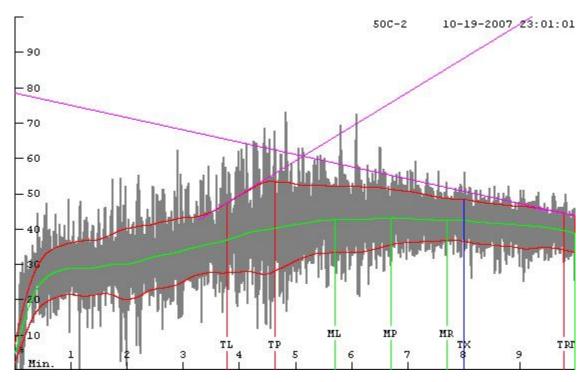


Figure 5.14 Mixogram for the flour from the wheat tempered at 50° C (64% absorption)

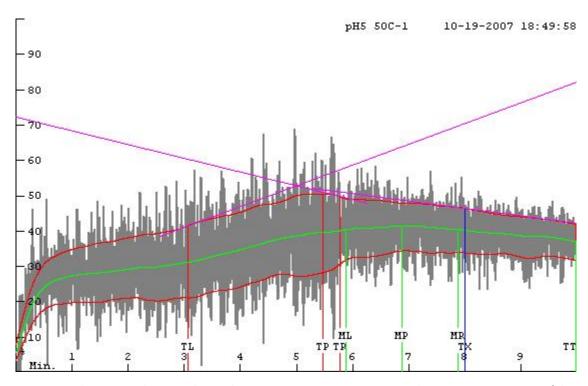


Figure 5.15 Mixogram for the flour from the wheat tempered with pH5 water at $50^{\circ} \mathrm{C}$ (absorption 64%)

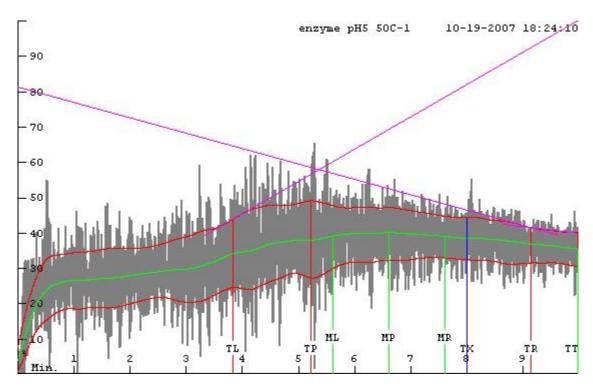


Figure 5.16 Mixogram for the flour from the wheat tempered with pH5 enzyme solution at $50^{\circ}\mathrm{C}$ (absorption 64%)

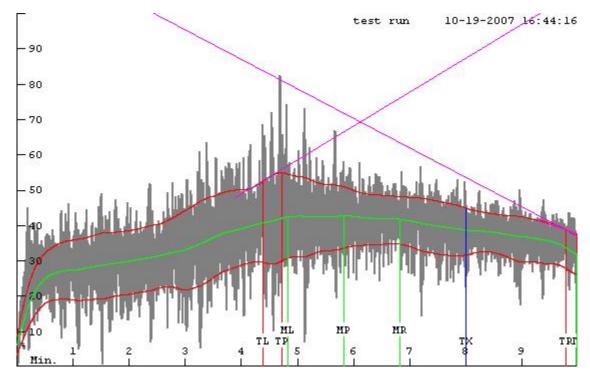


Figure 5.17 Mixogram for the flour from the wheat tempered with enzyme (absorption 64%)

Test baking

The results from the test baking are shown in Table 5.3 and 5.4, and Figure 5.18, and 5.19. There were no significant differences for the treatments in volume or staling rates. There were significant differences in proofing height and bread weight, but the differences were not reflected in the differences in final bread volume. The bread volumes for the treatments were not significantly different for the treatments. The treatment applied during tempering did not make a difference in softness after 24 hours. The bread with flour involving the tempering at 50°C without low pH treatment showed the greatest firmness after 3 and 5 days. Enzyme-only treated bread showed the lowest number in firmness after 1 day. However, enzyme treatment did not seem to slow down the staling rate over time, which was not in the agreement with the previous report (Courtin, C. M., and Delcour, 2002).



Figure 5.18 One lb loaf bread with different treatments

Control; pH5; 50°C; pH5 and 50°C; enzyme, pH5, and 50°C; and enzyme treated bread (from left to right)

Table 5.3 Test baking results

	Treatment	Proofing height (cm)	Bread weight (g)	Bread volume (cc)	Specific volume (cc/g)
1	Control	6.05 ^{a,b}	143.35 ^{a,b}	752.50 ^a	5.250 ^a
2	pH5	6.10 ^{a,b}	142.15 ^{a,b}	766.65 ^a	5.394 ^a
3	50°C	6.35 ^a	143.65 ^{a,b}	807.50 ^a	5.620 ^a
4	pH5 and 50°C	6.15 ^a	144.35 ^a	758.30 ^a	5.254 ^a
5	Enzyme, pH5, and 50°C	5.60 ^b	144.50 ^a	735.85 ^a	5.091 ^a
6	Enzyme	6.20 ^a	141.30 ^b	789.15 ^a	5.586 ^a

Means for a given parameter sharing the same letter are not significantly different at p<0.05 (n=2).

Table 5.4 Staling test with Voland Stevens Texture Analyser

	Treatment	Load, gram					
	Treatment	1 day	3 days	5 days			
1	Control	337.5 ^a	714.0 ^a	769.0 ^b			
2	pH5	335.0 ^a	623.5 ^{a,b}	903.0 ^a			
3	50°C	328.5 ^a	529.5 ^b	740.5 ^b			
4	pH5 and 50°C	334.0 ^a	580.5 ^{a,b}	891.0 ^a			
5	Enzyme, pH5, and 50°C	340.5 ^a	601.5 ^{a,b}	904.5 ^a			
6	Enzyme	282.0 ^a	548.0 ^b	852.0 ^a			

Means for a given parameter sharing the same letter are not significantly different at p<0.05 (n=2).

STALING

1000
900
800
700
500
400
300
200

1day
3days
5days

→ control → pH5 → 50C → pH5, 50C → E, pH5,50C → enzyme

Figure 5.19 Staling rate for breads with different treatments

Conclusions

Cell wall degrading enzymes; cellulase, xylanase, and pectinase were used in this study to hydrolyze the bran fraction and release the sugar. Five independent variables; enzyme concentration, incubation time, incubation temperature, wheat moisture content, and temper water pH were selected to assess their effects on the efficacy of bran removal during wheat milling. When three enzymes were combined and added in temper water under various conditions, no improvements in flour yields were observed. Six equations were arrived at to predict the product yield.

Enzymes seemed to harden the wheat kernel after tempering. Flour milled from the enzymatic tempered wheat contained significantly higher protein compared with flour from the non-enzymatic tempered wheat when the rest of experimental conditions remained the same. It was unclear if the protein came from the wheat kernel or from the enzyme. Although the treatments showed slight differences in mixing time between enzyme treated flour and non-enzyme treated flours, specific loaf volumes. However the firmness of enzyme treated bread was significantly higher than control bread after 5 days storage.

Enzyme penetration within the wheat kernel and its spatial distribution were not understood. Future work could include a study on the degree of enzyme penetration within the cross section of a wheat kernel. Scarifying of the kernel prior to enzyme application may improve enzyme penetration. Also, a study of the change in mechanical and biochemical characteristics of the enzyme treated kernel could give some insight into "if and how" enzymes could ease bran separation. Perhaps a shorter tempering time, allowing the temper water and enzymes to penetrate only into the bran layer, could loosen the bran, making its removal easier than by the existing method.

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Appendix A - Experimental Mill Data Sheet Reported in Grams

EXPERIMENTAL MILL DATA SHEET REPORTED IN GRAMS

									humidity and ¹ ME OF MILLEF O	Temperature:			
										Test #:			
	1BK	2BK	звк	4BK	SIZ	1M	1T	2M	3M	2T	4M	5M	LG
OV. 20WW:						><	\sim	><	\sim	><	><	><	><
OV. 50GG:											$>\!\!<$	$>\!\!<$	$>\!\!<$
OV. 70GG:			<u> </u>			> <		$>\!\!<$	> <		ot = ot	ot = ot	ot = ot
OV. 10XX:													
THRU 10XX:							•						
% HIING:													
/8 HONG.													
OUT:													
LOSS:													
1st Clear	(2BK, 3BK, S (1BK, 2T, 5M (4BK, LG)		1, 3M, 4M)		% Hung				Bran Germ Shorts Red Dog				
St. Grade flo	ur					ş					•		
Bran Total % Gain or lo	erm, & Shorts ss (circle one												
ilour yielu (b	aseu on the t	otal product)					Characteristi	ics of tampar	ed wheat usin	a SKCS			
% BREAK	RELEASE		Agtron				Citatacterist	1	•	_		1	
								weight (mg)	diameter (mm)	hardness	MC (%)]	
			Pat. Flour		•		1					Ì	
2ND:			Clear		•		2					Ì	
3RD:							average					1	
4TH:							std.dv.					İ	

Appendix B - Physical Characteristics of Tempered Wheat (SKCS Data)

Treatment						weight	(mg)	diameter	(mm)	hardness	index	moisture co	ntent (%)
Test #	Enzyme	time	Temp	MC	рН	average	Stdev.	average	Stdev.	average	Stdev.	average	Stdev.
						35.28	1.13	2.82	0.04	62.79	1.24	15.67	0.09
2	60	9	47.5	22	6	34.64	0.88	2.82	0.03	63.69	0.04	15.86	0.06
3	120	12	40.0	20	5	35.47	0.19	2.82	0.01	60.59	0.82	15.48	0.08
4	120	12	25.0	20	5	34.86	0.14	2.77	0.00	59.70	1.66	15.32	0.01
5	180	15	32.5	18	6	35.58	0.09	2.83	0.01	66.23	1.10	15.99	0.01
6	60	15	47.5	18	6	34.55	0.37	2.76	0.00	61.26	0.14	15.42	0.09
7	60	9	32.5	18	6	35.20	0.45	2.79	0.03	59.03	0.28	15.67	0.09
8	120	6	40.0	20	5	35.04	0.35	2.81	0.01	62.12	0.91	15.66	0.07
9	120	12	40.0	16	5	35.13	0.42	2.82	0.02	68.10	1.63	15.95	0.14
10	180	9	32.5	22	6	34.96	0.42	2.79	0.01	62.17	0.55	15.61	0.02
11	120	12	40.0	20	5	35.41	0.08	2.81	0.01	63.53	0.92	15.67	0.09
12	180	15	47.5	18	4	35.86	0.18	2.81	0.01	61.50	1.98	15.86	0.04
13	120	12	40.0	20	5	35.65	0.35	2.82	0.02	59.81	0.92	15.86	0.04
14	60	15	47.5	22	4	35.84	0.06	2.82	0.02	59.95	0.91	16.12	0.12
15	60	15	32.5	18	4	35.55	1.30	2.78	0.04	58.04	1.18	15.80	0.16
16	120	18	40.0	20	5	36.16	1.07	2.85	0.04	61.00	0.21	15.68	0.09
17	0	12	40.0	20	5	35.47	0.15	2.78	0.01	61.32	0.28	15.94	0.08
18	120	12	40.0	20	5	35.53	0.37	2.86	0.01	64.95	2.32	16.42	0.04
19	120	12	40.0	20	5	36.15	0.40	2.88	0.02	63.52	0.88	16.03	0.00
20	120	12	40.0	20	5	35.09	0.49	2.78	0.01	60.79	2.22	15.92	0.11
21	180	15	32.5	22	4	35.53	0.72	2.83	0.04	59.43	1.48	15.98	0.06
22	180	9	32.5	18	4	36.59	0.35	2.86	0.01	59.55	1.00	15.71	0.01
23	180	9	47.5	18	6	36.03	0.85	2.84	0.01	64.46	1.14	15.91	0.04
24	120	12	40.0	20	3	35.55	0.23	2.80	0.01	60.94	1.97	15.52	0.06
25	240	12	40.0	20	5	36.32	0.30	2.91	0.00	63.71	1.52	15.97	0.03
26	180	15	47.5	22	6	36.62	0.35	2.90	0.03	60.32	0.49	16.06	0.01
27	60	9	47.5	18	4	35.31	0.87	2.78	0.07	60.77	0.88	15.40	0.10
28	120	12	40.0	24	5	35.42	0.51	2.82	0.03	61.18	0.05	15.61	0.04
29	60	9	32.5	22	4	35.51	0.26	2.79	0.02	58.73	0.59	16.29	0.08
30	60	15	32.5	22	6	35.22	0.23	2.79	0.01	59.57	0.59	16.09	0.03
31	120	12	40.0	20	5	35.26	0.37	2.80	0.01	62.40	0.88	15.84	0.08
32	120	12	55.0	20	5	35.23	0.13	2.90	0.11	66.95	0.58	16.14	0.04
33	180	9	47.5	22	4	35.04	0.77	2.81	0.03	67.07	0.96	15.97	0.10

Appendix C - Milling Data

Test #	Ash cor	ntent, %	Protein c	ontent, %	Agtron	reading			Milling	product yield, %			
rest#	patent	clear	patent	clear	patent	clear	patent flour	1st clear	2nd clear	red dog, germ, shorts	bran	feed	yield
1	0.536	0.860	10.785	11.685	72	53	61.0	5.1	1.9	18.0	7.3	25.3	72.9
2	0.408	0.894	10.681	12.297	74	57	60.6	5.6	1.7	16.5	8.3	24.8	73.3
3	0.396	0.640	10.614	10.809	76	64	61.4	6.3	1.9	15.8	11.2	27.0	72.1
4	0.438	0.775	10.676	11.116	76	63	60.3	6.9	2.5	16.7	9.2	25.9	72.9
5	0.403	0.569	10.497	10.983	74	63	56.5	7.4	3.0	20.1	9.6	29.7	69.3
6	0.406	0.755	10.619	11.744	78	63	59.4	4.7	2.3	14.3	11.2	25.5	72.3
7	0.415	0.831	10.555	11.648	79	60	62.5	5.4	2.2	16.6	8.7	25.3	73.5
8	0.451	0.777	10.764	11.053	76	61	61.7	5.8	2.2	14.7	11.1	25.8	73.0
9	0.500	0.831	10.923	11.376	75	60	61.7	6.0	1.8	14.9	10.2	25.1	73.4
10	0.421	0.740	10.749	11.477	76	60	59.6	6.4	2.5	14.5	11.4	25.9	72.6
11	0.420	0.842	10.810	11.160	77	60	62.9	6.1	1.2	15.7	9.3	25.0	73.8
12	0.430	0.755	10.784	11.336	74	58	61.0	7.1	2.9	19.3	7.5	26.8	72.5
13	0.457	0.638	10.664	10.829	77	64	59.5	6.8	2.6	15.9	11.7	27.6	71.4
14	0.520	0.702	10.742	10.205	77	63	63.2	5.8	1.0	13.9	12.1	26.0	72.9
15	0.460	0.694	10.706	11.004	77	66	59.3	7.0	2.2	14.7	11.7	26.4	72.2
16	0.460	0.805	10.789	11.011	78	61	61.9	6.2	1.9	14.5	11.2	25.7	73.1
17	0.429	0.636	10.499	10.808	78	68	60.0	6.1	2.1	14.4	13.2	27.6	72.1
18	0.408	0.661	10.549	10.433	79	63	60.8	5.9	2.5	17.1	11.3	28.4	71.0
19	0.382	0.685	10.374	11.267	77	63	59.2	6.3	3.1	18.5	10.6	29.1	70.2
20	0.416	0.825	10.653	11.513	78	58	60.6	6.2	3.1	17.5	9.5	27.0	72.1
21	0.439	0.740	10.739	10.244	73	63	61.1	6.2	1.6	14.4	13.4	27.8	71.2
22	0.433	0.767	10.761	11.052	75	59	61.8	6.2	1.8	14.6	12.2	26.8	72.2
23	0.466	0.808	10.618	11.436	76	56	61.9	5.7	2.4	16.2	10.9	27.1	72.1
24	0.400	1.010	10.776	11.291	77	56	62.6	6.1	2.2	17.2	8.7	25.9	73.3
25	0.425	0.832	10.591	11.184	73	51	59.1	6.6	2.7	20.1	8.3	28.4	70.7
26	0.432	0.747	10.895	10.426	75	61	61.8	6.5	1.6	14.9	11.6	26.5	72.5
27	0.496	0.876	10.801	11.427	75	59	61.4	6.7	2.2	16.3	9.4	25.7	73.2
28	0.485	0.735	10.878	10.382	75	57	62.9	6.1	1.4	14.7	11.1	25.8	73.2
29	0.423	0.642	10.701	10.067	73	64	62.0	5.9	1.5	14.0	12.9	26.9	72.0
30	0.457	0.862	10.665	11.446	77	59	61.1	5.4	2.5	18.0	8.4	26.4	72.3
31	0.502	0.936	10.810	11.637	75	54	61.9	6.0	2.3	16.9	7.8	24.7	74.0
32	0.503	0.914	10.794	11.635	75	58	60.8	6.3	2.2	17.6	7.9	25.5	73.1
33	0.486	0.935	10.833	11.510	75	53	61.9	6.0	2.1	17.9	7.6	25.5	73.3

Appendix D - SAS data

Minolta Color Analysis for the Clear flour

				The	SAS Sy	stem			19: 1	12 Moi	nday,	Jul y	9,	2007	1
				The RSI	REG Pro	cedure	!								
		Res	pon	se Surface	e for V	'ari abl	e MCco	ol or	-						
		Roo't R-Sc	: MS Juar		ari ati d	n	(3284 1252 0. 71 3. 92	254 145						
Regressi o	n		DF		I Sum quares	R-S	quare		F Va	al ue	Pr	> F			
Linear Quadratic Crossprod Total Mod	uct		5 5 10 20	0. <i>i</i> 1. :	663188 412988 355562 431738	0	. 4819 . 0543 . 1783 . 7145		(1. 05 0. 46 0. 75 1. 50	0. 0.	0219 8009 6715 2369			
1	Resi dı	ual		DF		Sum o Square		Mea	an So	quare					
-	Total	Error	-	12	2	. 17008	7		0. 18	30841					
Paramete	r I	DF		Esti mate		Stand Er	ard	t	Val u	ıe	Pr >	t			
Intercep a b c d e *a b*a b*b c c d *b d *c d *b d *c d *a e *b e *c e *e e *e	t	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-0. -0.	17. 750118 -0. 015981 0. 086262 0. 180868 -1. 159589 0. 795931 000001889 -0. 000226 0. 006467 000098611 -0. 000750 -0. 000654 0. 001745 -0. 008438 000041667 0. 022362 -0. 001802 -0. 017708 -0. 018583 0. 010937 0. 030699	0.	13. 397 0. 023 0. 491 0. 203 0. 898 1. 511 0. 000 0. 008 0. 000 0. 004 0. 001 0. 007 0. 019 0. 001 0. 035 0. 014 0. 053 0. 077	679 032 403 766 193 487 591 595 5236 725 375 886 779 088 339 772 438 1157		1.	57 18 39 29 53 59 53 59 54 16 16 16 16 16 16 16 16 16 16 16 16 16	O. O. O. O. O. O. O. O. O. O. O. O. O. O	2099 5125 8635 3914 2213 6080 9314 7090 4663 6838 8765 6428 0724 6425 9954 2700 3292 6263 2144 8404 6984			
				The	SAS Sy	stem			19: 1	12 Moi	nday,	Jul y	9,	2007	2
				The RSI	REG Pro	cedure	!								
Factor	·	DF		Sum of Squares	Me	an Squ	are	F	Valu	ie	Pr >	F			
a b c d e		6 6 6 6		1. 624477 1. 367927 0. 716811 1. 963922 1. 116161		0. 270 0. 227 0. 119 0. 327 0. 186	988 468 320		1. 5 1. 2 0. 6 1. 8 1. 0	26 56 31	0. 25 0. 34 0. 68 0. 17 0. 45	39 28 97			

The RSREG Procedure Canonical Analysis of Response Surface

Factor	Cri ti cal Val ue
a b c d	218. 222345 19. 454567 32. 945685 19. 705237
е	5. 514043

Predicted value at stationary point: 10.594366

			Ei genvectors		
Ei genval ues	a	b	С	d	е
0. 038218	-0. 010666	-0. 286617	-0. 202439	0. 371813	0. 859366
0. 020410	0. 055147	-0. 045658	0. 164829	0. 911458	-0. 370067
0. 004373	-0. 016636	0. 911403	-0. 343489	0. 169487	0. 149521
-0.000033603	0. 993830	-0. 012905	-0. 102012	-0. 041530	0.001968
-0. 004095	0. 094180	0. 291450	0. 896359	-0. 023411	0. 319656

Stationary point is a saddle point.

The SAS System

19: 12 Monday, July 9, 2007 4

The RSREG Procedure

Estimated Ridge of Minimum Response for Variable MCcolor

Radi us	Estimated Response	Standard Error
0 0. 100000 0. 200000 0. 300000 0. 400000 0. 500000 0. 600000 0. 700000 1. 000000 1. 100000 1. 200000 1. 300000 1. 400000 1. 500000 1. 600000 1. 700000 1. 800000 1. 900000	10. 730490 10. 711206 10. 692370 10. 673971 10. 656001 10. 638450 10. 621307 10. 604562 10. 588204 10. 572223 10. 556608 10. 541348 10. 526431 10. 511846 10. 497581 10. 483624 10. 469963 10. 456585 10. 443478 10. 430630 10. 418028	0. 157548 0. 157483 0. 157302 0. 157037 0. 156461 0. 156488 0. 156302 0. 156595 0. 157264 0. 158406 0. 160114 0. 162472 0. 165554 0. 169417 0. 174099 0. 179621 0. 185987 0. 193185 0. 201188
555000		3.207702

Estimated Ridge of Minimum Response for Variable MCcolor

Radi us	а	b	Factor Values c	d	е
0 0. 100000 0. 200000 0. 300000 0. 400000 0. 500000 0. 600000 0. 700000 0. 800000 1. 000000 1. 1000000	120. 000000 119. 998416 119. 996519 119. 994291 119. 991711 119. 988760 119. 985417 119. 981662 119. 977476 119. 972839 119. 967732	12. 000000 12. 037525 12. 075359 12. 113506 12. 151965 12. 190729 12. 229789 12. 269127 12. 308720 12. 348537 12. 388539 12. 428680	40. 000000 39. 991075 39. 980242 39. 967413 39. 952497 39. 935402 39. 916034 39. 894301 39. 870109 39. 843368 39. 813989 39. 781885	20. 000000 20. 052177 20. 105502 20. 159880 20. 215210 20. 271388 20. 328304 20. 385844 20. 443893 20. 502329 20. 561030 20. 619871	5. 000000 4. 923926 4. 849044 4. 775367 4. 702904 4. 631664 4. 561650 4. 492864 4. 425306 4. 358972 4. 293855 4. 2293855

```
1. 500000 119. 934596 12. 589368 39. 624713 20. 854104 3. 986081
```

The SAS System

19: 12 Monday, July 9, 2007

The RSREG Procedure

Estimated Ridge of Minimum Response for Variable MCcolor

Radi us	а	b	Factor Values c	d	е
1. 600000	119, 926362	12. 629177	39. 577919	20. 911749	3. 927958
1. 700000	119. 917574	12. 668652	39. 528037	20. 968783	3. 870921
1. 800000 1. 900000	119. 908231 119. 898335	12. 707687 12. 746169	39. 475043 39. 418930	21. 025089 21. 080557	3. 814939 3. 759979
2. 000000	119. 887892	12. 783982	39. 359705	21. 135080	3. 706006

data a;

```
input a b c d e MCclolr;
cards;
             40.0
                           7
120
      12
                    20
                                        10.93
60
      9
             47.5
                    22
                           6
                                        11.07
             40.0
                           5
120
      12
                    20
                                        10.46
                           5
120
             25.0
                    20
                                        10.52
      12
180
      15
             32.5
                    18
                           6
                                        10.74
             47.5
                                        11.27
60
      15
                    18
                           6
60
             32.5
                                        11.52
      9
                    18
                           6
120
      6
             40.0
                    20
                           5
                                        11.59
                           5
120
      12
             40.0
                    16
                                        11.84
180
             32.5
                    22
                           6
                                        11.47
      9
                           5
120
      12
             40.0
                    20
                                        11.11
180
      15
             47.5
                    18
                           4
                                        10.78
120
             40.0
                    20
                           5
                                        10.04
      12
60
             47.5
                           4
      15
                    22
                                        10.17
60
      15
             32.5
                    18
                           4
                                        10.42
120
      18
             40.0
                    20
                           5
                                        10.56
      12
             40.0
                    20
                           5
                                        10.08
0
             40.0
                    20
                           5
120
      12
                                        10.43
                           5
120
      12
             40.0
                    20
                                        10.92
             40.0
                           5
120
      12
                    20
                                        10.80
180
                           4
      15
             32.5
                    22
                                        10.35
180
             32.5
                           4
      9
                    18
                                        10.60
180
      9
             47.5
                    18
                           6
                                        11.12
120
      12
             40.0
                    20
                           3
                                        11.00
                           5
240
      12
             40.0
                    20
                                        11.55
180
      15
             47.5
                    22
                           6
                                        10.68
60
      9
             47.5
                    18
                           4
                                        11.16
120
                           5
      12
             40.0
                    24
                                        10.56
60
      9
             32.5
                    22
                           4
                                        9.85
60
      15
             32.5
                    22
                           6
                                        10.47
120
      12
             40.0
                    20
                           5
                                        11.13
                           5
120
      12
             55.0
                    20
                                        10.87
180
      9
             47.5 22
                                        11.28
;
```

proc rsreg;

model MCcolor=a b c d e/nocode;
ridge min radius = 0 to 2 by .1;
run;

Product Yield of 1st Clear Flour

The SAS System	22: 34 Saturday,	Jul v 7. 2007	1

The RSREG Procedure

Response Surface for Variable yield

Response Mean	6. 145455
Roo't MSE	0. 271645
R-Square	0. 9134
Coefficient of Variation	4. 4203

Regressi on	DF	Type I Sum of Squares	R-Square	F Value	Pr > F
Linear	5	3. 853333	0. 3770	10. 44	0. 0005
Quadratic	5	1. 202995	0. 1177	3. 26	0. 0434
Crossproduct	10	4. 280000	0. 4187	5. 80	0. 0028
Total Model	20	9. 336328	0. 9134	6. 33	0. 0011

Res	Resi dual		Sum of Squares	Mean Square	е
Tot	al Error	12	0. 885490	0. 07379	1
Parameter	DF	Estimate	Standard Error	t Value	Pr > t
Intercept a b c d e a*a b*a b*b c*a c*b c*c d*a d*b d*c d*c e*a e*b e*c e*e	1 1 1 1 1 1 1 1 1 1 1 1 1	12. 212908 -0. 036152 0. 751144 -0. 140131 -0. 262377 -0. 801961 0. 000010008 0. 001250 -0. 005719 0 -0. 005556 0. 001752 -0. 000104 -0. 022917 0. 007500 -0. 009743 0. 005000 -0. 008333 -0. 020000 0. 118750 -0. 151471	8. 558119 0. 015125 0. 313663 0. 129930 0. 574116 0. 965324 0. 000013726 0. 0005490 0. 000151 0. 003018 0. 000878 0. 000566 0. 011319 0. 004527 0. 012353 0. 001132 0. 022637 0. 009055 0. 033956 0. 049413	1. 43 -2. 39 2. 39 -1. 08 -0. 46 -0. 83 0. 73 3. 31 -1. 04 0. 00 -1. 84 1. 99 -0. 18 -2. 02 1. 66 -0. 79 4. 42 -0. 37 -2. 21 3. 50 -3. 07	0. 1791 0. 0341 0. 0338 0. 3020 0. 6558 0. 4223 0. 4799 0. 0062 0. 3181 1. 0000 0. 0905 0. 0694 0. 8570 0. 0657 0. 1235 0. 4456 0. 0008 0. 7192 0. 0474 0. 0044

The SAS System 22:34 Saturday, July 7, 2007 2

The RSREG Procedure

Factor	DF	Sum of Squares	Mean Square	F Value	Pr > F
a b	6	3. 791732 1. 827565	0. 631955 0. 304594	8. 56 4. 13	0. 0009 0. 0176
C	6	1. 480899	0. 304394	3. 34	0. 0176
d	6	1. 657565	0. 276261	3. 74	0. 0330
e	6	4. 807565	0. 801261	10. 86	0.0003

The SAS System 22:34 Saturday, July 7, 2007 3

The RSREG Procedure Canonical Analysis of Response Surface

Factor	Cri ti cal Val ue		
a	82. 329561		
b	7. 590234		

23. 235118 d 23. 425707 e 5. 491282

Predicted value at stationary point: 5.971684

			Ei genvectors		
Ei genval ues	а	b	С	d	е
0. 018216	0. 022719	-0. 459549	0. 086243	0. 832018	0. 297668
0. 002722	-0. 123485	-0. 112051	0. 972577	-0. 120526	-0. 108461
0. 000054435	0. 989473	0. 059368	0. 131666	-0. 008791	0. 002559
-0. 012423	-0. 070672	0. 879053	0. 160092	0. 420605	0. 140478
-0 173739	-0 013603	0 001067	0 060753	-0 340930	0 938024

Stationary point is a saddle point.

The SAS System 22:34 Saturday, July 7, 2007 4

The RSREG Procedure

Estimated Ridge of Maximum Response for Variable yield

Radi us	Estimated Response	Standard Error
0 0. 100000 0. 200000 0. 300000 0. 400000 0. 500000 0. 600000 0. 700000 1. 000000 1. 100000 1. 200000 1. 300000 1. 400000 1. 500000 1. 700000 1. 800000 1. 800000 1. 900000	6. 223529 6. 247398 6. 269270 6. 289595 6. 308820 6. 327325 6. 345402 6. 363262 6. 381054 6. 398883 6. 416823 6. 434928 6. 453239 6. 471784 6. 490587 6. 509666 6. 529035 6. 548704 6. 568683 6. 588978 6. 609597	0. 100639 0. 100582 0. 100432 0. 100234 0. 100038 0. 099889 0. 099887 0. 100056 0. 100417 0. 100981 0. 101777 0. 102837 0. 104190 0. 105865 0. 107888 0. 110283 0. 113070 0. 116265 0. 119881 0. 123928
2. 000000	0. 007077	0. 120720

Estimated Ridge of Maximum Response for Variable yield

			Factor Values		
Radi us	а	b	ractor varues C	d	е
naar as	G		9	G	Ü
0	120.000000	12.000000	40.000000	20. 000000	5.000000
0. 100000	120. 001631	12. 018797	39. 993382	19. 974965	4. 905272
0. 200000	120. 003145	12. 042118	39. 986923	19. 935764	4.815829
0. 300000	120. 004467	12. 069859	39. 980708	19. 882862	4.733530
0.400000	120. 005547	12. 101339	39. 974774	19. 818626	4. 659168
0. 500000	120. 006369	12. 135644	39. 969098	19. 746189	4. 592342
0.600000	120. 006944	12. 171954	39. 963623	19. 668332	4. 531965
0. 700000	120. 007296	12. 209669	39. 958285	19. 587068	4. 476806
0.800000	120. 007453	12. 248392	39. 953028	19. 503713	4. 425771
0. 900000	120. 007437	12. 287862	39. 947809	19. 419094	4. 377983
1. 000000	120. 007271	12. 327910	39. 942593	19. 333722	4. 332766
1. 100000	120. 006972	12. 368423	39. 937358	19. 247913	4. 289607
1. 200000	120. 006555	12. 409322	39. 932086	19. 161867	4. 248113
1. 300000	120. 006031	12. 450550	39. 926766	19. 075708	4. 207984
1. 400000	120. 005412	12. 492065	39. 921389	18. 989515	4. 168987
1. 500000	120. 004706	12. 533835	39. 915949	18. 903339	4. 130938

The SAS System 22:34 Saturday, July 7, 2007 5

The RSREG Procedure

Estimated Ridge of Maximum Response for Variable yield

Factor Values

1. 600000 120. 003920 12. 575832 39. 910444 18. 817211 4. 093693 1. 700000 120. 003063 12. 618035 39. 904870 18. 731152 4. 057133 1. 800000 120. 002138 12. 660426 39. 899227 18. 645172 4. 021164 1. 900000 120. 001152 12. 702989 39. 893515 18. 559278 3. 985709 2. 000000 120. 000109 12. 745712 39. 887734 18. 473474 3. 950702	Radi us	а	b	С	d	е
	1. 700000	120. 003063	12. 618035	39. 904870	18. 731152	4. 057133
	1. 800000	120. 002138	12. 660426	39. 899227	18. 645172	4. 021164
	1. 900000	120. 001152	12. 702989	39. 893515	18. 559278	3. 985709

data a;

```
input a b c d e yield;
cards;
120
           40.0 20
                         7
      12
                                      5.1
60
      9
            47.5
                   22
                         6
                                      5.6
120
      12
            40.0
                   20
                         5
                                      6.3
120
      12
            25.0
                   20
                         5
                                      6.9
180
      15
            32.5
                  18
                         6
                                      7.4
60
      15
            47.5
                  18
                         6
                                      4.7
60
      9
            32.5
                         6
                                      5.4
                  18
120
      6
            40.0
                   20
                         5
                                      5.8
120
            40.0
                  16
                         5
                                      6.0
      12
180
      9
            32.5
                   22
                         6
                                      6.4
120
      12
            40.0
                  20
                         5
                                      6.1
180
            47.5
                  18
                         4
      15
                                      7.1
            40.0
                         5
120
      12
                  20
                                      6.8
60
            47.5
                  22
                         4
                                      5.8
      15
60
      15
            32.5
                  18
                         4
                                      7.0
120
            40.0
                   20
                         5
      18
                                     6.2
                         5
0
      12
            40.0
                   20
                                      6.1
120
                         5
      12
            40.0
                  20
                                     5.9
                         5
120
      12
            40.0
                  20
                                      6.3
120
            40.0
                         5
                                      6.2
      12
                  20
180
      15
            32.5
                  22
                         4
                                      6.2
180
            32.5
      9
                  18
                         4
                                      6.2
            47.5
180
      9
                  18
                         6
                                      5.7
120
      12
            40.0
                   20
                         3
                                      6.1
            40.0
                         5
240
      12
                  20
                                      6.6
180
            47.5
                         6
      15
                  22
                                      6.5
60
      9
            47.5
                  18
                         4
                                      6.7
120
            40.0
                   24
                         5
      12
                                      6.1
60
      9
            32.5
                   22
                         4
                                      5.9
60
      15
            32.5
                   22
                         6
                                      5.4
120
      12
            40.0
                   20
                         5
                                      6.0
                         5
120
      12
            55.0
                  20
                                      6.3
180
            47.5 22
      9
                                      6.0
;
```

proc rsreg;

model yield=a b c d e/nocode; ridge max radius = 0 to 2 by .1; run;

Product Yield of Shorts, Red Dog, and Germ

The SAS System				18: 25	Monday,	Jul y	9,	2007	1			
			The RSR	EG Proce	edure							
		Response	Surface	for Var	iable RGS	Syi el	d					
		Response M Root MSE R-Square Coefficier		riation		. 2545 . 0397 0. 87 6. 39	779 706					
Regressi oı	n	DF	Type of Sq		R-Square	е	F Valu	ue Pr	` > F			
Linear Quadratic Crossprod Total Mode		5 5 10 20	19. 6. 46. 2	05000 28142 35000 68142	0. 2135 0. 1958 0. 4612 0. 8706	8 2	3. 6 3. 6 4. 2 4. 0	53 0. 28 0.	0236 0312 0102 0083			
I	Resi dua	al	DF	_	Sum of quares	Mea	an Squa	are				
-	Total E	Error	12	12. 9	73676		1. 0811	140				
Paramete	r DF	Es	sti mate	S	Standard Error	t	Val ue	Pr >	· t			
Intercept a b c d e a*a b*a b*a b*b c*a c*b d*a d*b d*c d*a d*b d*c d*a e e e e e e e e e e e e e e e e e e e	t 11 11 11 11 11 11 11 11 11 11 11 11 11	0. 3. 3. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	871977 064906 468464 733366 785907 167157 0026144 002778 063154 000972 033333 001229 004688 066667 009167 129596 007292 083333 141667 043750 181618	0. 00 0. 00 0. 00 0. 00 0. 00 0. 00 0. 00 0. 00	2. 758046 0. 057896 1. 200613 0. 497336 2. 197554 3. 694986 00052538 0. 001444 0. 021015 0. 000578 0. 011553 0. 003362 0. 003362 0. 043324 0. 017330 0. 047284 0. 0044332 1. 086648 0. 034659 0. 129972 0. 189138		-2. 71 1. 12 2. 89 1. 47 2. 63 0. 86 0. 50 1. 92 -3. 01 1. 68 -2. 89 0. 37 -2. 16 -1. 54 0. 53 -2. 74 -1. 68 0. 96 -4. 09 0. 34 0. 96	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	0189 2842 0136 1661 0219 4082 0785 0110 1182 0137 7211 0514 1498 6065 0179 1182 3552 0015 7422 3559			
			The	SAS Syst	em		18: 25	Monday,	Jul y	9,	2007	2
			The RSR	EG Proce	edure							
Factor	DF	· (Sum of Squares	Mear	n Square	F	Val ue	Pr >	F			
a b c d e	6 6 6	26. 31. 5 19.	496879 605212 306879 108824 651046	4 5 3	5. 082813 I. 434202 5. 217813 B. 184804 I. 275174		4. 70 4. 10 4. 83 2. 95 3. 95	0. 01 0. 01 0. 01 0. 05 0. 02	80 00 26			
			The	SAS Syst	em		18: 25	Monday,	Jul y	9,	2007	3
		Canoni cal		EG Proce is of Re	edure Esponse Su	urfac	ce					
		į	actor	Cr	ri ti cal Val ue							

70. 991713 9. 645719

c 45. 096513 d 21. 088277 e 5. 541151

Predicted value at stationary point: 16.478209

			Ei genvectors		
Ei genval ues	a	b	С	d	е
0. 213974	-0.016067	0. 154727	-0. 321942	0. 040209	0. 933026
0. 000174 -0. 021208	0. 996861 0. 062951	0. 048381 -0. 148585	-0. 052404 0. 915885	-0. 033546 0. 150726	-0. 007493 0. 335256
-0. 055075 -0. 147741	-0. 044592 0. 007681	0. 886280 0. 407614	0. 230690 -0. 039303	-0. 395843 0. 904349	-0. 051084 -0. 119998

Stationary point is a saddle point.

The SAS System 18:25 Monday, July 9, 2007 4

The RSREG Procedure

Estimated Ridge of Minimum Response for Variable RGSyield

Radi us	Esti mated Response	Standard Error
0 0. 100000 0. 200000 0. 300000 0. 400000 0. 500000 0. 700000 0. 700000 1. 000000 1. 100000 1. 300000 1. 400000 1. 500000 1. 600000 1. 700000 1. 900000	16. 794118 16. 758412 16. 723591 16. 688732 16. 653038 16. 615911 16. 576926 16. 535795 16. 492318 16. 446353 16. 397800 16. 346586 16. 292656 16. 235967 16. 176487 16. 114190 16. 049056 15. 981068 15. 9810213	0. 385216 0. 385037 0. 384582 0. 383993 0. 383385 0. 382402 0. 382138 0. 382098 0. 382343 0. 382938 0. 383957 0. 385476 0. 390340 0. 393852 0. 398197 0. 403456 0. 409707
2.000000	15. 759858	0. 425464

Estimated Ridge of Minimum Response for Variable RGSyield

			Factor Values		
Radi us	а	b	С	d	е
0 0.100000 0.200000 0.300000 0.400000 0.500000 0.600000 0.700000 0.900000 1.000000 1.100000 1.200000 1.300000 1.400000	120. 000000 119. 996152 119. 992105 119. 988259 119. 984881 119. 979775 119. 977953 119. 976516 119. 975397 119. 974537 119. 974537 119. 973889 119. 973889 119. 973091	12. 000000 11. 992345 11. 990127 11. 994087 12. 003998 12. 019049 12. 038294 12. 060888 12. 086150 12. 113551 12. 142683 12. 173233 12. 204955 12. 271189	40. 000000 39. 989813 39. 973097 39. 952324 39. 930069 39. 908096 39. 887294 39. 867982 39. 850185 39. 833805 39. 818694 39. 804705 39. 791695 39. 779540 39. 768133	20. 000000 20. 054802 20. 122897 20. 202063 20. 288954 20. 380584 20. 474874 20. 570543 20. 666840 20. 763339 20. 859799 20. 956089 21. 052142 21. 147925 21. 243429	5. 000000 4. 917419 4. 845040 4. 783841 4. 732847 4. 690121 4. 653710 4. 622033 4. 593913 4. 568498 4. 545173 4. 523490 4. 503116 4. 483802 4. 465357
1. 500000	119. 972788	12. 305425	39. 757380	21. 338657	4. 447635

The SAS System
The RSREG Procedure

Estimated Ridge of Minimum Response for Variable RGSyield

Factor Values

18: 25 Monday, July 9, 2007 5

```
Radi us
                               а
                                                 b
                                                                  С
                                                                                    d
      1. 600000
                     119. 972776
119. 972840
119. 972969
                                        12. 340267
12. 375632
12. 411454
                                                          39. 747202
                                                                           21. 433618
                                                          39. 737530
39. 728308
                                                                           21. 528325
      1.700000
      1.800000
                                                                           21.622791
      1.900000
                      119. 973155
                                        12.447676
                                                          39. 719484
                                                                           21.717034
                                                                           21.811067
      2.000000
                      119.973390
                                        12. 484251
                                                          39.711017
data a;
input a b c d e RGSyield;
cards;
120
        12
                40.0
                        20
                                7
                                                 18
60
        9
                47.5
                        22
                                                 16.5
                                6
120
        12
                40.0
                        20
                                5
                                                 15.8
120
        12
                25.0
                        20
                                5
                                                 16.7
180
        15
                32.5
                        18
                                6
                                                 20.1
                                6
60
        15
                47.5
                        18
                                                 14.3
60
                32.5
                                                 16.6
        9
                        18
                                6
120
        6
                40.0
                        20
                                5
                                                 14.7
120
                40.0
                                5
                                                 14.9
        12
                        16
180
        9
                32.5
                        22
                                6
                                                 14.5
120
        12
                40.0
                        20
                                5
                                                 15.7
                47.5
                                4
                                                 19.3
180
        15
                        18
                                5
120
        12
                40.0
                        20
                                                 15.9
                47.5
                                4
60
        15
                        22
                                                 13.9
60
                32.5
                                4
                                                 14.7
        15
                        18
120
        18
                40.0
                        20
                                5
                                                 14.5
0
        12
                40.0
                        20
                                5
                                                 14.4
                                5
120
        12
                40.0
                        20
                                                 17.1
```

18.5

17.5 14.4

14.6

16.2

17.2

20.1

14.9

16.3

14.7

14.0

18.0

16.9

17.6

17.9

5

5

4

4

6

3

5

6

4

5

4

6

5

5

4

е

4.430518

4. 413914

4. 397749

4. 381962

4.366504

proc rsreg;

120

120

180

180

180

120

240

180

120

60

60

120 120

180

;

60

12

12

15

9

9

12

12

15

9

12

9

15

12

12

9

40.0

40.0

32.5

32.5

47.5

40.0

40.0

47.5

47.5

40.0

32.5

32.5

40.0

55.0

47.5

20

20

22

18

18

20

20

22

18

24

22

22

20

20

22

model RGSyield=a b c d e/nocode;
ridge min radius = 0 to 2 by .1;
run;

Hardness of Tempered Wheat

The SAS System	20: 58 Saturday,	July 7.	2007	1
THE SHE SYSTEM	zo. so saturday,	July 1,	2007	

The RSREG Procedure

Response Surface for Variable hard

Response Mean	61. 974848
Roo't MSE	2. 131031
R-Square	0. 7419
Coefficient of Variation	3. 4385

Regressi on	DF	Type I Sum of Squares	R-Square	F Value	Pr > F
Li near	5	87. 569854	0. 4147	3. 86	0. 0257
Quadrati c	5	14. 612785	0.0692	0.64	0. 6716
Crossproduct	10	54. 464063	0. 2579	1. 20	0. 3773
Total Model	20	156. 646701	0. 7419	1. 72	0. 1668

Resi dual	DF	Sum of Squares	Mean Square
Total Error	12	54. 495523	4. 541294

Parameter	DF	Esti mate	Standard Error	t Value	Pr > t
Intercept a b c d e a*a b*a b*b c*a c*b c*c d*b	DF 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-23. 376597 0. 124934 5. 687014 0. 753583 -0. 616979 13. 240833 -0. 000056424 -0. 000823 -0. 049097 -0. 00601 -0. 046528 -0. 000011111 -0. 002911 -0. 162604 0. 024958	Error 67. 137764 0. 118658 2. 460661 1. 019292 4. 503898 7. 572891 0. 000108 0. 002960 0. 043071 0. 001184 0. 023678 0. 006891 0. 004440 0. 088793 0. 035517	-0. 35 1. 05 2. 31 0. 74 -0. 14 1. 75 -0. 52 -0. 28 -1. 14 -0. 51 -1. 97 -0. 00 -0. 66 -1. 83 0. 70	0. 7337 0. 3131 0. 0394 0. 4739 0. 8933 0. 1059 0. 6098 0. 7857 0. 2766 0. 6207 0. 0730 0. 9987 0. 5243 0. 0920 0. 4956
d*d	1	0. 082031	0. 096910	0. 85	0. 4139
e*a	1	-0. 000448	0. 008879	-0. 05	0. 9606
e*b	1	0. 108958	0. 177586	0. 61	0. 5510
e*c	1	-0. 090083	0. 071034	-1. 27	0. 2288
e*d	1	-0. 329687	0. 266379	-1. 24	0. 2395
e*e	1	-0. 365625	0. 387638	-0. 94	0. 3642

The SAS System 20:58 Saturday, July 7, 2007 2

The RSREG Procedure

Factor	DF	Sum of Squares	Mean Square	F Value	Pr > F
a b	6	29. 683591 46. 150774	4. 947265 7. 691796	1. 09 1. 69	0. 4216 0. 2058
C	6	67. 702691	11. 283782	2. 48	0. 2038
d	6	37. 512935	6. 252156	1. 38	0. 2995
е	6	29. 890019	4. 981670	1. 10	0. 4178

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The RSREG Procedure Canonical Analysis of Response Surface

Factor	Cri ti cal Val ue
a	769. 096465
b	-14. 239580

c 277. 358286 d -40. 074826 e -0. 585803

Predicted value at stationary point: 97.166914

Ei genval ues	а	b	Ei genvectors c	d	е
0. 182169	-0. 005818	-0. 389392	0. 184214	0. 847887	-0. 309019
-0. 000037060	0. 989784	-0. 021407	0. 136565	-0. 034548	-0. 005044
-0. 000762	-0. 142055	-0. 065858	0. 956579	-0. 245255	-0. 017029
-0. 089090	0. 010558	0. 915932	0. 156849	0. 364005	-0. 062096
-0. 425038	0. 001508	-0. 068169	0. 088152	0. 295371	0. 948860

Stationary point is a saddle point.

The SAS System 20:58 Saturday, July 7, 2007 4

The RSREG Procedure

Estimated Ridge of Maximum Response for Variable hard

Radi us	Estimated Response	Standard Error
0 0. 100000 0. 200000 0. 300000 0. 400000 0. 500000 0. 600000 0. 700000 1. 000000 1. 100000 1. 200000 1. 300000 1. 400000 1. 500000 1. 600000 1. 700000 1. 800000 1. 900000	62. 471667 62. 543814 62. 612978 62. 680311 62. 746894 62. 813664 62. 881379 62. 950629 63. 021865 63. 095429 63. 171581 63. 250517 63. 332392 63. 417325 63. 505409 63. 596721 63. 691321 63. 789259 63. 890574 63. 995302	0. 789503 0. 789134 0. 788157 0. 786820 0. 785391 0. 784131 0. 783289 0. 783112 0. 783742 0. 789142 0. 794233 0. 810683 0. 822572 0. 837233 0. 854882 0. 875708 0. 899866 0. 927476
2. 000000	64. 103470	0. 958626

Estimated Ridge of Maximum Response for Variable hard

			Factor Values		
Radi us	а	b	С	d	е
0 0. 100000 0. 200000 0. 300000 0. 400000 0. 500000 0. 700000 0. 700000 0. 900000 1. 100000 1. 200000	120.000000 120.002425 120.005061 120.007810 120.010566 120.013246 120.015794 120.018186 120.022491 120.022491 120.024424 120.026228 120.027918	12. 000000 11. 979972 11. 963920 11. 953377 11. 949174 11. 951345 11. 959358 11. 972411 11. 989662 12. 010346 12. 033816 12. 059548 12. 087122	40. 000000 40. 023161 40. 045702 40. 066438 40. 084379 40. 098952 40. 110005 40. 117689 40. 122315 40. 124250 40. 123854 40. 121458 40. 117346	20. 000000 19. 954919 19. 897291 19. 828438 19. 750612 19. 666297 19. 577676 19. 486415 19. 393671 19. 300206 19. 206505 19. 112860 19. 019447	5. 000000 5. 083811 5. 161353 5. 232202 5. 296632 5. 355398 5. 409439 5. 459660 5. 506833 5. 551578 5. 594378 5. 635608 5. 675557
1. 300000 1. 400000	120. 029508 120. 031008	12. 116204 12. 146532	40. 111764 40. 104916	18. 926362 18. 833654	5. 714449 5. 752461
1. 500000	120. 032431	12. 177895	40. 096975	18. 741342	5. 789733

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The RSREG Procedure

Estimated Ridge of Maximum Response for Variable hard

Factor Values

Radi us	a	b	С	d	е
1. 600000	120. 033784	12. 210125	40. 088085	18. 649426	5. 826376
1. 700000	120. 035075	12. 243087	40. 078368	18. 557896	5. 862481
1. 800000	120. 036313	12. 276672	40. 067926	18. 466736	5. 898122
1. 900000	120. 037501	12. 310789	40. 056845	18. 375927	5. 933359
2. 000000	120. 038646	12. 345366	40. 045199	18. 285447	5. 968243

```
data d;
input a b c d e hard;
cards;
             40.0
120
                    20
                           7
                                         62.79
      12
              47.5
60
       9
                    22
                                         63.69
120
      12
              40.0
                    20
                           5
                                         60.59
120
       12
              25.0
                    20
                           5
                                         59.70
180
       15
              32.5
                    18
                           6
                                         66.23
60
       15
             47.5
                    18
                           6
                                         61.26
60
       9
             32.5
                    18
                           6
                                         59.03
120
                    20
                           5
       6
              40.0
                                         62.12
                           5
120
       12
              40.0
                    16
                                         68.10
180
             32.5
       9
                    22
                           6
                                         62.17
120
              40.0
       12
                    20
                           5
                                         63.53
             47.5
180
       15
                    18
                           4
                                         61.50
120
       12
             40.0
                    20
                           5
                                         59.81
60
       15
             47.5
                    22
                           4
                                         59.95
60
       15
             32.5
                    18
                           4
                                         58.04
120
       18
             40.0
                    20
                           5
                                         61.00
0
       12
             40.0
                    20
                           5
                                         61.32
120
              40.0
                    20
                           5
                                         64.95
       12
120
       12
             40.0
                    20
                           5
                                         63.52
120
       12
             40.0
                    20
                           5
                                         60.79
180
       15
             32.5
                    22
                           4
                                         59.43
180
       9
             32.5
                    18
                           4
                                         59.55
180
       9
              47.5
                    18
                           6
                                         64.46
120
       12
              40.0
                    20
                           3
                                         60.94
240
              40.0
                    20
                           5
       12
                                         63.71
180
              47.5
                           6
       15
                    22
                                         60.32
60
       9
              47.5
                    18
                           4
                                         60.77
120
             40.0
                    24
                           5
       12
                                         61.18
60
       9
             32.5
                    22
                           4
                                         58.73
60
       15
             32.5
                    22
                           6
                                         59.57
             40.0
120
       12
                    20
                           5
                                         62.40
             55.0
                           5
120
       12
                    20
                                         66.95
180
       9
             47.5
                    22
                                         67.07
;
proc rsreg;
model hard=a b c d e/nocode;
ridge max radius = 0 to 2 by .1;
run;
```

Stepwise Regression Analysis for Red Dog, Germ, and Shorts – Step 1

RSreg 18: 20 Fri day, October 12, 2007 1

The RSREG Procedure

Response Surface for Variable RGSyield

Response Mean	16. 254545
Roo't MSE	1. 039779
R-Square	0. 8706
Coefficient of Variation	6. 3968
Sum of Squared Residuals	12. 973676471
Predicted Residual SS (PRESS)	181. 83982772

Regressi on	DF	Type I Sum of Squares	R-Square	F Value	Pr > F
Li near Quadrati c Crossproduct Total Model	uadrati c 5 19.628142 rossproduct 10 46.235000		0. 2135 0. 1958 0. 4612 0. 8706	3. 96 3. 63 4. 28 4. 04	0. 0236 0. 0312 0. 0102 0. 0083
Resi dual	DF	Sum of Squares	Mean Square	F Value	Pr > F
Lack of Fit Pure Error Total Error	6 6 12	6. 479391 6. 494286 12. 973676	1. 079898 1. 082381 1. 081140	1. 00	0. 5011

RSreg 18: 20 Fri day, October 12, 2007 2

The RSREG Procedure

Parameter	DF	Estimate	Standard Error	t Value	Pr > t	
Intercept a b c d e a*a b*a b*b c c*b c c*c d*a d*c d*c d*c d*e e e e e e e e e	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-88. 871977 0. 064906 3. 468464 0. 733366 5. 785907 3. 167157 0. 000026144 0. 002778 -0. 063154 0. 000972 -0. 033333 0. 001229 -0. 004688 -0. 066667 0. 009167 -0. 129596 -0. 007292 0. 083333 -0. 141667 0. 043750 0. 181618	32. 758046 0. 057896 1. 200613 0. 497336 2. 197554 3. 694986 0. 000052538 0. 001444 0. 021015 0. 000578 0. 011553 0. 003362 0. 002166 0. 043324 0. 017330 0. 047284 0. 004332 0. 086648 0. 034659 0. 129972 0. 189138	-2. 71 1. 12 2. 89 1. 47 2. 63 0. 86 0. 50 1. 92 -3. 01 1. 68 -2. 89 0. 37 -2. 16 -1. 54 0. 53 -2. 74 -1. 68 0. 96 -4. 09 0. 34 0. 96	0. 0189 0. 2842 0. 0136 0. 1661 0. 0219 0. 4082 0. 6277 0. 0785 0. 0110 0. 1182 0. 0137 0. 7211 0. 0514 0. 1498 0. 6065 0. 0179 0. 1182 0. 3552 0. 0015 0. 7422 0. 3559	
Factor	DF	Sum of Squares	Mean Square	F Value	Pr > F	
a b c d e	6 6 6 6	30. 496879 26. 605212 31. 306879 19. 108824 25. 651046	5. 082813 4. 434202 5. 217813 3. 184804 4. 275174	4. 70 4. 10 4. 83 2. 95 3. 95	0. 0110 0. 0180 0. 0100 0. 0526 0. 0205	

RSreg 18: 20 Fri day, October 12, 2007 3

The RSREG Procedure Canonical Analysis of Response Surface

Factor	Cri ti cal Val ue
a b c d	70. 991713 9. 645719 45. 096513 21. 088277
е	5. 541151

Predicted value at stationary point: 16.478209

Ei genval ues	а	b	Ei genvectors c	d	е
0. 213974	-0. 016067	0. 154727	-0. 321942	0. 040209	0. 933026
0. 000174	0. 996861	0. 048381	-0. 052404	-0. 033546	-0. 007493
-0. 021208	0. 062951	-0. 148585	0. 915885	0. 150726	0. 335256
-0. 055075	-0. 044592	0. 886280	0. 230690	-0. 395843	-0. 051084
-0. 147741	0. 007681	0. 407614	-0. 039303	0. 904349	-0. 119998

Stationary point is a saddle point.

RSreg 18: 20 Fri day, October 12, 2007 4

The RSREG Procedure

Estimated Ridge of Minimum Response for Variable RGSyield

Radi us	Esti mated Response	Standard Error
0 0. 100000 0. 200000 0. 300000 0. 400000 0. 500000 0. 600000 0. 700000 1. 000000 1. 100000 1. 200000 1. 400000 1. 500000 1. 600000 1. 700000 1. 800000	16. 794118 16. 758412 16. 723591 16. 688732 16. 653038 16. 615911 16. 576926 16. 535795 16. 492318 16. 446353 16. 397800 16. 346586 16. 292656 16. 235967 16. 176487 16. 176487 16. 174190 16. 049056 15. 981068 15. 981068	0. 385216 0. 385037 0. 384582 0. 383993 0. 382835 0. 382402 0. 3822098 0. 382938 0. 382938 0. 385476 0. 387576 0. 390340 0. 393852 0. 398197 0. 403456 0. 409707
1. 900000 2. 000000	15. 836480 15. 759858	0. 417021 0. 425464

Estimated Ridge of Minimum Response for Variable RGSyield

Radi us	а	b	Factor Values c	d	e
0 0. 100000 0. 200000 0. 300000 0. 400000 0. 500000 0. 700000 0. 800000 1. 000000 1. 200000 1. 200000	120. 000000 119. 996152 119. 992105 119. 988259 119. 984881 119. 979775 119. 977953 119. 976516 119. 975397 119. 974537 119. 973889 119. 973889	12. 000000 11. 992345 11. 990127 11. 994087 12. 003998 12. 019049 12. 038294 12. 060888 12. 086150 12. 113233 12. 173233 12. 204955	40. 000000 39. 989813 39. 973097 39. 952324 39. 930069 39. 908096 39. 887294 39. 867982 39. 850185 39. 833805 39. 818694 39. 804705	20. 000000 20. 054802 20. 122897 20. 202063 20. 288954 20. 380584 20. 474874 20. 570543 20. 666840 20. 763339 20. 859799 20. 956089 21. 052142	5. 000000 4. 917419 4. 845040 4. 783841 4. 732847 4. 690121 4. 653710 4. 622033 4. 593913 4. 568498 4. 545173 4. 523490 4. 503116
1. 300000 1. 400000 1. 500000	119. 973091 119. 972888 119. 972788	12. 237658 12. 271189 12. 305425	39. 779540 39. 768133 39. 757380	21. 147925 21. 243429 21. 338657	4. 483802 4. 465357 4. 447635

RSreg 18: 20 Fri day, October 12, 2007 5

The RSREG Procedure

Estimated Ridge of Minimum Response for Variable RGSyield

Radi us	а	b	Factor Values c	d	е
1. 600000	119. 972776	12. 340267	39. 747202	21. 433618	4. 430518
1. 700000	119. 972840	12. 375632	39. 737530	21. 528325	4. 413914
1. 800000	119. 972969	12. 411454	39. 728308	21. 622791	4. 397749
1. 900000	119. 973155	12. 447676	39. 719484	21. 717034	4. 381962
2. 000000	119. 973390	12. 484251	39. 711017	21. 811067	4. 366504

Regressi on

The REG Procedure Model: MODEL1 Dependent Variable: RGSyield

Number of Observations Read Number of Observations Used 33

Analysis of Variance

Source		DF	Sum of Squares	Mean Square	F Value	Pr > F
Model Error Corrected To	tal	20 12 32	87. 26814 12. 97368 100. 24182	4. 36341 1. 08114	4. 04	0.0083
	Root MSE Dependent M Coeff Var	ean	1. 03978 16. 25455 6. 39685	R-Square Adj R-Sq	0. 8706 0. 6549	

Parameter Estimates

Vari abl e	DF	Parameter Estimate	Standard Error	t Value	Pr > t
Intercept	1	-88. 87198	32. 75805	-2. 71	0. 0189
a '	1	0. 06491	0.05790	1. 12	0. 2842
b	1	3. 46846	1. 20061	2. 89	0. 0136
С	1	0. 73337	0. 49734	1. 47	0. 1661
d	1	5. 78591	2. 19755	2. 63	0. 0219
е	1	3. 16716	3. 69499	0. 86	0. 4082
a2	1	0. 00002614	0. 00005254	0. 50	0. 6277
b2	1	-0. 06315	0. 02102	-3. 01	0. 0110
c2	1	0. 00123	0.00336	0. 37	0. 7211
d2	1	-0. 12960	0. 04728	-2.74	0. 0179
e2	1	0. 18162	0. 18914	0. 96	0. 3559
ab	1	0. 00278	0. 00144	1. 92	0. 0785
ac	1	0.00097222	0. 00057765	1. 68	0. 1182
ad	1	-0. 00469	0. 00217	-2. 16	0. 0514
ae	1	-0. 00729	0. 00433	-1. 68	0. 1182
bc	1	-0. 03333	0. 01155	-2.89	0. 0137
bd	1	-0. 06667	0. 04332	-1. 54	0. 1498
be	1	0. 08333	0. 08665	0. 96	0. 3552
cd	1	0. 00917	0. 01733	0. 53	0. 6065
ce	1	-0. 14167	0. 03466	-4. 09	0. 0015
de	1	0. 04375	0. 12997	0. 34	0. 7422

Regressi on/sel ecti on=stepwi se

The REG Procedure Model: MODEL1 Dependent Variable: RGSyield

Number of Observations Read 33 Number of Observations Used 33

Stepwise Selection: Step 1

Variable ac Entered: R-Square = 0.1711 and C(p) = 47.8579

Analysis of Variance

Source	DF	Sum of Squares	Mea Squar		al ue	Pr > F	
Model Error Corrected Total	1 31 32	17. 14766 83. 09416 100. 24182	17. 1476 2. 6804	-	6. 40	0. 0167	
Vari abl e	Parameter Estimate	Standard Error	Type II SS	F Value	Pr > F		
Intercept ac	14. 68766 0. 00032644	0. 68191 0. 00012906	1243. 52954 17. 14766	463. 92 6. 40	<. 0001 0. 0167		
Bounds on condition number: 1, 1							

All variables left in the model are significant at the 0.1500 level. No other variable met the 0.1500 significance level for entry into the model.

Summary of Stepwise Selection

Step		Variable Removed			Model R-Square	C(p)	F Value	Pr > F
1	ac		1	0. 1711	0. 1711	47. 8579	6. 40	0. 0167

Regressi on/sel ecti on=R^2

The REG Procedure Model: MODEL1 Dependent Variable: RGSyield

R-Square Selection Method

Number of Observations Read 33 Number of Observations Used 33

Number in Model	R-Square	Variables in Model
1 1 1 1 1 1 1 1 1 1 1 1 1 1	0. 1711 0. 1600 0. 1544 0. 1501 0. 1492 0. 1071 0. 0349 0. 0293 0. 0282 0. 0240 0. 0224 0. 0152 0. 0084 0. 0073 0. 0041 0. 0032 0. 0028 0. 0007 0. 0001 0. 0000	ac ab a2 a ae ad d2 d e2 e be cc cc cd bb bb bb
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0. 2093 0. 2059 0. 2030 0. 2004 0. 1993 0. 1951 0. 1949 0. 1936 0. 1935 0. 1894 0. 1891	a ad d2 ac ab bd d ac e2 ac e ac d2 ab b2 ab ac be d ab a2 d2

```
2 0. 1890 ac cd
2 0. 1882 e2 ab
2 0. 1849 a d2
2 0. 1841 d2 ae
2 0. 1840 e ab
2 0. 1837 d a2
```

The REG Procedure Model: MODEL1 Dependent Variable: RGSyield

R-Square Selection Method

Number in Model	R-Square	Variables in Model
2 2 2	0. 1836 0. 1828 0. 1828	ac ad ab ac a2 e2
333333333333333333333333333333333333333	0. 2932 0. 2789 0. 2744 0. 2695 0. 2679 0. 2594 0. 2571 0. 2497 0. 2485 0. 2476 0. 2459 0. 2451 0. 2432 0. 2421 0. 2411 0. 2408 0. 2379 0. 2375	b2 ab ad d d2 ac b b2 ab b b2 ac d d2 ab d a2 d2 a d d2 d d2 ae b a2 b2 a b b2 b b2 ae ab bd be b ab ad c ac ad d d2 ad a ad de ab ad bd b2 ab be c2 ac ad a e2 ad
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0. 3791 0. 3716 0. 3674 0. 3659 0. 3616 0. 3599 0. 3582 0. 3568 0. 3523 0. 3499 0. 3481 0. 3471 0. 3456 0. 3415 0. 3399 0. 3364	c e ac ce c e ab ce c e2 ac ce c e a2 ce a c e ce c e2 ab ce c e2 ab ce c e2 ac ce c a2 e2 ce e c2 ac ce a c e2 e2 e c2 ac ce a c e2 ce e c2 ac ce a c e2 ce e2 ac ad ce c2 e2 ab ce a2 c2 e2 ce b b2 ab ad e c2 ab ce a c2 e2 ce c ea c2 e2 ce c ea c2 e2 ce c ea c2 e2 ce
		Regression/selection=R^2

Regressi on/sel ecti on=R^2

The REG Procedure Model: MODEL1 Dependent Variable: RGSyield

Number in Model	R-Square	Variables in Model
4	0. 3354	b2 ab ad be
4	0. 3337	e ac ad ce
5	0. 4493	c e ac ad ce
5	0. 4376	c e2 ac ad ce
5	0. 4356	c2 e2 ac ad ce
5	0. 4331	e c2 ac ad ce
5	0. 4305	e d2 ac cd ce

```
0. 4265
0. 4215
0. 4213
0. 4212
0. 4209
                                                                      d2 ac cd ce de
c e ac ae ce
e d2 ab cd ce
d2 e2 ac cd ce
a c e ad ce
55555555555555
                               0. 4174
0. 4156
                                                                       d2 ab cd ce de
                                                                      c d2 ac ce de
e a2 d2 cd ce
                                0. 4148
                               0.4145
                                                                       c e ab bd ce
                               0. 4140
0. 4129
                                                                      c e d2 ac ce
d2 e2 ab cd ce
                                                                      a e d2 cd ce
a2 d2 cd ce de
a c e2 ad ce
a2 d2 e2 cd ce
                               0. 4113
0. 4104
                                0.4092
5
                               0.4090
                                                                    c e ab ad bc ce
c e b2 ab ad ce
c e2 ab ad bc ce
c b2 e2 ab ad ce
c d e d2 ac ce
b c e b2 ab ce
c e2 ab bc bc ce
b c e ab bc bc ce
c b2 e2 ab bc ce
c d e d2 ab ce
c d e d2 ab ce
c b2 e2 ab bc ce
c b2 e2 ab bc ce
c b2 e2 ab ac ce
b c e b2 ac ce
b2 c2 e2 ab ad ce
c e b2 ab ae ce
e d2 ab ad be ce
c b2 ab ad be ce
c b2 ab ad be ce
c e b2 ab ab ce
                               0. 5061
0. 5047
6
6
                               0. 4944
0. 4906
6
6
                               0. 4870
0. 4859
0. 4822
666666666
                               0. 4822
0. 4801
0. 4796
0. 4794
0. 4775
0. 4764
0. 4764
0. 4750
0. 4750
 6
 6
 6
                                                                      c e b2 ab be ce
c e ab bc be ce
b c e ac bc ce
                               0.4730
 6
                               0. 4726
0. 4717
```

The REG Procedure Model: MODEL1 Dependent Variable: RGSyield

Number in Model	R-Square	Variables in Model
6	0. 4717	d e d2 ac cd ce
7 7 7 7 7 7 7 7 7 7 7 7	0. 5757 0. 5673 0. 5573 0. 55567 0. 55566 0. 5530 0. 5519 0. 5501 0. 5501 0. 5498 0. 5483 0. 5477 0. 5477 0. 5479 0. 5383 0. 5382 0. 5382 0. 5356 0. 5355 0. 5354	b c e b2 ab bc ce b c e b2 ac bc ce c e2 ab ad bc be ce b c b2 e2 ab bc ce c b2 e2 ab ad be ce b c e b2 ab ad ce c e b2 ab ad be ce b c e b2 ab ad be ce b c e a2 b2 bc ce c e ab ad bc be ce a b c e b2 bc ce b c e b2 ac bc ce b c b2 e2 ac bc ce b c b2 e2 ac bc ce b c e b2 ac ad ce b c e ac ad bc ce b c e ac ad bc ce c e2 ac ad bc be ce b c e2 ac ad ce b c e2 ac ad bc ce c e2 ac ad bc be ce b c b2 d2 ab cd ce b b2 d2 ab cd ce c b2 ab ad bc ce c c2 ac ad bc ce c c2 ac ad bc ce c c2 ac ad bc ce c c2 ac ad bc ce c c2 ac ad bc ce c c2 ac ad bc ce c c2 ac ad bc ce c c2 ac ad bc ce c c2 ac ad bc ce c c2 ac ad bc ce c c2 ac ad bc ce c c2 ac ad bc ce c c2 ac ad bc ce c c2 ac ad bc ce
8 8 8 8 8 8 8 8 8	0. 6428 0. 6375 0. 6237 0. 6184 0. 6166 0. 6156 0. 6146 0. 6109 0. 6096 0. 6091 0. 6072	b c e b2 ab ad bc ce b c e b2 ac ad bc ce b c b2 e2 ab ad bc ce b c b2 e2 ac ad bc ce b c b2 e2 ac ad bc ce b c e b2 ab ae bc ce b c e b2 ab bc bd ce b c b2 d2 ab bc ce de b c e b2 d2 ab bc ce b c e b2 ac ae bc ce a b c e b2 ac bc bd ce b c e b2 ac bc bd ce

The REG Procedure Model: MODEL1 Dependent Variable: RGSyield

R-Square Selection Method

Number in Model	R-Square	Variables in Model
99999999999999999	0. 6923 0. 6838 0. 6754 0. 6663 0. 66660 0. 6545 0. 6576 0. 65564 0. 65549 0. 6528 0. 6528 0. 6528 0. 6515 0. 6507 0. 6500 0. 6500 0. 6599 0. 6499	b c d e b2 d2 ab bc ce b c d e b2 d2 ac bc ce b c e b2 ab ac ad bc ce a b c d e b2 d2 bc ce b c d b2 d2 e2 ab bc ce b c d e a2 b2 d2 bc ce b c d b2 d2 ab bc ce b c d b2 d2 ab bc ce b c d b2 d2 ab bc ce b c d b2 d2 ab bc ce b c b c d b2 d2 e2 ac bc ce b c e b2 ab ae bc bd ce b c b c e b2 e2 ab ad bc ce b c e b2 d2 ac bc ce b c d b2 d2 ac bc ce b c d b2 d2 ac bc ce b c d b2 d2 ac bc ce b c d b2 d2 ac bc ce b c b c e b2 ab ad bc bc ce b c e b2 ab ab bc ce b c e b2 d2 ab ae bc ce b c b c e a2 b2 ab ad bc ce b c b c e a2 b2 ab ad bc ce b c b c e2 ab ad bc bc ce b c b2 d2 ab ae bc ce b c b2 d2 ab ae bc ce b c b2 d2 ac ad ac bc ce b c e b2 ac ad ac bc ce b c e b2 ac ad ac bc ce
10 10 10 10 10 10 10 10 10 10 10 10 10 1	0. 7331 0. 7300 0. 7268 0. 7262 0. 7178 0. 7168 0. 7094 0. 7084 0. 7062 0. 7038 0. 7022 0. 7013 0. 7005 0. 6990 0. 6980 0. 6969 0. 6965 0. 6963 0. 6962	b c d e b2 d2 ab ae bc ce b c d e b2 d2 ab ad bc ce b c d e b2 d2 ac ad bc ce b c d e b2 d2 ac ae bc ce b c d e b2 d2 ab bc bd ce a b c d e b2 d2 ab bc bd ce b c d e b2 d2 ac bc bd ce b c d e b2 d2 ac bc bd ce b c e b2 ab ac ad ae bc ce b c e b2 ab ac ad ae bc ce a b c d e b2 d2 ab bc ce b c d b2 d2 e2 ab bc ce b c d b2 d2 e2 ab bc be ce b c d e b2 d2 ab bc ce b c d e b2 d2 ab bc ce b c d b2 d2 e2 ab bc ce b c d b2 d2 e2 ac ad bc ce b c d b2 d2 e2 ac ad bc ce b c d b2 d2 ab ad bc ce b c d b2 d2 ab ac ce b c d b2 d2 ab ac ce b c d b2 d2 ab ac bc ce a b c d e b2 d2 ac bc ce a b c d e b2 d2 ae bc ce b c e b2 ab ac ad bc ce de b c d b2 d2 ae bc ce b c d b2 d2 ae bc ce b c d b2 d2 ab ac ad bc ce de b c d b2 d2 ab ac ad bc ce de b c d b2 d2 ab ac ad bc ce de b c d b2 d2 ab ac ad bc ce de
11	0. 7825	b c d e b2 d2 ab ac ad bc ce

Regressi on/sel ecti on=R^2

The REG Procedure Model: MODEL1 Dependent Variable: RGSyield

Number in Model	R-Square	Variables in Model
11	0. 7632	b c d e b2 d2 ab ac ae bc ce
11	0. 7586	b c d e b2 d2 ab ae bc bd ce
11	0. 7567	a b c d e b2 d2 ab ad bc ce
11	0. 7563	b c d b2 d2 e2 ab ac ad bc ce
11	0. 7556	b c d e b2 d2 ab ad bc bd ce

11 11 11 11 11 11 11 11 11 11 11 11	0. 7523 0. 7517 0. 7515 0. 7474 0. 7474 0. 7447 0. 7431 0. 7424 0. 7422 0. 7400 0. 7391 0. 7381 0. 7373	b c d e b2 d2 ac ad bc bd ce b c d e b2 d2 ac ae bc bd ce b c d b2 d2 ab ac ad bc ce de a b c d e b2 d2 ac ad bc ce a b c d e b2 d2 ad ae bc ce b d e b2 d2 ab ac ad bc ce b c d e b2 d2 ab ac bc cd b c d e b2 d2 ab ae bc be ce a b c d e b2 d2 ad be bd ce b c d e b2 d2 ad be bd ce b c d e b2 d2 ab ae bc ce b c d e b2 d2 ab ad bc bd ce b c d e b2 d2 ab ad bc bc ce b c d e b2 d2 ab ad bc bc ce b c d e b2 d2 ab ad bc ce b c d e b2 d2 ab ad bc ce b c d e b2 d2 ab ad bc ce b c d e a2 b2 d2 ab ad bc ce b c d e a2 b2 d2 ab ad bc ce
12 12 12 12 12 12 12 12 12 12 12 12 12 1	0. 8081 0. 8007 0. 7925 0. 7916 0. 7887 0. 7873 0. 7873 0. 7855 0. 7843 0. 7837 0. 7828 0. 7823 0. 7823 0. 7779 0. 7777 0. 7751 0. 7751 0. 7729	b c d e b2 d2 ab ac ad bc bd ce b c d e b2 d2 ab ac ad ae bc ce b c d e b2 d2 ab ac ad bc be ce b c d e b2 d2 ab ac ad bc be ce b c d e b2 d2 ab ac ad bc ce b c d e b2 d2 ab ac ad bc ce a b c d e b2 d2 ab ac ad bc ce a b c d e b2 d2 ab ac ad bc ce a b c d e b2 d2 ab ac ad bc ce b c d e a2 b2 d2 ab ac ad bc ce b c d e a2 b2 d2 ab ac ad bc ce b c d e b2 d2 ab ac ad bc ce b c d b2 d2 ab ac ad bc be ce b c d e b2 d2 ab ac ad bc be ce b c d e b2 d2 ab ac ad bc ce b c d e b2 d2 ab ac ad bc ce b c d e b2 d2 ab ac ad bc ce b c d b2 d2 e2 ab ac ad bc ce b c d b2 d2 e2 ab ac ad bc be ce b c d b2 d2 e2 ab ac ad bc bd ce a b c d e b2 d2 ab ac ad bc bd ce b c d b2 d2 ac ad ae bc ce b c d b2 d2 ab ac ad bc bd ce a b c d e b2 d2 ab ac ad bc bd ce b c d b2 d2 ab ac ad bc bd ce b c d b2 d2 ab ac ad bc bd ce b c d b2 d2 ab ac ad bc bd ce b c d b2 d2 ab ac ad bc bd ce b c d b2 d2 ab ac ad bc bd ce b c d e b2 d2 ab ac ad bc bd ce
13 13	0. 8263 0. 8180	b c d e b2 d2 ab ac ad ae bc bd ce b c d e b2 d2 ab ac ad bc bd be ce

The REG Procedure Model: MODEL1 Dependent Variable: RGSyield

Number in Model	R-Square	Variables in Model
13 13 13 13 13 13 13 13 13 13 13 13 13 1	0. 8178 0. 8171 0. 8128 0. 81128 0. 8116 0. 8111 0. 8107 0. 8098 0. 8098 0. 8099 0. 8083 0. 8059 0. 8037 0. 8035 0. 8019 0. 8016	a b c d e b2 d2 ab ac ad ae bc ce b c d e b2 d2 e2 ab ac ad bc bd ce a b c d e b2 d2 ab ac ad bc bd ce a b c d e b2 d2 ab ac ad bc bd ce a b c d e b2 d2 ab ad ae bc bd ce b c d e a2 b2 d2 ab ac ad bc bd ce b c d e b2 d2 ab ac ad bc bd ce b c d e b2 d2 ab ac ad bc bd ce b c d e b2 d2 ab ac ad bc bd be ce b c d b2 d2 e2 ab ac ad bc bd be ce b c d e b2 d2 ab ac ad bc bd ce de b c d e b2 d2 ab ac ad bc bd ce de b c d e b2 d2 ab ac ad bc bd ce b c d e b2 c2 d2 ab ac ad bc bd ce b c d e b2 c2 d2 ab ac ad bc bd ce b c d b2 d2 e2 ab ac ad bc bd ce b c d e b2 d2 ab ac ad bc bd ce b c d e b2 d2 ab ac ad ae bc ce b c d e b2 d2 ab ac ad ae bc ce b c d e b2 d2 ab ac ad ae bc cd ce a b c d e b2 d2 ab ac ad ae bc ce b c d e b2 d2 ab ac ad ae bc ce b c d e b2 d2 ab ac ad ae bc ce b c d e b2 d2 ab ac ad ae bc ce b c d e b2 d2 ab ac ad ae bc ce b c d e b2 d2 ab ac ad ae bc ce
14 14 14 14 14 14 14 14 14 14	0. 8434 0. 8362 0. 8353 0. 8314 0. 8293 0. 8278 0. 8275 0. 8272 0. 8271 0. 8269 0. 8238 0. 8228	

14 14 14 14 14 14 14	0. 8228 0. 8228 0. 8219 0. 8219 0. 8216 0. 8216 0. 8213 0. 8210	a b c d e b2 d2 ab ad ae bc bd be ce b c d b2 d2 e2 ab ac ad ae bc bd ce de a b c d e b2 d2 e2 ab ac ad bc bd ce a b c d e b2 d2 e2 ab ad ae bc bd ce b c d b2 d2 e2 ab ad ae bc bd ce b c d b2 d2 e2 ab ac ad bc bd be ce b c d e a2 b2 d2 ab ac ad bc bd be ce b c d e a2 b2 d2 e2 ab ac ad bc bd ce b c d e a2 b2 d2 e2 ab ac ad bc bd ce b c d e b2 d2 ab ac ad bc bd ce
15	0. 8534	a b c d e b2 d2 ab ac ad ae bc bd be ce
15	0. 8525	a b c d e b2 d2 e2 ab ac ad ae bc bd ce
15	0. 8464	a b c d e b2 d2 ab ac ad ae bc bd cd ce

The REG Procedure Model: MODEL1 Dependent Variable: RGSyield

R-Square Selection Method

Number in Model	R-Square	Variables in Model
15 15 15 15 15 15 15 15 15 15 15 15 15	0. 8454 0. 8453 0. 8446 0. 8443 0. 8414 0. 8394 0. 8394 0. 8381 0. 8375 0. 8371 0. 8366 0. 8366 0. 8357 0. 8345	a b c d e a2 b2 d2 ab ac ad ae bc bd ce b c d e b2 d2 e2 ab ac ad ae bc bd be ce a b c d e b2 d2 ab ac ad ae bc bd ce de a b c d e b2 c2 d2 ab ac ad ae bc bd ce b c d e a2 b2 d2 ab ac ad ae bc bd be ce b c d e a2 b2 d2 e2 ab ac ad ae bc bd ce b c d b2 d2 e2 ab ac ad ae bc bd ce b c d b2 d2 e2 ab ac ad ae bc bd be ce b c d e b2 d2 ab ac ad ae bc bd be cd ce b c d e b2 d2 ab ac ad ae bc bd be cd ce b c d e b2 d2 e2 ab ac ad ae bc bd ce a b c d b2 d2 e2 ab ac ad ae bc bd ce b c d e b2 d2 e2 ab ac ad ae bc bd ce b c d e b2 d2 ab ac ad ae bc bd be ce b c d e b2 c2 d2 ab ac ad ae bc bd be ce a b c d e b2 c2 d2 ab ac ad ae bc bd ce b c d e b2 c2 d2 e2 ab ac ad ae bc bd ce b c d e b2 d2 e2 ab ac ad ae bc bd ce b c d e b2 d2 e2 ab ac ad ae bc bd ce b c d e b2 d2 e2 ab ac ad ae bc bd ce b c d e b2 d2 e2 ab ac ad ae bc bd ce b c d e a2 b2 d2 ab ac ad ae bc bd ce b c d e a2 b2 d2 ab ac ad ae bc bd ce
16 16 16 16 16 16 16 16 16 16 16 16 16 1	0. 8624 0. 8564 0. 8555 0. 8553 0. 8553 0. 8549 0. 8546 0. 8543 0. 8537 0. 8537 0. 8437 0. 8483 0. 8484 0. 8483 0. 8476 0. 8476 0. 8466 0. 8465 0. 8464 0. 8465	a b c d e b2 d2 e2 ab ac ad ae bc bd be ce a b c d e b2 d2 ab ac ad ae bc bd be cd ce a b c d e b2 d2 e2 ab ac ad ae bc bd cd ce a b c d e a2 b2 d2 ab ac ad ae bc bd be ce a b c d b2 d2 e2 ab ac ad ae bc bd be ce a b c d b2 d2 e2 ab ac ad ae bc bd be ce a b c d e a2 b2 d2 e2 ab ac ad ae bc bd ce a b c d e b2 d2 ab ac ad ae bc bd be ce a b c d e b2 c2 d2 ab ac ad ae bc bd be ce a b c d e b2 c2 d2 ab ac ad ae bc bd ce a b c d e b2 c2 d2 ab ac ad ae bc bd ce a b c d e b2 d2 e2 ab ac ad ae bc bd ce a b c d e b2 d2 e2 ab ac ad ae bc bd ce b c d e a2 b2 d2 e2 ab ac ad ae bc bd cc b c d e a2 b2 d2 ab ac ad ae bc bd cd ce b c d e b2 d2 e2 ab ac ad ae bc bd cd ce b c d e b2 d2 e2 ab ac ad ae bc bd cd ce b c d e b2 d2 ab ac ad ae bc bd cd ce a b c d e b2 d2 ab ac ad ae bc bd cd ce a b c d e a2 b2 d2 ab ac ad ae bc bd cd ce b c d e b2 c2 d2 ab ac ad ae bc bd cc de b c d e b2 c2 d2 ab ac ad ae bc bd ce a b c d e a2 b2 d2 ab ac ad ae bc bd ce b c d e b2 c2 d2 ab ac ad ae bc bd be ce b c d e b2 c2 d2 ab ac ad ae bc bd be ce b c d e b2 c2 d2 ab ac ad ae bc bd be ce b c d e b2 c2 d2 ab ac ad ae bc bd be ce b c d e b2 c2 d2 ab ac ad ae bc bd be ce b c d e b2 c2 d2 ab ac ad ae bc bd be ce b c d e b2 c2 d2 ab ac ad ae bc bd ce a b c d e a2 b2 c2 d2 ab ac ad ae bc bd ce b c d e b2 c2 d2 ab ac ad ae bc bd be ce b c d e b2 c2 d2 ab ac ad ae bc bd ce
17 17 17 17 17	0. 8654 0. 8649 0. 8637 0. 8637	

Regressi on/sel ecti on=R^2

The REG Procedure Model: MODEL1 Dependent Variable: RGSyield

Number in Model	R-Square	Variables in Model
17	0. 8584	a b c d e a2 b2 d2 ab ac ad ae bc bd be cd ce
17	0. 8583	a b c d b2 d2 e2 ab ac ad ae bc bd be cd ce de

```
17
17
                                                              a b c d a2 b2 d2 e2 ab ac ad ae bc bd be ce de a b c d e a2 b2 d2 e2 ab ac ad ae bc bd cd ce
                             0.8580
                             0.8579
17
17
17
17
17
                             0.8576
                                                              a b c d e b2 d2 ab ac ad ae bc bd be cd ce de
                                                              a b c d e b2 c2 d2 ab ac ad ae bc bd be cd ce
a b c d e b2 c2 d2 e2 ab ac ad ae bc bd cd ce
                             0.8573
                             0.8567
                             0.8567
                                                              a b
                                                                          c d e b2 d2 e2 ab ac ad ae bc bd cd ce de
                             0.8567
                                                              a b c d b2 c2 d2 e2 ab ac ad ae bc bd be ce de
                                                             a b c d e a2 b2 d2 ab ac ad ae bc bd be ce de a b c d e a2 b2 c2 d2 ab ac ad ae bc bd be ce de a b c d e a2 b2 c2 d2 ab ac ad ae bc bd ce a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd ce a b c d e a2 b2 d2 e2 ab ac ad ae bc bd ce de
                             0.8566
                             0.8564
                             0.8564
17
                             0.8561
                                                              a b c d e b2 c2 d2 ab ac ad ae bc bd be ce de a b c d e b2 c2 d2 e2 ab ac ad ae bc bd ce de
                             0.8555
                             0.8549
17
                             0.8542
                                                              b c d e a2 b2 d2 e2 ab ac ad ae bc bd be cd ce
                                                              a b c d e a2 b2 d2 e2 ab ac ad ae bc bd be cd ce a b c d e b2 c2 d2 e2 ab ac ad ae bc bd be cd ce
                             0.8679
18
                                                            a b c d e b2 c2 d2 e2 ab ac ad ae bc bd be cd ce a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be ce de a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be ce de a b c d e b2 c2 d2 e2 ab ac ad ae bc bd be ce de a b c d e b2 c2 d2 e2 ab ac ad ae bc bd be ce de a b c d a2 b2 d2 e2 ab ac ad ae bc bd be ce de a b c d a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce de a b c d a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce de a b c d a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce de a b c d a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce de a b c d e a2 b2 c2 d2 ab ac ad ae bc bd be cd ce a b c d e a2 b2 c2 d2 ab ac ad ae bc bd bc cd ce a b c d e a2 b2 c2 d2 ab ac ad ae bc bd bc cd ce a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd cd ce a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd cd ce de a b c d e b2 c2 d2 e2 ab ac ad ae bc bd cd ce de a b c d e b2 c2 d2 e2 ab ac ad ae bc bd cd ce de a b c d e a2 b2 c2 d2 ab ac ad ae bc bd bc cd ce de a b c d e a2 b2 c2 d2 ab ac ad ae bc bd bc cd ce de a b c d e a2 b2 c2 d2 ab ac ad ae bc bd bc cd ce de a b c d e a2 b2 c2 d2 ab ac ad ae bc bd bc cd ce de a b c d e a2 b2 c2 d2 ab ac ad ae bc bd bc cd ce de a b c d e a2 b2 c2 d2 ab ac ad ae bc bd bc cd ce de a b c d e a2 b2 c2 d2 ab ac ad ae bc bd bc cd ce de a b c d e a2 b2 c2 d2 ab ac ad ae bc bd bc cd ce de a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd bc cd ce de a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd bc cd ce
                             0.8667
18
                             0.8667
18
18
                             0.8663
                             0.8661
18
18
                             0.8649
                             0. 8610
0. 8597
18
18
18
18
18
                             0. 8596
0. 8596
                             0.8594
                            0. 8594
0. 8594
0. 8592
0. 8585
18
18
18
                             0.8579
18
                             0. 8576
0. 8576
18
                                                             a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd ce de b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd ce de b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce b c d e a2 b2 d2 e2 ab ac ad ae bc bd be cd ce de b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be ce de
18
                             0.8558
18
18
                             0.8555
18
                             0.8540
                                                              a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce a b c d e a2 b2 d2 e2 ab ac ad ae bc bd be cd ce de
19
                             0.8694
19
                             0.8691
                                                              a b c d e b2 c2 d2 e2 ab ac ad ae bc bd be cd ce de a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be ce de
19
                             0.8679
                             0.8676
19
                             0.8627
                                                              a b c d a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce de
```

The REG Procedure Model: MODEL1 Dependent Variable: RGSyield

R-Square Selection Method

Number in Model	R-Square	Variables in Model
19	0. 8606	a b c d e a2 b2 c2 d2 ab ac ad ae bc bd be cd ce de
19	0.8606	a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd cd ce de
19	0.8570	b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce de
19	0. 8471	a b d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce de
19	0.8450	a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc be cd ce de
19	0.8400	a b c d e a2 b2 c2 d2 e2 ab ac ad bc bd be cd ce de
19	0.8400	a b c d e a2 b2 c2 d2 e2 ab ad ae bc bd be cd ce de
19	0.8307	a b c d e a2 b2 c2 d2 e2 ac ad ae bc bd be cd ce de
19	0.8201	a b c d e a2 b2 c2 d2 e2 ab ac ae bc bd be cd ce de
19	0. 7958	a b c e a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce de
19	0. 7896	a b c d e a2 b2 c2 e2 ab ac ad ae bc bd be cd ce de
19	0. 7808	a b c d e a2 b2 c2 d2 e2 ab ac ad ae bd be cd ce de
19	0. 7806	a c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce de
19	0. 7732	a b c d e a2 c2 d2 e2 ab ac ad ae bc bd be cd ce de
19	0. 6904	a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd de
20	0. 8706	a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce de

data a;

```
60
             47.5 22
      9
                          6
                                       16.5
120
      12
             40.0
                   20
                          5
                                       15.8
120
             25.0
                          5
                                       16.7
      12
                   20
180
      15
             32.5
                   18
                          6
                                       20.1
60
      15
             47.5
                   18
                          6
                                       14.3
60
      9
             32.5
                   18
                          6
                                       16.6
120
      6
             40.0
                   20
                          5
                                       14.7
120
      12
             40.0
                   16
                          5
                                       14.9
180
      9
             32.5
                   22
                          6
                                       14.5
120
      12
             40.0
                   20
                          5
                                       15.7
180
      15
             47.5
                   18
                          4
                                       19.3
120
      12
             40.0
                   20
                          5
                                       15.9
60
      15
             47.5
                   22
                          4
                                       13.9
60
      15
             32.5
                   18
                          4
                                       14.7
120
      18
             40.0
                   20
                          5
                                       14.5
0
      12
             40.0
                   20
                          5
                                       14.4
120
      12
             40.0
                   20
                          5
                                       17.1
120
      12
             40.0
                   20
                          5
                                       18.5
120
      12
             40.0
                   20
                          5
                                       17.5
180
      15
             32.5
                   22
                          4
                                       14.4
180
      9
             32.5
                   18
                          4
                                       14.6
180
      9
             47.5
                   18
                          6
                                       16.2
120
                   20
      12
             40.0
                          3
                                       17.2
240
                          5
      12
             40.0
                   20
                                       20.1
180
             47.5
                          6
      15
                   22
                                       14.9
             47.5
60
                   18
                          4
      9
                                       16.3
120
      12
             40.0
                   24
                          5
                                       14.7
60
      9
             32.5
                   22
                          4
                                       14.0
60
      15
             32.5
                   22
                          6
                                       18.0
120
      12
             40.0
                   20
                          5
                                       16.9
120
      12
             55.0
                   20
                          5
                                       17.6
                          4
180
      9
             47.5 22
                                       17.9
data a;
set a;
a2=a*a;
b2=b*b;
c2=c*c;
d2=d*d;
e2=e*e;
ab=a*b;
ac=a*c;
ad=a*d;
ae=a*e;
bc=b*c;
bd=b*d;
be=b*e;
cd=c*d;
ce=c*e;
de=d*e;
run;
title 'RSreg';
proc rsreg data=a;
model RGSyield=a b c d e /nocode press predict lackfit ;
ridge min radius = 0 to 2 by .1;
run;
```

```
option nodate nonumber;
title 'Regression';
proc reg data=a;
model RGSyield=a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce de;
run;
quit;
title 'Regression/selection=stepwise';
proc reg data=a;
model RGSyield=a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce
de/selection=stepwise;
run;
quit;
title 'Regression/selection=R^2';
proc reg data=a;
model RGSyield=a b c d e a2 b2 c2 d2 e2 ab ac ad ae bc bd be cd ce
de/selection=rsquare;
run;
quit;
```

Stepwise Regression Analysis for Red Dog, Germ, and Shorts – Step 2

Regression/b c d b2 d2 ab ac ad bc ce de

The REG Procedure Model: MODEL1 Dependent Variable: RGSyield

Number of Observations Read Number of Observations Used 33

Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Value	Pr > F
Model Error Corrected Total	11 21 32	75. 32920 24. 91262 100. 24182	6. 84811 1. 18632	5. 77	0.0003
De	oot MSE ependent Mean oeff Var	1. 08918 16. 25455 6. 70078	R-Square Adj R-Sq	0. 7515 0. 6213	

Parameter Estimates

DF	Parameter Estimate	Standard Error	t Value	Pr > t
1	-59. 72917	20. 95802	-2. 85	0. 0096
1	2. 55949	0. 73889	3. 46	0.0023
1	0. 85390	0. 22782	3. 75	0.0012
1	4. 39230	2. 00811	2. 19	0. 0402
1	-0. 06507	0. 02192	-2. 97	0.0073
1	-0. 13391	0.04932	-2. 71	0.0130
1	0. 00310	0.00143	2. 17	0.0416
1	0. 00114	0.00054256	2. 11	0. 0475
1	-0. 00349	0.00127	-2. 76	0. 0118
1	-0. 03333	0. 01210	-2. 75	0. 0119
1	-0. 11353	0. 03206	-3. 54	0. 0019
1	0. 24158	0.06465	3. 74	0.0012
	DF 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	DF Estimate 1	DF Estimate Error 1	DF Estimate Error t Value 1 -59.72917 20.95802 -2.85 1 2.55949 0.73889 3.46 1 0.85390 0.22782 3.75 1 4.39230 2.00811 2.19 1 -0.06507 0.02192 -2.97 1 -0.13391 0.04932 -2.71 1 0.00310 0.00143 2.17 1 0.00114 0.00054256 2.11 1 -0.00349 0.00127 -2.76 1 -0.03333 0.01210 -2.75 1 -0.11353 0.03206 -3.54

data a;

input a b c d e RGSyield; cards; 120 40.0 20 7 18 12 47.5 60 22 16.5 120 12 40.0 20 5 15.8 5 120 12 25.0 20 16.7 180 15 32.5 18 6 20.1 60 15 47.5 18 6 14.3 60 9 32.5 18 6 16.6 120 6 40.0 20 5 14.7 120 12 40.0 16 5 14.9 180 9 32.5 22 6 14.5 120 12 40.0 20 5 15.7 180 15 47.5 18 4 19.3 120 12 40.0 20 5 15.9 60 15 47.5 22 4 13.9 60 15 32.5 18 4 14.7 120 18 40.0 20 5 14.5 12 40.0 20 14.4

```
120
     12
          40.0 20
                                      17.1
                         5
120
            40.0
                         5
                                      18.5
      12
                   20
                         5
120
      12
            40.0
                   20
                                      17.5
180
      15
            32.5
                   22
                         4
                                      14.4
180
      9
            32.5
                  18
                         4
                                     14.6
180
      9
            47.5
                  18
                         6
                                     16.2
120
      12
            40.0
                   20
                         3
                                     17.2
                                     20.1
240
            40.0
                   20
                         5
      12
180
            47.5
                   22
                         6
      15
                                     14.9
60
      9
            47.5
                  18
                         4
                                      16.3
120
      12
            40.0
                   24
                         5
                                      14.7
                         4
60
      9
            32.5
                   22
                                     14.0
60
      15
            32.5
                   22
                         6
                                      18.0
120
      12
            40.0
                   20
                         5
                                     16.9
120
      12
            55.0
                  20
                         5
                                     17.6
180
    9
            47.5 22
                         4
                                      17.9
;
data a;
set a;
a2=a*a;
b2=b*b;
c2=c*c;
d2=d*d;
e2=e*e;
ab=a*b;
ac=a*c;
ad=a*d;
ae=a*e;
bc=b*c;
bd=b*d;
be=b*e;
cd=c*d;
ce=c*e;
de=d*e;
run;
title 'Regression/b c d b2 d2 ab ac ad bc ce de';
proc reg data=a;
model RGSyield= b c d b2 d2 ab ac ad bc ce de;
run;
quit;
```