

EFFECTS OF PRECIPITATION ENHANCEMENT ON THE HYDROLOGIC
CYCLE FOR THREE KANSAS WATERSHEDS

by

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A MASTER'S THESIS

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requirements for the degree

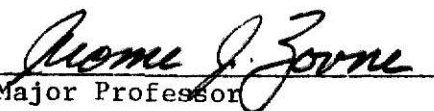
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INTRODUCTION

Man's desires to control the weather have existed through the ages. In recent years there have been breakthroughs in the understanding of climatic processes and technological development designed to alter the naturally occurring weather events. Whether technology for weather modification at present produces significant or predictable alterations of the naturally occurring phenomenon remains a scientific uncertainty and controversy. The potential for weather control today is, however, within the realm of feasibility and thus the potential effects of weather modification on the economy and the environment gain importance. Possible outcomes of precipitation enhancement on the hydrology of Kansas are investigated in this report.

The term weather modification is rather vague. One definition for clarity is "the object of weather and climate modification is concerned with any artificially produced changes in the composition, behavior, or dynamics of the atmosphere. Such changes may be deliberate or inadvertent, they may be transient or permanent, and they may be manifested on any scale from the microclimate of plants to the macrodynamics of the worldwide atmospheric circulation" (31, p.1).

Deliberate weather modification efforts can increase or decrease precipitation, suppress hail, dissipate fog, mitigate hurricanes, prevent frost, and alter the radiation balance. The objective of weather and climatic control is "to produce deliberate beneficial changes in the environment and to bring under control, or avert, changes damaging to society" (31, p.2). The levelling of natural variations in climatic conditions could increase productivity and reduce the failure risk of the

affected area. To be free of the consequences of a regional crop failure in important production areas, such as the recent Soviet wheat crop failure, is a dream of all mankind. The potential benefits of controlling severe storms are incalculable. Man's ability to initiate these changes is still limited and uncertain, but the potentialities offer incentive for continued research.

HISTORY

The hydrologic cycle involves many complex variables whose interrelations may never be completely understood. The role of precipitation as we accept it today was first recognized by Marcus Vitruvius Pollio in 1000 B.C. However it was not until Leonardo de Vinci (1452-1519) that the modern view of the hydrologic cycle was developed (14). In the prescientific era of weather modification, it was thought that rain could be controlled by great noises, explosions, and great fires (4). The weather control was basically superstitious, involving ringing of church bells, ceremonial dances or rituals, or periodic cannon fire to ward off evil spirits, appease rain gods or drive away violent rain and hail storms. Gradually, scientific investigation has resulted in improved understanding of weather phenomena, although even today our understanding is limited.

In 1819, the United States Surgeon General of the Army started a program to measure precipitation. The records are currently being kept by the National Weather Service. It was not until 1888 that the U.S. Geological Survey began systematic streamflow measurements of the Mississippi River. The establishment of a record keeping division of government is a milestone, since long continuous environmental data collections are essential in

establishing accurate probabilities for design and in forecasting events.

James P. Espy, an advisor to Congress on meteorological problems from the War Department (later from the Navy), proposed in 1851 what could have been the first federally financed large scale modification program. Espy proposed the production of rain by fire. His plan was based on his view that "all precipitation and the other aspects of storms are explained as direct consequences of convection and the release of latent heat of condensation" (4, p.6). He proposed to simultaneously set fire to 40 acre parcels of timber spaced at twenty mile intervals along a north-south line in the western states at regular seven day intervals. He believed that this holocaust would initiate a "rain of great length" (4, p.6). The plan was not endorsed by Congress but not because of doubts about Espy's theories. His views on atmospheric static stability in vertical convection do contain important elements of storm mechanisms. Espy's fire proposal was discounted in 1871 after the Chicago fire, when a heavy rain fell under very adverse conditions according to Espy's theories (7).

In the period of time from 1875-1933 significant elements of the scientific framework for weather modification were established. In 1875 and 1879 accurate explanations of mechanism were advanced by Coulier and Aitken (7). In 1930 and 1938 Tor Bergeron and Walter Findeisen advanced the theory of rain based on coexistence of ice crystals and super-cooled droplets in clouds at the same temperature, and on the rapid transfer of vapor from droplets to crystals. This work formed the basis for artificial modification of clouds. Bergeron founded the basis for cloud seeding with silver iodide in the early 1930's (4).

During this time period weather modification demonstration tests were also being conducted. In 1880, General Daniel Ruggles was granted a

patent on his scheme of using balloon carried explosives to cause rain (4,7). In 1890 and 1891 at Washington, D.C., and later in Texas, General Robert Dyrenforth conducted tests using Ruggle's scheme. The tests were regarded as unsuccessful, but it was the first federally funded project supporting weather modification through the Department of Agriculture. In 1891, Louis Gathman conducted tests to produce rain by exploding shells containing liquified carbonic acid at cloud height. In 1961 Soviet scientists were using the same method to dissipate clouds rather than produce precipitation (7). There were a variety of field tests at many different locations with the results varying from inconclusive to successful. Tests were also directed in the areas of tornado dissipation and fog dispersion.

The modern era of weather modification began in 1946 when Schaefer, Langmuir, and Vonnegut completed the first laboratory verification of the atmospheric ice crystal formation process. Schaefer completed the first field demonstration of large scale modification of super-cooled clouds by seeding them with dry ice from an airplane. With this successful demonstration, weather modification claimed a foundation in scientific theory (4,7,19).

Langmuir, the director of the crystal formation study, influenced the Defense Department to support Project Cirrus. This project (1947-1951) demonstrated the possibilities in modifying, dissipating, and causing precipitation from super-cooled clouds. The project was instrumental in establishing the methods of investigation still being followed in present experiments.

Immediately following these studies a flurry of commercial seeding activities began and soon reached a maximum coverage of approximately

10% of the land area in the United States (13). The decline of these enterprises began in the mid-50's. The intense activity in cloud seeding resulted in the formation of the President's Advisory Committee on Weather Control in 1953. The committee's primary goal was to assess the effectiveness of cloud seeding efforts. The committee reported in 1958 that seeding was producing an increase of 10-15% in winter snowfall in the western United States mountains (21,23). Their major recommendation was to increase substantially the support for research into all aspects of the atmospheric sciences. The National Science Foundation (NSF) was given a lead role in directing this research. NSF was directed by Congress to initiate and support a program of study, research, and evaluation in the field of weather modification. In the years following, many research projects and field experiments were conducted at various locations throughout the world, and research is still continuing. These tests added greatly to the fundamental knowledge of cloud seeding. Although the effectiveness of seeding is still difficult to evaluate, understanding is improving due to increased knowledge of cloud physics, more stringent statistically designed control tests, and more and better radar and raingage network observation (14). In 1966, The National Academy of Sciences, (NAS) published a report presenting conclusions based on 41 projects involved in seasonal operation for winter orographic seeding and 14 operational projects in which cumulus clouds were seeded. The programs were designed as randomized experiments to test if ice-nuclui seeding increased precipitation. NAS concluded "...there is increasing but still somewhat ambiguous statistical evidence that precipitation from some type of clouds and storm systems can be modestly increased or redistributed by seeding techniques. The implications are manifold and of immediate national concern" (31, p.4). A report

published by NSF, complementary to the NAS conclusions, reassessed projects involved in weather modification and recommended continued financial support for research of weather modification in order to increase the scientific base from which decisions can be made (30).

Numerous agencies are now involved in work or provide funds for continued research (22). The Bureau of Reclamation funds approximately one-third of all activities. The Bureau is primarily concerned with precipitation enhancement in the water short western United States. NSF funds studies for all types of weather modification. Other governmental agencies fund studies within their concern. The Forest Service is interested in research of lightning suppression. The Department of Transportation through the Federal Aviation Administration funds fog clearance experiments. The Defense and Agricultural Departments, as well as other state and local governmental agencies, provide research funding.

This effort has resulted in significant progress since 1966. The progress, in summary by Kostecki (13, p.7) is "1) in understanding the weather and how it might be changed by man, 2) in ability to affect changes in clouds and weather, and 3) in capacity to measure both natural and modified conditions of the atmosphere." This progress prompted a further assessment of weather modification technology by NAS in 1973. This publication pointed to increasing water demands, extremely limited water resources at various locations, and increased vulnerability of urbanized and industrialized area to weather phenomena in emphasizing the need for economic justification of continued development of our weather modification capabilities. The report noted, "it is essential that there be expanded research programs to develop the knowledge base from which more reliable technological assessments can

be made" (33, p.16). The 1973 report summarizes findings of past and current studies.

OBJECTIVES

In response to operational weather modification programs which have been known to make overly optimistic claims of success without well-documented evidence, several studies and experiments have been undertaken to answer the question of social and economic impact. One of these is sponsored by the Kansas Water Resources Board. It is a multi-year, interdisciplinary study to evaluate the potential impact of a full-scale operational precipitation enhancement program on the agriculturally-orientated economy of Kansas. Particular attention is being directed to the possible responses of agriculture as a result of assumed alterations in the precipitation pattern which might result from weather modification activities (1).

The objectives of the project are ambitious. They involve disciplines studying environmental factors including effects of modification on insects and disease in relation to crop production, and plant species distribution and production. The study also considers possible economic alterations, such as changes in farm resource inputs, farm outputs, organization, and other economic conditions. The project is obtaining data to aid future evolution of weather modification activities by gathering meteorological, ecological, and crop phenological data.

The objective of this particular report is to evaluate the effects of altered precipitation pattern upon the hydrology of the state.

PROCEDURE

The Model.--A modified version of the Kansas Watershed model (KWM) was used in this study to simulate the response of a watershed to enhanced

precipitation. The general concepts of KWM are described by Smith and Lumb (20). In addition the new evapotranspiration (ET) function description, included in the modified program, can be obtained in a report by Zovne and Nowaz (32). The model uses daily maximum and minimum temperatures and daily (or hourly) precipitation data read from magnetic tape containing the historical data record for the particular watershed. The ET is calculated using average monthly values of relative humidity, percent sunshine, wind speed, and solar radiation (6,24). The program also requires input watershed parameters that describe its physical characteristics. KWM can be generally described as follows: 1) it is a continuous model that generates daily flows, 2) it is a lumped-parameter model, which means average watershed properties are used without regard to spatial distribution, and 3) it is designed to model as completely as possible the land phase of the hydrologic cycle. A generalized flowchart of KWM is presented in Fig. 1.

Precipitation Enhancement.--In this study three Kansas watersheds were tested for streamflow pattern changes due to a precipitation enhancement program, assuming that cloud seeding can produce additional precipitation. Since the program monitors other information in addition to streamflow, comparisons of ET and general observations of soil moisture changes and recharge can be made.

Historical precipitation and stream flow records were used to match simulated and natural streamflows as closely as possible. The portions of the land phase of the hydrologic cycle were checked to make certain they were within reasonable limits for the conditions present at each watershed location. The historical precipitation record was then modified based on the enhancement expected from current available technology. The

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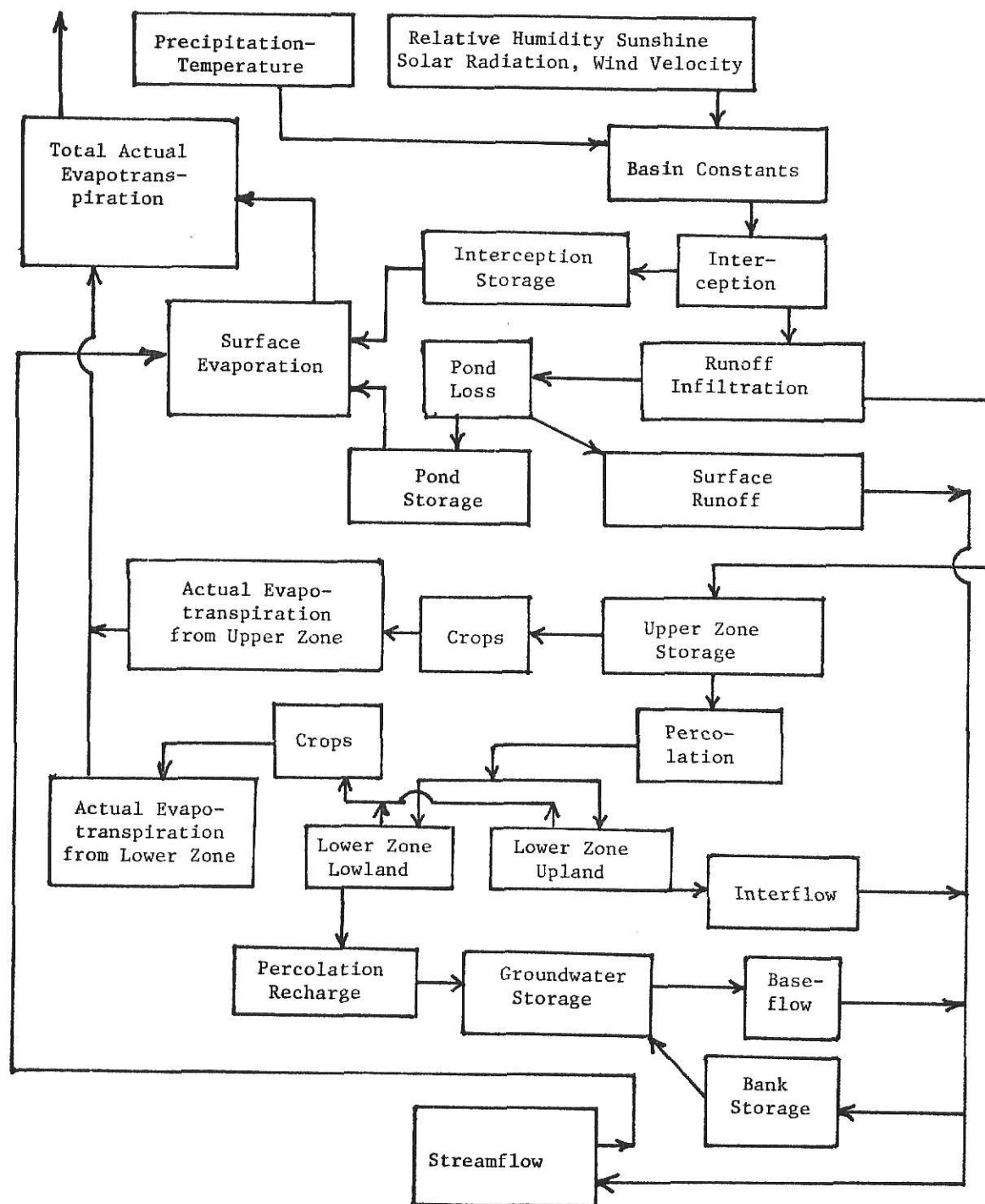


Fig. 1.--Flowchart of KSU Version of Kansas Watershed Model [from Zovne and Nawaz (32)].

possible enhancement programs for representing modification effects were discussed with many researchers and commercial operators (1). Eventually, Model B, as shown in Table 1, developed by Changnon and Huff (2), was selected as the best estimate of the possible effects of an operational seeding program for Kansas.

Smaller rainfall events are greatly enhanced by cloud seeding, assuming the seeding beneficially aids the efficiency of the clouds. Larger events are naturally more efficient and seeding is sometimes evidenced to interfere

TABLE 1.--Model B Precipitation Enhancement Program

Actual Amount of 24 hour Centimeters	Inches	% Increase
0.25 or less	0.10 or less	75
0.26 to 1.27	0.11 to 0.50	30
1.28 to 2.54	0.51 to 1.00	10
over 2.54	over 1.00	-10

with this natural efficiency, thus reducing the magnitude of the event. Model B represents the average expected results in large-scale operation. Individual seeding events would experience large variations from Model B increases. Model B also accounts for inefficiencies arising from the technical inability to detect and seed every seedable cloud, especially at night.

Model B applies only to convective clouds that produce most of the precipitation in Kansas. Since winter clouds in Kansas are usually of non-convective origin, the Model B enhancement schedule was not applied to rainfalls occurring in winter months. Two schemes were actually used which were designated B-ZERO and B-TEN, respectively. Both schemes used Model B applied to rainfalls experienced during the seven-month growing season from March through September. The rainfall producing clouds during this

season are predominantly convective. In Model B-ZERO, the winter precipitation during the months of October through February are left unaltered, thus assuming a seeding operation confined to summer convective cloud season. In Model B-TEN it was assumed that seeding operations were continued in winter but that the basic Model B alteration scheme in Table 1 would not apply. Since there is little experience in seeding non-convective clouds on the Great Plains, a simple alteration scheme was applied in which all winter rainfalls were increased a uniform 10%, hence the term B-TEN.

The Watersheds.--The watersheds studied are the Black Vermillion, South Fork Solomon, and Beaver Creek drainage basins (Fig. 2).

The Black Vermillion basin (Fig. 3) is located in northeastern Kansas near the Nebraska border. It is the smallest of the three watersheds studied, draining 1067 km^2 (412 mi^2). The watershed lies in three counties, Marshall (74.75%), Nemaha (24.27%), and Pottawattomie (0.97%). The stream-flow has been gaged continuously since 1954 at Frankfort. The area is located at the western edge of the Central Lowland physiographic province and is largely contained in the Dissected Till plains subdivision. This portion of the subdivision is further classified as the Kansas drift plains, due to the area being covered with deposits of till and loess. The till is a heterogenous, unstratified, and unsorted mixture of clay, silt, sand, and pebbles, and boulders deposited by glacial ice up to thirty feet thick. The loess is wind deposited silt. The area is a dissected plain with relatively broad gentle slopes, except where streams cut deeply into the thick glacial till deposits. The total relief is approximately 96.26 m (283 ft).

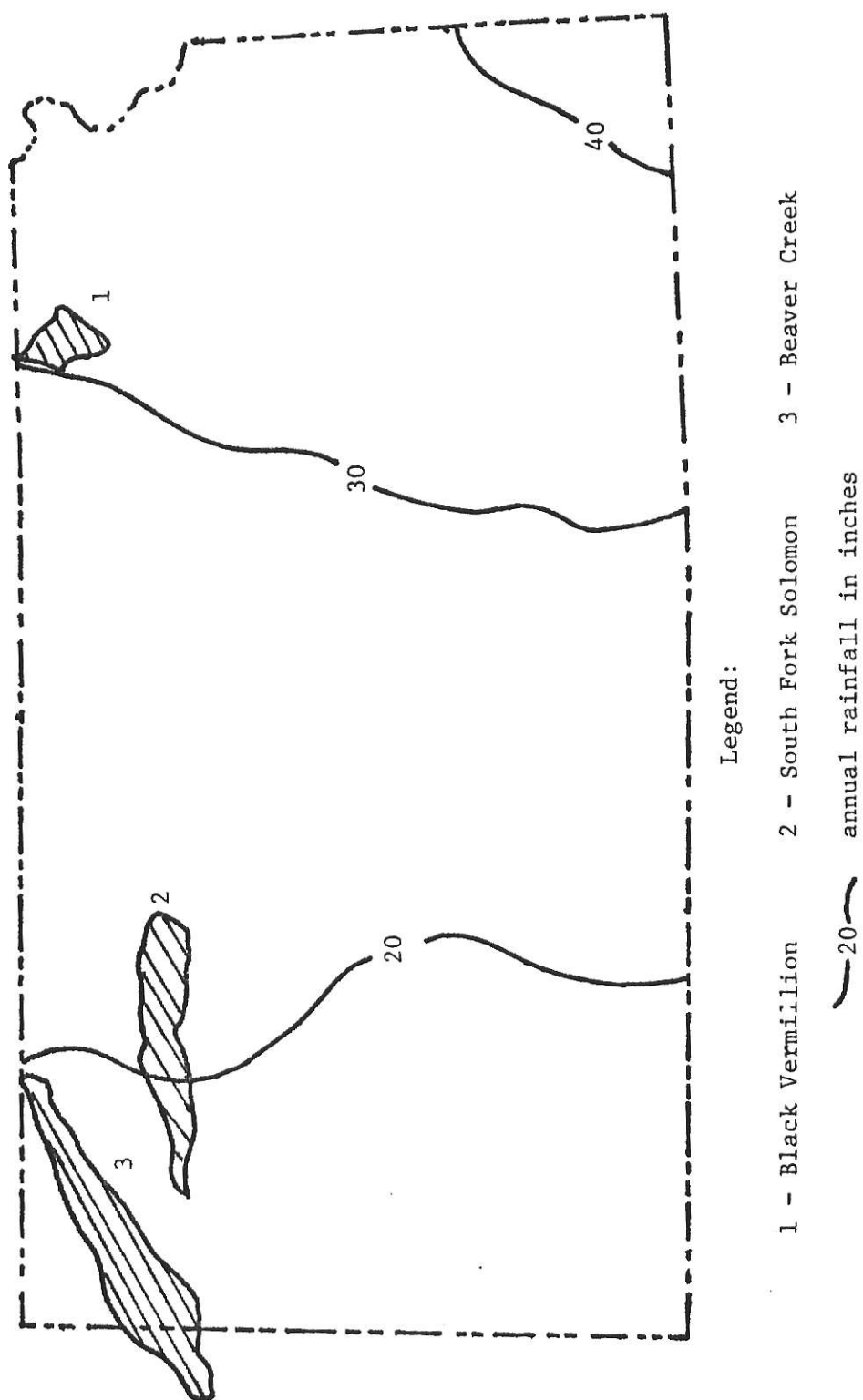


Fig. 2.--Location map of Kansas basins.

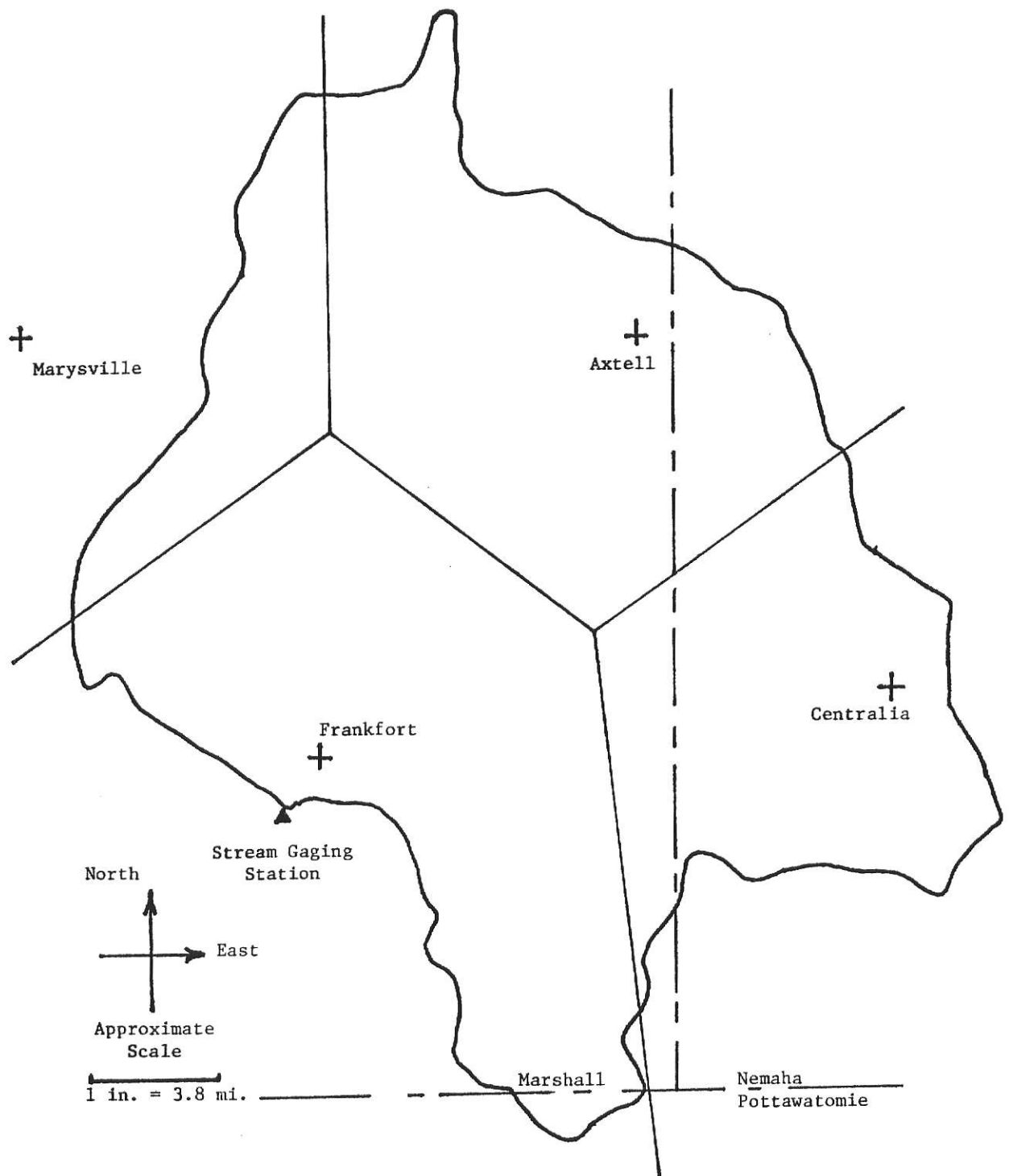


Fig. 3.--Black Vermillion Watershed.

The area is predominantly agriculturally oriented with the principle crops being wheat, sorghum, corn, soybeans, and alfalfa. The majority of the area is devoted to pasture land. The average annual precipitation is 79 cm (31 in.) and the majority of the precipitation falls within the growing season. The growing season averages 173 days in length. The mean annual temperature is 12°C (54°F) with summer temperatures rising to over 38°C (100°F) and winter temperatures falling below -18°C (0°F).

Most wells in the region are used for municipal and domestic supply. The watershed has characteristicly low well yields generally below 16 liters per sec (250 gallons per minute) (lps, gpm). The depth to groundwater in the major valleys is generally less than 6 m (20 ft) while in the upland areas selected locations may be 30.5 m (100 ft) to water. The saturated thickness of the principle water-bearing formation is from 12 to 24 m (40 to 80 ft) (12,15,18,29).

The Beaver Creek and South Fork Solomon basins, in contrast to the smaller rounded Black Vermillion watershed, are long, narrow watersheds.

The South Fork Solomon watershed (Fig. 4) is located in the second layer of counties from the northern Kansas border. The drainage area covers 2694 km² (1040 mi²) with 46% in Graham county, 34.9% in Sheridan county, 18.9% in Thomas county, and the remaining 0.2% in Rooks county. Rooks county contains the gaging station which is located above Webster Reservoir.

This watershed is located within the area known as the High Plains section of the Great Plains physiographic province. The region generally slopes eastwardly at a rate of 0.28% (12 ft/mi). The western end of the basin, consists mainly of nearly flat to gently rolling upland broken by

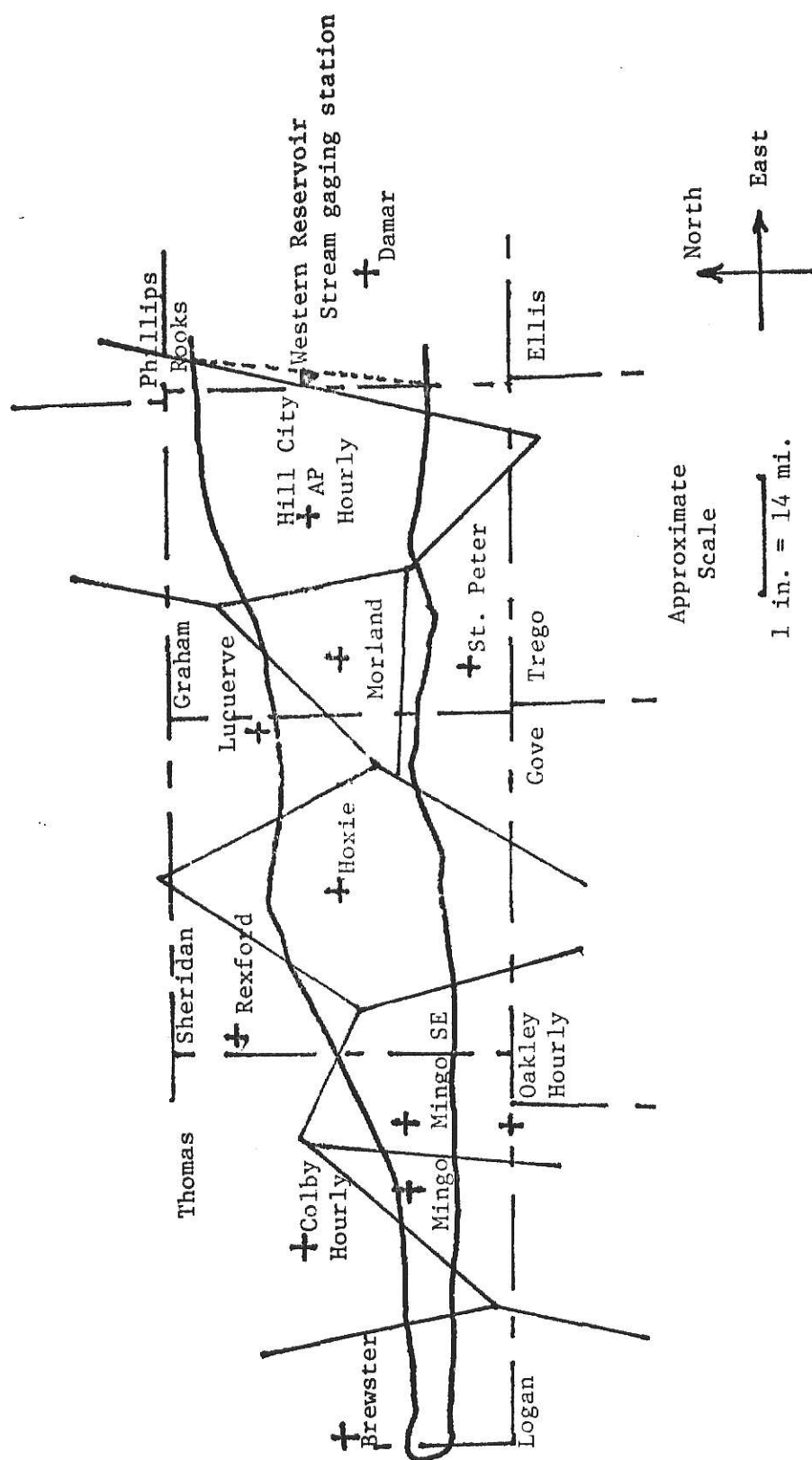


Fig. 4.--South Fork Solomon Watershed.

relatively shallow valleys. The upland areas of the basin are not always well drained because of the extreme flatness and the presence of shallow depression areas. In contrast, the eastern end of the watershed is well drained, sloping ground that is moderately to well dissected.

The basin is underlain by Pierre shale which is impervious to water from the water-bearing formation above it. The Ogallala formation rests on the Pierre shale. It averages 50 m (165 ft) thickness in the west but thins to almost nothing in the east. The Ogallala is the primary groundwater source. The well yields range from over 63 lps (1000 gpm) in the west to a few liters per second on the east. The Ogallala is overlain by unconsolidated deposits of silt or loess. This deposit is usually around 12 m (40 ft) thick and is above the water table.

The area is primarily agricultural with wheat being the main crop. The wheat-fallow rotation accounts for 50% of the cropland use. Pastures cover 40% of the area and the remaining land is largely devoted to sorghum, although other small grains and corn are present. The climate can be described as subhumid to semiarid. The average annual temperature is 12°C (53°F) with extremes recorded from -31°C (-24°F) to 47°C (117°F). The average precipitation is approximately 48 cm (19 in.) with extreme variations of 17 to 100 cm (7 to 39 in.). The average growing season is about 162 days (5,8,9,11,12).

Beaver Creek basin (Fig. 5) is located mainly in extreme northwestern Kansas. It drains 4190 km² (1168 mi²) but 761 km² (294 mi²) of which are probably non-contributing. The gaging station is located at Cedar Bluffs in Decatur county. The watershed lies in Kit Carson county, Colorado (20%), Sherman County (including a portion of Thomas, 31%), Cheyenne county (16%), and Decatur county (including Red Willows County, Nebraska, 6%).

The area is also located in the High Plains section of the Great Plains physiographic province. The upland areas are flat to gently rolling terrain and characterized by having numerous shallow undrained depressions. The watershed slopes eastwardly at a rate of 0.23 to 0.27% (12 to 14 ft/mi). The uplands are moderately dissected by small drainage ways. The areas bordering streams tend to be gentle until the stream becomes major in size when the slope then becomes more rugged and steeper, especially along the south side of Beaver Creek. The area of dissection extends 3 to 5 km (2 to 3 mi) either side of the streams and the flat valley floor may be 61 m (200 ft) below the upland plateau.

The basin is underlain by Pierre shale. It outcrops in only a few areas where the younger formations have eroded away. The Ogallala formation overlies the Pierre shale and is nearly 91 m (300 ft) thick in places. In other areas it is very thin or completely removed by erosion. The Ogallala outcrops along many stream valleys but it is generally covered by a 15 m (50 ft) thick deposit of wind-blown loess. The soils of the region are deep, well-drained, nearly level or gently sloping silt loams of the upland. The valley terraces are covered by deep, well-drained, strongly sloping loams.

The area is predominantly agricultural with wheat, sorghum, barley, corn, and pastures being the main crops. Summer fallowed areas are also present. Irrigation was increasing during the final years of the test period. The region is semiarid with a mean annual temperature of 12°C (53°F) with extremes of over 38°C (100°F) to less than 18°C (0°F). The rainfall also varies extremely from the average annual amount of 43 cm (17 in.). Test well yields range from 9 to 58 lps (150 to 900 gpm). The depth

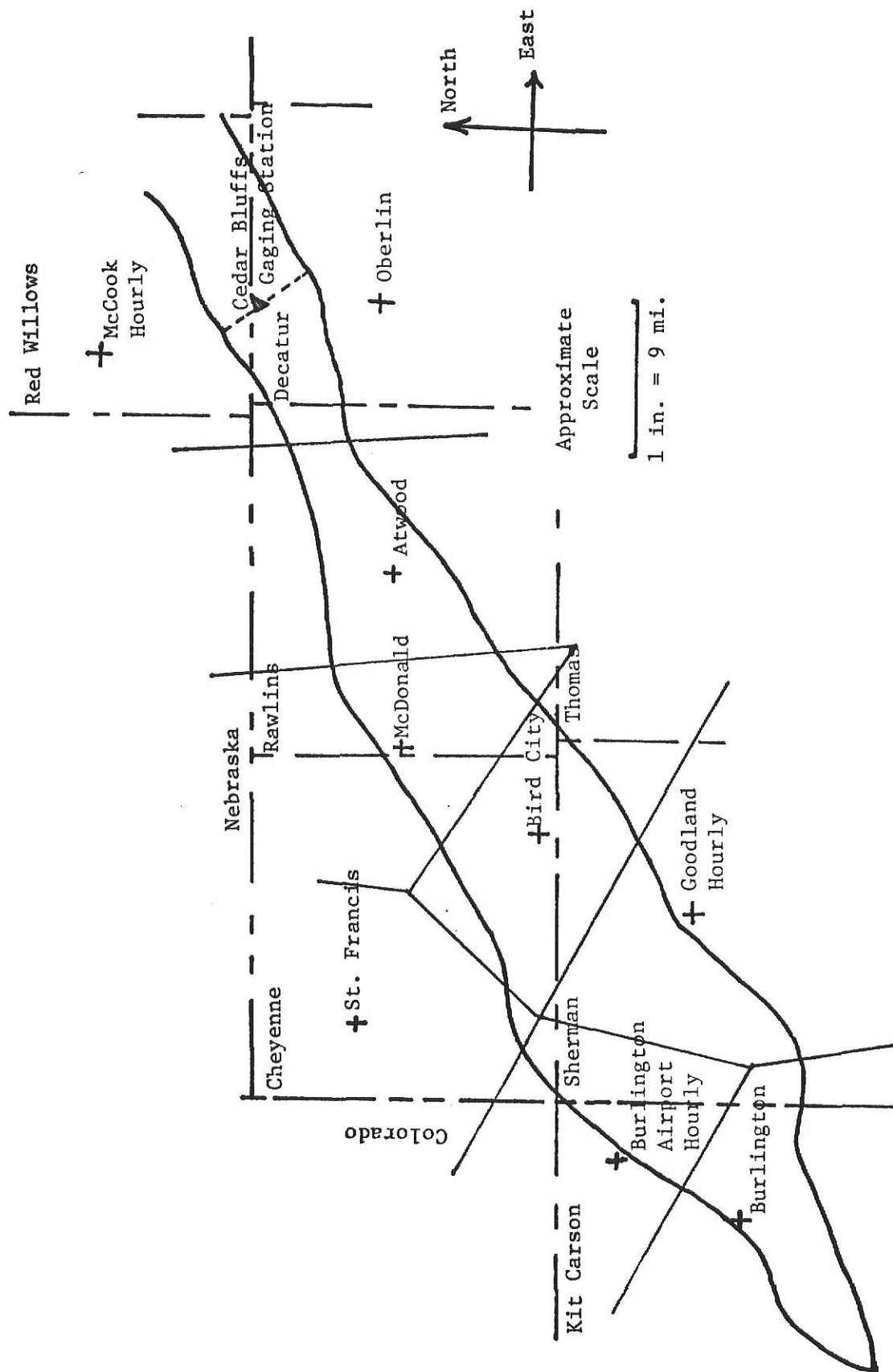


Fig. 5.--Beaver Creek Watershed.

to water for the upland wells is generally more than 30 m (100 ft) while in the valleys the depth can be as little as 3 m (10 ft). The saturated thickness of the water-bearing deposit range from less than 6 m (20 ft) in eastern Rawlins county to almost 60 m (200 ft) in Sherman county. Generally the thickness is over 30 m (100 ft) (10,13,16,17).

Model Calibration.--The Kansas Watershed Model is calibrated by comparing the calculated streamflows to observed stream flows. Coefficients are adjusted until long term observed and calculated streamflows agree, as shown in Table 2. In the calibration process, elements of the budget such as interception, evapotranspiration, and soil moisture variations are similarly adjusted to yield reasonable values for the particular location. The correlations listed in Table 2 are the average of the monthly coefficients (r^2) computed from daily values of observed and calculated streamflows.

TABLE 2.--Observed and Modeled Accumulated Streamflows

Watershed	Simulation Period	Observed* Flow	Modeled Flow	Average Correlation (r^2)
Black Vermillion	1954-1967	142.65 (56.16)	144.04 (56.71)	.731
South Fork Solomon	1948-1961	47.78 (18.81)	46.40 (18.23)	.677
Beaver Creek ⁺	1947-1965	11.68 (4.60)	12.34 (4.86)	.711

*Flows are in centimeters (inches)

+Flows for Beaver Creek exclude 1957 and 1960.

Two problem years, 1957 and 1960, were encountered in calibrating the Beaver Creek model. The program substantially underpredicted the flow for these two years. The observed flow was gaged at 15.82 cm (6.227 in.) for the 1947-1965 record period but KWM predicted only 13.27 cm (5.233 in.).

This is under-estimation of almost 16%. A check of the climatological data records and streamflow records (28,26,27) did not reveal any inconsistencies in the information recorded on the magnetic tape used as input for KWM. The model simply did not predict the extremely high May, 1957 flows. KWM tends to underpredict the peaks of extreme runoff events. For this particular event, however, the recorded precipitation could not have produced a runoff event of the observed magnitude, although there are damage accounts for the flood that occurred in May of 1957. This region typically experiences spotty high intensity storms. It is possible for a storm of sufficient magnitude to have occurred in the gaps of the rain gage network. Of the nine stations used in the program, four experienced a relatively large storm, two light to moderate, and three recorded no precipitation, which may explain the difficulty.

The 1960 streamflow difficulty was due to a very cold winter in which snow accumulation occurred from mid-January to mid-March. Several north western stations reported 68 consecutive days of snow cover. The low temperatures prevented most snowmelt until mid-March when above normal temperatures caused rapid melt and high runoff. KWM contains a simple snow accumulation and snowmelt subroutine, which is uncalibrated due to the infrequency of substantial snow accumulations in Kansas. The extreme conditions of this winter were not modeled accurately by this subroutine.

Since the two years accounted for most of the underprediction of the total flow measurement, they were not used in comparing the effects of weather modification. The years are included in figures only to provide a continuous record. Computed averages, percentages, or deviations exclude these years.

RESULTS

The assumed modification schemes, B-ZERO and B-TEN, result in increased precipitation, streamflow, and runoff. There are some interesting effects resulting from applying B-ZERO and B-TEN assumptions to these watersheds.

Precipitation.--The Black Vermillion Watershed experienced an average of 5.36 cm (2.11 in.) per year of additional rainfall for the fourteen year test period due to B-ZERO modification. B-TEN caused an average increase of 6.81 cm (2.66 in.) per year. South Fork Solomon average increases were 5.54 cm (2.18 in.) and 6.27 cm (2.47 in.) per year. Beaver Creek experienced increased precipitation averaging 5.52 cm (2.18 in.) and 6.10 cm (2.40 in.) per year.

In the summaries presented in Tables 3, 4, and 5, the climatic difference between the subhumid Black Vermillion and the semiarid South Fork and Beaver Creek region are apparent. Although all these watersheds had similar absolute increases in precipitation under B-ZERO, the Beaver Creek, percentage increase over natural ormal precipitation was twice that of the Black Vermillian. South Fork experienced a similar result.

The effects of B-TEN modification were similar to B-ZERO, except that B-TEN is always somewhat higher. The Black Vermillian watershed showed the most significant increase in winter precipitation as a result of the B-TEN program. Since winter modification assumes a uniform percentage increase, a larger absolute increase in precipitation would be expected in the wetter region.

Runoff.--B-ZERO modification resulted in reduced streamflows for five years for the Black Vermillion, two years for the South Fork Solomon, and one year for Beaver Creek. There is quite a difference in streamflows for

TABLE 3.--Black Vermillion Watershed Summary

Year	Precipitation		Runoff		Eta & Interception		Storage Change					
	Normal	Mod B-ZERO	Mod B-TEN	Normal	B-ZERO	B-TEN	Normal	B-ZERO	B-TEN			
1954	73.15 (28.80)	78.69 (30.98)	79.65 (31.36)	7.529 (2.965)	7.686 (3.046)	7.844 (3.088)	73.552 (28.957)	75.883 (29.875)	76.253 (30.021)	- 7.948 (-3.129)	- 4.938 (-1.944)	- 4.564 (-1.797)
1955	58.47 (23.02)	65.35 (25.73)	66.85 (26.32)	3.754 (1.478)	4.214 (1.658)	4.420 (1.740)	65.395 (25.746)	68.214 (26.856)	68.608 (27.011)	-10.678 (-4.204)	- 7.069 (-2.783)	- 6.185 (-2.435)
1956	51.69 (20.33)	57.79 (22.75)	59.03 (23.24)	2.052 (0.808)	3.454 (1.360)	3.729 (1.468)	60.333 (23.753)	62.949 (24.783)	62.669 (24.673)	-10.744 (-4.230)	- 8.621 (-3.394)	- 7.369 (-2.901)
1957	87.48 (34.44)	94.08 (37.04)	96.09 (37.83)	8.950 (3.327)	9.365 (3.687)	10.163 (4.001)	69.540 (27.378)	69.868 (27.507)	69.872 (27.609)	9.467 (3.727)	14.826 (5.837)	16.048 (6.318)
1958	96.57 (37.98)	99.67 (39.24)	100.79 (39.68)	19.207 (7.562)	16.683 (6.568)	16.746 (6.593)	66.372 (26.131)	73.609 (28.980)	74.475 (29.321)	10.861 (4.276)	9.347 (3.680)	9.568 (3.767)
1959	104.57 (41.17)	107.80 (42.44)	109.60 (43.15)	20.246 (7.971)	18.872 (7.430)	21.021 (8.276)	74.285 (29.246)	77.249 (30.413)	77.602 (30.552)	9.996 (3.935)	11.643 (4.584)	10.980 (4.323)
1960	74.42 (24.30)	80.19 (31.67)	81.69 (32.16)	5.921 (2.331)	11.254 (4.431)	14.846 (5.845)	6.953 (24.391)	75.671 (29.792)	75.761 (29.827)	- 6.152 (-2.422)	- 6.764 (-2.663)	- 8.910 (-3.508)
1961	99.39 (29.13)	104.90 (41.30)	107.01 (42.13)	12.421 (4.890)	15.969 (6.287)	18.075 (7.116)	75.827 (29.853)	76.736 (30.211)	76.799 (30.236)	11.128 (4.381)	12.159 (4.787)	12.144 (4.781)
1962	87.22 (34.34)	91.47 (36.01)	93.32 (36.74)	13.424 (5.285)	19.759 (7.779)	21.608 (8.507)	78.161 (30.772)	78.628 (30.960)	78.674 (30.974)	- 4.399 (-1.732)	- 6.975 (-2.746)	- 6.960 (-2.740)
1963	56.16 (22.11)	62.84 (24.74)	63.60 (25.04)	2.802 (1.103)	4.427 (1.793)	5.141 (2.024)	77.008 (30.318)	79.964 (31.982)	80.185 (31.569)	-23.645 (-9.309)	-21.557 (-8.487)	-21.717 (-8.550)
1964	82.55 (32.50)	86.16 (33.92)	87.27 (34.36)	12.098 (4.763)	10.902 (4.292)	10.496 (4.329)	68.405 (26.931)	74.673 (29.399)	75.499 (29.724)	2.029 (0.799)	0.549 (0.216)	0.772 (0.304)
1965	96.67 (38.06)	104.60 (41.18)	106.22 (41.82)	14.742 (5.804)	15.193 (5.962)	15.740 (6.197)	73.345 (28.876)	76.4921 (30.115)	76.723 (30.206)	8.547 (3.365)	12.931 (5.091)	13.757 (5.416)
1966	58.52 (23.04)	62.74 (24.70)	63.53 (25.01)	6.327 (2.491)	5.872 (2.312)	5.918 (2.330)	61.913 (24.375)	68.356 (26.912)	68.849 (27.106)	- 9.728 (-3.830)	-11.501 (-9.528)	-11.245 (-4.427)
1967	91.90 (36.18)	97.51 (38.39)	99.09 (39.01)	14.801 (5.827)	13.759 (5.917)	14.186 (5.585)	71.128 (28.003)	76.985 (30.309)	77.460 (30.496)	5.941 (2.339)	6.734 (2.651)	7.452 (2.934)
Total	1118.62 (440.40)	1193.75 (469.98)	1213.76 (477.86)	144.043 (56.710)	157.709 (62.090)	170.454 (67.108)	989.909 (389.728)	1035.258 (407.582)	1039.424 (409.222)	-15.326 (-6.034)	0.762 (0.300)	3.894 (1.533)
Average	79.91 (31.46)	85.27 (33.57)	86.69 (34.13)	10.290 (4.051)	11.265 (4.435)	12.174 (4.793)	70.709 (27.838)	73.947 (29.113)	74.244 (29.230)	- 1.095 (-0.431)	0.053 (0.021)	0.279 (0.110)
% Increase	---	6.72	8.51	---	9.70	10.35	---	4.58	5.00			
% Water	100	100	100	12.88	13.21	14.04	88.49	86.73	85.63	- 1.37	0.06	0.33

NOTE: All numbers in centimeters (inches)

TABLE 4.--South Fork Solomon Summary

Year	Precipitation		Runoff		Eta & Interception		Storage Change	
	Normal	Mod B-ZERO	Normal	B-TEN	Normal	B-ZERO	Normal	B-ZERO
1948	48.77 (19.20)	54.28 (21.37)	1.788 (0.704)	2.090 (0.823)	49.456 (19.471)	54.475 (21.447)	-2.477 (-0.975)	-2.296 (-0.909)
1949	62.59 (24.64)	70.74 (28.20)	2.230 (0.878)	2.677 (1.054)	60.053 (23.643)	61.351 (24.154)	0.290 (-0.114)	6.701 (2.635)
1950	53.62 (21.11)	59.49 (23.42)	6.279 (2.472)	6.050 (2.382)	47.427 (18.672)	55.789 (21.964)	-0.099 (-0.039)	2.362 (-0.930)
1951	84.02 (33.08)	88.37 (34.79)	13.678 (6.386)	19.632 (7.729)	60.154 (23.683)	62.011 (24.414)	10.201 (4.016)	6.715 (2.250)
1952	32.69 (12.87)	39.29 (15.47)	1.699 (0.699)	3.381 (1.331)	42.520 (16.740)	46.667 (18.373)	-11.529 (-4.539)	-10.744 (-4.230)
1953	48.21 (18.98)	53.11 (20.91)	1.321 (0.520)	1.588 (0.625)	41.740 (16.433)	46.909 (18.468)	6.149 (2.027)	4.618 (1.818)
1954	37.36 (14.71)	41.63 (16.39)	1.316 (0.518)	1.577 (0.621)	41.886 (16.412)	47.036 (18.510)	-5.723 (-2.253)	-6.734 (-2.445)
1955	38.63 (15.21)	41.86 (16.48)	0.960 (0.378)	1.008 (0.397)	35.817 (14.101)	39.091 (15.390)	1.869 (0.736)	1.758 (0.692)
1956	24.79 (9.76)	29.21 (11.50)	0.490 (0.193)	0.660 (0.260)	27.181 (10.701)	31.237 (12.248)	-2.663 (-1.136)	-2.695 (-1.061)
1957	69.63 (27.42)	75.90 (29.88)	5.230 (2.059)	4.940 (1.945)	59.149 (23.287)	61.571 (24.240)	5.271 (2.075)	9.388 (3.696)
1958	57.51 (22.64)	64.39 (26.35)	3.518 (1.385)	6.619 (2.606)	52.281 (20.583)	54.346 (21.396)	1.717 (0.676)	3.426 (1.349)
1959	55.19 (21.73)	61.29 (24.13)	1.514 (0.596)	1.974 (0.777)	51.951 (20.453)	57.503 (22.639)	1.722 (0.678)	0.061 (0.025)
1960	52.83 (20.80)	58.29 (22.95)	2.611 (1.028)	5.845 (2.301)	51.608 (20.318)	54.188 (21.334)	-1.379 (-0.543)	-1.735 (-0.683)
1961	66.45 (26.16)	72.01 (28.35)	3.594 (1.415)	5.456 (2.148)	57.498 (22.637)	59.644 (23.482)	5.347 (2.105)	6.914 (2.722)
Total	732.31 (288.31)	809.85 (318.84)	46.309 (18.232)	63.497 (24.999)	678.520 (267.134)	731.817 (288.117)	7.475 (2.943)	12.017 (4.731)
Average	52.309 (20.594)	57.846 (22.774)	3.307 (1.302)	4.536 (1.786)	48.466 (19.081)	52.273 (20.580)	0.533 (0.210)	0.864 (0.340)
% Increase	---	10.59	---	37.12	---	7.85	---	---
% Budget	100	100	4.52	7.74	92.66	90.36	1.02	1.48

NOTE: All numbers in centimeters (inches).

TABLE 5.—Beaver Creek Watershed Summary

Year	Normal	Precipitation Mod B-ZERO	Mod B-TEN	Normal	Runoff B-ZERO	B-TEN	Normal	Eta & Interception B-ZERO	B-TEN	Normal	Storage Change B-ZERO	B-TEN
1947	37.87 (14.91)	43.74 (17.22)	44.42 (17.49)	0.869 (0.342)	0.902 (0.355)	0.902 (0.355)	42.174 (16.604)	44.613 (17.564)	44.780 (17.630)	-5.171 (-2.036)	-1.775 (-0.699)	-1.230 (-0.496)
1948	49.17 (19.36)	54.53 (21.53)	55.22 (21.74)	1.036 (0.408)	0.960 (0.378)	0.963 (0.379)	44.516 (17.526)	47.821 (18.827)	47.897 (18.857)	3.586 (1.412)	5.895 (2.321)	6.353 (2.501)
1949	58.34 (22.97)	66.24 (26.08)	66.78 (26.29)	0.574 (0.226)	3.513 (1.383)	4.445 (1.750)	53.769 (21.169)	55.578 (21.881)	55.799 (21.698)	4.003 (1.576)	7.163 (2.830)	6.525 (2.569)
1950	36.04 (14.19)	42.27 (16.84)	42.75 (16.83)	0.432 (0.170)	0.904 (0.356)	0.980 (0.386)	43.602 (17.166)	48.146 (18.953)	48.494 (18.952)	-7.910 (-3.114)	-6.695 (-2.675)	-6.731 (-2.650)
1951	60.07 (23.65)	64.36 (25.35)	57.15 (22.50)	1.654 (0.651)	3.172 (1.249)	3.627 (1.428)	49.685 (19.561)	52.601 (20.709)	52.601 (20.709)	8.738 (3.440)	8.603 (3.387)	8.545 (3.364)
1952	32.69 (12.95)	39.57 (15.58)	39.80 (15.67)	0.401 (0.158)	4.166 (1.640)	4.440 (1.748)	40.427 (15.916)	44.912 (17.682)	45.204 (17.797)	-7.930 (-3.122)	-9.512 (-3.745)	-9.845 (-3.876)
1953	38.91 (15.32)	4.09 (17.36)	84.73 (17.69)	0.236 (0.093)	0.612 (0.241)	0.615 (0.242)	38.011 (14.965)	43.868 (17.271)	43.812 (17.249)	0.660 (0.260)	0.904 (0.356)	0.498 (0.196)
1954	24.28 (9.56)	28.65 (11.28)	29.08 (11.45)	0.249 (0.089)	0.274 (0.108)	0.279 (0.110)	27.826 (10.955)	38.052 (14.981)	38.270 (15.067)	-3.774 (-1.486)	-9.865 (-3.884)	-9.462 (-3.725)
1955	27.56 (10.85)	32.44 (12.77)	32.67 (12.94)	0.155 (0.061)	0.191 (0.075)	0.196 (0.077)	27.541 (10.863)	33.754 (13.289)	34.963 (13.765)	-0.150 (-0.055)	-1.501 (-0.591)	-2.436 (-0.959)
1956	28.55 (11.24)	33.93 (13.36)	34.54 (13.60)	0.213 (0.084)	0.274 (0.108)	0.274 (0.108)	27.450 (10.807)	31.011 (12.209)	31.615 (12.360)	0.884 (0.345)	2.652 (1.044)	2.860 (1.126)
1957	55.98 (22.04)	63.80 (25.12)	64.29 (25.31)	0.612 (0.241)	0.714 (0.281)	0.716 (0.282)	50.808 (20.003)	51.996 (20.274)	42.276 (20.581)	4.552 (1.792)	10.831 (4.264)	11.295 (4.447)
1958	53.16 (20.93)	61.09 (24.05)	61.77 (24.32)	0.648 (0.255)	2.078 (0.818)	3.155 (1.242)	48.466 (19.081)	51.436 (20.279)	51.450 (20.256)	4.041 (1.591)	7.521 (2.961)	7.176 (2.825)
1959	40.82 (16.07)	47.73 (18.79)	48.62 (19.14)	0.323 (0.127)	1.046 (0.412)	1.374 (0.541)	44.950 (17.697)	49.647 (19.546)	50.058 (19.708)	-0.404 (-0.158)	-2.962 (-1.166)	-2.827 (-1.113)
1960	43.82 (17.25)	48.72 (19.18)	50.34 (19.82)	0.348 (0.137)	5.829 (2.295)	7.371 (2.902)	43.325 (17.057)	46.305 (18.357)	46.373 (18.757)	0.142 (0.056)	-3.612 (-1.422)	-3.409 (-1.342)
1961	51.00 (20.08)	56.90 (22.40)	57.48 (22.63)	0.701 (0.276)	1.300 (0.512)	1.882 (0.741)	50.409 (19.846)	50.630 (19.933)	50.630 (19.933)	2.685 (1.057)	5.199 (2.047)	9.971 (1.957)
1962	57.33 (22.57)	61.32 (24.14)	61.80 (24.33)	2.111 (0.831)	6.988 (2.755)	7.374 (2.903)	50.460 (19.866)	53.040 (20.882)	53.274 (20.974)	4.750 (1.870)	1.273 (0.501)	1.158 (0.456)
1963	44.75 (17.62)	50.22 (19.77)	50.72 (19.97)	0.617 (0.243)	2.563 (1.009)	3.081 (1.213)	47.567 (18.727)	50.937 (20.054)	51.227 (20.168)	-3.434 (-1.352)	-3.284 (-1.297)	-3.592 (-1.414)
1964	31.65 (12.46)	35.36 (13.92)	35.61 (14.02)	0.671 (0.264)	0.749 (0.295)	0.782 (0.306)	38.852 (15.246)	41.171 (16.509)	41.389 (16.757)	-7.869 (-3.078)	-6.508 (-2.506)	-6.566 (-2.585)
1965	49.14 (27.22)	72.82 (28.71)	73.81 (29.06)	1.463 (0.576)	4.978 (1.960)	5.497 (2.164)	49.108 (19.334)	52.207 (20.554)	52.306 (20.563)	18.166 (7.152)	15.728 (6.192)	16.012 (6.304)
Total	741.53 (291.99)	835.46 (328.92)	844.91 (332.64)	12.332 (4.385)	34.676 (13.652)	39.865 (15.695)	722.015 (284.358)	789.262 (310.733)	793.570 (312.429)	10.801 (4.284)	11.059 (4.354)	10.996 (4.329)
Average	43.51 (17.17)	49.15 (19.35)	49.71 (19.57)	0.726 (0.286)	2.040 (0.803)	2.344 (0.923)	42.474 (16.721)	46.426 (18.721)	46.680 (18.378)	0.640 (0.252)	0.650 (0.256)	0.645 (0.254)
% Increase	---	12.67	13.94	---	181.19	223.27	---	9.31	9.91	---	---	---
% Budget	100	100	100	1.66	4.15	4.72	97.37	94.45	93.92	1.47	1.32	1.30

NOTE: All numbers in centimeters (inches)

the two regions. The Black Vermillion experienced a 10% runoff increase due to modification, which represents only a slight change in the percent of the watershed budget represented by runoff. In the unmodified model, runoff was 12.88% of the entire water budget. B-ZERO and B-TEN modifications increased the runoff budget percentage to 13.21 and 14.04%, respectively. The other two watersheds show more variation. The South Fork experienced 37.12 and 47.73% increases in runoff, representing increases from 4.52% of the water budget to 7.74 and 8.95%, respectively. Beaver Creek, which has a very low average runoff per year, experienced increases of 181.19% and 223.27%, respectively. These represent an increase in the percentage of the total budget from 1.66% for normal conditions to 4.15 and 4.72% for the two modified conditions. The natural average runoff in centimeters (inches) for the three watersheds from east to west is 10.29 (4.05), 3.31 (1.30), and 0.73 (0.29), respectively while for B-ZERO the runoffs are 11.26 (4.44), 4.54 (1.79), and 2.04 (0.80) centimeters (inches).

Evapotranspiration.--The Black Vermillion was calibrated to produce an average of 70.71 cm (27.84 in.) of evapotranspiration (ET) per year, which is 22.25 cm (8.76 in.) per year more than South Fork and 28.24 cm (11.12 in.) per year more than Beaver Creek ET. The Black Vermillion ET is, however, less responsive to increased precipitation, as 4.58 and 5.00% increases were experienced in comparison to 9.31 and 9.91% increases for Beaver Creek. Unfortunately the 9.31% only translates into a 3.96 cm (1.56 in.) per year average increase in ET for Beaver Creek while the 4.58% increase for the Black Vermillion yields 3.25 cm (1.28 in.) per year. The South Fork B-ZERO average increase was 3.81 cm (1.50 in.) per year. Increase of any magnitude in ET would usually be termed beneficial.

Table 6 represents an attempt to show that weather modifications may result in a change of the variability of runoff and ET. The standard deviation ($\hat{\sigma}$) is used to characterize the degree to which B-ZERO and B-TEN either increases or decreases the dispersion (variability) about the mean. The rainfalls experience almost no change in variability, which may or may not be a surprising result. The runoff dispersion is decreased by modification for the Black Vermillion, but increased for the other two watersheds. In all cases, the modified ET's were less variable than the unmodified ET's.

Figures 6 through 14 illustrate the carry over effects of wet to dry years and the differing effects of weather modification in wet and dry years. Figures 15, 16 and 17 present the general trend of B-ZERO and B-TEN in relation to the normal precipitation. All figures illustrate the usual trend is for the greatest percent increase to occur during the years of below natural rainfall. This does not mean dry years receive larger absolute amounts of precipitation, but that these increases are a function of the number and magnitude of the rainfalls experienced in each year.

Water Storage.--In the fourth column of the summary tables, the changes in storage from the beginning of the test period at initial conditions to the final ending conditions are listed. The storage change consists of the sum of soil moisture changes and groundwater level changes. The long term average of this account should be near zero since there are cyclic trends in water consumption and the total water available for consumption is limited.

The Black Vermillion simulation ends with 15.33 cm (6.03 in.) of deficit or an average loss from storage of 1.09 cm (0.43 in.) per year. The B-ZERO modification provides enough moisture that this deficit is overcome and provides enough extra rainfall for a 0.05 cm (.02 in.) per year gain. B-TEN modification raises the net average gain to 0.28 cm (0.11 in.) per year.

TABLE 6.--Comparison of Statistics for Precipitation,
Runoff, and Evapotranspiration.

Watershed	Precipitation		Runoff		Evapotranspiration	
	$\bar{\mu}$	$\hat{\sigma}$	$\bar{\mu}$	$\hat{\sigma}$	$\bar{\mu}$	$\hat{\sigma}$
Black Vermillion						
Natural	79.91 (31.46)	17.75 (6.99)	10.240 (0.051)	8.405 (3.309)	70.709 (27.838)	5.977 (2.353)
B-ZERO	85.27 (33.57)	17.58 (6.92)	11.265 (4.435)	5.585 (2.199)	73.962 (29.118)	4.989 (1.964)
B-TEN	86.69 (39.13)	17.78 (7.00)	12.174 (4.793)	5.791 (2.280)	74.244 (29.230)	4.892 (1.926)
South Fork						
Natural	52.31 (20.59)	15.77 (6.21)	3.307 (1.302)	3.411 (1.343)	48.466 (19.081)	9.787 (3.853)
B-ZERO	57.85 (22.77)	16.20 (6.38)	4.536 (1.786)	4.912 (1.934)	42.273 (20.580)	9.091 (3.579)
B-TEN	58.59 (23.07)	16.24 (6.40)	4.887 (1.924)	5.164 (2.033)	52.563 (20.694)	8.865 (3.498)
Beaver Creek						
Natural	43.61 (17.17)	13.09 (5.15)	0.726 (0.246)	0.554 (0.218)	42.721 (16.721)	8.245 (3.246)
B-ZERO	49.15 (19.35)	12.312 (5.202)	2.040 (0.803)	1.938 (0.763)	46.426 (18.278)	7.00 (2.756)
B-TEN	49.71 (19.57)	13.274 (5.226)	2.344 (0.423)	2.129 (0.838)	46.680 (18.378)	6.853 (2.698)

NOTE: All numbers in centimeters (inches).

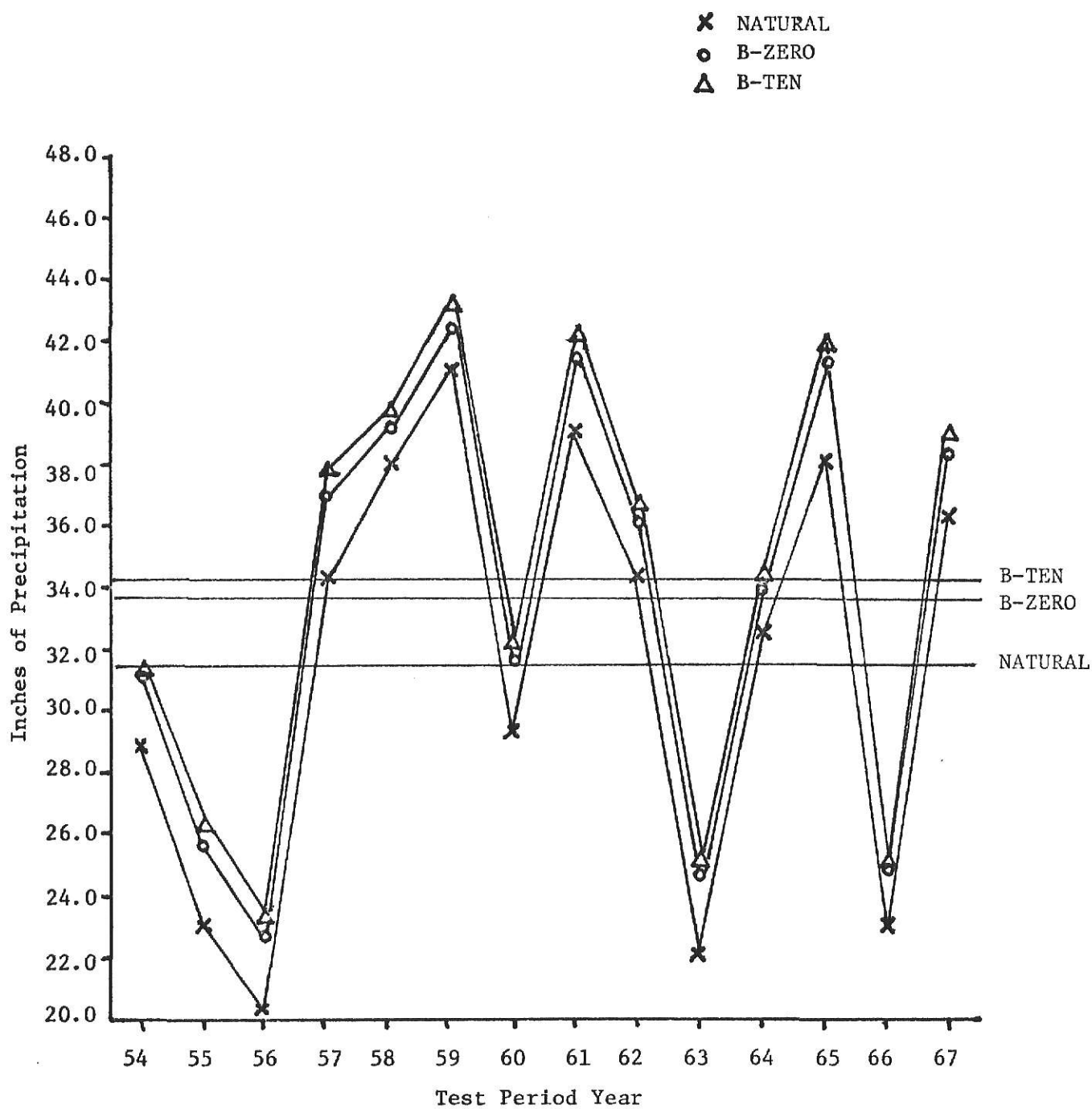


Fig. 6.--Precipitation for the Black Vermillion.

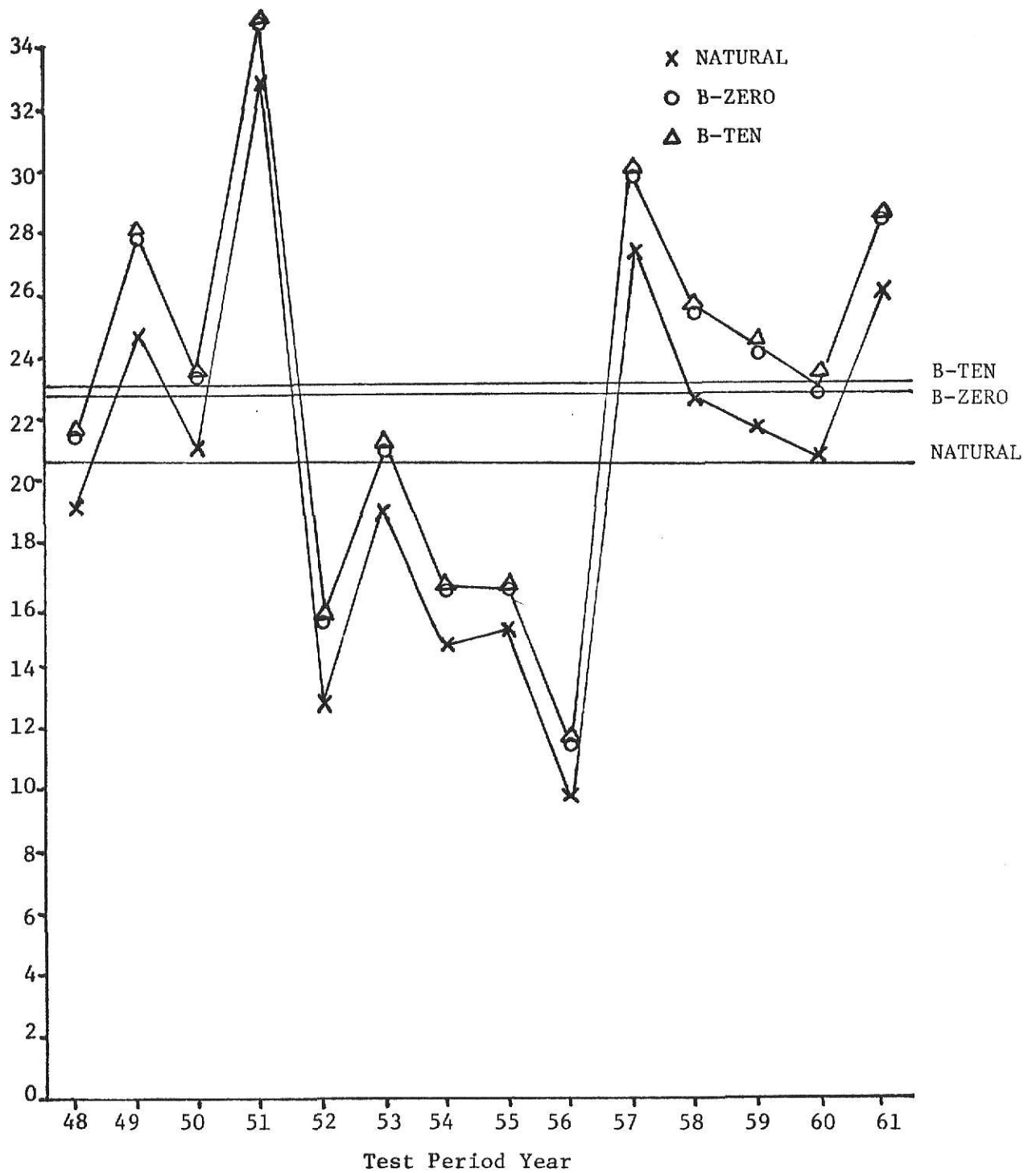


FIG. 7.--Precipitation for the South Fork Solomon

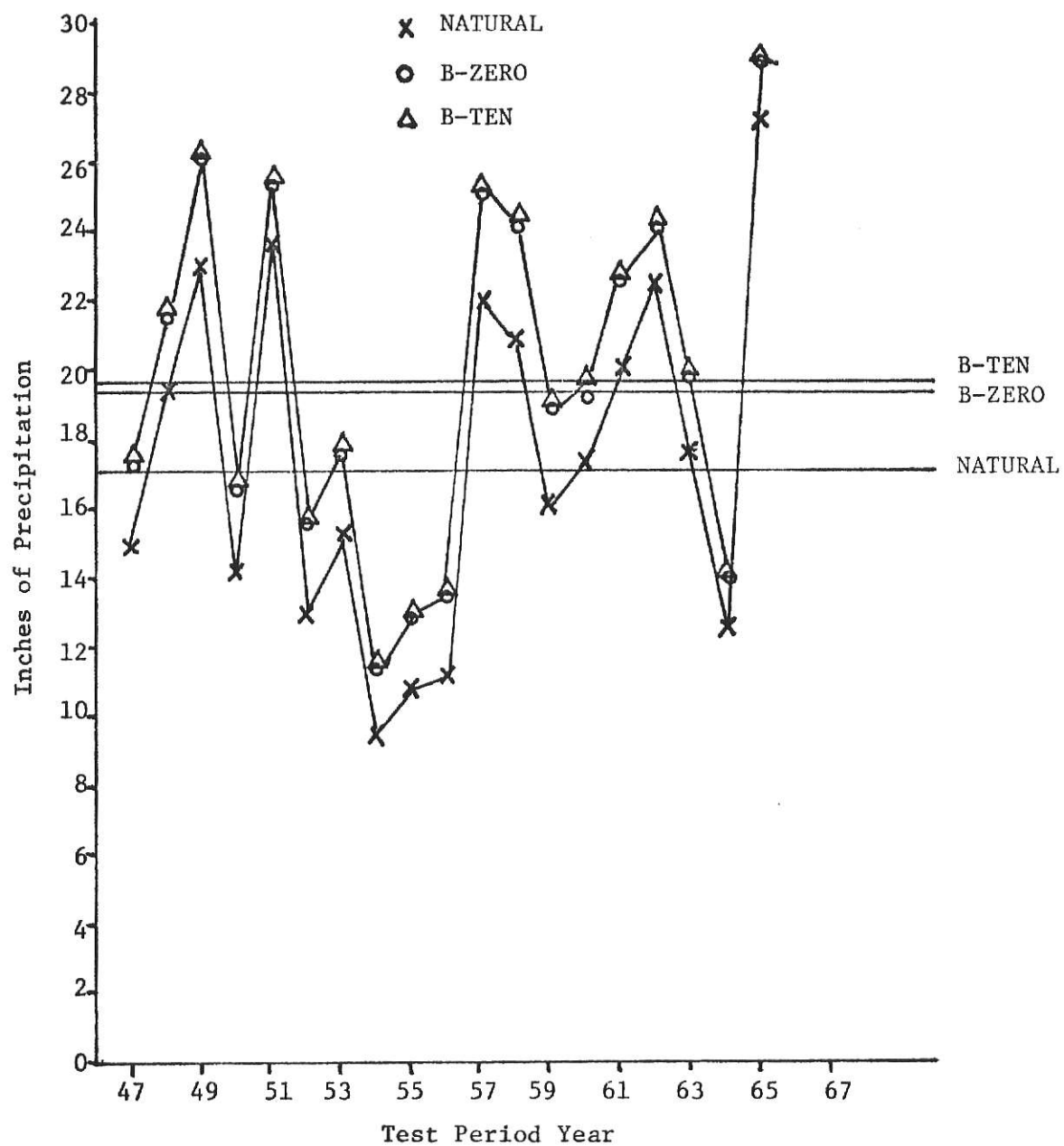


Fig. 8.--Precipitation for the Beaver Creek

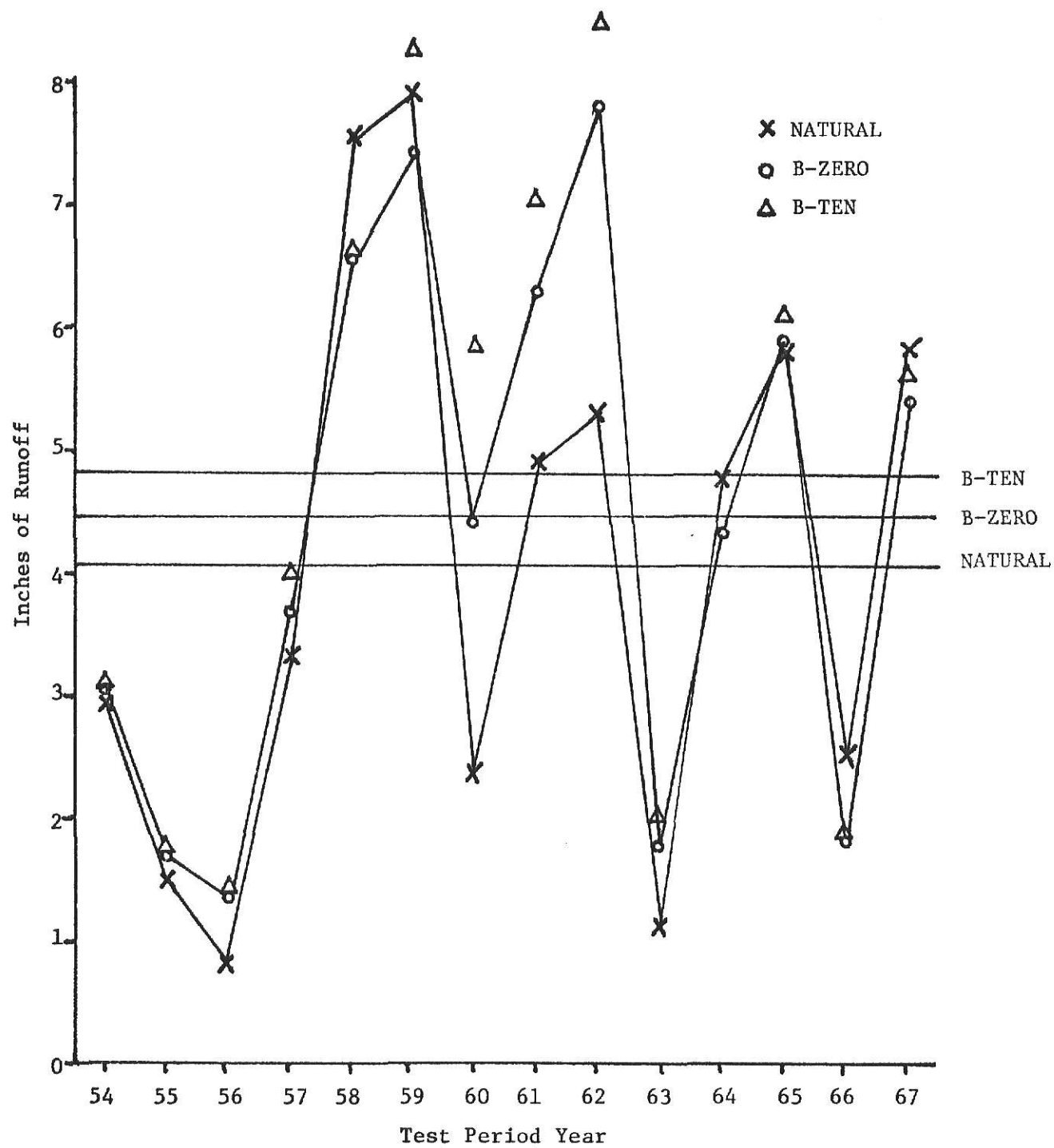


Fig. 9.--Runoff for the Black Vermillion.

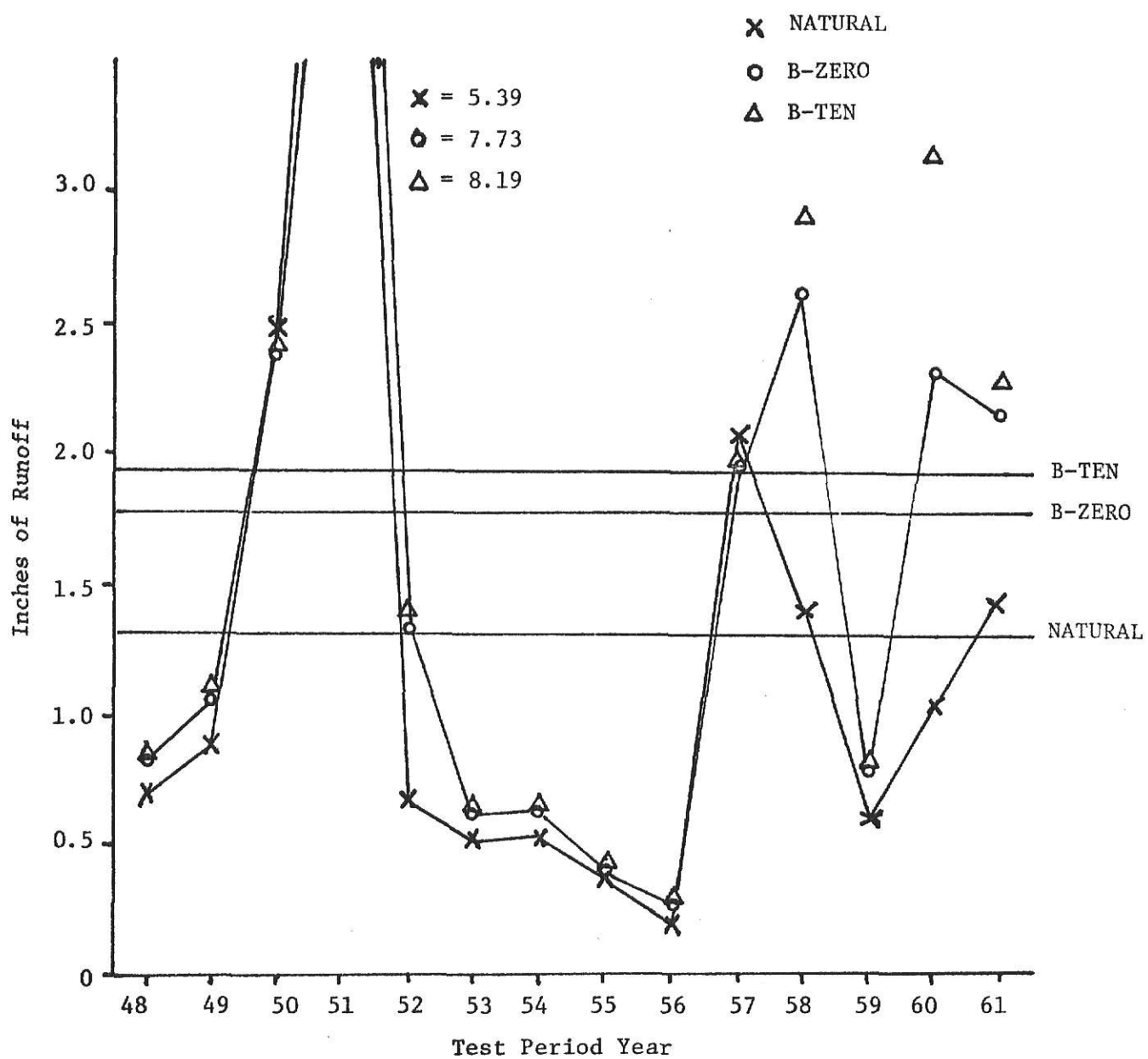


Fig. 10.--Runoff for the South Fork Solomon

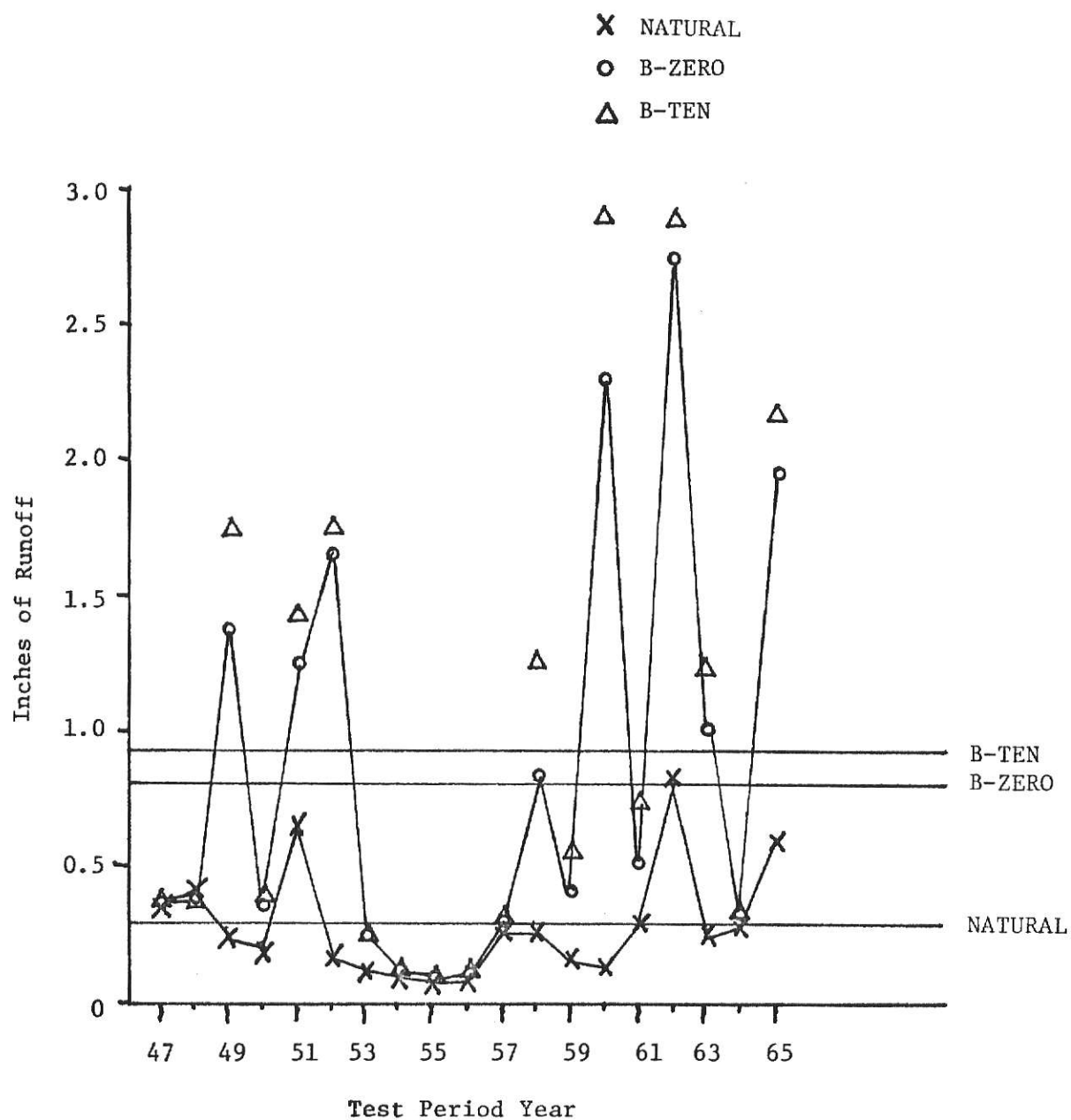


Fig. 11.--Runoff for the Beaver Creek

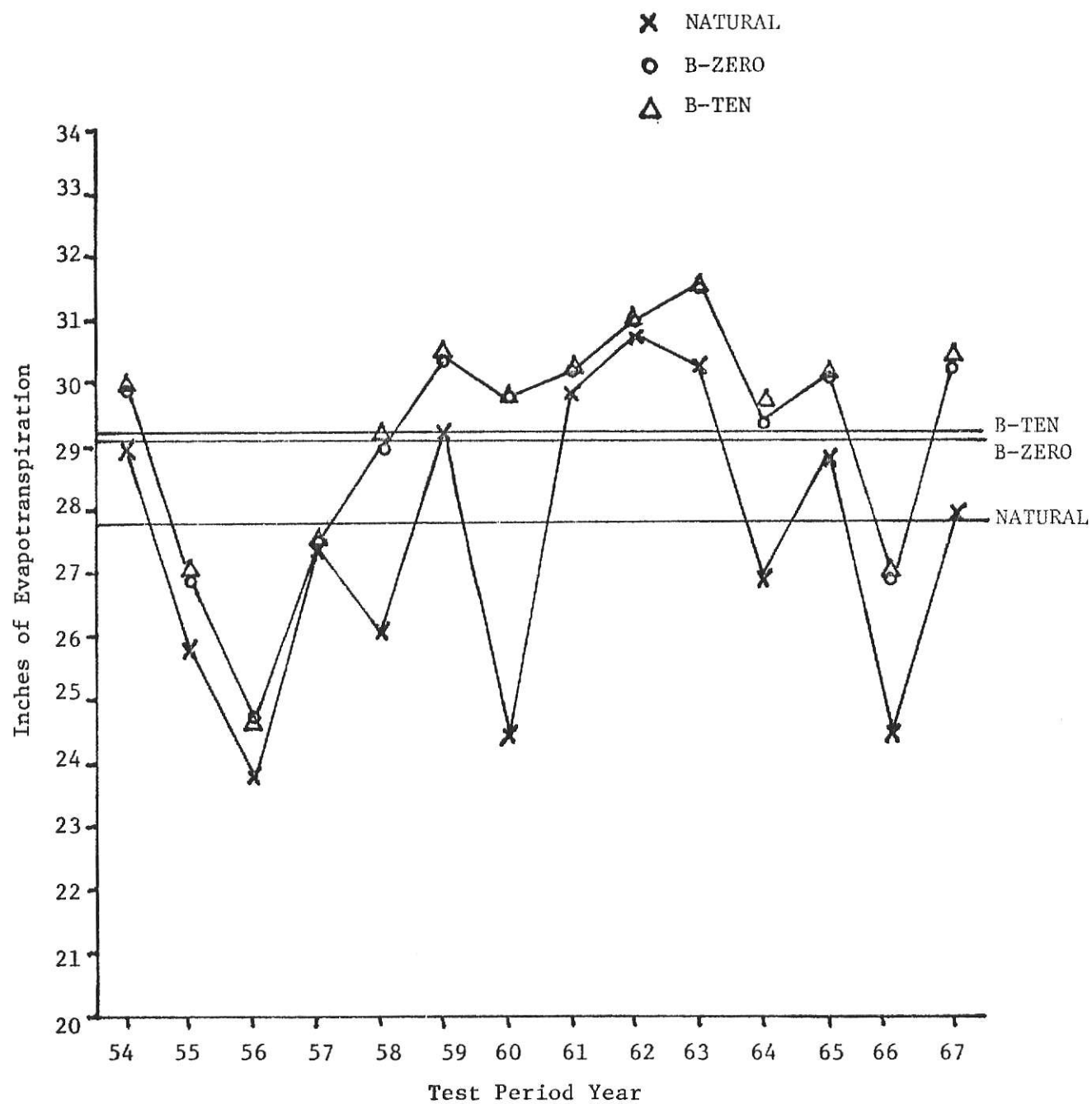


Fig. 12.--Evapotranspiration for the Black Vermillion.

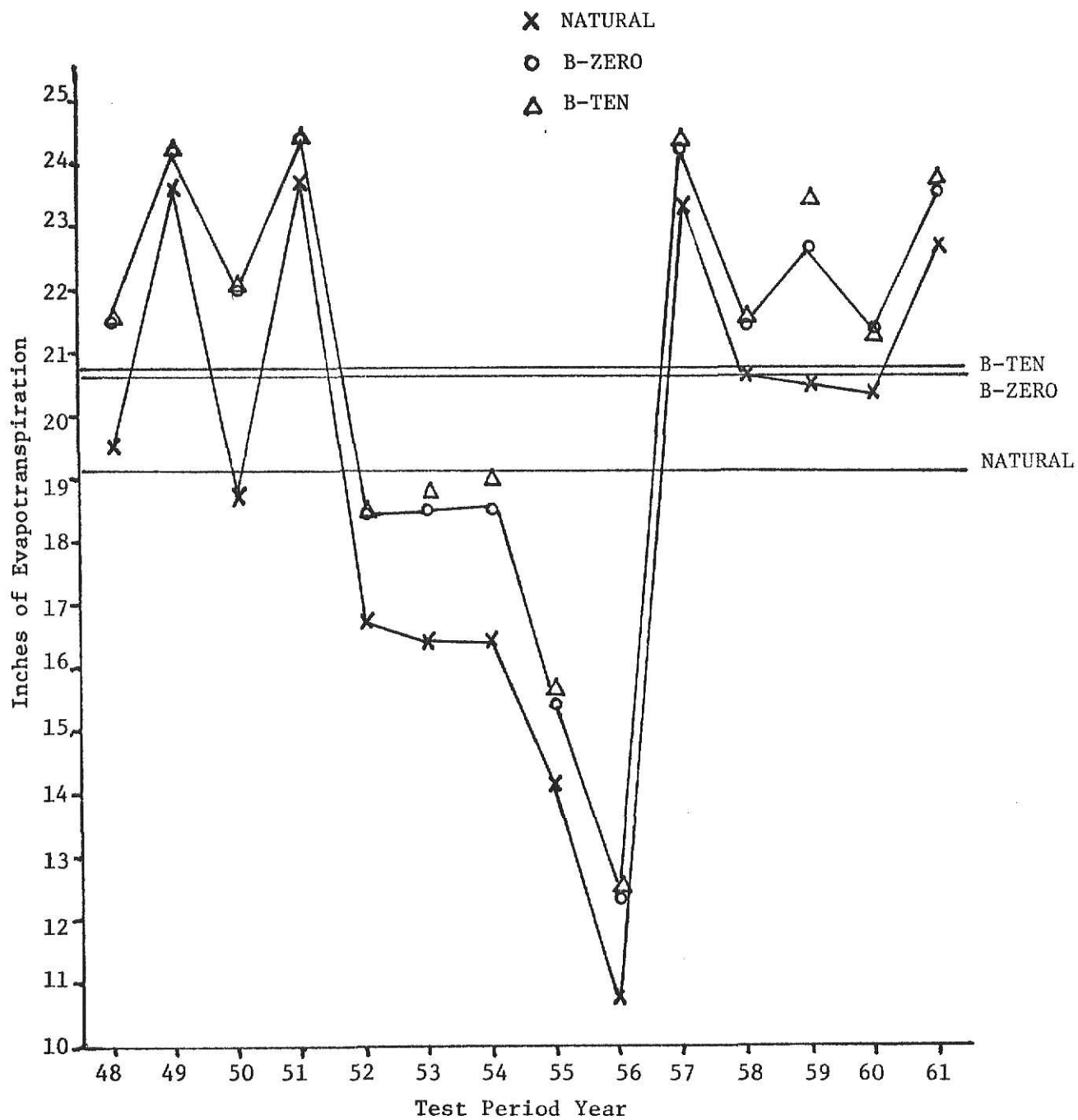


Fig. 13.--Evapotranspiration for the South Fork.

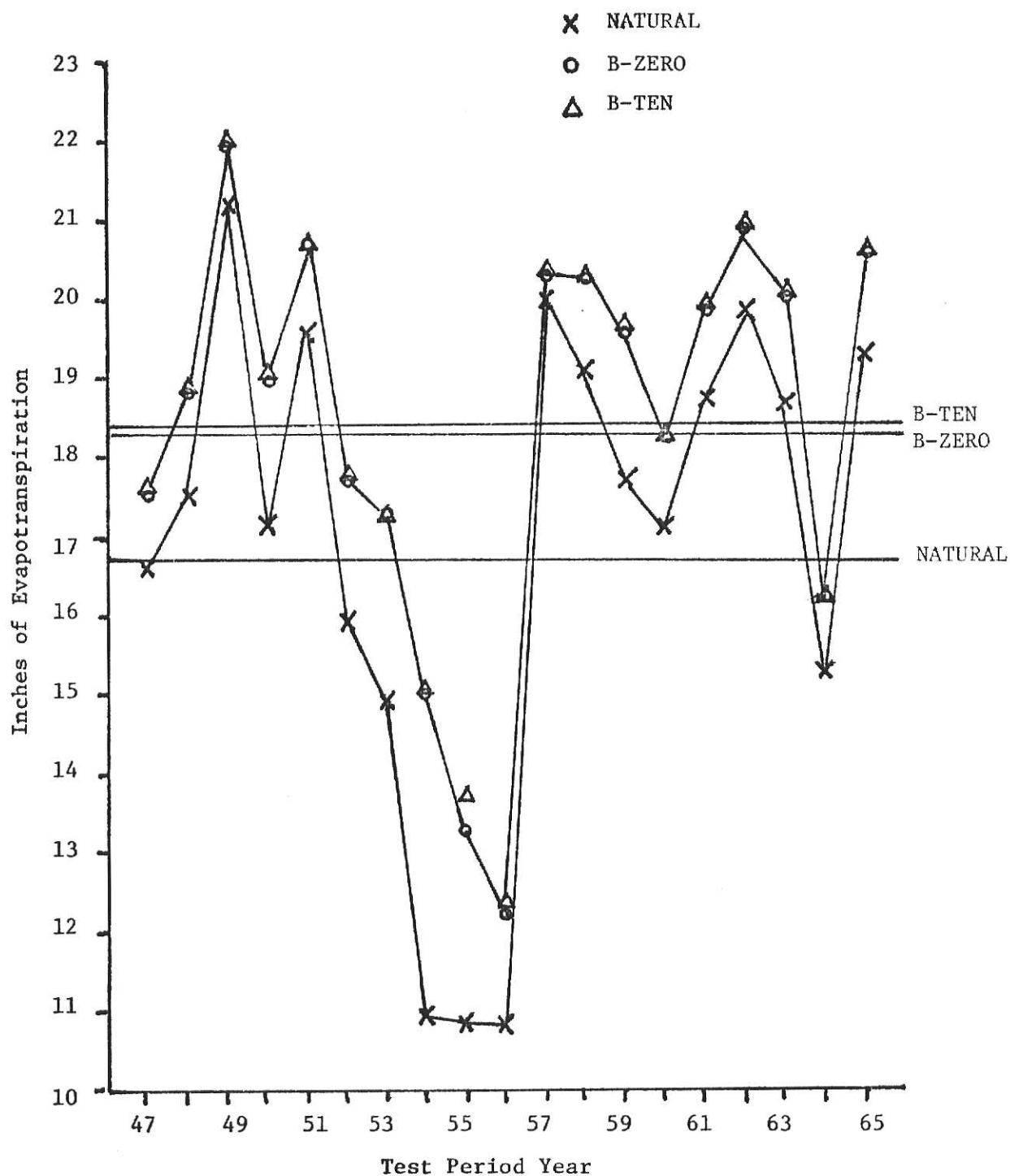


Fig. 14.--Evapotranspiration for the Beaver Creek.

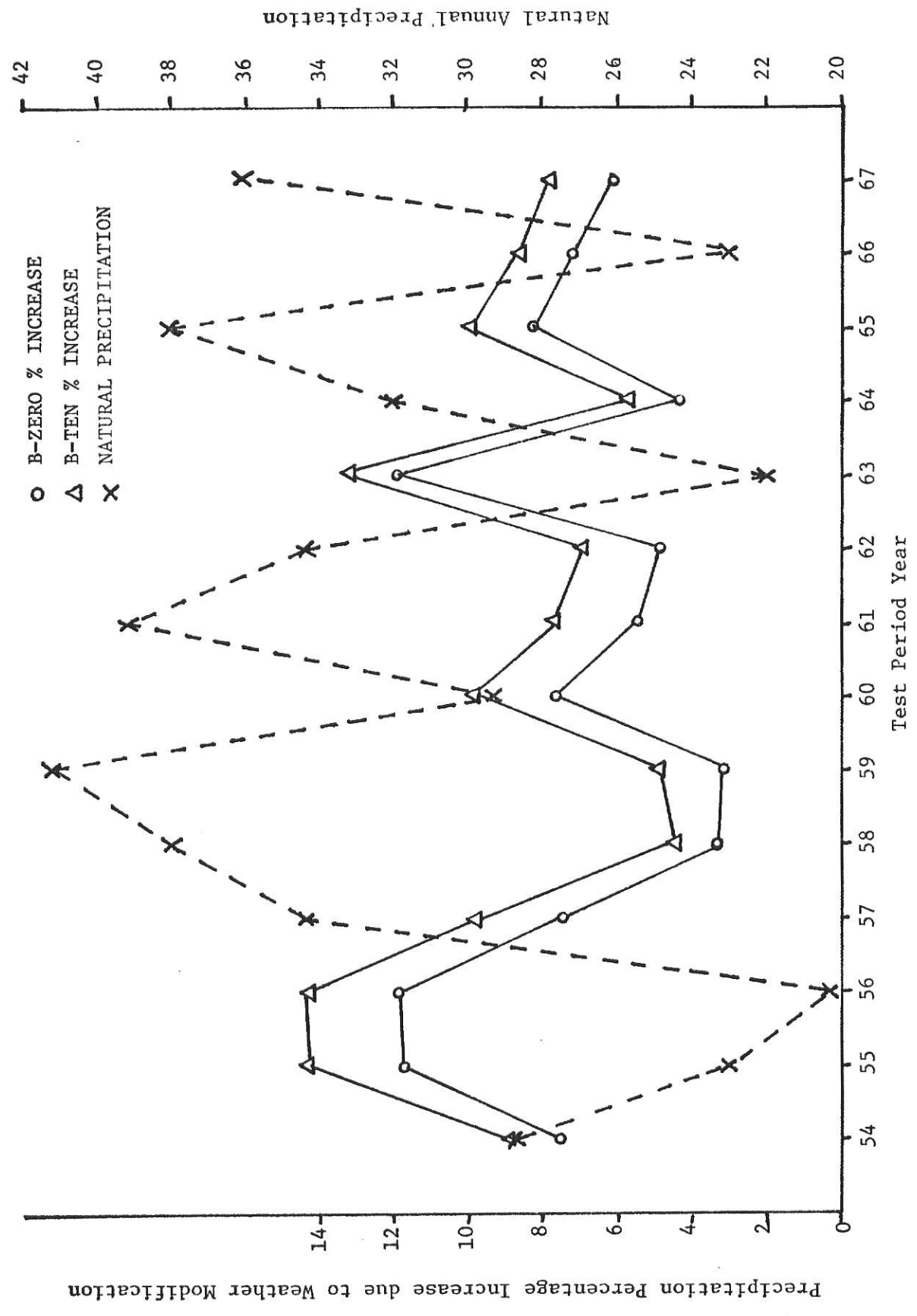


Fig. 15.--Percent Increase of Precipitation for Black Vermillion

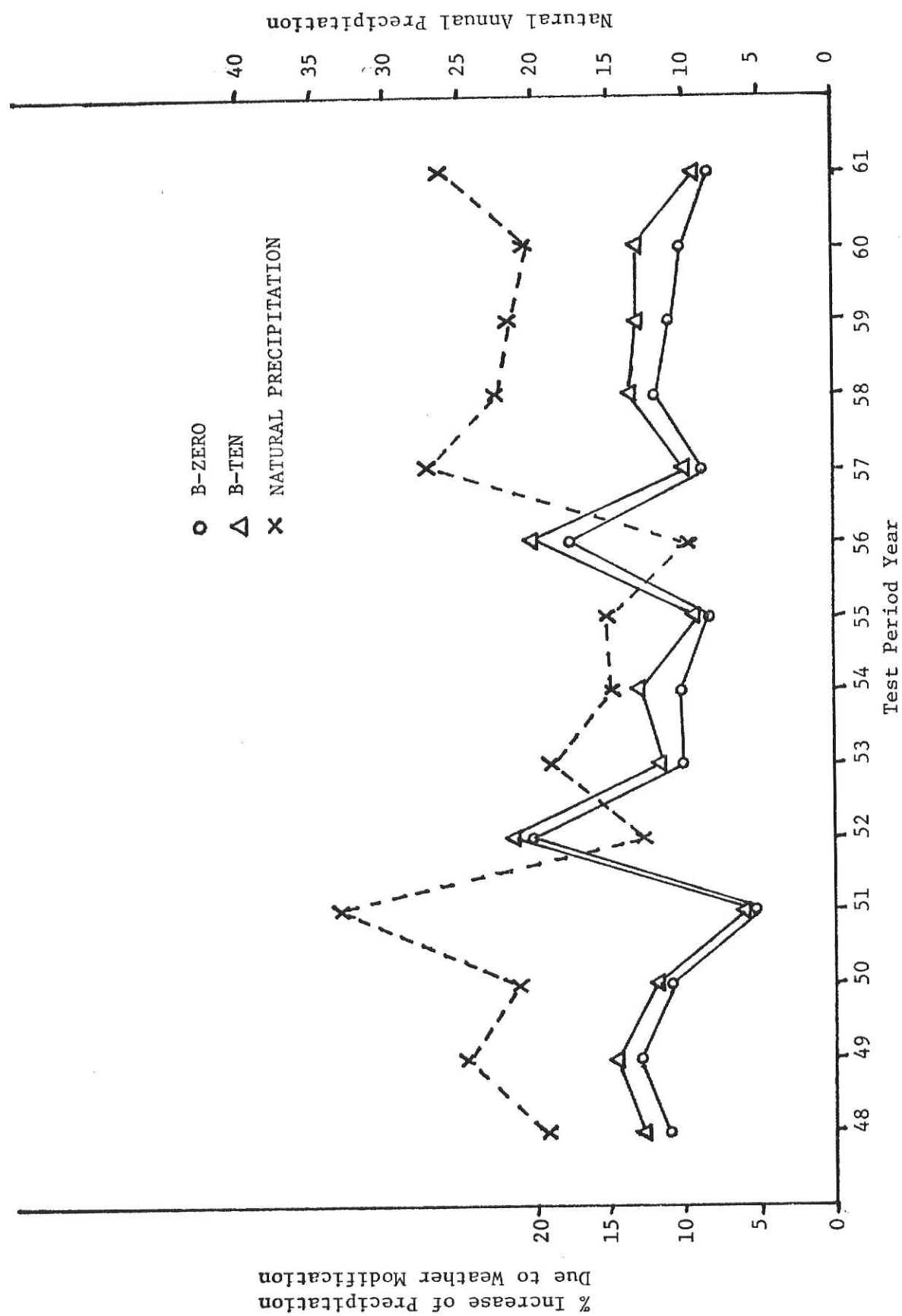


Fig. 16.--Percentage Increase of Precipitation for South Fork

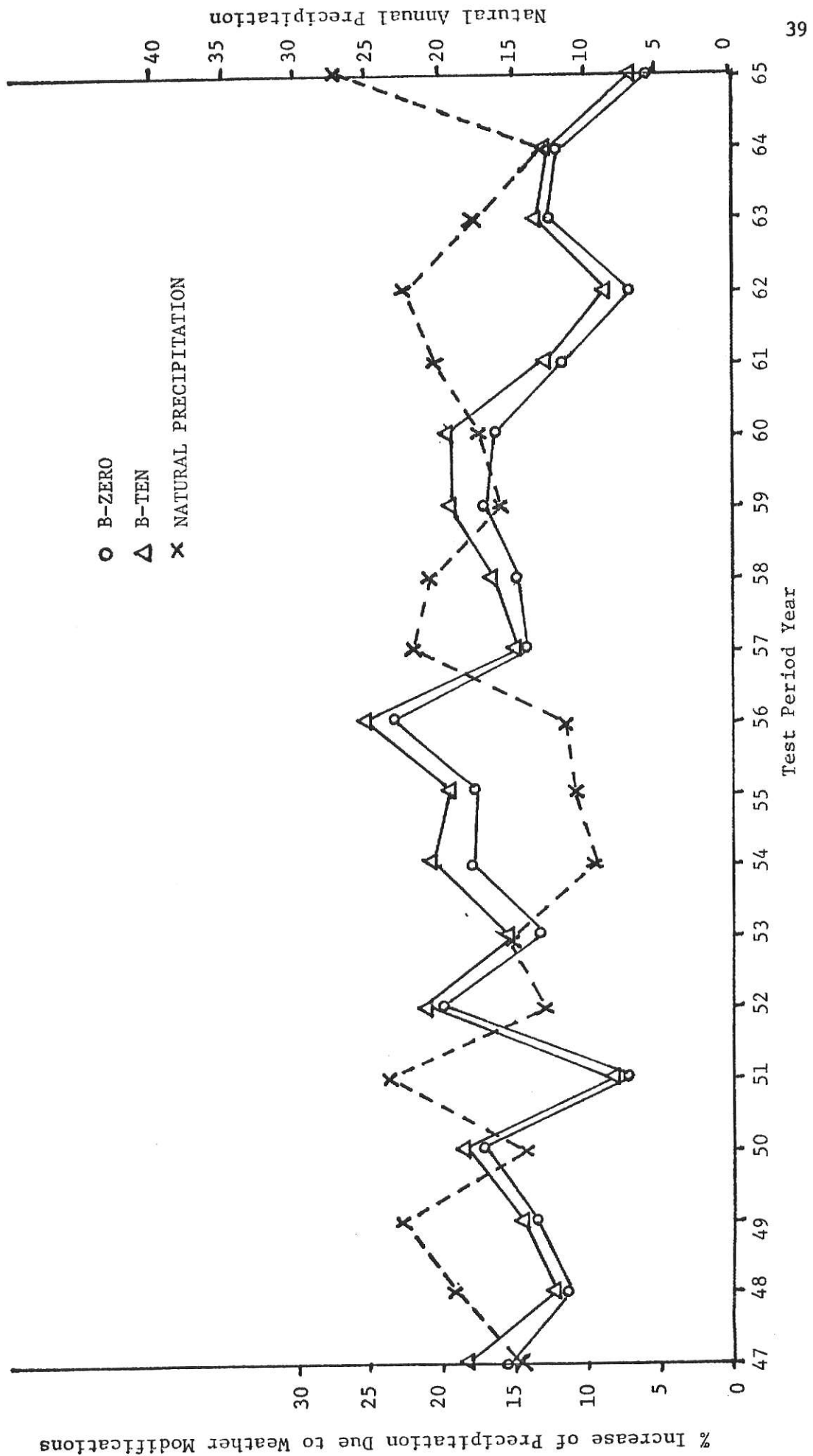


Fig. 17.--Percentage Increase of Precipitation for Beaver Creek

Test Period Year

% Increase of Precipitation Due to Weather Modifications

Natural Annual Precipitation

The South Fork Solomon has 7.48 cm (2.94 in.) net gain for its test period. The gain may seem large for this semiarid region, however, the test period ended on the relatively wet year of 1961. In 1961, 5.35 cm (2.11 in.) were added to storage accounting for most of the gain. This watershed also experienced a positive addition to storage due to the weather modification programs.

The Beaver Creek Basin also ended on an extremely wet year in 1965. This year added 18.17 cm (7.15 in.) to storage, which brought the storage budget from a deficit to a 10.88 cm (4.28 in.) gain. Beaver Creek experiences slight storage gains due to the precipitation enhancement.

Recharge.--The South Fork Solomon and the Beaver Creek Watersheds have one additional printout not included on the earlier completed Black Vermillion. This additional printout was the quantity of recharge from the lower zone to groundwater. Table 7 is a summary of the information generated. The results of weather modification on the amount of water passing through the lower zone is quite significant. Beaver Creek experienced no recharge under unmodified conditions but under modification averages of 1.54 cm (0.61 in.) and 1.86 cm (0.731 in.) per year were obtained for B-ZERO and B-TEN, respectively. The South Fork experienced only one year in which recharge occurred under unmodified conditions resulting in 0.41 cm (0.16 in.) average over the record period. B-ZERO and B-TEN modifications recharged an average of 1.74 cm (0.68 in.) and 2.06 cm (0.81 in.) per year.

TABLE 7.--Recharges for South Fork and Beaver Creek

Watershed	No. Years of Record	No. Years of Recharge	Total Recharge Centimeters (inches)	Average Recharge cm per yr (in per yr)
South Fork				
Natural	14	1	5.766 (2.270)	0.412 (0.162)
B-ZERO	14	4	23.305 (9.569)	1.736 (0.684)
B-TEN	14	5	28.867 (11.365)	2.062 (0.812)
Beaver Creek				
Natural	17	0	0 (0)	0 (0)
B-ZERO	17	9	26.208 (10.318)	1.542 (0.607)
B-TEN	17	9	31.824 (12.434)	1.872 (0.731)

CONCLUSIONS

The weather modification program B-ZERO resulted in average precipitation increases for the three watersheds of 6.72, 10.59, and 12.67 percent from the eastern Black Vermillion to the western Beaver Creek. This variability is significant since cloud seeding success is dependent on the number of events and the magnitude of the storm experienced in the area, as reflected in the Model B formulation. The wet-year, dry-year variation is also important. The dry years, due to the magnitude of increase for light rainfalls have increases comparable to those for wet years. Although it did not occur during any of the test years, B-ZERO could have reduced the total rainfall if enough of the storms were of high magnitude greater than one inch. It could also be possible to reduce the total rainfall for a given year and still experience better growing conditions, particularly if the

smaller magnitude storms were distributed properly throughout the growing season to provide the crop the necessary water requirements. The use of B-ZERO did result in reduced streamflows in some years, especially on the Black Vermillion, where higher runoff percentage naturally occur. The reductions are again the result of B-ZERO reducing the high magnitude storms. The soils at any location have only a certain capacity for surface storage and infiltration. When these are exceeded the remainder of the rainfall is essentially wasted in terms of crop utilization or benefit since it flows away through the drainage network. Any reduction of the storm size for a storm that exceeds the moisture retaining properties of the basin is reflected in reduced surface runoff. The reduction of runoff could have possible economic benefits in erosion control and flood damage suppression. The B-ZERO storms that are greatly enhanced are small enough that any additional rainfall from them could be fully utilized. It is the middle to high magnitude storm that is either enhanced or reduced that determines whether runoff is increased or decreased.

The increased runoff in the drier western watersheds may have a more important economic benefit. The additional runoff would add storage to ponds and reservoirs. In addition, a more reliable streamflow would benefit industries and municipalities that use the water.

The amount of evapotranspiration experienced and the reduction of the variability of this quantity is an important occurrence. In all cases the average ET is increased for the test periods by weather modification. The reduction of the variability of ET is largely due to the decreased percentage of the total budget it represents in modified conditions. This means more water is available for either runoff or storage. If the additional moisture is stored within the soil profile it allows the crop

to pull from this reserve in no rainfall situations. This carryover soil moisture effect is illustrated in Fig. 12 for the Black Vermillion. In 1960 the modified ET remains above average while the normal ET dropped to more than three inches below the average. The 1960 ET level remained high since 1959 was a wet year that replenished soil moistures. Other illustrations are less pronounced than this event.

A change in ET may be associated with a change in crop yield. The average ET increases, as presented earlier, are larger in the western regions where the water supply is more limited. Of the extra rainfall received on the Black Vermillion 60% of it was utilized as ET. The South Fork used 69% of the B-ZERO precipitation gain as ET and the Beaver Creek utilized 71% of extra precipitation as gain. Preliminary results from a different discipline on crop yields (1) support this trend. In the northwestern district of Kansas the average effect of B-ZERO on wheat yields was an annual increase of 2.18 hectoliters per hectare (2.50 bushels per acre), while the Black Vermillion in the northeast district had only a predicted yield increase of 0.02 hectoliters per hectare (0.03 bushels per acre).

Groundwater recharge under natural conditions for northwest Kansas is near zero. Only in 1951, with heavy rainfalls for two months, did recharge occur in the South Fork Solomon. The enhanced rainfalls always increased the recharge, both in absolute quantity and in frequency of occurrence. Increased recharge due to weather modification would have a very limited effect on extending diminishing groundwater supplies because of the small increases involved.

The effects of the winter uniform percentage increase, B-TEN, are difficult to evaluate in terms of benefits gained for the expenditure

required. B-TEN resulted in only small increases above the B-ZERO amounts. The Black Vermillion received an extra 1.42 cm (0.56 in) per year from B-TEN above B-ZERO. Of that amount, 0.86 cm (0.34 in.) per year were added to runoff. The remaining 0.56 cm (0.22 in.) per year resulted in additional ET. The drier basins in the west, where winter precipitation enhancement is less than the Black Vermillion, received 0.74 and 0.56 cm (0.29 and 0.22 in.) per year increases by modification for the South Fork and the Beaver Creek, respectively. This extra amount was split almost in half in allocation to runoff and to ET. The smaller increases afforded by B-TEN seem insignificant and hardly justifiable to extend weather modification the additional five months.

In summary, these conclusions of this report are enumerated as follows:

- 1) The precipitation enhancement program, Model B, provides a realistic approach to modeling weather modification activities by allowing variable percentage increases based on the number and magnitude of precipitation events. This results in more uniform absolute increases in precipitation for wet and dry years and for wet and dry regions.
- 2) The precipitation enhancement program, Model B, effected streamflows in a varying manner. The streamflows were increased or decreased as a function of the number and magnitude of events falling into the different levels of precipitation enhancement.
- 3) Both enhancement schemes resulted in an average ET increase and a decrease in the variability of ET. Carryover effects of increased soil moisture possibly accounts for the reduced variability.

- 4) Both enhancement schemes increased the recharge for the two western watersheds. The increases are not large enough to be of significance in augmenting groundwater supplies.
- 5) There is a relatively insignificant difference between the precipitation enhancement programs B-ZERO and B-TEN. The additional five months of winter operation does not produce significant additional rainfall, runoff, ET, carryover effects or recharge.

APPENDIX I - REFERENCES

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APPENDIX II - SELECTED WATERSHED PRINTOUT

KANSAS WATERSHED MODEL PROGRAM

ILLEGIBLE DOCUMENT

**THE FOLLOWING
DOCUMENT(S) IS OF
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THE ORIGINAL**

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0001 DIMENSION IBUF(11000)
0002 DIMENSION FLOW(368), SIMQ(368), AFT(368), PET(368)
0003 DIMENSION TEMP(368), WMP(368), DAY(368), CCM(12), CCSG(12), CGC(12)
0004 DIMENSION SUSU(10), FAX(9,24), CCSR(12), CCP(12), CCA(12), CCF(12)
0005 DIMENSION P3UMS(12), RHD(12), RAI(12), WIND(12)
0006 COMMON TOTAL(13,27), MONH(15), CKN(20), MMTH(12,6), CK(20), UZS(20),
1 PLTR(4,31), P24(20), CSE(24), SERR(24), SERA(24), SIZ(4),
2 CASI(24), SQER(24), AVAR(24), AVER(24), PI(24), P2(24),
3 DPTH(20), RPR(9), SRX(9), ICHAR(121), LZST(10), IFL(10)

0007 INTEGER ACT,LY
0008 REAL IFW,IIA,LZSA,LZST,LZSU,LZZTN,IA,IBI,IMI,LZSTN
0009 REAL LZSAN,LZSO,LZMX,LZMN,IKR,IFL,LZSTZ
0010 REAL ETP,ETA,T,ABST
0011 REAL TAU,R,ES,ESA,CENT,ETPH,CCREL,IMAX,IMIN,ETPS
0012 REAL LETA,KSU,KCW,KCSG,KCC,KCP,KCA,KCSR,KCS
0013 REAL KWM,KWSC,KWC,KWSH,KWP,KWA
0014 DATA CCW/0.30,0.40,0.60,0.85,1.10,1.06,0.0,0.0,0.45,0.60,0.30/
0015 DATA CCSG/0.0,0.0,0.0,0.0,0.0,0.25,0.85,1.10,0.75,0.30,0.0,0.0/
0016 DATA CCF/0.0,0.0,0.0,0.0,0.0,0.15,0.45,1.0,1.0,0.85,0.60,0.0,0.0/
0017 DATA CCSR/0.0,0.0,0.0,0.0,0.0,0.35,0.95,0.75,0.0,0.0,0.0,0.0/
0018 DATA CCP/0.0,0.0,0.0,0.50,0.65,0.90,0.85,0.85,0.90,0.55,0.0,0.0/
0019 DATA CCA/0.0,0.0,0.0,0.55,0.70,0.90,1.0,1.0,0.85,0.60,0.0,0.0/
0020 DATA CCF/0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0/
0021 NAMELIST/ DATA/ SRI,SMI,IRI,IMI,UZSN,URP,UMP,UZMX,UZMN,LZMX,LZMN,
*ETRO,M,X,Y,STRT,IKR,PCL,RGWB,RGWM,GWSN,BK,AGM,PDY,TLL,LZSAN,LZSTN,
*AREA,UZSO,LZSG,GWSN,YREND,GWRP,PORF,IIA,GWMN,PTPOND,ETR,FM,POWER,
*PWRE,QUANTY,R,C,PONDDP,PONDAR,ZZT,MODEL,MPCNT
CALL PLOTS (19UF,11000)
CALL ORIGIN (2.5,1.5,11.0)
READ(5,1010)(MONH(K),K=1,13)
1010 FORMAT(13A6)
1015 READ(5,1015)((MMTH(J,K),K=1,6),J=1,12)
1015 FORMAT(72A1)
1012 WRITE(6,1012)
1012 FORMAT(2H1 )
C THE CKN(J) ARRAY IS FOR THE 6-HOUR INCREMENTAL VALUES OF THE UNIT HYDROGRAPH*
READ(5,1009) (CKN(J),J=1,20)
WRITE(6,919)
919 FORMAT(15X,'THE 6-HOUR INCREMENTAL VALUES OF THE UNIT HYDROGRAPH*')
1009 WRITE(6,1009)(CKN(J),J=1,20)
1009 FORMAT(10F8.4)
READ(5,DATA)
WRITE(6,DATA)
C CALCULATION OF CONSTANTS AND SETTING INITIAL VALUES
PACK=0.0
NSTRT=YSTRT
NEND=YEND
LL=TLL+5
TAREA=AREA
AREA=AREA-PCNDAR/640.
ARFAX=AREA*26.9
UZS=0.0
STORGE=1500.
PONDDL=PCNDP*PONDAR
UDELT=UZMX-UZSN
DELT=LZMX-LZSAN
PCU=1.0-PCL
WFI=AREA* (-ALOG(IKR))

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0051 PFR=(1.0-ACK)
0052 IZTN=I/STN
0053 FCT=PER/(LZMX**POWER-LZZTN**POWER)
0054 UPR=PER-FCT*(LZMX**POWER)
0055 DIF=(LZMX-LZZTN)/10.
0056 FRAREA=AGW*(-ALOG(BK))
0057 AE=1.0/(LZMX*AGW)
0058 FCTP=0.97/(132.**POWER)
0059 FCTP2=(.03)/(10000.-132.)
0060 DO 3 L=6,LL
0061 3 UZS(L)=UZSN
0062 DO 111 K=1,10
0063 111 LZST(K)=LZSO
0064 LZSA=LZSN
0065 GWS=GWSC
0066 DO 20 L=6,LL
0067 CK(L)=0.0
0068 20 DEPTH(L)=0.0
0069 DO 409 K=1,7
0070 409 RRO(K)=0.0
0071 DO 903 J=1,24
0072 CSE(J)=0.0
0073 CAS(J)=0.0
0074 SFR(J)=0.0
0075 SFRAL(J)=0.0
0076 S(J)=0.0
0077 903 SQR(J)=0.0
0078 DO 919 JIG=1,8
0079 919 SUSU(JIG)=0.0
0080 RAL=0.0
0081 AIA=0.0
0082 SFA=0.0
0083 SFEYAF=0.0
0084 NV=0
0085 CUS=0.0
0086 CLS=0.0
0087 TIME=0.0
0088 R=0.23
0089 READ(5,50) (PSUMS(I),RHO(I),RA(I),WIND(I),I=1,12)
0090 50 FORMAT(2X,F2.2,F2.0,F4.2,F3.1)
0091 C BEGIN YEARLY LUCP
0092 DO 909 NNN=NSTRT,NEND
0093 ACT=1
0094 DO 901 KK=1,13
0095 DO 901 K=1,27
0096 901 TOTALM(KK,K)=0.0
0097 AIA=0.0
0098 EPV=0.0
0099 YSTN=0.0
0099 YSDACQ=0.0
0100 YSDSYQ=0.0
0101 READ(1,4444) (TOTALM(LK,8),LK=1,12)
0102 WRITE(6,4443)
0103 4443 FORMAT(10*,1X,'AVERAGE MONTHLY BASE FLOW')
0104 4444 WRITE(6,4444) (TOTALM(LK,8),LK=1,12)
0105 4444 FORMAT(12F6.1)
0106 C CK(J)=THIESSEN COEFFICIENTS
0107 READ(1,220) (CK(J),J=8,14),LV

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06500

06900

07000

07100

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07300

07400

07500

07600

07700

07800

07900

08100

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0137      220 FORMAT(7F10.4,8X,I2)
0108      CK(18)=0.2302
0109      CK(11)=0.0
0110      CK(12)=0.3691
C PERCENTAGE OF THE WATERSHED COVERED BY WHEAT SORGHUM CORN SOYBEAN
C PASTURES ALFALFA CROPS.
0111      CKW=0.0882
0112      CKSG=0.2346
0113      CKC=0.0449
0114      CKSR=0.0281
0115      CKP=0.5571
0116      CKA=0.0471
0117      WRITE(6,505) LY
0118      505 FORMAT('0',5X,'LEAP YEAR INDICATOR=',I2,5X,'YES=1 & NO=0')
0119      READ(1,123) ITHAW,IFREZ,IYEAR
0120      WRITE(6,122)
0121      122 FORMAT('0',2X,'ITHAW',3X,'IFREZ',59X,'YEAR')
0122      WRITE(6,123) ITHAW,IFREZ,IYEAR
0123      123 FORMAT(2I8,60X,I4)
0124      K9=24
0125      NTD1=1
C BEGIN MONTHLY LOOP
0126      DO 888 NN=1,12
0127      IDY=31
0128      IF(NN.EQ.4.OR.NN.EQ.6.OR.NN.EQ.9.OR.NN.EQ.11)IDY=30
0129      IF(NN.EQ.2) IDY=28+LY
C CROP COEFFICIENTS FOR WHEAT
0130      KCW=CCW(NN)
C CROP COEFFICIENTS FOR SORGHUM
0131      KCSG=CCSG(NN)
C CROP COEFFICIENTS FOR CORN
0132      KCC=CCC(NN)
C CROP COEFFICIENTS FOR SOYBEANS
0133      KCSR=CCSR(NN)
C CROP COEFFICIENTS FOR PASTURES
0134      KCP=CCP(NN)
C CROP COEFFICIENTS FOR ALFALFA
0135      KCA=CCA(NN)
0136      TOTAL(MNN,8)=TOTALM(MNN,8)
0137      NTD2=NTD1+IDY-1
0138      XIDY=IDY
0139      XIDY=1.0/XIDY
0140      SOTO=0.0
0141      SDACO=0.0
0142      SDSYO=0.0
0143      NCZ=0.0
C BEGIN DAILY LOOP
0144      DO 777 N=NTD1,NTD2
0145      READ(1,221)(P24(J),J=1,LL)
0146      221 FORMAT(2X,F7.0,3X,F7.1,3X,F2.0,2X,F4.0,1X,F4.0,9(1X,F4.2))
0147      DO 1111 J=6,LL
0148      IF(P24(J).GT.PDY) GO TO 1112
0149      1111 CONTINUE
0150      GO TO 4269
0151      1112 READ(1,607) PDATE,(PI(J),J=1,24)
0152      607 FORMAT(1X,F7.0,24F3.2)
0153      TIME=-1
0154      4269 NCZ=NCZ+1

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10800
10900
11600
11700
11800
11900
12000

12100
12200
12400
12500
12600
12700
12800
12900
13100
13200
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13500
13600

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0155 TIME=TIME+1
0156 NV=NV+1
0157 DO 622 K=1,6
0158 RRR(K)=RRR(K+1)
0159 622 SRX(K)=0.0
0160 613 TPERC=0.0
0161 AUZS=0.0
0162 TPA=0.0
      C CALCULATION OF POTENTIAL ET USING PENMAN COMBINATION EQUATION
0163 T=(P24(4)+P24(5))/2
0164 TMEL=T
0165 IF(T.LT.0.0) T=0.0
0166 CENT=100*(1-32)/180)
0167 ABST=CENT+273.16
0168 ES=33.9*(10.00738*CENT+0.8072)**8-0.000019*ABS(1.8*CENT+48)
      1 *0.00136)
0169 ESA=ES*RRR(NN)/100
0170 RNE=(1-R)*RA(NN)=(0.22+0.54*PSUNS(NN))-2.010E-09*ABST**4*(0.98-0.68
      1 -0.036*SOFT(ESA))*(0.1+0.9*PSUNS(NN))
0171 WVD=(WIND(NN)*24)*(ALOG10(6.6)/ALOG10(30.1))
0172 EA=0.26*(0.75+0.01*WVD)*(ES-ESA)
0173 DELTA=0.039*T**0.673
0174 GUM=1-DELTA
0175 FE=(DELTA*RN)+(GUM*EA)
      C FE IN MM, RA IN MM, ABST IN DEG, K, ES & ESA IN MB,
      C WVD IN MILES, (LANGLEYS OR CAL/CM2)*0.0171=MM
0176 IF(EE.LT.0.0) EE=0.0
0177 ETP=EE/25.39998
0178 ETPH=ETP/24
0179 ETPS=ETP*(PCNDAR/(640*AREA))
0180 D7 623 L=6,LL
0181 M=L-5
0182 RX(M,12)=0.0
0183 CALL WTCMOD(P24(L),NN,MODEL,WPCNT)
0184 IF(P24(L).GT.PDY) GO TO 615
0185 TPA=TPA+P24(L)*CK(L)
0186 RAN=P24(L)
0187 IF(P24(L).LE.0.0) GO TO 22
0188 IA=IR1-IM1*UZS(L)
0189 IF(UZS(L).LT.UZS) IA=8-C*UZS(L)
0190 IF(IA.LT.IIA) IA=IIA
0191 DIFF=IA-DEPTH(L)
0192 IF(DEPTH(L).GE.IA) DIFF=0.0
0193 IF(DIFF.GE.P24(L)) GO TO 23
0194 DEPTH(L)=DEPTH(L)+DIFF
0195 P24(L)=P24(L)-DIFF
      GO TO 22
0196 23 DEPTH(L)=DEPTH(L)*P24(L)
0197 P24(L)=0.0
0198 22 DEPTH(L)=DEPTH(L)-ETP
0199 IF(DEPTH(L).LE.0.0) DEPTH(L)=0.0
0200 71 IF(P24(L).LE.FM) GO TO 726
0201 SNN=SRI-SM1*UZS(L)
0202 IF(SNN.LT.0.0) SNN=0.0
0203 RX(M,12)=(P24(L)*P24(L))/(P24(L)+SNN)
0204 IF((P24(L)-RX(M,12)).LT.FM) RX(M,12)=P24(L)-FM
0205 SRX(12)=SRX(12)+RX(M,12)*CK(L)
0206 726 PERC=0.0
0207
14200
14300
14400
14500
14600
14700
14800
15500
15700
15800
15900
16000
16100
16200
16300
16400
16500
16600
16700
16800
16900
17000
17100
17200
17300
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17900
18000
18100

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0208      AATA=AAIA+(RAN-P24(L))*CK(L)
0209      EXCESS=UZZS(L)-UZZN
0210      DO 873 K=1,10
0211      IF(EXCESS-PEPC)876,876,873
0212      873 PERC=PERC+UBP*((EXCESS-PERC)/(UZZM-UZZN))*UMP/10.
0213      876 UZS(L)=UZS(L)+P24(L)-RX(M,12)-PERC
0214      TPERC=TPERC+PERC*CK(L)
0215      GO TO 729
0216
0217      615 K99=0
0218      IF(M.LE.7) K99=0
0219      DO 728 J=1,24
0220      K9=J+K99
0221      P12=P11(K9)*P24(L)
0222      TPA=TPA+P12*CK(L)
0223      RAN=P12
0224      IF(P12.LE.0.0) GO TO 5
0225      IA=IR1-IM1*UZS(L)
0226      IF(UZS(L).LT.UZZS)IA=8-C*UZS(L)
0227      IF(IA.LT.11)IA=11A
0228      DIFF=IA-DEPTH(L)
0229      IF(DEPTH(L).GE.1A) DIFF=0.0
0230      IF(DIFF.GT.P12) GO TO 6
0231      DEPTH(L)=DEPTH(L)+DIFF
0232      P12=P12-DIFF
0233      GO TO 5
0234
0235      6 DEPTH(L)=DEPTH(L)+P12
0236      P12=0.0
0237
0238      5 DEPTH(L)=DEPTH(L)-ETPH
0239      IF(DEPTH(L).LE.0.0) DEPTH(L)=0.0
0240      RX(M,J)=0.0
0241      IF(P12.LE.FM) GO TO 17
0242      SNN=S81-SM1*UZS(L)
0243      IF(SNN.LT.0.0) SNN=0.0
0244      RX(M,J)=(P12-P12)/(P12+SNN)
0245      IF(P12-PX(M,J).LT.FM) RX(M,J)=P12-FM
0246      IF(PX(M,J).LE.0.0) RX(M,J)=0.0
0247      I=(J+5)/6
0248      SRX(I)=SRX(I)+RX(M,J)*CK(L)
0249
0250      17 PERC=0.0
0251      AATA=AAIA+(RAN-P12)*CK(L)
0252      EXCESS=UZZS(L)-UZZN
0253      IF(EXCESS.GT.0.001)PERC=UBP*(EXCESS/UDELTA)*UMP/24.
0254      UZS(L)=UZS(L)+P12-RX(M,J)-PERC
0255      IF(UZS(L)-UZZX) 30,30,40
0256      40 RX(M,J)=RX(M,J)+UZS(L)-UZZX
0257      I=(J+5)/6
0258      SRX(I)=SRX(I)+(UZS(L)-UZZX)*CK(L)
0259      UZS(L)=UZZX
0260      30 TPERC=TPERC+PERC*CK(L)
0261      728 CONTINUE
0262      729 UZS(L)=UZS(L)-CUZS
0263      IF(UZS(L).LT.0.0) UZS(L)=0.0
0264      AUZS=AUZS+UZS(L)*CK(L)
0265      623 CONTINUE
0266      IF(AUZS.LE.UZMN) AUZS=0.0
0267      A7=SRX(1)+SRX(2)+SRX(3)+SRX(4)
0268      C ROUTING
0269      IF(A7)83,83,84
0270
0271      83500
0272      23600
0273      23700
0274      23800
0275      23900

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0317      RTW=((KCSG*KS)+KHW)
0318      RTSG=((KCSG*KS)+KMSG)
0319      RTC=((KCC*KS)+KWC)
0320      RTS9=((KCSR*KS)+KWSB)
0321      RTP=((KCP*KS)+KWP)
0322      RTA=((KCA*KS)+KWA)
0323      ETAW=RTW*ETP
0324      ETASG=RTSG*ETP
0325      ETAC=RTC*ETP
0326      ETASB=RTS9*ETP
0327      ETAP=RTP*ETP
0328      ETAA=RTA*ETP
0329      C DETERMINATION OF ACTUAL EVAPOTRANSPIRATION
0330      ETA=(ETAW*CKW+ETASG*CKSG+ETAC*CKC+ETASB*CKSB+ETAP*CKP+ETAA*CKA)*
0331      IO=.846*AREA/TAREA
0332      UETA=PCU*ETA
0333      CUZS=UETA
0334      CLZS=LFTA
0335      TETA=ETPS+UETA+LETA
0336      C POND ROUTINE
0337      RR=RRF(1)*AREAX
0338      ETTT=(ETP*PONDAR)/12
0339      CFSIN=0.0
0340      CFSOUT=0.0
0341      CFSQ=RR+IFW*TPA*PONDAR*26.9/640.0
0342      IF(CFSQ.LE.0.0) GO TO 333
0343      CFSIN=CFSQ*PTPOND
0344      CFSOUT=CFSQ-CFSIN
0345      ACFT=CFSIN/0.5042
0346      FREEVL=PUNDVL-STORGE
0347      IF(FREEVL.GT.ACFT) GO TO 222
0348      IF(FREEVL.LE.0.0) FREEVL=0.0
0349      STORGE=STORGE+FREEVL
0350      CFSIN=ACFT-FREEVL
0351      GO TO 333
0352      222 STORGE=STORGE+CFSIN
0353      CFSIN=0.0
0354      333 STORGE=STORGE-ETTT
0355      IF(STORGE.LT.0.0) STORGE=0.0
0356      OUTFLC=0.5042*CFSIN+CFSOUT
0357      EPV=EPY*(CFSQ-OUTFLC)/AREAX
0358      IF(OUTFLC) 79,79,81
0359      79 RP=0.0
0360      IFW=0.0
0361      GO TO 82
0362      81 IFW=IFW*(OUTFLC/CFSQ)
0363      RR=RRP*(OUTFLC/CFSQ)
0364      C STREAMFLOW-GROUNDWATER INTERACTION
0365      C THE STATEMENTS THROUGH 784 REPRESENT A LINEAR APPROXIMATION OF
0366      C THE STAGE DISCHARGE RELATIONSHIP. THEY MUST BE CHANGED FOR EACH NEW
0367      C BASIN TO WHICH THE MODEL IS APPLIED.
0368      82 Q=RR+IFW
0369      STG=0.0
0370      IF(Q.LT.3400) STG=0.251*Q**0.539
0371      IF(Q.GE.3400) STG=3.72*Q**0.207
0372      784 EXCESS=GWS-GWSN
0373
0374      28600
0375      28700
0376      28800
0377      28900
0378      29000
0379      29100
0380      29200
0381      29300
0382      29400
0383      29500
0384      29600
0385      29700
0386      29800
0387      29900
0388      30000
0389      30100
0390      30200
0391      30300
0392      30400
0393      30500
0394      30600
0395      30700
0396      30800
0397      30900
0398      31000
0399      31100
0400      31200
0401      31300
0402      31400
0403      31500
0404      31600
0405      31700
0406
0407      32100

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0367 IF(EXCESS.LT.0.0) EXCESS=0.0
0368 GIGI=STG-PORF*EXCESS-1.500
0369 IF(GIGI.LT.0.0) GO TO 785
0370 GWFC=GWRF*STG*GIGI
0371 BF=EXCESS*FB
0372 IF(EXCESS.LE.0.5) BF=10.0
0373 GO TO 786
0374 785 BF=EXCESS*FB
0375 GWFC=0.0
0376 786 BFIN=BF*AF
0377 GWIN=GWFC*AF
C BUDGET EQUATIONS
0378 IF(PP.LT.GWREC) GO TO 751
0379 RR=RR-GWFC
0380 PORF=RR+IFW*BF
0381 GO TO 751
0382 751 IF(RP+IFW.LT.GWREC) GO TO 752
0383 IFW=RR+IFW-GWREC
0384 RR=0.0
0385 RORF=IFW*BF
0386 GO TO 753
0387 752 GWIN=(RR+IFW)*AF
0388 RR=0.0
0389 IFW=0.0
0390 RORF=0.0
0391 753 CONTINUE
0392 IF(RORF.LE.0.0) GO TO 41
0393 RORF1=RORF
0394 IF(RORF1) 29,29,31
0395 29 AF=0.0
0396 RR=0.0
0397 IFW=0.0
0398 GO TO 41
0399 31 RR=RR-(RORF/RORF1)
0400 IFW=IFW*(RORF/RORF1)
0401 BF=BF*(RORF/RORF1)
0402 41 CONTINUE
0403 GWS=GWS+RECGW+GWIN-BFIN
0404 PLTP(1,NCZ)=BF
0405 PLTP(2,NCZ)=IFW*BF
0406 IF(PLTP(2,NCZ).GT.RORF) PLTR(2,NCZ)=RORF
0407 PLTR(3,NCZ)=P24(2)
0408 PLTR(4,NCZ)=RORF
0409 DWP(1,NCZ)=TPA
0410 IF(P24(2).LT.1.0) FLOW(1,NCZ)=1.0
0411 IF(P24(2).GE.1.0) FLOW(1,NCZ)=P24(2)
0412 IF(RORF.LT.1.0) SIMQ(1,NCZ)=1.0
0413 IF(RORF.GE.1.0) SIMQ(1,NCZ)=RORF
0414 PET(1,NCZ)=ETP
0415 AET(1,NCZ)=ETA
0416 TEMP(1,NCZ)=T
0417 DAY(1,NCZ)=ACT
C MONTHLY TOTALS
0418 TOTAL(MN,1)=TOTAL(MN,1)+TPA
0419 TOTAL(MN,2)=TOTAL(MN,2)+RORF
0420 TOTAL(MN,3)=TOTAL(MN,3)+P24(2)
0421 TOTAL(MN,4)=TOTAL(MN,4)+RR
0422 TOTAL(MN,5)=TOTAL(MN,5)+P24(2)

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38600
38800
38900
39000
39100

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0423 TOTALM(NN,6)=TOTALM(NN,6)+IFW
0424 TOTALM(NN,7)=TOTALM(NN,7)+RF
0425 TOTALM(NN,9)=TOTALM(NN,9)+FIP
0426 TOTALM(NN,10)=TOTALM(NN,10)+UETA
0427 TOTALM(NN,11)=TOTALM(NN,11)+LETA
0428 TOTALM(NN,12)=TOTALM(NN,12)+TETA
0429 TOTALM(NN,13)=TOTALM(NN,13)+TPERC
0430 TOTALM(NN,14)=TOTALM(NN,14)+AUZS*XIDY
0431 TOTALM(NN,15)=TOTALM(NN,15)+LZSA*XIDY
0432 TOTALM(NN,16)=TOTALM(NN,16)+LZST(10)*XIDY
0433 TOTALM(NN,17)=TOTALM(NN,17)+GWS*XIDY
0434 TOTALM(NN,18)=TOTALM(NN,18)+T*XIDY
C CORRELATION COEFFICIENT CALCULATIONS
0435 ACV=TOTALM(NN,3)*XIDY
0436 SYM=TOTALM(NN,2)*XIDY
0437 DAC=PLTR(3,NCZ)-ACM
0438 DSY=PLTR(4,NCZ)-SYM
0439 SDTD=SDTD+DAC*DSY
0440 SDACO=SDACO+DAC*DAC
0441 SDSYQ=SDSYQ+DSY*DSY
0442 IF(SDACQ.LE-0.0-DR-SDSYQ.LE-0.0) GO TO 112
0443 CCORREL=SDTD/SDACO*SDSYQ
0444 GO TO 113
0445 112 IF(SDTP.EQ-0.0) GO TO 1121
0446 CCORREL=0.0
0447 GO TO 113
0448 1121 CCORREL=1.0
0449 113 CCORREL=CCORREL**2
0450 TOTALM(NN,19)=TOTALM(NN,19)+CCORREL*XIDY
C FLOW DURATION CALCULATIONS
0451 IF(NV-1R3) 777,777,108
0452 ERR=ROPE-P24(2)
0453 IF(P24(2).LT.1.0) IND=1.0
0454 IF(P24(2).GE.1.0) IND=4.0*ALOG10(P24(2))+2.0
0455 CAS(IND)=CAS(IND)+1.0
0456 IF(ROBF.LT.1.0) IDN=1.0
0457 IF(ROBF.GE.1.0) IDN=4.0*ALOG10(ROBF)+2.0
0458 CSE(IND)=CSE(IND)+1.0
0459 SERR(IND)=SERR(IND)+EPP
0460 SERR(IND)=SERR(IND)+ABS(ERR)
0461 SQER(IND)=SQER(IND)+ERR*EPR
0462 AVER(IND)=SERR(IND)/CAS(IND)
0463 AVAR(IND)=SERR(IND)/CAS(IND)
0464 S(IND)=0.0
0465 IF(CAS(IND).GT.1.0) S(IND)=SQER(IND)-SERR(IND)**2/CAS(IND))/41800
1(CAS(IND)-1.0))
777 ACT=ACT+1
TOTALM(NN,5)=TOTALM(NN,5)-TOTALM(NN,8)
C YEARLY TOTALS
0466 DY=IDY
0467 YL=LY+365
0468 DO 806 K=1,8
0469 TOTALM(13,K)=TOTALM(13,K)+TOTALM(NN,K)
0470 DO 104 K=9,13
0471 TOTALM(13,K)=TOTALM(13,K)+TOTALM(NN,K)
0472 DO 105 K=14,18
0473 TOTALM(13,K)=TOTALM(13,K)+TOTALM(NN,K)*DY/YL
0474 TOTALM(13,K)=TOTALM(13,K)+TOTALM(NN,19)*DY/YL
0475
0476

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43800

44400

44500

44600

40300

40400

40500

40600

40700

40800

40900

41000

41100

41200

41300

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41500

41600

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42900

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0477      888 NTD1=NTD2+1
0478      C YEARLY OUTPUT
0479      1 WRITE(6,1013) NNN
0480      1013 FORMAT('1',34X,SIMSUMMARY TABLE -- BLACK VERMILLION RIVER BASIN
0481      WRITE(6,1002)
0482      1002 FORMAT('13X',JAN. FEB. MAR. APR. MAY. JUN.
0483      1 JUL. AUG. SEP. OCT. NOV. DEC. TOTAL')
0484      1003 FORMAT(9H PRECIP,13F9.2//17H CALCULATED TOTAL/9H RUNOFF,13F9.046200
0485      1//15H OBSERVED TOTAL/9H RUNOFF,13F9.0//19H CALCULATED SURFACE/9H46300
0486      2 RUNOFF,13F9.0//17H OBSERVED SURFACE/9H RUNOFF,13F9.0//18H CAL46400
0487      3CULATED INTER-/9H FLOW,13F9.0//11H CALCULATED/9H BASEFLOW,13F9.046500
0488      4.0//9H OBSERVED/9H BASEFLOW,13F9.0//9H ETP,13F9.3//9H UEA6600
0489      5TA,13F9.3//9H LETA,13F9.3//9H ETA,13F9.3//9H PER-/9H
0490      6COLATION,13F9.3//9H UZS,13F9.3//9H LZSA,13F9.3//9H
0491      7LZST,13F9.3//9H GWS,13F9.3//9H TEMP.,13F9.1//18H CORREL
0492      8ATION CREF-/9H FICIENTS,13F9.3)
0493      BALNCE=TOTALM(13,1)-TOTALM(13,2)/AREAX-TOTALM(13,12)
0494      V=BALNCE-AAIA-FPY
0495      WRITE(6,1006) BALNCE,AAIA-FPY,V
0496      1006 FORMAT('1//18H DELTA STORAGE =,F10.3,8H INCHES/18H AAIA = 47400
0497      1 ,F10.3/18H POND STORAGE = ,F10.3/28H-----
0498      2-----/18H TOTAL CHANGE = ,F10.3//)
0499      SEW=SEW*EPY
0500      RAL=RAL + RALNCE
0501      AIA=AAIA+AAIA
0502      LDY=365+LY
0503      SUSU(1)=SUSU(1)+TOTALM(13,2)
0504      SUSU(2)=SUSU(2)+TOTALM(13,3)
0505      SUSU(3)=SUSU(3)+TOTALM(13,4)+TOTALM(13,6)
0506      SUSU(4)=SUSU(4)+TOTALM(13,5)
0507      SUSU(5)=SUSU(5)+TOTALM(13,7)
0508      SUSU(6)=SUSU(6)+TOTALM(13,8)
0509      SUSU(7)=SUSU(7)+TOTALM(13,1)
0510      SUSU(8)=SUSU(8)+TOTALM(13,12)
0511      WRITE(6,15) SUSU(1),SUSU(2),SUSU(3),SUSU(4),SUSU(5),SUSU(6)
0512      15 FORMAT('14X,17HSUM CAL TOTAL = ,F15.0/4X,17HSUM OBS TOTAL = ,F15.48900
0513      1.0/4X,17HSUM CAL SRINT = ,F15.0/4X,14HSUM OBS SR = ,F18.0/4X,14H49000
0514      2SUM CAL RF = ,F18.0/4X,14HSUM OBS BF = ,F18.0//)
0515      999 CONTINUE
0516      WRITE(6,1012)
0517      C CALCULATIONS AND OUTPUT OF FLOW DURATION
0518      WRITE(6,1019)
0519      1019 FORMAT('1H1//41X,35HDAIY FLOW DURATION AND ERROR TABLE //11X,93HF49600
0520      1LCW INTERVAL ACT-CASES PCT. CALC-CASES PCT. AVE.ERROR 49700
0521      2 AV-ARS-ERROR STD-ERROR /)
0522      SSERR=0.0
0523      SSERRA=0.0
0524      SSERRF=0.0
0525      SCASE=0.0
0526      SSC=0.0
0527      DO 911 J=1,24
0528      SCASE=SCASEF+CAS(J)
0529      SSC=SSC+CSE(J)
0530      SSERR=SSERR+SERR(J)
0531      SSERRA=SSERRA+SERA(J)
0532      911 J=J+1
0533      50500
0534      50600
0535      50700
0536      50800

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0517 911 SSTER=SSTER+S(J)          50900
0518 SCLS=SCASE
0519 SCSE=SCSC
0520 DO 981 J=1,74
0521 IF(J.GT.2) GO TO 912
0522 IF(J.EQ.1) FLOO=0.0
0523 IF(J.EQ.2) FLOO=1.0
0524 GO TO 913
0525 912 FJ=J
0526 POWR=FJ/4.0-0.5
0527 FLOO=10.0*POWR
0528 913 IF(SCASE.LE.0.0) GO TO 1447
0529 PSCLS=100.0*SCLS/SCASE
0530 GO TO 1448
0531 1447 PSCLS=0.0
0532 1448 CLS=CAS(J)
0533 SCLS=SCLS-CLS
0534 IF(SCSC.LE.0.0) GO TO 1449
0535 PSCE=100.0*SCSE/SCSC
0536 GO TO 1450
0537 1449 PSCE=0.0
0538 1450 SCL=SCF(J)
0539 SCSE=SCSF-SCL
0540 IF(CLS.EQ.0.0) GO TO 980
0541 SFRACS=SFRA(J)/CLS
0542 SFRRCS=SFRR(J)/CLS
0543 IF(CLS.EQ.1.0) WRITE(6,1018) FLOO,CLS,PSCLS,SCL,PSCE,SFRRCS
0544 IF(CLS.GT.1.0) WRITE(6,1018) FLOO,CLS,PSCLS,SCL,PSCE,SFRRCS,
1,S(J)
1018 FORMAT(12X,F10.1,1H-,F9.1,F11.3,F10.1,F11.3,F12.1,2F13.2)
0545 GO TO 981
0546 980 WRITE(6,1018) FLOO,CLS,PSCLS,SCL,PSCE
0547 981 CONTINUE
0548 1020 WRITE(6,1020) SCASE,SCSC,SSERR,SSERA,SSTER
0549 1020 FORMAT(73X,F9.1,11X,F10.1,11X,F12.1,F13.2,F13.2)
0550 C END OF CALCULATIONS
0551 V=RAL-AIA-SFW
0552 WRITE(6,1006) RAL,AIA,SEW,V
0553 WRITE(6,1273) SUSU(7)
0554 1273 FORMAT(122H TOTAL PRECIPITATION =,F10.3/)
0555 TRD=SUSU(1)/AREAX
0556 CKPAL=TRD+SUSU(8)+AIA+V
0557 WRITE(6,1274) TRD,SUSU(8),AIA+V,CKPAL
0558 1274 FORMAT(116H TOTAL RUN OFF =,F10.3,8H INCHES/16H TOTAL ETA =,
1F10.3/16H TOTAL AIA =,F10.3/16H TOTAL CHANGE =,F10.3/26H-----
2-----/16H CHECK BALANCE =,F10.3/)
0559 CALL PLOT (0.0,0.0,999)
0560 STOP
0561 END

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PLOTT

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0001 SUBROUTINE PLOTT(X,YH,YHC,YP,I,IYEAR,PET,AET,TEMP)
0002 DIMENSION X(368),YH(368),YP(368),PET(368),AET(368)
0003 DIMENSION TEMP(368),YHC(368)
0004 INTEGER FSTV,DLTV
0005 INTEGER YEARS(14)
0006 DATA YEARS/'1954','1955','1956','1957','1958','1959','1960',
* '1961','1962','1963','1964','1965','1966','1967',/
0007 I=1-1
0008 FSTV=1+1
0009 DLTV=1+2
0010 X(FSTV)=0.0
0011 X(DLTV)=30.5
0012 YH(FSTV)=1.0
0013 YH(DLTV)=1.0
0014 YHC(FSTV)=1.0
0015 YHC(DLTV)=1.0
0016 TEMP(FSTV)=0.0
0017 TEMP(DLTV)=25.0
0018 PET(FSTV)=0.0
0019 PET(DLTV)=0.125
0020 AET(FSTV)=0.0
0021 AET(DLTV)=0.125
0022 CALL PLOT (0.0,0.0,3)
0023 CALL SCALE (YP,3,0,1,1)
0024 CALL AXISC (0.0,0.0,0.0,YEARS(IYEAR-1953),-4,12.0,0.0,1.0,1.0)
0025 DO 450 I=1,4
0026 CALL PAXIS (0.0,L/YH(DLTV),12.0,0.0,12.0,1)
0027 CALL LGAXIS (0.0,0.0,'CALC.-* & OBS.-+ DISCHARGE (CFS)',32,8.0,
* 0.0,YH(FSTV),YH(DLTV))
0028 CALL AXIS (0.0,8.0,'THIESSEN WEIGHTED DAILY PRECIPITATION',37,
* 12.0,0.0,X(FSTV),X(DLTV))
0029 CALL AXIS (12.0,8.0,'INCHES',6,3.0,-90.0,YP(FSTV),YP(DLTV))
0030 CALL LGLINE (X,YH,1,1,4,3,1)
0031 CALL LGLINE (X,YHC,1,1,4,11,1)
0032 DO 500 L=1,I
0033 XQ=X(L)/X(DLTV)-(1/(2*X(DLTV)))-(X(FSTV)/X(DLTV))
0034 YQ=Y(L)-YP(L)/YP(DLTV)
0035 H=YP(L)/YP(DLTV)
0036 W=1/X(DLTV)
0037 IF(IYEAR.LT.1970) GO TO 650
0038 CALL ORIGIN (16.0,1.5,11.0)
0039 CALL PLT (0.0,0.0,3)
0040 CALL AXISC (0.0,0.0,0.0,YEARS(IYEAR-1953),-4,12.0,0.0,1.0,1.0)
0041 CALL AXIS (0.0,0.0,'PET--+ & AET-* (INCHES)',22,8.0,90.0,0.0,0.125)
0042 IF(IYEAR.LT.1970) GO TO 510
0043 CALL AXIS (0.0,8.0,'AVERAGE DAILY TEMPERATURE',25,12.0,0.0,0.0,
* X(FSTV),X(DLTV))
0044 CALL AXIS (12.0,8.0,'DEGREES FAHRENHEIT',18,4.0,-90.0,
* TEMP(FSTV),TEMP(DLTV))
0045 DO 600 L=1,I
0046 CALL LINE (X,PET,1,1,4,3)
0047 CALL LINE (X,AET,1,1,4,11)
0048 XQ=(X(L)/X(DLTV))-(1/(2*X(DLTV)))-(X(FSTV)/X(DLTV))
0049 YQ=Y(L)-TEMP(L)/TEMP(DLTV)
0050 H=TEMP(L)/TEMP(DLTV)
0051 W=1/X(DLTV)
0052 CALL BAR (XQ,YQ,0.0,H,W,0.0,1.0)
0053

```

PAGE 0002

20/16/08

DATE = 76307

PLOT

FORTAN IV G LEVEL 21

```
0054 650 CALL ORIGIN (16.0,1.5,11.0)
0055 CALL PLOT (0.0,0.0,3)
0056 RETURN
0057 END
```

PAGE 0001

20/16/08

DATE = 76307

WTRMOD

FORTRAN IV G LEVEL 21

```

0001 SURROUTINE WTRMOD(PRECIP, MONTH, MODEL, WPCNT)
0002 IF (MODEL.EQ.1) GO TO 30
0003 IF (MONTH.LT.3.OR.MONTH.GT.9) GO TO 10
0004 ADJ=1.75
0005 IF (PRECIP.GT.0.10) ADJ=1.30
0006 IF (PRECIP.GT.0.50) ADJ=1.10
0007 IF (PRECIP.GT.1.00) ADJ = 0.90
0008 GO TO 20
0009 10 ADJ = 1.0
0010 IF (MODEL.EQ.3) ADJ=WPCNT
0011 20 PRECIP=PRECIP*ADJ
0012 30 RETURN
0013 END

```

**THE FOLLOWING
PAGE WAS BOUND
WITHOUT A PAGE
NUMBER.**

**THIS IS AS
RECEIVED FROM
CUSTOMER.**

RESULTS - UNMODIFIED MODEL

THE 6-FOUR INCREMENTAL VALUES OF THE UNIT HYDROGRAPH

Category	0.0250	0.0350	0.0450	0.0550	0.0650	0.0750	0.0850	0.0950	0.1050	0.1150	0.1250	0.1350	0.1450	0.1550	0.1650	0.1750	0.1850	0.1950	0.2050	0.2150	0.2250	0.2350	0.2450	0.2550	0.2650	0.2750	0.2850	0.2950	0.3050	0.3150	0.3250	0.3350	0.3450	0.3550	0.3650	0.3750	0.3850	0.3950	0.4050	0.4150	0.4250	0.4350	0.4450	0.4550	0.4650	0.4750	0.4850	0.4950	0.5050	0.5150	0.5250	0.5350	0.5450	0.5550	0.5650	0.5750	0.5850	0.5950	0.6050	0.6150	0.6250	0.6350	0.6450	0.6550	0.6650	0.6750	0.6850	0.6950	0.7050	0.7150	0.7250	0.7350	0.7450	0.7550	0.7650	0.7750	0.7850	0.7950	0.8050	0.8150	0.8250	0.8350	0.8450	0.8550	0.8650	0.8750	0.8850	0.8950	0.9050	0.9150	0.9250	0.9350	0.9450	0.9550	0.9650	0.9750	0.9850	0.9950	1.0050	1.0150	1.0250	1.0350	1.0450	1.0550	1.0650	1.0750	1.0850	1.0950	1.1050	1.1150	1.1250	1.1350	1.1450	1.1550	1.1650	1.1750	1.1850	1.1950	1.2050	1.2150	1.2250	1.2350	1.2450	1.2550	1.2650	1.2750	1.2850	1.2950	1.3050	1.3150	1.3250	1.3350	1.3450	1.3550	1.3650	1.3750	1.3850	1.3950	1.4050	1.4150	1.4250	1.4350	1.4450	1.4550	1.4650	1.4750	1.4850	1.4950	1.5050	1.5150	1.5250	1.5350	1.5450	1.5550	1.5650	1.5750	1.5850	1.5950	1.6050	1.6150	1.6250	1.6350	1.6450	1.6550	1.6650	1.6750	1.6850	1.6950	1.7050	1.7150	1.7250	1.7350	1.7450	1.7550	1.7650	1.7750	1.7850	1.7950	1.8050	1.8150	1.8250	1.8350	1.8450	1.8550	1.8650	1.8750	1.8850	1.8950	1.9050	1.9150	1.9250	1.9350	1.9450	1.9550	1.9650	1.9750	1.9850	1.9950	2.0050	2.0150	2.0250	2.0350	2.0450	2.0550	2.0650	2.0750	2.0850	2.0950	2.1050	2.1150	2.1250	2.1350	2.1450	2.1550	2.1650	2.1750	2.1850	2.1950	2.2050	2.2150	2.2250	2.2350	2.2450	2.2550	2.2650	2.2750	2.2850	2.2950	2.3050	2.3150	2.3250	2.3350	2.3450	2.3550	2.3650	2.3750	2.3850	2.3950	2.4050	2.4150	2.4250	2.4350	2.4450	2.4550	2.4650	2.4750	2.4850	2.4950	2.5050	2.5150	2.5250	2.5350	2.5450	2.5550	2.5650	2.5750	2.5850	2.5950	2.6050	2.6150	2.6250	2.6350	2.6450	2.6550	2.6650	2.6750	2.6850	2.6950	2.7050	2.7150	2.7250	2.7350	2.7450	2.7550	2.7650	2.7750	2.7850	2.7950	2.8050	2.8150	2.8250	2.8350	2.8450	2.8550	2.8650	2.8750	2.8850	2.8950	2.9050	2.9150	2.9250	2.9350	2.9450	2.9550	2.9650	2.9750	2.9850	2.9950	3.0050	3.0150	3.0250	3.0350	3.0450	3.0550	3.0650	3.0750	3.0850	3.0950	3.1050	3.1150	3.1250	3.1350	3.1450	3.1550	3.1650	3.1750	3.1850	3.1950	3.2050	3.2150	3.2250	3.2350	3.2450	3.2550	3.2650	3.2750	3.2850	3.2950	3.3050	3.3150	3.3250	3.3350	3.3450	3.3550	3.3650	3.3750	3.3850	3.3950	3.4050	3.4150</
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THE

[illegible]

MONTHLY BASE FLOW

	1970	1980	1990	2000	2010	2020					
13.6	72.5	527.0	300.0	58.9	875.0	1240.0	402.0	12.0	4.7	120.0	310.0

LEAP YEAR INDICATOR= 1 YES=1 & NO=0

IT-AN	1F8EZ
123	235

YEAR 48

RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE

[illegible]

SUMMARY TABLE - SOUTH FORK SLOMOM RIVER BASIN - 1948

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.04	0.53	1.54	0.34	3.54	4.91	1.69	3.76	0.76	0.59	1.04	0.46	19.20
CALCULATED TOTAL RUNOFF	0.	6.	219.	20.	2335.	6182.	1781.	6108.	1045.	731.	862.	401.	19692.
OBSERVED TOTAL RUNOFF	21.	423.	1409.	390.	2101.	13298.	2454.	3513.	40.	5.	131.	338.	24114.
CALCULATED SURFACE RUNOFF	0.	6.	189.	20.	2205.	5880.	1311.	5586.	327.	122.	425.	43.	16174.
OBSERVED SURFACE RUNOFF	2.	351.	882.	90.	2042.	12418.	1214.	3110.	28.	1.	11.	28.	20177.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	0.	0.	30.	0.	70.	202.	471.	523.	718.	610.	437.	353.	3519.
OBSERVED BASEFLOW	19.	73.	527.	300.	59.	870.	1243.	403.	12.	5.	120.	310.	3937.
ETP	0.887	0.845	1.444	4.549	5.315	6.210	6.537	5.709	5.012	3.045	1.100	0.708	41.361
UETA	0.168	0.119	0.344	1.209	1.706	2.579	2.126	2.203	1.226	0.695	0.233	0.105	12.711
LETA	0.0	0.0	0.0	0.0	0.500	1.385	1.146	0.897	0.035	0.0	0.0	0.0	3.967
FTA	0.175	0.273	0.646	1.209	2.205	3.568	3.272	3.100	1.261	0.695	0.431	0.217	17.456
PER-CORRELATION	0.0	0.0	0.001	0.0	0.477	1.104	0.051	0.699	0.035	0.0	0.0	0.0	2.367
UZS	2.890	2.939	3.565	3.605	3.295	3.580	3.769	4.079	3.506	2.882	2.949	3.595	3.422
L7SA	5.400	5.400	5.400	5.401	5.277	5.595	8.483	7.901	7.800	7.800	7.800	7.800	8.627
LZST	5.400	5.400	5.400	9.401	9.277	9.099	3.483	7.901	7.800	7.800	7.800	7.800	8.627
GAS	2.000	2.000	2.000	1.959	2.001	2.063	2.086	2.126	2.119	2.089	2.067	2.051	2.050
TEMP.	28.5	30.0	33.8	58.8	63.2	70.9	76.5	76.8	71.2	55.0	37.7	30.5	52.8
CORRELATION COEFFICIENTS	1.000	0.636	0.570	0.424	0.809	0.586	0.46	0.571	0.810	0.589	0.286	0.905	0.639

SUMMARY TABLE - SOUTH FORK SCLOMCH RIVER BASIN - 1949

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.33	1.16	1.24	2.08	4.34	6.41	2.66	3.15	0.30	1.58	0.07	0.11	24.64
CALCULATED TOTAL RUNOFF	320.	484.	443.	928.	4586.	8633.	3024.	7018.	948.	2242.	540.	407.	24572.
OBSERVED TOTAL RUNOFF	37.	6127.	2325.	1554.	3496.	12838.	1529.	809.	57.	504.	569.	521.	30807.
CALCULATED SURFACE RUNOFF	50.	301.	271.	751.	4284.	8181.	2428.	1336.	229.	1679.	13.	6.	19538.
OBSERVED SURFACE RUNOFF	3.	5035.	310.	294.	1388.	5838.	1278.	635.	58.	269.	-1.	25.	19132.
CALCULATED INTER-FLC4	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	251.	183.	172.	177.	302.	451.	556.	482.	719.	562.	528.	401.	5034.
OBSERVED BASEFLOW	34.	1002.	2015.	1260.	2108.	3000.	651.	174.	39.	236.	570.	496.	11674.
ETP	0.0	0.509	2.677	3.584	5.333	6.288	6.642	5.547	4.588	3.011	1.903	1.017	41.100
UETA	0.0	0.110	0.796	1.457	2.452	2.817	2.248	1.960	1.276	0.800	0.213	0.098	14.227
LETA	0.0	0.0	0.0	0.122	1.207	1.517	1.210	1.055	0.687	0.359	0.0	0.0	6.157
ETA	0.159	0.393	0.828	1.810	3.659	4.333	3.458	3.315	1.963	1.159	0.213	0.098	21.068
PER-CORRELATION	0.0	0.424	0.220	0.929	1.557	2.965	0.234	0.155	0.0	0.165	0.0	0.0	6.570
U25	3.831	4.217	4.267	4.306	4.307	4.158	3.547	3.445	3.291	3.499	3.408	3.313	3.795
L25A	7.800	7.892	8.290	9.103	5.664	10.978	10.494	9.467	8.700	8.263	8.213	8.213	8.927
L23T	7.800	7.892	8.280	9.103	5.664	10.978	10.494	9.467	8.700	8.263	8.213	8.213	8.927
G4S	2.037	2.027	2.020	2.014	2.033	2.120	2.151	2.133	2.111	2.097	2.077	2.057	2.073
TEMP.	18.3	29.9	39.5	51.9	63.5	71.9	78.0	74.3	64.3	54.2	47.3	32.4	52.2
CORRELATION COEFFICIENTS	0.590	0.672	0.680	0.476	0.617	0.492	0.699	0.633	0.603	0.648	0.968	0.983	0.672

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1950

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.12	1.20	0.39	0.93	2.45	1.50	7.29	6.28	9.30	0.55	0.07	0.02	21.11
CALCULATED TOTAL RUNOFF	243.	380.	233.	282.	560.	1023.	34175.	22206.	3612.	2576.	1943.	1474.	69152.
OBSERVED TOTAL RUNOFF	371.	1027.	1041.	721.	599.	449.	21805.	31911.	2063.	952.	710.	725.	62374.
CALCULATED SURFACE RUNOFF	6.	175.	120.	158.	770.	868.	33824.	18941.	152.	208.	2.	0.	55221.
OBSERVED SURFACE RUNOFF	-1.	19.	18.	121.	134.	344.	20410.	28501.	533.	208.	20.	12.	50319.
CALCULATED INTER-FLCN	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	293.	205.	163.	125.	190.	155.	301.	3265.	3460.	2358.	1940.	1474.	13940.
OBSERVED BASEFLOW	372.	1008.	1023.	600.	465.	105.	1395.	3410.	1530.	744.	690.	713.	12055.
ETP	0.795	1.558	2.302	3.978	5.046	6.390	6.258	5.308	4.622	3.284	1.589	1.099	42.130
UETA	0.019	0.206	0.473	1.009	1.751	1.968	2.304	2.273	1.356	0.693	0.196	0.061	12.310
LETA	0.0	0.0	0.0	0.0	0.535	0.0	0.826	1.230	0.741	0.389	0.014	0.0	3.735
ETA	0.036	0.206	0.599	1.009	2.286	1.566	3.131	3.503	2.097	1.082	0.210	0.061	16.187
PER-CORRELATION	0.0	0.077	0.023	0.022	0.0	0.0	1.805	2.330	0.0	0.0	0.0	0.0	4.307
UFS	3.232	3.695	3.911	3.741	3.550	3.201	2.834	4.209	3.560	3.090	2.689	2.602	3.444
LZSA	8.213	8.231	8.307	8.325	8.139	7.800	8.090	8.603	9.517	8.961	8.785	8.785	8.571
LZST	8.213	8.231	8.207	8.325	8.139	7.800	8.080	9.683	9.517	8.961	8.785	8.785	8.571
GWS	2.042	2.031	2.023	2.016	2.011	2.007	2.084	2.555	2.508	2.386	2.285	2.209	2.181
TEMP.	27.3	36.8	39.2	48.4	56.3	73.3	72.7	70.6	64.9	59.8	38.9	34.5	52.1
CORRELATION COEFFICIENTS	0.902	0.627	0.538	0.636	0.539	0.332	0.527	0.639	0.865	0.694	0.936	0.717	0.667

DELTA STORAGE = 2.446 INCHES												
ADJ = 2.627												
POND STORAGE = 0.0												

TOTAL CHANGE = -0.181												

SLM CAL TOTAL = 113426.												
SLM OBS TOTAL = 117255.												
SLM CAL SRINT = 90523.												
SLM OBS SR = 89629.												
SLM CAL RF = 22453.												
SLM OBS RF = 27666.												

PACK CN DECEMBER 31 = 0.0												
CHANGE IN SNOW STORAGE = 0.00												
AVERAGE MONTHLY BASE FLOW												
368.C 952.01240.01170.01612.04800.06820.03410.02760.02294.02250.01085.0												
LEAP YEAR INDICATOR= C YES=1 & NO=0												
IT-34	IFREZ											
122	283											
YEAR 51												
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE												
JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
0.0	0.0	0.0	0.0	0.0	0.0	2.276	0.0	0.0	0.0	0.0	0.0	2.270

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1951

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.29	0.93	0.62	2.29	5.75	9.28	7.49	2.35	3.10	0.70	0.18	0.10	33.08
CALCULATED TOTAL RUNOFF	1035.	766.	746.	1465.	20102.	26612.	43234.	20034.	15442.	9482.	6648.	5049.	150864.
OBSERVED TOTAL RUNOFF	392.	576.	1249.	1503.	17401.	53000.	79382.	9426.	11537.	2494.	2386.	1452.	181699.
CALCULATED SURFACE RUNOFF	7.	57.	165.	1072.	15420.	24519.	28877.	2966.	3134.	133.	1.	0.	80351.
OBSERVED SURFACE RUNOFF	24.	24.	5.	333.	15789.	46200.	72562.	6016.	8777.	200.	126.	367.	152437.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	402.	220.	53.	0.	0.	0.	675.
CALCULATED BASEFLOW	1077.	769.	581.	393.	683.	2093.	13955.	16847.	12255.	9349.	6647.	5049.	69633.
OBSERVED BASEFLOW	868.	652.	1240.	1170.	1612.	4880.	6820.	3410.	2760.	2294.	2250.	1085.	29261.
ETP	0.458	1.240	2.572	3.869	5.735	5.774	6.353	5.626	4.494	2.938	1.491	0.666	40.716
UESTA	0.025	0.183	0.429	0.957	1.883	2.947	2.634	2.139	1.756	0.814	0.244	0.054	13.566
LETA	0.0	0.0	0.0	0.0	0.619	1.533	1.418	1.152	0.946	0.194	0.0	0.0	5.861
ETA	0.206	0.262	0.429	0.957	2.502	4.380	4.052	3.291	2.702	1.008	0.266	0.112	20.168
PER-CORRELATION	0.0	0.0	0.0	0.259	1.519	4.217	3.503	0.369	0.861	0.0	0.0	0.0	11.128
UZS	2.657	2.737	2.563	3.491	3.395	4.412	4.272	3.887	3.879	3.079	2.925	2.793	3.422
LZSA	9.785	8.785	8.785	8.878	9.578	11.701	13.055	12.454	12.257	11.807	11.792	11.782	10.820
LZST	8.765	8.785	8.765	8.878	9.578	11.701	14.440	14.764	14.527	14.077	14.052	14.052	11.889
GWS	2.153	2.113	2.036	2.066	2.142	2.500	4.065	4.393	3.799	3.327	2.975	2.717	2.868
TEMP.	27.3	35.4	36.1	48.3	62.1	64.9	74.0	75.6	62.8	52.6	37.5	27.5	50.4
CORRELATION COEFFICIENTS	0.801	0.637	0.836	0.721	0.641	0.885	0.515	0.597	0.647	0.311	0.954	0.836	0.740

550.01595.01550.02400.02325.0 330.0 55.8 34.1 0.0 1.6 45.0 155.0

LEAP YEAR INDICATOR= 1 YES=1 & NO=0

ITP-4W 1FREQ
132 280YEAR
52

RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE

JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1952

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.10	0.20	1.27	2.34	2.25	0.26	2.33	2.54	3.61	0.03	0.07	0.86	12.87
CALCULATED TOTAL RUNOFF	3691.	2549.	2138.	1575.	3032.	1137.	1566.	1283.	751.	400.	284.	297.	18703.
OBSERVED TOTAL RUNOFF	1869.	1885.	3100.	4200.	4656.	488.	110.	117.	23.	2.	50.	255.	16751.
CALCULATED SURFACE RUNOFF	0.	0.	125.	304.	2315.	161.	854.	729.	255.	0.	0.	81.	4825.
OBSERVED SURFACE RUNOFF	310.	290.	1550.	1800.	2321.	158.	57.	83.	28.	0.	5.	100.	6710.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	3691.	2549.	2013.	1271.	716.	577.	712.	553.	496.	400.	284.	216.	13878.
OBSERVED BASEFLOW	1553.	1595.	1550.	2400.	2325.	230.	56.	34.	0.	2.	45.	155.	10041.
ETP	6.555	1.537	0.945	3.736	5.155	6.844	6.458	5.754	4.887	2.943	1.402	0.268	40.888
UETA	0.823	0.110	0.179	1.016	1.867	1.810	1.218	1.219	0.807	0.199	0.020	0.031	8.549
LETA	0.0	0.0	0.0	0.0	0.259	1.265	1.127	1.056	0.674	0.065	0.0	0.0	4.447
ETA	0.667	0.132	0.783	1.101	2.065	3.075	2.345	2.375	1.481	0.265	0.035	0.296	14.020
PER-CORRELATION	0.0	0.0	0.677	0.177	0.203	0.0	0.0	0.0	0.014	0.0	0.0	0.0	0.470
UTS	2.751	2.699	3.079	3.496	3.739	2.787	2.386	2.362	2.538	2.150	2.051	2.521	2.714
LZSA	11.782	11.782	11.780	11.909	12.065	11.346	10.095	9.045	8.164	7.810	7.305	7.805	10.111
LZST	14.052	14.052	14.060	14.179	14.335	13.619	12.365	11.315	10.434	10.080	10.075	10.075	12.381
GWS	2.524	2.387	2.246	2.212	2.183	2.151	2.121	2.097	2.077	2.057	2.042	2.031	2.180
TEMP.	32.4	36.1	34.1	49.2	60.9	70.5	87.6	71.5	69.1	52.9	36.9	29.6	53.9
CORRELATION COEFFICIENTS	0.994	0.994	0.991	0.988	0.609	0.75	0.41	0.434	0.799	0.322	0.470	0.766	0.724

SUMMARY TABLE - SOUTH FORK SCLOWEN RIVER BASIN - 1953

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.33	0.19	1.39	1.89	2.07	2.40	3.19	3.14	0.35	1.21	1.77	1.05	18.58
CALCULATED TOTAL RUNOFF	102.	116.	447.	514.	1051.	1528.	3814.	4624.	670.	734.	371.	492.	14553.
OBSERVED TOTAL RUNOFF	771.	673.	1125.	995.	635.	317.	2267.	1315.	7.	5.	152.	351.	3627.
CALCULATED SURFACE RUNOFF	35.	11.	325.	425.	501.	1402.	3530.	4193.	235.	380.	105.	275.	11316.
OBSERVED SURFACE RUNOFF	393.	35.	155.	189.	103.	311.	2167.	1225.	4.	0.	6.	41.	4731.
CALCULATED INTER-FLUX	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	153.	195.	122.	85.	150.	126.	284.	430.	436.	354.	266.	217.	2737.
OBSERVED BASEFLOW	372.	588.	930.	810.	527.	6.	99.	30.	3.	5.	156.	310.	3896.
ETP	0.531	1.509	2.535	5.822	5.092	5.667	6.584	5.599	4.906	3.239	1.267	0.118	42.259
UETA	0.016	0.125	0.389	1.107	1.554	2.160	1.808	2.011	1.115	0.613	0.262	0.044	11.210
LETA	0.0	0.0	0.0	0.0	0.177	0.367	0.756	0.702	0.091	0.0	0.0	0.0	2.092
ETA	0.116	0.125	0.590	1.107	1.731	2.527	2.563	2.713	1.256	0.613	0.450	0.386	14.161
PER-CORRELATION	0.0	0.0	0.111	0.043	0.073	0.105	0.672	0.611	0.031	0.0	0.051	0.569	2.253
U75	2.892	2.525	3.104	3.455	3.581	3.145	3.625	3.857	3.016	2.628	3.745	4.428	3.371
L754	7.805	7.805	7.877	7.915	7.961	7.803	7.842	7.876	7.800	7.800	7.828	8.131	7.872
L757	10.075	10.075	10.147	10.189	10.231	9.609	8.838	8.487	7.862	7.800	7.825	8.131	9.101
G45	2.022	2.017	2.012	2.008	2.005	2.004	2.028	2.076	2.068	2.051	2.039	2.029	2.030
TEMP.	37.9	36.1	44.0	47.5	60.0	77.1	77.2	75.0	69.4	58.8	41.6	29.8	54.6
CORRELATION COEFFICIENTS	0.763	0.801	0.387	0.397	0.670	0.624	0.477	0.439	0.634	0.467	0.519	0.419	0.548

DELTA STORAGE = 4.299 INCHES											
DATA = 3.131											
PCND STORAGE = 0.0											
TOTAL CHANGE = 1.168											
SUM CAL TOTAL = 257346.											
SUM PDS TOTAL = 324371.											
SUM CAL SPINT = 188559.											
SUM OBS SR = 253507.											
SUM CAL BF = 108747.											
SUM OBS BF = 70664.											
PACK CN DECEMBER 31 = 0.06											
CHANGE IN SNOW STORAGE = -0.39											
AVERAGE MONTHLY FASE FLOW											
248.0 812.0 744.0 510.0 1085.0 870.0 24.8 1.6 0.0 6.2 16.5 15.5											
LEAP YEAR INDICATOR = 0 YES=1 & NO=0											
YEAR 54											
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE											
JAN. FEB. MAR. APR. MAY. JUN. JUL. AUG. SEP. OCT. NOV. DEC. TOTAL											
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0											

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1954

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.14	0.48	0.57	0.55	5.23	2.08	1.19	2.39	0.48	1.52	0.02	0.06	14.71
CALCULATED TOTAL RUNOFF	197.	173.	129.	246.	5576.	4700.	572.	1696.	536.	678.	236.	183.	13327.
OBSERVED TOTAL RUNOFF	389.	1021.	789.	744.	5110.	5216.	48.	134.	0.	6.	18.	23.	13790.
CALCULATED SURFACE RUNOFF	52.	80.	40.	165.	5350.	4223.	367.	1240.	114.	356.	0.	4.	11999.
OBSERVED SURFACE RUNOFF	132.	209.	45.	234.	4025.	4646.	23.	133.	0.	0.	1.	7.	9457.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	146.	58.	80.	80.	226.	477.	605.	456.	422.	323.	236.	179.	3328.
OBSERVED BASEFLOW	243.	812.	744.	510.	1085.	873.	25.	2.	0.	6.	17.	16.	4334.
ETP	6.501	1.865	2.535	4.357	4.904	6.560	6.582	5.807	5.109	2.951	1.819	1.048	44.920
UETA	0.031	0.364	0.591	1.056	2.063	2.410	1.433	1.499	0.531	0.551	0.077	2.086	10.772
LETA	0.0	0.0	0.0	0.0	0.804	1.363	0.715	0.031	0.0	0.027	0.0	0.0	2.800
ETA	0.031	0.364	0.591	1.096	2.567	3.772	2.209	1.530	0.531	0.618	0.077	0.109	13.594
PER-CORRELATION	0.141	0.041	0.0	0.006	1.537	0.396	0.0	0.031	0.0	0.027	0.0	0.0	2.179
U75	4.130	4.093	3.571	3.564	4.093	3.642	2.366	2.672	2.360	2.715	2.672	2.601	3.236
L75A	8.546	8.575	8.692	8.604	8.586	9.105	8.050	7.800	7.800	7.800	7.800	7.800	3.287
L75T	8.546	8.575	8.692	8.604	8.586	9.105	8.050	7.800	7.800	7.800	7.800	7.800	3.287
G45	2.021	2.015	2.011	2.008	2.026	2.092	2.084	2.078	2.062	2.046	2.035	2.025	2.043
TEMP.	28.2	44.5	77.5	50.4	57.3	75.6	82.7	78.3	72.7	53.7	44.8	34.7	55.6
CORRELATION COEFFICIENTS	0.751	0.717	0.781	0.878	0.754	0.565	0.592	0.392	0.231	0.282	0.910	0.676	0.615

DELTA STORAGE = 0.564 INCHES AREA = 2.840 PEND STORAGE = 0.0											
----- TOTAL CHANGE = -2.275											
SLW CAL TOTAL = 312673. SLW ORS TOTAL = 338162. SLW CAL SPINT = 200568. SLV ORS SR = 262564. SLW CAL RF = 112075. SLV ORS RF = 75158.											
PACK ON DECEMBER 31 = 0.20 CHANGE IN SNOW STORAGE = 0.12											
AVERAGE MONTHLY BASE FLOW 16.6 148.4 291.4 294.0 9.3 9.0 0.0 0.0 0.0 6.2 9.0 77.5											
LEAP YEAR INDICATOR= 0 YES=1 & NO=0											
YEAR 55											
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE											
JAN. FEB. MAR. APR. MAY. JUN. JUL. AUG. SEP. OCT. NOV. DEC. TOTAL 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0											

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1955

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.49	0.59	0.34	1.04	2.39	3.41	1.24	1.43	3.85	0.19	0.05	0.18	15.21
CALCULATED TOTAL RUNOFF	126.	100.	100.	299.	936.	3124.	1433.	1312.	2359.	338.	211.	200.	10573.
OBSERVED TOTAL RUNOFF	32.	325.	512.	427.	74.	686.	1.	6.	2176.	147.	10.	85.	4481.
CALCULATED SURFACE RUNOFF	5.	39.	28.	233.	820.	2859.	1178.	1062.	2131.	43.	2.	41.	8478.
OBSERVED SURFACE RUNOFF	13.	170.	221.	133.	65.	677.	1.	6.	2176.	140.	1.	7.	3617.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	131.	88.	72.	66.	116.	225.	259.	250.	228.	295.	210.	150.	2055.
OBSERVED BASEFLOW	19.	148.	291.	294.	9.	9.	0.	0.	0.	6.	9.	78.	863.
ETP	0.139	0.635	2.434	4.375	5.391	6.028	6.949	5.878	4.870	3.142	1.466	0.490	41.855
UETA	0.013	0.179	0.240	0.923	1.235	2.031	1.558	1.261	0.857	0.810	0.191	0.040	9.269
LETA	0.0	0.0	0.0	0.340	0.258	0.452	0.036	0.0	0.215	0.382	0.0	0.0	1.434
ETA	0.317	0.255	0.303	0.963	1.493	2.483	1.644	1.261	1.073	1.192	0.191	0.188	11.364
PER-CORRELATION	0.017	0.106	0.031	0.655	0.685	0.452	0.086	0.0	0.619	0.0	0.0	0.0	1.455
UTS	2.651	2.929	2.987	2.764	2.657	3.213	2.836	2.643	2.634	3.653	3.240	3.221	2.944
L75A	7.801	7.875	7.936	7.586	7.828	7.944	7.801	7.800	7.891	7.941	7.821	7.821	7.862
L75T	7.801	7.879	7.936	7.586	7.828	7.844	7.801	7.800	7.891	7.941	7.821	7.821	7.862
GWS	2.019	2.014	2.610	2.807	2.505	2.922	2.034	2.034	2.030	2.042	2.031	2.023	2.023
TEMP.	27.7	26.8	35.0	50.1	64.3	68.4	82.7	70.4	68.8	56.9	36.8	28.8	53.1
CORRELATION COEFFICIENTS	0.836	0.595	0.540	0.651	0.711	0.833	0.971	0.229	0.949	0.623	0.128	0.727	0.604

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1956

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.16	0.53	0.19	0.77	1.35	1.23	2.71	1.66	0.36	0.96	0.11	0.06	9.76
CALCULATED TOTAL RUNOFF	121.	117.	78.	407.	636.	267.	2719.	587.	110.	214.	100.	44.	5359.
OBSERVED TOTAL RUNOFF	226.	368.	627.	450.	371.	363.	2306.	155.	0.	0.	0.	0.	4568.
CALCULATED SURFACE RUNOFF	4.	36.	15.	321.	557.	222.	2460.	414.	0.	123.	42.	0.	4224.
OBSERVED SURFACE RUNOFF	9.	123.	38.	120.	222.	360.	2301.	154.	0.	0.	0.	0.	3339.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	115.	80.	63.	86.	79.	45.	229.	173.	110.	92.	58.	44.	1175.
OBSERVED BASEFLOW	217.	235.	589.	330.	149.	3.	5.	2.	0.	0.	0.	0.	1529.
ETP	0.634	0.401	2.604	3.833	5.458	6.768	6.019	5.752	4.945	3.293	1.645	1.111	43.103
UETA	0.031	0.006	0.240	0.924	1.233	1.539	1.601	1.164	0.259	0.220	0.150	0.075	7.392
LETA	0.0	0.0	0.0	0.002	0.128	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.130
ETA	0.124	0.342	0.420	0.926	1.360	1.239	1.601	1.164	0.249	0.220	0.150	0.075	8.031
PER-CORRELATION	0.0	0.009	0.000	0.099	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.109
UZS	3.291	3.400	3.727	3.501	2.784	2.299	2.174	2.492	2.113	2.083	2.299	2.225	2.763
LZSA	7.821	7.823	7.831	7.923	7.833	7.805	7.800	7.800	7.800	7.800	7.800	7.800	7.819
LZST	7.821	7.823	7.831	7.923	7.833	7.800	7.800	7.800	7.800	7.800	7.800	7.800	7.819
GWS	2.017	2.012	2.009	2.007	2.005	2.005	2.024	2.022	2.016	2.012	2.008	2.006	2.012
TEMP.	28.1	25.2	41.0	47.7	65.8	78.5	77.7	77.5	70.1	60.0	39.7	35.7	54.4
CORRELATION COEFFICIENTS	0.759	0.595	0.727	0.427	0.506	0.141	0.567	0.441	1.000	1.000	1.000	0.871	0.684

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1957

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.22	0.42	2.44	2.78	6.18	7.81	1.03	3.23	1.61	1.43	0.67	0.01	27.42
CALCULATED TOTAL RUNOFF	32.	31.	119.	1999.	9217.	26774.	6402.	4186.	4306.	2112.	1521.	1112.	57601.
OBSERVED TOTAL RUNOFF	2.	13.	105.	2253.	13469.	31743.	6602.	3589.	4873.	657.	833.	665.	64824.
CALCULATED SURFACE RUNOFF	0.	10.	52.	1848.	8814.	26320.	3824.	2184.	2593.	240.	58.	1.	45993.
OBSERVED SURFACE RUNOFF	1.	8.	55.	1803.	12446.	29853.	4866.	3456.	4735.	99.	23.	14.	57398.
CALCULATED INTER-FLUX	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	32.	21.	27.	150.	403.	455.	2578.	2002.	1502.	1863.	1463.	1111.	11608.
OBSERVED BASEFLOW	2.	6.	5.	450.	1023.	1890.	1736.	133.	139.	558.	810.	651.	7406.
ETP	0.293	1.375	1.883	3.759	5.002	6.050	6.782	5.756	4.560	2.957	1.304	1.228	40.589
UETA	0.031	0.034	0.200	1.322	2.280	2.890	2.402	1.476	1.348	0.814	0.229	0.070	13.195
LETA	0.0	0.0	0.0	0.130	1.156	1.556	1.293	1.010	0.738	0.394	0.0	0.0	6.278
ETA	0.135	0.509	0.648	1.504	3.435	4.446	3.696	2.486	2.086	1.209	0.342	0.070	22.156
PER-CORRELATION	0.0	0.0	0.0	0.944	2.150	2.150	0.373	0.055	0.278	0.001	0.011	0.000	6.502
UIS	2.161	2.187	2.293	4.230	4.290	4.342	3.612	2.726	3.671	3.623	3.782	3.963	3.410
LES	7.800	7.800	7.800	8.426	8.426	10.064	10.385	9.297	8.627	8.175	8.015	8.024	8.621
LST	7.800	7.800	7.800	8.426	8.426	10.064	10.385	9.297	8.627	8.175	8.015	8.024	8.621
GAS	2.005	2.003	2.002	2.096	2.076	2.310	2.480	2.383	2.361	2.288	2.215	2.158	2.192
TEMP.	21.2	37.0	38.2	48.3	58.7	69.7	79.9	77.6	63.9	53.8	37.7	37.8	52.0
CORRELATION COEFFICIENTS	0.318	0.673	0.768	0.769	0.705	0.875	0.611	0.637	0.863	0.952	0.985	0.976	0.769

DELTA STORAGE = 5.206 INCHES											
AIA = 3.814											
PCND STORAGE = 0.0											

TOTAL CHANGE = 1.352											
SUM CAL TOTAL = 386245.											
SUM GAS TOTAL = 412314.											
SUM CAL SPRINT = 259298.											
SUM OVS SR = 327319.											
SUM CAL BF = 126552.											
SUM CBS BF = 84556.											
PACK ON DECEMBER 31 = 0.04											
CHANGE IN SNOW STORAGE = 0.05											
AVERAGE MONTHLY BASE FLOW											
806.0 616.01519.02700.02046.0 720.01240.01054.0 660.0 496.0 760.0 868.0											
LEAP YEAR INDICATOR = 0 YES=1 & NO=0											
YEAR											
53											
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE											
JAN. FEB. MAR. APR. MAY. JUN. JUL. AUG. SEP. OCT. NOV. DEC. TOTAL											
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0											

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1958

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.37	0.33	1.51	3.20	4.11	2.98	6.37	2.26	0.99	0.12	0.80	0.47	22.64
CALCULATED TOTAL RUNOFF	879.	634.	588.	3515.	4404.	1529.	9438.	11157.	2478.	1623.	1170.	920.	38742.
OBSERVED TOTAL RUNOFF	325.	644.	1860.	3473.	4184.	2408.	8396.	7233.	2369.	602.	825.	520.	33745.
CALCULATED SURFACE RUNOFF	67.	95.	545.	3062.	3947.	593.	9000.	5501.	831.	0.	16.	44.	28203.
OBSERVED SURFACE RUNOFF	19.	20.	341.	173.	2138.	1688.	7158.	6179.	1709.	112.	45.	52.	20240.
CALCULATED INTER-FLCN	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	313.	537.	442.	456.	461.	536.	433.	1555.	1647.	1623.	1154.	876.	10539.
OBSERVED BASEFLOW	306.	616.	1519.	2700.	2046.	720.	1240.	1054.	660.	496.	780.	868.	13505.
ETP	0.796	0.710	0.0	3.344	5.369	6.213	6.334	5.647	4.882	3.059	1.281	0.848	39.523
UETA	0.032	0.172	0.0	1.155	2.302	2.235	2.435	2.042	1.352	0.454	0.095	0.113	12.483
LETA	0.0	0.0	0.0	0.012	0.538	1.232	1.338	1.099	0.845	0.015	0.0	0.0	5.479
ETA	0.166	0.232	0.742	1.435	3.240	3.921	3.773	3.141	2.137	0.471	0.238	0.157	19.363
PES-CCUATION	0.095	0.175	1.082	2.050	1.291	0.076	1.393	0.735	0.088	0.0	0.0	0.0	7.023
U75	3.977	4.072	4.147	4.269	4.093	2.384	3.743	3.416	3.290	2.579	2.502	3.090	3.579
L75A	8.022	8.148	8.404	11.283	11.837	11.194	10.566	10.528	9.955	9.563	9.563	9.568	9.895
L25T	8.032	8.148	8.404	11.282	11.837	11.194	10.566	10.528	9.955	9.568	9.568	9.568	9.895
GWS	2.115	2.086	2.064	2.083	2.094	2.053	2.151	2.302	2.308	2.230	2.169	2.124	2.153
TEMP.	31.9	28.5	25.7	48.0	64.0	70.0	73.7	75.0	69.1	56.0	40.8	31.1	51.4
CCRELATION COEFFICIENTS	0.670	0.609	0.644	0.591	0.872	0.633	0.575	0.407	0.571	0.586	0.938	0.202	0.701

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1959

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.39	0.65	2.16	0.86	1.89	2.65	2.99	3.59	3.10	3.19	0.05	0.21	21.73
CALCULATED TOTAL RUNOFF	652.	560.	600.	465.	935.	3277.	1599.	2905.	1825.	2525.	484.	301.	16687.
OBSERVED TOTAL RUNOFF	568.	1254.	1505.	1337.	1184.	1619.	263.	325.	202.	2175.	771.	876.	12233.
CALCULATED SURFACE RUNOFF	11.	14.	445.	198.	695.	2936.	1642.	2580.	1496.	2110.	125.	23.	12505.
OBSERVED SURFACE RUNOFF	11.	54.	300.	37.	254.	1169.	201.	313.	196.	1586.	51.	8.	5218.
CALCULATED INTER-FLC.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	641.	416.	255.	266.	240.	341.	317.	325.	329.	416.	359.	279.	4283.
OBSERVED BASEFLOW	558.	1260.	1209.	1350.	930.	450.	62.	12.	6.	539.	720.	868.	8014.
ETP	6.470	0.827	2.758	3.999	5.231	6.517	6.426	5.875	4.551	2.829	1.496	1.157	42.037
UEIA	0.076	0.135	0.635	1.267	1.653	2.147	2.022	1.920	1.505	1.023	0.265	0.255	12.958
LEIA	0.0	0.0	0.0	0.028	0.778	1.327	0.855	0.357	0.217	0.254	0.0	0.0	3.826
ETA	0.210	0.252	0.689	1.295	2.431	3.473	2.837	2.277	1.732	1.276	0.265	0.255	17.035
PEP - CORRELATION	0.0	0.020	0.542	0.006	0.133	0.473	0.071	0.237	0.426	1.589	0.003	0.0	3.607
U25	3.154	3.472	3.750	3.716	3.468	3.283	2.806	3.424	3.471	4.119	4.198	4.044	3.575
U25A	5.563	5.566	9.706	10.114	9.870	9.185	8.060	7.819	7.844	9.102	9.348	9.348	9.124
L751	5.538	9.538	5.736	10.114	5.870	9.185	8.060	7.819	7.844	9.102	9.348	9.348	9.124
G45	2.001	2.063	2.051	2.039	2.029	2.051	2.046	2.055	2.051	2.066	2.054	2.040	2.053
TEMP.	25.8	29.1	35.7	50.3	62.0	75.0	75.0	74.4	63.7	50.3	36.0	35.0	51.9
CORRELATION COEFFICIENTS	0.789	0.853	0.840	0.789	0.748	0.835	0.423	0.423	0.725	0.677	0.660	0.965	0.729

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1960

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	5.57	1.86	1.57	1.60	3.90	3.55	0.82	2.97	1.11	1.86	0.16	0.52	26.80
CALCULATED TOTAL RUNOFF	258.	856.	822.	3022.	9817.	4759.	1642.	3310.	1159.	1050.	571.	473.	28753.
OBSERVED TOTAL RUNOFF	615.	1843.	5734.	3728.	10007.	4543.	622.	1741.	264.	245.	503.	719.	34993.
CALCULATED SURFACE RUNOFF	91.	668.	657.	3550.	9224.	3963.	495.	2529.	327.	360.	29.	61.	21954.
OBSERVED SURFACE RUNOFF	20.	335.	7564.	428.	7310.	3233.	64.	1672.	231.	84.	23.	6.	20976.
CALCULATED INTER- FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	207.	188.	165.	372.	593.	836.	1146.	781.	863.	690.	542.	412.	6785.
OBSERVED BASEFLOW	589.	1508.	2170.	3300.	2697.	1710.	558.	68.	63.	161.	480.	713.	14317.
ETP	0.415	0.171	0.694	4.244	5.105	6.148	6.457	5.650	4.833	3.128	1.685	0.545	39.114
UETA	0.102	0.041	0.120	1.479	2.186	2.567	1.730	1.445	0.941	0.635	0.302	0.123	11.722
LETA	0.0	0.0	0.0	0.032	0.559	1.382	1.150	1.072	0.740	0.364	0.0	0.0	5.700
ETA	3.239	0.302	0.753	1.511	3.145	3.949	2.931	2.518	1.681	0.999	0.302	0.288	18.588
PER- COLLATION	0.057	1.434	1.412	0.342	1.296	0.591	0.021	0.114	0.011	0.057	0.009	0.028	5.412
U2S	4.072	4.505	4.520	3.946	4.204	3.892	2.865	2.764	2.797	3.107	3.479	3.537	3.639
L2SA	9.376	10.569	11.282	12.621	13.083	12.575	11.574	10.474	9.705	9.122	9.032	9.038	10.702
L2ST	5.376	10.569	11.292	12.621	12.583	12.575	11.574	10.474	9.705	9.122	9.032	9.038	10.712
GAS	2.029	2.022	2.017	2.059	2.130	2.204	2.139	2.134	2.137	2.105	2.073	2.058	2.099
TEMP.	24.4	21.4	31.0	54.1	60.2	73.0	75.4	76.5	68.3	56.6	40.9	30.0	50.8
CORRELATION COEF- FICIENTS	0.542	0.580	0.715	0.601	0.585	0.574	0.776	0.523	0.589	0.801	0.847	0.806	0.667

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1961

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.12	0.13	1.72	1.22	6.42	4.87	2.78	4.14	1.80	0.76	1.94	0.26	26.16
CALCULATED TOTAL RUNOFF	302.	206.	886.	544.	8054.	11583.	3309.	6640.	2758.	1518.	2413.	978.	35642.
OBSERVED TOTAL RUNOFF	792.	1001.	1145.	1385.	5954.	11571.	2110.	5168.	863.	795.	1207.	1047.	33038.
CALCULATED SURFACE RUNOFF	1.	5.	682.	766.	7724.	10606.	2121.	5631.	1435.	178.	1425.	18.	39591.
OBSERVED SURFACE RUNOFF	17.	21.	51.	275.	4280.	5441.	1397.	4672.	413.	51.	67.	24.	20749.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	301.	201.	204.	176.	331.	577.	1138.	1009.	1273.	1440.	980.	560.	9051.
OBSERVED BASEFLOW	775.	580.	1054.	1110.	1674.	2130.	713.	456.	450.	744.	1140.	1023.	12289.
ETP	1.018	1.367	2.820	3.125	4.579	5.203	6.560	5.534	4.435	2.988	1.305	0.355	40.745
UFTA	0.029	0.069	0.785	0.525	2.137	2.717	2.124	1.920	1.236	0.752	0.314	0.037	13.145
LETA	0.0	0.0	0.0	0.032	0.588	1.463	1.226	1.094	0.705	0.295	0.0	0.0	5.813
ETA	0.023	0.101	0.785	1.230	3.175	4.179	3.360	3.015	1.991	1.047	0.407	0.196	19.516
PER-CORRELATION	0.070	0.009	0.396	0.225	2.554	2.368	0.260	0.354	0.221	0.028	0.776	0.054	7.584
UTS	3.775	3.761	3.834	3.852	4.191	4.106	2.563	3.475	3.623	3.432	3.659	3.911	3.714
L254	5.050	9.064	5.317	9.588	10.442	12.420	11.608	10.937	10.517	10.067	10.398	10.786	10.360
L757	5.050	5.064	5.217	9.588	10.442	12.420	11.608	10.937	10.517	10.067	10.398	10.786	10.360
GAS	2.043	2.032	2.025	2.022	2.361	2.268	2.258	2.263	2.268	2.216	2.170	2.136	2.147
TEMP.	39.2	35.7	40.5	45.3	58.4	70.8	76.8	74.9	61.8	53.8	36.2	24.9	51.0
CORRELATION COEFFICIENTS	0.859	0.907	0.525	0.447	0.757	0.734	0.301	0.320	0.712	0.917	0.541	0.891	0.721

DELTA STORAGE =	5.226	INCHES
PAID =	3.679	
POND STORAGE =	0.0	
TOTAL CHANGE =	1.547	
SLM CAL TOTAL =	51066.	
SLM OBS TOTAL =	526323.	
SLM CAL SPRINT =	352445.	
SUM OBS SR =	393501.	
SLM CAL RF =	157621.	
SLM OBS RF =	132822.	
PACK ON DECEMBER 31 =	0.30	
CHANGE IN SNOW STORAGE =	0.20	

DAILY FLOW DURATION AND ERROR TABLE

FLOW INTERVAL	ACT.CASES	PCT.	CALC.CASES	PCT.	AVE.FPKDP	AV.ABS.ERROR	SID.ERROR
0.0-	910.0	100.000	65.0	100.000	18.4	18.35	31.22
1.0-	164.0	81.545	148.0	58.682	22.5	22.55	38.51
1.8-	146.0	78.219	206.0	55.680	26.0	26.12	37.22
3.2-	163.0	75.259	420.0	51.503	30.0	30.58	57.23
5.6-	303.0	71.953	558.0	82.485	14.3	19.50	31.87
10.0-	416.0	65.707	671.0	70.858	12.3	19.48	31.25
17.8-	544.0	57.230	655.0	57.250	11.7	25.76	48.63
31.6-	777.0	38.096	741.0	43.967	6.9	37.64	59.57
55.2-	487.0	22.328	683.0	28.939	48.5	83.74	113.21
100.0-	302.0	12.452	936.0	16.711	40.4	123.14	179.02
177.8-	112.0	6.327	201.0	10.595	102.7	232.03	320.64
316.2-	77.0	4.056	156.0	6.429	160.5	352.55	516.02
562.3-	47.0	2.494	88.0	2.265	226.9	630.23	834.49
1000.0-	33.0	1.541	35.0	1.480	107.6	1071.89	1574.94
1778.3-	20.0	0.972	25.0	0.771	-873.2	1835.33	2377.70
3162.3-	11.0	0.466	7.0	0.264	-2518.6	2518.58	756.16
5623.4-	5.0	0.243	5.0	0.122	-3829.8	3829.83	799.83
10000.0-	6.0	0.142	1.0	0.020	-7037.3	7037.26	4748.14
17782.7-	6.0	0.020	0.0	0.0	-30162.2		
31622.7-	1.0	0.020	0.0	0.0			
56234.6-	0.0	0.0	0.0	0.0			
69555.8-	0.0	0.0	0.0	0.0			
177827.4-	0.0	0.0	0.0	0.0			
316226.5-	0.0	0.0	0.0	0.0			
	4931.0		4931.0		-7124.3	448933.31	12557.65

DELTA STORAGE = 39.368 INCHES
 AREA = 45.527
 FORD STORAGE = 0.0

 TOTAL CHANGE = -6.139

TOTAL PRECIPITATION = 288.308

 TOTAL IA 45.507
 TOTAL SURFACE RUNOFF 12.487
 TOTAL DELTA 163.903
 TOTAL PERC 60.961
 CHANGE IN UZSM 1.049

 CHECK BALANCE 287.911

RESULTS - MODEL B-ZERO

KSU_REMOTE..COMPUTING..LABORATORY..	SEASON.....JOB 232.....	1 APR 77..RCL06587..	ROGERS.	START.....
KSU_REMOTE..COMPUTING..LABORATORY..	SEASON.....JOB 232.....	1 APR 77..RCL06587..	ROGERS.	START.....
KSU_REMOTE..COMPUTING..LABORATORY..	SEASON.....JOB 232.....	1 APR 77..RCL06587..	ROGERS.	START.....
KSU_REMOTE..COMPUTING..LABORATORY..	SEASON.....JOB 232.....	1 APR 77..RCL06587..	ROGERS.	START.....
KSU_REMOTE..COMPUTING..LABORATORY..	SEASON.....JOB 232.....	1 APR 77..RCL06587..	ROGERS.	START.....

[illegible]

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SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1948

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.04	0.53	1.92	0.48	3.60	5.60	2.00	4.14	0.98	0.50	1.04	0.45	21.37
CALCULATED TOTAL RUNOFF	0.	6.	315.	55.	2457.	7245.	2267.	6984.	1350.	878.	973.	492.	23025.
OBSERVED TOTAL RUNOFF	21.	423.	1409.	390.	2101.	13288.	2454.	3513.	40.	5.	131.	338.	24114.
CALCULATED SURFACE RUNOFF	0.	6.	275.	55.	2361.	6946.	1743.	6439.	464.	119.	434.	44.	18887.
OBSERVED SURFACE RUNOFF	2.	351.	882.	90.	2042.	12418.	1214.	3110.	28.	1.	11.	28.	20177.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	0.	0.	40.	0.	96.	238.	524.	545.	986.	760.	539.	449.	4137.
OBSERVED BASEFLOW	19.	73.	527.	300.	59.	870.	1240.	403.	12.	5.	120.	310.	3937.
ETP	0.887	0.845	1.337	4.549	5.315	6.210	6.537	5.709	5.012	3.045	1.100	0.708	41.253
UETA	0.168	0.119	0.380	1.239	1.834	2.765	2.277	2.320	1.408	0.737	0.245	0.107	13.593
LETA	0.0	0.0	0.0	0.0	0.521	1.489	1.226	1.249	0.700	0.0	0.0	0.0	5.185
ETA	0.179	0.273	0.731	1.239	2.355	4.254	3.504	3.569	2.107	0.737	0.442	0.220	19.609
PER-COLATION	0.0	0.0	0.183	0.0	0.549	1.678	0.091	1.017	0.066	0.0	0.0	0.0	3.585
UZS	2.880	2.939	3.646	3.801	3.619	4.161	3.909	4.195	3.636	2.967	3.024	3.660	3.538
LZSA	9.400	9.400	9.468	9.583	9.487	9.437	9.173	8.645	8.047	7.800	7.800	7.800	8.835
LZST	9.400	9.400	9.468	9.583	9.487	9.437	9.173	8.645	8.047	7.800	7.800	7.800	8.835
GWS	2.000	2.000	2.000	1.999	2.003	2.064	2.104	2.152	2.149	2.111	2.084	2.564	2.061
TEMP.	28.5	30.0	33.8	58.8	63.2	70.9	76.5	76.8	71.2	55.0	37.7	30.5	52.8
CORRELATION COEFFICIENTS	1.000	0.636	0.552	0.419	0.802	0.603	0.470	0.207	0.817	0.590	0.307	0.002	0.644

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1949

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.33	1.16	1.69	3.45	5.16	6.90	2.95	3.62	0.42	1.98	0.37	0.11	27.85
CALCULATED TOTAL RUNOFF	392.	543.	695.	1379.	5937.	8601.	3391.	2893.	1268.	3077.	748.	567.	29491.
OBSERVED TOTAL RUNOFF	37.	6127.	2325.	1554.	3496.	12838.	1929.	809.	97.	504.	569.	521.	30807.
CALCULATED SURFACE RUNOFF	64.	316.	486.	1165.	5614.	8123.	2846.	2177.	398.	2336.	12.	8.	23544.
OBSERVED SURFACE RUNOFF	3.	5035.	310.	294.	1388.	9938.	1278.	635.	58.	269.	-1.	25.	19132.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	328.	227.	209.	214.	323.	478.	545.	717.	870.	741.	737.	560.	5948.
OBSERVED BASEFLOW	34.	1092.	2015.	1260.	2108.	3000.	651.	174.	39.	236.	570.	496.	11574.
ETP	0.0	0.509	2.677	3.584	5.333	6.288	6.642	5.547	4.568	3.311	1.903	1.017	41.100
UETA	0.0	0.110	0.757	1.452	2.479	2.853	2.269	2.102	1.344	0.921	0.240	0.109	14.636
LETA	0.0	0.0	0.0	0.121	1.217	1.536	1.222	1.132	0.724	0.403	0.0	0.0	6.360
ETA	0.139	0.393	0.788	1.805	3.696	4.390	3.490	3.233	2.368	1.329	0.240	0.109	21.680
PER-CORRELATION	0.0	0.497	0.576	1.394	2.285	3.285	0.314	0.691	0.000	0.190	0.0	0.0	9.231
UZS	3.896	4.258	4.331	4.402	4.370	4.205	3.781	3.837	3.546	3.702	3.535	3.435	3.939
LZSA	7.800	7.915	8.407	9.789	10.962	12.882	12.547	11.684	11.198	10.735	10.671	10.671	10.452
LZST	7.800	7.915	8.407	9.789	10.962	12.882	12.547	11.684	11.198	10.735	10.671	10.671	10.452
GWS	2.047	2.034	2.026	2.020	2.051	2.144	2.176	2.162	2.148	2.134	2.108	2.079	2.094
TEMP.	18.3	29.9	39.5	51.9	63.5	71.9	78.0	74.3	64.3	54.2	47.3	32.4	52.2
CORRELATION COEFFICIENTS	0.659	0.692	0.692	0.537	0.670	0.494	0.744	0.690	0.521	0.657	0.970	0.983	0.688

DELTA STORAGE = 5.112 INCHES												
AATA = 3.158												
POND STORAGE = 0.0												
TOTAL CHANGE = 1.954												
SUM CAL TOTAL = 52516.												
SUM OBS TOTAL = 54920.												
SUM CAL SRINT = 42431.												
SUM OBS SR = 39309.												
SUM CAL BF = 10085.												
SUM OBS BF = 15611.												
PACK ON DECEMBER 31 = 0.0												
CHANGE IN SNOW STORAGE = -0.26												
AVERAGE MONTHLY BASE FLOW												
372.01008.01023.0 600.0 465.0 105.01395.03410.01530.0 744.0 690.0 713.0												
LEAP YEAR INDICATOR = 0 YES=1 & NO=0												
ITHAW IFREZ												
120 306												
YEAR 50												
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE												
JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1950

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.12	1.20	0.63	1.25	3.12	1.83	7.43	6.76	0.44	0.55	0.07	0.02	23.42
CALCULATED TOTAL RUNOFF	414.	452.	378.	467.	1720.	1647.	30767.	21070.	3702.	2595.	1947.	1476.	66635.
OBSERVED TOTAL RUNOFF	371.	1027.	1041.	721.	599.	449.	21805.	31911.	2063.	952.	710.	725.	62374.
CALCULATED SURFACE RUNOFF	5.	176.	150.	288.	1491.	1440.	30452.	17864.	238.	225.	3.	0.	52333.
OBSERVED SURFACE RUNOFF	-1.	19.	18.	121.	134.	344.	20410.	28501.	533.	208.	20.	12.	50319.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	409.	276.	227.	180.	229.	207.	315.	3206.	3463.	2371.	1943.	1476.	14303.
OBSERVED BASEFLOW	372.	1008.	1023.	600.	465.	105.	1395.	3410.	1530.	744.	690.	713.	12055.
ETP	0.795	1.558	2.302	3.873	5.046	6.390	6.258	5.308	4.622	3.284	1.589	1.099	42.130
UETA	0.024	0.282	0.666	1.205	1.840	2.326	2.473	2.410	1.393	0.711	0.199	0.063	13.593
LETA	0.0	0.0	0.0	0.0	0.602	1.289	1.361	1.293	0.750	0.399	0.014	0.0	5.713
ETA	0.041	0.282	0.793	1.205	2.442	3.615	3.834	3.708	2.143	1.109	0.213	0.063	19.448
PER-CORRELATION	0.0	0.027	0.016	0.057	0.283	0.011	2.231	2.768	0.0	0.0	0.0	0.0	5.392
UZS	3.403	3.820	4.028	3.898	3.913	3.587	3.974	4.273	3.679	3.237	2.830	2.742	3.615
LZSA	10.671	10.675	10.705	10.743	10.622	9.808	9.254	11.080	11.099	10.532	10.350	10.350	10.490
LZSI	10.671	10.675	10.705	10.743	10.622	9.808	9.264	11.080	11.099	10.532	10.350	10.350	10.490
GWS	2.058	2.043	2.032	2.024	2.019	2.019	2.113	2.558	2.506	2.387	2.285	2.209	2.164
TEMP.	27.3	36.8	38.2	48.4	59.3	73.3	72.7	70.6	64.9	59.8	38.9	34.5	52.1
CORRELATION COEFFICIENTS	0.903	0.668	0.638	0.599	0.510	0.457	0.582	0.659	0.887	0.715	0.936	0.717	0.687

DELTA STORAGE = 1.586 INCHES												
AATA = 2.658												
POND STORAGE = 0.0												
TOTAL CHANGE = -1.072												
SUM CAL TOTAL = 119151.												
SUM OBS TOTAL = 117295.												
SUM CAL SRINT = 94764.												
SUM OBS SR = 89629.												
SUM CAL RF = 24388.												
SUM OBS RF = 27666.												
PACK ON DECEMBER 31 = 0.0												
CHANGE IN SNOW STORAGE = 0.0												
AVERAGE MONTHLY BASE FLOW												
868.0 952.01240.01170.01612.04800.06820.03410.02760.02294.02250.01085.0												
LEAP YEAR INDICATOR= 0 YES=1 & NO=0												
ITHAW IFREZ	YEAR											
122 283	51											
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE												
JAN. 0.0	FEB. 0.0	MAR. 0.0	APR. 0.0	MAY. 0.0	JUN. 1.915	JUL. 3.935	AUG. 0.0	SEP. 0.0	OCT. 0.0	NOV. 0.0	DEC. 0.0	TOTAL 5.850

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1951

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.29	0.93	0.78	2.58	6.00	9.56	7.51	2.75	3.42	0.70	0.18	0.10	34.79
CALCULATED TOTAL RUNOFF	1087.	774.	795.	1756.	18678.	26098.	56869.	38848.	28786.	19007.	13379.	10160.	216237.
OBSERVED TOTAL RUNOFF	892.	976.	1249.	1503.	17401.	53000.	79382.	9426.	11537.	2494.	2386.	1452.	181698.
CALCULATED SURFACE RUNOFF	8.	64.	220.	1370.	17992.	20883.	23583.	3381.	3202.	139.	4.	1.	70848.
OBSERVED SURFACE RUNOFF	24.	24.	9.	333.	15769.	48200.	72562.	6016.	8777.	203.	136.	367.	152437.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	228.	2887.	2822.	1960.	849.	562.	427.	9734.
CALCULATED BASEFLOW	1079.	710.	575.	386.	686.	4987.	30398.	32645.	23625.	18019.	12813.	9732.	135655.
OBSERVED BASEFLOW	868.	952.	1240.	1170.	1612.	4800.	6820.	3410.	2760.	2294.	2250.	1085.	29261.
ETP	0.458	1.240	2.453	3.869	5.235	5.774	6.353	5.626	4.494	2.938	1.491	0.666	40.598
UETA	0.025	0.185	0.440	1.139	2.038	2.886	2.728	2.154	1.800	0.847	0.255	0.058	14.554
LETA	0.0	0.0	0.0	0.0	0.652	1.554	1.469	1.160	0.969	0.196	0.0	0.0	6.000
ETA	0.206	0.264	0.491	1.139	2.690	4.440	4.197	3.313	2.769	1.043	0.277	0.116	20.945
PER-COLATION	0.0	0.0	0.0	0.542	2.161	4.591	3.669	0.604	0.978	0.0	0.0	0.0	12.546
UZS	2.804	2.960	3.240	3.837	4.027	4.449	4.297	3.966	4.044	3.287	3.154	3.021	3.593
LZSA	10.350	10.350	10.350	10.558	11.507	13.447	12.585	11.583	11.512	11.072	11.046	11.046	11.288
LZST	10.350	10.350	10.350	10.558	11.507	13.975	16.809	16.901	16.550	15.975	15.909	15.880	13.782
GWS	2.153	2.114	2.086	2.068	2.145	2.979	6.456	6.637	5.468	4.558	3.880	3.382	3.674
TEMP.	27.3	35.4	36.1	48.3	62.1	64.9	74.0	75.6	62.8	52.6	37.5	27.5	50.4
CORRELATION COEFFICIENTS	0.803	0.687	0.828	0.711	0.634	0.677	0.502	0.535	0.546	0.974	0.954	0.836	0.724

550.01595.01550.02400.02325.0	330.0	55.8	34.1	0.0	1.6	45.0	155.0
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LEAP YEAR INDICATOR= 1 YES=1 & NO=0

ITHAW	IFREZ
132	280

YEAR 52

RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE

[illegible]

SUMMARY TABLE - SOUTH FORK SOLCHON RIVER BASIN - 1952

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.10	0.20	1.75	3.10	2.76	0.37	2.59	2.92	0.75	0.03	0.07	0.85	15.47
CALCULATED TOTAL RUNOFF	7428.	5131.	4042.	3237.	5285.	2870.	2766.	2109.	1675.	1158.	823.	709.	37232.
CONSERVED TOTAL RUNOFF	1860.	1885.	3100.	4200.	4656.	488.	110.	117.	28.	2.	50.	255.	16751.
CALCULATED SURFACE RUNOFF	0.	2.	323.	722.	3012.	238.	849.	858.	341.	0.	0.	84.	6430.
OBSERVED SURFACE RUNOFF	310.	290.	1550.	1800.	2331.	158.	54.	83.	28.	0.	5.	100.	6710.
CALCULATED INTERFLOW	312.	216.	232.	997.	1963.	521.	0.	0.	0.	0.	0.	0.	4241.
CALCULATED BASEFLOW	7115.	4914.	3486.	1518.	310.	2111.	1917.	1250.	1334.	1158.	823.	625.	26561.
OBSERVED BASEFLOW	1550.	1595.	1550.	2400.	2325.	330.	56.	34.	0.	2.	45.	155.	10041.
ETP	0.955	1.537	0.804	3.630	5.155	6.844	6.458	5.754	4.887	2.948	1.402	0.208	40.641
UETA	0.036	0.119	0.170	1.247	2.163	2.199	1.391	1.458	1.110	0.250	0.044	0.031	10.218
LETA	0.0	0.0	0.0	0.0	0.307	1.330	1.151	1.072	0.693	0.059	0.0	0.0	4.622
ETA	0.069	0.141	0.835	1.378	2.470	3.529	2.542	2.530	1.503	0.318	0.059	0.297	15.972
PERCOLATION	0.0	0.0	0.362	0.855	0.482	0.0	0.0	0.006	0.022	0.0	0.0	0.0	1.727
UZS	2.978	2.934	3.580	4.051	4.003	2.922	2.446	2.431	2.760	2.229	2.087	2.541	2.913
LZSA	11.046	11.046	11.094	11.665	12.477	11.765	10.476	9.407	8.523	8.157	8.152	8.152	10.163
LZST	15.858	15.843	15.879	16.368	16.899	15.955	14.649	13.580	12.696	12.329	12.324	12.324	14.554
GWS	3.010	2.746	2.553	2.444	2.455	2.439	2.338	2.271	2.223	2.154	2.121	2.089	2.403
TEMP.	32.4	36.1	34.1	49.2	60.9	79.5	87.6	77.5	69.1	52.9	36.9	29.6	53.0
CORRELATION COEFFICIENTS	0.994	0.994	0.983	0.835	0.666	0.603	0.454	0.286	0.568	0.322	0.470	0.662	0.652

DELTA STORAGE = -1.829 INCHES												
AIA = 3.533												
POND STORAGE = 0.0												
TOTAL CHANGE = -5.362												
SUM CAL TOTAL = 372620.												
SUM OBS TOTAL = 315744.												
SUM CAL SRINT = 186017.												
SUM OBS SR = 248776.												
SUM CAL BF = 185603.												
SUM OBS RF = 66968.												
PACK ON DECEMBER 31 = 0.47												
CHANGE IN SNOW STORAGE = 0.47												
AVERAGE MONTHLY BASE FLOW												
372.0 588.0 930.0 813.0 527.0 6.0 99.2 89.9 3.0 4.7 156.0 310.0												
LEAP YEAR INDICATOR=0 YES=1 & NO=0												
ITHAW IFREZ												
134 303												
YEAR 53												
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE												
JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1953

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.33	0.19	1.63	2.29	2.50	2.61	3.43	3.43	0.44	1.21	1.79	1.05	20.91
CALCULATED TOTAL RUNOFF	492.	317.	780.	930.	1621.	2030.	4019.	4731.	824.	824.	451.	575.	17493.
OBSERVED TOTAL RUNOFF	771.	673.	1125.	999.	635.	317.	2267.	1315.	7.	5.	162.	351.	8627.
CALCULATED SURFACE RUNOFF	35.	11.	513.	610.	1381.	1806.	3695.	4268.	304.	404.	127.	319.	13471.
OBSERVED SURFACE RUNOFF	399.	85.	195.	189.	108.	311.	2167.	1225.	4.	0.	5.	41.	4731.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	457.	306.	268.	220.	240.	224.	324.	463.	520.	420.	324.	256.	4022.
OBSERVED BASEFLOW	372.	588.	930.	810.	527.	6.	99.	90.	3.	5.	156.	310.	3896.
ETP	0.931	1.509	2.535	3.822	5.092	6.667	6.584	5.590	4.906	3.239	1.257	0.118	42.259
UETA	0.021	0.134	0.451	1.148	1.719	2.469	2.046	2.143	1.188	0.653	0.276	0.051	12.309
LETA	0.0	0.0	0.0	0.0	0.194	1.082	0.814	0.779	0.155	0.074	0.0	0.0	3.107
ETA	0.151	0.134	0.652	1.148	1.913	3.551	2.859	2.922	1.353	0.737	0.464	0.393.	16.276
PER-CORRELATION	0.0	0.0	0.195	0.156	0.301	0.220	0.725	0.685	0.340	0.0	0.086	0.707	3.115
UZS	2.908	2.934	3.141	3.652	3.920	3.429	3.704	3.984	3.212	2.782	3.919	4.431	3.506
LZSA	8.152	8.152	8.264	8.397	8.406	8.180	7.848	7.900	7.800	7.800	7.833	8.297	8.103
LZST	12.324	12.324	12.437	12.570	12.778	12.323	11.510	11.195	10.481	9.991	9.839	10.304	11.502
GWS	2.065	2.048	2.037	2.028	2.023	2.023	2.045	2.092	2.083	2.062	2.048	2.035	2.049
TEMP.	37.9	36.1	44.0	47.5	50.0	77.1	77.2	75.0	69.4	58.8	41.6	29.8	54.6
CORRELATION COEFFICIENTS	0.652	0.847	0.451	0.497	0.729	0.590	0.498	0.494	0.628	0.470	0.522	0.431	0.565

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1954

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.14	0.48	0.76	0.78	5.60	2.36	1.39	2.67	0.62	1.52	0.02	0.06	16.39
CALCULATED TOTAL RUNOFF	233.	201.	203.	392.	6506.	4885.	1116.	1898.	675.	762.	284.	219.	17374.
OBSERVED TOTAL RUNOFF	389.	1021.	789.	744.	5110.	5516.	48.	134.	0.	5.	18.	23.	13790.
CALCULATED SURFACE RUNOFF	51.	80.	103.	290.	6275.	4386.	425.	1406.	187.	385.	0.	4.	13591.
OBSERVED SURFACE RUNOFF	132.	209.	45.	234.	4025.	4646.	23.	133.	0.	0.	1.	7.	9457.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	181.	121.	100.	102.	231.	499.	690.	492.	489.	378.	284.	216.	3783.
OBSERVED BASEFLOW	248.	812.	744.	510.	1085.	870.	25.	2.	0.	5.	17.	16.	4334.
ETP	0.901	1.865	2.535	4.397	4.904	6.560	6.982	5.807	5.109	2.931	1.819	1.048	44.920
UEIA	0.028	0.361	0.594	1.127	2.139	2.567	1.682	1.696	0.659	0.598	0.078	0.085	11.613
LEIA	0.0	0.0	0.0	0.0	0.616	1.392	1.218	0.468	0.156	0.111	0.0	0.0	3.962
ETA	0.028	0.361	0.594	1.127	2.755	3.459	2.903	2.164	0.815	0.709	0.078	0.109	15.599
PER-CORRELATION	0.144	0.042	0.047	0.012	1.952	0.481	0.0	0.078	0.0	0.062	0.0	0.0	2.820
UZS	4.129	4.092	4.020	3.719	4.231	3.772	2.478	2.772	2.432	2.747	2.693	2.622	3.304
LZSA	8.721	8.751	8.791	8.830	9.394	9.808	8.647	7.824	7.800	7.832	7.830	7.800	8.495
LZST	10.728	10.757	10.797	10.836	11.400	11.814	10.653	9.531	8.633	8.130	8.057	8.057	9.944
GWS	2.026	2.019	2.014	2.010	2.032	2.110	2.109	2.092	2.074	2.056	2.042	2.031	2.051
TEMP.	28.2	44.9	37.5	56.4	57.3	75.6	82.7	78.3	72.7	53.7	44.8	34.7	55.6
CORRELATION COEFFICIENTS	0.779	0.742	0.711	0.874	0.761	0.677	0.616	0.308	0.293	0.282	0.910	0.677	0.618

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1955

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.49	0.59	0.48	1.27	2.75	3.75	1.43	1.47	3.83	0.19	0.95	0.18	16.48
CALCULATED TOTAL RUNOFF	162.	145.	117.	438.	1122.	3750.	1409.	1229.	2039.	315.	191.	186.	11103.
OBSERVED TOTAL RUNOFF	32.	325.	512.	427.	74.	686.	1.	6.	2176.	147.	10.	85.	4481.
CALCULATED SURFACE RUNOFF	5.	39.	31.	348.	999.	3498.	1116.	957.	1795.	48.	2.	42.	8877.
OBSERVED SURFACE RUNOFF	13.	176.	221.	133.	65.	677.	1.	6.	2176.	140.	1.	7.	3617.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	158.	106.	87.	91.	123.	752.	293.	273.	244.	267.	190.	144.	2227.
OBSERVED BASEFLOW	19.	148.	291.	294.	9.	9.	0.	0.	0.	6.	9.	78.	863.
ETP	0.199	0.635	2.353	4.375	5.391	6.028	6.949	5.878	4.870	3.152	1.466	0.490	41.775
UETA	0.013	0.109	0.225	1.080	1.381	2.241	2.021	1.334	0.867	0.802	0.189	0.042	10.306
LETA	0.0	0.0	0.0	0.040	0.457	0.757	0.053	0.000	0.217	0.310	0.0	0.0	1.836
ETA	0.317	0.255	0.324	1.120	1.839	2.998	2.074	1.335	1.085	1.112	0.189	0.190	12.839
PER-COLATION	0.017	0.106	0.057	0.114	0.152	0.758	0.053	0.000	0.527	0.0	0.0	0.0	1.784
UZS	2.671	2.953	2.925	2.895	2.826	3.605	3.100	2.652	2.663	3.685	3.294	3.276	3.045
LZSA	7.801	7.880	7.940	8.054	7.862	7.916	7.800	7.800	7.872	7.866	7.800	7.800	7.865
LZSI	8.058	8.137	8.197	8.311	8.011	7.916	7.800	7.800	7.872	7.866	7.800	7.800	7.962
GWS	2.022	2.017	2.012	2.009	2.007	2.028	2.042	2.038	2.032	2.038	2.028	2.020	2.024
TEMP.	27.7	26.8	39.0	56.1	64.3	68.4	82.2	79.4	68.8	56.9	36.8	28.8	53.1
CORRELATION COEFFICIENTS	0.829	0.494	0.948	0.643	0.716	0.814	0.773	0.234	0.940	0.655	0.128	0.787	0.605

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1956

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.16	0.53	0.34	1.00	1.55	1.61	3.00	2.07	0.10	0.96	0.11	0.06	11.50
CALCULATED TOTAL RUNOFF	111.	110.	86.	644.	786.	592.	3327.	1025.	159.	258.	123.	58.	7278.
OBSERVED TOTAL RUNOFF	226.	368.	627.	450.	371.	363.	2306.	155.	0.	0.	0.	0.	4868.
CALCULATED SURFACE RUNOFF	5.	37.	29.	550.	760.	475.	3065.	795.	12.	133.	47.	0.	5849.
OBSERVED SURFACE RUNOFF	9.	133.	38.	120.	222.	360.	2301.	154.	0.	0.	0.	0.	3339.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	105.	73.	57.	94.	86.	117.	262.	230.	147.	125.	75.	58.	1429.
OBSERVED BASEFLOW	217.	235.	589.	330.	149.	3.	5.	2.	0.	0.	0.	0.	1523.
ETP	0.634	0.401	2.604	3.833	5.498	6.768	6.619	5.752	4.945	3.293	1.645	1.111	43.103
UETA	0.034	0.007	0.367	0.957	1.360	1.880	1.880	1.416	0.564	0.434	0.150	0.075	9.123
LETA	0.0	0.0	0.0	0.002	0.179	0.0	0.086	0.020	0.0	0.0	0.0	0.0	0.287
ETA	0.127	0.342	0.446	0.959	1.539	1.880	1.966	1.436	0.564	0.434	0.150	0.075	9.919
PER-COLATION	0.0	0.012	0.001	0.168	0.0	0.0	0.086	0.020	0.0	0.0	0.0	0.0	0.287
UZS	3.345	3.655	3.840	3.763	3.055	2.667	3.195	2.964	2.547	2.257	2.403	2.330	3.000
LZSA	7.800	7.803	7.813	7.967	7.857	7.800	7.800	7.800	7.800	7.800	7.800	7.800	7.820
LZST	7.800	7.803	7.813	7.967	7.857	7.800	7.800	7.800	7.800	7.800	7.800	7.800	7.820
GWS	2.015	2.011	2.008	2.008	2.006	2.007	2.028	2.028	2.022	2.016	2.011	2.008	2.014
TEMP.	28.1	29.2	41.9	47.7	65.8	78.5	77.7	77.5	70.1	60.0	39.7	35.7	54.4
CORRELATION COEFFICIENTS	0.592	0.592	0.662	0.437	0.468	0.148	0.560	0.411	1.000	1.000	1.000	0.871	0.668

DELTA STORAGE = 1.318 INCHES
 AATA = 2.888
 POND STORAGE = 0.0

TOTAL CHANGE = -1.570

SUM CAL TOTAL = 425869.
 SUM OBS TOTAL = 347510.
 SUM CAL SRINT = 227805.
 SUM OBS SR = 269920.
 SUM CAL BF = 198064.
 SUM OBS BF = 77590.

PACK ON DECEMBER 31 = -0.01

CHANGE IN SNOW STORAGE = -0.01

AVERAGE MONTHLY BASE FLOW

1.6 5.6 9.3 450.0 1023.0 1890.0 1736.0 133.3 138.0 558.0 810.0 651.0

LEAP YEAR INDICATOR = 0 YES=1 & NO=0

ITHAW IFREZ
 104 298

YEAR
 57

RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE

JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1957

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.02	0.40	3.00	3.27	6.69	8.06	1.33	3.21	1.77	1.43	0.68	0.01	29.89
CALCULATED TOTAL RUNOFF	42.	37.	189.	2452.	8604.	24412.	5801.	4180.	4051.	2365.	1430.	1084.	54410.
CSERVED TOTAL RUNOFF	2.	13.	105.	2253.	13469.	31743.	6602.	3589.	4673.	657.	833.	665.	64804.
CALCULATED SURFACE RUNOFF	0.	9.	157.	2276.	8208.	23971.	3699.	2224.	2584.	251.	63.	1.	43444.
CSERVED SURFACE RUNOFF	1.	8.	95.	1803.	12446.	29853.	4866.	3456.	4735.	99.	23.	14.	57398.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	42.	28.	32.	176.	395.	441.	2101.	1956.	1468.	1817.	1426.	1093.	10967.
CSERVED BASEFLOW	2.	6.	9.	450.	1023.	1890.	1736.	133.	138.	558.	810.	651.	7406.
ETP	0.293	1.324	1.883	3.759	5.002	6.050	6.782	5.756	4.560	2.997	1.304	1.228	40.938
UETA	0.031	0.033	0.392	1.316	2.286	2.894	2.452	1.778	1.476	0.880	0.254	0.052	13.874
LETA	0.0	0.0	0.0	0.132	1.136	1.558	1.323	1.021	0.797	0.414	0.0	0.0	6.399
ETA	0.135	0.117	0.740	1.501	3.442	4.453	3.772	2.799	2.273	1.294	0.368	0.082	20.975
PES-COLATION	0.0	0.0	0.059	1.542	2.783	3.144	0.375	0.113	0.299	0.027	0.024	0.009	8.347
UTS	2.265	2.290	2.463	4.343	4.352	4.306	3.744	2.950	3.806	5.674	3.807	3.974	3.509
LZSA	7.800	7.800	7.802	9.122	10.178	11.614	12.108	11.027	10.380	9.889	9.728	9.748	9.778
LZSI	7.800	7.800	7.802	9.122	10.178	11.614	12.108	11.027	10.380	9.889	9.728	9.748	9.778
GWS	2.006	2.004	2.003	2.012	2.074	2.289	2.463	2.374	2.352	2.281	2.203	2.154	2.166
TEMP.	21.2	37.0	38.2	48.3	58.7	68.7	79.9	77.6	63.9	53.8	37.7	37.8	52.0
CORRELATION COEFFICIENTS	0.583	0.685	0.730	0.710	0.879	0.879	0.879	0.647	0.848	0.954	0.985	0.976	0.748

DELTA STORAGE = 6.962 INCHES ARIA = 3.367 POND STORAGE = 0.0												
TOTAL CHANGE = 2.994												
SUM CAL TOTAL = 480279. SUM OBS TOTAL = 412314. SUM CAL SRINT = 271245. SUM OBS SR = 377313. SUM CAL BF = 209031. SUM OBS BF = 84996.												
PACK ON DECEMBER 31 = 0.04 CHANGE IN SNOW STORAGE = 0.05												
AVERAGE MONTHLY BASE FLOW 806.0 616.0 1519.0 2700.0 2046.0 720.0 1240.0 1054.0 660.0 496.0 780.0 868.0												
LEAP YEAR INDICATOR = 0 YES=1 NO=0												
ITHAN IFREZ 115 274												
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE												
JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
0.0	0.0	0.0	0.300	1.163	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.463

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1959

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.38	0.30	1.69	4.23	4.39	2.61	6.79	2.33	1.18	0.12	0.79	0.47	25.35
CALCULATED TOTAL RUNOFF	856.	621.	1164.	6209.	10123.	9455.	17292.	13784.	5534.	3465.	2474.	1915.	72892.
OBSERVED TOTAL RUNOFF	825.	644.	1860.	3473.	4184.	2406.	8396.	7232.	2369.	508.	825.	970.	33745.
CALCULATED SURFACE RUNOFF	64.	97.	735.	4769.	4107.	1562.	10775.	7943.	992.	5.	15.	47.	31113.
OBSERVED SURFACE RUNOFF	19.	28.	341.	773.	2138.	1688.	7156.	6179.	1709.	112.	45.	52.	20240.
CALCULATED INTER-FLOW	0.	0.	0.	48.	361.	49.	1.	0.	0.	0.	0.	0.	459.
CALCULATED BASEFLOW	792.	524.	429.	1392.	5655.	7843.	6516.	5841.	4542.	3459.	2459.	1868.	41320.
OBSERVED BASEFLOW	806.	616.	1519.	2700.	2046.	720.	1240.	1054.	660.	495.	783.	868.	13505.
ETP	0.736	0.710	0.0	3.228	5.369	6.213	6.334	5.547	4.882	3.099	1.281	0.849	38.407
UETA	0.040	0.111	0.0	1.143	2.292	2.435	2.694	2.177	1.580	0.497	0.100	0.115	13.123
LETA	0.0	0.0	0.0	0.011	0.921	1.311	1.450	1.172	0.861	0.016	0.0	0.0	5.743
ETA	0.174	0.221	0.742	1.434	3.213	3.746	4.144	3.350	2.440	0.513	0.243	0.158	20.378
PER-CORRELATION	0.056	0.181	1.258	3.031	1.472	0.145	1.953	0.746	0.106	0.0	0.0	0.0	9.008
UZS	3.986	4.158	4.249	4.297	4.165	3.671	4.138	4.004	3.445	2.563	2.559	3.138	3.705
LZSA	9.752	9.832	10.114	13.837	13.891	12.783	12.417	12.534	11.343	11.550	11.550	11.550	11.821
LZST	9.752	9.832	10.114	14.022	14.819	14.246	13.881	13.993	13.404	13.013	13.013	13.013	12.771
GWS	2.112	2.083	2.063	2.281	2.941	3.151	2.931	2.834	2.697	2.491	2.301	2.265	2.517
TEMP.	31.9	28.9	25.7	48.0	64.0	70.9	73.7	75.9	69.1	56.3	40.6	31.1	51.4
CORRELATION COEFFICIENTS	0.870	0.910	0.628	0.582	0.783	0.645	0.568	0.390	0.573	0.584	0.966	0.916	0.693

DELTA STORAGE = 2.367 INCHES												
AAIA = 2.470												
POND STORAGE = 0.0												
TOTAL CHANGE = -0.103												
SUM CAL TOTAL = 553171.												
SUM OBS TOTAL = 446039.												
SUM CAL SRINT = 302320.												
SUM OBS SR = 347558.												
SUM CAL BF = 250351.												
SUM OBS BF = 98501.												
PACK ON DECEMBER 31 = -0.00												
CHANGE IN SNOW STORAGE = -0.05												
AVERAGE MONTHLY BASE FLOW												
558.01260.01209.01350.0 930.0 450.0 62.0 12.4 6.0 589.0 720.0 868.0												
LEAP YEAR INDICATOR = 0 YES=1 NO=0												
ITHAW IFREZ	YEAR											
112 284	59											
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE												
JAN. 0.0	FEB. 0.0	MAR. 0.0	APR. 0.0	MAY. 0.0	JUN. 0.0	JUL. 0.0	AUG. 0.0	SEP. 0.0	OCT. 0.0	NOV. 0.0	DEC. 0.0	TOTAL 0.0

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1957

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.39	0.65	2.62	1.19	2.35	2.82	3.20	3.71	3.75	3.19	0.05	0.21	24.13
CALCULATED TOTAL RUNOFF	1377.	1010.	1292.	923.	1463.	3536.	2353.	3013.	2736.	2603.	668.	456.	21728.
OBSERVED TOTAL RUNOFF	569.	1354.	1509.	1387.	1184.	1619.	263.	325.	202.	2175.	771.	876.	12233.
CALCULATED SURFACE RUNOFF	11.	155.	619.	364.	1047.	3163.	1946.	2654.	2303.	2225.	123.	24.	14632.
OBSERVED SURFACE RUNOFF	11.	94.	300.	37.	254.	1169.	201.	313.	196.	1585.	51.	8.	4213.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	1366.	856.	673.	559.	415.	475.	407.	360.	433.	576.	545.	432.	7096.
OBSERVED BASEFLOW	558.	1260.	1209.	1350.	930.	450.	62.	12.	6.	589.	720.	868.	8014.
ETP	0.470	0.827	2.758	3.999	5.231	6.517	6.426	5.875	4.551	2.820	1.406	1.157	42.037
UETA	0.076	0.135	0.723	1.399	1.814	2.365	2.107	2.082	1.595	1.076	0.283	0.220	13.874
LETA	0.0	0.0	0.0	0.020	0.829	1.367	1.178	1.152	3.866	0.266	0.0	0.0	5.708
ETA	0.210	0.252	0.723	1.429	2.643	3.732	3.304	3.234	2.461	1.342	0.283	0.220	12.833
PER-COLATION	0.0	0.043	0.747	0.052	0.303	0.688	0.108	0.391	0.810	1.754	0.002	0.0	4.899
UZS	3.199	3.502	3.847	3.951	3.734	3.393	3.015	3.534	3.654	4.147	4.236	4.092	3.692
L25A	11.550	11.563	11.791	12.367	12.234	11.744	10.554	9.688	8.999	10.526	10.740	10.740	11.038
L25I	13.013	13.026	13.255	13.830	13.698	13.208	12.018	11.152	10.463	11.989	12.204	12.204	12.501
GWS	2.194	2.145	2.111	2.087	2.071	2.090	2.080	2.088	2.082	2.104	2.083	2.061	2.099
TEMP.	25.8	29.1	39.7	50.3	62.0	75.0	75.0	79.4	63.7	50.3	36.0	35.0	51.9
CORRELATION COEFFICIENTS	0.763	0.522	0.843	0.824	0.666	0.615	0.374	0.761	0.794	0.971	0.743	0.743	

DELTA STORAGE = 3.522 INCHES
 ARIA = 3.748
 POND STORAGE = 0.0

TOTAL CHANGE = -0.226

SUM CAL TOTAL = 574899.
 SUM OBS TOTAL = 458292.
 SUM CAL SRINT = 317452.
 SUM OBS SR = 351776.
 SUM CAL BF = 257447.
 SUM OBS BF = 106515.

PACK ON DECEMBER 31 = 0.0 CHANGE IN SNOW STORAGE = 0.00

AVERAGE MONTHLY BASE FLOW
 589.01508.02170.03300.02697.01710.0 558.0 68.2 63.0 161.2 480.0 713.0

LEAP YEAR INDICATOR = 1 YES-1 NO=0

ITHAW IFREZ
 113 297

YEAR
 60

RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE

JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
0.0	0.0	0.0	0.325	1.205	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.530

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1960

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.57	1.66	2.20	2.01	4.23	3.99	1.04	3.15	1.46	1.86	0.15	0.63	22.95
CALCULATED TOTAL RUNOFF	410.	920.	1147.	4605.	18085.	13985.	7338.	7313.	3640.	3027.	2190.	1707.	64369.
OBSERVED TOTAL RUNOFF	615.	1843.	9734.	3728.	10007.	4943.	622.	1741.	294.	245.	503.	719.	34993.
CALCULATED SURFACE RUNOFF	95.	676.	767.	3176.	7967.	4468.	642.	2403.	614.	402.	34.	69.	21312.
OBSERVED SURFACE RUNOFF	26.	335.	7564.	428.	7310.	3233.	54.	1672.	231.	84.	23.	6.	20976.
CALCULATED INTER-FLOW	0.	0.	144.	1129.	2204.	1073.	53.	0.	0.	0.	0.	0.	4504.
CALCULATED BASEFLOW	315.	244.	236.	300.	7914.	8444.	6643.	4911.	3026.	2625.	2157.	1638.	38453.
OBSERVED BASEFLOW	589.	1508.	2170.	3300.	2697.	1710.	558.	68.	53.	161.	480.	713.	14017.
ETP	0.415	0.171	0.582	4.244	5.105	6.148	6.457	5.690	4.833	3.128	1.685	0.545	39.002
UETA	0.129	0.041	0.105	1.498	2.276	2.719	1.961	1.590	1.159	0.654	0.305	0.124	12.560
LETA	0.0	0.0	0.0	0.032	1.000	1.464	1.165	1.081	0.755	0.370	0.0	0.0	5.867
EIA	0.236	0.302	0.791	1.530	3.276	4.182	3.126	2.670	1.914	1.024	0.305	0.298	19.644
PER-COLATION	0.054	1.516	1.672	0.478	1.722	0.837	0.035	0.111	0.054	0.103	0.000	0.057	6.639
UZS	4.138	4.525	4.537	4.020	4.265	3.984	2.992	2.934	2.921	3.291	3.641	3.703	3.743
LZSA	10.767	11.985	12.764	14.062	14.012	13.349	12.413	11.304	10.529	9.986	9.925	9.937	11.749
LZST	12.230	13.448	14.228	15.805	16.594	16.045	15.080	13.970	13.195	12.652	12.591	12.603	14.036
GWS	2.045	2.035	2.027	2.345	3.240	3.241	2.943	2.698	2.534	2.419	2.316	2.233	2.508
TEMP.	24.4	21.4	31.0	54.1	60.2	70.0	75.4	76.5	68.3	56.6	40.9	30.0	50.8
CORRELATION COEFFICIENTS	0.599	0.597	0.690	0.642	0.525	0.531	0.915	0.419	0.564	0.658	0.903	0.886	0.661

DELTA STORAGE = 1.007 INCHES												
AAIA = 2.907												
POND STORAGE = 0.0												
TOTAL CHANGE = -1.900												
SUM CAL TOTAL = 639268.												
SUM OBS TOTAL = 493285.												
SUM CAL SRINI = 343368.												
SUM OBS SR = 372752.												
SUM CAL BF = 295899.												
SUM OBS BF = 120533.												
PACK ON DECEMBER 31 = 0.10												
CHANGE IN SNOW STORAGE = 0.10												
AVERAGE MONTHLY BASE FLOW												
775.0 980.01054.01110.01674.02130.0 713.0 496.0 450.0 744.01140.01023.0												
LEAP YEAR INDICATOR=0 YES=1 & NO=0												
ITHAW IFREZ												
111 292												
YEAR 61												
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE												
JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
0.0	0.0	0.0	0.0	0.0	0.726	0.0	0.0	0.0	0.0	0.0	0.0	0.726

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1961

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.11	0.13	2.17	1.48	6.70	5.18	3.06	4.42	2.14	0.76	1.94	0.26	28.35
CALCULATED TOTAL RUNOFF	1199.	809.	1501.	1647.	8265.	16537.	7918.	10359.	4000.	2873.	3253.	1734.	60095.
OBSERVED TOTAL RUNOFF	792.	1001.	1145.	1385.	5954.	11571.	2110.	5168.	863.	795.	1207.	1047.	33038.
CALCULATED SURFACE RUNOFF	1.	7.	928.	1133.	7675.	9364.	2035.	6147.	1366.	224.	1498.	20.	30398.
OBSERVED SURFACE RUNOFF	17.	21.	91.	275.	4280.	9441.	1397.	4672.	413.	51.	67.	24.	20749.
CALCULATED INTER-FLOW	0.	0.	0.	0.	109.	2141.	578.	1.	0.	0.	0.	0.	2828.
CALCULATED BASEFLOW	1197.	802.	573.	514.	481.	5033.	5305.	4211.	2635.	2649.	1756.	1714.	26870.
OBSERVED BASEFLOW	775.	980.	1054.	1110.	1674.	2130.	713.	496.	450.	744.	1140.	1023.	12289.
ETP	1.018	1.367	2.820	2.996	4.979	6.208	6.560	5.584	4.435	2.988	1.359	0.355	40.669
UETA	0.029	0.069	0.799	1.018	2.298	2.759	2.268	2.078	1.331	0.771	0.377	0.063	13.860
LETA	0.0	0.0	0.0	0.037	1.039	1.485	1.248	1.132	0.722	0.301	0.0	0.0	5.965
ETA	0.029	0.101	0.799	1.388	3.337	4.244	3.516	3.210	2.053	1.072	0.447	0.222	20.419
PER-CORRELATION	0.001	0.009	0.707	0.454	2.850	2.687	0.376	0.757	0.317	0.046	0.857	0.018	9.079
UZS	3.928	3.914	3.984	4.038	4.290	4.132	3.978	3.603	3.777	3.670	3.874	4.038	3.859
LZSA	9.982	9.988	10.423	10.951	12.140	13.792	12.883	12.283	11.943	11.559	11.933	12.355	11.695
LZST	12.649	12.654	13.089	13.617	14.807	16.880	15.908	15.298	14.959	14.575	14.948	15.371	14.573
GWS	2.170	2.126	2.100	2.084	2.116	2.813	2.754	2.601	2.504	2.400	2.311	2.243	2.353
TEMP.	30.2	35.7	40.9	46.3	58.4	70.8	76.8	74.9	61.8	53.8	36.2	24.9	51.0
CORRELATION COEFFICIENTS	0.894	0.717	0.498	0.805	0.654	0.686	0.549	0.708	0.869	0.598	0.891	0.730	

[illegible]

DAILY FLOW DURATION AND ERROR TABLE

FLOW INTERVAL	ACT. CASES	PCT.	CALC. CASES	PCT.	AVE. ERROR	AV. ABS. ERROR	STD. ERROR
0.0-	910.0	100.000	21.0	100.000	25.5	25.50	33.57
1.0-	164.0	81.545	120.0	99.574	34.1	34.11	48.61
1.8-	146.0	78.219	162.0	97.141	44.3	44.40	52.58
3.2-	163.0	75.259	280.0	93.855	58.5	59.00	67.92
5.6-	308.0	71.953	429.0	88.177	32.0	34.12	51.16
10.0-	418.0	65.707	486.0	79.477	31.9	37.05	51.98
17.6-	944.0	57.230	732.0	69.621	33.0	42.35	69.30
31.6-	777.0	38.086	687.0	54.776	40.6	62.45	36.11
56.2-	487.0	22.328	648.0	40.844	165.3	184.99	220.83
100.0-	302.0	12.452	517.0	27.702	138.6	186.15	275.89
177.6-	112.0	6.327	349.0	17.218	236.7	327.70	411.33
316.2-	77.0	4.056	245.0	10.140	352.6	468.15	573.83
562.3-	47.0	2.494	135.0	5.171	324.1	684.93	829.85
1000.0-	33.0	1.541	82.0	2.434	118.0	941.08	1358.99
1778.3-	20.0	0.872	25.0	0.771	-873.4	1578.16	1977.46
3162.3-	11.0	0.466	9.0	0.264	-2552.8	2552.82	705.84
5623.4-	5.0	0.243	4.0	0.081	-4276.1	4276.09	580.90
10000.0-	6.0	0.142	0.0	0.0	-7642.9	7642.91	4218.50
17782.7-	0.0	0.020	0.0	0.0			
31622.7-	1.0	0.020	0.0	0.0	-30667.4		
56234.0-	0.0	0.0	0.0	0.0			
99999.8-	0.0	0.0	0.0	0.0			
177827.4-	0.0	0.0	0.0	0.0			
316226.5-	0.0	0.0	0.0	0.0			
4931.0			4931.0		160808.9	597691.94	11624.63

DELTA STORAGE = 40.303 INCHES
 AATA = 44.753
 POND STORAGE = 0.0

TOTAL CHANGE = -4.449

TOTAL PRECIPITATION = 318.839

TOTAL IA 44.753
 TOTAL SURFACE RUNOFF 16.715
 TOTAL UETA 177.301
 TOTAL PERC 78.450
 CHANGE IN UZSM 1.205

CHECK BALANCE 318.425

RESULTS - MODEL B-TEN

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.....K$U..REMOTE...COMPUTING...LABORATORY...SEATON.....JOB 393.....1 APR 77..RCLQ6598...ROGERS...START.....
.....K$U..REMOTE...COMPUTING...LABORATORY...SEATON.....JOB 398.....1 APR 77..RCLQ6598...ROGERS...START.....
.....K$U..REMOTE...COMPUTING...LABORATORY...SEATON.....JOB 398.....1 APR 77..RCLQ6598...ROGERS...START.....
.....K$U..REMOTE...COMPUTING...LABORATORY...SEATON.....JOB 398.....1 APR 77..RCLQ6598...ROGERS...START.....
.....K$U..REMOTE...COMPUTING...LABORATORY...SEATON.....JOB 398.....1 APR 77..RCLQ6598...ROGERS...START.....
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COMPUTING MADE FUN
COMPUTER-GAME DAY
APRIL 2

APRIL 2

THE GENERAL PUBLIC IS INVITED TO PLAY A VARIETY OF GAMES (STAR TREK, KINGDOM, ETC.) APRIL 2, 9:00 A.M. TO 3:00 P.M., IN FAIRCHILD 117 (MINI-LAB). THIS EVENT IS SPONSORED BY THE STUDENT CHAPTER OF ACM IN CONJUNCTION WITH THE COMPUTER SCIENCE DEPARTMENT AS A PART OF THE UNIVERSITY OPEN HOUSE.

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1948

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.04	0.58	1.92	0.48	3.60	5.60	2.00	4.14	0.98	0.64	1.13	0.53	21.64
CALCULATED TOTAL RUNOFF	0.	8.	332.	56.	2434.	7244.	2265.	6082.	1349.	895.	1092.	505.	23151.
OBSERVED TOTAL RUNOFF	21.	423.	1409.	390.	2101.	13268.	2454.	3513.	40.	5.	131.	338.	24114.
CALCULATED SURFACE RUNOFF	0.	8.	292.	56.	2337.	6945.	1742.	6438.	464.	143.	546.	46.	19023.
OBSERVED SURFACE RUNOFF	2.	351.	882.	93.	2042.	12413.	1214.	3110.	28.	1.	11.	28.	20177.
CALCULATED INTERFLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	0.	0.	40.	0.	57.	298.	523.	544.	885.	745.	535.	460.	4129.
OBSERVED BASEFLOW	19.	73.	527.	300.	59.	870.	1240.	403.	12.	5.	120.	310.	3937.
ETP	0.887	0.776	1.337	4.549	5.315	6.210	6.537	5.709	5.012	3.045	1.100	0.703	41.194
UETA	0.168	0.111	0.380	1.267	1.834	2.800	2.278	2.320	1.415	0.737	0.245	0.108	13.662
LETA	0.0	0.0	0.0	0.0	0.520	1.508	1.227	1.249	0.720	0.0	0.0	0.0	5.224
ETA	0.179	0.292	0.731	1.267	2.354	4.308	3.505	3.569	2.135	0.737	0.442	0.220	19.741
PER-CORRELATION	0.0	0.0	0.254	0.0	0.532	1.666	0.091	1.016	0.066	0.0	0.0	0.002	3.627
UZS	2.880	2.970	3.709	3.801	3.618	4.166	3.598	4.195	3.635	2.974	3.137	3.871	3.574
LZSA	9.400	9.400	9.456	9.654	9.557	9.471	9.195	8.666	8.065	7.900	7.800	7.802	8.857
LZST	9.410	9.400	9.496	9.654	9.557	9.471	9.195	8.666	8.065	7.800	7.800	7.802	8.857
GWS	2.070	2.000	2.000	1.999	2.003	2.063	2.104	2.152	2.149	2.111	2.095	2.065	2.061
TEMP.	29.5	30.0	33.8	58.8	63.2	70.9	76.5	76.8	71.2	55.0	37.7	30.5	52.8
CORRELATION COEFFICIENTS	1.000	0.640	0.552	0.418	0.807	0.605	0.470	0.607	0.818	0.591	0.294	0.917	0.645

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1949

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.34	1.32	1.65	3.45	5.16	6.90	2.95	3.62	0.42	2.19	0.09	0.13	28.20
CALCULATED TOTAL RUNOFF	412.	738.	700.	1376.	5920.	8605.	3395.	2900.	1285.	3709.	825.	624.	30489.
OBSERVED TOTAL RUNOFF	37.	6127.	2325.	1554.	3496.	12838.	1929.	809.	97.	504.	569.	521.	30807.
CALCULATED SURFACE RUNOFF	76.	485.	489.	1161.	5597.	8121.	2842.	2170.	398.	2932.	16.	10.	24298.
OBSERVED SURFACE RUNOFF	3.	5035.	310.	294.	1388.	5838.	1278.	635.	58.	269.	-1.	25.	19132.
CALCULATED INTERFLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	336.	252.	211.	215.	323.	495.	553.	730.	887.	777.	809.	614.	6191.
OBSERVED BASEFLOW	34.	1092.	2015.	1260.	2108.	3000.	651.	174.	39.	236.	570.	496.	11674.
ETP	0.0	0.342	2.677	3.584	5.333	6.288	6.642	5.547	4.588	3.011	1.903	1.017	40.933
UETA	0.0	0.089	0.804	1.476	2.481	2.856	2.271	2.105	1.348	0.940	0.244	0.110	14.724
LETA	0.0	0.0	0.0	0.126	1.218	1.538	1.223	1.133	0.726	0.416	0.0	0.0	6.380
ETA	0.139	0.437	0.835	1.833	2.700	4.394	3.495	3.239	2.073	1.356	0.244	0.110	21.853
PER-CORRELATION	0.004	0.503	0.545	1.370	2.280	3.283	0.313	0.685	0.000	0.240	0.0	0.0	9.622
UZS	4.117	4.380	4.317	4.405	4.370	4.205	3.779	3.834	3.543	3.788	3.634	3.550	3.991
LZSA	7.805	8.085	8.807	10.157	11.310	13.224	12.894	12.017	11.526	11.094	11.039	11.039	10.763
LZST	7.805	8.085	8.807	10.157	11.310	13.227	12.889	12.022	11.531	11.099	11.044	11.044	10.766
GWS	2.048	2.035	2.026	2.020	2.051	2.147	2.180	2.166	2.151	2.144	2.119	2.087	2.098
TEMP.	18.3	29.9	39.5	51.9	63.5	71.9	78.0	74.3	64.3	54.2	47.3	32.4	52.2
CORRELATION COEFFICIENTS	0.538	0.702	0.649	0.536	0.672	0.498	0.745	0.691	0.525	0.659	0.969	0.982	0.685

DELTA STORAGE = 5.255 INCHES
AAIA = 3.088
PCND STORAGE = 0.0

TOTAL CHANGE = 2.166

SUM CAL TOTAL	=	53640.
SUM OBS TOTAL	=	54920.
SUM CAL SPRINT	=	43321.
SUM OBS SR	=	39309.
SUM CAL RF	=	10320.
SUM OBS BF	=	15611.

PACK CN DECEMBER 31 = 0.0 CHANGE IN SNTH STORAGE = -0.39

AVERAGE MONTHLY BASE FLOW	
372.01C08.01023.0	630.0465.0 105.01395.03410.01530.0 744.0 690.0 713.0

LEAP YEAR INDICATOR= 0 YES=1 & NO=0

ITHAW IPREZ
120 306

YEAR
50

RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE

[illegible]

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1950

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.13	1.29	0.63	1.25	3.12	1.83	7.43	6.76	0.44	0.61	0.08	0.03	23.59
CALCULATED TOTAL PUNCFF	456.	539.	448.	503.	1766.	1637.	30649.	21063.	3700.	2645.	1949.	1477.	66828.2 ³⁸⁷
OBSERVED TOTAL RUNOFF	371.	1027.	1041.	721.	599.	449.	21895.	31911.	2063.	952.	710.	725.	62374.
CALCULATED SURFACE RUNOFF	7.	239.	195.	306.	1529.	1421.	30333.	17855.	238.	272.	5.	0.	52400.
OBSERVED SURFACE RUNOFF	-1.	19.	18.	121.	134.	344.	20410.	26501.	533.	208.	20.	12.	50319.
CALCULATED INTER- FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	449.	300.	253.	197.	237.	216.	315.	3205.	3462.	2372.	1944.	1477.	14429.
OBSERVED BASEFLOW	372.	1008.	1023.	600.	465.	105.	1395.	3410.	1530.	744.	690.	713.	12355.
ETP	6.795	1.558	2.302	3.978	5.046	6.390	6.258	5.308	4.622	3.284	1.589	1.099	42.130
UETA	0.025	0.275	0.652	1.282	1.929	2.317	2.492	2.413	1.397	0.714	0.200	0.063	13.758
LETA	0.0	0.0	0.0	0.0	0.632	1.301	1.364	1.299	0.753	0.401	0.014	0.0	5.765
ETA	0.041	0.275	0.778	1.282	2.561	3.619	3.856	3.713	2.159	1.115	0.214	0.063	19.668
PER- COLATION	0.0	0.082	0.057	0.085	0.289	0.003	2.183	2.764	0.0	0.0	0.0	0.0	5.468
UZS	3.525	3.584	4.207	2.591	3.936	3.539	3.965	4.272	3.675	3.282	2.870	2.702	3.670
LZSA	11.039	11.066	11.144	11.225	11.098	10.266	9.678	11.479	11.465	10.925	10.743	10.742	10.907
LZST	11.044	11.071	11.149	11.230	11.103	10.271	9.683	11.434	11.500	10.930	10.748	10.748	10.912
GWS	2.064	2.048	2.036	2.026	2.021	2.021	2.114	2.556	2.508	2.387	2.285	2.210	2.191
TEMP.	27.3	36.8	38.2	48.4	50.3	73.3	72.7	70.6	64.9	59.9	38.9	34.5	52.1
CORRELATION CCEFF- FICIENTS	0.992	0.653	0.611	0.606	0.518	0.442	0.587	0.559	0.887	0.774	0.935	0.716	0.691

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1951

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	9.32	1.01	0.77	2.58	6.00	5.56	7.51	2.75	3.42	0.77	0.20	0.10	34.99
CALCULATED TOTAL RUNOFF	1090.	795.	849.	1829.	18418.	23391.	60144.	41292.	30551.	20434.	14286.	10926.	229105.
OBSERVED TOTAL RUNOFF	892.	576.	1249.	1503.	17401.	53000.	79382.	9426.	11537.	2494.	2386.	1452.	181698.
CALCULATED SURFACE RUNOFF	11.	85.	280.	1438.	17734.	20820.	23464.	3325.	3144.	155.	4.	2.	70460.
OBSERVED SURFACE RUNOFF	24.	24.	9.	333.	15789.	49200.	72562.	6016.	8777.	200.	136.	367.	152437.
CALCULATED INTER-FLW	0.	0.	0.	0.	0.	450.	3570.	3307.	2324.	1140.	770.	585.	12195.
CALCULATED BASEFLW	1080.	711.	569.	391.	684.	7081.	33110.	34661.	25083.	19139.	13613.	10339.	146459.
OBSERVED BASEFLW	868.	952.	1243.	1170.	1612.	4800.	6820.	3413.	2760.	2294.	2250.	1085.	29261.
ETP	0.408	1.192	2.453	3.869	5.235	5.774	6.353	5.626	4.494	2.938	1.491	0.633	47.462
UETA	0.025	0.176	0.441	1.237	2.056	2.888	2.729	2.155	1.801	0.848	0.254	0.037	14.667
LETA	0.0	0.0	0.0	0.0	0.654	1.555	1.470	1.160	0.970	0.196	0.0	0.0	6.005
ETA	0.227	0.278	0.492	1.237	2.710	4.443	4.109	3.315	2.771	1.044	0.276	0.125	21.117
PER-CCLATION	0.0	0.0	0.0	0.653	2.162	4.588	3.669	0.602	0.977	0.0	0.0	0.0	12.692
U25	2.673	3.075	3.458	3.928	4.025	4.445	4.297	3.966	4.043	3.313	3.232	3.107	3.649
L25A	10.742	10.742	10.742	11.059	12.046	13.671	12.582	11.579	11.506	11.066	11.040	11.040	11.487
L25T	10.748	10.748	10.748	11.064	12.051	14.513	17.291	17.255	16.809	16.165	16.048	15.982	14.141
G25	2.153	2.114	2.087	2.069	2.146	3.261	6.841	6.923	5.662	4.717	3.997	3.468	3.892
TEMP.	27.3	35.4	36.1	48.3	62.1	64.9	74.0	75.6	62.8	52.6	37.5	27.5	50.4
CORRELATION COEFFICIENTS	0.684	0.779	0.703	0.635	0.681	0.501	0.529	0.538	0.974	0.954	0.835	0.719	

[illegible]

Case	Year	Age	Sex	Occupation	Education	Income	Health	Family	Community	Environment	Policy	Outcome
550.01595.01550.02400.02325.0	330.0	55.8	34.1	0.0	1.6	45.0	155.0					

LEAP YEAR INDICATOR= 1 YES=1 & NO=0

ITIAW	IFREZ
132	280

YEAR 52

RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE

[illegible]

SUMMARY TABLE - SOUTH FORK SCLOWEN RIVER BASIN - 1952

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.09	0.22	1.76	3.10	2.76	0.37	2.59	2.92	0.75	0.04	0.08	0.92	15.63
CALCULATED TOTAL RUNOFF	7987.	5517.	4803.	2774.	5801.	2955.	2877.	2176.	1753.	1228.	873.	775.	39518.
OBSERVED TOTAL RUNOFF	1860.	1885.	3100.	4200.	4656.	488.	110.	117.	28.	2.	50.	255.	16751.
CALCULATED SURFACE RUNOFF	0.	2.	343.	721.	2981.	235.	849.	858.	341.	0.	0.	112.	6441.
OBSERVED SURFACE RUNOFF	310.	290.	1550.	1800.	2331.	158.	54.	83.	28.	0.	5.	103.	6710.
CALCULATED INTER-FLOW	428.	295.	333.	1155.	2100.	589.	0.	0.	0.	0.	0.	0.	4900.
CALCULATED BASEFLOW	7559.	5220.	4124.	898.	721.	2131.	2029.	1318.	1412.	1228.	873.	553.	23177.
OBSERVED BASEFLOW	1550.	1595.	1550.	2400.	2325.	330.	56.	34.	0.	2.	45.	155.	10041.
ETP	0.516	1.537	0.804	3.630	5.155	6.844	6.458	5.754	4.887	2.948	1.402	0.134	43.468
UETA	0.032	0.120	0.177	1.271	2.164	2.198	1.391	1.458	1.110	0.250	0.044	0.027	13.242
LETA	0.0	0.0	0.0	0.0	0.308	1.331	1.151	1.072	0.694	0.069	0.0	0.0	4.624
ETA	0.081	0.142	0.842	1.402	2.472	3.529	2.542	2.530	1.804	0.319	0.059	0.344	16.065
PER-CORRELATION	0.0	0.0	0.442	0.874	0.482	0.0	0.0	0.000	0.022	0.0	0.0	0.0	1.825
UFS	3.069	3.032	3.677	4.074	4.002	2.920	2.446	2.431	2.760	2.229	2.087	2.603	2.943
LZSA	11.040	11.040	11.113	11.744	12.570	11.857	10.567	9.498	8.613	8.246	8.242	8.242	10.228
LZSI	15.533	15.898	15.544	16.467	16.582	16.016	14.706	13.636	12.752	12.385	12.380	12.380	14.619
GAS	3.073	2.792	2.586	2.477	2.492	2.464	2.358	2.288	2.237	2.174	2.128	2.094	2.429
TEMP.	32.4	36.1	34.1	49.2	60.9	79.5	87.6	77.5	66.1	52.9	36.9	20.6	53.9
CORRELATION COEFFICIENTS	0.994	0.992	0.992	0.609	0.657	0.596	0.448	0.275	0.543	0.322	0.470	0.653	0.628

DELTA STORAGE	=	-1.882	INCHES
AAIA	=	3.510	
PEND STORAGE	=	0.0	

TOTAL CHANGE = -5.393

SUM CAL	TCIAL	=	389091.
SUM OBS	TCIAL	=	315744.
SUM CAL	SRINT	=	185707.
SUM OBS	SR	=	248776.
SUM CAL	RF	=	199384.
SUM OBS	BF	=	66568.

PACK ON DECEMBER 31 = 0.50 CHANGE IN SNOW STORAGE = 0.50

AVERAGE MONTHLY BASE FLOW			
372.0	588.0	930.0	810.0
527.0	6.0	99.2	89.5
3.0	4.7	156.0	310.0

LEAP YEAR INDICATOR= 0 YES=1 & NE=0

ITHAW IFREZ
134 303

YEAR
53

RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE

[illegible]

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1953

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.37	0.21	1.63	2.29	2.50	2.61	3.43	3.43	0.44	1.33	1.99	1.13	21.37
CALCULATED TOTAL RUNOFF	520.	349.	803.	864.	1615.	2021.	3574.	4740.	825.	920.	515.	630.	17775.
OBSERVED TOTAL RUNOFF	771.	673.	1125.	959.	635.	317.	2267.	1315.	7.	5.	152.	351.	9627.
CALCULATED SURFACE RUNOFF	35.	24.	523.	634.	1370.	1793.	3649.	4275.	304.	497.	183.	366.	13655.
OBSERVED SURFACE RUNOFF	399.	85.	195.	189.	108.	311.	2167.	1225.	4.	0.	6.	41.	4731.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	485.	325.	281.	229.	245.	228.	325.	464.	521.	422.	332.	264.	4121.
OBSERVED BASEFLOW	372.	583.	930.	910.	527.	6.	59.	60.	3.	5.	156.	319.	3896.
ETP	0.931	1.509	2.535	3.822	5.092	6.667	6.564	5.590	4.906	3.239	1.267	0.118	42.259
UETA	0.020	0.136	0.453	1.150	1.818	2.478	2.047	2.143	1.189	0.664	0.321	0.051	12.470
LETA	0.0	0.0	0.0	0.0	0.199	1.220	0.791	0.781	0.165	0.076	0.0	0.0	3.231
ETA	0.150	0.136	0.653	1.150	2.017	3.699	2.837	2.925	1.354	0.739	0.539	0.393	15.562
PER-COLLATION	0.008	0.035	0.260	0.182	0.256	0.218	0.696	0.683	0.040	0.002	0.304	0.775	3.463
UZS	3.033	3.058	3.193	3.693	3.912	3.413	3.696	3.984	3.211	2.822	4.043	4.479	3.550
LZSA	8.245	8.259	8.452	8.608	8.805	8.326	7.844	7.931	7.810	7.800	7.906	8.571	8.210
L7SI	12.333	12.397	12.591	12.746	12.943	12.459	11.623	11.799	10.595	10.096	10.018	10.682	11.648
GWS	2.069	2.051	2.039	2.030	2.024	2.025	2.045	2.093	2.083	2.053	2.049	2.036	2.051
TEMP.	37.9	36.1	44.0	47.5	60.0	77.1	77.2	75.0	69.4	58.8	41.6	29.8	54.6
CORRELATION COEFFICIENTS	0.643	0.833	0.456	0.501	0.747	0.590	0.530	0.494	0.628	0.465	0.542	0.416	0.566

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1954

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.19	0.53	0.76	0.78	5.60	2.36	1.39	2.67	3.62	1.67	0.02	0.06	16.65
CALCULATED TOTAL RUNOFF	233.	235.	208.	392.	6565.	4867.	1119.	1895.	677.	868.	291.	223.	17574.
OBSERVED TOTAL RUNOFF	380.	1021.	789.	744.	5110.	5516.	48.	134.	0.	6.	18.	23.	13790.
CALCULATED SURFACE RUNOFF	45.	104.	106.	289.	6334.	4365.	425.	1401.	186.	468.	0.	2.	13747.
OBSERVED SURFACE RUNOFF	132.	209.	45.	234.	4025.	4646.	23.	133.	0.	0.	1.	7.	9457.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	187.	131.	102.	103.	231.	502.	684.	494.	491.	380.	291.	221.	3827.
OBSERVED BASEFLOW	248.	812.	144.	510.	1065.	870.	25.	2.	0.	6.	17.	16.	4334.
ETP	0.859	1.865	2.535	4.397	4.904	6.560	6.982	5.837	5.109	2.991	1.819	1.048	44.878
UEIA	0.048	0.348	0.616	1.158	2.159	2.598	1.702	1.701	0.656	0.618	0.085	0.092	11.782
LEIA	0.0	0.0	0.0	0.0	0.618	1.399	1.220	0.731	0.157	0.129	0.0	0.0	4.254
EIA	0.065	0.348	0.616	1.158	2.777	3.968	2.922	2.432	0.812	0.747	0.085	0.115	16.076
PER-CULATION	0.156	0.070	0.041	0.011	1.532	0.484	0.0	0.077	0.0	0.084	0.0	0.0	2.894
UZS	4.175	4.178	4.083	3.748	4.273	3.803	2.474	2.766	2.427	2.840	2.795	2.727	3.353
LZSA	9.060	9.098	9.155	9.188	9.732	10.142	8.976	7.945	7.800	7.903	7.800	7.800	9.705
LZST	11.172	11.209	11.267	11.300	11.843	12.253	11.038	9.960	9.038	8.568	8.501	8.501	10.398
GWS	2.027	2.020	2.014	2.011	2.033	2.111	2.109	2.092	2.074	2.057	2.043	2.031	2.052
TEMP.	28.2	44.9	37.5	56.4	57.3	75.6	62.7	73.3	72.7	53.7	44.8	34.7	55.6
CORRELATION COEFFICIENTS	0.815	0.712	0.709	0.874	0.761	0.479	0.616	0.308	0.293	0.288	0.910	0.678	1.619

DELTA STORAGE = -0.050 INCHES												
AIIA = 2.920												
PCND STORAGE = 0.0												
TOTAL CHANGE = -2.971												
SUM CAL TOTAL = 424440.												
SUM OBS TOTAL = 338162.												
SUM CAL SRIN = 217108.												
SUM OBS SR = 262964.												
SUM CAL BF = 207332.												
SUM OBS BF = 75198.												
PACK ON DECEMBER 31 = 0.23												
CHANGE IN SNOW STORAGE = 0.08												
AVERAGE MONTHLY BASE FLOW												
18.6 148.4 291.4 294.0 9.3 9.0 0.0 0.0 0.0 6.2 9.0 77.5												
LEAF YEAR INDICATOR= 0 YES=1 & NO=0												
ITHA4 IFREZ												
110 258												
YEAR 55												
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE												
JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1955

	JAN.	FEB.	MAR.	APR.	MAY	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.55	0.64	0.48	1.27	2.75	3.75	1.43	1.47	3.83	0.21	0.05	0.22	16.63
CALCULATED TOTAL RUNOFF	152.	127.	127.	528.	1162.	4045.	1426.	1247.	2049.	335.	202.	198.	11645.
OBSERVED TOTAL RUNOFF	32.	325.	512.	427.	74.	686.	1.	5.	2176.	147.	10.	85.	4481.
CALCULATED SURFACE RUNOFF	8.	44.	38.	415.	1040.	3784.	1112.	956.	1794.	58.	2.	47.	9298.
OBSERVED SURFACE RUNOFF	13.	176.	221.	133.	65.	677.	1.	6.	2176.	140.	1.	7.	3617.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	162.	108.	89.	112.	122.	261.	314.	231.	255.	281.	200.	152.	2346.
OBSERVED BASEFLOW	19.	148.	291.	294.	9.	9.	0.	3.	0.	6.	9.	78.	863.
ETP	0.157	0.531	2.353	4.375	5.391	6.028	6.849	5.378	4.870	3.142	1.466	0.490	41.628
UETA	0.016	0.095	0.241	1.151	1.478	2.249	2.078	1.333	0.867	0.802	0.189	0.042	10.492
LETA	0.0	0.0	0.0	0.041	0.540	0.901	0.100	0.300	0.217	0.309	0.0	0.0	2.109
ETA	0.337	0.281	0.340	1.191	2.018	3.150	2.126	1.334	1.084	1.111	0.189	0.190	13.355
PER-CULATION	0.027	0.131	0.057	0.156	0.151	0.867	0.053	0.000	0.527	0.0	0.0	0.0	1.559
UZS	2.700	3.163	3.166	3.053	2.560	3.668	3.057	2.451	2.662	3.700	3.314	3.305	3.130
LZSA	7.801	7.905	7.575	8.129	7.899	7.946	7.800	7.800	7.877	7.866	7.800	7.800	7.882
LZST	8.502	8.606	8.676	8.830	8.515	8.060	7.801	7.800	7.872	7.866	7.600	7.800	8.174
G+S	2.023	2.017	2.013	2.008	2.007	2.031	2.646	2.041	2.035	2.040	2.029	2.022	2.026
TEMP.	27.7	26.8	39.0	56.1	64.3	68.4	62.2	79.4	66.8	55.9	36.8	28.8	53.1
CORRELATION COEFFICIENTS	0.829	0.477	0.932	0.658	0.713	0.826	0.074	0.223	0.940	0.635	0.128	0.784	0.606

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1956

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.16	0.63	0.34	1.00	1.55	1.61	3.00	2.97	0.19	1.06	0.12	0.07	11.71
CALCULATED TOTAL RUNOFF	117.	117.	94.	717.	783.	587.	3240.	1317.	155.	293.	142.	55.	7317.
OBSERVED TOTAL RUNOFF	226.	369.	627.	450.	371.	363.	2306.	155.	0.	0.	0.	0.	4968.
CALCULATED SURFACE RUNOFF	6.	41.	34.	617.	692.	467.	2591.	791.	12.	171.	62.	0.	5974.
OBSERVED SURFACE RUNOFF	9.	133.	38.	120.	222.	360.	2301.	154.	0.	0.	0.	0.	3339.
CALCULATED INTER-FLOW	0.	0.	0.	0.	9.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	111.	76.	60.	100.	91.	120.	260.	226.	143.	122.	80.	55.	1443.
OBSERVED BASEFLOW	217.	235.	589.	330.	149.	3.	5.	2.	0.	0.	0.	0.	1529.
ETP	0.604	0.401	2.604	3.833	5.498	6.768	6.619	5.752	4.945	3.293	1.645	1.111	43.073
UETA	0.022	0.034	0.369	0.972	1.438	1.878	1.880	1.416	0.564	0.438	0.153	0.075	9.210
LETA	0.0	0.0	0.0	0.002	0.282	0.0	0.059	0.020	0.0	0.0	0.0	0.0	0.363
EYA	0.127	0.340	0.448	0.974	1.720	1.878	1.939	1.436	0.564	0.438	0.153	0.075	10.093
PER-CORRELATION	0.0	0.066	0.009	0.209	0.0	0.0	0.059	0.020	0.0	0.0	0.0	0.0	0.363
UTS	3.354	3.740	3.552	3.934	3.083	2.644	3.180	2.959	2.541	2.267	2.486	2.412	3.039
LZSA	7.800	7.816	7.872	8.063	7.920	7.800	7.800	7.800	7.800	7.800	7.800	7.800	7.839
LZST	7.800	7.816	7.872	8.063	7.920	7.800	7.800	7.800	7.800	7.800	7.800	7.800	7.839
GWS	2.016	2.012	2.009	2.009	2.007	2.008	2.028	2.028	2.021	2.015	2.011	2.005	2.014
TEMP.	28.1	29.2	41.9	47.7	65.8	78.5	77.7	77.5	70.1	60.0	39.7	35.7	54.4
CORRELATION COEFFICIENTS	0.756	0.566	0.641	0.435	0.478	0.148	0.560	0.411	1.000	1.000	1.000	0.871	0.665

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1957

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.02	0.44	3.00	3.27	6.69	8.06	1.33	3.21	1.77	1.58	0.76	0.02	30.15
CALCULATED TOTAL RUNOFF	40.	43.	206.	2504.	8604.	24409.	5802.	4180.	4051.	2141.	1531.	1086.	54598.
OBSERVED TOTAL RUNOFF	2.	13.	105.	2253.	13469.	31743.	6602.	3589.	4873.	657.	833.	665.	64804.
CALCULATED SURFACE RUNOFF	0.	16.	175.	2325.	8207.	23968.	3699.	2222.	2582.	322.	102.	1.	43619.
OBSERVED SURFACE RUNOFF	1.	8.	95.	1803.	12446.	29853.	4866.	3456.	4735.	99.	23.	14.	57398.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	40.	27.	31.	178.	397.	442.	2103.	1958.	1469.	1819.	1429.	1085.	10979.
OBSERVED BASEFLOW	2.	6.	9.	450.	1023.	1390.	1736.	133.	138.	558.	810.	651.	7406.
ETP	0.203	1.275	1.883	3.759	5.002	6.050	6.782	5.756	4.560	2.997	1.304	1.228	40.889
UETA	0.033	0.034	0.405	1.218	2.287	2.395	2.453	1.778	1.478	0.881	0.269	0.162	13.994
LETA	0.0	0.0	0.0	0.133	1.157	1.559	1.321	1.022	0.777	0.415	0.0	0.0	6.403
ETA	0.138	0.137	0.753	1.503	3.444	4.454	3.774	2.800	2.275	1.295	0.383	0.162	21.113
PER-CCLATION	0.0	0.0	0.131	1.608	2.781	3.143	0.375	0.112	0.298	0.012	0.080	0.0	8.539
UZS	2.346	2.383	2.600	4.344	4.352	4.396	3.743	2.949	3.804	3.744	3.949	4.089	3.561
LZSA	7.800	7.800	7.804	9.259	10.314	11.749	12.240	11.159	10.510	10.020	9.879	9.936	9.884
LZST	7.800	7.800	7.804	9.259	10.214	11.748	12.240	11.159	10.510	10.020	9.879	9.936	9.884
GAS	2.006	2.004	2.003	2.013	2.074	2.290	2.463	2.374	2.352	2.282	2.210	2.154	2.187
TEMP.	21.2	37.0	38.2	48.3	58.7	68.7	76.9	77.6	63.9	53.8	37.7	37.8	52.0
CORRELATION COEFFICIENTS	0.318	0.676	0.650	0.719	0.710	0.879	0.864	0.847	0.848	0.963	0.989	0.975	0.753

DELTA STORAGE = 7.080 INCHES											
AATA = 3.940											
PCNC STORAGE = 0.0											
TOTAL CHANGE = 3.140											
SUM CAL TOTAL = 458000.											
SUM OBS TOTAL = 412314.											
SUM CAL SRINT = 275900.											
SUM OBS SR = 327519.											
SUM CAL BF = 222100.											
SUM OBS BF = 84956.											
PACK ON DECEMBER 31 = 0.05											
CHANGE IN SNOW STORAGE = 0.06											
AVERAGE MONTHLY BASE FLOW											
836.0 616-01519-02700-02046.0 720-01240-01054.0 660.0 496.0 780.0 868.0											
LEAP YEAR INDICATOR= 0 YES=1 & NO=0											
ITHAW IFREZ											
115 274											
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE											
YEAR 58											
JAN. FEB. MAR. APR. MAY. JUN. JUL. AUG. SEP. OCT. NOV. DEC. TOTAL											
0.0 0.0 0.0 0.659 1.161 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.820											

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1958

	JAN.	FEB.	MAR.	APR.	MAY	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP.	0.43	0.43	1.69	4.33	4.39	2.61	6.79	2.33	1.18	0.13	0.87	0.51	25.69
CALCULATED TOTAL RUNOFF	854.	641.	1187.	8313.	12586.	10560.	18090.	14366.	5952.	3792.	2706.	2104.	81160.
OBSERVED TOTAL RUNOFF	825.	644.	1860.	3473.	4164.	2408.	8386.	7233.	2369.	608.	825.	520.	33745.
CALCULATED SURFACE RUNOFF	63.	123.	755.	4955.	4065.	1557.	10154.	7933.	992.	6.	21.	65.	31286.
OBSERVED SURFACE RUNOFF	19.	28.	341.	773.	2138.	1688.	7156.	6179.	1709.	112.	45.	52.	20240.
CALCULATED INTERFLOW	0.	0.	0.	168.	625.	113.	12.	3.	0.	0.	0.	0.	921.
CALCULATED BASEFLOW	794.	518.	422.	3190.	7895.	8509.	7324.	6430.	4960.	3776.	2685.	2039.	48952.
OBSERVED BASEFLOW	806.	616.	1519.	2700.	2046.	720.	1240.	1054.	660.	496.	780.	868.	13505.
ETP	0.796	0.710	0.0	3.228	5.369	6.213	6.354	5.647	4.882	3.099	1.226	0.848	38.351
UETA	0.057	0.159	0.0	1.145	2.294	2.439	2.657	2.130	1.580	0.500	0.095	0.115	13.261
LETA	0.0	0.0	0.0	0.011	0.522	1.313	1.452	1.174	0.861	0.016	0.0	0.0	5.749
ETA	0.191	0.270	0.742	1.435	3.215	3.752	4.149	3.354	2.441	0.517	0.262	0.159	20.485
PER-CORRELATION	0.080	0.210	1.233	3.178	1.471	0.145	1.947	0.745	0.105	0.0	0.0	0.0	9.169
UZS	4.040	4.203	4.278	4.297	4.163	3.669	4.135	4.032	3.443	2.662	2.583	3.292	3.729
LZSA	5.943	10.032	10.364	13.920	13.891	12.731	12.410	12.523	11.927	11.536	11.536	11.536	11.876
LZST	5.943	10.052	10.364	14.368	15.176	14.601	14.230	14.343	13.747	13.356	13.356	13.356	13.089
GWS	2.113	2.084	2.063	2.520	3.160	3.307	3.066	2.917	2.726	2.536	2.394	2.289	2.505
TEMP.	31.9	28.9	25.7	48.0	64.0	70.9	73.7	75.9	69.1	56.0	40.8	31.1	51.4
CORRELATION COEFFICIENTS	0.870	0.822	0.586	0.627	0.802	0.633	0.562	0.387	0.568	0.584	0.966	0.617	0.693

DELTA STORAGE = 2.308 INCHES												
A41A = 2.457												
PCND STORAGE = 0.0												
TOTAL CHANGE = -0.150												
SUM CAL TOTAL = 579160.												
SUM OBS TOTAL = 446059.												
SLM CAL SRINT = 390107.												
SUM OBS SF = 347558.												
SLM CAL BF = 271053.												
SUM OBS BF = 58501.												
PACK ON DECEMBER 31 =-0.00												
CHANGE IN SNOW STORAGE =-0.05												
AVERAGE MONTHLY BASE FLOW												
558.01260.01209.01350.0 930.0 450.0 62.0 12.4 6.0 589.0 720.0 868.0												
LEAP YEAR INDICATOR= 0 YES=1 & NO=0												
ITHAW IFREZ												
112 284												
YEAR 59												
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE												
JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

SUMMARY TABLE - SOUTH FORK SOLICMON RIVER BASIN - 1959

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.42	0.71	2.62	1.19	2.35	2.82	3.20	3.71	3.75	3.51	0.06	0.23	24.57
CALCULATED TOTAL RUNOFF	1139.	1289.	1289.	976.	1485.	3828.	2357.	3009.	2736.	3436.	764.	524.	23011.
OBSERVED TOTAL RUNOFF	1354.	1509.	1509.	1387.	1184.	1619.	265.	325.	202.	2175.	771.	876.	12233.
CALCULATED SURFACE RUNOFF	17.	207.	660.	366.	1041.	3134.	1938.	2645.	2290.	2864.	161.	33.	15355.
OBSERVED SURFACE RUNOFF	11.	94.	300.	37.	254.	1169.	201.	313.	196.	1586.	51.	8.	4218.
CALCULATED INTER-FLOW	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
CALCULATED BASEFLOW	1491.	932.	729.	610.	444.	494.	423.	364.	446.	632.	603.	401.	7656.
OBSERVED BASEFLOW	558.	1260.	1209.	1250.	930.	450.	62.	12.	6.	589.	720.	868.	3014.
ETP	0.425	0.765	2.758	3.999	5.231	6.517	6.426	5.875	4.551	2.820	1.406	1.157	41.931
UETA	0.079	0.128	0.777	1.416	1.651	2.374	2.106	2.085	1.597	1.070	0.299	0.229	14.011
LETA	0.0	0.0	0.0	0.030	0.838	1.365	1.199	1.154	0.868	0.266	0.0	0.0	5.725
ETA	0.230	0.269	0.777	1.446	2.689	3.744	3.306	3.239	2.465	1.336	0.299	0.229	20.028
PER-CORRELATION	0.0	0.164	0.886	0.051	0.295	0.676	0.137	0.337	0.809	2.011	0.004	0.0	5.382
U2S	3.394	3.705	4.009	3.570	3.735	3.391	3.010	3.528	3.646	4.170	4.265	4.110	3.744
L2SA	11.536	11.611	11.532	12.613	12.459	11.462	10.759	9.837	9.202	10.880	11.193	11.193	11.269
L2ST	13.356	13.431	13.752	14.432	14.289	13.787	12.588	11.717	11.022	12.700	13.013	13.013	13.089
G4S	2.212	2.159	2.121	2.096	2.078	2.095	2.084	2.092	2.085	2.116	2.095	2.070	2.102
TEMP.	25.8	29.1	35.7	50.3	62.0	75.0	75.0	79.4	63.7	50.3	36.0	35.0	51.9
CORRELATION COEFFICIENTS	0.784	0.793	0.926	0.861	0.836	0.866	0.620	0.375	0.759	0.671	0.764	0.969	0.752

DELTA STORAGE = 3.715 INCHES												
AAIA = 3.662												
PCND STORAGE = 0.0												
TOTAL CHANGE = 0.053												
SUM CAL TOTAL = 602171.												
SUM OBS TOTAL = 458292.												
SUM CAL SRINT = 223462.												
SUM OBS SR = 351776.												
SUM CAL BF = 278703.												
SUM OBS BF = 106515.												
PACK IN DECEMBER 31 = 0.0												
CHANGE IN SNOW STORAGE = 0.00												
AVERAGE MONTHLY BASE FLOW												
589.01508.02170.03300.02697.01710.0 558.0 68.2 63.0 161.2 480.0 713.0												
LEAP YEAR INDICATOR= 1 YES=1 & NO=0												
ITHAW IFREZ												
113 297												
YEAR 60												
RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE												
JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
0.0	0.0	0.620	0.581	1.201	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.403

SUMMARY TABLE - SOUTH FORK SALTWATER RIVER BASIN - 1960

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.52	1.75	2.34	2.01	4.23	3.99	1.04	3.15	1.46	2.05	0.18	0.71	23.54
CALCULATED TOTAL RUNOFF	495.	1126.	2181.	12594.	22338.	17067.	9408.	8684.	5191.	3653.	2646.	2101.	87975.
OBSERVED TOTAL RUNOFF	615.	1843.	9734.	3728.	10007.	4943.	622.	1741.	254.	245.	503.	719.	34993.
CALCULATED SURFACE RUNOFF	130.	784.	774.	3020.	7741.	4330.	622.	2403.	613.	508.	53.	131.	21110.
OBSERVED SURFACE RUNOFF	26.	335.	7564.	428.	7310.	3233.	64.	1672.	231.	84.	23.	6.	23976.
CALCULATED INTERFLOW	0.	71.	667.	2499.	3307.	1858.	270.	0.	0.	0.	0.	0.	3672.
CALCULATED BASEFLOW	357.	271.	740.	7075.	11790.	10879.	8515.	6280.	4578.	3145.	2593.	1970.	53193.
OBSERVED BASEFLOW	589.	1508.	2170.	3300.	2657.	1710.	558.	68.	63.	161.	480.	713.	14017.
ETP	0.415	0.0	0.532	4.244	5.105	6.148	6.457	5.690	4.833	3.129	1.685	0.513	28.800
UETA	0.078	0.0	0.106	1.501	2.279	2.721	1.560	1.591	1.160	0.658	0.305	0.126	12.484
LETA	0.0	0.0	0.0	0.032	1.001	1.465	1.166	1.032	0.756	0.370	0.0	0.0	5.874
ETA	0.185	0.326	0.791	1.533	3.280	4.186	3.126	2.672	1.916	1.029	0.305	0.303	13.652
PER-CORRELATION	0.343	1.740	1.835	0.479	1.720	0.835	0.035	0.111	0.053	0.155	0.001	0.112	7.163
U25	4.220	4.546	4.545	4.021	4.265	3.983	2.990	2.933	2.970	3.341	3.796	3.906	3.785
L75A	11.231	12.652	13.413	14.063	14.012	13.347	12.406	11.298	10.522	9.995	9.963	9.992	11.504
L75I	13.051	14.472	15.330	16.829	17.345	16.594	15.536	14.424	13.648	13.121	13.094	13.119	14.711
GWS	2.051	2.041	2.133	3.060	3.718	3.599	3.209	2.892	2.672	2.503	2.360	2.280	2.713
TEMP.	24.4	21.4	31.0	54.1	60.2	70.0	75.4	76.5	68.3	56.6	40.9	30.0	50.8
CORRELATION COEFFICIENTS	0.579	0.616	0.649	0.814	0.548	0.516	0.930	0.398	0.579	0.661	0.901	0.890	0.673

DELTA STORAGE = 0.746 INCHES
AAIA = 2.850
PCNC STORAGE = 0.0

TOTAL CHANGE = -2.104

SUM CAL TOTAL =	490146.
SUM OBS TOTAL =	493285.
SUM CAL SRINT =	35324.
SUM OBS SP =	372752.
SUM CAL RF =	336901.
SUM OBS RF =	120533.

PACK ON DECEMBER 31 = 0.10

AVERAGE MONTHLY BASE FLOW

LEAP YEAR INDICATOR= 0 YES=1 E NC=0

IPFW	IFREQ	YEAR
111	292	61

RECHARGE TO GROUND WATER FROM THE LOWER SOIL ZONE

JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
0.0	0.0	0.0	0.0	0.0	0.748	0.0	0.0	0.0	0.0	0.0	0.0	0.748

SUMMARY TABLE - SOUTH FORK SOLOMON RIVER BASIN - 1961

	JAN.	FEB.	MAR.	APR.	MAY.	JUN.	JUL.	AUG.	SEP.	OCT.	NOV.	DEC.	TOTAL
PRECIP	0.12	0.13	2.17	1.48	6.70	5.13	3.36	4.42	2.14	0.84	2.13	0.26	29.61
CALCULATED TOTAL RUNOFF	578.	1564.	1739.	1739.	8464.	17223.	8455.	10547.	4190.	2912.	3684.	1959.	63359.
OBSERVED TOTAL RUNOFF	792.	1001.	1145.	1385.	5954.	11571.	2110.	5168.	863.	795.	1207.	1047.	33033.
CALCULATED SURFACE RUNOFF	4.	13.	526.	1133.	7702.	9261.	1678.	6133.	1365.	264.	2003.	21.	30803.
OBSERVED SURFACE RUNOFF	17.	21.	51.	275.	4280.	5441.	1357.	4672.	413.	51.	67.	24.	23749.
CALCULATED INTER-FLOW	0.	0.	0.	0.	310.	2631.	553.	35.	0.	0.	46.	115.	4391.
CALCULATED BASEFLOW	1440.	565.	638.	606.	452.	5331.	5525.	4379.	2325.	2648.	1835.	1422.	28465.
OBSERVED BASEFLOW	775.	580.	1054.	1110.	1674.	2130.	713.	496.	453.	744.	1140.	1073.	12289.
ETP	1.018	1.313	2.820	2.596	4.579	6.208	6.560	5.584	4.435	2.988	1.305	0.356	40.561
UETA	0.054	0.161	1.030	1.039	2.325	2.751	2.268	2.079	1.331	0.773	0.357	0.043	14.223
LETA	0.0	0.0	0.0	0.039	1.044	1.487	1.249	1.132	0.723	0.301	0.0	0.0	5.575
ETA	0.054	0.214	1.030	1.411	3.370	4.248	3.517	3.211	2.054	1.074	0.450	0.203	20.836
PER-CORRELATION	0.001	0.005	0.588	0.451	2.909	2.687	0.375	0.755	0.316	0.072	0.936	0.038	9.182
UTS	4.143	4.099	4.118	4.127	4.337	4.131	3.675	3.691	3.775	2.689	3.949	4.159	3.929
LZSA	10.031	10.034	10.454	10.623	12.148	13.755	12.831	12.278	11.927	11.567	12.020	12.507	11.732
LZSY	13.207	13.210	13.580	14.045	15.267	17.269	16.134	15.550	15.239	14.839	15.292	15.779	14.963
GWS	2.204	2.152	2.120	2.101	2.131	2.343	2.755	2.625	2.520	2.411	2.225	2.259	2.374
TEMP.	30.2	35.7	40.5	46.3	58.4	70.8	76.8	74.9	61.8	53.3	36.2	24.9	51.0
CORRELATION COEFFICIENTS	0.898	0.899	0.758	0.510	0.813	0.779	0.679	0.550	0.701	0.879	0.568	0.891	0.733

[illegible]

DAILY FLOW DURATION AND ERROR TABLE

FLOW INTERVAL	ACT. CASES	PCT.	CALC. CASES	PCT.	AVE. ERROR	AV. ABS. ERROR	STD. ERROR
0.0-	910.0	100.000	23.0	100.000	26.3	26.31	34.30
1.0-	164.0	81.545	109.0	95.534	25.8	36.82	53.76
1.8-	146.0	78.219	161.0	47.343	46.8	46.88	60.27
3.2-	163.0	75.259	267.0	94.078	66.5	66.95	77.05
5.6-	303.0	71.953	374.0	88.664	36.6	38.50	59.55
10.0-	418.0	65.707	502.0	81.076	36.2	40.88	58.29
17.8-	544.0	57.230	716.0	70.853	37.7	46.49	78.42
31.6-	777.0	38.083	678.0	56.378	47.3	65.26	108.65
56.2-	487.0	22.328	644.0	42.623	196.0	213.68	236.68
100.0-	302.0	12.452	517.0	25.568	170.0	215.33	293.61
177.8-	112.0	8.327	369.0	19.383	273.1	352.02	431.75
316.2-	77.0	4.056	291.0	11.600	374.8	504.34	593.71
562.3-	47.0	2.494	152.0	5.659	355.8	704.91	846.59
1000.0-	33.0	1.541	87.0	2.616	161.7	928.30	1359.51
1778.3-	21.0	0.872	29.0	0.852	-831.6	1537.55	1974.71
3162.3-	11.0	0.466	9.0	0.264	-2526.2	2529.18	704.01
5623.4-	5.0	0.243	4.0	0.081	-4230.6	4250.60	586.95
10000.0-	6.0	0.142	0.0	0.0	-7531.5	7631.45	4174.19
17792.7-	0.0	0.020	0.0	0.0	-30552.1		
56234.0-	0.0	0.0	0.0	0.0			
99999.8-	0.0	0.0	0.0	0.0			
177827.4-	0.0	0.0	0.0	0.0			
316226.9-	0.0	0.0	0.0	0.0			
	4931.0		4931.0		234452.9	630077.44	11730.00

DELTA STORAGE = 39.354 INCHES
 AATA = 43.674
 PCND STORAGE = 0.0

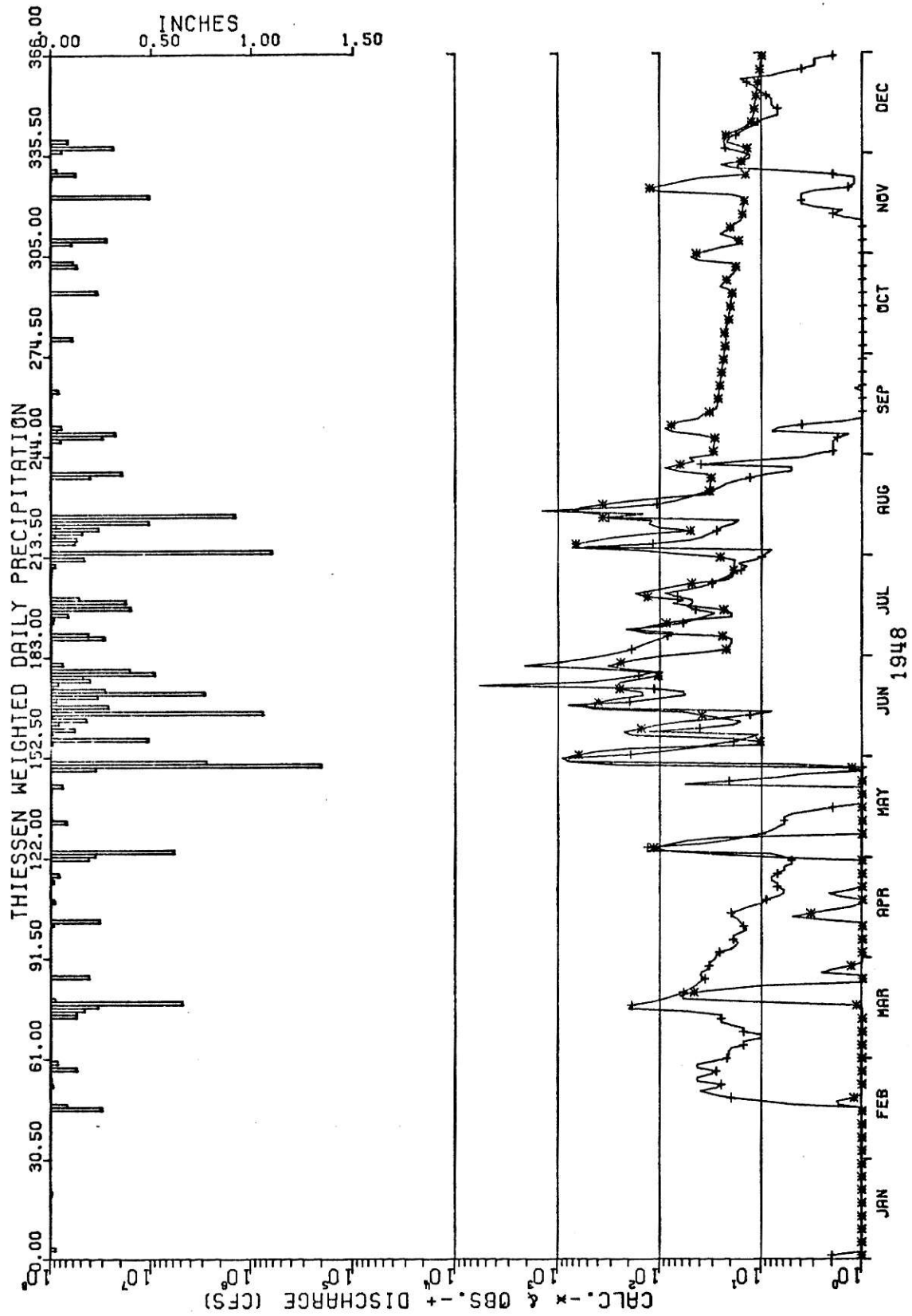
TOTAL CHANGE = -4.620

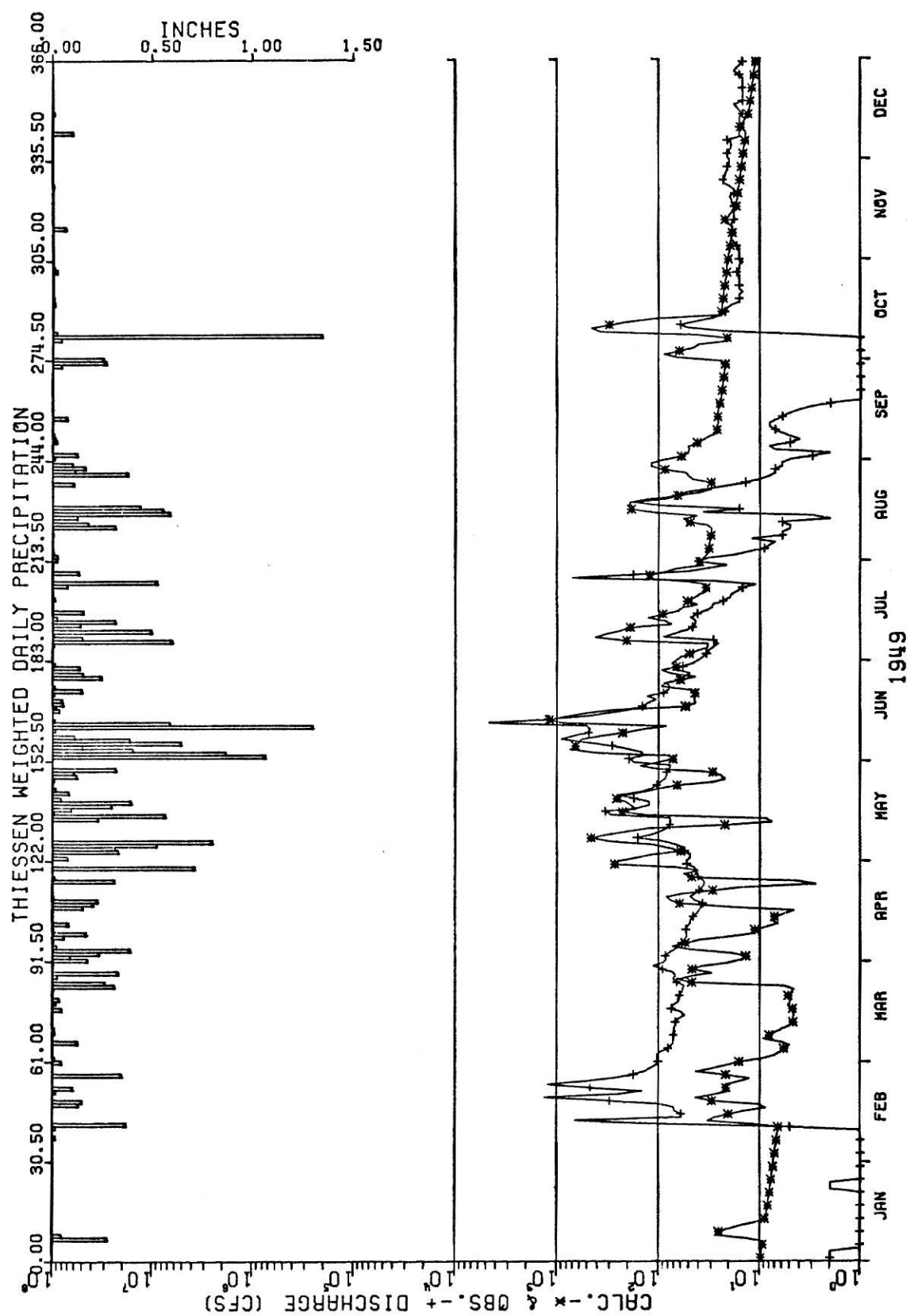
TOTAL PRECIPITATION = 322.934

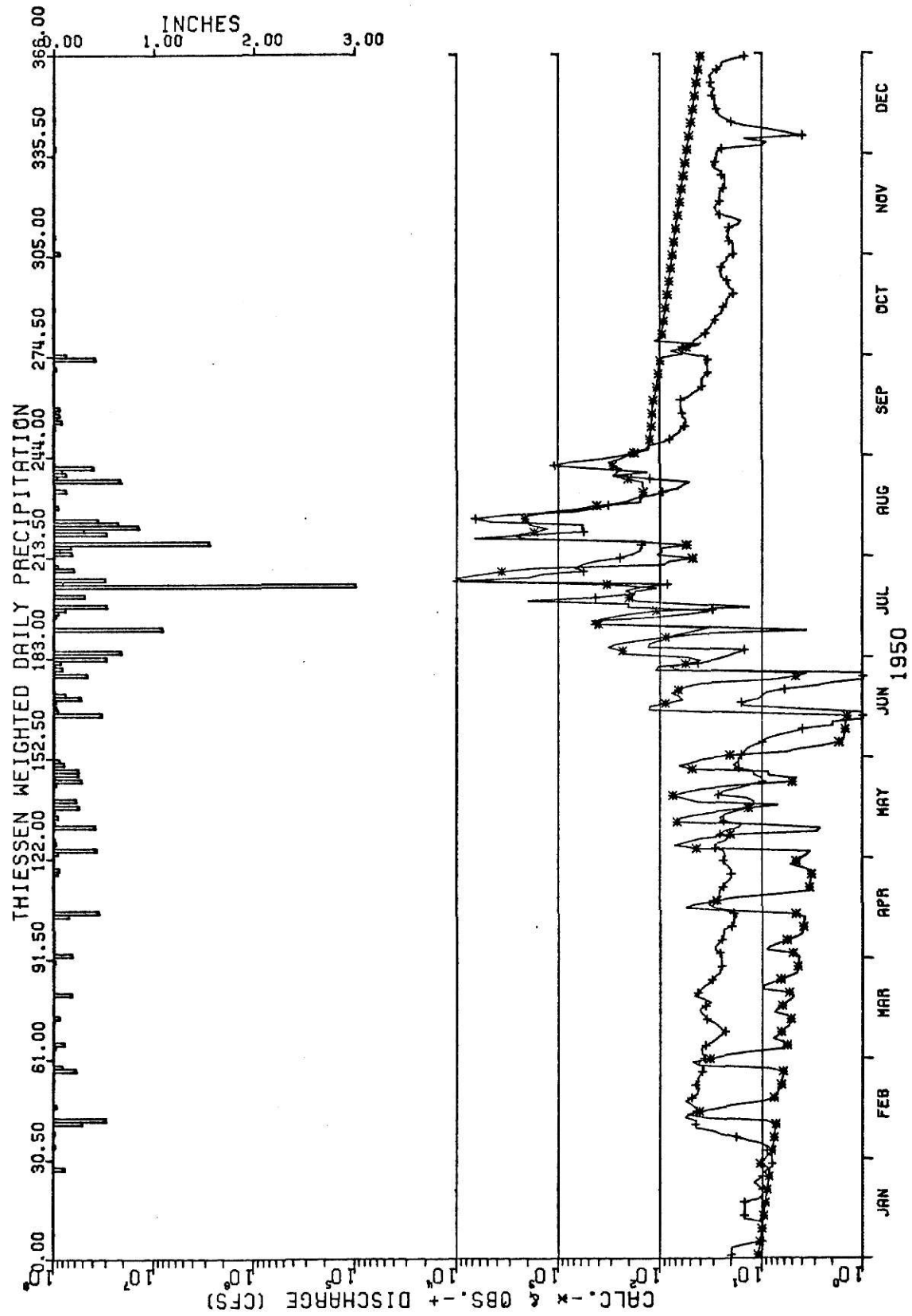
TOTAL IA 43.674
 TOTAL SURFACE RUNOFF 16.891
 TOTAL UETA 178.680
 TOTAL PERC 31.350
 CHANGE IN UZSM 1.314

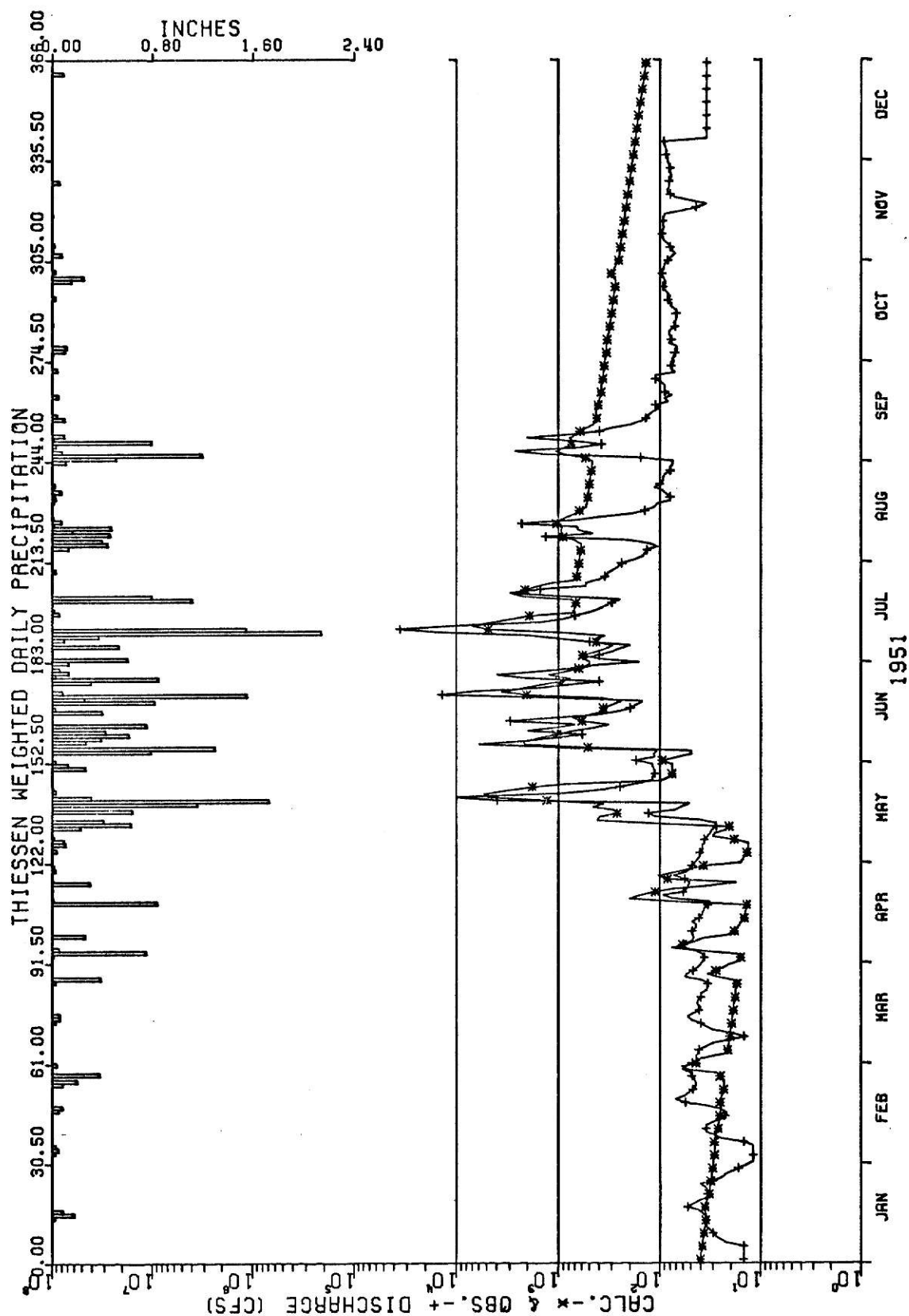
CHECK BALANCE 322.508

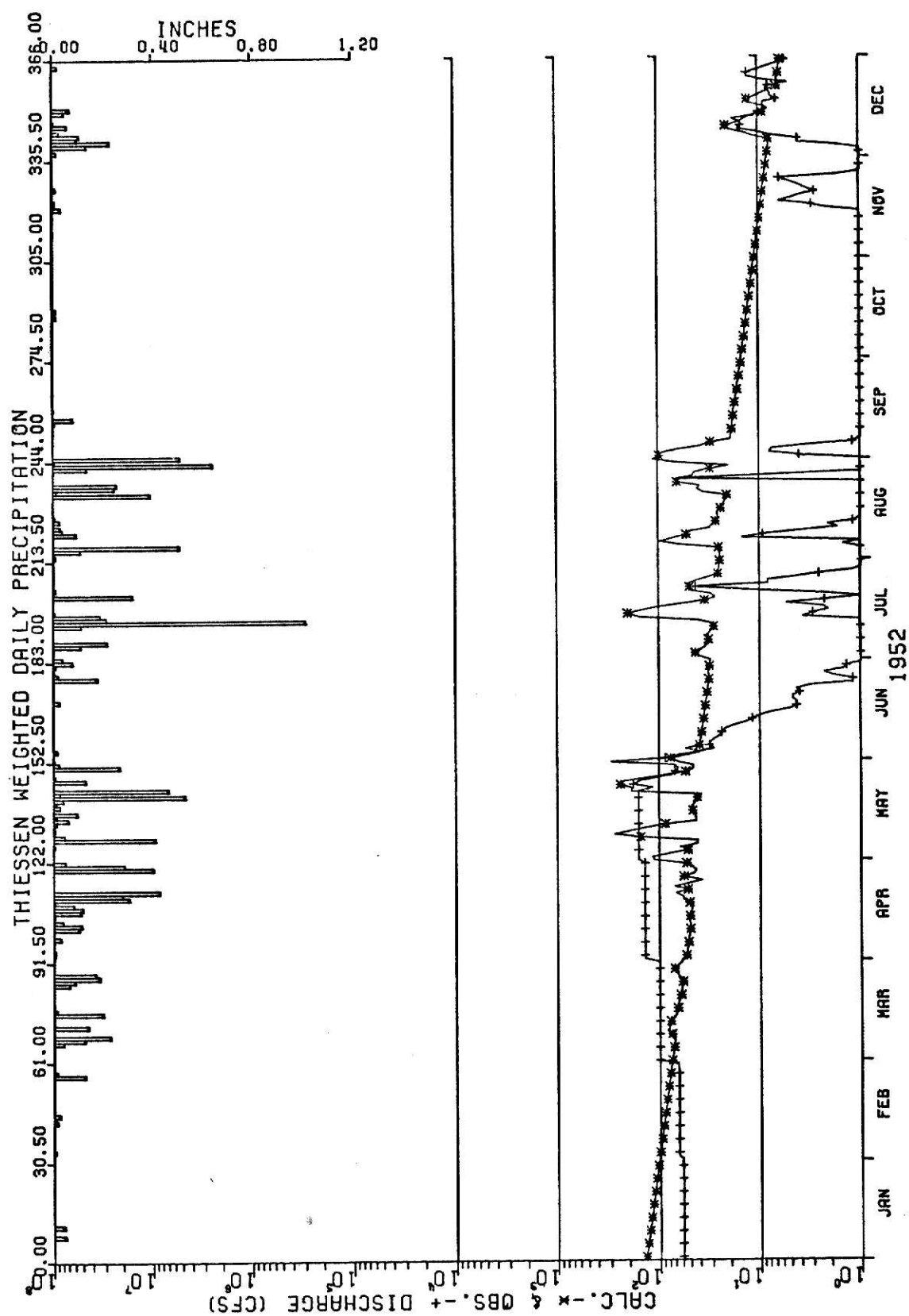
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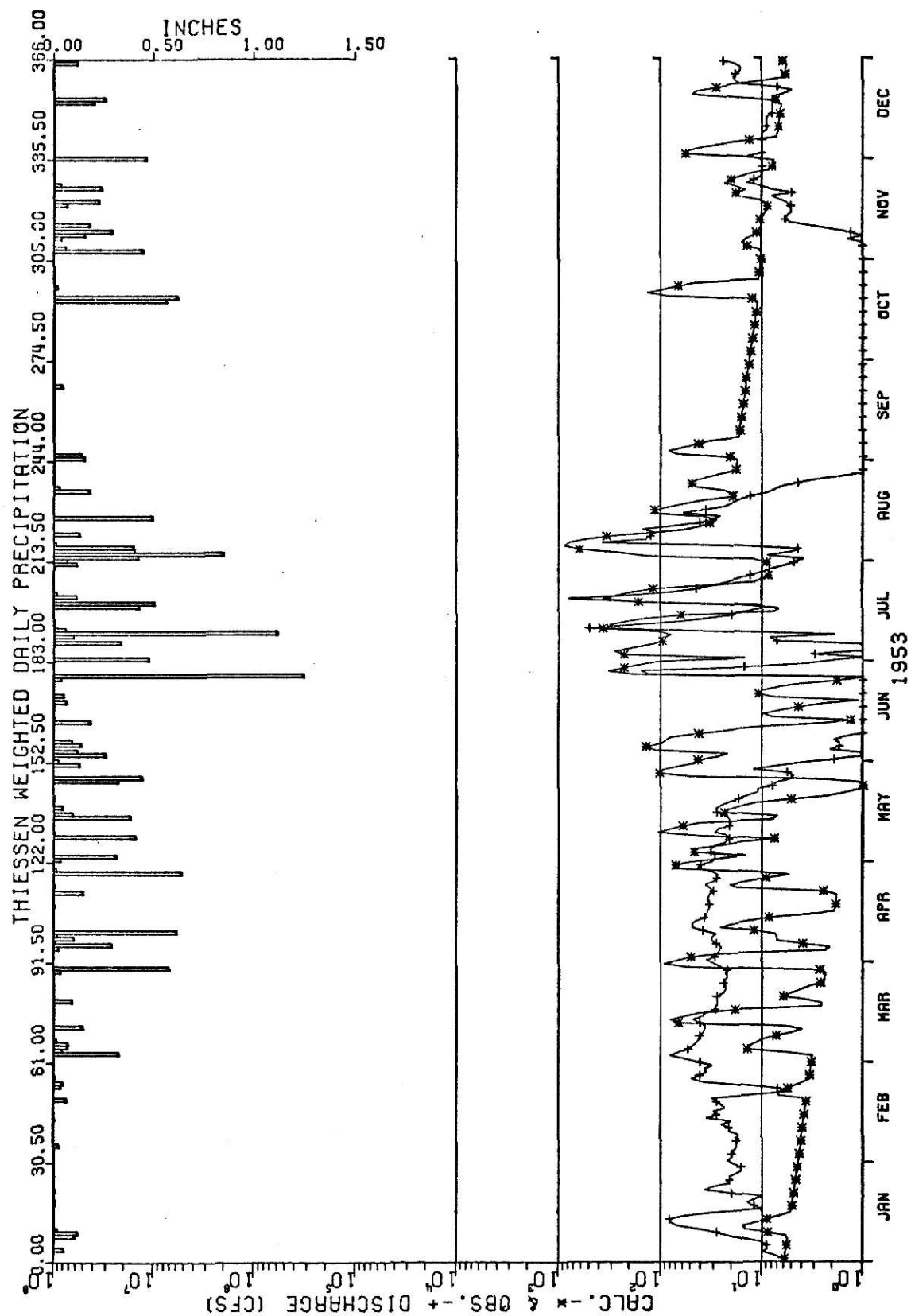


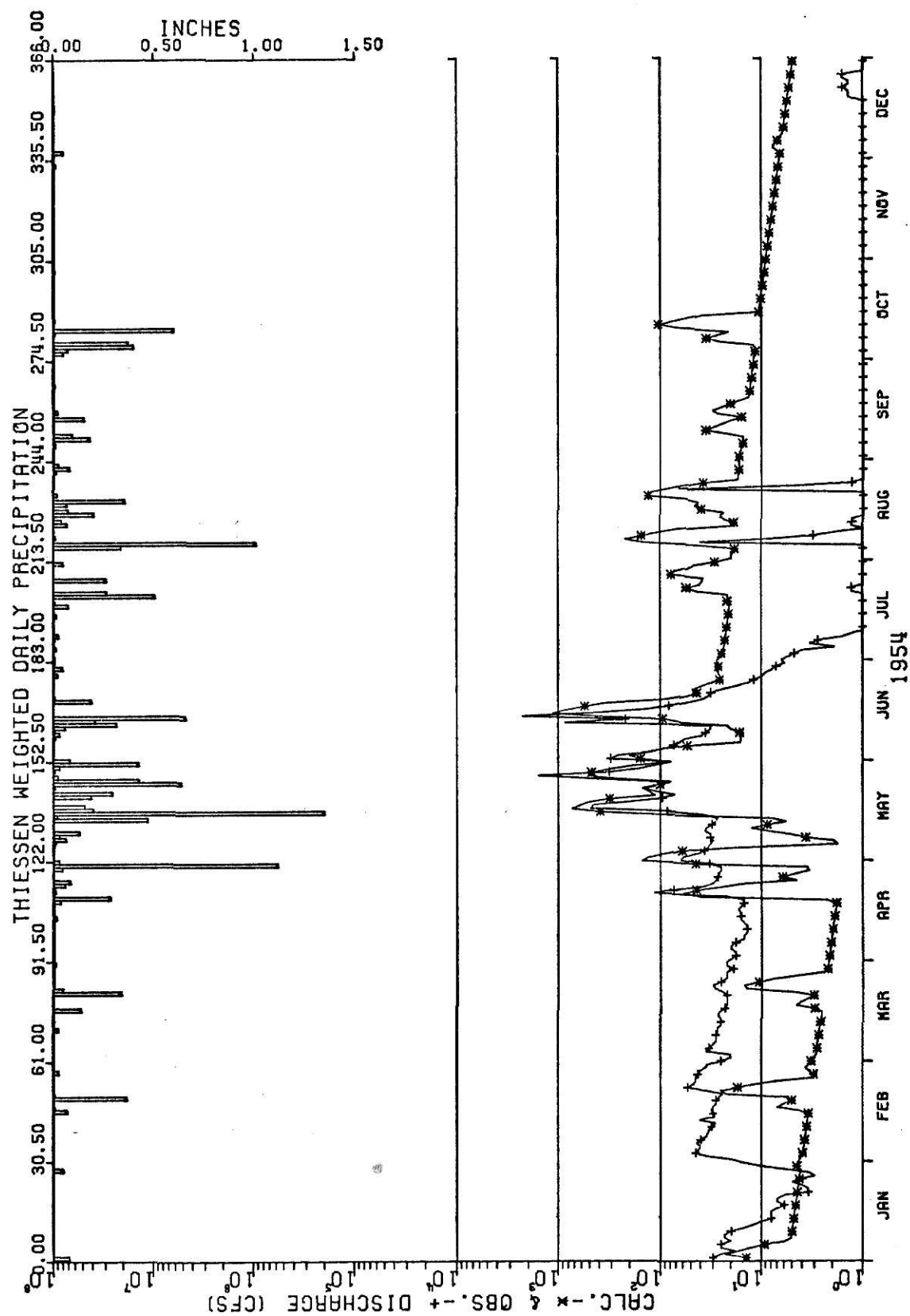


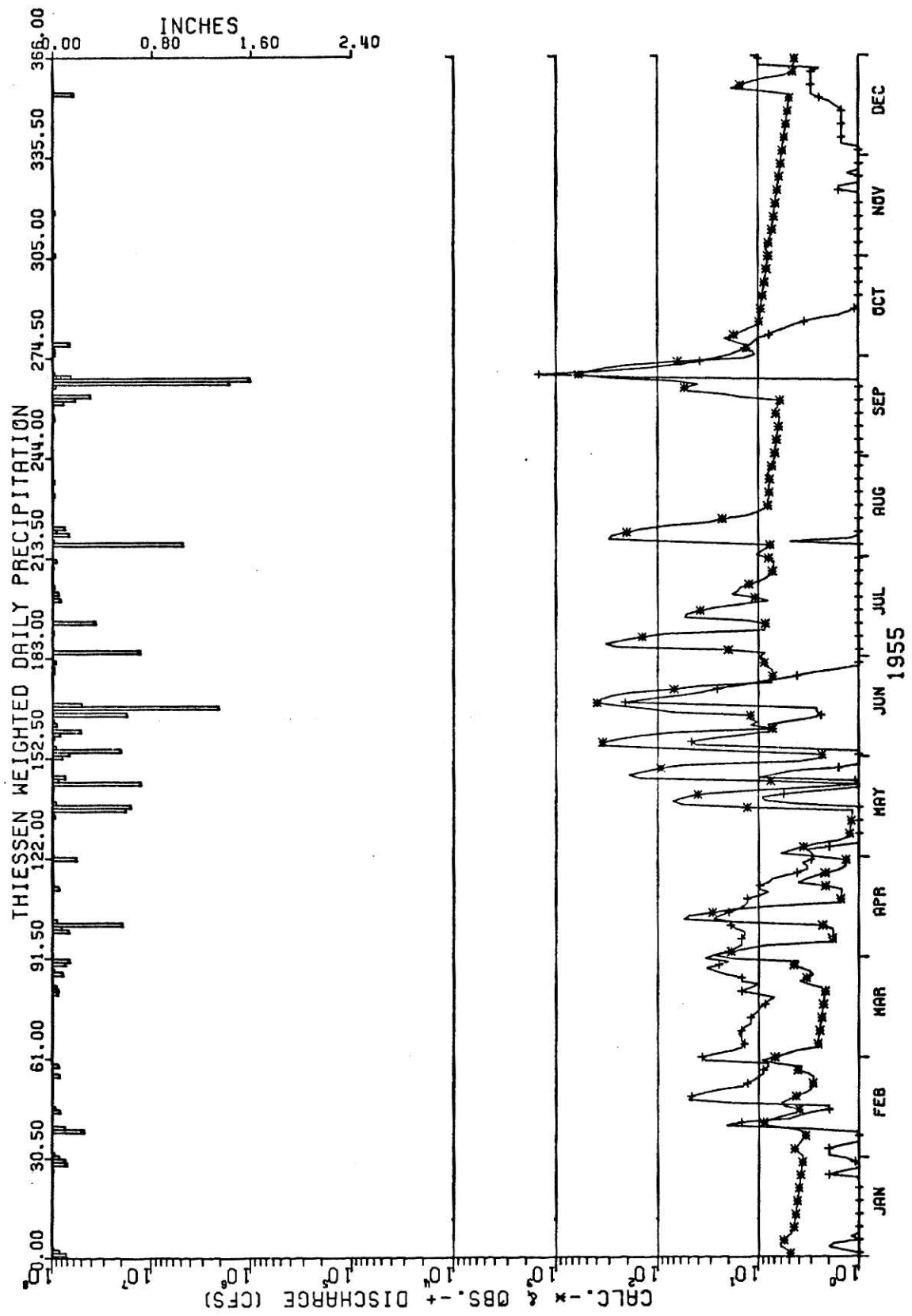


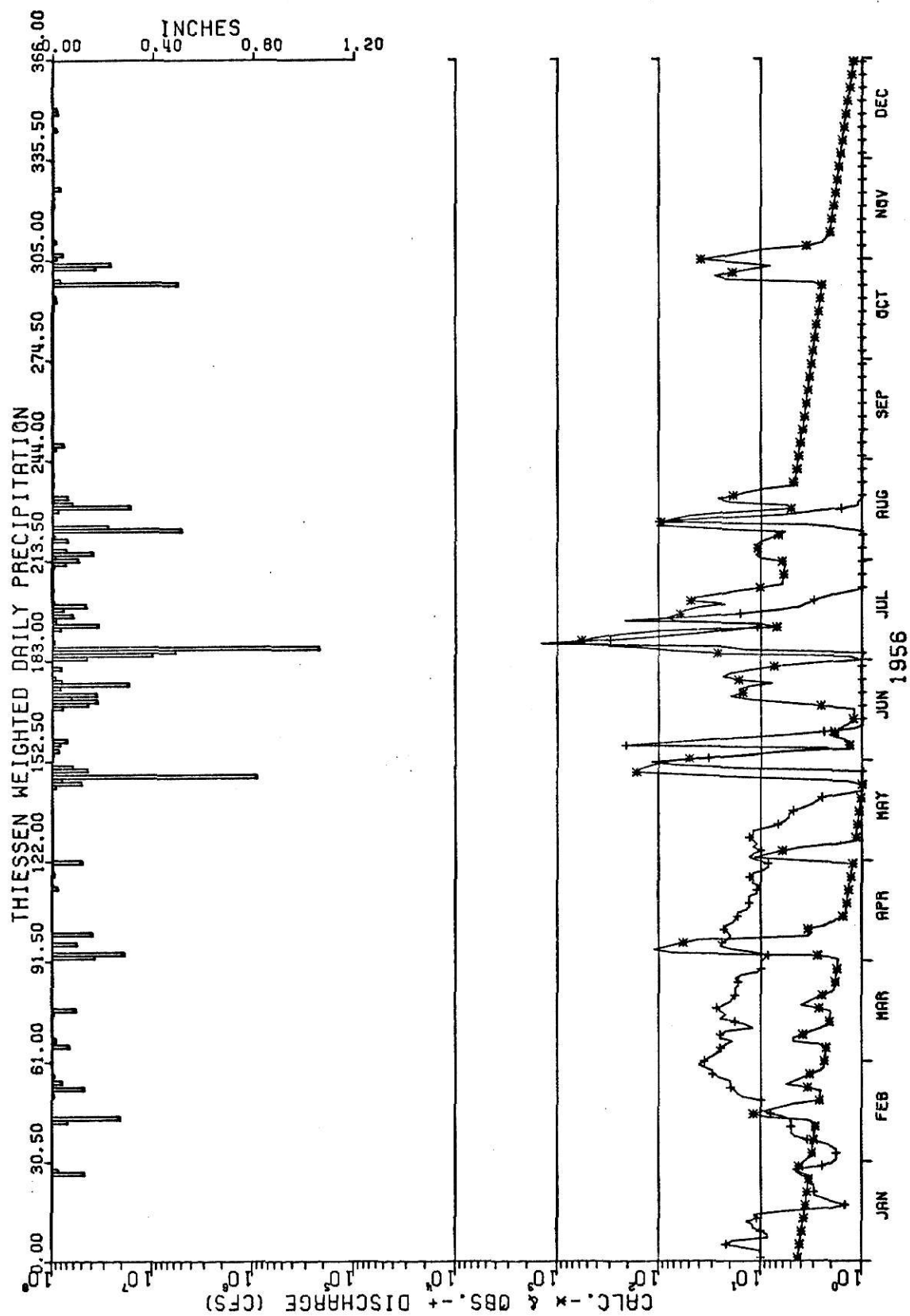


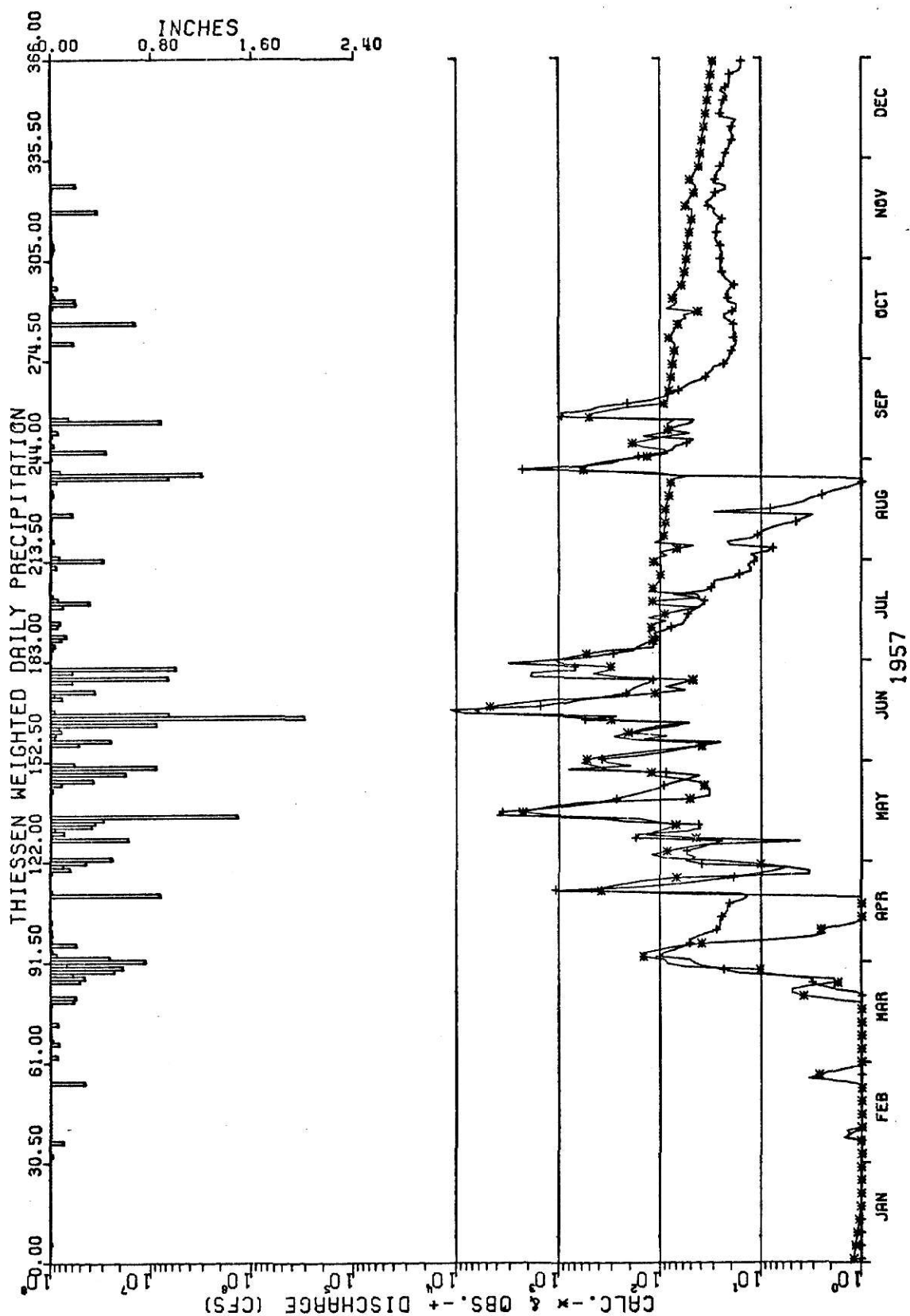


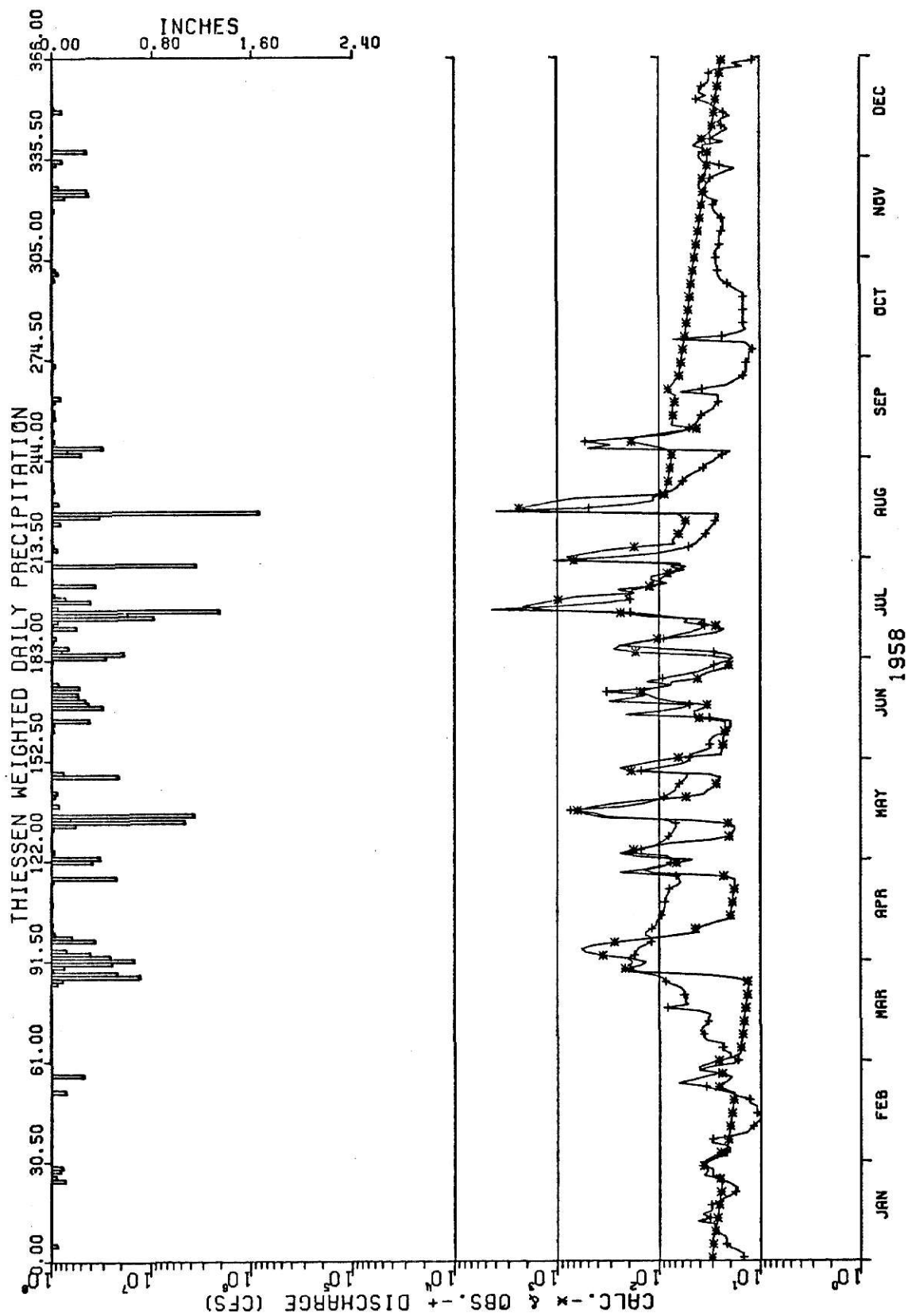


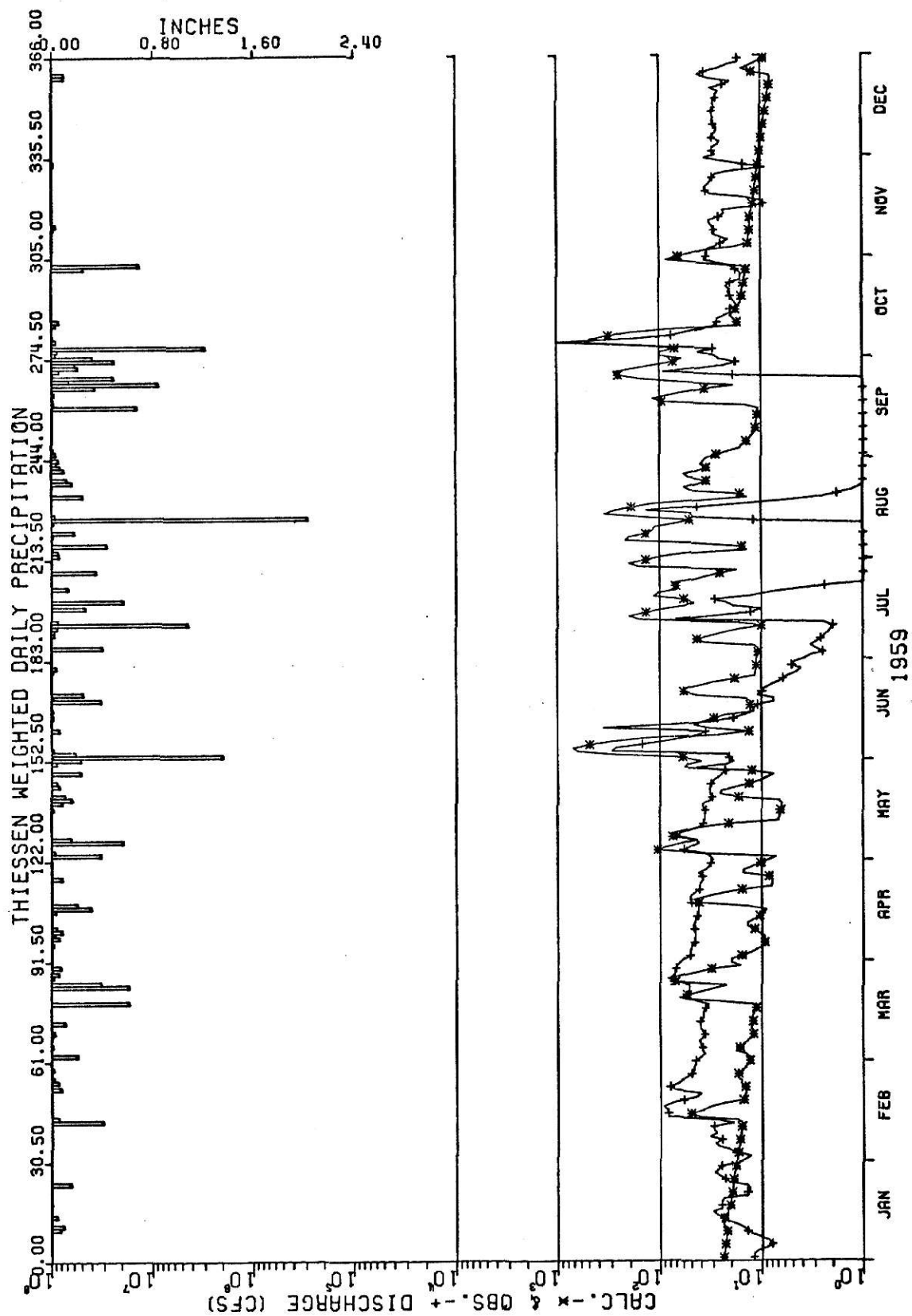


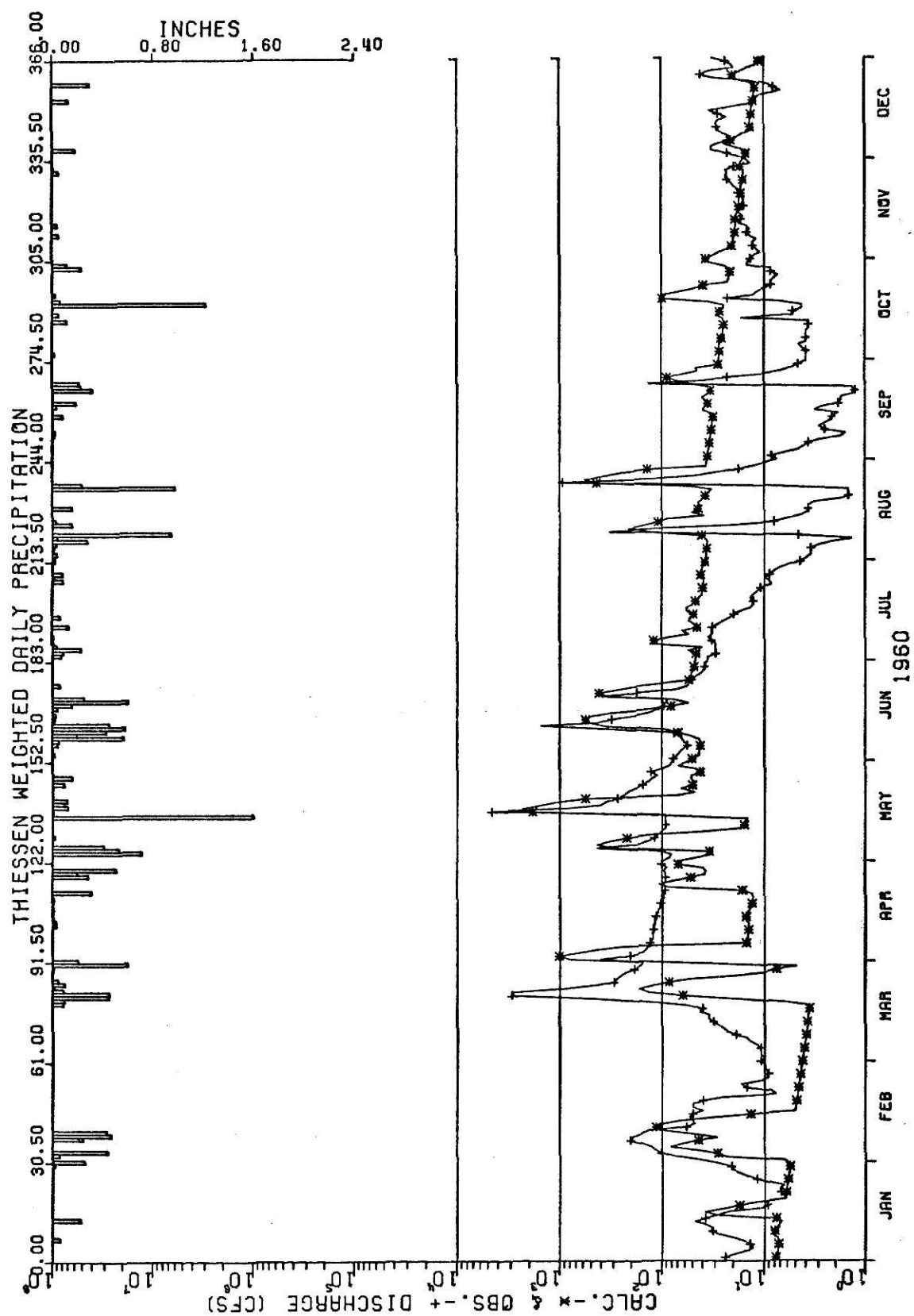


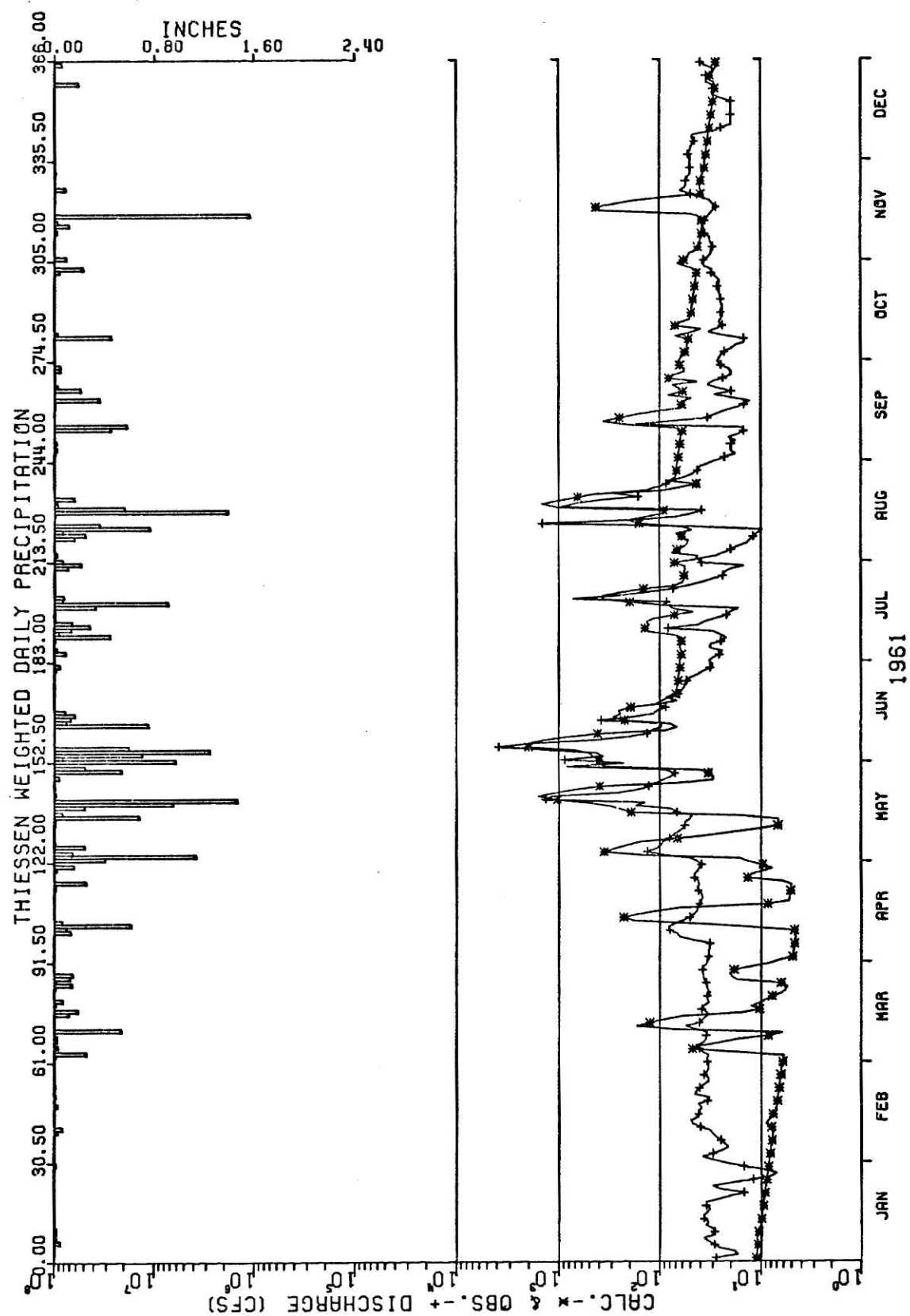




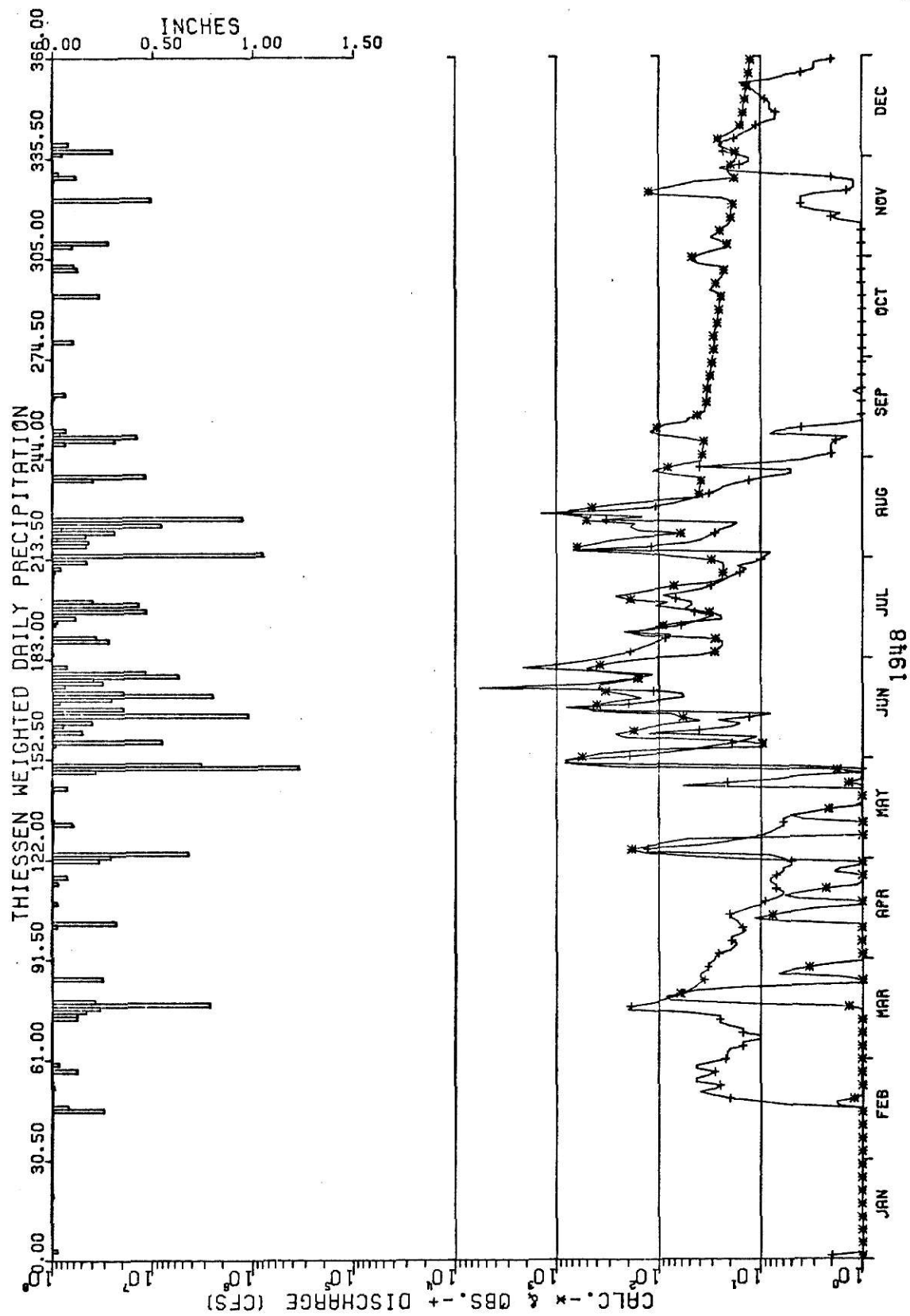


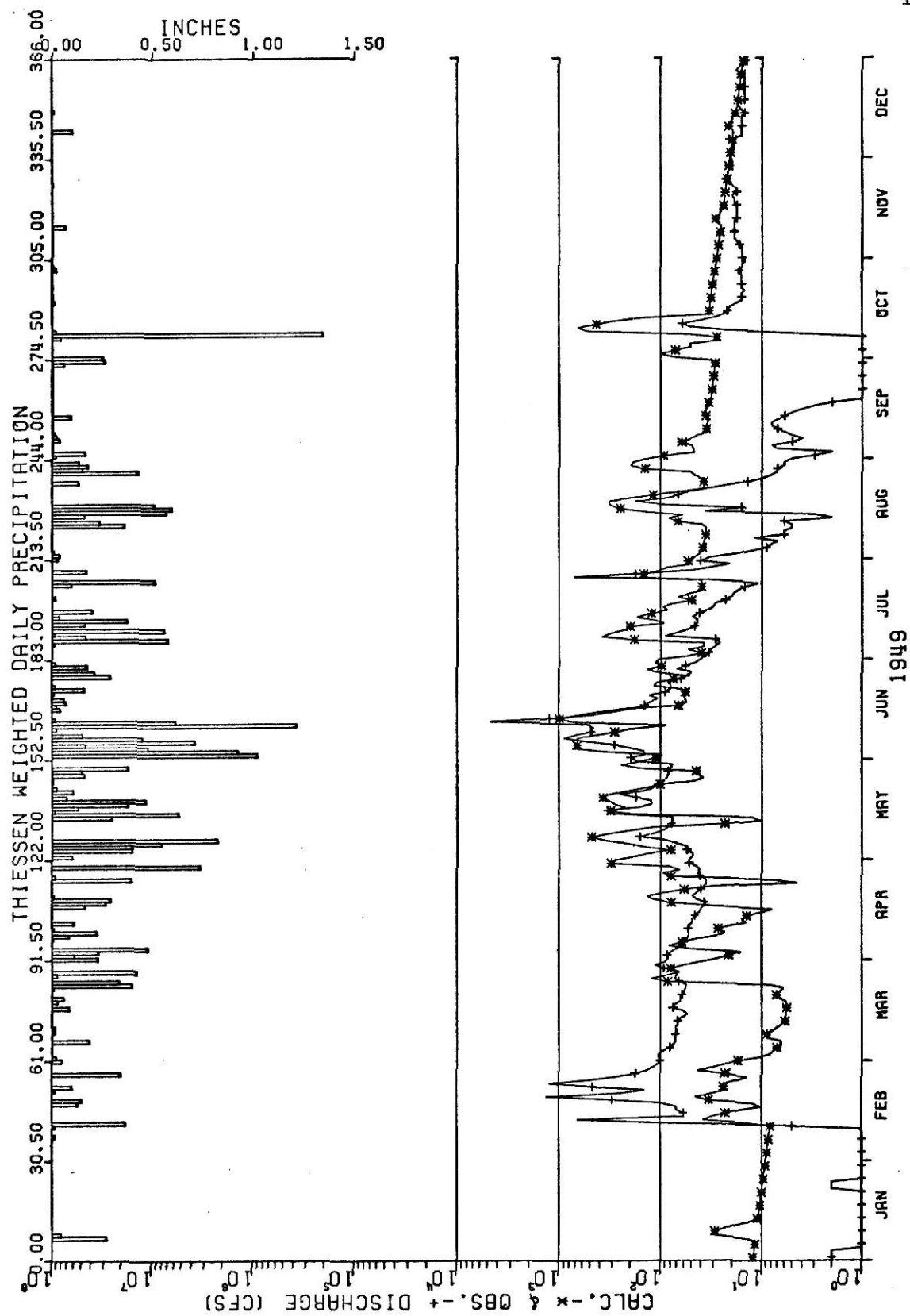


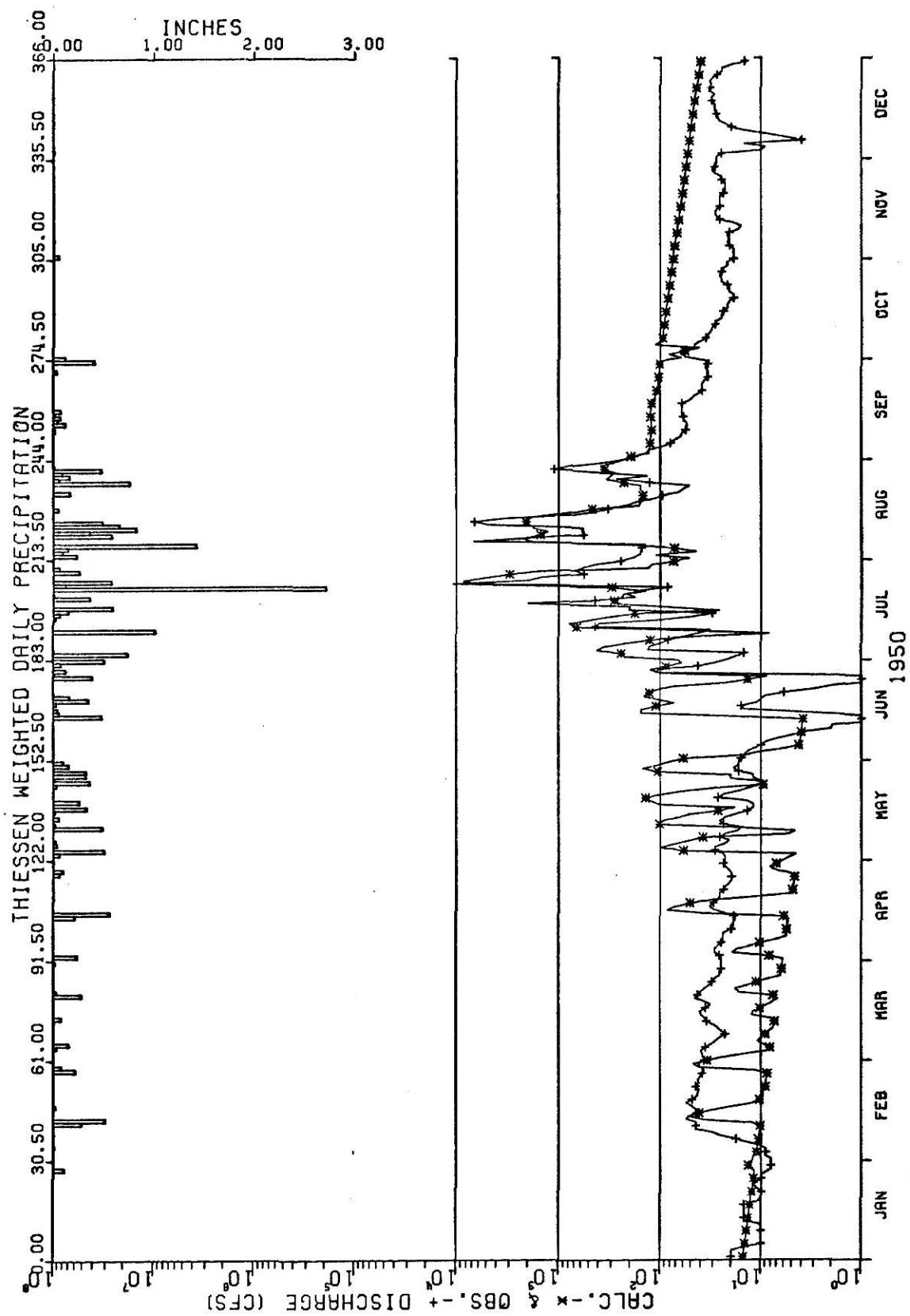


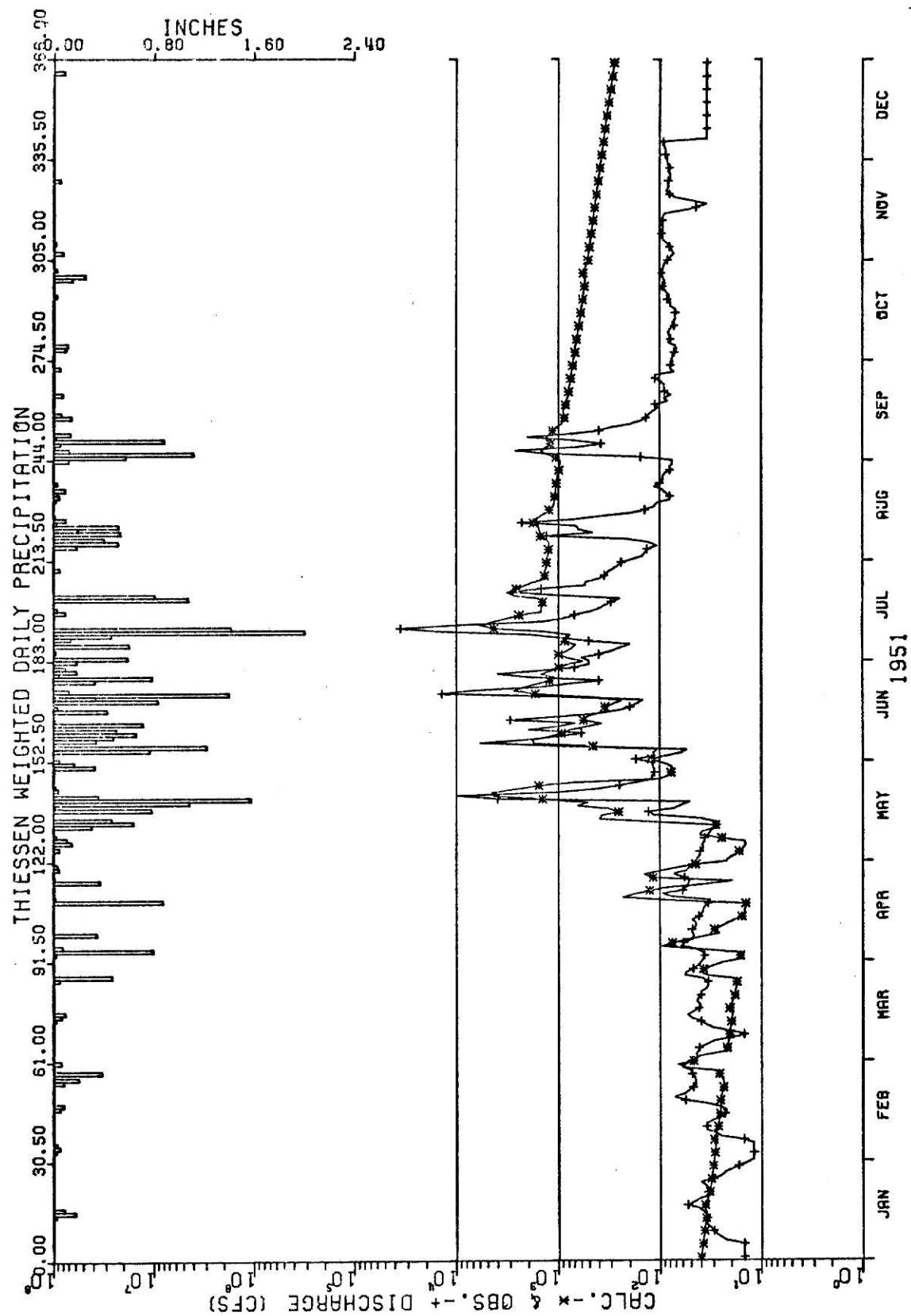


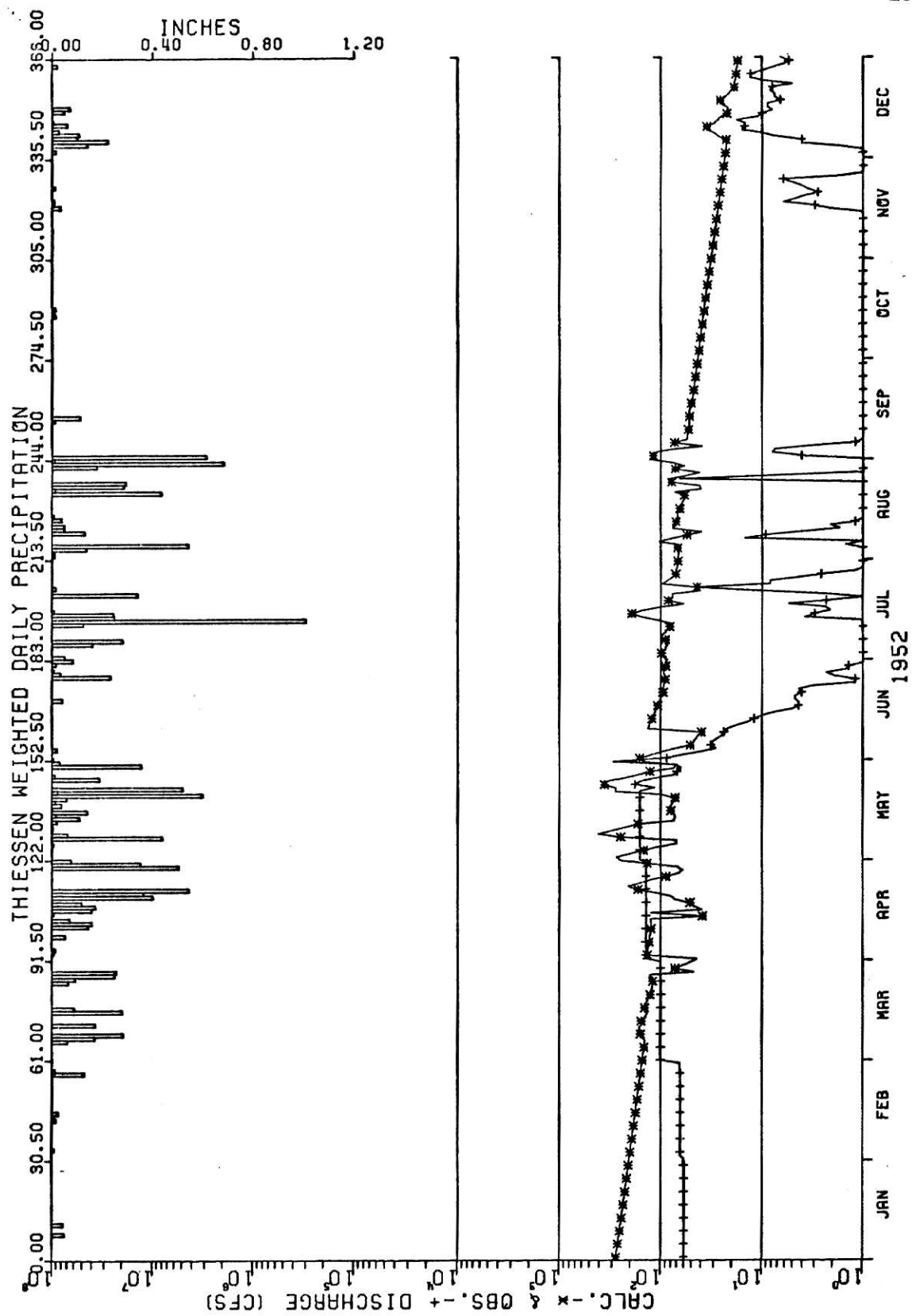
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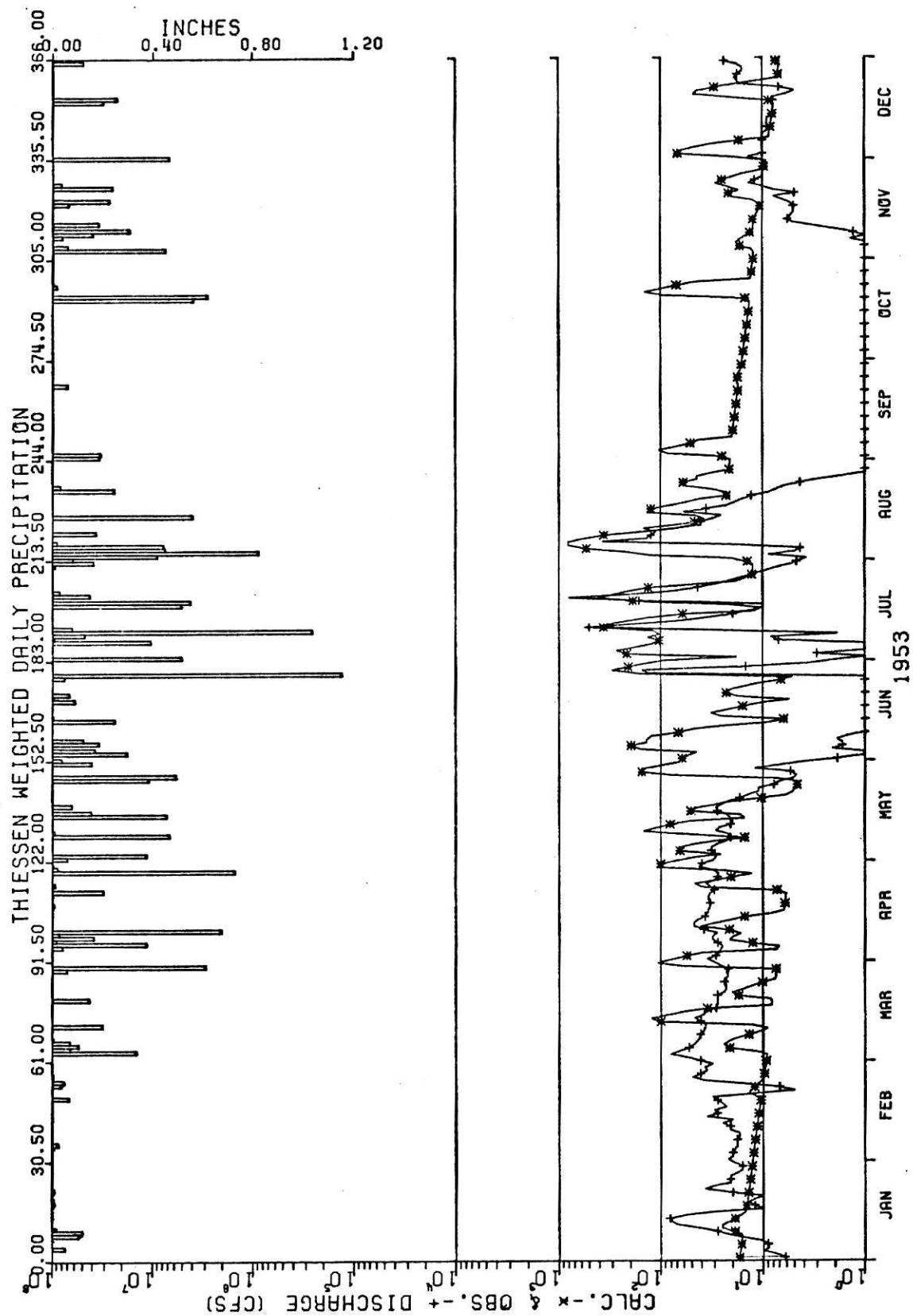


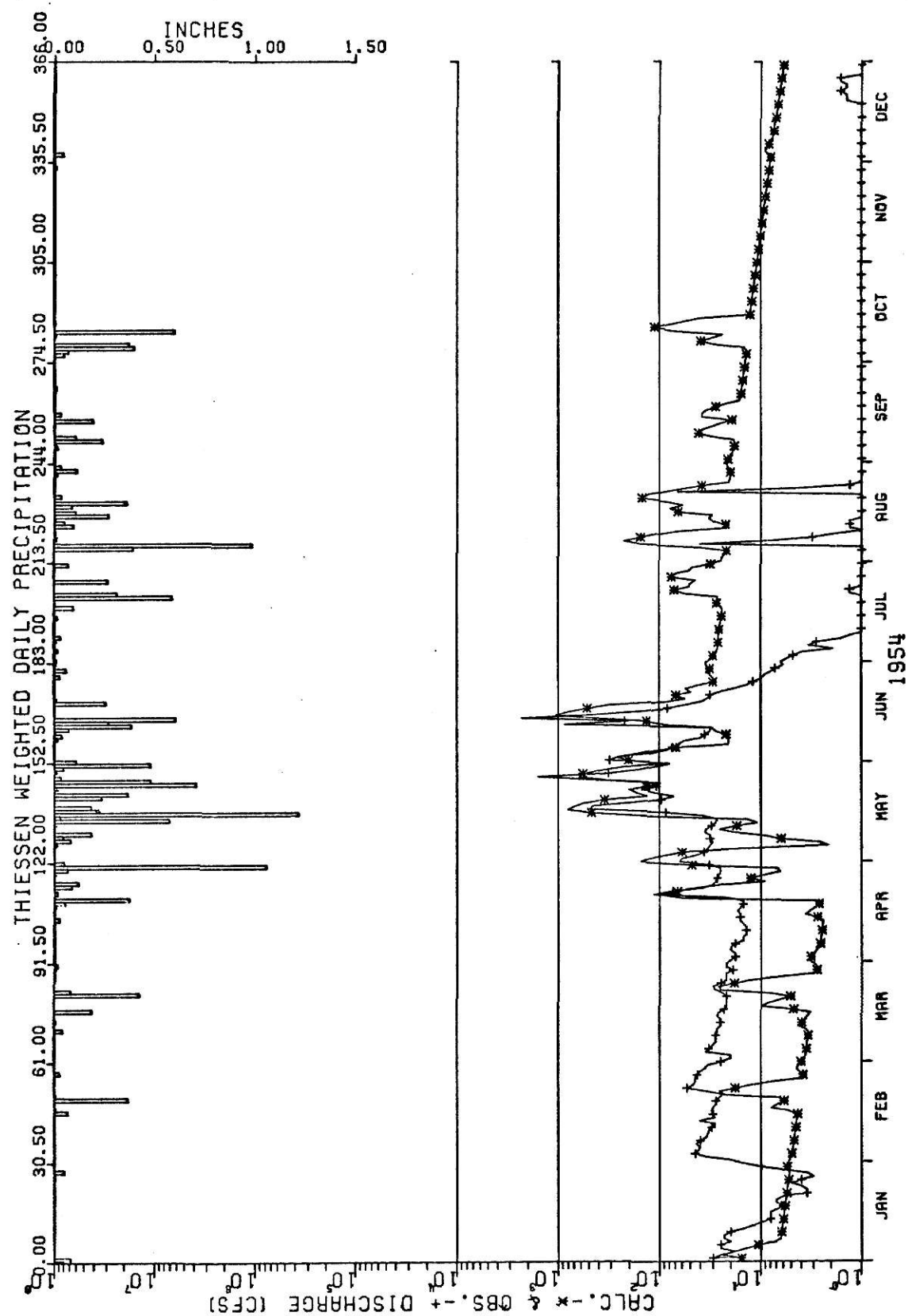


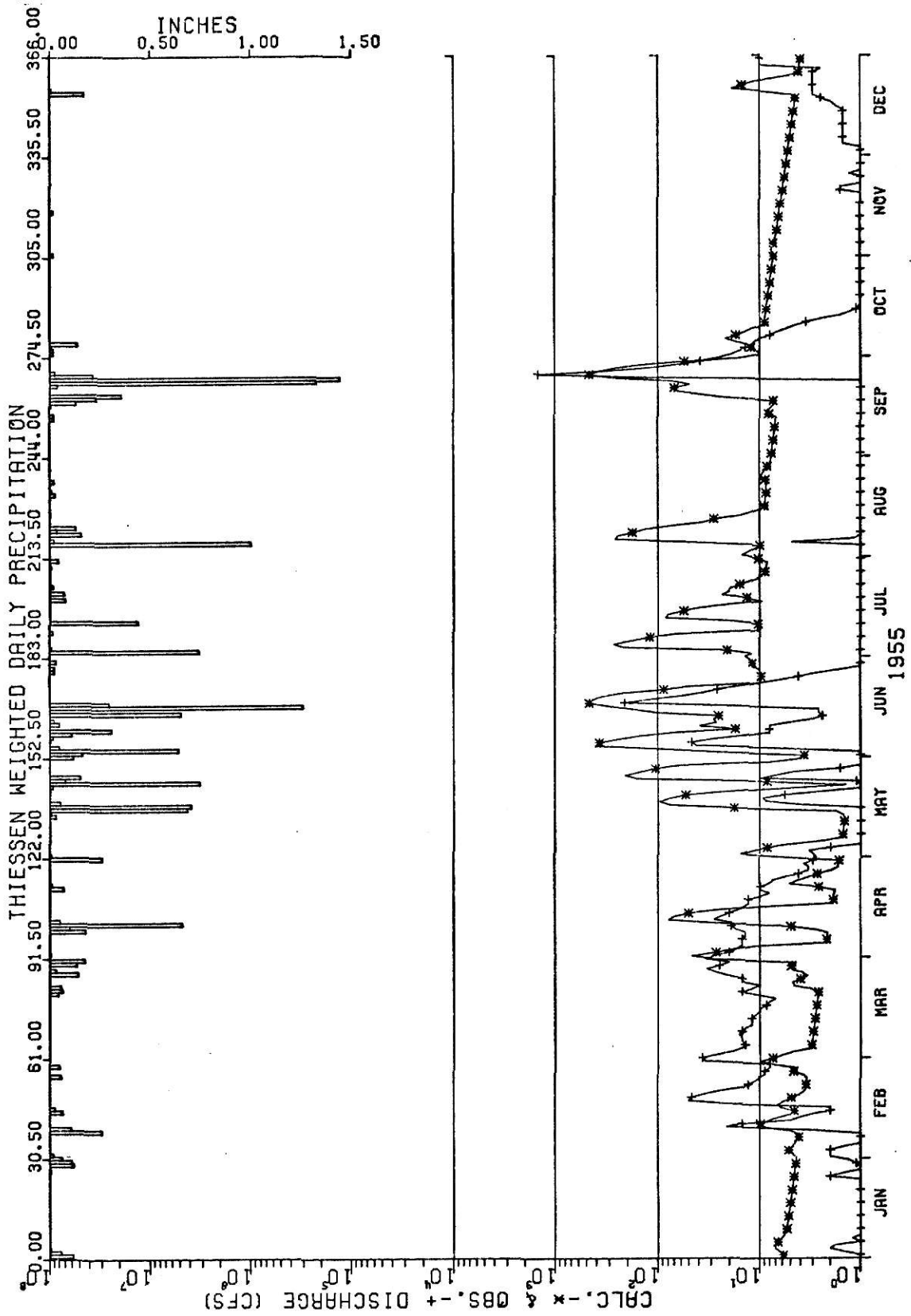


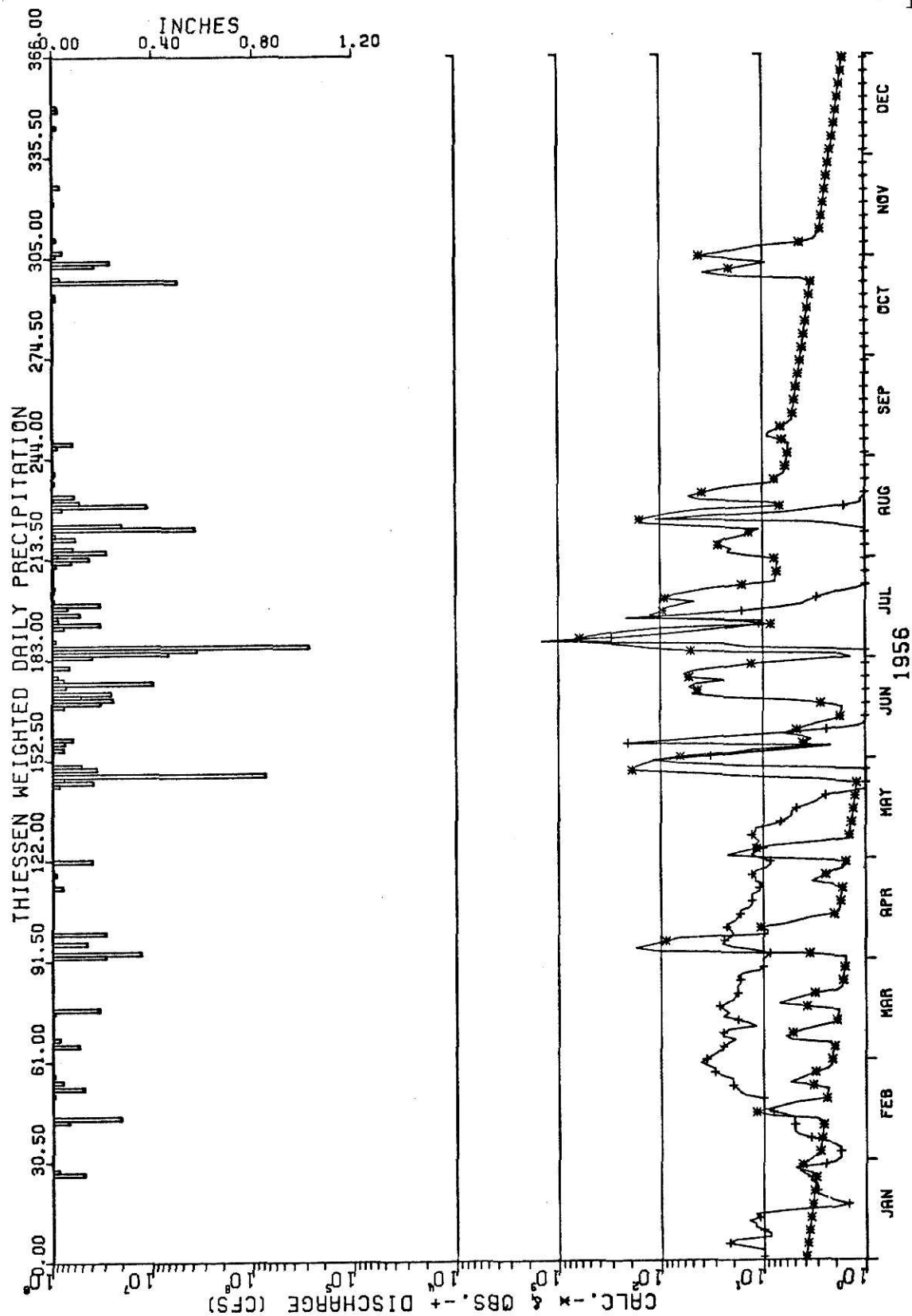


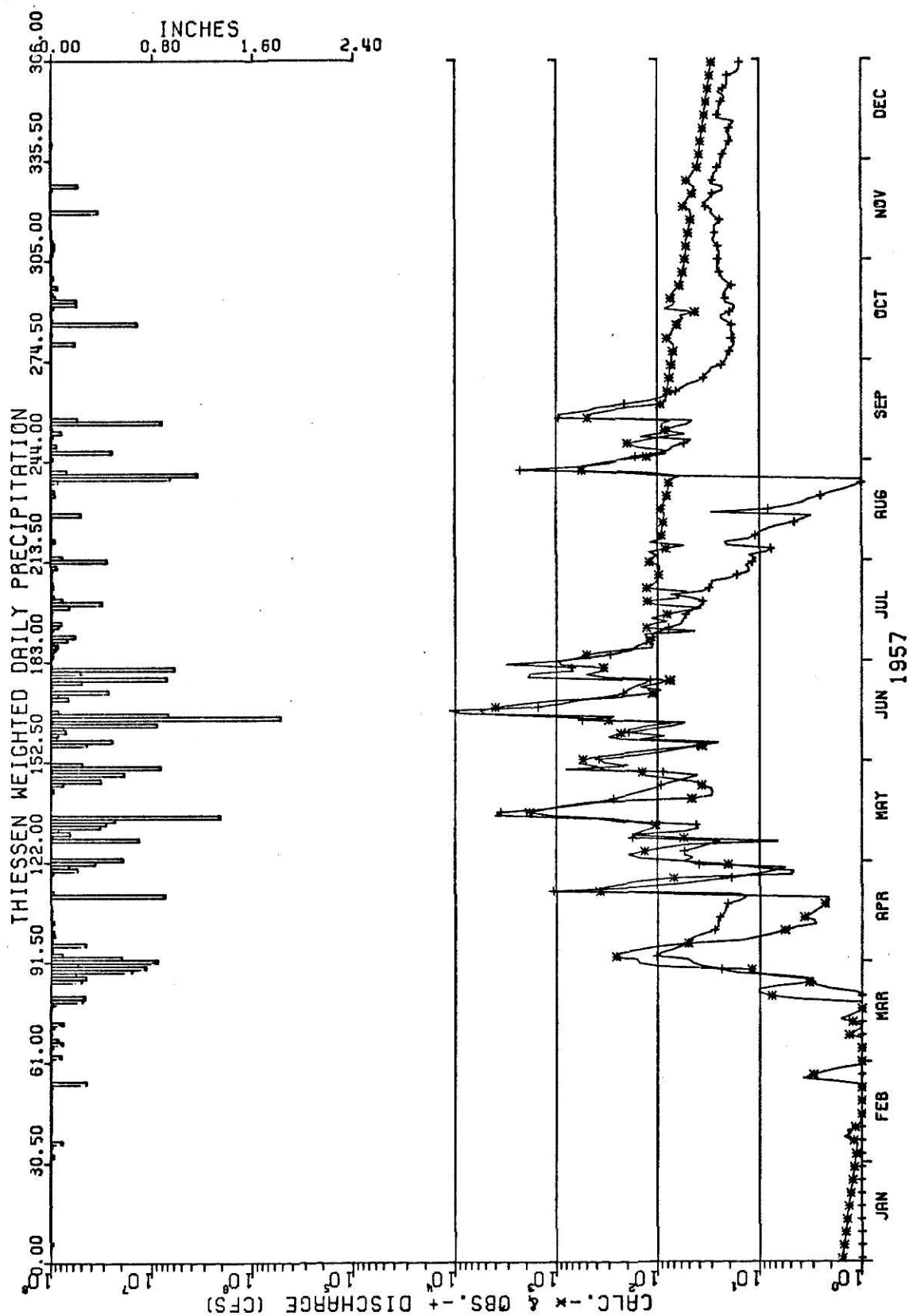


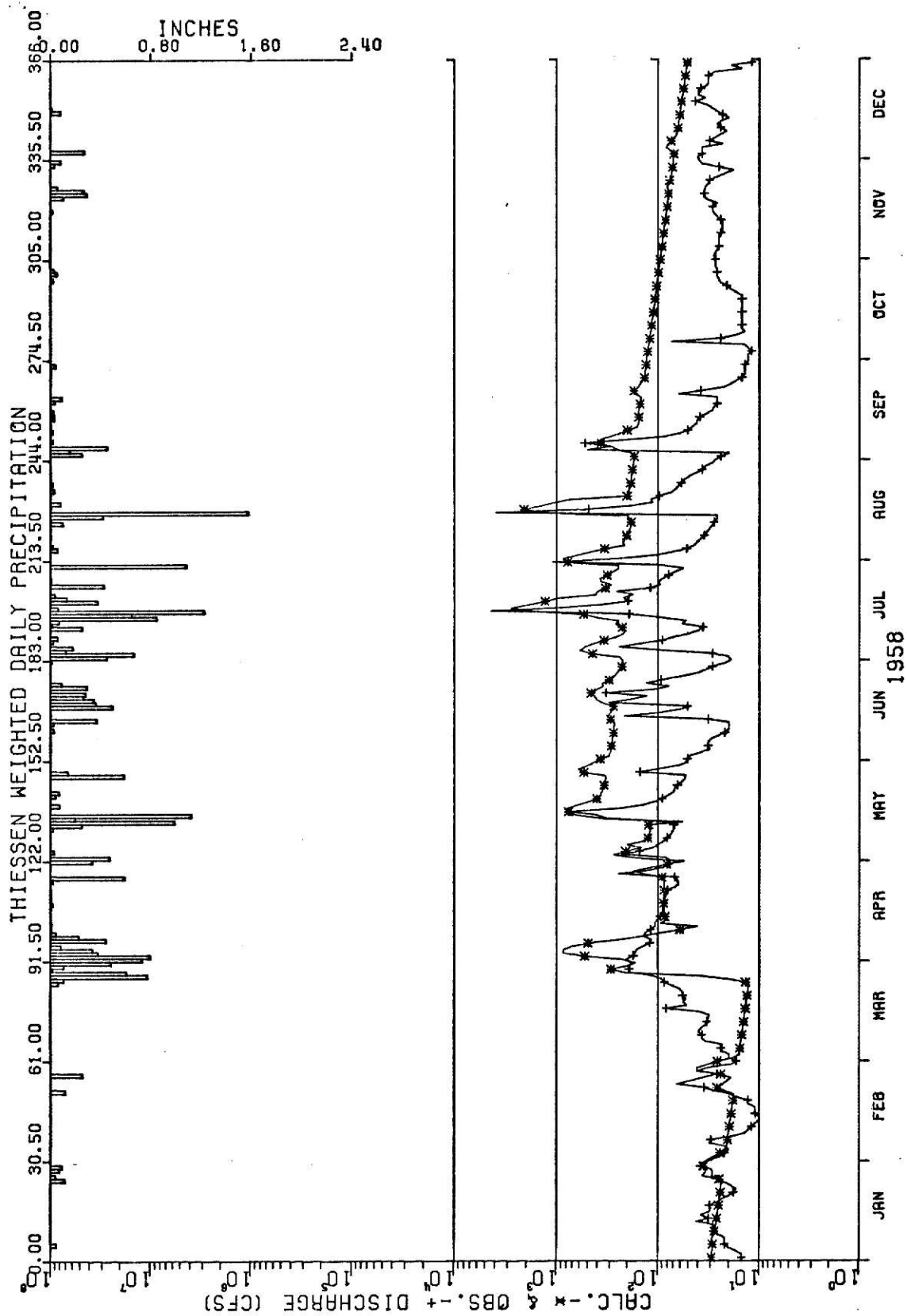


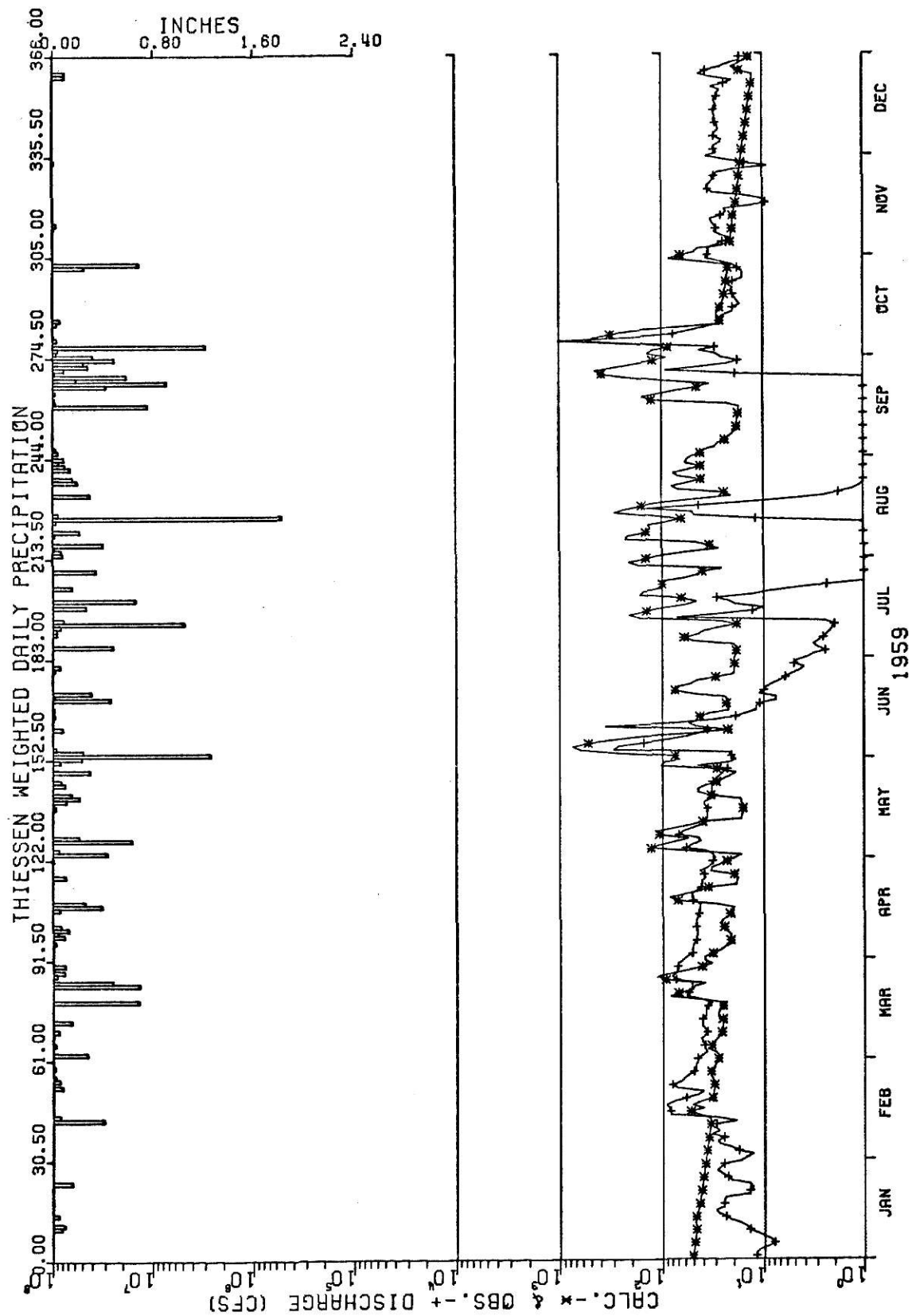


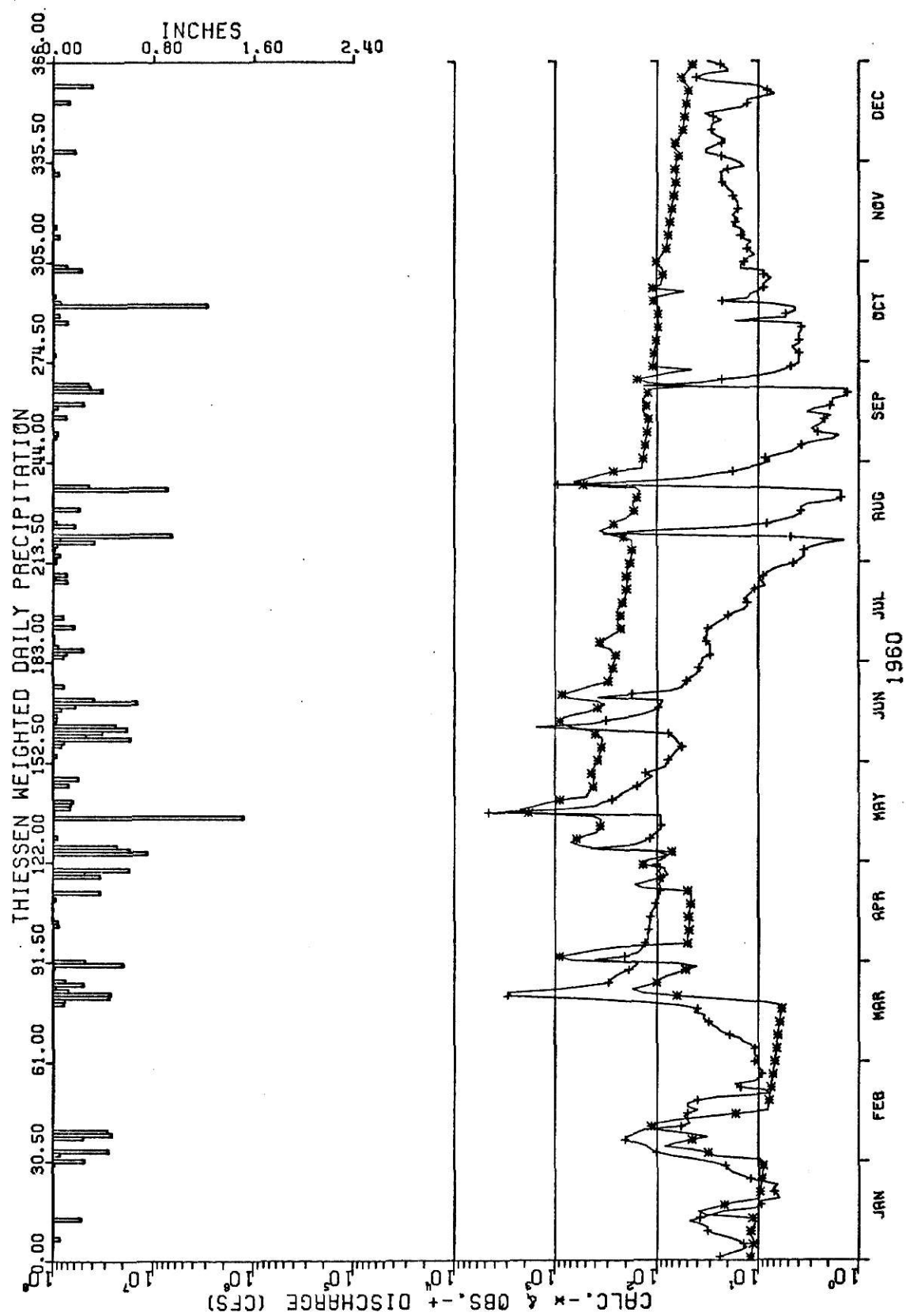


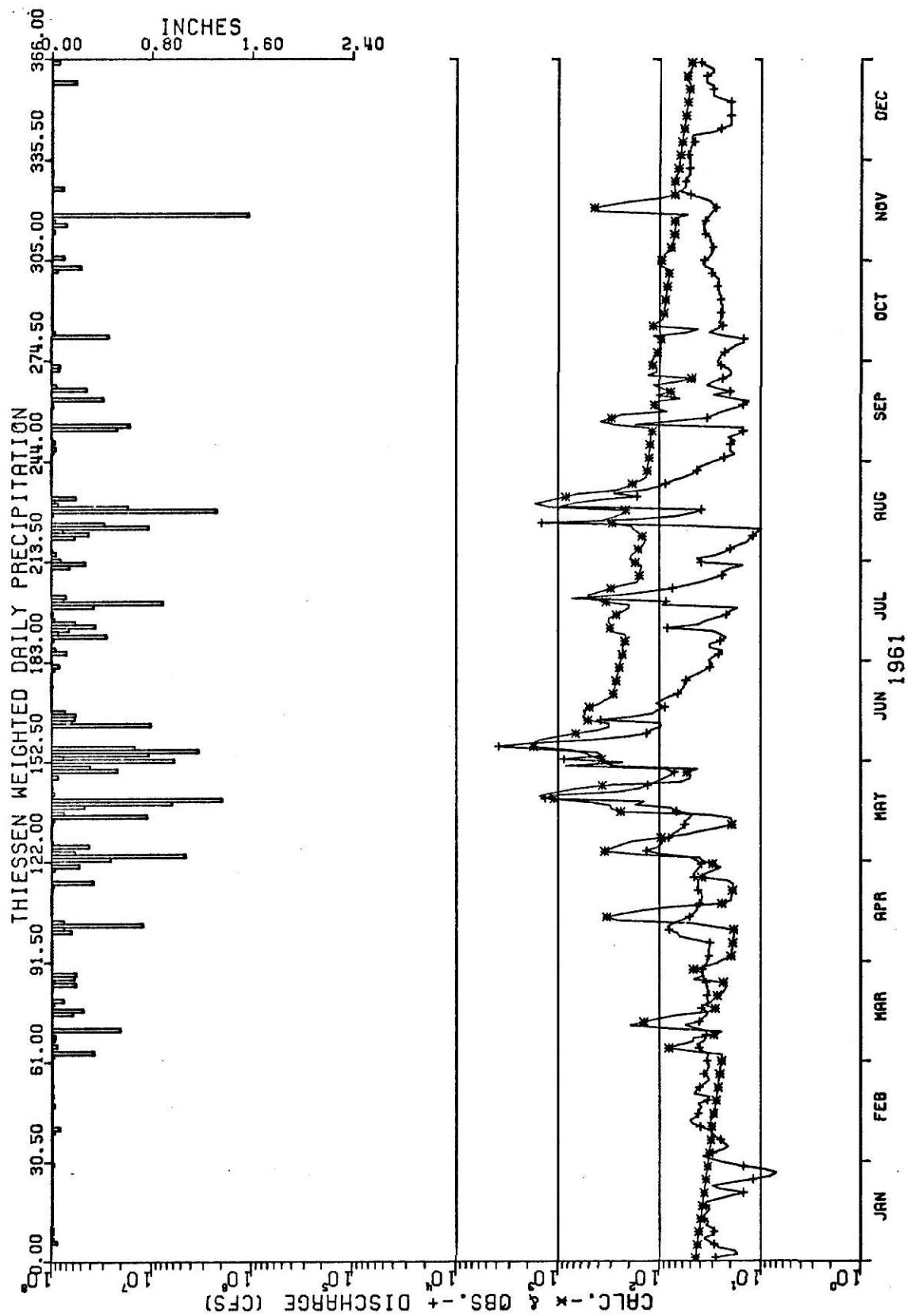




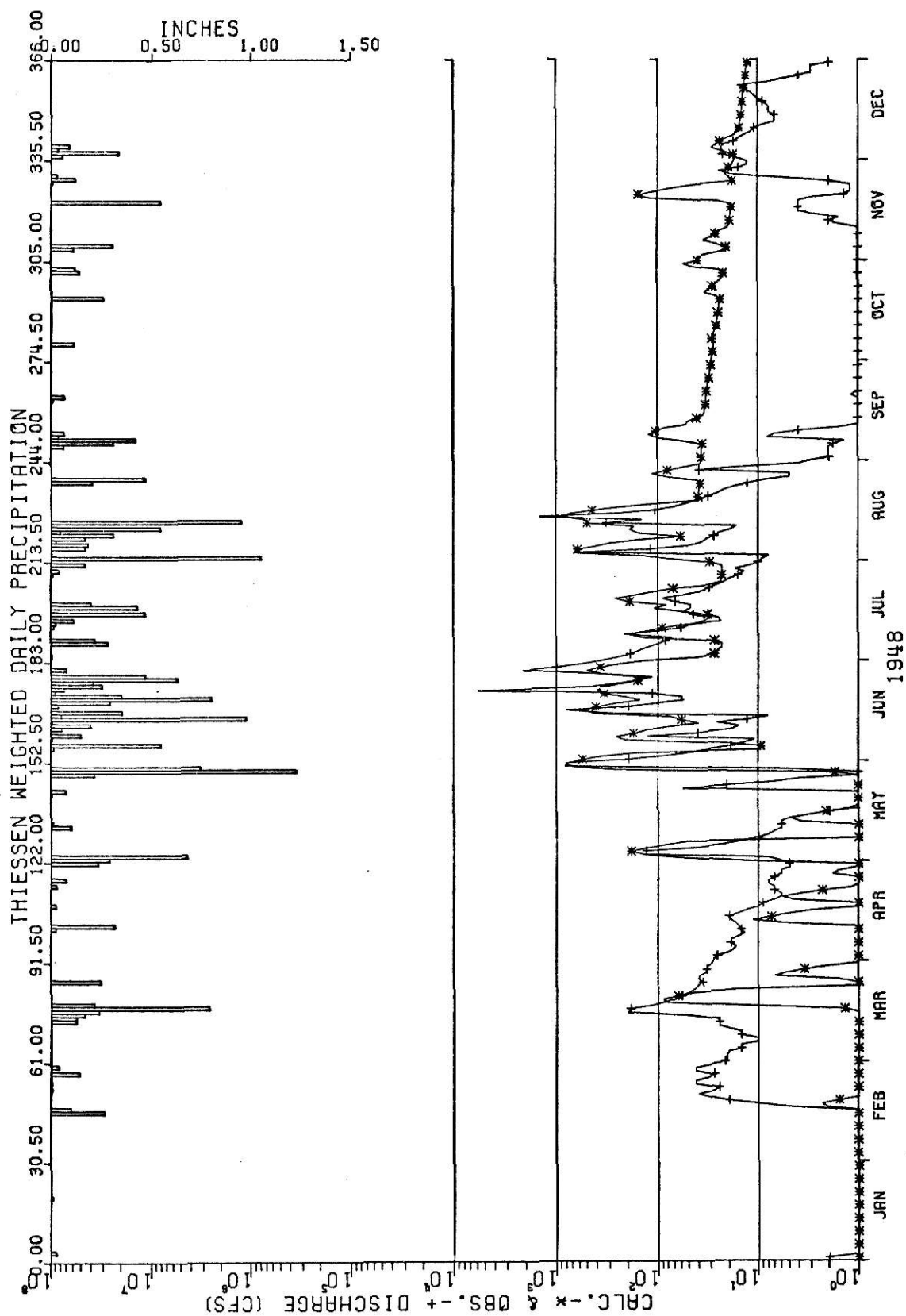


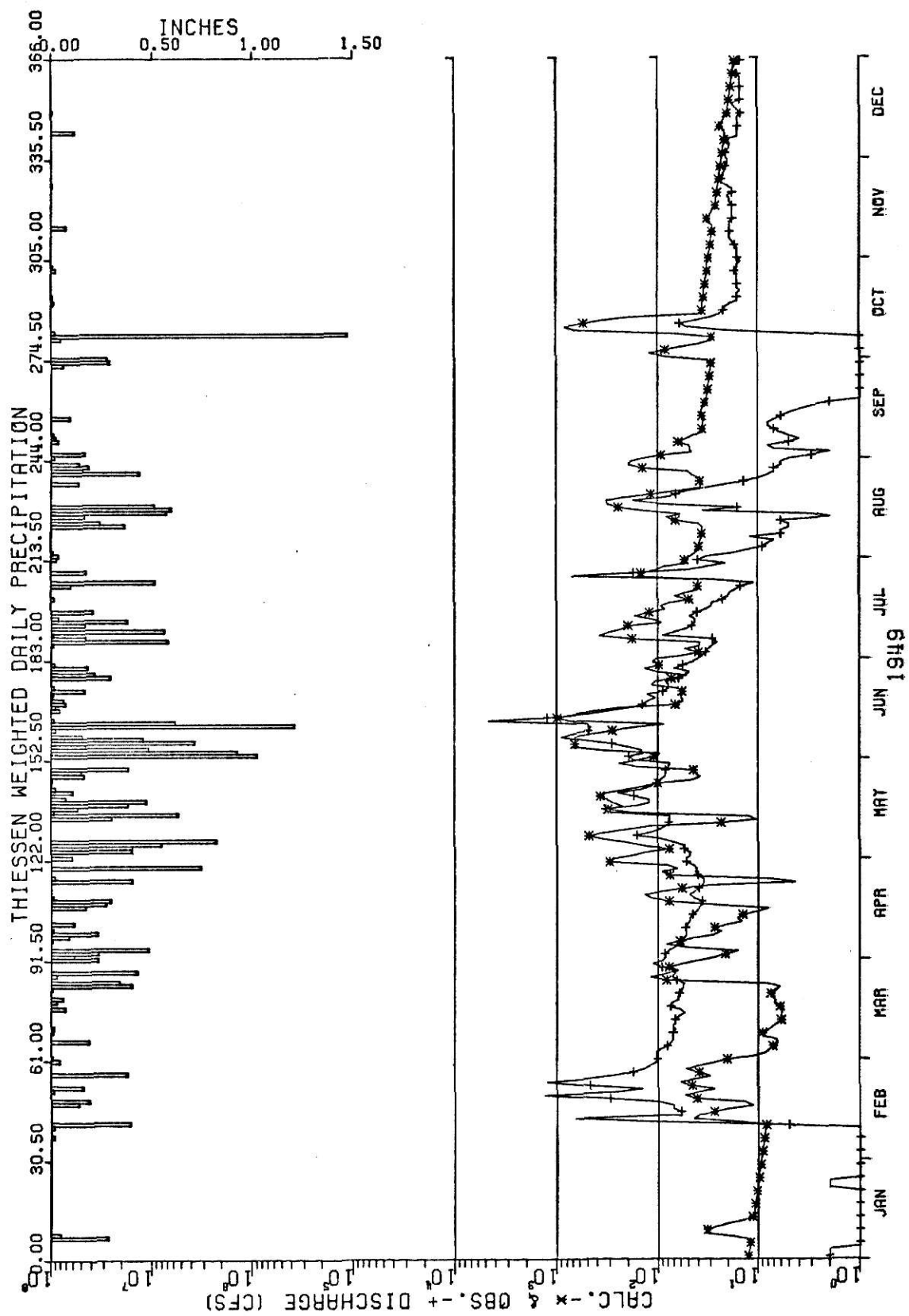


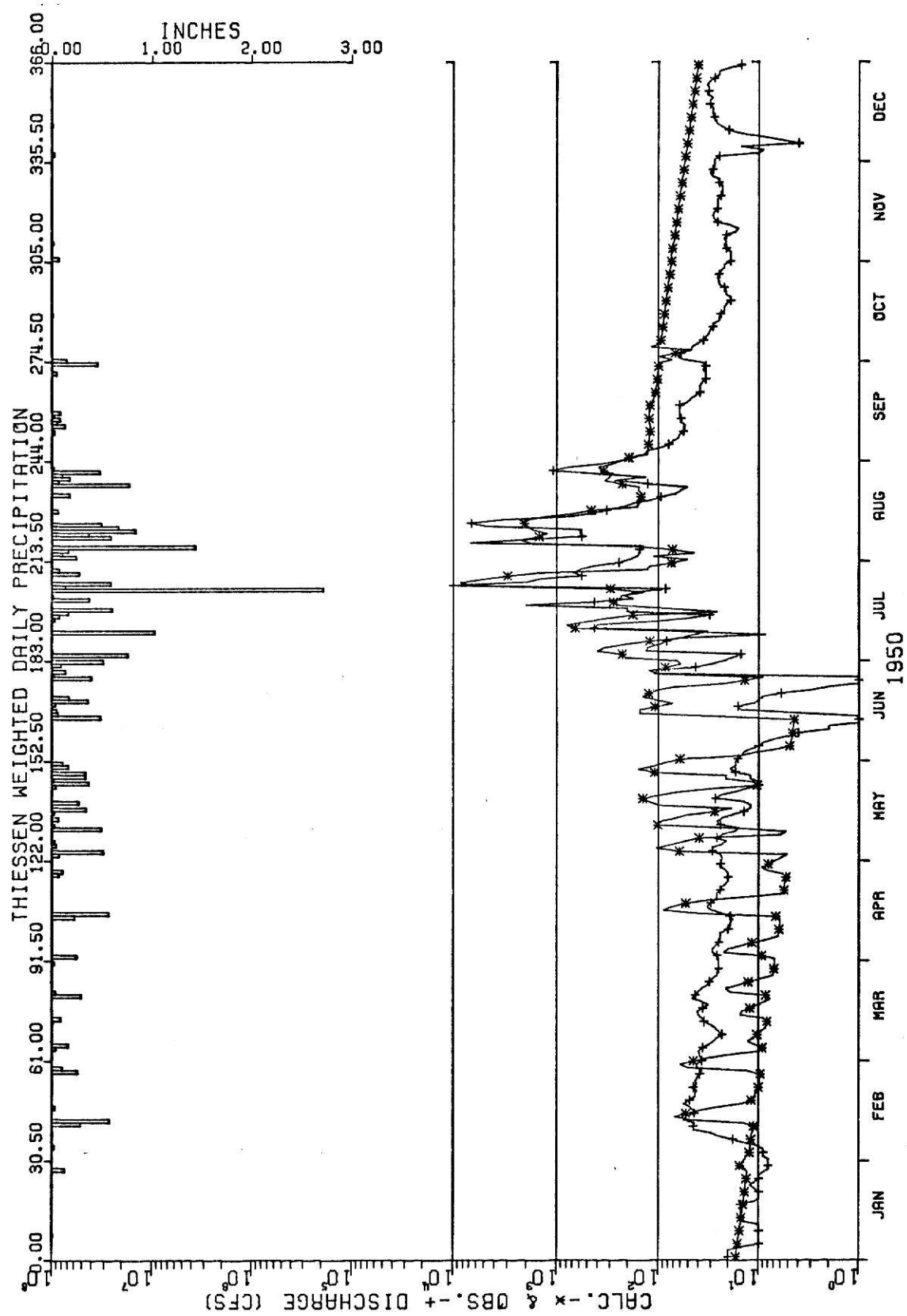


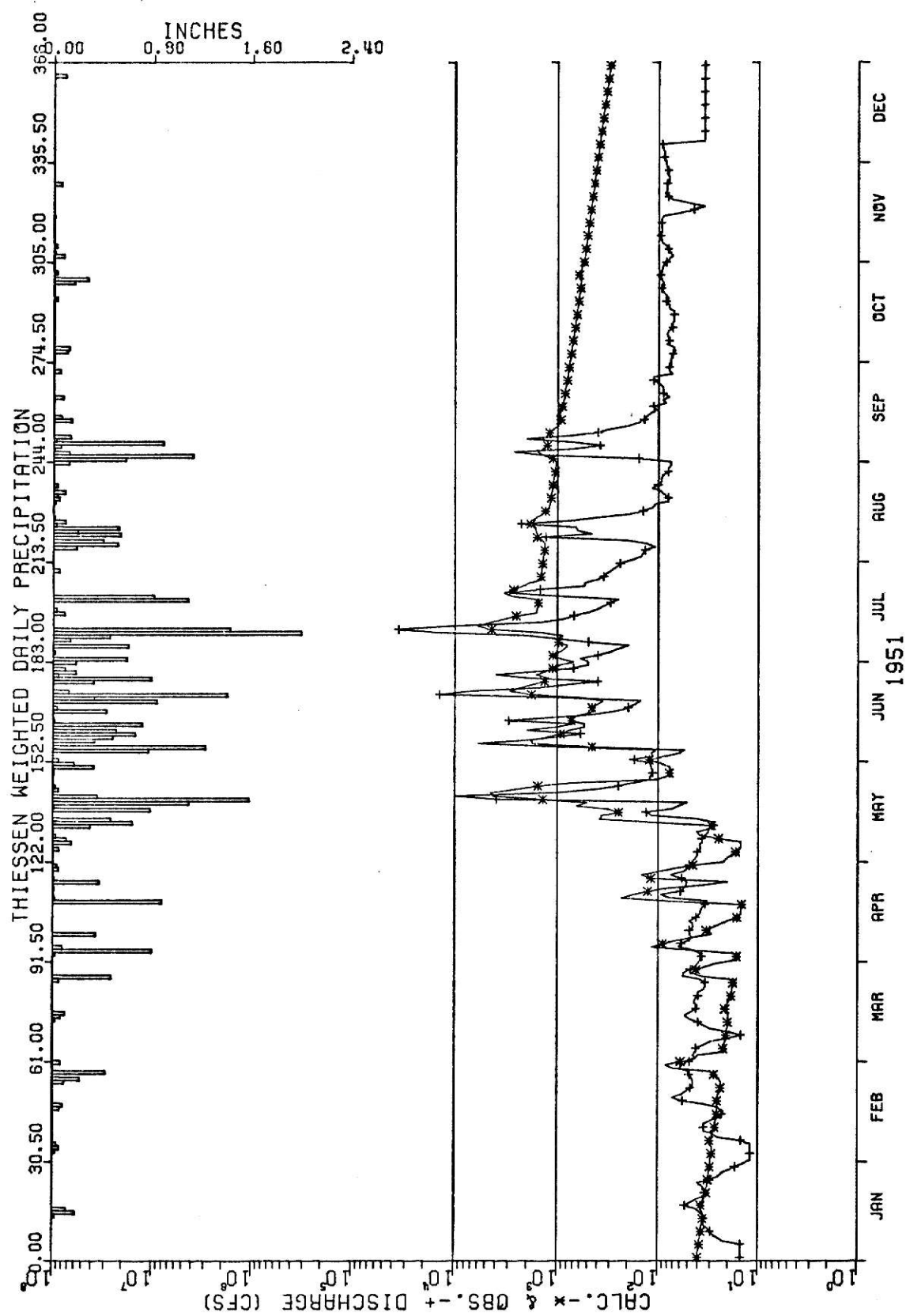


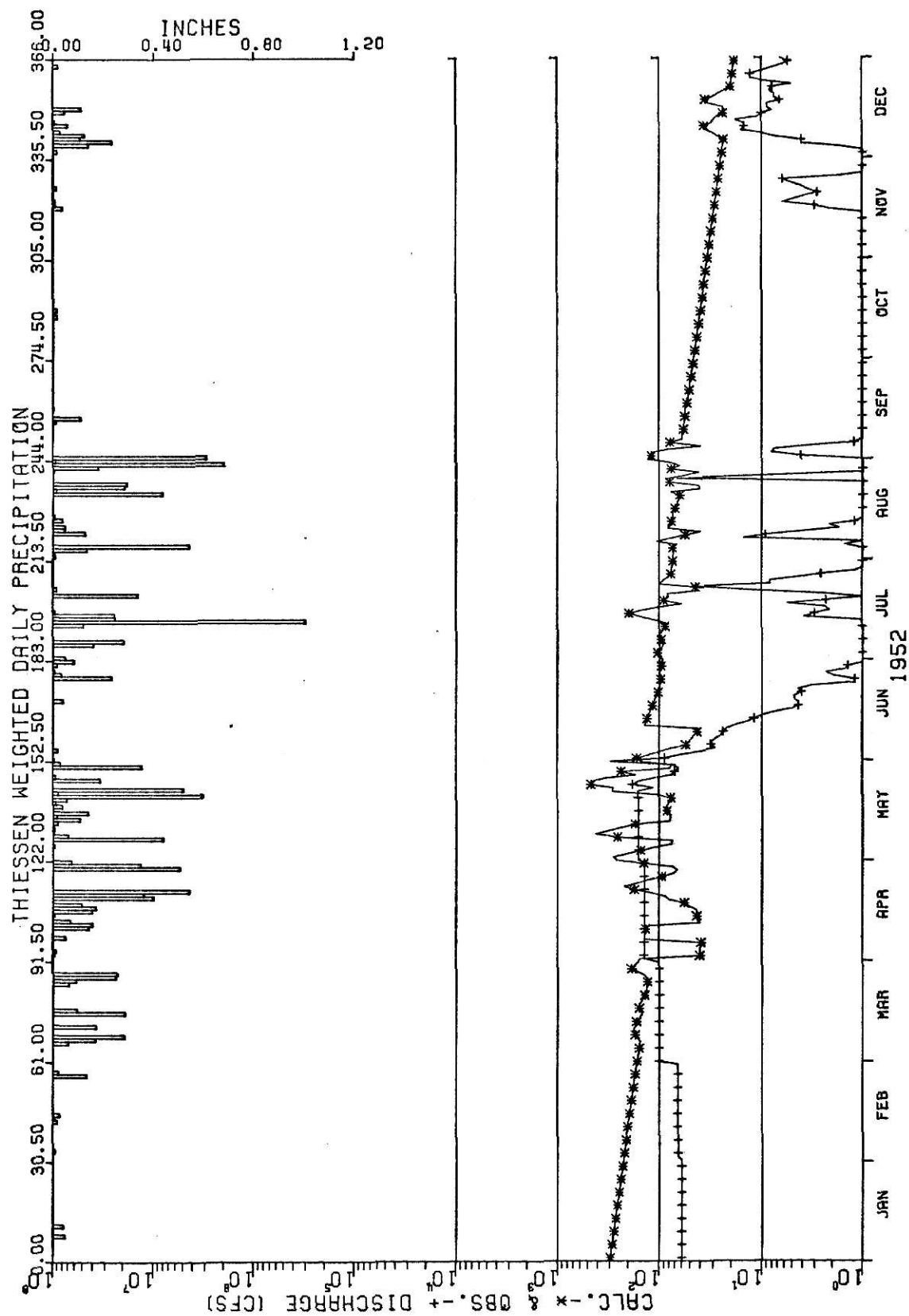
HYDROGRAPHS - MODEL B-TEN

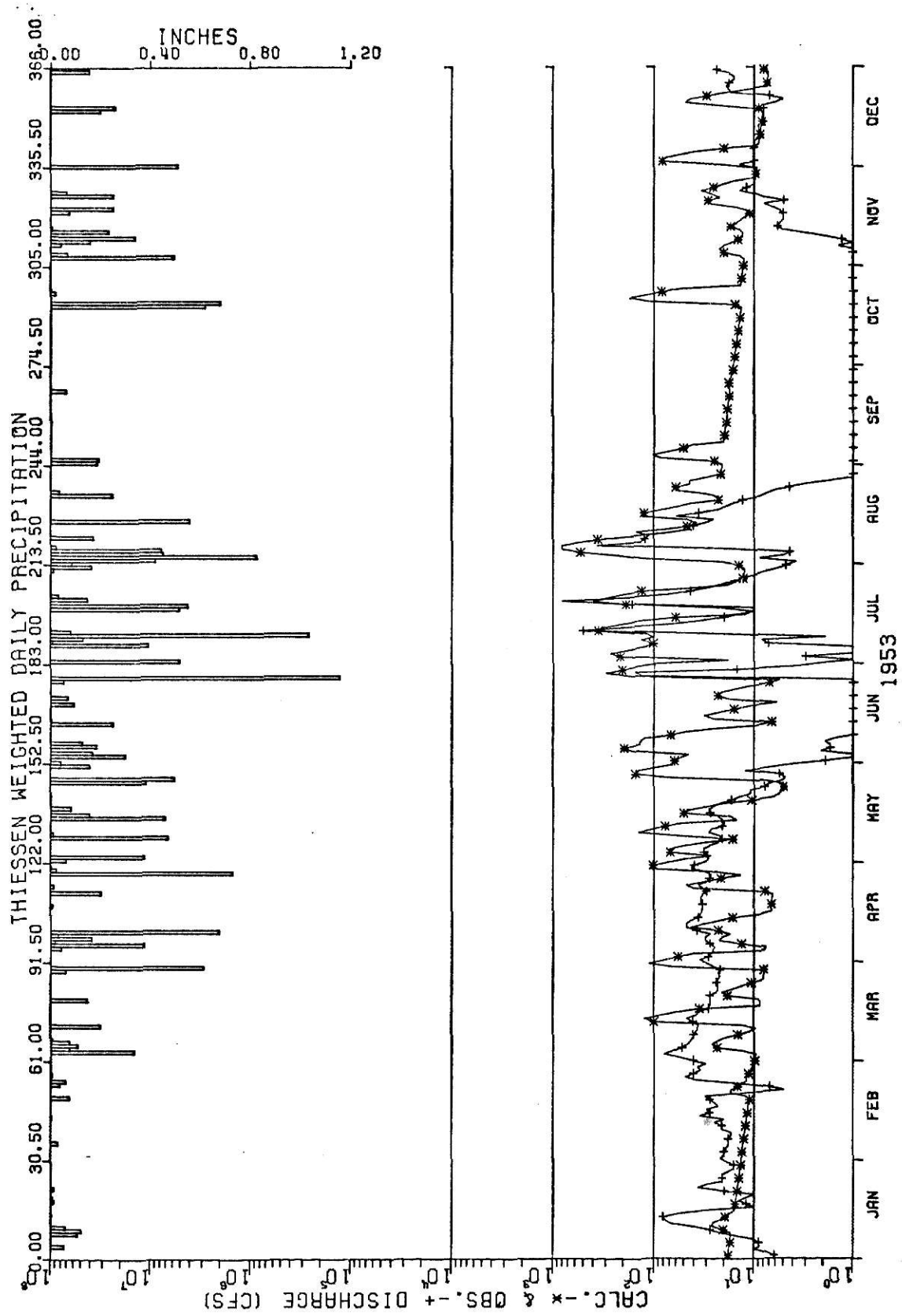


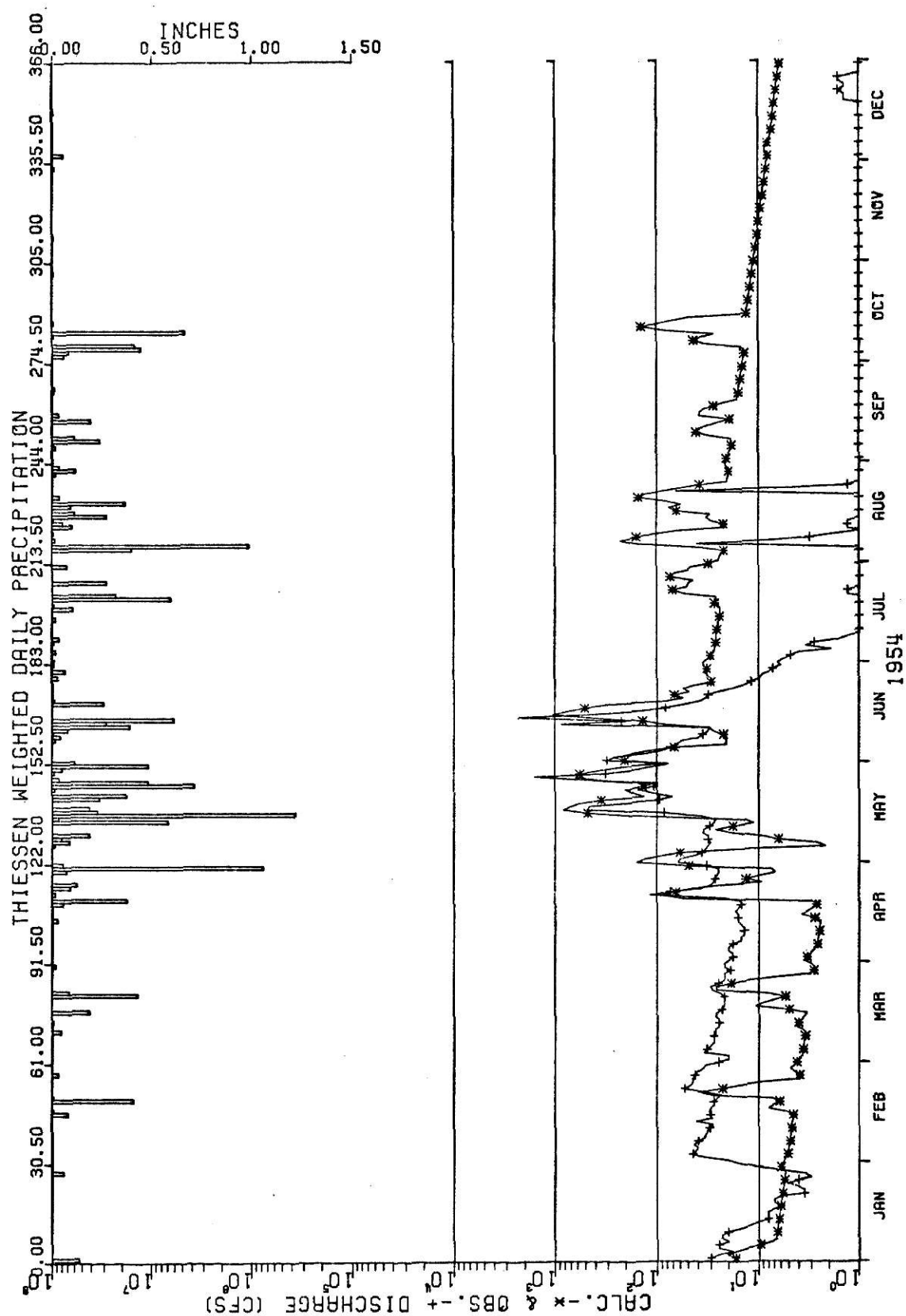


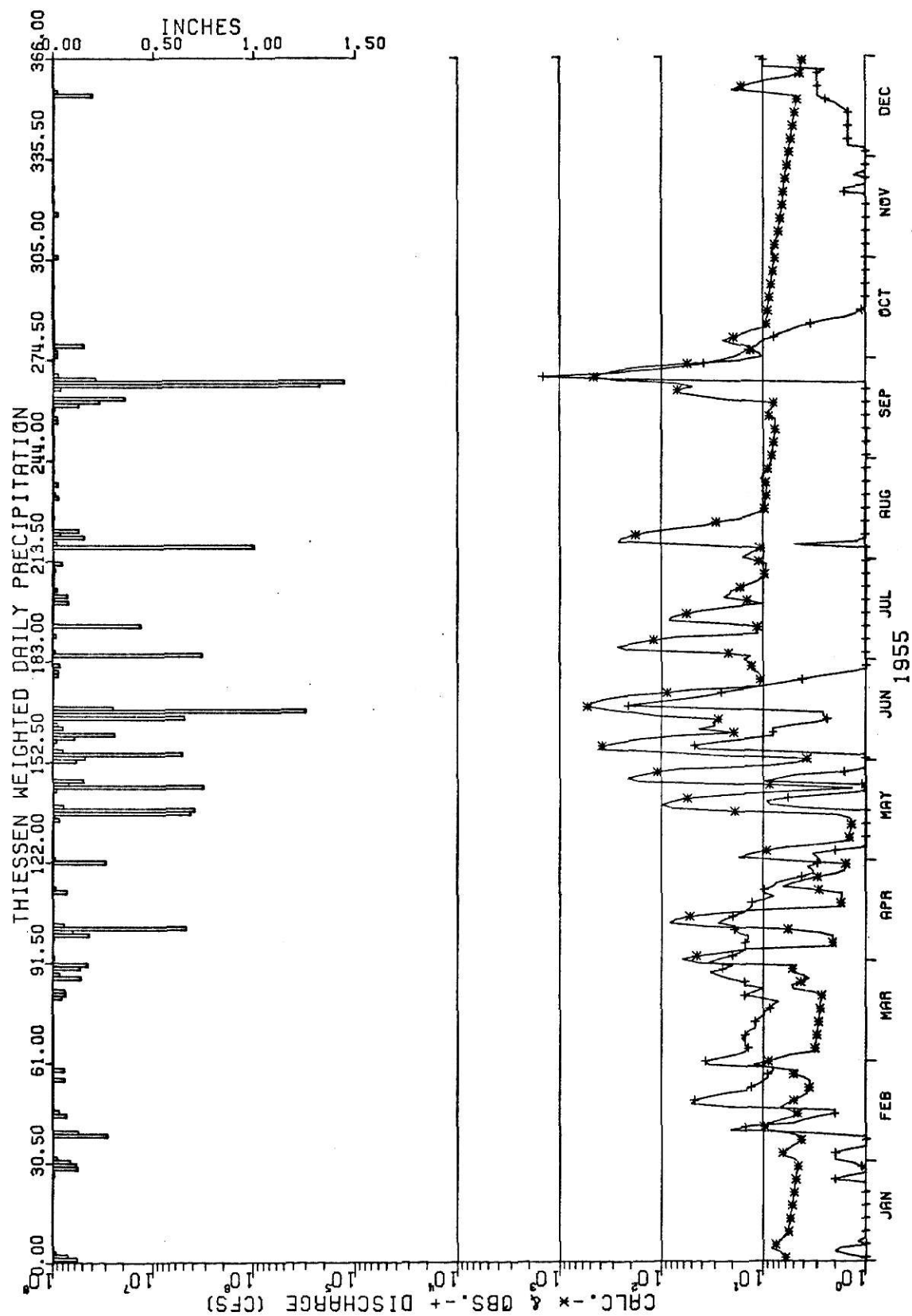


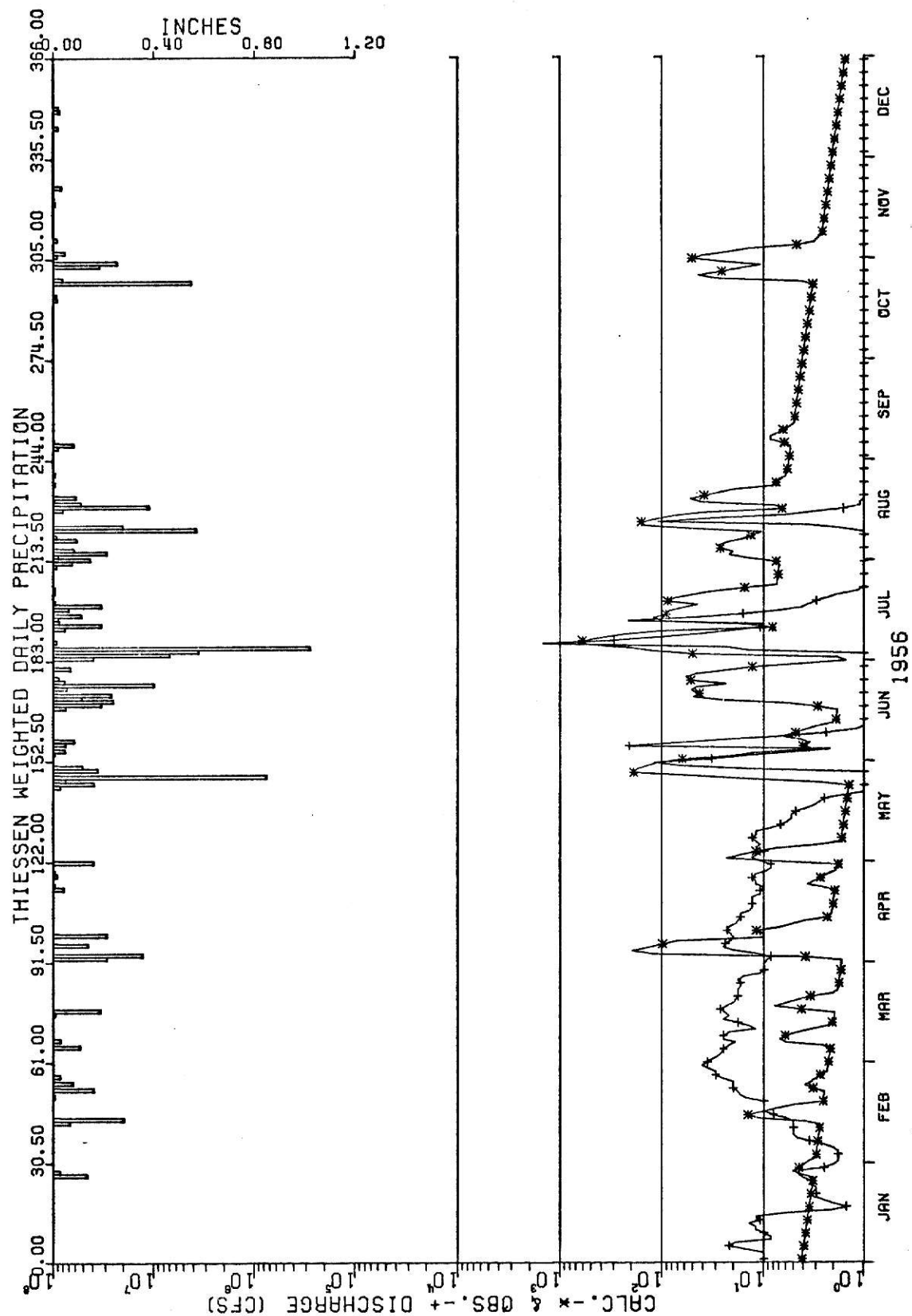


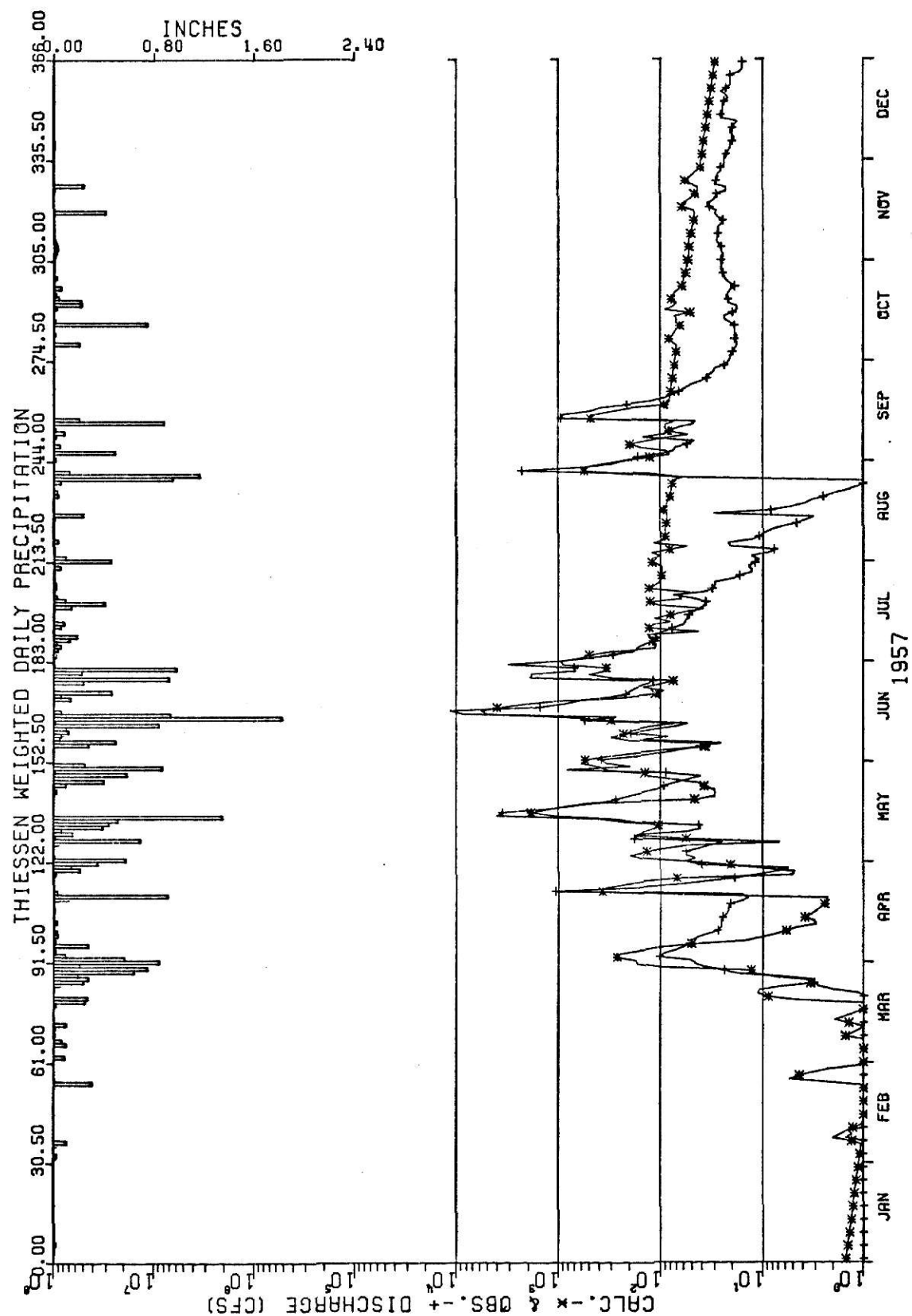


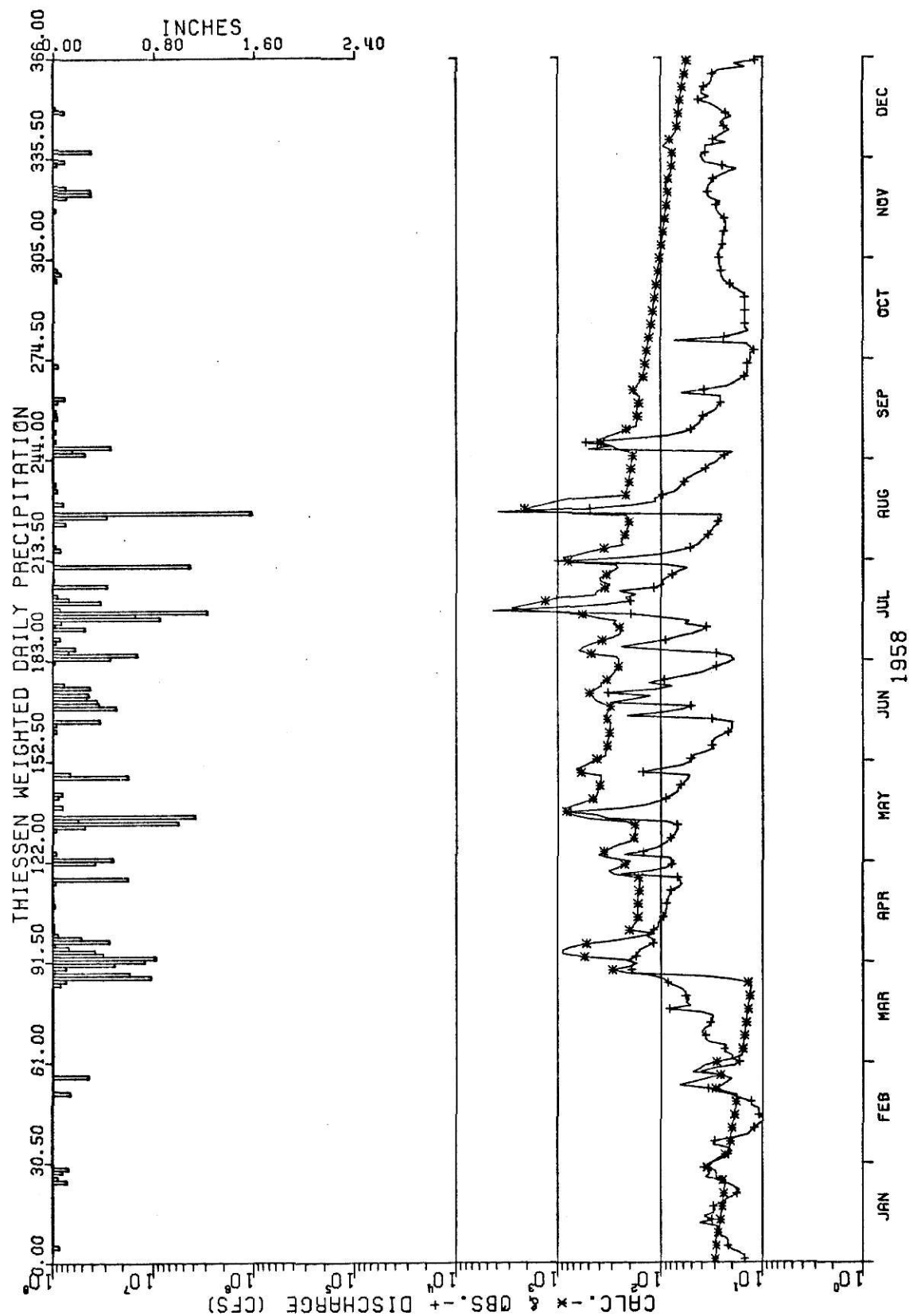


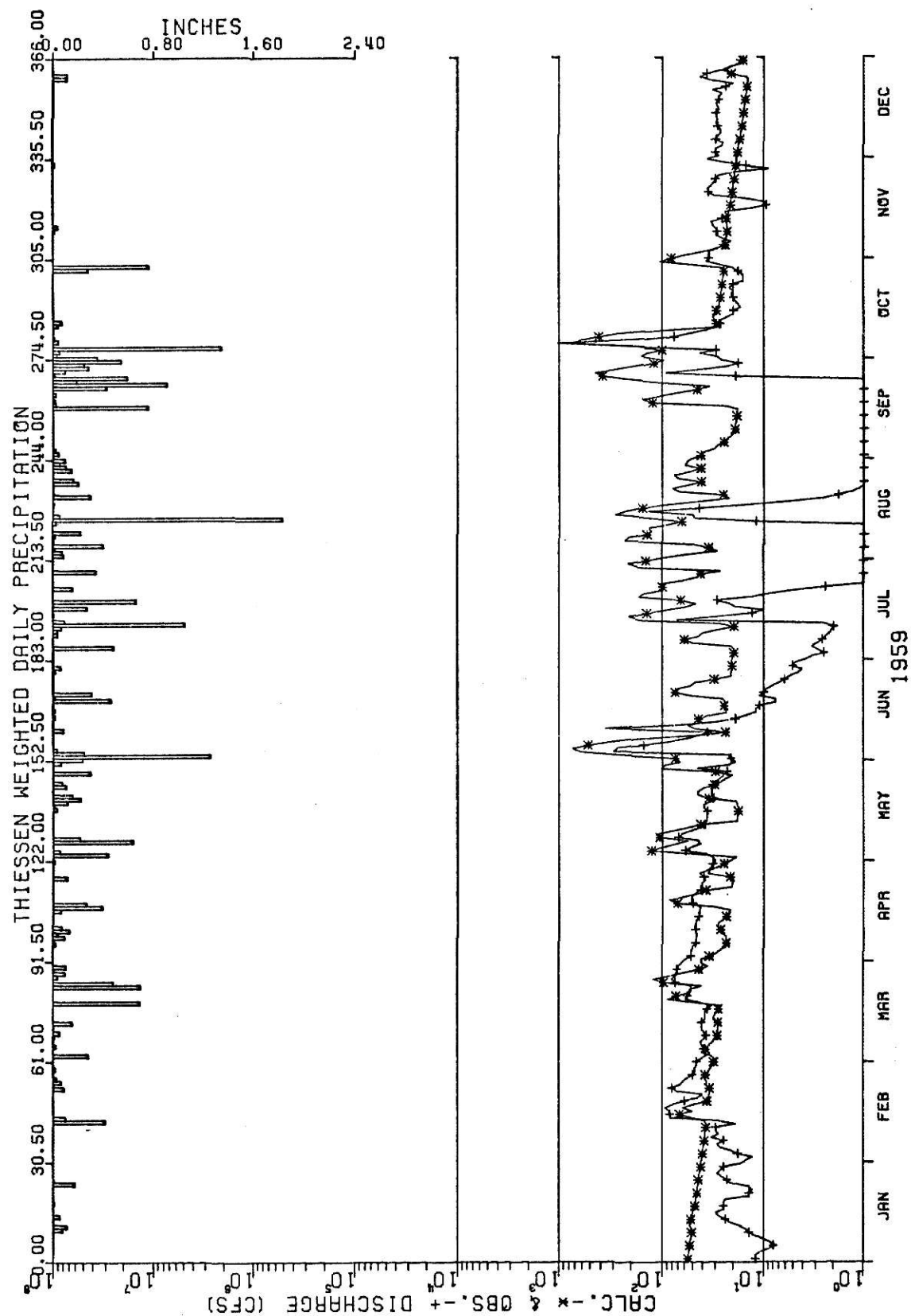


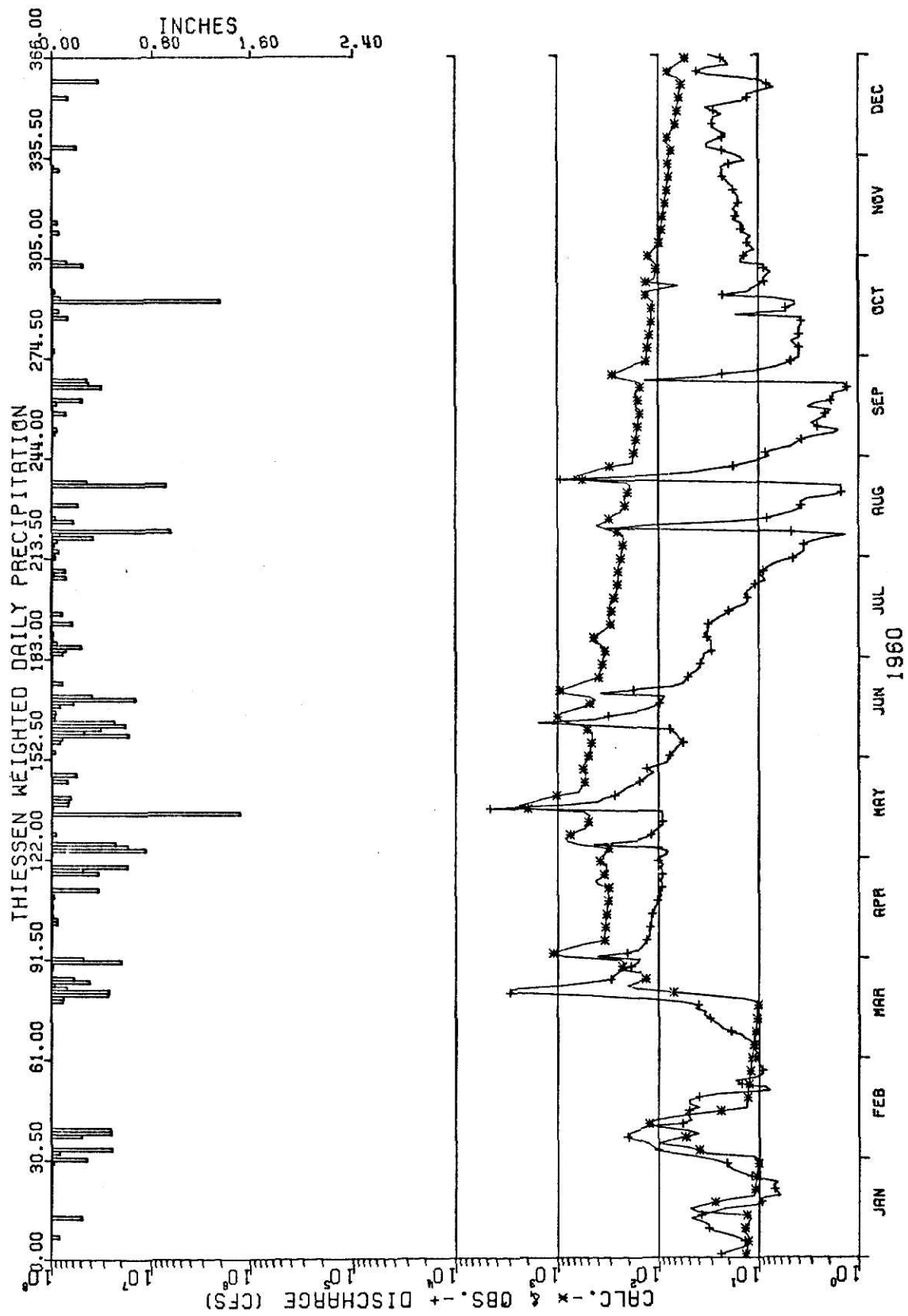


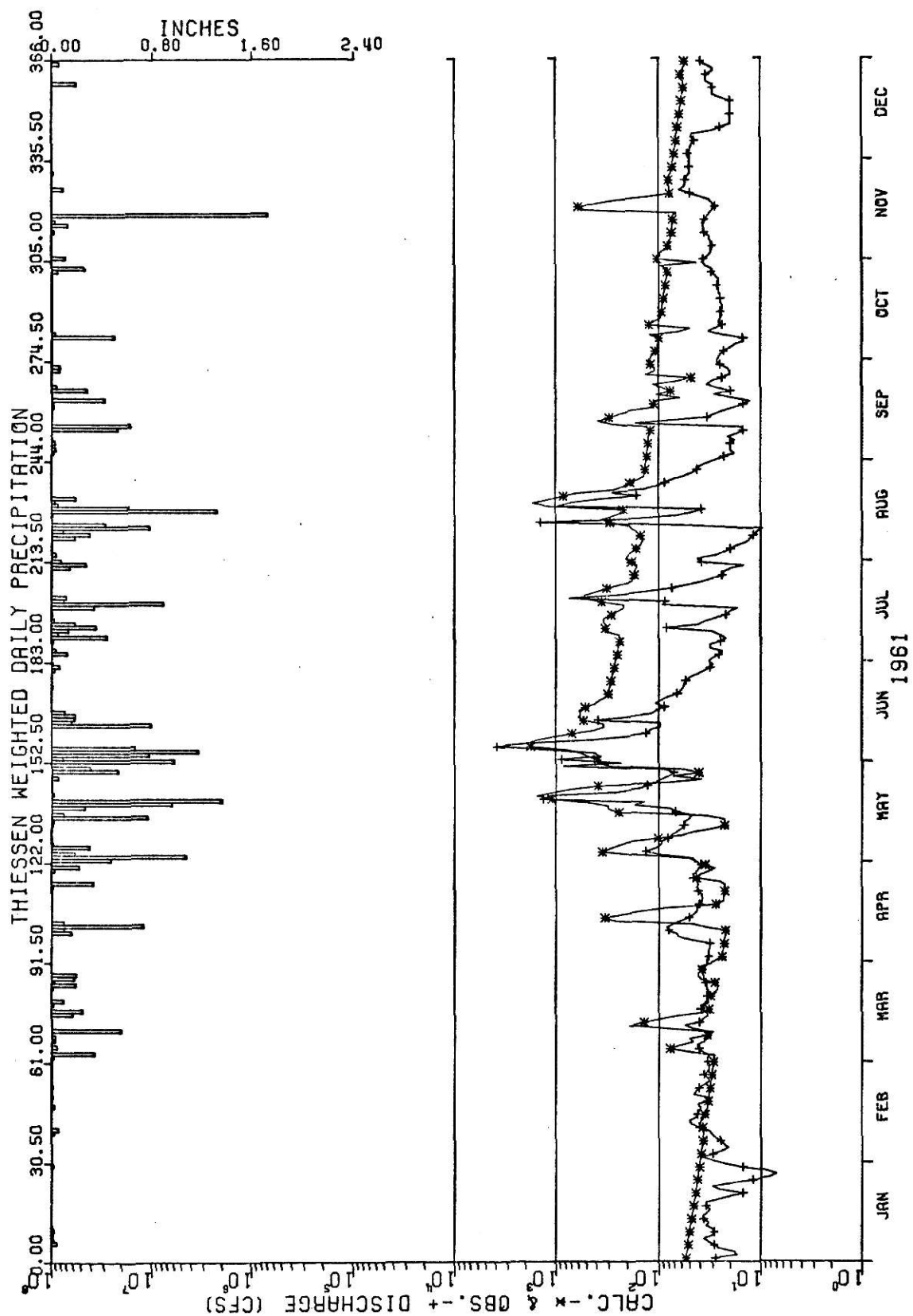












EFFECTS OF PRECIPITATION ENHANCEMENT ON THE HYDROLOGIC
CYCLE FOR THREE KANSAS WATERSHEDS

by

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ABSTRACT

The effect of weather modification on the land phase of the hydrologic cycle, particularly the alteration of stream flow patterns, is the concern of this report. The question of weather modification effects has arisen in recent times, since the technological capability of weather modification is expanding.

The historical records for three Kansas watersheds were obtained. The watersheds in this study were the Black Vermillion, the South Fork Solomon, and the Beaver Creek. These watersheds were studied by calibrating the KSU version of the Kansas Watershed Model to match historical stream flow records. Once calibrated, the precipitation pattern was altered by two modification schemes, B-ZERO and B-TEN. B-ZERO and B-TEN both modify the seven month growing season by the expected average results of full scale modification for different magnitude storms. B-ZERO has no winter time modification, while B-TEN has a uniform percentage increase of winter time precipitation.

The results of the precipitation enhancement for B-ZERO are 6.72, 10.59, 12.67 percent increases for the Black Vermillion, South Fork, and Beaver Creek, respectively. The general result of the increased precipitation is increased runoff and increased evapotranspiration. However, since the modification schemes are representative of actual modification occurrences, large magnitude storms are actually reduced in magnitude and this reduction is sometimes reflected by reduced stream flows.