

DEVELOPMENT OF SUPPLEMENTAL IRRIGATION
SYSTEM MODEL FOR A FARM IN
SOUTHEASTERN KANSAS

by

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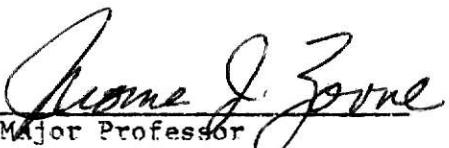
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And, I want to dedicate my thesis to my father-in-law, Dr. Jeong Haeng Lee and my wife.

CHAPTER I

INTRODUCTION

The boundary between sub-humid and sub-arid regions passes through Kansas near the 100° meridian. The southeastern part of Kansas is in the sub-humid region for which sufficient precipitation is received to allow crop production to reach full potential under the condition of proper rainfall distribution over the growing season. However, uncertain and poorly distributed rainfall is nearly always the case. Supplemental irrigation has been practiced to ensure uniform maximum crop yields because rainfall is inadequate in either amount or distribution, or both, in most growing seasons.

Irrigation water may be taken from wells, streams, lakes or springs and transferred to the point of application by pumping or by gravity. In this region, the water source is often surface runoff from a small watershed, while in Western Kansas, groundwater is used as the main source for irrigation. If there is a suitable site on the farm, a surface reservoir can be constructed to store runoff for later use as supplemental irrigation.

Supplemental irrigation systems have often been designed and operated without knowing the reliability of the system. An irrigation system is restricted by various factors such as the site topography, climatology, irrigable land area, watershed size, farm boundary, type of soil and crop, and so on. A continuous watershed hydrologic yield model originally developed by Zovne and Koelliker (1) and modified by Hayden (2) can be used to study the site-specific performance of a supplemental irrigation system. The model allows one to compute a continuous variation

of surface runoff, interception, actual evapotranspiration, soil moisture, groundwater recharge, the flux of water to the pond, and irrigation demand, by using meteorological data and some observations on the soil and crop.

The purpose of this study is to examine the reliability of a pond water supply for irrigation and the possibility of supplemental irrigation on a specified site. By means of a multi-purpose hydrologic simulation model, the complex hydrologic interactions are analyzed. The major considerations in design of a supplemental irrigation system are runoff inputs to the pond, irrigation demands, and pond level fluctuations. To study the hydrologic balance for a pond, the variability of surface runoff yields to the pond in response to precipitation, and irrigation needs are examined, after overall hydrologic characteristics of each component are outlined as a result of a long-term simulation (1948-1970). The reliability of the pond can, thereby, be determined. The probability or risk of not enough water available for this system can be predicted based on the pond level fluctuation and irrigation demand.

In addition, a general method of crop management system adaptable to any typical cropping schedule for Southeastern Kansas is designed.

CHAPTER II

REVIEW OF KANSAS STATE UNIVERSITY
HYDROLOGIC YIELD MODEL (KSUHYDRO)

The objective of this chapter is to review the basic theory and principles incorporated in each component of the hydrologic cycle adopted in a continuous simulation model, which has been developed by Zovne and Koelliker (1), and by Hayden (2).

Evapotranspiration

Transpiration is the loss of water from the stomatal openings in the leaves of plants. When evaluating water loss from a vegetated surface, it is always impossible to separate transpiration and soil surface evaporation. These two mechanisms are combined and called evapotranspiration, being synonymous with the term consumptive use in agronomy. The calculation of irrigation water requirement is based on evapotranspiration both in the planning phase of a project and in the control of water supply at the farm level.

When a vegetated surface is losing water to the atmosphere at a rate unlimited by source of water supply, it is called evapotranspiration potential. If supply water is limited, actual evapotranspiration may be less than the potential.

Several acceptable methods of computing potential and actual evapotranspiration have been developed and used. Bean (3) suggested using the Penman formula for calculating evapotranspiration potential for the simulation model. Penman (4) developed his mathematical expression predicting evapotranspiration from a vegetative cover by using energy balance and mass transfer theory. The mathematical formula, known as

the Penman combination method, was calibrated by Bean and presented as (1),

$$\begin{aligned}
 PET = & 0.039 T_a^{0.673} [(1-r) R_a (0.22 + 0.54 PSUNS) - \\
 & 2.010 \times 10^{-9} T^4 (0.98 - a - b \sqrt{ES \times RHD}) x \\
 & (0.1 + 0.9 PSUNS)] + (1 - 0.039 T_a^{0.673}) x \\
 & 0.26 (e + 0.01 WVD)(ES - ES \times RHD) \quad \text{----- (1)}
 \end{aligned}$$

where

PET = potential evapotranspiration, in inches

Ta = mean daily air temperature, in °F (Fahrenheit)

T = mean daily air temperature, in °K (Absolute)

r = reflectance coefficient (albedo)

Ra = solar radiation, in mm of H₂O

PSUNS = percent sunshine, in percent

ES = saturation vapor pressure of a water surface at
the Ta, in mb

a,b = empirical coefficients, which can vary geographically

RHD = relative humidity, in percent

WVD = wind velocity, in miles/day

e = mass transfer coefficient

The reflectivity of a surface can be measured in the field with an inverted pyrheliometer. Albedo varies with sun altitude and cloud cover. However, in most studies, the albedo of water surface is assumed to be constant of r = 0.05 which can obtain evapotranspiration potential from free water surface, while the albedo for green crops varies from 0.20 to 0.25. The geographic constants of c and d can be determined approximately by using the figure explained by Zovne and

Koelliker (1), and then can be calibrated so that they may reflect the actual case of moisture deficit. Due to the lack of available data on daily basis for the variables Ra, RHD, WVD, and PSUNS, mean monthly values are used by interpolating data from nearby first order weather station, while Ta and T are computed from the daily meteorological records. The saturation vapor pressure of a water surface at the air temperature can be obtained from Equation (2).

$$ES = 33.9 [(0.00738T + 0.8072)^8 - 0.0019 |1.8Ta + 48| + 0.001316] \quad (2)$$

where ES, T, and Ta were previously defined.

The actual evapotranspiration rate is governed by climate, vegetation, and soil factors.

When moisture conditions in soil are suitable, the actual rate of evapotranspiration is equal to the potential for either bare soil or vegetated soil. The most common method to estimate actual evapotranspiration is through the calculation of potential evapotranspiration. If there is enough water in the soil, the two cases are equal. Otherwise, the potential rate is modified according to the amount of water in the soil as following relationship (3),

$$AET = PET \times f\left(\frac{AW}{AWC}\right) \quad (3)$$

where

f = a certain function

AET = actual evapotranspiration

PET = potential evapotranspiration

AW = the available soil moisture

= (soil moisture content - permanent wilting point)
x root profile depth

AWC = available water capacity

$$= (\text{field capacity} - \text{permanent wilting point}) \\ \times \text{root profile depth}$$

The available soil moisture at any time is the amount of water held at a moisture content above the permanent wilting point. The available water capacity is defined as the difference between field capacity and permanent wilting point (6).

The actual rate of evapotranspiration for either bare or vegetated soil is affected by soil and crop type. Evaporation from bare soil differs in two stages (1). First stage evaporation occurs when the soil is sufficiently wet to readily transport water to the soil surface. To estimate the first stage evaporation, Equation (1) is used for the bare soil condition with r equal to 0.20. When a threshold amount, U , is reached, hydraulic properties of the soil begin to limit the evaporation rate. The second stage evaporation from bare soil is computed by following equation (4).

$$E_S = c' t^{\frac{1}{2}} - c' (t-1)^{\frac{1}{2}} \quad (4)$$

where

E_S = soil evaporation, in inches

c' = hydraulic coefficient of the soil, in inches/day $^{\frac{1}{2}}$

t = time after the first stage evaporation, in days

The rate of evapotranspiration of a crop is dependent upon atmospheric, plant, and soil factors. The atmospheric factors are incorporated in the computation of PET by the Penman method. A plant consumptive use factor, K , by Blaney-Criddle method (7) is applied to the modification of PET in accounting for a plant factor.

If a vegetated soil surface is considered, equation (5) is used to calculate evapotranspiration,

$$AET = PET \times K \times AW/0.3 AWC \quad \text{----- (5)}$$

where

AET, PET, AW, and AWC are previously defined,

K = crop consumptive use coefficient.

When the available soil moisture is greater than thirty percent of the maximum available soil moisture, evapotranspiration will occur at the maximum rate of the product of PET and crop consumptive use factor, K. When the soil moisture falls below thirty percent of the maximum available soil moisture, the actual evapotranspiration decreases linearly from the maximum rate to zero at the permanent wilting point.

The crop coefficients, K, in Equation (5) can be determined by Blaney-Criddle method described in SCS, Technical Release No. 21 (7). These coefficients incorporate K_t , a climatic coefficient which is related to the mean air temperature (t) and K_c , a coefficient reflecting stage of crop growth. According to the procedure outlined in (7), Zovne, et al. (1) developed a subroutine CROPCO to simply calculate crop coefficients as monthly average values during the growing season. Inputs to the subroutine are mean monthly air temperature, type of crop, planting, and harvesting date.

The climatic coefficients are estimated by using mean monthly air temperature. The growth stage coefficients are obtained from crop growth stage curves illustrated in (7). However, these curves are internally programmed in the subroutine CROPCO by regression analysis. Each curve has its own third or fourth order polynomial equation. The

crop coefficient (K_{CROP}) is finally generated by the product of K_t and K_c . When the soil lies fallow, or during the dormant season, the K is zero.

Surface Runoff

For a given plot, surface runoff is calculated by the method developed by the U.S. Soil Conservation Service (SCS) (8).

$$Q = \frac{(P - 0.2S)^2}{P + 0.8S} \quad \text{----- (6)}$$

where

Q = surface runoff, in inches

P = precipitation, in inches

S = potential maximum difference between precipitation and runoff, in inches

The initial abstraction, IA, consists of interception, infiltration, and surface detention. The empirical relationship is:

$$IA = 0.2S \quad \text{----- (7)}$$

The unknown parameter S must be established from the soil-cover complex, which relates antecedent moisture conditions, hydrologic soil groups, land use, and conservation practices. For those soil-cover properties, the curve number CN is obtained from Table I for Antecedent Moisture Condition II (AMC II). The maximum potential difference, S , can be evaluated by the equation,

$$S = \frac{1000}{CN} - 10 \quad \text{----- (8)}$$

where

S = maximum potential difference, in inches

CN = runoff curve number

TABLE I ** SCS RUNOFF CURVE NUMBERS FOR AMC II *

Soil Class	Row Crops	Alfalfa	Wheat	Pasture	Fallow
1	86	83	84	80	84
2	86	83	84	80	84
3	82	78	81	74	78
4	82	78	81	74	78
5	75	69	73	61	69
6	75	69	73	61	69
7	75	69	73	61	69
8	75	69	73	61	69
9	75	69	73	61	69
10	75	69	73	61	69
11	75	69	73	61	69
12	65	55	61	39	61

*AMC II - During the growing season, soil moisture in the top 1 ft is between 0.5 and 0.8 of field capacity, or for the non-growing season, 0.6 to 0.9 of field capacity.
 AMC I occurs when soil moisture less than 0.5(0.6) and
 AMC III when soil moisture greater than 0.8(0.9).

** From BEAN(3)

TABLE II ** CROP CODES USED IN THE COMPUTER PROGRAM

Crop	Reference Number
Wheat	1
Grain Sorghum	2
Corn	3
Soybeans	4
Pasture	5
Alfalfa	6
Fallow Soils	7

** From HAYDEN(2)

**TABLE III ** IRRIGATION DESIGN CLASS DESCRIPTIONS FOR SOILS IN THE
DISPOSAL AREA (Kansas Irrigation Guide) (8)**

Irrigation soil class	Profile Depth in cm (ft)	Soil class description
1	90 (3.0)	Deep soils with silt loam or silty clay loam surface layers and slowly to very slowly permeable heavy clay and claypan subsoils.
2	90 (3.0)	Deep soils with silty clay or clay textures throughout. Surface infiltration and subsoil permeability are very slow when the soil is moist. Shrinkage from drying causes extensive cracking, resulting in high infiltration rates until swelling occurs.
3	150 (5.0)	Deep soils with silt loam, loam, clay loam, or silty clay loam surface layers and clay loam, silty clay loam, or silty clay subsoils. Subsoil permeability is slow to moderately slow. Shrinkage cracks resulting from drying in the soils with more clayey subsoil textures give a relatively high initial infiltration rate.
4	75 (2.5)	Moderately deep soils with silt loam, clay loam, or silty clay loam surface layers and clay loam or silty clay subsoils with predominantly moderately slow permeability.
5	150 (5.0)	Deep soils with silt loam, loam, clay loam, or silty clay loam surface layers and subsoils. Subsoil permeability: moderate to moderately slow
6	90 (3.0)	Moderately deep soils with silt loam or loam surface layers and loam, clay loam, or silty clay subsoils with moderate to moderately slow permeability.
7	150 (5.0)	Deep soils with silt loam, loam or very fine sandy loam surface layers and moderately permeable, medium textured subsoils.
8	75 (2.5)	Moderately deep soils with silt clay loam, loam or very fine sandy loam surface layers and moderately permeable clay loam, loam, or silt loam subsoils.
9	150 (5.0)	Deep soils with fine sandy loam and loam surface layers and subsoils that have moderately rapid permeability. Available water capacity is moderate to low.
10	150 (5.0)	Soils are moderately deep over sand with sandy loam to loam surface layers and moderately rapid to rapidly permeable subsoils with low available water capacity.

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CUSTOMER.**

Irrigation soil class	Profile Depth in cm (ft)	Soil class description
11	150 (5.0)	Deep soils with loamy fine sand or loamy sand surface layers and moderately rapid to rapidly permeable subsoils.
12	150 (5.0)	Deep rapidly permeable soils with sand or fine sand textures throughout.

** FROM BEAN (3)

For user convenience input CN'S shown in Table I are arranged by the crop and soil types introduced in Table II and Table III, respectively. The input CN is based on antecedent moisture condition (AMC II) two. The CN is modified for other moisture conditions (see footnote, Table I).

For AMC I,

$$CN_I = CN \times 0.39 \times e^{(0.009 \times CN)}, \quad (9)$$

and for the AMC III,

$$CN_{III} = CN \times 1.95 \times e^{(-0.00663 \times CN)}. \quad (9a)$$

Interception

All the precipitation does not reach the soil to supply plants or generate surface runoff. A certain part of the precipitation is intercepted by vegetation or other cover and is evaporated back to the atmosphere. The amount of interception depends on the nature of the surface cover, the characteristics of the rainfall. Many different kinds of interception measurement have been developed. However, for convenience in computer simulation, Bean (3) suggested using an interception-storage capacity of 2.54 mm (0.1 inch), which is evaporated at the free potential rate. The maximum amount of water stored on the wetted surface of the vegetation is called interception storage capacity. The amount of infiltration into soil is assumed to be the remainder of the maximum potential difference (S) which is not evaporated and intercepted.

Infiltration and Redistribution

Infiltration is the movement of water into the soil. Infiltration involves three interdependent processes; entry through the soil surface, storage within the soil, and transmission through the soil profile.

Bean (3) assumed that root zone is composed of two layers; the upper zone is 30 cm (one foot) thick and the lower zone is 90 cm (three feet) thick, as shown in part (a) of Figure 1. Infiltrated water would fill each layer to ninety percent of maximum storage in saturated condition and then any excess would be redistributed to the next layer by gravitational force. Since field capacity is generally defined to be a soil moisture content evaluated two days after saturation (9), the soil moisture of the upper zone is decreased to field capacity in two days, redistributing the excess moisture to the lower zone. Furthermore, if the soil moisture of the lower zone exceeds field capacity, it is decreased to ninety percent of field capacity in two days and the excess is considered to percolate out of the root zone. In this concept of moisture redistribution, the upward movement of water was neglected, but reasonable estimates of vertical movement of infiltrating water can be obtained.

Along with Bean's method, Hayden (2) developed another version of soil moisture movement by using Darcy Equation for one-dimensional flow.

$$q' = K\Delta t i \quad \text{----- (10)}$$

where

q' = volume of water movement per unit area, in inches

K = hydraulic conductivity, in inches/day

Δt = time increment, in days

i = hydraulic gradient, in feet/feet

The hydraulic conductivity, which can be evaluated from laboratory test, is a function of the water content in the soil. The value of

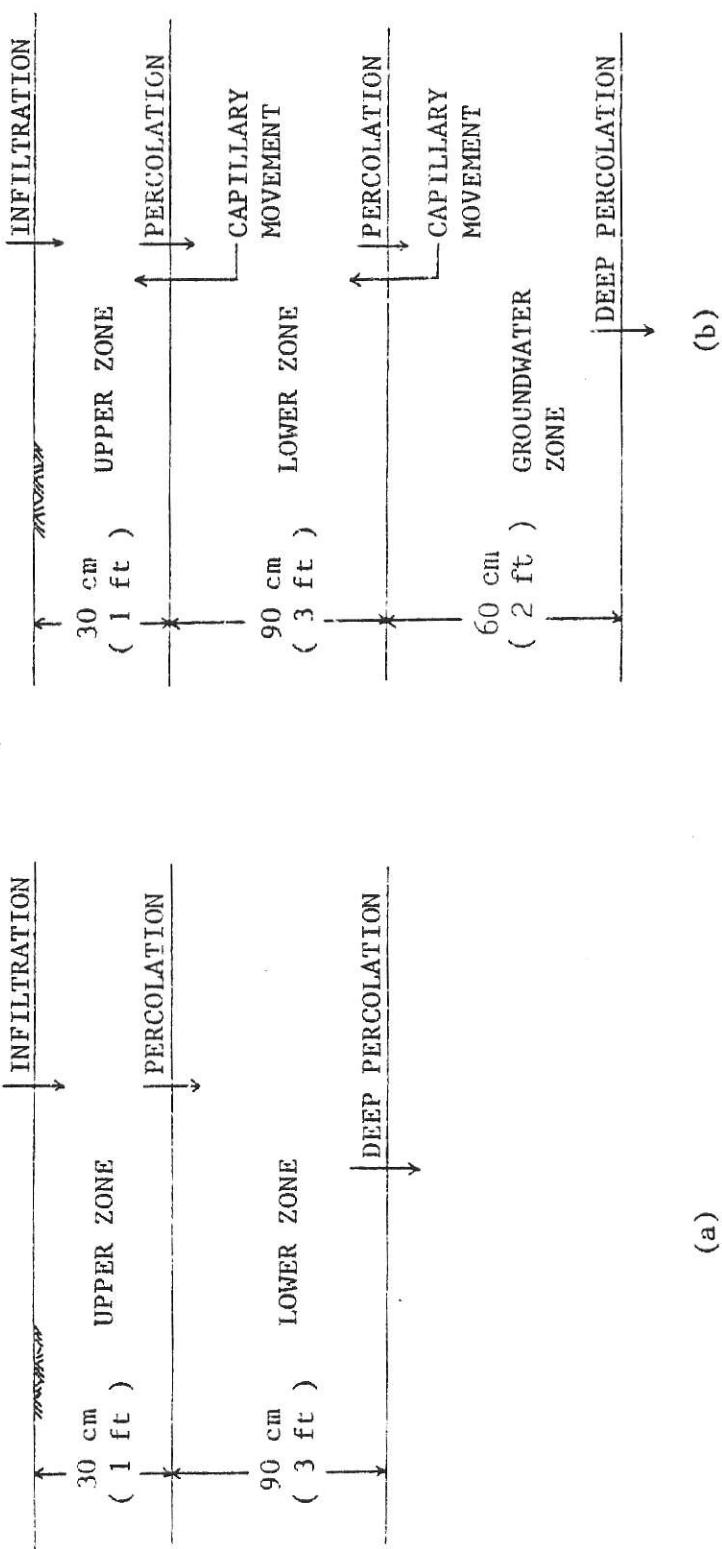


Figure 1. Schematic View of The Subsurface Profile

** From HAYDEN (2)

hydraulic conductivity is maximum potential at saturation. As water content in the soil decreases, its value decreases steeply.

The hydraulic gradient is the sum of the gravitational gradient and the soil water potential,

$$i = \frac{\Delta z + \Delta h}{\Delta z} \quad \text{--- (11)}$$

where

Δz = change in elevation, in feet

Δh = change in soil water potential over distance Δz , in feet

i = hydraulic gradient

For the downward movement of water in soil, the value of the soil water potential is positive. For the upward movement of water flow, it is negative.

To evaluate the redistribution of soil moisture using Darcy's equation for one-dimensional flow, the root zone is divided into three layers; the upper layer being 30 cm (1 foot) thick, the middle being 90 cm (three feet) thick, the lower layer being 60 cm (two feet) thick. Infiltration water fills each successive layer to field capacity, and excess water, if any, eventually migrates out of root zone to ground-water recharge at the unsaturated conductivity rate. The time increment, Δt , is assumed to be equal to one day when no water infiltrates the soil surface on a given day and equal to 1/6 day when an infiltration event occurs.

Irrigation Criteria

Irrigation from storage facility to an irrigation plot is not allowed under the following conditions:

1. When water stored in pond is less than one full day's irrigation amount,
2. When the ground is frozen,
3. When the mean daily temperature is less than 0°C, and
4. When the upper zone soil moisture is greater than a specified percentage of available moisture capacity, defined as the difference between the field capacity and the permanent wilting point.

The soil is considered to be frozen if the sum of the previous two days average temperature is less than 64°F (0.0°C), while thawing is assumed if the sum of the temperatures for any consecutive three day period is greater than 114°F (10.0°C).

The percentage of available moisture capacity in the upper zone, PAVLU, initiates an irrigation scheme. PAVLU can vary from zero, which means a "non-irrigation" scheme. PAVLU = 0.90 tests an intensive irrigation, while PAVLU = 0.50 tests a normal application of irrigation.

The application rate of irrigation water is arbitrarily determined by the irrigation rate (DSRATE). It can vary from zero to a certain rate not to cause direct surface runoff unless rainfall occurs on an irrigation day. When DSRATE = 0, irrigation is not performed. Intake rate family of the soil and pump sizes are important considerations in setting DSRATE.

A watershed concerned can be divided up to nine sub-areas depending upon crop and soil type, or irrigation implementation plan. After an arbitrary number of plots are selected, an irrigation plan on each plot is made. The order of application of water to each plot on an irrigation day is automatically assigned by the loop mechanism in the program. If a storage pond has a water volume less than a designated percent

(PCVMAX) of the maximum capacity after the first-ordered field area is irrigated, the second-ordered plot will not be irrigated.

It is more reasonable not to irrigate on a rainy day, but, by the KSUHYDRO model, irrigation may or may not occur depending upon the amount of precipitation. If one day has enough rainfall to meet the fourth criteria for irrigation, water from the pond is not applied to a plot. Otherwise, irrigation water is added to compensate for the soil moisture deficit even on a rainy day.

Crop Management

Three schemes are used in crop management. The first is to have only one crop on each plot throughout the period, which is called continuous cropping. The second is to implement an annual crop/fallow rotation, with fallow the first year followed by a crop, or crop on the first year followed by fallow. The third is a multiple cropping rotation which allows three crops in two years and other very flexible options as discussed in detail in Chapter III.

Storage Facility

A storage pond in the shape of an inverted frustum of a pyramid stores water from direct precipitation and from runoff, or optionally from municipal waste water and other external sources. By specifying the length, width, and side slope of the pond, the surface area can be computed for any storage volume. The volumetric equation for a general prismatic is:

$$V = \frac{1}{6} h (B_1 + 4B_m + B_2) \quad \text{--- (12)}$$

where

V = volume

h = depth

B_1 = bottom surface area

B_m = area of a plane at $h/2$ above the bottom

B_2 = top surface area.

Even if seepage through the reservoir bottom is suspected, a sealed or zero exfiltration is assumed because of the difficulty in knowing seepage rates. Outputs from the facility consist of irrigation, overflow, and surface evaporation.

Program Options

The KSUHYDRO model possesses multiple capabilities to simulate actual field conditions. The model simulates climatological conditions by using previously recorded daily precipitation and temperature patterns for a specified location. In addition, the model can be used to predict the effects of weather modification by cloud seeding. The modified precipitation pattern is obtained from subroutine WTRMOD, which contains four options designated variable name MODEL. When MCDEL is equal to 1, there will be no modification of the precipitation data. When MODEL is equal to 2, the 'B-Zero' modification is implemented. When MODEL = 3 is used, rainfall is increased by any specified percentage represented by variable name WPCNT. The integer 4, indicates the implementation of the 'B-Zero' modified alteration scheme.

Not only variations in terms of area, soil and crop type for each irrigation plot, but capability of yielding runoff to the storage

facility and an irrigation plan can also be incorporated in the program.

Each plot can be characterized under the following three conditions:

1. A plot which yields runoff as inflow to the storage facility and on which irrigation is not implemented,
2. A plot which yields runoff as inflow to the storage facility and on which irrigation is implemented, and
3. A plot on which only irrigation is implemented, without runoff yield to the pond.

The model can also be used for the study of feedlot runoff and/or municipal waste water control. The variable BYPASS establishes feedlot runoff and/or municipal waste as a source of inflow to the facility.

BYPASS is represented by the integer 1,2,3, or 4 with each integer establishing the following options:

1. BYPASS = 1; no feedlot runoff nor municipal waste,
2. BYPASS = 2; feedlot runoff,
3. BYPASS = 3; municipal waste, and
4. BYPASS = 4; both feedlot runoff and municipal waste.

When DARCEQ is equal to 1, the redistribution of soil moisture within the soil profile is evaluated by the Darcy equation for one-dimensional unsaturated flow. When DARCEQ is equal to 2, soil moisture redistribution is analyzed by the simplified method described previously.

CHAPTER III

DEVELOPMENT OF CROP MANAGEMENT FUNCTIONS

This chapter provides a descriptive account of the development of a flexible technique for crop management which allows multiple crop rotations with single or double cropping for use in KSUHYDRO. This was the major objective of this research.

To be able to simulate prevailing irrigation field plot operations, and to examine a number of crop management alternatives for an individual farmer, a very flexible crop management plan is required in KSUHYDRO. Seven crops can be selected in the continuous simulation model and various combinations of these crops can be used corresponding to the crop management of interest.

Due to the variability in climate and soils in eastern Kansas, a variety of cropping practices exist, although generally restricted to one crop per year in dryland operations. However, it is possible for farmers to adopt double cropping operations to obtain a greater return from their investment with irrigation.

For the single-cropping management, a specified crop for every year is practiced on a farm field, depending upon crop rotation plan, which may be continuously same crop, biennially two different crops, three different crops, or up to seven different types as already defined in KSUHYDRO. In addition to that, more flexible crop rotation combinations can be made: for example,

1. One crop in the first year, another crop for the next two years, with this sequence repeated throughout the simulation, and
2. Two different crops for two years, followed by fallow, followed by two different crops for two years, with this five-year sequence repeated throughout the simulation.

For the double-cropping management, only wheat can be selected as a winter crop, which can be combined with some crops chosen from the summer row crop group to make the double-cropping concept. The wheat crop as a counterpart to any summer crop is usually rotated with fallow, so this flexibility is needed in the program.

A subroutine ROTATN for crop scheduling is developed with these concepts in mind. Its generalized flow chart is illustrated in Figure 2. The purpose of this subroutine is to provide much more flexibility in simulating supplemental irrigation systems. Subroutine ROTATN is optional if the programmer desires this flexibility. Firstly, a watershed is divided into several irrigation or runoff plots, currently dimensioned up to nine, and then crop management on each area is scheduled. Various rotation patterns can be decided by the variable name RCYCLE. Since seven kinds of crops, including fallow, are incorporated, it is capable of defining rotation schedules having up to seven different crops. For instance, by specifying the value of RCYCLE equal to seven, and arranging the sequence of crops in the following way; corn - corn - corn - soybeans - soybeans - soybeans - soybeans, this rotation would be repeated every seven years. Likewise, any irregular combination of less than seven years can be made, such as corn - soybeans - soybeans - corn - sorghum - corn - sorghum. Following the specification of rotation cycle RCYCLE on an area, the variable name DOUBLE provides for double-cropping. The term of double-cropping is typically characterized by a winter wheat-fallow rotation combined with a summer crop rotation. When an irrigation area is to be double-cropped, the name IFALWT specifies whether the simulation starts with a fallow term in January of the first year, or begins with winter wheat. To avoid some

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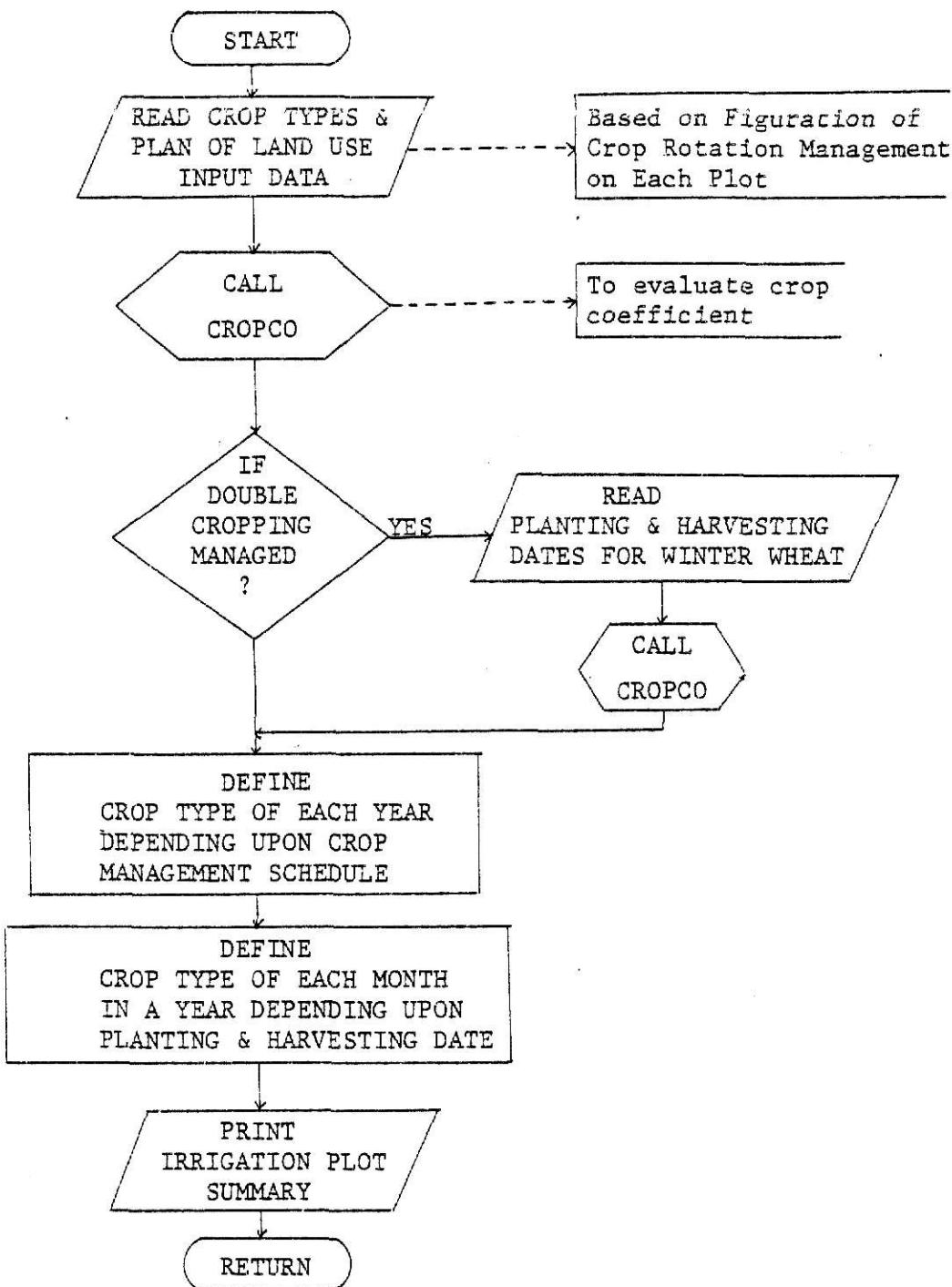


Figure 2. Generalized Flowchart for Crop Management
(Subroutine ROTATN)

inconvenience in using the computer program, the area, soil type, and irrigation implementation plan for each irrigation area can also be read in the subroutine ROTATN rather than in the main program. Crop type, planting month and day, and harvesting month and day are represented by NRCROP, MGSBP, DGSBP, MGSEP, and DGSEP, respectively. The planting and harvesting dates and monthly average temperature data are used to evaluate the monthly average crop coefficients necessary in the estimation of the evapotranspiration on the irrigation or runoff plot under consideration.

In addition to those irrigation management criteria mentioned in the previous chapter, an irrigation plot should not be irrigated in the dormant season. This season is therefore defined as one with zero value of crop coefficients.

CHAPTER IV
CASE STUDY FOR FELT FARM

A continuous simulation model has been developed by Zovne, et al. (1), to provide a means of designing various disposal control facilities. This model is easily adapted to small watersheds for the particular soil, climate and farm management operations that exist at that location. The computer program, KSUHYDRO, is composed of the main program and several subroutines which have various options as can be seen in Appendix (I). Hayden (2) made a detailed description of program usage and on the properties of each subroutine. From the generalized flow chart on KSUHYDRO illustrated in Appendix (I), the characteristics of the program can be found.

Guideline for input data necessary to handle this multi-purposed hydrologic yield model is prepared in Appendix (II), and definitions of the variable names used in the program are arranged in alphabetical order in Appendix (III), so as to be helpful to quickly understand the program.

The main function of KSUHYDRO is to optimize the size of a surface storage facility of a supplemental irrigation or land treatment system which regulates various water sources of precipitation, feedlot input, runoff from a watershed, municipal waste water, and external water supply. It can be used to test the dependable supply of water by examining interaction of components in the system. Accordingly, possibility of water catchment from a specific watershed to meet a supplemental irrigation requirement can be studied by means of the KSUHYDRO.

In this chapter, the data required to run KSUHYDRO is discussed in order to simulate the operation of Ronnie Felt's farm in Bourbon County, Kansas.

Climatological Data

The sub-humid, continental climate of Bourbon County ($94^{\circ}59'W$, $37^{\circ}51'N$) is characterized by abundant precipitation, warm to hot summers, generally mild winters, moderate to high humidity, light to moderate winds, and low annual snowfall (10).

The selected experimental farm is about 10 miles to the north of Uniontown located in the center of this County. Since this specific location does not have good meteorological data, Fort Scott, the county seat, is chosen as a representative place to obtain daily precipitation, and maximum and minimum daily air temperatures, which can be secured from tapes provided by the National Weather Service Climatic Center in Asheville, North Carolina.

As directed in (1), the 12 monthly values of relative humidity (RHD), percent sunshine (PSUNS), wind velocity (WIND), and mean air temperature (MMAT) are obtained from published records (11). These are necessarily estimated through interpolation by using the records of Topeka and Springfield, the nearest first-order weather stations whose values are available in (11). The interpolated data are shown in Table IV.

Moisture deficit (MD) is defined as the long-term average annual lake evaporation minus the long-term average precipitation. The MD can be computed using charts or figures provided by the U.S. Weather Bureau. This value can be used to select tentative values of geographical coefficients, c and d, for the Penman Combination Equation, by

TABLE IV MONTHLY CLIMATOLOGICAL DATA

Station : Fort Scott

L=37° 51' N

Month	Percent Sunshine (%)	Wind Velocity in km/h (mph)	Relative Humidity (%)	Mean Monthly Air Temp. in °C (°F)	Solar Radiation (mmH ₂ O/day)
	PSUNS	WIND	RHD	MMAT	RA
Jan.	50	19.0 (11.8)	77	-0.3 (31.4)	6.54
Feb.	54	19.2 (11.9)	78	1.9 (35.5)	8.77
Mar.	56	21.7 (13.5)	78	6.3 (43.4)	11.37
Apr.	57	21.2 (13.2)	79	12.8 (55.1)	14.09
May.	60	18.3 (11.4)	84	17.9 (64.2)	15.92
Jun.	65	17.7 (11.0)	86	23.3 (74.0)	16.66
Jul.	66	15.0 (9.3)	87	26.1 (79.0)	16.28
Aug.	70	15.1 (9.4)	87	25.4 (77.8)	14.91
Sep.	72	16.3 (10.1)	86	21.0 (69.8)	12.48
Oct.	67	17.1 (10.6)	82	14.9 (58.9)	9.73
Nov.	57	18.8 (11.7)	80	6.6 (43.9)	7.22
Dec.	51	18.8 (11.7)	79	1.5 (34.7)	6.02

* PSUNS,WIND,RHD,MMAT - Obtained from Climates of the States,
Vol. 2, Water Information Center, Inc. Port Washington, N.Y., 1974

** RA - Irrigation Principles and Practices, O.W.Israelson and V.E.
Hansen, John Wiley and Sons, Inc. , N.Y., 1962

using Figure 3 in Zovne (1). After running the program several times, the values c and d are adjusted slightly so that the average annual lake evaporation for the simulation period corresponds to the published value. An increase in c of 0.01 results in a 25.4 ± 6.4 mm (1.0 ± 0.25 in.) increase in lake evaporation while an increase in d of 0.001 results in an increase of 10.2 ± 2.5 mm (0.4 ± 0.1 in.) (1). For the Fort Scott location the moisture deficit is found to be 177.8 mm (7 inches) using the evaporation charts (12) and (11). The geographic coefficients eventually result in c = 0.64 and d = 0.04.

Data for Soils

The drainage area of interest has gently rolling topography like the prairie soils regions. They are characterized by a dark colored silty loam to silty clay loam A horizon, a heavy silty clay loam B₁ horizon, and a B₂ horizon which is very high in clay content and forms a layer which is very slowly permeable. The experimental site is contained in the series of claypan soils prevailing from northeastern to southwestern part of Missouri (13).

The claypan soils have a moderate available moisture holding capacity and crop yields are often low in seasons of deficient rainfall. Also, claypan soils can cause the problems of excess moisture, and relatively greater runoff during the rainy season. The soil types are generally classified by the Soil Conservation Service as having land capability units II or III, which means that soils have moderate or severe limitations that reduce the choice of plants or require moderate or special conservation practices so as to be quite productive (10).

It is difficult to select a typical soil type which can be representative for a watershed area. The total drainage area in question,

including the pond, covers 166 hectares (410 acres) excluding 34.4 irrigated hectares (85 acres) which do not drain back into the pond. The drainage area of concern is broken down in Table V according to the area and the soil series located in Figure 3. Table V indicates that more than half of the drainage area consists of D hydrologic soil group, while a quarter of the total area is C group and another quarter B group. In other words, most of the area is composed of soil type 1 as defined in Kansas Irrigation Guide (8). Even though watershed should be subdivided according to various types of soil, it is more convenient to use a prevailing type throughout the area. Thus, soil type 1 is used in the program.

Crop Management and Irrigation Practice

The watershed area is subdivided into 6 plots according to various cropping and irrigation practices. Crops commonly grown in the county are corn, wheat, soybeans, and alfalfa. Sorghums are grown both for ensilage and for grain. The cropping plans in Table VI for the plots shown in Figure 3 were made simply on the basis of the owner's intention. It is not common to practice double-cropping in this area, but for plot 1 double-cropping is managed in order to get early return on the investment in irrigation facilities. The corn crop is planted in April of the first simulation year. Winter wheat is planted immediately following the corn crop which is harvested the next summer. After wheat harvest, soybeans are planted, followed by a fallow term during the winter season. On finishing one cycle of rotation, corn is planted again. Care should be taken in selecting proper planting and harvesting dates for a preceding crop and for a following crop on a plot, in order

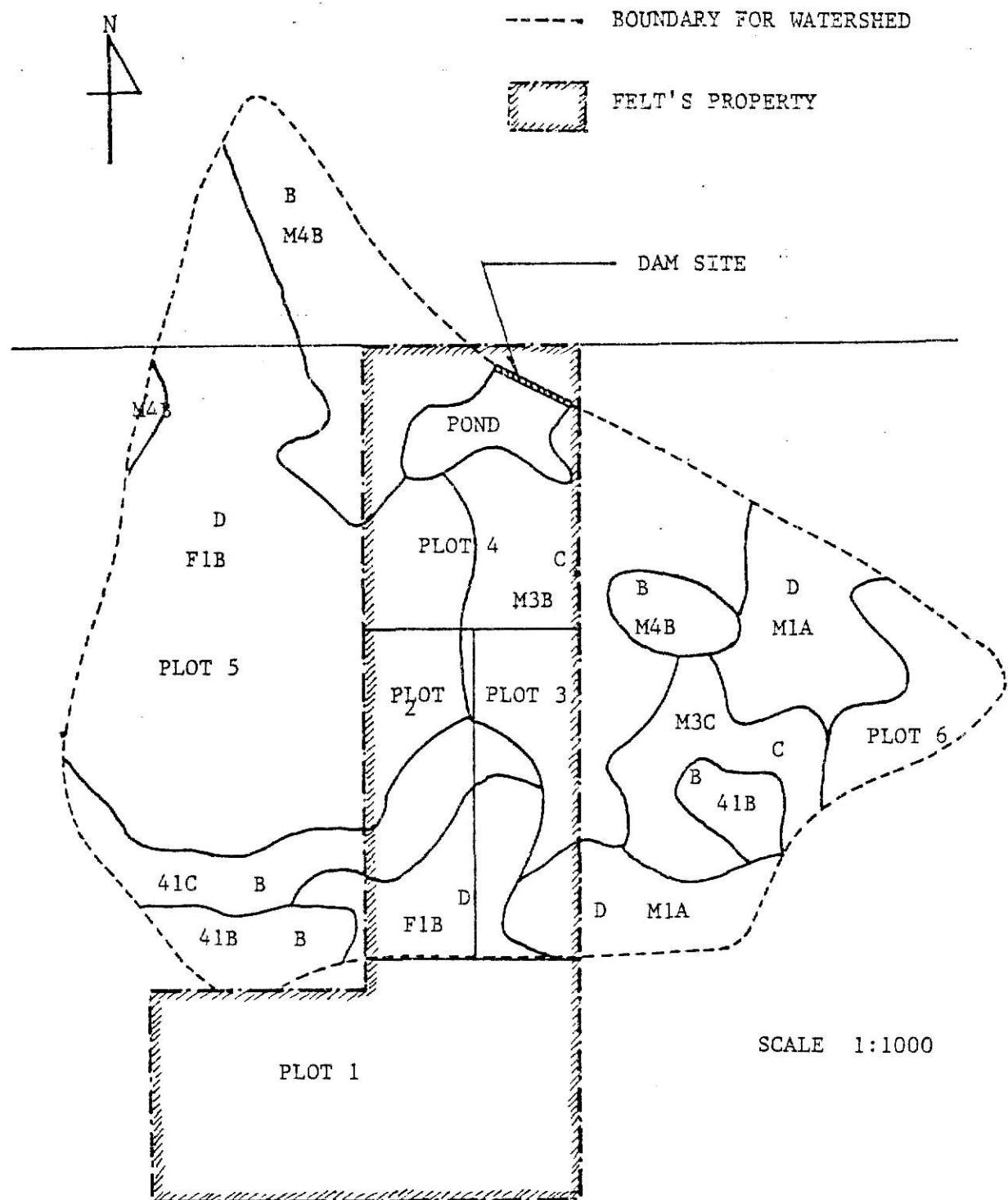


Figure 3. General Layout of Drainage Area

TABLE V CLASSIFICATION OF SOIL TYPES FOR DRAINAGE AREA

Mapping Unit	Irrigation Soil Group (1)	SCS Hydro Group	LCU (2)	Percent of Drain Area	Area in ha (acres)
Kenoma silt loam	1	D	IIIe-3	39.8	66 (163.1)
Dennis silt loam 1-3. %	3	C	IIIe-1	16.6	27.5 (68.0)
Catoose silt loam	6	B	IIIe-2	12.8	21.3 (52.7)
Parsons silt loam	1	D	IIIe-3	10.7	17.7 (43.7)
Bates loam 4-7 %	8	B	IIIe-1	6.0	10.0 (24.8)
Dennis silt loam 3-6 %	3	C	IIIe-4	5.3	8.8 (21.8)
Bates loam 1-4 %	8	B	IIIe-2	4.4	7.4 (18.2)
Unknown				4.3	7.2 (17.7)

(1) Kansas Irrigation Guide, Irrigation Soil Group (8)

(2) Land Capability Units, Soil Conservation Service (10)

TABLE VI LAND USE PLAN AND CROP MANAGEMENT

Plot	Area in ha (acres)	Irrigation Plan Implemented	Soil Type (SCS Group)	Crop Management
1	34.4 (85)	Irrigation Only	1	Corn-Wheat-Soybeans *(1)
2	12.1 (30)	Runoff & Irrigation	1	Corn-----Sorghum ***(2)
3	12.1 (30)	Runoff & Irrigation	1	Soybeans ****(3)
4	76.9 (190)	Runoff Only	1	Pasture ****(3)
5	48.6 (120)	Runoff Only	1	Corn ****(3)
6	16.2 (40)	Runoff Only	1	Sorghum ****(3)

*(1) Double-cropping with biennially repeated rotation

**(2) Single-cropping with biennially repeated rotation

****(3) Single-cropping with continually same crop

TABLE VII PLANTING AND HARVESTING DATES

Crop	Planting Date	Harvesting Date
Corn	April 10	September 20
Soybeans	June 30	October 30
Sorghum	June 15	October 10
Wheat	October 10	June 20

not to have them overlapped. Planting and harvesting dates for the crops are given in Table VII. On the plots except plot 1, a single-cropping is practiced with only plot 2 crop-rotated.

The irrigation plan for each plot is illustrated in Table VI. A watershed area of 410 acres contributes runoff to the storage pond corresponding to plots 2-6 on Figure 3 and Table VI. Irrigation water from the pond is applied to the area of 58.7 hectares (145 acres) (plots 1-3) at a specified rate depending upon the previously described irrigation criteria. When the pond storage on a day is less than 5 percent of its maximum storage capacity ($PCVMAX = 0.05$), when the upper zone soil moisture is greater than 50 percent of maximum available moisture ($PAVLU = 0.5$), or when the temperature is below freezing, irrigation is not allowed.

Study of Storage Facility

Although the water sources for a pond can be direct rainfall on the surface area, inflow from municipal disposal, feedlot runoff, and surface runoff from the drainage area, only precipitation and runoff are considered as water sources for storage.

Information on the small farm reservoir was secured from Agricultural Engineering Associates, Inc., Uniontown, Kansas, which participated in construction in 1976. Figure 4 shows the relationships of volume-depth and area-depth for this reservoir.

In order to obtain pond parameters readily adaptable to the computer program, the irregular shape of reservoir was modified to the shape of an inverted prismatioid with the surface area and the volume at each level of depth reflecting actual conditions as far as possible. It is

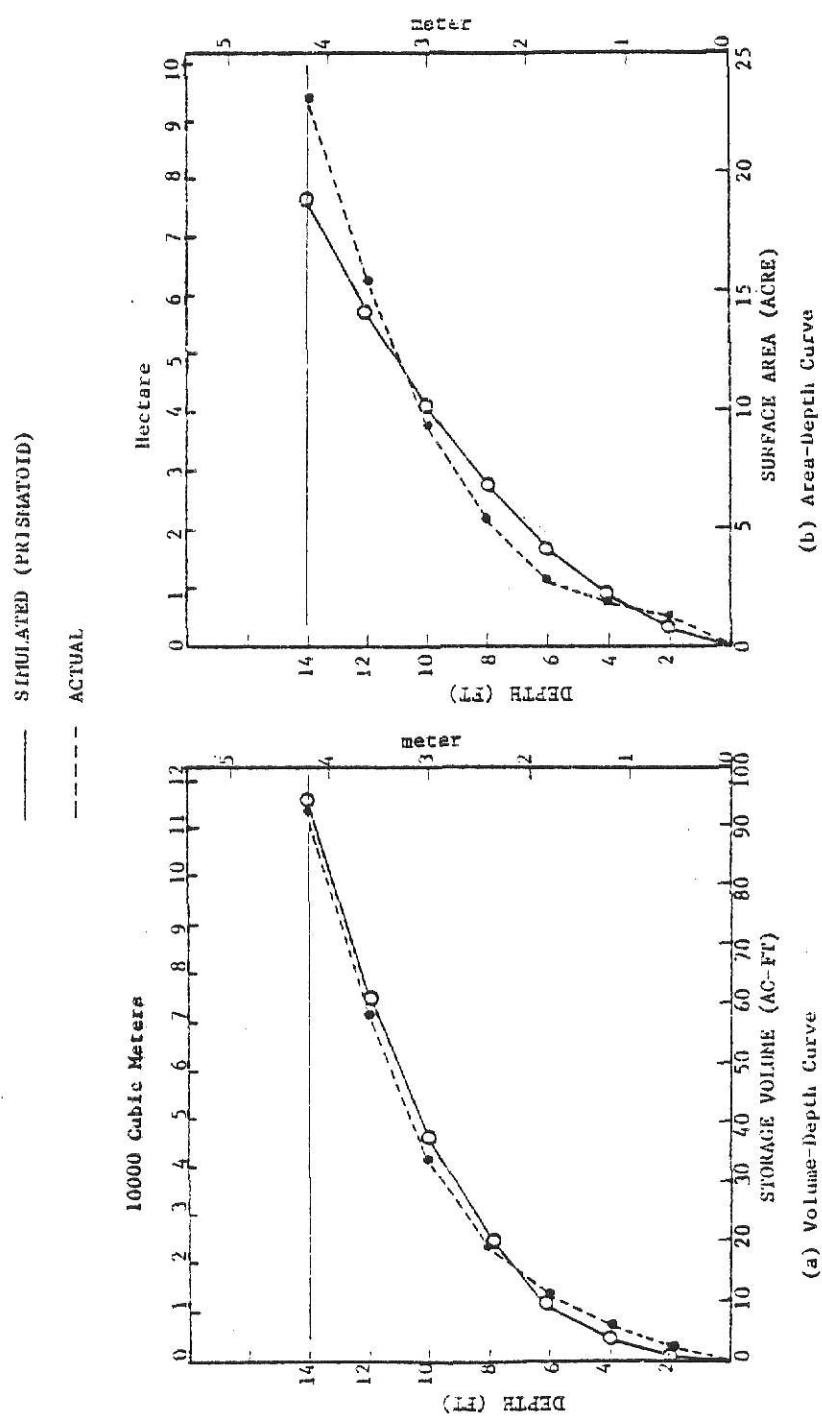


Figure 4. Reservoir Storage Capability

necessary to adjust actual dimensions for each reservoir to make use of the pond facility scheme already programmed in KSUHYDRO whenever a case study on a specific site is pursued.

The desired dimensions were selected by a trial and error method to minimize area-depth and volume-depth differences between the actual and simulated pond. The dimensions of base width $W = 19.5$ meters (65 ft.), base length, $L = 19.5$ meters (65 ft.), side slope, $S = 30$, and maximum height, $H_{MAX} = 4.2$ meters (14 ft.) resulted in the correspondence shown in Figure 4. The maximum surface area is reduced from an actual value of 9.27 hectares (22.91 acres) to 7.61 hectares (18.81 acres) in the model, while the maximum volume increases from an actual value of 11.42 ha-m (92.6 acre-ft) to 11.65 ha-m (94.5 acre-ft) in the model. Accordingly, it can be supposed that the reduction of maximum surface area causes relatively a small decrease in evaporation loss from the surface because of the small moisture deficit in the area.

The outputs from storage reservoir that are taken into account are overflows over spillway, evaporation, irrigation to the disposal area, and seepage. The last factor, seepage, is difficult to estimate because the storage-depth relationship is unique for each reservoir. Under assumption that the reservoir was well-constructed by sealing pond bottom with highly impermeable material like bentonite, zero seepage was considered in this study.

CHAPTER V
RESULTS AND DISCUSSION

The capability of a farm irrigation supply pond may be restricted by various factors, such as meteorology, the site topography, the size of the irrigable crop land, the drainage area size, vegetation, and so forth. Observations on Felt's farm were made for a 23-year simulation period (1948-1970). This chapter presents the results obtained from this simulation. Hydrologic simulation is a tool that can be used to manage or predict water budget between the income of water from precipitation, and snowmelt and the outflow of water by evaporation, transpiration, irrigation withdrawal, groundwater recharge, and streamflow. Water balance calculations are made on long-term-average climatic data to obtain an approximate picture of the seasonal or annual trend of hydrologic characteristics.

The possibility of supplemental irrigation in Southeastern Kansas, the main point of this study, was examined under three different conditions with varying irrigation rates of 0.00, 6.35 (0.25), and 12.7 mm/day (0.50 inches/day).

In the first part of this chapter, general hydrologic aspects of each irrigation rate are discussed, and then an interpretation on irrigation demand is made combined with reservoir water budget.

GENERAL HYDROLOGY

The purpose of irrigation may be to increase crop yield by supplementing rainfall. Irrigation is an artificial method to overcome deficiencies in the natural rainfall pattern. These deficiencies may stem from lack of precipitation, or for other factors related with

TABLE VIII SUMMARY OF LONG-TERM SIMULATION RESULTS (a)

Precipitation in mm/yr (in/yr)	977 (38.45)
High	1533 (60.36)
Low	669 (26.35)
Moisture Deficit in mm/yr (in/yr)	174 (6.86)
Lake Evaporation in mm/yr (in/yr)	1151 (45.31)
Maximum Pond Depth in meters (ft)	4.2 (14)
Maximum Pond Volume in ha-m (ac-in)	11.66 (1133.98)
Pond Dimensions in meters (ft)	19.5 X 19.5 (65X65)
Direct Receiving Area in ha (ac)	7.6 (18.8)
Minimum Pond Depth in meters (ft)	1.17 (3.91)
Pond Discharges--No. of Years	23
Total No. of Discharges	668
Total Discharge in ha-m (ac-in)	797 (77542.63)

	Plots					
	1 C-W-B	2 C-S	3 B	4 P	5 C	6 S
Crop						
Area in hectares (acres)	34.4 (85)	12.1 (30)	12.1 (30)	76.9 (190)	48.6 (120)	16.2 (40)
Irrigation in cm/yr (in/yr)	12.6 (4.95)	16.1 (6.32)	4.3 (1.68)	0	0	0
Runoff in cm/yr (in/yr)	29.6 (11.66)	32.6 (12.82)	32.8 (12.92)	19.6 (7.73)	28.8 (11.34)	30.8 (12.12)
Percolation in cm/yr (in/yr)	2.7 (1.06)	3.5 (1.37)	3.4 (1.32)	4.0 (1.59)	2.0 (0.80)	3.5 (1.37)
Evapotranspiration in cm/yr (in/yr)	56.6 (22.28)	55.1 (21.68)	47.0 (18.49)	56.6 (22.27)	49.5 (19.48)	46.1 (18.14)
Interception in cm/yr (in/yr)	21.5 (8.45)	22.7 (8.95)	18.9 (7.44)	17.5 (6.88)	17.5 (6.88)	17.5 (6.88)
Change in Soil moisture in cm/yr (in/yr)	-0.15 (-0.06)	-0.13 (-0.05)	-0.13 (-0.05)	-0.10 (-0.03)	-0.13 (-0.05)	-0.15 (-0.06)
No. of Irrigation Days	19.8	25.3	6.7	-	-	-

** C-Corn, W-Wheat, S-Sorghum, B-Soybeans, P-Pasture, F-Fallow

TABLE VIII SUMMARY OF LONG-TERM SIMULATION RESULTS (b)

Precipitation in mm/yr (in/yr)	977 (38.45)
High	1533 (60.36)
Low	669 (26.35)
Moisture Deficit in mm/yr (in/yr)	174 (6.86)
Lake Evaporation in mm/yr (in/yr)	1151 (45.31)
Maximum Pond Depth in meters (ft)	4.2 (14)
Maximum Pond Volume in ha-m (ac-in)	11.66 (1133.98)
Pond Dimensions in meters (ft)	19.5 X 19.5 (65X65)
Direct Receiving Area in ha (ac)	7.6 (18.8)
Minimum Pond Depth in meters (ft)	1.12 (3.73)
Pond Discharges--No. of Years	23
Total No. of Discharges	678
Total Discharge in ha-m (ac-in)	810 (78846.94)

	Plots					
	1	2	3	4	5	6
Crop	C-W-B	C-S	B	P	C	S
Area in hectares (acres)	34.4 (85)	12.1 (30)	12.1 (30)	76.9 (190)	48.6 (120)	16.2 (40)
Irrigation in cm/yr (in/yr)	11.7 (4.60)	14.1 (5.55)	4.2 (1.65)	0	0	0
Runoff in cm/yr (in/yr)	30.4 (11.98)	33.3 (13.11)	33.3 (13.12)	19.6 (7.73)	28.8 (11.34)	30.8 (12.12)
Percolation in cm/yr (in/yr)	2.7 (1.05)	3.5 (1.39)	3.3 (1.30)	4.0 (1.59)	2.0 (0.80)	3.5 (1.37)
Evapotranspiration in cm/yr (in/yr)	57.0 (22.45)	55.0 (21.76)	47.1 (18.56)	56.6 (22.27)	49.5 (19.48)	46.1 (18.14)
Interception in cm/yr (in/yr)	19.3 (7.61)	19.6 (7.78)	18.2 (7.15)	17.5 (6.88)	17.5 (6.88)	17.5 (6.88)
Change in Soil moisture in cm/yr (in/yr)	-0.13 (-0.05)	-0.13 (-0.05)	-0.13 (-0.05)	-0.10 (-0.03)	-0.13 (-0.05)	-0.15 (-0.06)
No. of Irrigation Days	9.2	11.1	3.3	-	-	-

** C-Corn, W-Wheat, S-Sorghum, B-Soybeans, P-Pasture, F-Fallow

TABLE VIII SUMMARY OF LONG-TERM SIMULATION RESULTS (c)

Station : Fort Scott Simulation Period : 1948-1970
Critical Event : 168 mm (6.6 inches) PAVLU : 0.5
Soil Type : 1
Irrigation Rate : 0 mm (0 inches/day)

Precipitation in mm/yr (in/yr)	977	(38.45)				
High	1533	(60.36)				
Low	669	(26.35)				
Moisture Deficit in mm/yr (in/yr)	174	(6.86)				
Lake Evaporation in mm/yr (in/yr)	1151	(45.31)				
Maximum Pond Depth in meters (ft)	4.2	(14)				
Maximum Pond Volume in ha-m (ac-in)	11.66	(1133.98)				
Pond Dimensions in meters (ft)	19.5 X 19.5	(65X65)				
Direct Receiving Area in ha (ac)	7.6	(18.8)				
Minimum Pond Depth in meters (ft)						
Pond Discharges--No. of Years	23					
Total No. of Discharges	776					
Total Discharge in ha-m (ac-in)	919	(89394.5)				
Crop	Plots					
	1 C-W-B	2 C-S	3 B	4 P	5 C	6 S
Area in hectares (acres)	34.4 (85)	12.1 (30)	12.1 (30)	76.9 (190)	48.6 (120)	16.2 (40)
Irrigation in cm/yr (in/yr)	0	0	0	0	0	0
Runoff in cm/yr (in/yr)	27.0 (10.63)	29.6 (11.66)	31.5 (12.41)	19.6 (7.73)	28.8 (11.34)	30.8 (12.12)
Percolation in cm/yr (in/yr)	2.5 (0.98)	3.3 (1.28)	3.1 (1.23)	4.0 (1.59)	2.0 (0.80)	3.5 (1.37)
Evapotranspiration in cm/yr (in/yr)	50.9 (20.02)	47.4 (18.68)	45.7 (17.98)	56.6 (22.27)	49.5 (19.48)	46.1 (18.14)
Interception in cm/yr (in/yr)	17.5 (6.88)	17.5 (6.88)	17.5 (6.88)	17.5 (6.88)	17.5 (6.88)	17.5 (6.88)
Change in Soil moisture in cm/yr (in/yr)	-0.13 (-0.06)	-0.13 (-0.05)	-0.13 (-0.05)	-0.10 (-0.03)	-0.13 (-0.05)	-0.15 (-0.06)
No. of Irrigation Days	0	0	0	-	-	-

** C-Corn, W-Wheat, S-Sorghum, B-Soybeans, P-Pasture, F-Fallow

natural crop growth which requires more water than naturally provided. The character of each component of hydrologic cycle at a location should be examined in order to plan intelligently for the use of the available water.

The long-term average hydrologic budgets for each irrigation rate are tabulated in Table VIII (a-c). Table VIII briefly outlines pond operations, crop, plot hydrology, and precipitation characteristics.

Precipitation

The sub-humid region is normally considered to receive sufficient rainfall resulting from the interaction of warm and cold air masses. The main source of precipitation is affected by the Gulf of Mexico for this region (11).

The annual rainfall totals at Fort Scott ranged from 669 mm (26.35 inches) to 1533 mm (60.36 inches) during the simulation period (1948-1970). As can be seen in Figure 5, the droughts of 1952, 1953, 1963 and 1966 were recorded, and the average annual precipitation was 977 mm (38.45 inches). The annual precipitation data were arrayed and plotted, using normal probability distribution. The ordinate of Figure 6 is the ratio of the observed value divided by the mean value for the simulation period and the abscissa is probability, as defined by the equation $m/(n+1)$, where "m" is the order number or rank of the plotted point with the largest value having $m = 1$, and "n" is the total number of points in the array (14). The 80 percent chance of rainfall, i.e., once in 5 years, is 762 mm (30 inches) by Figure 6.

Distribution of rainfall through the year favors crop production, with an average of 75 percent of the total annual rainfall occurring

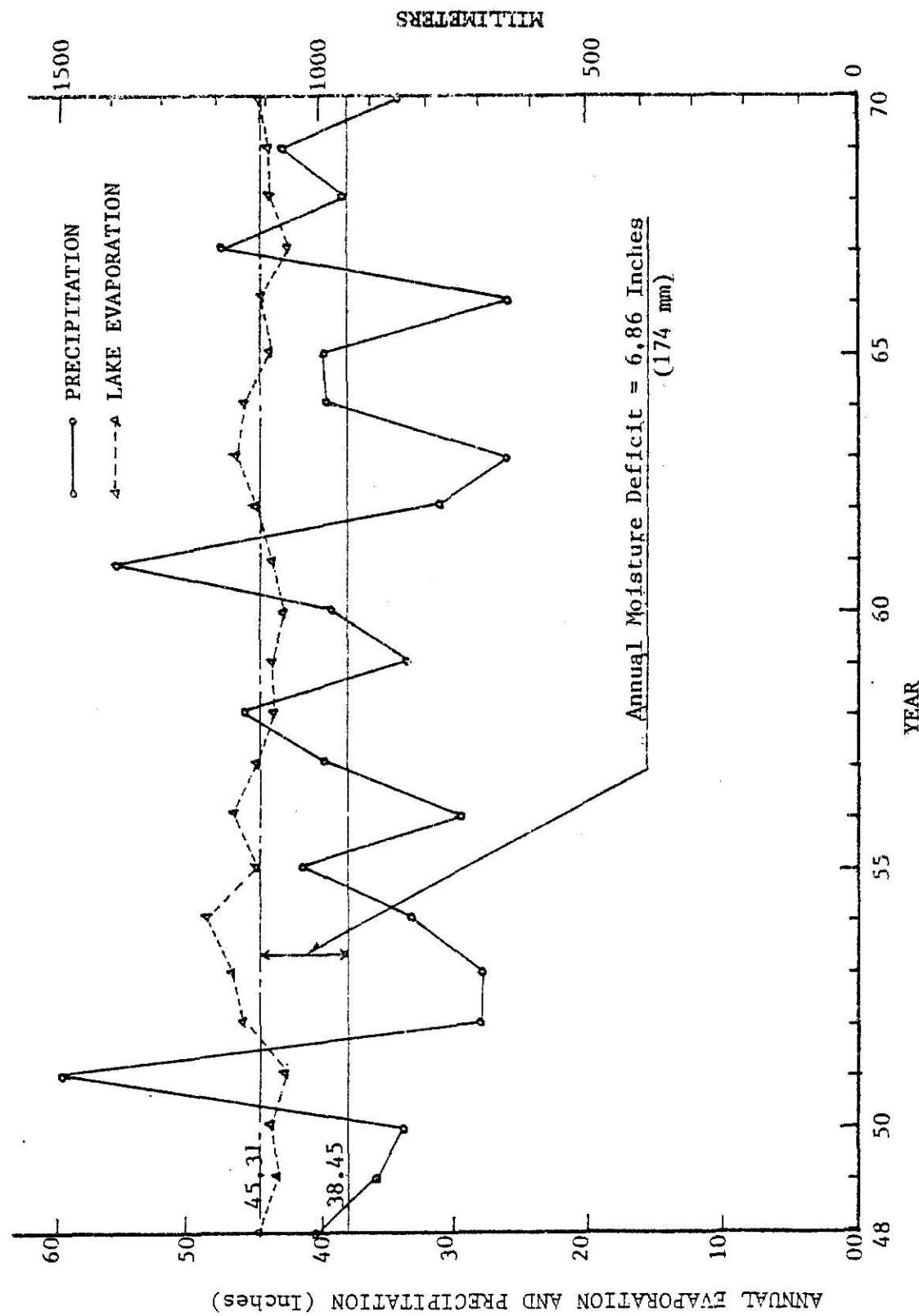


Figure 5. Distribution of Annual Precipitation and Lake Evaporation
(1948-1970)

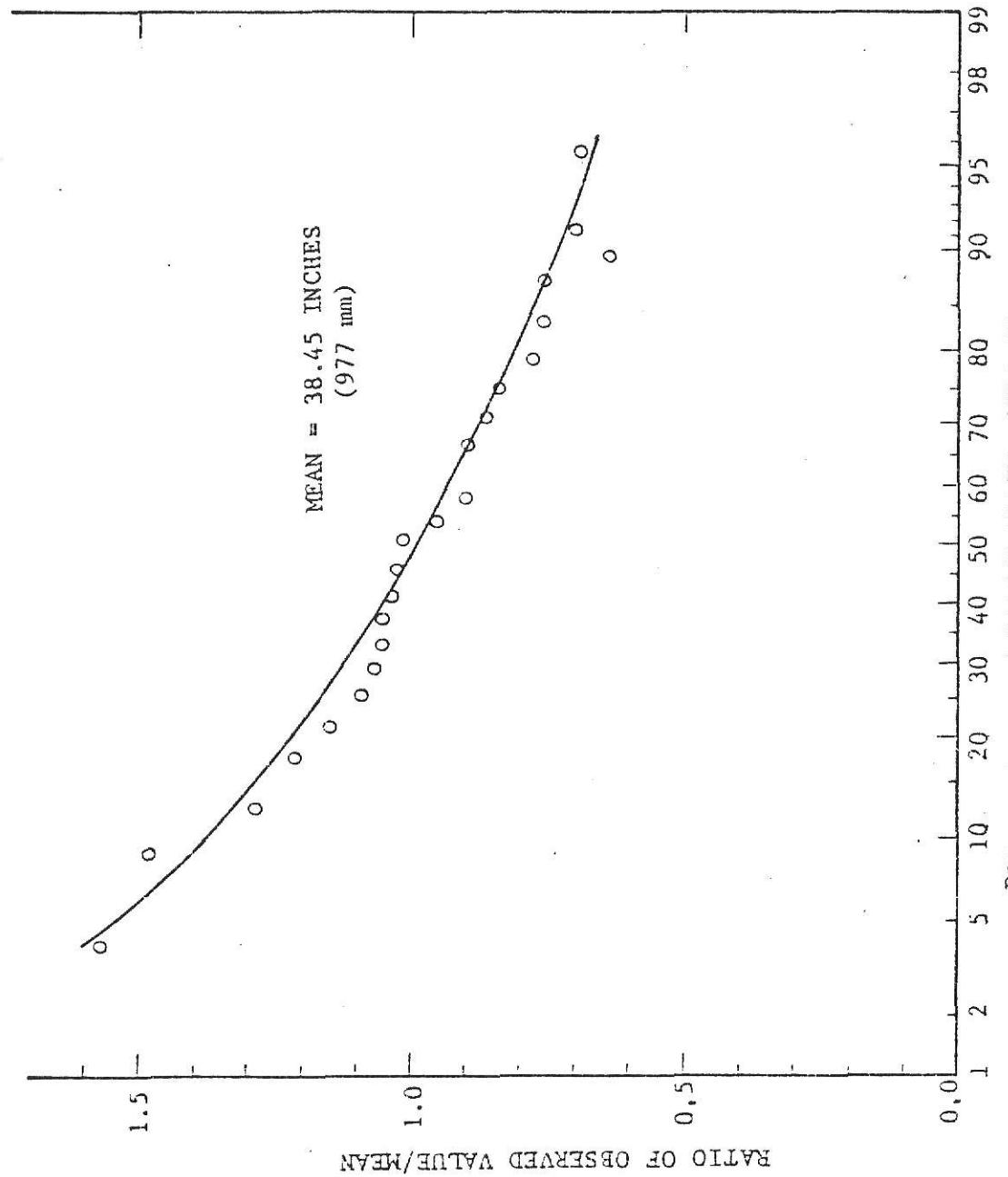


Figure 6. Simulated Annual Precipitation Probabilities (1948-1970)

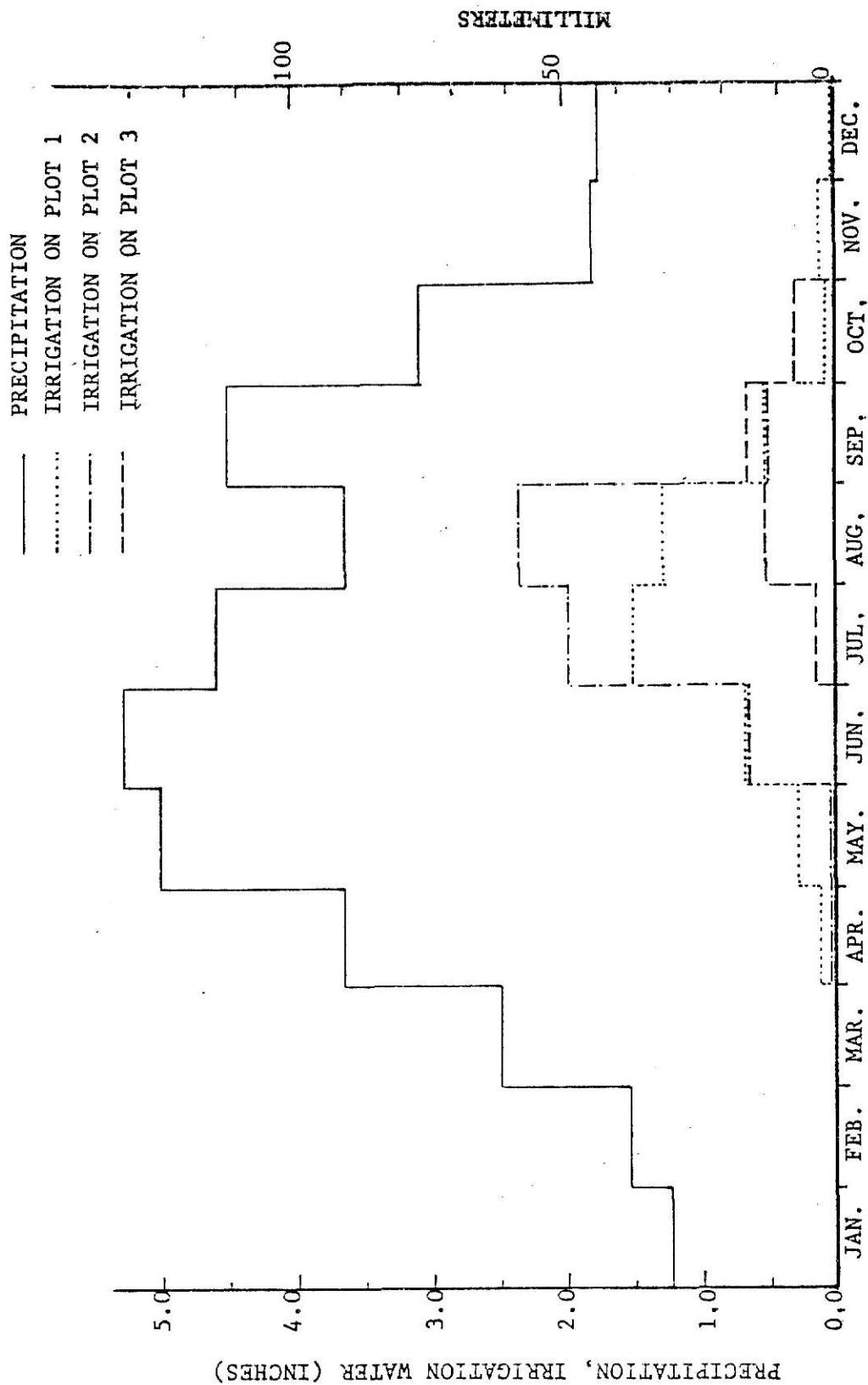


Figure 7. Monthly Distribution of Precipitation and Monthly Average Irrigation Amount at the Irrigation Rate of 0.25 Inches/Day (1948-1970)

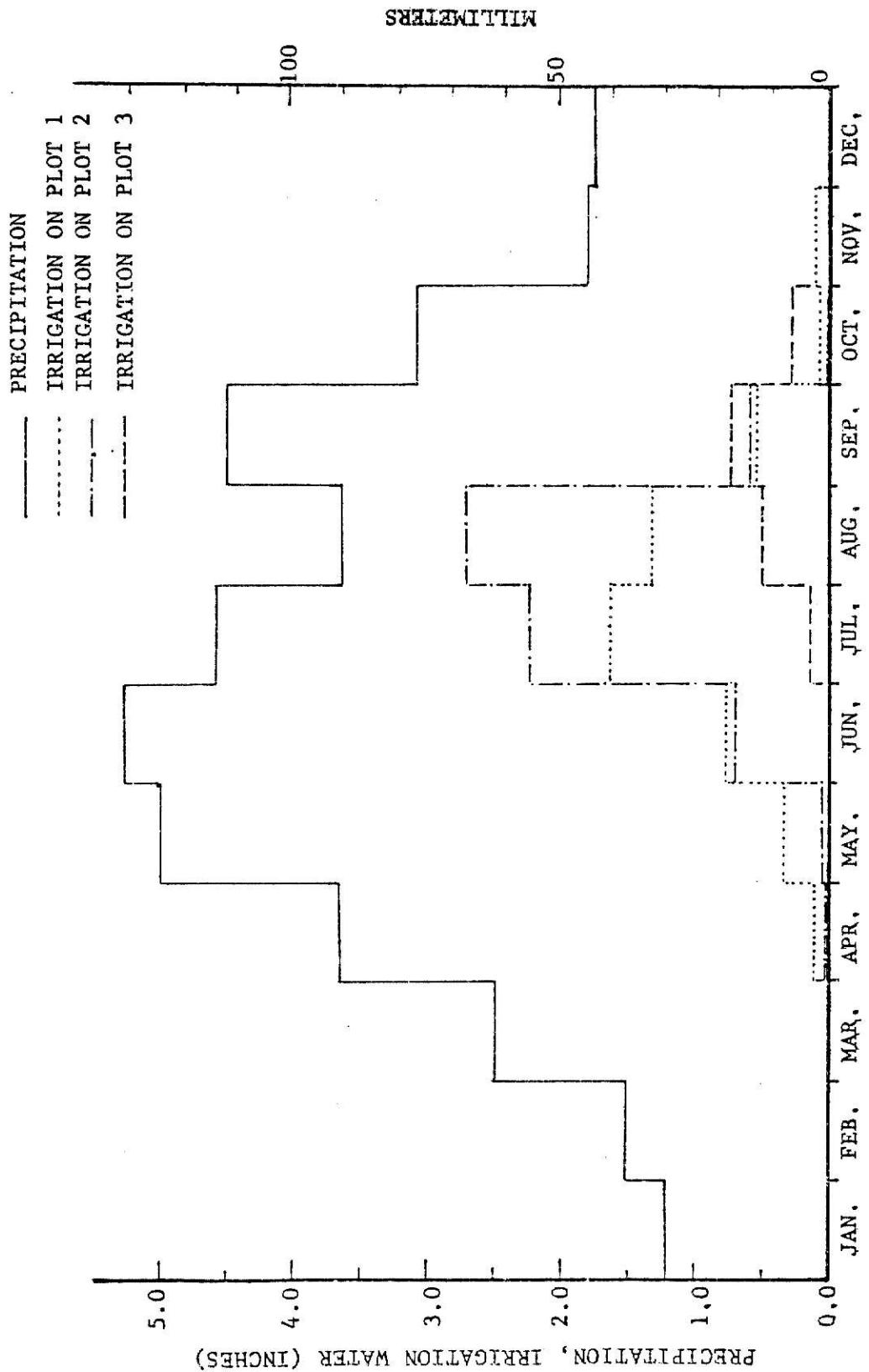


Figure 8. Monthly Distribution of Precipitation and Monthly Average Irrigation Amount at the Irrigation Rate of 0.50 Inches/Day (1948-1970)

in the growing season of April to September. May and June were the months of greatest rain, while a noticeable decrease in the average rainfall occurs in July and to a greater extent in August. An increase occurs again in September, as shown in Figure 7 and Figure 8. The reduction in the amount of rainfall in August may be critical for some crop such as corn.

Runoff

It is evident that more rainfall causes more runoff which can be a major source to fill the reservoir. The response of runoff to annual precipitation is explained in a simple linear regression equation in Figure 9. A map of annual average runoff yield for Kansas was developed by Kansas Water Resources Board (15) based on 1920-1956 records. The runoff by this map is 277 mm (10.9 inches) in the southeast. The average value of 250 mm (9.84 inches) under the condition of dryland cultivation in Figure 9, may reasonably approximate the estimate of 277 mm (10.9 inches). Annual surface runoff amounts were arrayed and plotted by the same method described previously in Figure 10. For a 90 percent probability of occurrence, 50.8 mm (2.0 inches) runoff may be estimated from Figure 11 based on a manual fit of data points.

Much of the runoff occurs in the early spring and the late fall as does precipitation. Figure 11 shows monthly distribution of runoff amount into the pond under consideration of non-irrigation.

Interception

It is difficult to estimate the amount of water intercepted. Lull (16) reported the results of U.S. Department of Agriculture experiments on total interception by various crops. In Missouri,

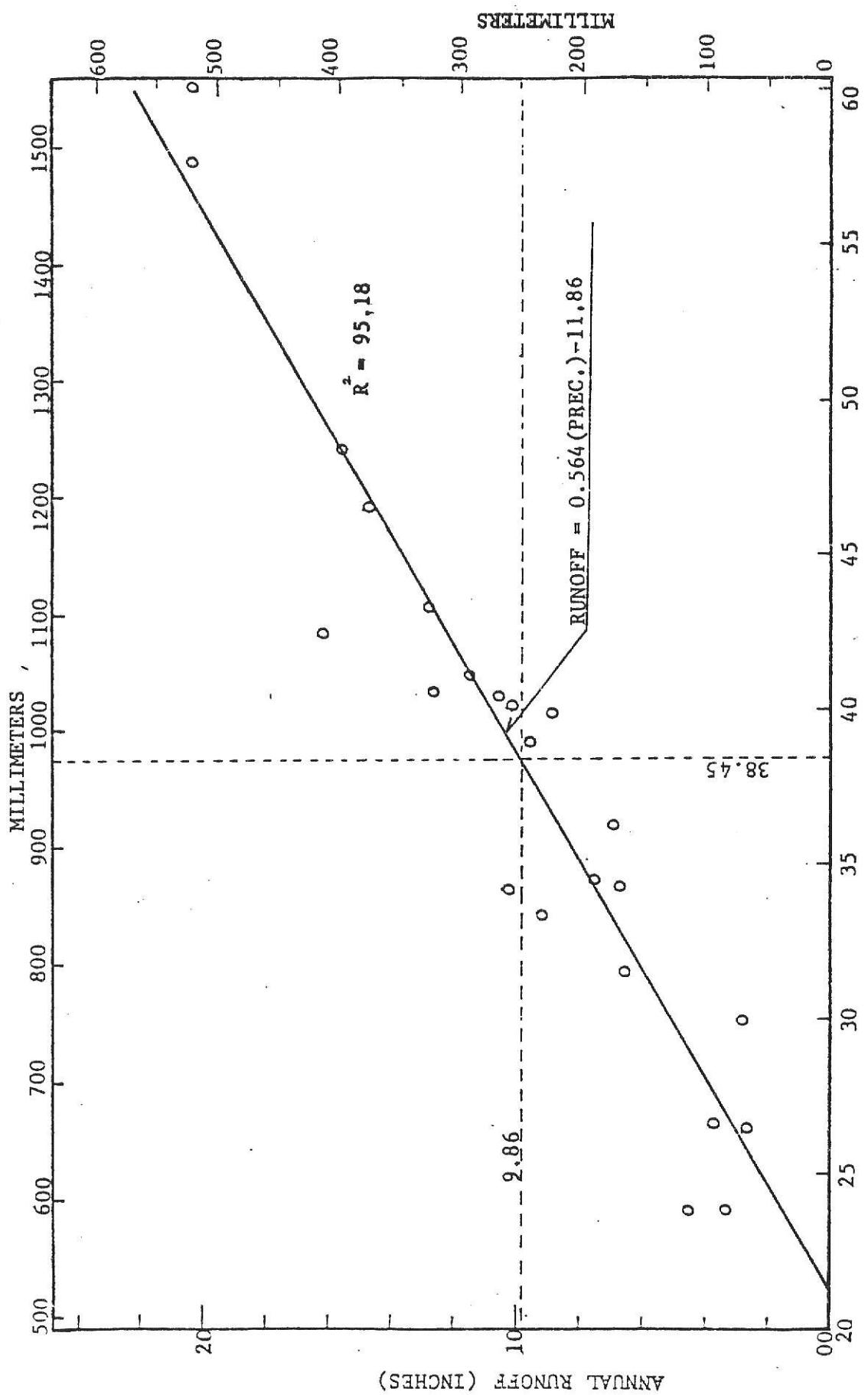


Figure 9. Relationship Between Annual Precipitation and Simulated Annual Average Runoff (1948-1970)

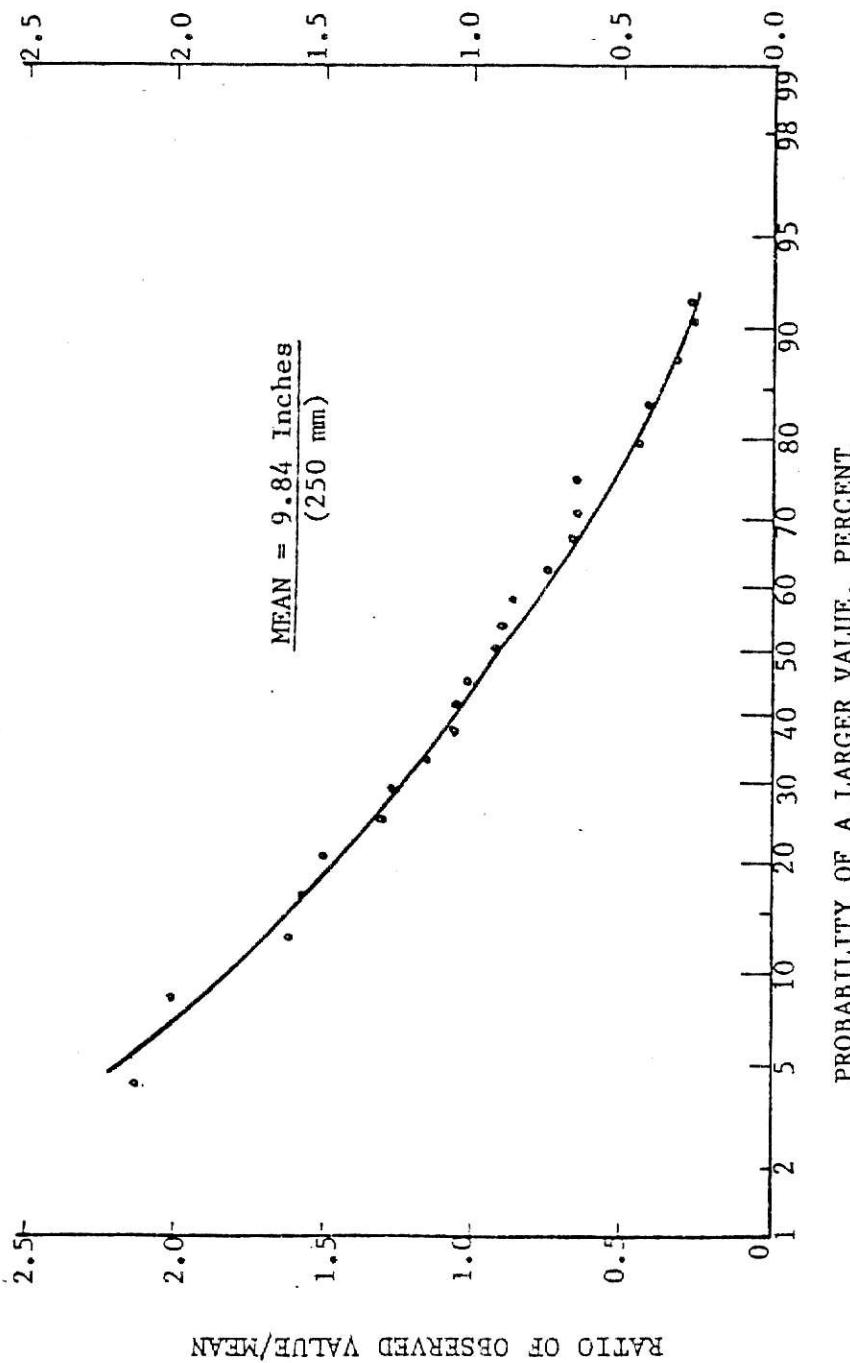


Figure 10. One-Year Simulated Annual Surface Runoff Probabilities
(1948-1970)

bluegrass intercepted 17 percent of the rainfall during the month prior to harvest. During the growing season, it was found to intercept 7 to 36 percent and during low vegetation development it was found to intercept 3 to 22 percent for alfalfa, corn, soybean, and oats.

The total annual interception based on long-term simulation was 175 mm (6.88 inches) on an unirrigated area, which would be equivalent to 17.9 percent of the average annual rainfall of 977 mm (38.45 inches). The suggestion made by Bean (3) to use 2.54 mm (0.1 inch) interception-storage-capacity in the computer program, may therefore be reasonable.

Evapotranspiration

Evapotranspiration (ET) includes bare soil evaporation and transpiration. As shown in Table VIII, long-term average annual ET varies from 461 mm (18.14 inches) to 570 mm (22.45 inches), depending upon the schedule of crop management and the plan of irrigation. These values indicate that approximately one-half of the annual total precipitation is dissipated by ET. The irrigation quantity on irrigation plots causes an increase in ET, as would be anticipated.

Storage Facility

The average monthly runoff volumes from the 166 hectare (410 acre) watershed under natural conditions, are shown in Figure 11. The distribution of runoff throughout the year is very important with regard to the irrigation water supply. The lowest expected runoff is in August during the growing season from April to September. Needless to say, when runoff is low, the irrigation demands are greatest.

The rainfall volumes contributing to the increase of storage volume are greatest in June and lowest in August. The lake evaporation is relatively uniformly distributed from year to year.

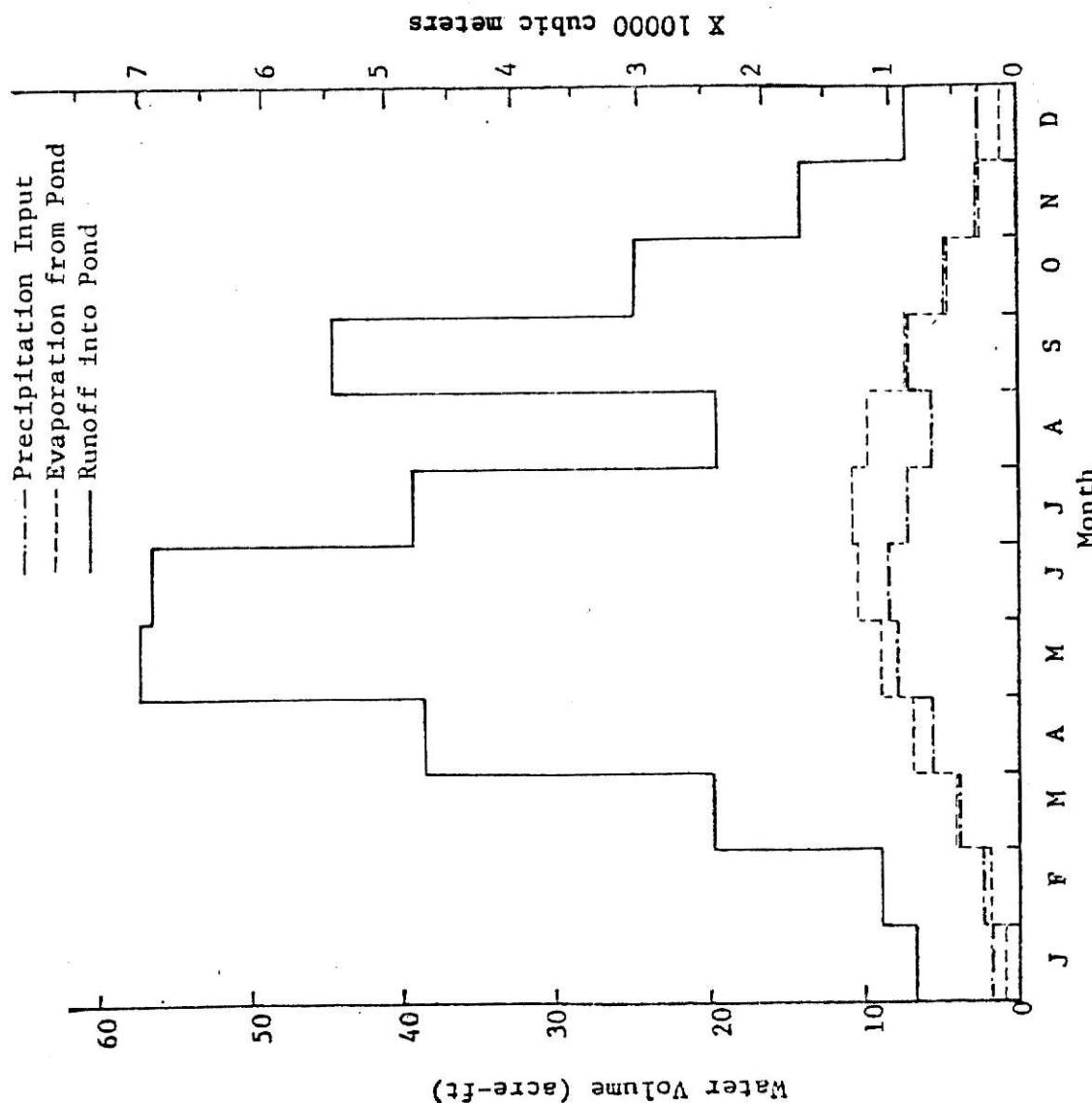


Figure 11. Monthly Distribution of Precipitation, Evaporation, and Runoff to Pond

The average monthly net available water for irrigation shown in Figure 12, was estimated by the summation of expected runoff yield and direct precipitation on the pond and the subtraction of evaporation. The net available water is always positive. The irrigation withdrawals from the reservoir reduce the water available, but the pond was never dry during the simulation period.

In order to impound all of the runoff without overflow for the simulation period would have required a pond of 360 x 360 meter (1200 x 1200 ft.) base dimension with the height of 4.2 meter (14 ft.) and the side slope of 30 to 1, which is a pond volume 9.13 times the actual pond volume. Through the year, the reservoir, however, accumulates the monthly available water to the maximum degree of storage capacity of 11.66 ha-m (94.5 acre-ft.). Thus, there is sufficient water available to irrigate more land.

IRRIGATION NEEDS

The timing of irrigations is determined by the irrigation limitation criteria described in previous chapter. The amount of irrigation applied each time was at two rate levels of 6.35 (0.25) and 12.7 mm/day (0.50 inches/day). For the irrigation rate of 6.35 mm/day (0.25 inches/day), as shown in Table VIII, the water depths irrigated were annually 12.6 cm (4.95 inches) for plot 1 double-cropped rotation management, 16.1 cm (6.32 inches) for plot 2 single-cropped rotation management, and 4.3 cm (1.68 inches) for plot 3 of continuous soybeans. For the 12.7 mm/day (0.50 inches/day), average irrigation amounts were somewhat smaller than for the 6.35 mm/day (0.25 inches/day) rate. It is suggested that seasonal net requirements in Bourbon County are 7.4 cm (2.9) for

soybeans, 10.4 cm (4.1) for sorghum, 17.3 cm (6.8 inches) for corn by Kansas Irrigation Guide (8).

The monthly distributions of irrigation amount are presented in Figure 7 and Figure 8, on the basis of various plots. Figure 12 shows the mean monthly overall irrigation water in units of hectare-meter (acre-ft.). These values were modified by considering weighted value of each plot and mean monthly irrigation depths on each plot shown in Figure 7 and Figure 8. From Figure 12, it can be seen that irrigation water for both irrigation rates were mostly needed in July and August. The values in this study are lower than stated requirements, but the differences are not large.

As can be seen in Figure 12, when the available water volume is taken into consideration, August may be a critical month to have a risk not to meet irrigation demand in a certain year. The ultimate purpose of supplemental irrigation is to save crops from disaster of drought and to increase crop yield even with a normal precipitation distribution. The monthly fluctuations of pond depth are presented in Figure 13 showing mean annual depths of 4.16 meters (13.86 ft.) for Zero-rate, 3.8 meters (12.68) for 6.35 mm/day (0.25 inch/day)-rate, and 3.87 meters (12.89) for 12.7 mm/day (0.50 inch/day)-rate. For the latter two irrigation rates, the mean pond depth in August was lowest. The observed pond depths in August were arrayed and plotted by manual fitting of curve, as shown in Figure 14 and in Figure 15, for the 6.35 (0.25) and 12.7 (0.50) rates, respectively.

By the irrigation criteria, when the reservoir storage volume is less than 5 percent of the maximum pond volume, irrigation is not allowed. The maximum pond volume is 11.65 ha-m (94.5 acre-ft.). Its 5 percent

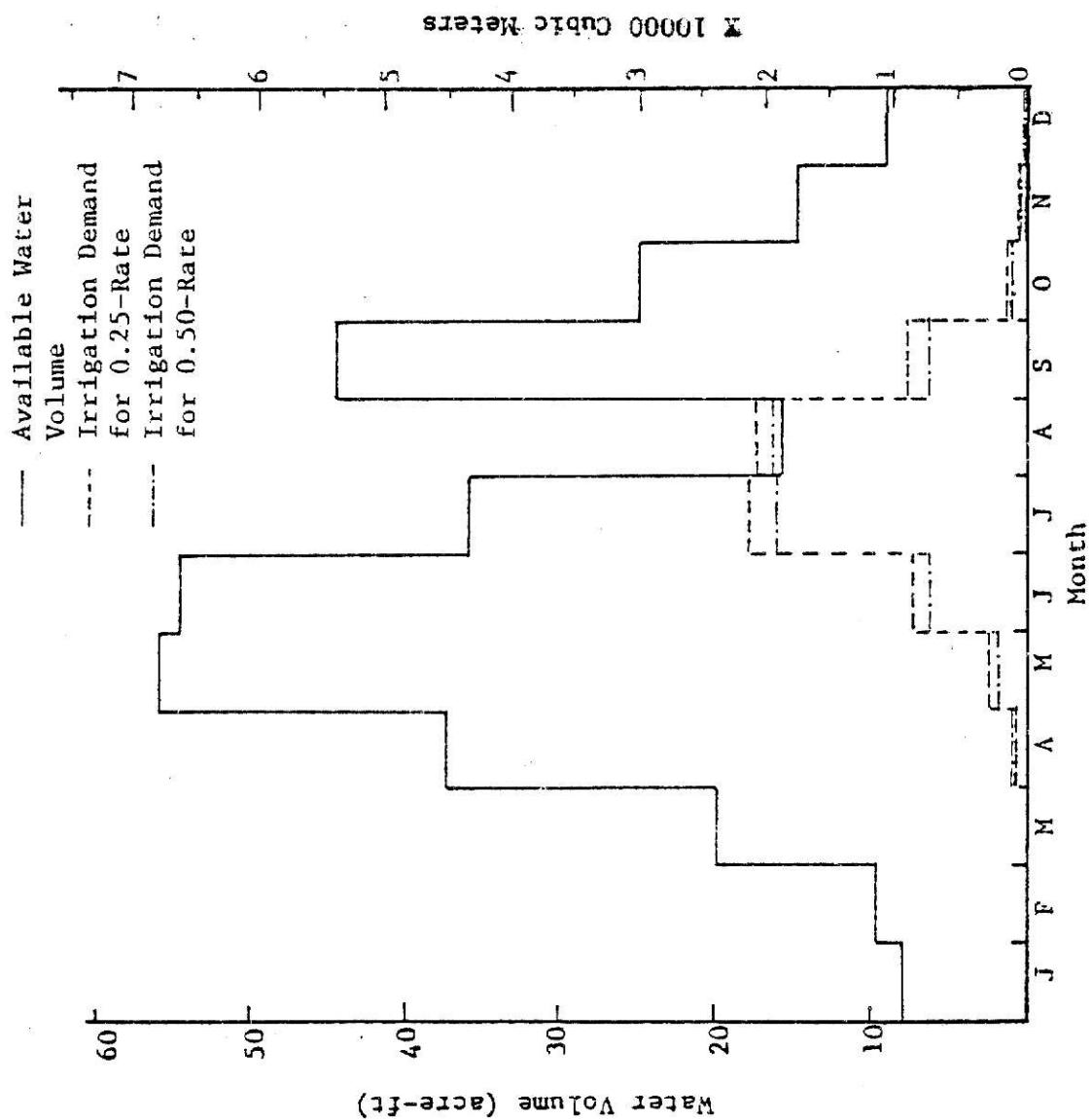


Figure 12. Available Water Volume and Irrigation Demand

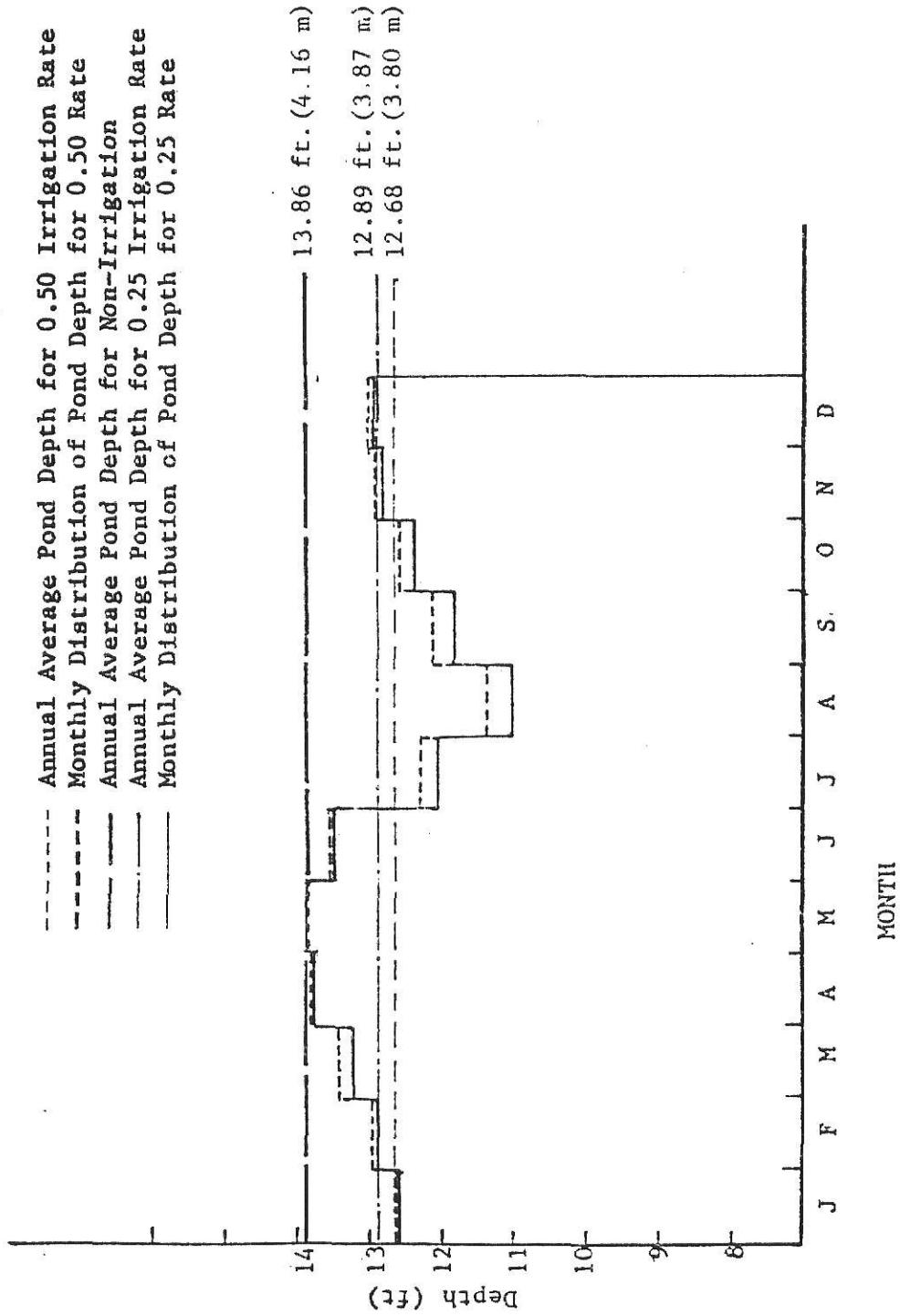


Figure 13. Monthly Distribution of Pond Depth

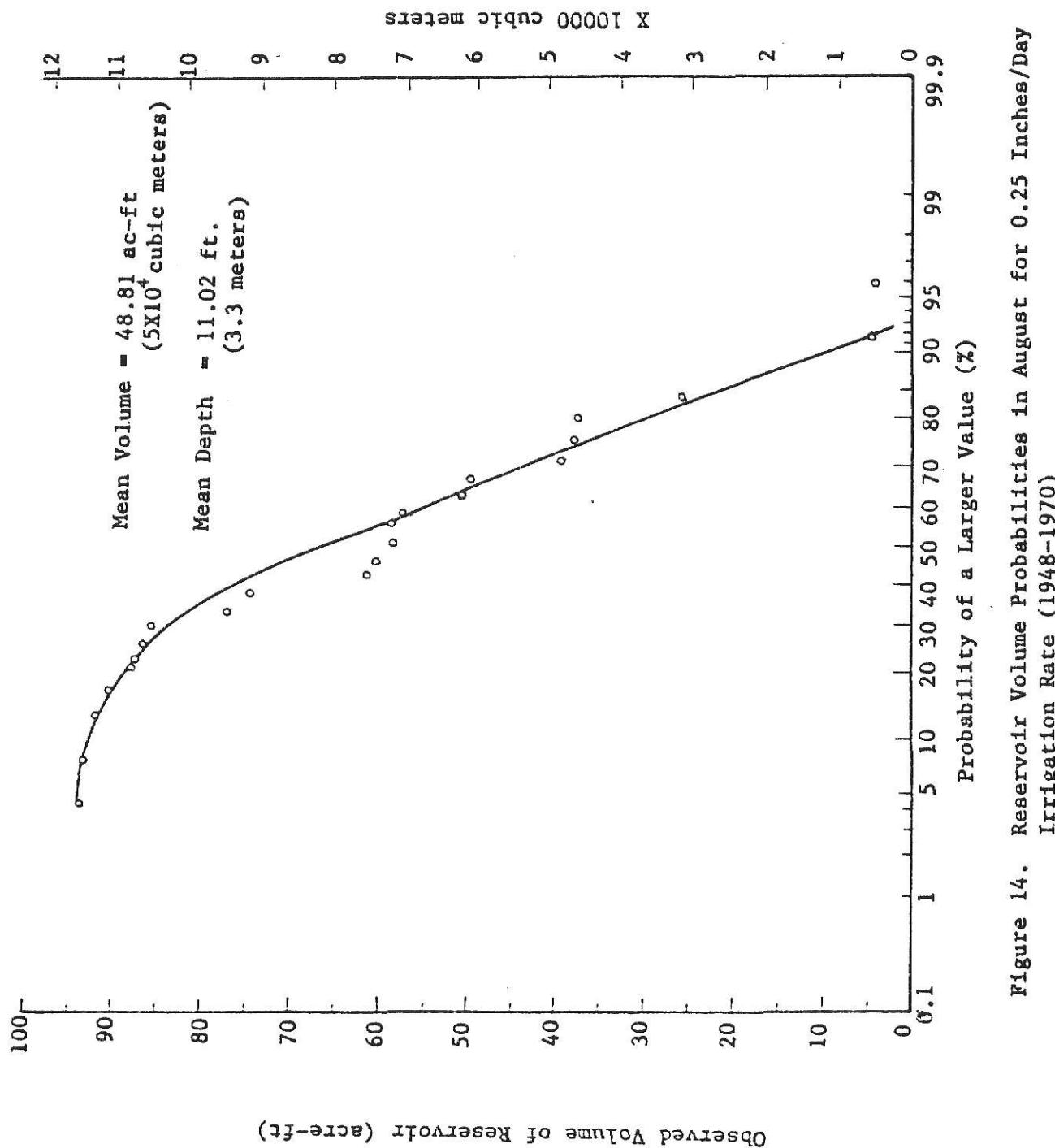


Figure 14. Reservoir Volume Probabilities in August for 0.25 Inches/Day Irrigation Rate (1948-1970)

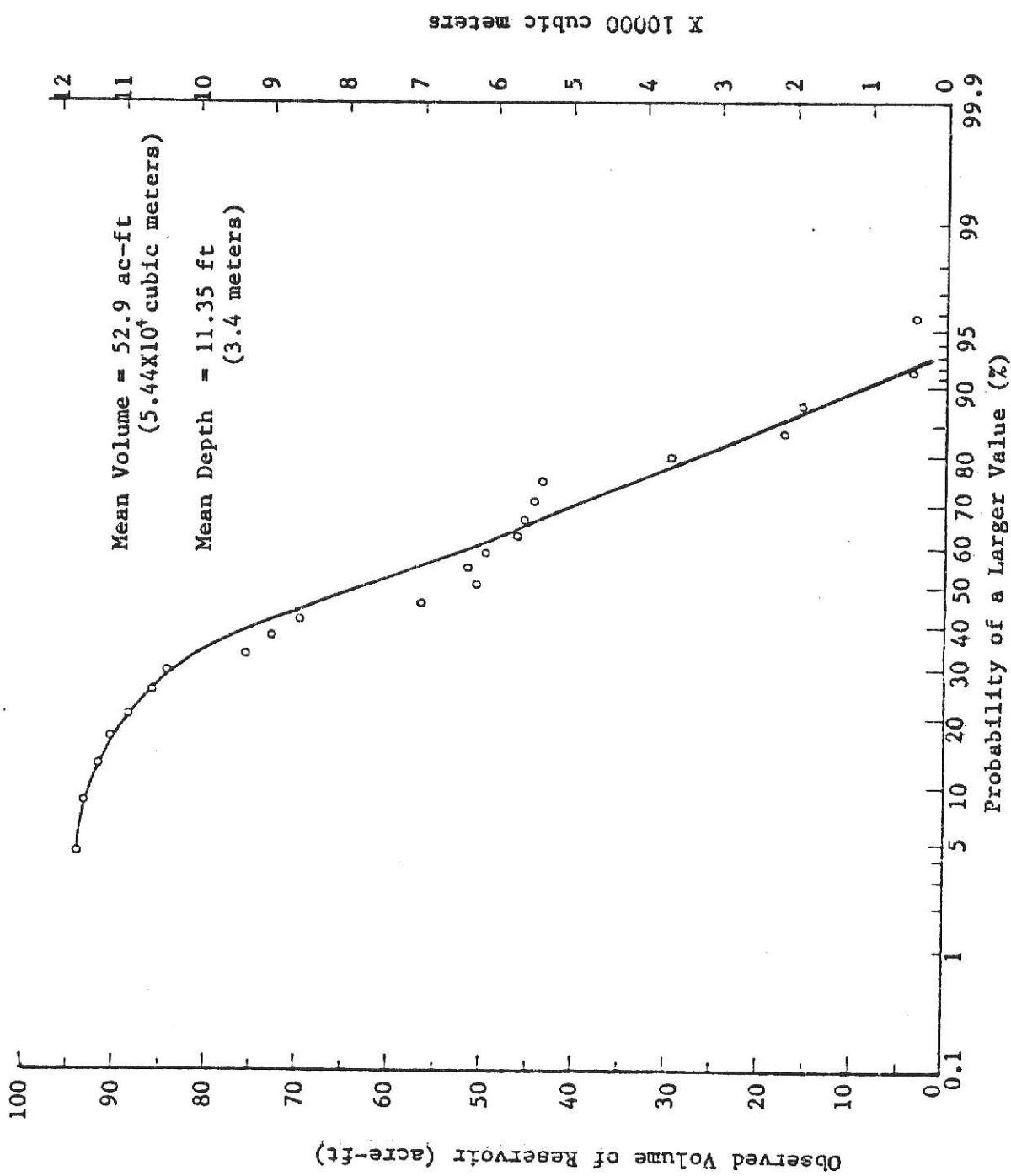


Figure 15. Reservoir Volume Probabilities in August for 0.50 Inches/Day Irrigation Rate (1948-1970)

volume is 0.583 ha-m (4.72 acre-ft.). This volume is equivalent to the pond depth of about 1.35 meters (4.5 ft.). Provided that the pond depth falls below 1.35 meters (4.5 ft.) in a month, there may be a risk not to meet the irrigation demand. It can be seen that the probability not to meet irrigation need in August is about 9 percent. The 9 percent risk can also be interpreted as one year out of 11 years. In other words, 58.68 ha (145 acres) could be irrigated at a 9 percent risk by the reservoir volume of 11.66 ha-m (94.5 acre-ft.).

CHAPTER VI
CONCLUSIONS AND RECOMMENDATIONS

Conclusions

The aim of this research is to study the feasibility of supplemental irrigation in sub-humid region by developing a general hydrologic crop management model. This purpose was achieved by testing a continuous watershed model. The runoff yield, precipitation to the storage pond, and evaporation were evaluated by this model. In addition, the irrigation demands were also estimated. Hence, the reliability of the pond was predicted. As a result of the model evaluation of Felt's farm,

1. an average of 75 percent of the total annual rainfall occurs in the growing season of April to September, and May and June are the months of greatest rain, while a noticeable decrease occurs in July and to a greater extent in August,
2. the runoff yield is sufficient to fill the storage reservoir so that the reservoir can be kept at the level of 3.80 meter (12.68 ft.) on the average when irrigation is conducted at the rate of 12.7 mm/day (0.5 inches/day),
3. the average annual water volume to be supplemented averages 6.17 to 6.78 ha-m (50 to 55 acre-ft.) for the 58.68-hectare (145-acre) irrigated area, and irrigation occurs mostly in August,
4. although the existing pond facility was never dry during the simulation period, in August it cannot meet the irrigation demand for the 58.68 hectares (145 acres) at the 9 percent probability level,
5. the model for general crop management is an effective tool to simulate various alternative cropping schedule on multiple irrigation plots.

Recommendations

In relation with future research, the following recommendations are made:

1. At a favorable probability level to meet irrigation demands, the optimal area of irrigable land with a specific pond should be studied.
2. Because of the assumption of no seepage loss from the reservoir yield budget, the net available water could be overestimated. Accordingly, a possibility failing to satisfy the water need might be neglected. A study for seepage loss should be conducted.

During the research project period, a crop yield model and an economic model will be developed to determine the feasibility of supplemental irrigation system by examining investment and operating costs, cash return from crop yield, and cash flow over an extended period of time.

NOTATIONS

a = empirical coefficient, which can vary geographically
AET = actual evapotranspiration
AW = available soil moisture (soil moisture content - permanent wilting point)
AWC = available water capacity (field capacity - permanent wilting point)
b = empirical coefficient, which can vary geographically
 B_1 = bottom surface area of a storage pond
 B_m = area of a plane at $h/2$ above the bottom
 B_2 = top surface area of a storage pond
c = geographic coefficient for Brunt relation in Penman Eq.
c' = hydraulic coefficient
cm = centimeter
CN = runoff curve number
d = geographic coefficient for Brunt relation in Penman Eq.
e = mass transfer coefficient
ES = saturated vapor pressure of a water surface at the Ta
 E_S = soil evaporation
h = depth of a pond
ha = hectare
ha-m = hectare-meter, unit of volume
i = hydraulic gradient
IA = initial abstraction
K = crop consumptive use coefficient
 K_c = coefficient of crop growth stage
 K_t = climatic coefficient for the calculation of crop consumptive use coefficient

m = meter
mm = millimeter
P = precipitation
PET = potential evaporation
PSUNS = percent sunshine
Q = surface runoff
r = reflectance coefficient (albedo)
Ra = solar radiation
RHD = relative humidity
S = potential maximum difference between precipitation and runoff
t = time after the first stage evaporation
T = mean daily air temperature in °K (Kelvin)
Ta = mean daily air temperature in °F (Fahrenheit)
U = upper limit stage two evaporation
V = volume of a pond
WVD = wind velocity
 Δh = change in soil water potential over distance ΔZ
 ΔZ = change in elevation

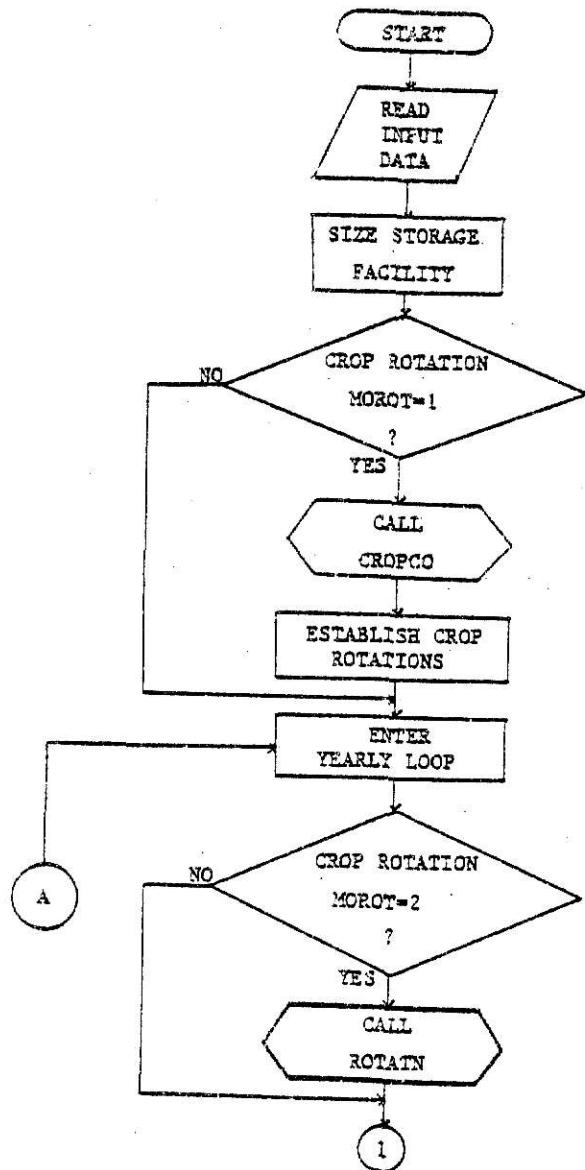
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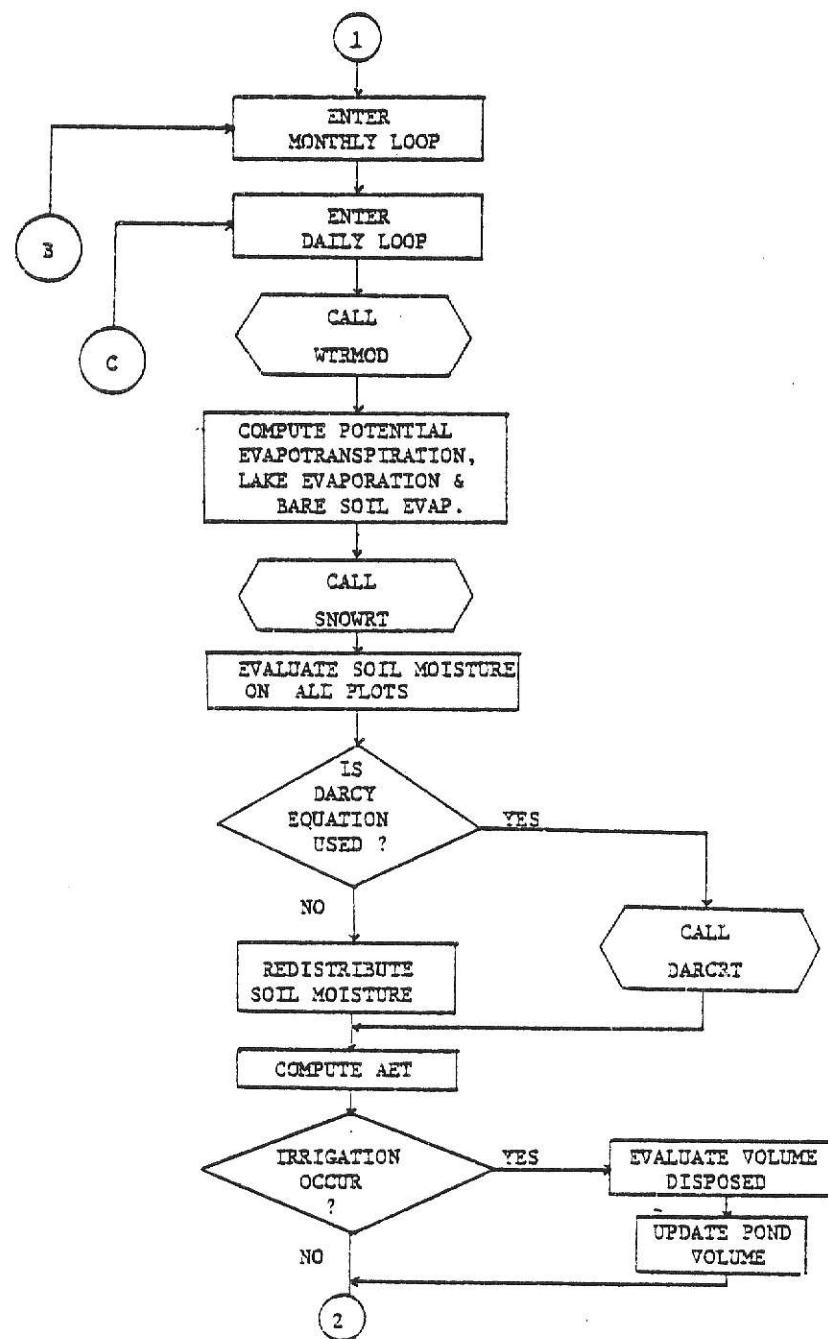
APPENDICES

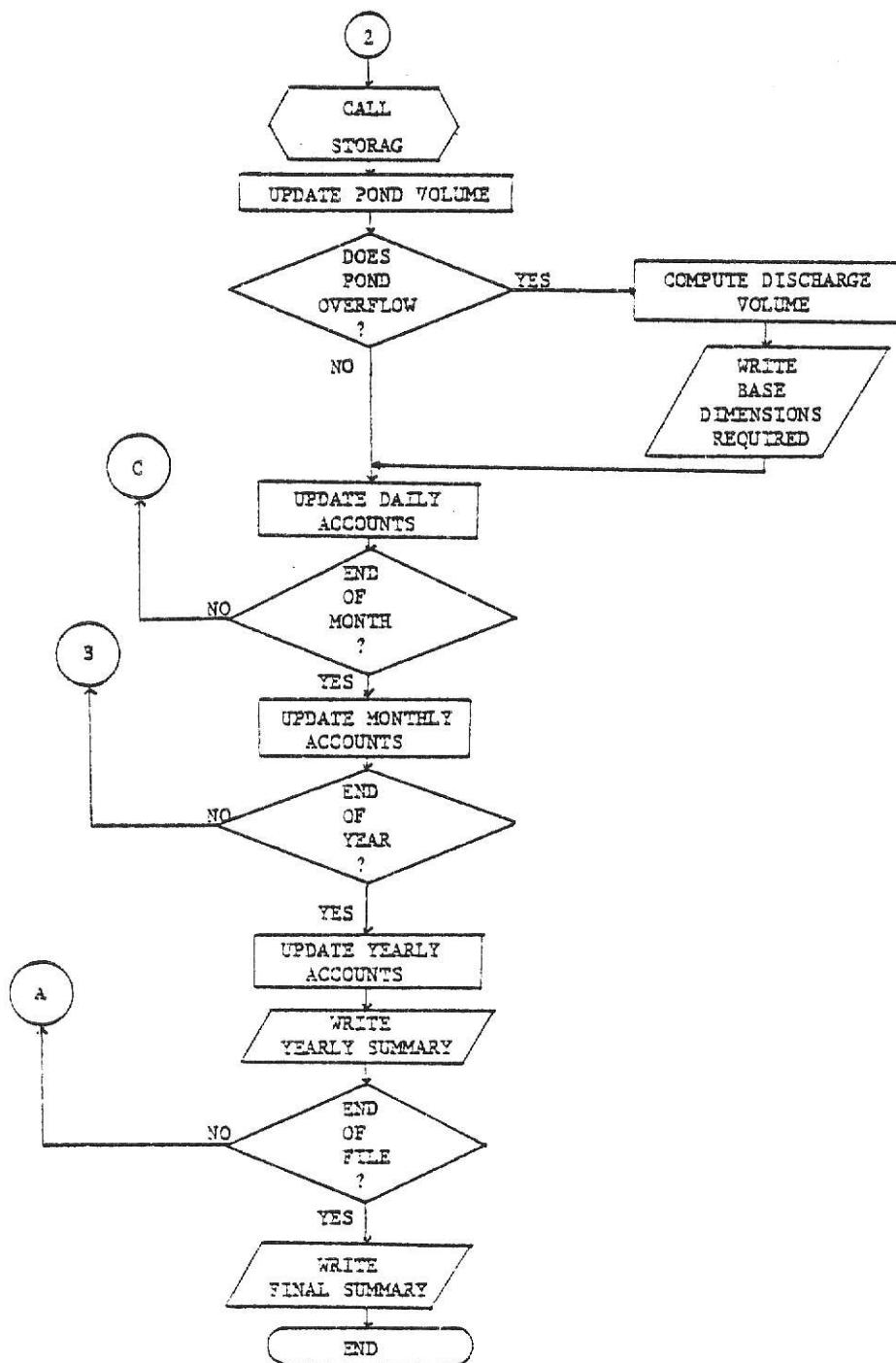
- I Generalized Flow Chart For KSUHYDRO Model
- II-(a) Guideline For Input Data Cards
- II-(b) Description Of Input Data
- II-(c) Example Of Input Data Card Deck
- III Nomenclature Of Variable Names Used
In The Computer Program
- IV Listing Of Computer Program

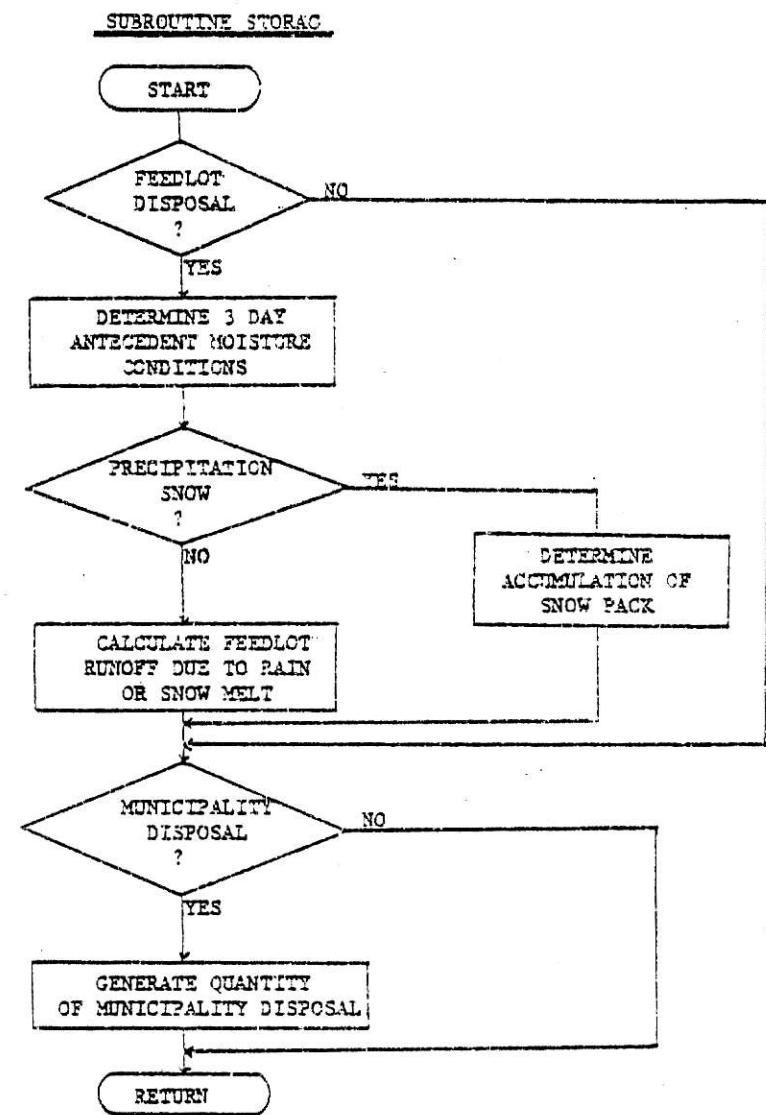


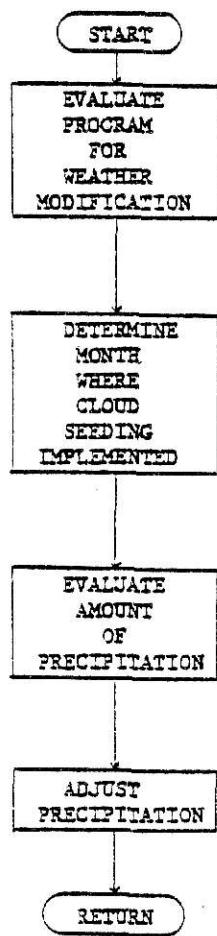
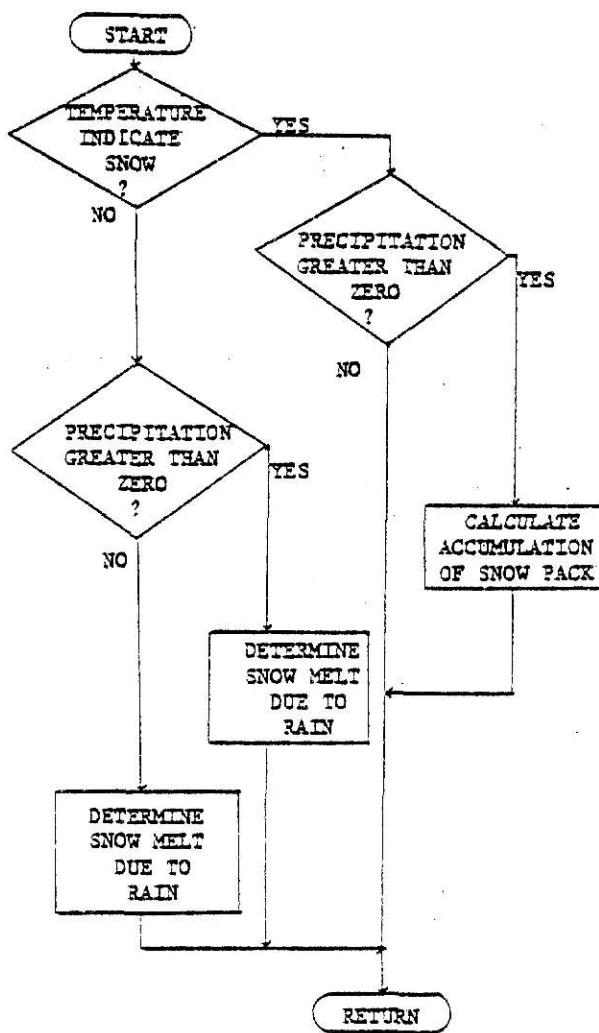
APPENDIX I GENERALIZED FLOW CHART FOR MAIN

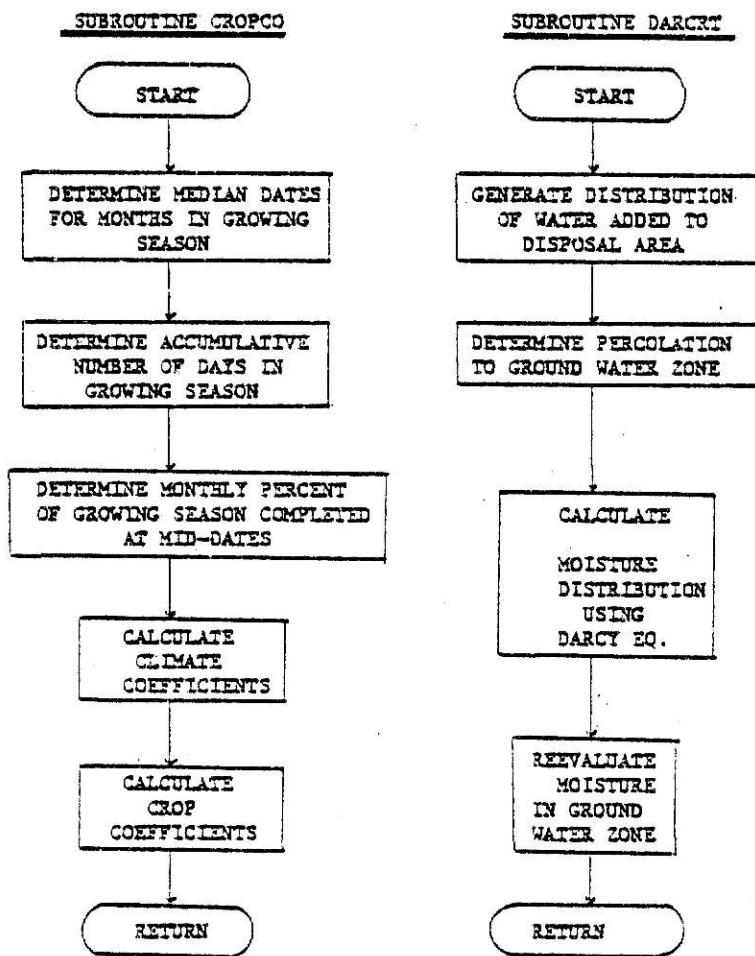
*FROM HAYDEN (2)







SUBROUTINE WTRMODSUBROUTINE SNOWRT



APPENDIX II-(a) GUIDELINE FOR INPUT DATA CARDS (KSUHYDRO)

1. Location and Model Identifiers

NAME OF CITY AND STATE		
1	20	40

1	2	22
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1	2	6	8
---	---	---	---

2. Simulation Model Parameters

1	2	6	8
---	---	---	---

1	2	7	9
---	---	---	---

1	2	6	8
---	---	---	---

3. Meteorological Data (one card for each month)

1	3	4	5	6	7	10	11	13	14	16
---	---	---	---	---	---	----	----	----	----	----

4. Disposal Area Data

Scheme I (when MOROT=1) (one card for each area)

IAREA(1,1)	80
1 3 6 8	i j
<hr/>	
AREA	80
1 2 7	

IPLAN	ROTATE	80		
1 2	3 4			
<hr/>				
MGSBP	DGSBP	MGSEP	DGSEP	80
1 2	3 5	6 8	9 11	12

Scheme II (when MOROT=2)

(1) Crop Rotation Data and Disposal Area Data (one card for each area)

RCYCLE	DOUBLE	TEALWT	IPLAN	IAREA(soil type)	AREA	80
1 3	4 5	6 7	8 9	10 11	12 13	18

(2) Crop type and Planting and Harvesting Data (Depending on repetition year, select required number of crops and planting and harvesting dates on each plot)

NRCCROP	MGSBP	DGSBP	MGSEP	DGSEP	80
1 3	4 5	6 7	8 9	10 11	

(3) Wheat Crop Data (If double cropping managed, select planting and harvesting dates matching the number of plots double cropping being concerned)

MGSBW	DGSBW	MGSEW	DGSEW
1	6	7	8
10	11	12	13

5. Unsaturated Flow Data (one card for each area) Skip, if DARCEQ=2

CONDUZ	CONDLZ	CONDGW	HUZ	HLZ	HGWZ
1	10	11	20	21	30
31	40	41	50	51	60

6. Municipal Waste Water Data (one card for each month) Skip, if BYPASS=1 or 2

MUNDIS	
1	10

7. Magnetic Tape Driver to Control Climatological Data of Daily Rainfall and Max. and Min. Air Temperature for a Specified Weather Station

APPENDIX II-(b) DESCRIPTION OF INPUT DATA

1. Location and model identifiers

2. Simulation model parameters

(1) NAMELIST/SEED

MODEL=1	No Cloud Seeding	WPCNT=1.0
	2 B-Zero Modification	1.0
	3 Rainfall Increase (%)	any value
	4 B-Zero Modified Alteration Scheme	1.0

(2) NAMELIST/ALPHA

DORM :	Precipitation routed through SCS Eq. from April through October	Usually 1.0 inch
GROW :	Precipitation routed through SCS Eq. from November through March	Usually 1.25 inches
PCVMAX :	Level of pond below which irrigation not allowed, expressed as a ratio of max. volume	Usually 0.05
RCROP :	Reflectance coeff. (albedo) of crop as a ratio	Usually 0.23
E :	Wind coeff. e , in Penman Eq. when calculating potential ET.	Usually 0.75
PAVLU :	Percentage (as a ratio) of available soil moisture in upper zone below which irrigation allowed	0.9 : Intensive Irrigation 0.5 : Normal Irrigation 0.0 : No Irrigation
DSRATE :	Irrigation disposal rate (inch/day)	
MOROT :	Identifier for rotation scheme	1 : Scheme I 2 : Scheme II
BRUNTA, BRUNTB :	Coeff. , c and d , respec- tively, for Brunt relation in Penman Eq.	

Location	BRUNTA	BRUNTB	Location	BRUNTA	BRUNTB
Belleville	0.62	0.039	Hays	0.78	0.035
Colby	0.79	0.035	Horton	0.60	0.040
Dodge City	0.79	0.034	Independence	0.59	0.039
Ellsworth	0.60	0.033	Topeka	0.66	0.041
Garden City	0.80	0.034	Chanute	0.62	0.039
Good Land	0.75	0.036	Ft. Scott	0.64	0.040

(3) NAMELIST/BETA

HMAX : Max. depth of pond (ft)	
W : Base width of pond (ft)	
L : Base length of pond (ft)	
S : Pond side-slope as a ratio of Run/Rise	
INDST : Weather station identifier	
MSTART : Beginning month of simulation	
YSTART : Beginning year of simulation	
YEND : Ending year of simulation	
ROTAYR : Parameter for rotation scheme I	1 : Crop/Fallow 2 : Fallow/Crop
STORM : 25 year-24 hour storm	
LTAREA : Total area of plots (acre)	
NPLOTS : No. of plots in accordance with land use plan	
BYPASS : Source of inflow to the pond	1 : No feedlot and No municipal input 2 : Feedlot and No municipal input 3 : No feedlot and Municipal input 4 : Feedlot and Municipal input

DARCEQ : Moisture redistribution Parameter	1 : Moisture redistribution within the soil profile by Darcy Eq. for one-di- mensional flow. 2 : Moisture redistribution by the simplified method
---	--

Location	INDST	YSTART	YEND	STORM
Belleville	0682	1949	1973	5.1
Colby	1699	1950	1962	4.5
Dodge City	2164	1949	1973	4.6
Ellisworth	2459	1946	1970	5.4
Garden City	2980	1950	1974	4.5
Goodland	3153	1949	1973	4.3
Hays	3527	1948	1973	4.7
Horton	3810	1946	1970	5.9
Independence	3954	1948	1972	6.7
Topeka	8167	1949	1973	6.1
Chanute	1427	1948	1973	6.7
Ft. Scott	2835	1948	1973	6.6

3. Meteorological Data

PSUNS : Percent sunshine (%)
 RHD : relative humidity (%)
 WIND : Wind velocity (mph)
 RA : Mid-monthly intensity of solar radiation
 MMAT : Mean monthly air temperature

4. Disposal Area Data

Scheme I (when MOROT=1)

IAREA(i,j) : Name for crop and soil type

i : Crop type	j : Soil type
1 : wheat	One among 12 types of soil
2 : sorghum	classified by SCS
3 : corn	
4 : soybean	
5 : pasture	
6 : alfalfa	
7 : fallow	
AREA : Area of a plot	
IPLAN : Plan implemented on disposal area	
ROTATE : Parameter for rotation scheme I	
MGSBP,DGSBP,MGSEP,DGSEP : Planting and harvesting dates	
	1 : Collect Runoff
	2 : Runoff and Irrigation
	3 : Irrigation only
	1 : Crop rotation with fallow
	2 : Same crop each year

Scheme II (when MOROT=2)

(1) Crop Rotation Data and Disposal Area Data

RCYCLE : Required number of year for sequential crop rotation	
1 : No crop rotation , i.e., same crop each year	
2 : Two-year crop rotation	
Up to seven-year rotation	
DOUBLE : 1 : Single cropping	
2 : Double cropping with one fallow term in two years (wheat)	
IFALWT : 1 : For the first year of simulation period, begins with wheat on a double-cropped area	
2 : For the first year of simulation period, begins with fallow on a double-cropped area	
IPLAN,IAREA,AREA : previously defined	

(2) Crop type and planting and harvesting dates

(N number of cards for each area : N= The value of RCYCLE)

NCROP : Name of crop

MGSBP,DGSBP,MGSEP,DGSEP : Planting and harvesting dates

(3) Wheat crop data

MGSBW : Month growing season begins, for winter wheat

DGSBW : Day growing season begins, for winter wheat

MGSEW : Month growing season ends , for winter wheat

DGSEW : Day growing season ends , for winter wheat

(Cards for some area which double cropping is considered)

5. Unsaturated flow data

CONDUZ,CONDLZ,CONDGW : Hydraulic conductivity for upper zone, lower
zone, and ground water zone, respectively

Huz,HLZ,HGZW : Soil water potential

6. Municipal waste water input to the pond

MUNDIS : Municipal disposal (gal/day) - (One card per month)

7. Magnetic tape driver to handle TMAX(ND),TMIN(ND),and PREC(ND) data

for a location of simulation analysis

Note : TMAX Daily maximum air temperature

TMIN Daily minimum air temperature

PREC Daily rainfall

*ND Number of days in a month

APPENDIX II-(c) EXAMPLE OF INPUT DATA CARD DECK (MROT=2)

4. (1)

(2)

(3)

2

APPENDIX III

NOMENCLATURE OF VARIABLE NAMES
USED IN THE COMPUTER PROGRAM

Variables	Definition
AREA	Size of plot (acres)
AVAILL	Percent of available soil moisture remaining in lower zone
AVAILU	Percent of available soil moisture remaining in upper zone
AET	Actual evapotranspiration
AETLZ	Actual evapotranspiration of lower zone
A1	Length times width of pond base
A2	$S * (L + W)$
A3	$(4/3) * S ** 2$
A4	$2 * A2$
A5	$4 * S ** 2$
ACTIRR	Accumulated total irrigation
ABST	Average daily air temperature in degree Kelvin
APREC	Average annual precipitation
AVGMD	Average annual moisture deficit
ASTAT	Alphanumeric input statistical occurrences of intensity
AREA	Size of plots
AETU	Actual evapotranspiration for the upper zone
AETL	Actual evapotranspiration for the lower zone
AMONTH	Alphanumeric names for months to make table
AVLFCL	Available water capacity for the lower zone
AVLFCU	Available water capacity for the upper zone
AINTER	Average annual disposal area interception
AAETRS	Average annual disposal area evapotranspiration
ACHSOM	Average annual disposal area change in soil moisture
ALPHA	Feedlot parameters in NAMELIST
B2	$(W + 2SH) * (L + 2SH)$
BYPASS	Establishes feedlot runoff and/or municipal waste as inflow to pond
BRUNTA	Geographical constant for radiation
BRUNTB	Geographical constant for radiation
BETA	Pond and plot parameters in NAMELIST
CROP	Name of crop
CM	Total number of discharges
CTPDAY	Cumulative total of days rainfall occurred
CENT	Average daily air temperature in degrees Centigrade
CCROP	Type of crop on plot
CTRL	Amount of control to stop pond from overflowing
CNTR	Increment for number of times runoff occurred from plot
CMNEW	Average number of discharges
COUNT	Average number of years having a discharge per year
CONOUZ	Moisture conductivity of the upper zone
CONDLZ	Moisture conductivity of the lower zone
CONDGW	Moisture conductivity of the ground water zone
CTP	Percent of days rainfall exceeded frequency

Variables	Definition
CNS1	Curve numbers of soil type 1 SCS Method
CNS3	Curve numbers of soil type 3 SCS Method
CNS5	Curve numbers of soil type 5 SCS Method
CNS12	Curve numbers of soil type 12 SCS Method
CTPR	Name of month for statistical data
CTRDAY	Number of days runoff occurred from plot during simulation period
C	Degree-day coefficient in °F-day
DGSB	Day growing season begins for crop
DGSE	Day growing season ends for crop
DGSBW	Day growing season begins for wheat
DSRATE	Disposal rate
DOUBLE	Double cropping with wheat and some summer crop reserving fallow term
DGSBP	Day of month crop is planted
DGSEP	Day of month crop harvested
DSCVOL	Discharge volume
DSDAYS	Number of disposal days
DPERC	Amount of percolation out of lower zone
DARCEQ	Integer that determines whether soil is saturated or unsaturated for flow of water through the soil
DSDAY	Cumulative sum of disposal days
DELTA	Slope of saturated vapor pressure-temperature curve
DSAREA	Area of plot on disposal area
DORM	Applies to feedlot runoff
DV	Difference between actual volume and calculated volume of zone
DVDH	Difference between actual and calculated volume with respect to the difference between actual and calculated height of pond
DSCHRG	Amount of water overflowed from pond (VC1 - VCB)*12
DIM	
DSNOW	Change in snow storage
DRY	Lowest annual precipitation
DSCRG	Discharge to plots from pond, also uncontrolled discharge for municipal control
DGSBP	Day of month crop is planted
DGSEP	Day of month crop is harvested
DISVOL	Disposal volume or irrigation volume
DSRNFF	Average annual disposal area runoff
DSPERC	Average annual disposal area percolation
DAYDS	Average annual number of disposal or irrigation days
EPRIM	E prime factor for Penman equation, wind coefficient when calculating lake evaporation
EVAPLK	Cumulative sum of lake evaporation
EXCESS	Runoff and excess water
ES	Daily calculated actual saturated vapor pressure in millibars (mb)
ESA	Daily calculated actual vapor pressure, mb

Variables	Definition
EA	Convective losses, mm H ₂ O
E	Emissivity
EALAKE	Convective losses for a large body of water
ER	Amount of water that could runoff, unadjusted
EVAP	Average annual lake evaporation
EO	Difference between field capacity and actual soil moisture in upper zone
FREEZE	Sum of three consecutive days average temperature, if less than 64°F, then soil is frozen
FROZE	Condition of moisture in soil
FCGW	Field capacity in the ground water zone
FREQ	Specified amount of rainfall for stacistical analysis
FCL	Field capacity of the lower zone
FCU	Field capacity of the upper zone
GAMMA	1 - DELTA, psychrometric constant
GROW	Applies to feedlot runoff
H	Height of water in pond or length of base of pond
HMAX	Maximum depth of pond
HAPRX	Approximate height of surface of pond
HUZ	Soil water potential variable for hydraulic conductivity in upper zone
HLZ	Soil water potential variable for hydraulic conductivity in lower zone
HGW	Soil water potential variable for hydraulic conductivity below lower zone
I	Integer increment for plots
IW	Integer increment for plots
IAREA	Crop name defined monthly, and soil type
IYRCRP	Name of crop defined yearly
IWHT	Temporary storage for wheat or fallow for double cropping
IWI	Temporary storage for wheat or fallow for double cropping
ITEMP	Temporary storage for crop name for data inputs
IFALWT	In first year of simulation, begin with wheat 1 or fallow 2
IPLAN	Irrigation implementation plan
IRRSUM	Cumulative sum of irrigation water applied
IA	Amount of intercepted rain on surface (Initial abstraction)
IDAY	Number of irrigation days
I	Number of individual plot integer increment
II	Number of plot
IDISDA	Number of potential disposal days yearly
INDST	Index of station in question
IPLCT	Number of plot
IRRVOL	Average annual volume of irrigation water, also average annual depth of water applied
INUMI	Number of individual plots plus five
INUM	Number of individual plots plus one
IYRCRP	Name of crop defined yearly

Variables	Definition
IAREA	Crop name defined monthly for subroutine ROTATN
IPLAN	Irrigation plan implementation
INCROP	Temporary storage for type of crop
IAADD	Amount of interception storage for each month
IAET	Initial absolute evaporation
J	Integer increment
JJ	Number of plot
JDISDA	Cumulative number of disposal days
JM	Incremental number of plot
K	Integer increment for rotating crops for each year
KCROP	Crop coefficient
K	Integer increment of plot
KAN	Name of state, Kansas
KI	Incremental number of a plot
KT	Number of plot
KCROP	Crop coefficient from Blaney-Criddle Method
KROP	Alphanumeric name for crop of interest
L	Length of base of storage pond in feet
LTAREA	Feedlot area
LKEVPT	Estimated lake evaporation yearly
LAKEVP	Potential evaporation from lake
MSTART	Number of month program starts
MMM	Required years of rotating crops on an individual plot
MGSB	Month growing season begins for crop
MGSE	Month growing season ends for crop
MGSBW	Month growing season begins for wheat
MGSEW	Month growing season ends for wheat
MMAT	Mean monthly air temperature
MGSBP	Month crop is planted
MGSEP	Month crop is harvested
M	Snowmelt due to atmospheric conditions and rain
MA	Snowmelt due to atmospheric conditions
MR	Snowmelt due to rain
MM	Integer increment
MOROT	Indicates type of rotation model
MAXVOL	Percent of maximum pond volume required yearly
MSTART	Month that program starts in
MONTH	Month of data on tape
MODEL	Denotes type of crop management
MQ	Number of plot
MS	Incremental integer of plot
MP	Incremental integer of a plot
MMAT	Mean monthly air temperature
MUNDIS	Municipal disposal amount on a monthly basis
MGSBP	Month when crop is planted
MGSEP	Month when crop is harvested

Variables	Definition
NPLOTS	Number of plots
NNN	First year of simulation for a single plot
NDIM	Number of days in month
NRCROP	Crop name for data inputs
NPLOTS	Total number of plots
NY	Number of years in loop
NM	Number of month after MSTART to end of year
NDAYS	Number of days in month
ND	Number of days in daily loop
NNN	Number of plot plus one
NCNT	Incremental integer of plot that needs irrigated
NR	Number of years in rotation period
NRCROP	Crop name for data input
NIA	Net intercepted amount for each plot
NRNOF	Monthly amount of direct stored runoff
NOPERC	Amount of deep percolation
NAMES	Alphanumeric input for headings
PLAREA	Area of plot
POT	Potential daily temperature
PEAK	Greatest single discharge in a given time period
PREVDS	Previous disposal carry over
PACK	Amount of snow on ground at end of year
PACKPY	Amount of snow on ground
PDVOL	Pond volume
PERC	Percolation
P1	Previous day's moisture
P2	2 day's previous moisture
P3	3 day's previous moisture
PLOT	Number of plot
PREVYR	Previous year before current year
PSAREA	The direct receiving area of the facility
PLAREA	Area of plot
PAVLU	Percentage of available water field capacity
PET	Calculated potential evapotranspiration
PETBS	Potential evaporation from bare soil
PRECIP	Amount of rainfall for a single day
PERCL	Water cascaded to lower zone for storage
PCVMAX	Usually five percent of pond volume
PCNTRL	Percent of control to stop pond from overflowing
PCWW	Percent of wastewater controlled
PDACCT	Pond account
PREC	Daily precipitation
PSUNS	Percent amount of sunlight each month
PWPLZ	Permanent wilting point of lower zone
PWPZ	Permanent wilting point of upper zone
PRECAC	Accumulated precipitation by plot and month
PWG	Permanent wilting point of growing zone

Variables	Definition
RPAVLU	Percentage of available water in soil
RCYCLE	Required years of rotating crops on a plot
RPAVLU	Percent of available moisture capacity in upper zone to start irrigation
ROTAYR	Crop/fallow rotation plan
R	Equals RCROP
RCROP	Shortwave reflectance
RN	Daily calculated net radiation in mm water
RNSOIL	Daily net radiation on soil
RNLAKE	Daily net radiation on lake
RUNMDS	Runoff from disposal area
RAIN	Amount of rain for a single storm
RNOF	Amount of water that could run off, unadjusted
RUNOFF	Feedlot runoff
RANGE	Annual precipitation range for years of study
ROTATE	Crop rotation
RCYCLE	Required years of rotating crops on a plot
RA	Monthly average of solar radiation
RCM	Runoff curve number modified
RCN	Runoff curve number
RHD	Monthly average relative humidity
RUNACO	Accumulated runoff by plot and month
SOIL	Type of soil ***SCS Method***
SMMAXL	0.9 * FCL (SOIL) - SMLZ (JJ), % of maximum available water in lower zone
SMUZPR	Initial amount of soil moisture in the upper zone, 3.25 in.
SMPREV	Soil moisture initially in growing zone
SNOW	Amount of snow covering soil
SNOMLT	Amount of snow melted each day
STRVOL	Cumulative amount of stored runoff
S	Run to rise of side slope
STORM	Size of critical event
STIND	Station index
SNOVAP	Amount of snow melted for a single day
STRNOF	Stored runoff per area of watershed
SI	Maximum potential difference between rainfall and runoff at start of storm
SMMAXU	Present storage available in upper zone
SEVAP	Free surface evaporation of the pond
SMPD	Soil moisture in the upper and lower zone, combined
SM	Soil moisture in the growing zone
SMUZ	Soil moisture in the upper zone
SMLZ	Soil moisture in the lower zone
SMGWZ	Soil moisture in the groundwater zone
SMACCT	Soil moisture account (plot, crop, water, month)
SMASTL	Saturated soil moisture content of lower zone
SMSATU	Saturated soil moisture content of upper zone
SMSATG	Soil moisture at saturation in growing zone
SEED	Weather modification parameters in NAMELIST

Variables	Definition
TPAREA	Total disposal area
TPREC	Total precipitation
TOPERC	Total deep percolation
TRNOF	Total runoff
T1	Previous day's average temperature
T2	Average temperature of two day's prior
THAWED	Sum of three consecutive day's average temperature, if greater than 114, then soil is thawed
T	Days
TAVG	The average daily air temperature degrees Farenheit
TMAX	Highest temperature of the day °F
TMIN	Lowest temperature of the day °F
UZSMCH	Change in upper zone soil moisture
UZEVAP	Upper zone moisture evaporation
U	Upper limit of stage 2 evaporation
VOLDIS	Amount of water disposed
VLOMAX	Maximum volume held by storage facility
VOLIRR	Volume for irrigation
VOLCHG	Amount of change in volume for pond
V	Volume of pond in cubic feet
VC	Calculated volume of pond
VOLMX1	Size of pond to stop overflowing
VCB	$2 * S * HMAX$
VCC	$(4/3) * S ** 2 - (VOLMX1 * 3630/HMAX)$
VCD	$VCB ** 2 - (4 * VCC)$
WASTWW	Cumulative sum of waste water controlled
WET	Highest annual precipitation for years of study
WATER	Daily precipitation
W	Width of base of storage pond in feet
WPCNT	Percent increment
WINDD	Monthly average daily windrun miles per day at 2 mtrs hgt
WIND	Monthly average windrun
YSTART	Starting year of simulation
YEARS	Number of years of simulation
YEND	Last year of simulation
YEAR	Year of data on tape

APPENDIX IV
LISTING OF COMPUTER PROGRAM

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KANSAS STATE UNIVERSITY
HYDROLOGICAL WATERSHED MODEL

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 0079 50 FORMATT(10,2)
 C*** RUMOUFF CURVE NUMBERS FOR SOIL AND CROP TYPES
 0080 DO 55 K=1,7
 0081 RCM1(K)=CNS1(K)
 0082 RCM2(K)=CNS1(K)
 0083 RCM3(K)=LNS3(K)
 0084 RCM4(K)=CNS3(K)
 0085 RCM5(K)=CNS5(K)
 0086 RCM6(K)=CNS5(K)
 0087 RCM7(K)=CNS5(K)
 0088 RCM8(K)=CNS5(K)
 0089 RCM9(K)=CNS5(K)
 0090 RCM10(K)=CNS5(K)
 0091 RCM11(K)=CNS5(K)
 0092 RCM12(K)=LNS2(K)
 0093 55 SIZING PUND VOLUNE ROUTINE
 A1=L*H
 A2=S*(L+W)
 A3=S*/3.*S**2
 A4=S*/A2
 A5=S**4
 C*** VOLMAX IS THE MAXIMUM VOLUME HEAD BY THE STORAGE FACILITY
 0094 VOLMAX=(A1*HMAX+A2*HMAX**2+A3*HMAX**3)/3600.
 C*** PSAREA IS THE DIRECT LIVING AREA OF THE FACILITY
 0095 PSAREA=(W**2*S*HMAX)*(L**2*S*HMAX)/43560.
 C*** CALCULATE THE CROP COEFFICIENTS
 0096 IF(MORDT-E02) GO TO 61
 0097 DO 60 K=1,NPLOTS
 0098 MGSE=MGSDP(K)
 0099 MGSD=DSUP(K)
 0100 MGSE=MGSEP(K)
 0101 MGSE=DUSEP(K)
 0102 CROP=IAREA(K,1)
 0103 CROP=CROP*(ACROP,MGSD,DSUB,MGSE,DUSEP,MAT1)
 0104 INCRUP(K)=IAREA(K,1)
 0105 60 CONTINUE
 0106 61 CONTINUE
 0107 INITLIZE VARIABLES
 0108 C*** INITLIZE VARIABLES
 0109 60 CONTINUE
 0110 61 CONTINUE
 0111 62 CONTINUE
 0112 63 CONTINUE
 0113 64 CONTINUE
 0114 65 CONTINUE
 0115 66 CONTINUE
 0116 67 CONTINUE
 0117 68 CONTINUE
 0118 69 CONTINUE
 0119 70 CONTINUE
 0120 71 CONTINUE
 0121 72 CONTINUE
 0122 73 CONTINUE
 0123 74 CONTINUE
 0124 75 CONTINUE
 0125 76 CONTINUE
 0126 77 CONTINUE
 0127 78 CONTINUE
 0128 79 CONTINUE
 0129 80 CONTINUE
 C*** RUNACC(L,J)=0.0
 0130 70 J=2,9
 0131 71 J=1,12
 0132 72 J=0,0
 0133 73 I=1,NPLOTS
 0134 74 IPAREA=IPAREA+AREA(I,I)
 0135 75 EOL(I)=0.0
 0136 76 LAE(I)=0.0
 0137 77 IADD(I)=0.0
 0138 78 DISVAL(I)=0.0
 0139 79 DAYSDS(I)=0.0
 0140 80 DSROFF(I)=0.0
 0141 81 AINER(I)=0.0
 0142 82 AAETRS(I)=0.0
 0143 83 ALISOM(I)=0.0

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0171      C      00 980 NY=1,YEARS
0172      C      DO 160 I=1,13
0173      C      DO 150 J=1,11
0174      C      DO 140 K=1,NPLOTS
0175      C      IF(J.LE.8)SMACCT(I,J,K)=0.0
0176      C      150 PDACCT(I,J)=0.0
0177      C*** CONTINUE
0178      C*** ESTABLISH CROP ROTATIONS
0179      C      IFIMUR1=I.O.2) GO TO 195
0180      C      DO 170 K=1,NPLOTS
0181      C      LAREA(K,1)=INCROP(K)
0182      C      IF(ROTAYR1.O.1) GO TO 190
0183      C      DO 180 J=1,NPLOTS
0184      C      IF(LAREA(J,1)) EO.1) GO TO 180
0185      C      IF(ROTATE(J,1)) EO.2) GO TO 180
0186      C      LAREA(J,1)=I
0187      C      180 CONTINUE
0188      C      ROTAYR1
0189      C      190 ROTAYR2
0190      C      195 CONTINUE
0191      C      C*** INITIALIZE VARIABLES
0192      C      IDISDA=0.0
0193      C      MAXVOL=0.0
0194      C      LKFVP=0.0
0195      C      VOLIRR=0.0
0196      C      VOLCHG=0.0
0197      C      IF(NY>1) MSTART=1
0198      C      IF(MUR1.EU.2) GO TO 215
0199      C      WRITE(6,210) **** ANNUAL SUMMARY *****
0200      C      215 CONTINUE
C      C      *** ENTER MONTHLY LOOP ***
C      C      0201      C      00 840 NM=MSTAR1,12
C      C*** ESTABLISH CROP ROTATIONS FOR WHEAT
C      C      IF(HUR1.EO.2) GO TO 235
C      C      DO 230 LI=1,NPLOTS
C      C      IF(INCROP(LI,NE,1)) GO TO 230
C      C      IF(ROTATE(LI,1)) EO.2) GO TO 230
C      C      IF(ROTAYR1.O.2) GO TO 220
C      C      IF(NM.GT.MGSEPT(LI)) LAREA(LI,1)=7
C      C      GO TO 230
C      C      IF(NM.LT.MGSDP(LI)) LAREA(LI,1)=7
C      C      IF(NM.GE.MGSDP(LI)) LAREA(LI,1)=INCROP(LI)
C      C      230 CONTINUE
C      C      GO TO 240
C      C*** CALL SUBROUTINE ROTATE TO ESTABLISH ROTATION SYSTEM FOR MODEL TWO
C      C*** CROP MANAGEMENT
C      C*** 235 CALL ROTATE(NM,PMAT,INDM,KCRUP,AREA,INPLOTS,KROP,IPLAN,MSTART,
C      C      LDRATE,PAV,LRCYCLE,NCRUP,DOUBLE,LYCRP,AREA,IFALT)
C      C*** READ MONTHLY METEORLOGICAL DATA
C      C      240 READ(1,250,END=1520) KAN,SI,IND,YEAR,MONTH,(PREC(I),I=1,11).

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0215      250 IF( MAX(1,2,3,4,5,6,7,8,9)=1,10) GO TO 240
0216      IF( STIND-NEIND$1) GO TO 10
0217      IF( YEAR-GIYEAR-1900) GO TO 990
0218      IF( MUNTH-GIYEND-1900) GO TO 990
0219      IF( MUNTH-GIYEAR-1900) GO TO 240
0220      ACTIR=0.0
0221      DS DAY=0
0222      NDAT2=20
0223      IF( NM>0,2,AND.,IMAX(29).LT.900) NDIM(2)=29
0224      NDAYS=NDIM(NM)

```

C **** ENTER DAILY LOOP ****

00 800 ND=1.NDAYS

```

0225      C*** THE FOLLOWING STATEMENTS CORRECT FOR MISSING DATA ON INPUT TAPE
0226      IF( IMAX(IND)-GI-250.0) MAX(IND)=PDI+100.0
0227      IF( MIN(IND)-GI-250.0) MIN(IND)=PDI+100.0
0228      IF( PREC(IND)-GI-99.97) PREC(IND)=0.0
0229      AVG=15. THE AVERAGE DAILY AIR TEMPERATURE. DEGREE FAHRENHEIT
      LAVG(IND)=1(MAX(IND)+MIN(IND))/2.0-100.0
      SUBROUTINE WINDRD ADJUSTS THE PRECIPITATION RESULTING FROM
      SEEDING CLOUDS
      CALL WRMDUP(PREC(IND),NM,MODEL,WPCNT)
0230      C*** THE FOLLOWING CARD EVALUATES WHETHER THE 24 HOUR DESIGN STORM
      HAS BEEN EXCEEDED
      IF( PREC(IND)>GE-STORM/1.4) WRITE(6,260) NM,NO. YEAR, PREC(IND)
      260 FORMAT(1X,12.7,12.7,12.7)
      C*** CRITICAL EVENT EXCEEDED .

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C *** CALCULATION OF POTENTIAL EVAPOTRANSPIRATION BY MEANS OF
 PENMAN EQUATION ***

```

0233      C*** R=RCKUP
      C*** THE FOLLOWING CARD CHECKS FOR SNOW COVER
      C*** IF(PACK GT 0,1) R=0.70
      C*** THE NEXT TWO CARDS CONVERT TAUG TO ABSOLUTE. DEGREE KELVIN
      CEN1=(TAUG(IND)-32.0)*100.0/180.0
      ABST=CEN1+273.16
      C*** ES IS THE DAILY CALCULATED SATURATED VAPOR PRESSURE. IN MILLIBARS
      ES=13.9*((0.00738*ABST+0.000019*ABST*.8*CEN1+.4))
      1+(0.00136)
      IF(ES<E-0.0) ES=0.0
      C*** ESA IS THE DAILY CALCULATED ACTUAL VAPOR PRESSURE. IN MILLIBARS
      ESA=ES*RH(IND)/100.0
      C*** RN IS THE CALCULATED DAILY NET RADIATION. IN MM OF WATER
      RN=(1-R)*(RAINM)*10.22+0.54*PSUN(NM)-2.010E-05*ABST**1.5
      1+(0.98*(1-BRUNA-BRUNB*SQRT(ESA)))*10.1*0.9*PSUN(NM))
      1+0.0
      C*** WINDD IS THE DAILY AVERAGE WINDRUN. MILES/DAY AT 2 METERS HEIGHT
      WINDD=(WIND(IND)*24)*0.555
      C*** EA IS THE CONVECTIVE LOSSES/MM WATER
      EA=0.26*(E+0.01*WINDD)*(ES-ESA)
      IF(TAUG(IND)) 270.270.280

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0246      270  DELTA=0.0
0247      290  DELTA=0.049*(AVG(IND)*0.071
0248      290  GAMMA=1-DELTA
0249      C*** PEL IS CALLED DAILY POTENTIAL EVAPOTRANSPIRATION, INLIES
0250      C*** PEL=(DELTA*RN)+(GAMMA*EAI)/25.4

0251      C*** CALCULATE LAKE AND BARE SOIL EVAPORATION
0252      C*** RNLAKE=RN*(1.0-0.20)/(1.0-R)
0253      C*** PETIS=(DELTA*LN*NSULL)*(GAMMA*EAI)/25.4
0254      C*** LAKV=(DELTA*LN*NSULL)+(GAMMA*EAI)/25.4
0255      C*** PEL=AVG(IND)
0256      IF(AVG(IND)<1.0)PEL=0.0
0257      IF(AVG(IND)>1.0)PEL=0.0
0258      IF(AVG(IND)<1.0)PEL=0.0
0259      DO 300 MU=1,NPLOTS
0260      IADD(MU)=PEL(MU)-PEL
0261      CCRP=AREA(MO,1)
0262      IF(CCROP(CCROP(NM))<0.0)IAADD(MU)=IAET(MU)-PETBS
0263      IF(IADD(MU)<0.0)IAADD(MU)=0.0
0264      IF(IADD(MU)>0.0)IAADD(MU)=0.0
0265      C*** SUBROUTINE SNOWML CALCULATES THE MOISTURE ADDED TO THE DISPUSAL
0266      C*** SITE DUE TO SNOWMELT ON THE AREA
0267      SNIVAP=0.0
0268      WATER-PRECIP
0269      CALL SNOWML(PRECIP,WATER,PACK,PET,AVG(IND),SNOVAP)

C     C*** EVALUATION OF SOIL MOISTURE AND CALCULATION
C     C*** OF ACTUAL EVAPOTRANSPIRATION ****
C
0270      STRMUL=0.0
0271      RUNDS=0.0
0272      JJ=0
0273      MN=MN+1
0274      IF(MN=MN+1)GO TO 350
0275      STRMUL=0.0
0276      JJ=JJ+1
0277      CROP=AREA(JJ,1)
0278      SOIL=AREA(JJ,2)
0279      DSAREA=AREA(JJ)
0280      RAIN=RAIN+(DISVOL(JJ)/USARTA)
0281      IF(DSAREA<0.0)AND.PRECIP.LT.0.4) GO TO 410
0282      IF(DSAREA>0.0)GO TO 400
0283      IF(RAINLE<0.01)GO TO 400
0284      C*** CALCULATE SURFACE RUNOFF VOLUME BY SCS METHOD
0285      IF(CCROP(CCROP(NM))<0.0)GO TO 370
0286      IF(SNUZ(JJ).LT.(PWPZ(SOIL)*0.5*AVERFCU(SOIL))) GO TO 350
0287      GO TO 360
0288      C*** ADOPT RUNOFF CURVE NUMBER TO CONDITION 1 ANTECEDENT MOISTURE
0289      RCMSUIT(CCROP)=RCN(SOIL,CCROP)*0.39*EXP(0.009*RCN(SOIL,CCROP))
0290      C*** MUDIFY RUNOFF CURVE NUMBER TO CONDITION 1 ANTECEDENT MOISTURE
0291      RCMSUIT(CCROP)=RCN(SOIL,CCROP)*1.95*EXP(-0.00634*RCN(SOIL,CCROP))

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0291      310  GO TO 320
0292      IF (SMUZ(JJ) .LT. 0.6*FCUT(SOIL)) GO TO 320
0293      IF (SMUZ(JJ) .GT. 0.9*FCUT(SOIL)) GO TO 320
0294      READ(SOIL,CROP)=RCNSOIL(CROP)
0295      SI=1000.0/NCM(SOIL,CROP)-10.0
0296      EK=RAIN-0.2*SI
0297      IFLER=I-O.10  GO TO 310
0298      RNOF=ER*27*(RAIN-0.8*SI),
0299      GO TO 420
C*** EVALUATE INTERCEPTION STORAGE
0300      RNOF=0.0
0301      LA=0.0
0302      GO TO 430
0303      LA=0.1
0304      IF (LA .LT. RAIN) LA=RAIN
0305      IF ((LA .LT. LAADD(JJ)).GE.0.1) LA=0.1-LAADD(JJ)
0306
C*** EVALUATE INFILTRATION INTO THE UPPER ZONE
0307      PERC=0.0
0308      QZEVAP=0.0
0309      IF (DARKEO .EQ. 2) GO TO 435
C*** SURROUNDING DARKET EVALUATES THE FLOW WITHIN THE SOIL PROFILE
C*** BY APPLYING THE ONE-DIMENSIONAL Darcy EQUATION
C*** CALL DARKE(PERC,FLUSOIL), SHUZ(JJ,FCGSOIL), SML2(JJ,FCGSOIL)
0310      ISGWZ(JJ,PERC,CONGW(JJ),H2(JJ,FCGSOIL))
2GW(JJ,PWPUZS(JJ),PWPL2(JJ),PWG(SOIL))
GO TO 450
C*** CALLULATE PRESENT STORAGE AVAILABLE IN UPPER ZONE
0311      SHMAXU=0.9*SMUZ(SOIL)-SMUZ(JJ)
C*** EVALUATE WATER CASCADED TO LOWER ZONE FOR STORAGE
0312      CPERC=PERC-SHMAXU
0313      IF (CPERC .LT. SHMAXU) PERC=SHMAXU
0314      IF (PERC .LT. 0.0) PERC=0.0
0315      IF (SHUZ(JJ).GT.FLU(SOIL)) GO TO 440
0316      EXCESS=0.0
0317      GO TO 450
0318      C*** EVALUATE GRAVITATIONAL WATER IN UPPER ZONE
0319      C*** EXCESS=SMUZ(JJ)-PWUZ(SOIL)
C*** IF THE CROP IS DORMANT OR THE SOIL LIES FALLOW, SOIL
C*** EVAPORATION IS EVALUATED
0320      450  IF (CROP(CROP,NM).LE.0.0) GO TO 560
0321      LA=0.0
C*** MODIFY PET BY THE PLANT CONSUMPTIVE USE COEFFICIENT
0322      IF (PET .LE. 1.0) AEI=0.0
0323      IF (PET .LE. 1.0) AEI=0.0
C*** CHECK WHETHER SOIL MOISTURE LIMITS AT FROM THE UPPER ZONE
0324      IF (SMUZ(JJ) .LT. 0.3*AVFCUT(SOIL)) AEI=.60,.490
C*** CALCULATE AEI FROM THE UPPER ZONE WHEN LIMITED BY SOIL MOISTURE
0325      460  AVAILU-SMUZ(JJ)-PWUZ(SOIL)
0326      IF (AVAILU.LE.0.0) AVAILU=0.0
0327      IF (AEI=0.7*AEI*(AVAILU/(0.3*AVFCUT(SOIL))) EVALU=AVAILABLE WATER IN THE LOWER ZONE
0328      IF (AVAILL=SMUZ(JJ)-PWPL2(SOIL)) AEI=.60,.490
C*** CHECK WHETHER SOIL MOISTURE LIMITS AT FROM THE LOWER ZONE
0329      IF (AVAILL.LE.0.0) AVAILL=0.0
0330      IF (SHUZ(JJ) .LT. 0.3*AVFCUT(SOIL)) PWPL2(SOIL)) AEI=.60,.490
  
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MAIN

C * * * CALCULATE AET FROM HUMIDITY & AVAILABILITY (SOIL) BY SOIL MOISTURE

0331 0370 AETLZ=0.3*AET+AVAIL(JJ)-PWP(LZ)(SOIL) }
 0332 GO TO 500
 0333 AETLZ=AET-AETUZ
 0334 GO TO 500

C * * * EVALUATE AET FROM BOTH ZONES UNDER WET CONDITIONS

0335 0390 AETLZ=0.7*AET
 AETLZ=0.3*AET
 AVAIL=SML(JJ)-PWP(LZ)(SOIL)
 IF(SAL((JJ,1E-0.3*(AVAIL(SOIL)+PWP(LZ)(SOIL))) GO TO 470
 500 500 (DARCEO=0.1-0) GO TO 605
 IF(PERC-SMMAZU)=510.520.520

C * * * EVALUATE SOIL MOISTURE

510 SMUZ(JJ)=SMUZ(JJ)+PERC-AE10Z-EXCESS
 SMUZ(JJ)=SMUZ(JJ)-AETLZ+EXCESS
 GO TO 610

520 SMUZ(JJ)=SMUZ(JJ)+SMMAZU-EXCESS-AETUZ
 530 SMMAXL=0.9*FC(LSOIL)-SMUZ(JJ)
 IF(PERCL+EXCESS-SMMAZL)=540.540.550
 540 SMUZ(JJ)=SMUZ(JJ)+PERCL-AETLZ+EXCESS
 GO TO 610
 550 SMUZ(JJ)=SMUZ(JJ)+SMMAZL-AETLZ
 PERC=PERCL+EXCESS-SMMAZL
 GO TO 620

C * * * CALCULATE EVAPORATION FROM BARE SOIL SURFACE (SEVAP) FOR MULCH OCTOBER

C * * * THROUGH MARCH OR WHEN THE DISPOSAL AREA IS FALLOW

560 AETLZ=0.0
 AETLZ=0.0
 IF(PACK(GT,0.01 GO TO 590
 IF(SMUZ(JJ,LT,(FC(LSOIL)-UT(SOIL))) GO TO 570
 EDUZ(JJ)=FC(LSOIL)-SMUZ(JJ)
 IF(SMUZ(JJ,GE,FC(LSOIL)) EOUJJ=0.0
 CALCULATE STAGE 1 SOIL EVAPORATION
 EOUJJ=EOU(JJ)+UZL(VAP
 IF(UZL(VAP,GT,UT(SOIL)) UZEVAP=EOU(JJ)-UT(SOIL)
 UZEVAP=0.0
 GO TO 590

C * * * CALCULATE STAGE 2 SOIL EVAPORATION

570 UZEVAP=C(SOIL)*(EOUJJ*0.51-C(SOIL)*(UZL(VAP,GT,UT(SOIL))-AE10Z-AETLZ))
 580 IF(UZEVAP,LT,0.0) JZEVAP=0.0
 IF(SMUZ(JJ)-PWP(LZ)(SOIL),LT,UZEVAP) UZEVAP=SMUZ(JJ)-PWP(LZ)(SOIL)
 GO TO 600

590 UZEVAP=0.0
 600 IF(DARCEO,FO,1) PERC=0.0
 IF(DARCEO,FO,1) EXCESS=0.0
 SHUZ(JJ)=SMUZ(JJ)-UZEVAP+PERC-EXCESS
 IF(SMUZ(JJ,AE,PWP(LZ)(SOIL)) SMUZ(JJ)=PWP(LZ)(SOIL)
 IF(DARCEO,FO,2) GO TO 530

605 SMUZ(JJ)=SMUZ(JJ)-AE10Z
 610 IF(SMUZ(JJ,-1,-PWP(LZ)(SOIL)) AETLZ=AETLZ-(PWP(LZ)(SOIL)-SMUZ(JJ))
 IF(SMUZ(JJ,-1,-PWP(LZ)(SOIL)) SMUZ(JJ)=PWP(LZ)(SOIL)
 IF(DARCEO,FO,3) GO TO 620
 IF(DARCEO,FO,3) DPERC=SMUZ(JJ)-0.9*FC(LSOIL)

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0381 IF (OPERC(JJ)=0.0) OPERC(SOIL) SMUZ(JJ)=0.9+FC(SOIL)
0382 AFIUZ=AFIUZ+ZE*VAP
0383 SM IS THE SOIL MOISTURE IN THE GROWING ZONE, IN INCHES
C*** SMUZ=SMUZ(JJ)+SMUZ(JJ)
0384 IAE(JJ)=IA+IA*DD(JJJ)
0385 IAEW(JJ)=IA*DD(JJJ)
0386 AET(JJ)=AI*DD(JJJ)
0387 AETL(JJ)=AI*DD(JJJ)
0388 NPERC(JJ)=OPERC
0389 NI(L,J)=IA
0390 NMOF(JJ)=RHOE
0391 IF (PLAN(JJ)*LE>2) STRNUF = RNDF
0392 STRVUL = STRVUL + STRNUF*ARCA(JJJ)
0393 GO TO 330
0394 CONTINUE
C*** EVALUATION OF VOLUME USED AS IRRIGATION ***
C*** THIS IS THE PREVIOUS DAY'S AVERAGE TEMPERATURE IN FAHRENHEIT
C*** PRIOR TO TODAY
C*** VOLDIS=0.0
0395 JDISDA=0
0396 NCNT=0
0397 DO 675 MS=1,NPLUIS
0398 DISVOL(MS)=0.0
0399 IF (BYPASS*NE=1) GO 10 655
0400 MCROP=LARLA(MS)
0401 IF (KCRP=MCRP) NM=0.0
0402 GO TO 655
0403 CONINUE
0404 IF (PLAN(MS)=EQ(1)) GO 10 660
0405 THAWED=TAVG(IND)+1+12
0406 FREEZE=TAVG(IND)+11
0407 12=1
0408 1=TAVG(IND)
0409 1=FREEZE(LI+64,0) FREEZE=1
0410 IF (THAWED.GT.1.14,0) FROZEN=0
C*** WHEN FROZEN EQUALS 1 THE SOIL IS CONSIDERED TO BE FROZEN IT IS THAWED
0411 DISVOL(FROZEN)=0
0412 IF (FROZEN.EQ.1) GO 10 660
C*** SHOT IS THE SOIL MOISTURE IN THE TOP 12 INCHES OVER EACH
C*** PLOT; AVOLC IS THE AVAILABLE WATER CAPACITY OF THAT SOIL.
C*** IRRIGATION WILL NOT OCCUR ON DAYS THAT THE SOIL MOISTURE IS AT
C*** A LEVEL GREATER THAN THAT OF THE PERCENTAGE OF AVAILABLE WATER
C*** SPECIFIED BY THE VARIABLE PAVL.
0413 SOIL=LARLA(MS)
0414 IF (SMUZ(MS)>2) (PAVLV*AVFC(SOIL))+PVWUL(SOIL) GO 10 660
JDISDA=JDISDA+1
NCNT=NCNT+1
0415 IF (PVNOL.LT.PCMAX*VOLMAX) GO 10 660
0416 DISVOL(MS)=DSRAVE*AREA(MS)
0417 C*** IF THE POND VOLUME IS LESS THAN THE VOLUME REQUIRED FOR ONE FULL
C*** DAY OF IRRIGATION, IT WILL BE ASSUMED THAT NO IRRIGATION WILL OCCUR
ON THAT DAY.
0418 PVNOL=PVNOL-DISVOL(MS)
0419 IF (PVNOL.GT.0.0) GO 10 670
0420 DISVOL(MS)=DISVOL(MS)+PVNOL

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PUNVOL=0.0
GO TO 670
660 OISVOL(MSI)=0.0
670 SMALLT(1:M,3:MSI)=SMACC((1:M,3:MSI)+OISVOL(MSI)/AREA(MSI)
670 VOLDS=VOLDS+OISVOL(MSI)
670 IF(OISVOL(MSI)>0.0) DAYSDS(MSI)=DAYSDS(MSI)+1.0
675 CONTINUE
675 IF(DAYSDS(MSI)>0) DISDA=DISDA+JDISDA/NCN
675 UPDATE DISPOSAL DAY ACCOUNT
675 IF(VOLDS.GT.0.0) USDAY=USDAY+1
675 IF(OVPASS.NE.1) GO TO 680
675 RUNOFF=0.0
675 GO TO 730
C*** SURFACE STORAGE CALCULATIONS ADDITIONAL LOADING TO THE SURFACE
C*** POND DUE TO FEEDLOT RUNOFF FROM MUNICIPALITY DISPOSAL
C*** WHO CALL SURAG(P1,P2,P3,PRCLP,SNOW,FRZL,MCH,MGRW,MRUNOFF,MUNO
113MM,MRUNDS)
C*** C*** CALCULATION OF SURFACE AREA AND DETERMINATION OF SURFALL
C*** EVAPORATION FROM STORAGE FACILITY ***#
C*** THE FOLLOWING CALCULATIONS DETERMINE THE SURFACE AREA OF THE STORAGE
C*** STORAGE FACILITY IN CUBIC FEET.
C*** IF(PONVOL.LT.0.0) GO TO 750
C*** V=PONVOL*3600
C*** THE FOLLOWING CALCULATIONS DETERMINE THE SURFACE AREA OF THE STORAGE
C*** FACILITY AS A FUNCTION OF STORAGE VOLUME AREA IS IN SQUARE FEET
C*** VOLUME IS IN CUBIC FEET. THE STORAGE FACILITY IS SHAPED LIKE AN INVERTED
C*** FRUSTUM OF A PYRAMID. INPUT PARAMETERS TO SIZE THE FACILITY ARE LENGTH
C*** (L) OF THE BASE IN FEET. WIDTH OF THE BASELW IN FEET AND SLOPE OF
C*** THE POND DUE TO LEAKS. INPUTS TO THE STORAGE WILL BE NATURAL
C*** INSIDE EMBANKMENTS GIVEN AS A RATIO OF RUNOFF TO RIS(S). IT IS ASSUMED
C*** RUNOFF FEEDLOT RUNOFF MUNICIPALITY DISPOSAL AND PRECIPITATION.
C*** LOSSES FROM THE POND INCLUDE EVAPORATION AND DISPOSAL VOLUME.
C*** 0.2 IS THE AREA OF THE SURFACE LIQUID IN SQUARE FEET.
C*** HAPRX=(PONVOL/VOLMAX)*HMAX
C*** VC=A1*A2*HAPRX+A3*HAPRX**2
C*** DVOD=A1+A2*HAPRX+A3*HAPRX**3
C*** H=HAPRX+DV/DVOD
C*** IF(LAUSIH-HAPRX).LT.-0.1 GO TO 750
C*** HAPRX=H1
C*** GO TO 740
750 IF (LAUJ-EVAP)>0 H=HMAX
750 02=1.42+.5*(1+(L+2**S**H))
750 IF(LAUJ-EVAP)<0 LAKEVP=LAKEVP
750 LAKEVP=LKEVP+LAKEVP
750 SEVAP=B2*(LAKEVP/12)
750 SEVAP IS THE VOLUME OF WATER EXTRACTED FROM THE STORAGE FACILITY BY
750 FREE SURFACE EVAPORATION.
750 IF(LSEVAP>.56016*PVOL) SEVAP=PVOL
750 PVOL=PVOL-1.5*EVAP/.36301
750 IF(PONVOL.LE.0.0) PVONVOL=0.0
C*** THE VOLUMES OF CALCULATED RUNOFF FEEDLOT RUNOFF MUNICIPALITY
C*** DISPOSAL AND PRECIPITATION FALLING ON THE FACILITY ARE ADDED
C*** TO THE VOLUME OF WATER IN THE STORAGE FACILITY (ACRE-IN).

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IF(PREC(IND).GT.FRECU(1))CTP(11)=CTP(11)+1.0
CNTR=0.0
DO 790 KI=1,NPLOTS
IF(NKNOF(KI).GT.0.0)AND(EQ(1,1))CTDAY(KI)=CTDAY(KI)+1.0
IF(NKNUF(KI).GT.0.0)AND(EQ(1,1))CNR(KI)=CNR(KI)+1.0
IF(NKNUF(KI).GT.0.0)AND(EQ(1,1))CIR(KI)=CIR(KI)+1.0
IF(PREC(IND).GT.FRECU(1))AND.CNTR.EQ.1.0)CTP(11)=CTP(11)+1.0
NPLOTS=NPLOT
CONTINUE
C
C *** EXIT DAILY LOOP ***
C
C*** UPDATE ACCOUNTS
POACC(1,NM,1)=AMOUNT(NM)
POACC(1,NM,2)=SMACC(1,NM,2,1)*PSAREA
POACC(1,NM,6)=DSDAY
POACC(1,NM,7)=ACTIRR
DO 810 JI=2,10
DO 810 JI=2,10
DO 810 JI=2,10
DO 810 JI=2,10
DO 820 SHACCT(13,J,MP)=SMALL(13,J,MP)+SHACCT(13,J,MP)
SHACCT(13,J,MP)=AMOUNT(NM)
SHACCT(13,J,MP)=AMOUNT(NM)
SHACCT(13,J,MP)=AMOUNT(NM)
SHACCT(13,J,MP)=AMOUNT(NM)
YULIRK=YULIRK+ACTIRR
CONTINUE
C
C *** EXIT MONTHLY LOOP ***
C
C USNOW=PACK-PACKPV
PACKPV=PACK
PLWN=(POACC(1,1,2)+POACC(1,3,2)+POACC(1,13,2)+POACC(1,13,4)+POACC(1,13,5))/100.
WASTWH=WASTWH+PLWN
POACC(1,1,1)=POACC(1,12,1)
DO 840 KI=1,NPLOTS
DSNFF(KI)=DSNFF(KI)+SMACL(13,5,KI)
AINTER(KI)=AINTER(KI)+SMACCT(13,4,KI)
AAEIKS(KI)=AAEIKS(KI)+SMACC(13,7,KI)
ACHSOKI=ACHSOKI+SMOKI(13,6,KI)
DSPERC(KI)=DSPERC(KI)+SMACCT(13,6,KI)
IRISUA=IRRSMU+VOLR
PREC=PREC+SMACCT(13,2,1)
IF(VLAR>1900)-EJ.VSTAK(DRY=SMACCT(13,2,1)
IF(SMACCT(13,2,1).GE.WET)WET=SMACCT(13,2,1)
IF(SMACCT(13,2,1).LE.DRY)DRY=SMACCT(13,2,1)
C*** PRINT POND ACCOUNT
WRIT(6,1601)YEAR
BUD FORMATT(0,27X,-19,12/9X,
INCHES)-----/20X,*INFLUX*,40X,OUTFLUX*-----/X,
2-----/X,MONTH,4X,PRECLP,X,MUNICIPAL,HEELOUT
3-----/X,RUNOFF,X,
4-----/X

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6IRR. DAYS *4X* DISPOSAL VOL. SURFACE EVAP. DISCHARGE *4X* 'VOL.
7 CHANGE IN ETGHT
WRITE(6,870) 1, (PAACC(I,K),I=1,11),K=1,13)
070 FORMAT(4X,A4,F10.1,F12.1,2,I0,I,F16.0,F17.1,F13.1,F15.1,F10.
12)

C*** PRINT SOIL MOISTURE ACCUMULS
0549 DO 910 JM=1,NPLOTS
0550 IF(MORU1-E,0.1) CROP=1,AREA(JM,1)
0551 IF(MORU1-E,0.2) CROP=1,YRCRP(JM)
0552 SOIL=AREA(JM,2)
0553 WRITE(6,880) JM,KICP(CROP),SOIL,AREA(JM)
0554 800 FORMAT(17,1,10X,PLOT NO.,13,/,1,25X,CROP--*,2AB,5X,SUITL TYPE--,
1- 1,13,5X,DISPOSAL AREA--,F6.2*,ACRES)
0555 1,IF(MORU1-E,0.2),AND,DOUBLE(JM),FO,21,WRITE(6,580)
0556 5600 FORMAT(1,30X,DOUBLE CROPPING WITH WHEAT)
C

C WRITE(6,890) YEAR
890 FORMAT(4,10,35X,WATER BALANCE (INCHES) IN THE DISPOSAL AREA - 19*,
1,2/10X,1-1,3X,2-1,3X,3-1,3X,4-1,3X,5-1,3X,6-1,3X,7-1,3X,8-1,3X,9-1,3X,10-1,3X,11-1,3X,12-1,3X,
2-1,3X,3-1,3X,4-1,3X,5-1,3X,6-1,3X,7-1,3X,8-1,3X,9-1,3X,10-1,3X,11-1,3X,12-1,3X,
3 * INPUT * 3BX, * OUTPUT S* /2IX,* 1-1,3X,2-1,3X,3-1,3X,4-1,3X,5-1,3X,6-1,3X,7-1,3X,8-1,3X,9-1,3X,10-1,3X,11-1,3X,12-1,3X,
4-1,3X,5-1,3X,6-1,3X,7-1,3X,8-1,3X,9-1,3X,10-1,3X,11-1,3X,12-1,3X,
57X,* PRELIMINARY *4X* IRRIGATION *3X* INTERCEPTION *2X* SURFACE R
6UNOFF *3X* PERCOLATION *8X* AET *9X* CHANGE IN SA *1
WRITE(6,900) 1,(SMACC(I,K),JM),K=1,13),I=1,13)
900 FORMAT(10X,A4,7F1.2)
910 CONTINUE
910 WRITE(6,920) PCHW
920 FORMAT(10X,10X,PERCENT OF WASTEWATER CONTROLLED= *F10.2)
921 WRITE(6,930) IDISUA
930 FORMAT(10X,10X,POTENTIAL DISPOSAL DAYS= *14)
931 WRITE(6,940) PACK.DSNOW
940 FORMAT(10X,10X,'PACK ON DECEMBER 31 = *FS.2 *15X.
1-1,CHANGE IN SNOW STORAGE= *F5.2)
941 WRITE(6,950)
950 FORMAT(10X,10X,INPUTS-OUTPUTS-CHANGE IN SNOW STORAGE=CHANGE IN
1-SOIL MOISTURE)
951 MAXVOL=MAXVOL+100.0/VOLMAX
952 WRITE(6,960) MAXVOL
953 FORMAT(10X,10X,PERCENT OF MAXIMUM POND VOLUME REQUIRED = *F7.2)
954 EVAPLK=EVAPLK+LKEVP
955 WRITE(6,970) LKEVP
956 FORMAT(10X,10X,ESTIMATED LAKE EVAPORATION, INCHES = *F6.2)
957 DO 7000 KK=1,NPLOTS
958 IF(IPLAN(KK)=FO,1,OR,USRATE(FO,0,1) GO TO 7000
959 RRLJAN(KK)=RR(JAN,KK),SHACC(1,1,3,KK)
960 RRJFEB(KK)=RR(FEB,KK)+SHACC(1,2,3,KK)
961 RRIMAR(KK)=RR(MAR,KK)+SHACC(1,3,3,KK)
962 RRJAP(KK)=RR(APR,KK)+SHACC(1,4,3,KK)
963 RRJMY(KK)=RR(MAY,KK)+SHACC(1,5,3,KK)
964 RRLJUN(KK)=RR(JUN,KK)+SHACC(1,6,3,KK)
965 RRJUL(KK)=RR(JUL,KK)+SHACC(1,7,3,KK)
966 RRJAUG(KK)=RR(AUG,KK)+SHACC(1,8,3,KK)
967 RRSEPT(KK)=RR(SEP,KK)+SHACC(1,9,3,KK)
968 RRLOC(KK)=RR(LOC,KK)+SHACC(1,10,3,KK)
969 RRINOV(KK)=RR(INOV,KK)+SHACC(1,11,3,KK)

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9000 RRDDEC(KK)=RRDDEC(KK)+SMACC(112+3+KK)
980 CINI(INUE)          2212541

C   **** EXIT YEARLY LOOP ****
C
C   0579 990 CONTINUE
0580 1520 CONTINUE
C*** CALCULATE AVERAGE ANNUAL VALUES
C      CNNEW=CM
C      IF(CM>=EU.O) MM=1
C      COUNT=LH/NH
C      IF(COUNT>0.O) MM=0
C      IF(CM-EU.O>0.O) CM=YEARS
C      DSCRG=DSCVOL/CM
C      CM=CNNEW
C      COUNT=LW/NH
C      IRRVOL=IRRSUM/YEARS
C      APREC=TPREC/YEARS
C      RANGE=HE-OK
C      AVGMD=LVAP-APREC
DO 1000 J=1,NPLOTS
  DO 1000 J=1,NPLOTS
    DSPEC(J)=USPERC
    DSRNFF(J)=DSRNFF(J)/YEARS
    ACHSUM(J)=ACHSUM(J)/YEARS
    AINTER(J)=AINTER(J)/YEARS
    AAETRS(J)=AAETRS(J)/YEARS
    DAYSDS(J)=DAYSDS(J)/YEARS
    INPLUTS(J)=INPLUTS(J)/NPLOTS
    DU 1020 J=1,25
    IF(CLIPDAY>0.O) CIP(J)=CIP(J)/CLIPDAY+100.0
    PRECAL(J,1)=ASAI(J)
    PRECAL(J,2)=CIP(J)
    PRECAL(J,3)=CIP(J)
    PRECAL(J,4)=CIP(J)
    PRECAL(J,5)=CIP(J)
    DU 1010 J=1,NPLOTS
    RUNALL(J,1)=NUM1(J)
    RUNALL(J,2)=G1(J)
    RUNALL(J,3)=CIR(J,1)
    RUNALL(J,4)=CIR(J,2)
    RUNALL(J,5)=CIR(J,3)
    RUNALL(J,6)=CIR(J,4)
    RUNALL(J,7)=CIR(J,5)
    RUNALL(J,8)=CIR(J,6)
    RUNALL(J,9)=CIR(J,7)
    RUNALL(J,10)=CIR(J,8)
    RUNALL(J,11)=CIR(J,9)
    RUNALL(J,12)=CIR(J,10)
    INUM=1
    1010 RUNACC(J,1)=INUM=CIR(J,1)
    1020 RUNACC(J,2)=INUM=CIR(J,2)
    NPLOTS=NPLOT
C*** PRINT INPUT PARAMETERS
  0618  WRITE(6,B5) NAME,OFL,NAME,STATE,START,YEND,WETH,MUDIF,MUD,EL
  0619  LINELDM,TU,STURGE,POND,LAREA,STORM,LW,S,HMAX,VOLMAX,PSAREA
  0620  LEMRKT,EU,2,GU TO 1085
  0621  DO 1080 J=1,NPLOTS
  0622  CROP=INCRUP(J)
  0623  PLACE=AREA(J)
  0624  SOIL=LAREA(J,2)
  0625  REAVLU=PAVLU
  0626  WRITE(6,1030) PLATEA,KRUP(CROP),SOIL,OSRATE,PAVLU
  0627  FORMAT(7/15X,PLATEA,11/25X,7/15X,PLATEA-1,F6.2*,13;2*ACRES//25X;/
  1(CB) CROP--,2AU/25X,*(C) Soil TYPE--)

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2/25X. (1) IRRIGATION RATE-- 15.2" INCHES/CAY
 3GATION MANAGEMENT-- 1/25X. (1) FIELD CAPACITY
 1FLIP(LAN(J);EO-1) WRI1E(6.1040)
 1FLIP(LAN(J);EO-2) WRI1E(6.1050)
 1FLIP(LAN(J);EO-3) WRI1E(6.1060)
 KUNOFF F
 RUNOFF AND IRIGATION)
 1040 FORMAT(1/25X, '(1) PLAN IMPLEMENTED--
 1050 FORMAT(1/25X, '(1) PLAN IMPLEMENTED--
 1060 FORMAT(1/25X, '(1) PLAN IMPLEMENTED--
 1FLKUATE(J);EO-1) WR1E(6.1070)
 1070 FORMAT(1/25X, '(1) CROP ROTATION WITH -- FALICK*)
 PAVLU=PAVLU
 1080 COUNTRUE
 00530 J=1 NPLOUS
 PLARE=AREA(J)
 SOIL=AREA(J,2)
 RPAVLU=PAVLU
 1FLIP(LAN(J);EO-1) PAVLU=0.0
 NR=RCYCLE(J)
 WRITE(6,260) J,PLARE A
 WRITE(6,15X) ,PLD1 * 11/25X, *(A) AREA-- * 11/6.2,* ACRES*)
 5260 FORMAT(1/25X, '(1) WR1E(6.5261) KROP(NRCROP(J,1))
 1F(NR-EU-1) WR1E(6.5262) KROP(NRCROP(J,2))
 1F(NR-EU-2) WR1E(6.5263) KROP(NRCROP(J,3))
 1F(NR-EU-3) WR1E(6.5264) KROP(NRCROP(J,4))
 1F(NR-EU-4) WR1E(6.5265) KROP(NRCROP(J,5))
 1F(NR-EU-5) WR1E(6.5266) KROP(NRCROP(J,6))
 1F(NR-EU-6) WR1E(6.5267) KROP(NRCROP(J,7)),K=1.7)
 5261 FORMA1(1/25X, '(1) CROP-- * 2AB
 5262 FORMA1(1/25X, '(1) CROP-- * 4AB
 5263 FORMA1(1/25X, '(1) CROP-- * 6AB
 5264 FORMA1(1/25X, '(1) CROP-- * 8AB
 5265 FORMA1(1/25X, '(1) CROP-- * 10AB
 5266 FORMA1(1/25X, '(1) CROP-- * 12AB
 5267 FORMA1(1/25X, '(1) CROP-- * 14AB
 1WR1E(6.5268) SOIL_TYPE--PAVLU
 5268 FORMA1(1/25X, '(1) SOIL_TYPE-- * 13* INCHES/CAY 1/25X, *(1) CROP ROTATION MANA
 1IRRIGATION RATE-- * 5.2* INCHES/CAY 1/25X, *(1) CROP ROTATION MANA
 2GATION-- IRRIGATION RATE-- * 5.2* INCHES/CAY 1/25X, *(1) CROP ROTATION MANA
 1FLIP(LAN(J);EO-1) WRI1E(6.5270)
 1FLIP(LAN(J);EO-2) WRI1E(6.5280)
 1FLIP(LAN(J);EO-3) WRI1E(6.5290)
 5270 FORMAT(1/25X, '(1) PLAN IMPLEMENTED--
 5280 FORMAT(1/25X, '(1) PLAN IMPLEMENTED--
 1F(RCYCLE(J);EO-1) WR1E(6.5300)
 5290 FORMAT(1/25X, '(1) CROP MANAGEMENT--
 5291 FORMAT(1/25X, '(1) CROP MANAGEMENT--
 5310 FORMAT(1/25X, '(1) CROP MANAGEMENT--
 1YEAR REPE1T1GN
 1F(DOUBLE(J);EO-1) WR1E(6.5325)
 1F(DOUBLE(J);EO-2) WR1E(6.5320)
 5320 FORMAT(1/25X, '(1) DOUBLE CROPPING MANAGEMENT WITH WINTER WHEAT BEIN
 1EEN CROPS MENTIONED IN PART (1)
 5325 FORMAT(1/25X, '(1) SINGLE CROPPING MANAGEMENT)
 PAVLU=PAVLU
 5330 COUNTRUE

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0680 1095 CONINUE

C*** PRINT FINAL SUMMARY

1090 FORMATTED FINAL SUMMARY * * * * *

WRITE(6,1090)

1100 FORMATTED * * * * * METEOROLOGICAL SUMMARY * * *

WRITE(6,1100)

1110 FORMATTED AVERAGE ANNUAL LAKE EVAPORATION= .F6.2. * INCHES *)

WRITE(6,1110) EVAP

1111 FORMATTED * * * * * AVERAGE ANNUAL PRECIPITATION= * ,F6.2. * INCHES *)

WRITE(6,1111) APREL

1120 FORMATTED * * * * * AVERAGE ANNUAL PRECIPITATION= * ,F6.2. * INCHES *)

WRITE(6,1120) APRIL

1130 FORMATTED * * * * * RANGE OF PRECIPITATION RANGE= * ,F6.2. * INCHES *)

WRITE(6,1130) WET

1131 FORMATTED * * * * * RANGE OF PRECIPITATION RANGE= * ,F6.2. * INCHES *)

WRITE(6,1131) HIGH OF F6.2. INCHES)

1140 FORMATTED * * * * * AVERAGE ANNUAL MOISTURE DEFICIT= .F6.2. * INCHES *)

WRITE(6,1140) AVGMD

1150 FORMATTED * * * * * AVERAGE ANNUAL MOISTURE DEFICIT= .F6.2. * INCHES *)

WRITE(6,1150) 150

1160 FORMATTED * * * * * SUMMARY OF POND OPERATIONS *)

WRITE(6,1160) MM

1161 FORMATTED * * * * * NO. OF YEARS HAVING A DISCHARGE= * ,I6.1

WRITE(6,1161) COUN

1170 FORMATTED * * * * * AVERAGE NO. OF DISCHARGES / YEAR HAVING A DISCHARG

1E+0,F6.2)

1180 FORMATTED * * * * * DISCHRG TOTAL DISCHARGE= .F6.2. * ACRE-INCHES *)

WRITE(6,1180) CML

1190 FORMATTED * * * * * TOTAL NO. OF DISCHARGES= * ,F4.0

WRITE(6,1190) CNTRL

1191 FORMATTED * * * * * AVERAGE PERCENT OF DISCHARGE CONTROLLED BY EVAPURA

ITION AND IRRIGATION= .F6.2)

1200 FORMATTED * * * * * DS VOL TOTAL DISCHARGE VOLUME= .F9.2. * ACRE-INCHES *)

WRITE(6,1200) CM

1210 FORMATTED * * * * * TOTAL NO. OF DISCHARGES= * ,F4.0

WRITE(6,1210) PTAK

1220 FORMATTED * * * * * MAXIMUM DISCHARGE= .F6.2. * ACRE-INCHES *)

WRITE(6,1220) KVAL

1230 FORMATTED * * * * * AVERAGE ANNUAL VOLUME OF IRRIGATED WATER TO THE FI

ELD= F6.2. * ACRE-INCHES *)

1240 FORMATTED * * * * * SUMMARY OF DISPOSAL PLOTS *)

NO.1220,J=1,NPLOTS

1250 FORMATTED * * * * * PLOT * ,I11

WRITE(6,1250) J

1260 FORMATTED * * * * * AREA RUNOFF= .F6.2. * INCH

1S.1

1270 FORMATTED * * * * * DISPERG * ,I11

WRITE(6,1270) J

1280 FORMATTED * * * * * DAYS(J) * ,I11

WRITE(6,1280) DAYS(J)

1290 FORMATTED * * * * * AVERAGE ANNUAL NO. OF DISPOSAL DAYS= .F6.1)

WRITE(6,1290) AINTERJ

1300 FORMATTED * * * * * AVERAGE ANNUAL DISPOSAL AREA INTERCEPTION= .F6.2. *

WRITE(6,1300) AACINTERJ

1310 FORMATTED * * * * * AVERAGE ANNUAL DISPOSAL AREA CHANGE IN SOIL MOISTU

RE

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PCD

FORTRAN IV LEVEL 21

*** SUBROUTINE CROPG0 CALCULATES THE CROP COEFFICIENTS FOR USE IN THE MAIN PROGRAM. THE CROP COEFFICIENTS ARE CALCULATED BY THE PROCEDURES OUTLINED IN THE TECHNICAL RELEASE NO. 21, IRRIGATION WATER REQUIREMENTS, UNITED STATES DEPARTMENT OF AGRICULTURE, SOIL CONSERVATION SERVICE, ENGINEERING DIVISION.

*** SLIGHT MODIFICATIONS HAVE BEEN MADE FOR ALIGNMENT IN THE MODEL. EQUATIONS FOR THE CROP GROWTH STAGE COEFFICIENTS WERE DEVELOPED WHICH ELIMINATES THE NECESSITY OF READING THE VALUES FROM THE CURVES. INPUTS TO THE SUBROUTINE INCLUDE THE CROP MONTH AND DAY GROWING BEGINS AND ENDS, NUMBER OF DAYS IN EACH MONTH, AND THE MEAN MONTHLY AVERAGE TEMPERATURES IN FAHRENHEIT DEGREES.

```

0002      INTEGER LCRP, UGSD, DGSE
0003      INTEGER ROLM(12), SHIFT
0004      REAL HLO(12), UHMO(12), ACC(12)
0005      REAL HMA(12), K1(12), PCGST(12),
0006          RCROF(7,12), PCGS(11,12)
0007      DO 65 H=1,12

```

C*** CONTINUE
 65 GDSB= MONTH GROWING SEASON BEGINS EXPRESSED NUMERICALLY IE 1-12
 C*** DGSU= DAY GROWING SEASON BEGINS EXPRESSED NUMERICALLY
 C*** DGSE= MONTH GROWING SEASON ENDS EXPRESSED NUMERICALLY IE 1-12
 C*** DGSF= DAY GROWING SEASON ENDS EXPRESSED NUMERICALLY
 C*** DMD= MEDIAN DAYS OF THE MONTHS IN THE GROWING SEASON
 C*** DMD= DAYS BETWEEN MID DATES
 C*** ACC= ACCUMULATIVE DAYS IN GROWING SEASON
 C*** PGS= PERCENT OF GROWING SEASON REACHED AT MID DATES
 C*** MMT= MEAN MONTHLY AVERAGE TEMPERATURES
 C*** MGSDI= TEMPORARY STORAGE FOR MGSB
 C*** HSGS1= TEMPORARY STORAGE FOR MGSE
 C*** PCGS1= TEMPORARY STORAGE FOR PGGS

0012
0013
0014
0015

*** CANNED USE-*** THIS QUOTINE WILL NOT EXPIRE IF THE GROWING SEASON EXCEEDS ONE YEAR.


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FORTRAN IV G LEVEL 21           CROPC0          DATE = 00036      PAGE CCC4
0114
0117   B=0.
0118   C=0.
0119   D=0.
0120   E=0.
0120 DO 220 J=1,12
0120   Z=PCGS(J)-XBAR
0121   KCROP(KCROP,J)=(A+B*Z*C*I*2*D*Z+E*J+F*4)*KI(J)
0122   IF (PCGS(J).LE.0.0) KCROP(KCROP,J)=0.0
0123
0124 220 CONTINUE
0125 CONINUE
0125
0126 C*** SINCE THE MAIN PROGRAM APPLIES THE CROP COEFFICIENT (KCROP) TO
0126 THE ENTIRE MONTH, THE KCROP WAS PROPORTIONED ACCORDINGLY TO
0126 COMPENSATE FOR THIS. THE NEXT TWO CARDS EDU THIS
0126 KCROP(KCROP,MGSB)=KCROP(KCROP,MGSB)*(NDIM(MGSB)-DGSB+1)/NDIM(MGSB)
0126 KCROP(KCROP,MGSE)=KCROP(KCROP,MGSE)*(NDIM(MGSE)-DGSB+1)/NDIM(MGSE)
0127 RETURN
0128
0129 END

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0001      SUBROUTINE ROTATN (NY,NM,MMA),KCROP,TAKLA,NPLTS,KROP,IPLAN.
0002      IMSTART,DSRATE,PAVL,U,RCYCLE,NCROP,DOUBLE,TVRCP,AREA,IFALWI,
0003      INTEGR,DSBW,DUSE,DSBW,DS,EW,SOIL
0004      INTEGR,RCYCLE(9),DOUBLE(9),AREA(9),CROP,DSBP(9,9),DS(9,9)
0005      REAL,MMA(12),KCROP(12),AREA(9)
0006      MGSE(9,9),MGSE(9,12),MGSE(9,21),AREA(9,21),TVRCP(9,9)
0007      DIMENSION INTR(9,50),INT(9,50),IMPL(9,50),IFALWI(9
1).IPLAN(9)
2).KCROP(16)
3).SUBROUTINE ROTATN IS USED TO DETERMINE CROP PLANNING MANAGEMENT
4).ONE: FOR SINGLE-CROPPING. A SAME SORT OF CROP MAY BE ASSIGNED TO
5).A SPECIFIC FARM PLOT CONTINUOUSLY THROUGH SIMULATION PERIOD.
6).OR A CERTAIN SET OF DIFFERENT CROPS WITH A SPECIFIC FIELD ROTATING
7).CYCLE UP TO SEVEN-YEAR TERM OR MORE CAN BE MANAGED ON A PLOT.
8).TWO: FOR DOUBLE-CROPPING, THREE CROPS IN TWO YEARS CAN BE GROWN
9).ON A PLOT COMBINING WITH WINTER WHEAT; EXHEAT-CORN-FALWI-
10).SUGARBEAN-FALLOW-SUGARBEAN-WHEAT-SORGHUM ETC.
11).PARTICULARLY IT IS POSSIBLE TO GROW ONE CROP FOR EACH YEAR FOR
12).THE FIRST THREE YEARS AND THEN THE OTHER CROP FOR THE NEXT TWO YEARS.
13).NRCROP= CROP NAME FOR DATA INPUTS
14).FYRCRP= CROP NAME FOR CROP DEFINED YEARLY
15).IAREA1=1= CROP NAME DEFINED MONTHLY FOR SUBROUTINE ROTATN
16).DSBW= DAY GROWING SEASON BEGINS FOR WHEAT
17).DSEW= DAY GROWING SEASON ENDS FOR WHEAT
18).RCYCLE= REQUIRED YEARS OF ROTATING CROPS ON A PLOT
19).DOUBLE= DOUBLE CROPPING WITH WHEAT AND SOME CROP,RESERVING FALLOW
20).TERM
21).IWLT= TEMPORARY STORAGE FOR WHEAT OR FALLOW FOR DOUBLE CROPPING
22).IFALWI= IN THE FIRST YEAR OF SIMULATION. BEGIN WITH WHEAT?
23).IF (NM.GT.1) .AND. (NY.GT.1) GO TO 110
24).CAUTION: IN ADDITION TO CROP TYPES, DOUBLE CROPPING OR NOT
25).AND. ROTATION CYCLE, USERS MUST INPUT SOIL TYPE, IRRIGATION
26).MANAGEMENT AND AREA OF EACH PLOT
27).READ(5,101) (KCYCLET),DOUBLE(I),AREAI,I,AREA
28).111,1,NPLTS
29).10 FORMAT(1X,5,12,6,1)
30).C*** READ TYPES OF CROP,PLANTING, AND HARVESTING DATE
0009      00 40 J=NPLTS
31).      MM4=RCLC(J)
32).      DU,JO,K=1,MMA
33).      READ(PLAN,1,OK,MG,STARII) GO TO 90
34).      READ(5,20) NKROP(J,K),MGSUB(J,K),DSBP(J,K),DS(9,J,K)
35).      20 FORMAT(1X,11,4,12)
36).      30 CONTINUE
37).      40 CONTINUE
38).      C*** CALCULATE CROP COEFFICIENTS
39).      IF(NY.GT.1,OK,MG,STARII) GO TO 90
40).      DO BO K=1,NPLTS
41).      M0A=RCLC(K)
42).      DO 70 J=1,MM
43).      HGSB=MGSEP(K,J)
44).      DGSB=DGSBP(K,J)
45).      MGSE=MGSEP(K,J)

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PAGE 00C2

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FORTRAN IV G LEVEL 21 ROTAIN

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0025      DGSE=DGSEP(K,J)
          CROP=NRCROP(K,J)
          CALL CROP.COTCRUP,MGSB,MGSE,MGSE,MU1W,MU1H
0026      70 CONTINUE
0027      80 CONTINUE
0028      90 CONTINUE
0029      C*** CROP COEFFICIENT FOR WHEAT OF DOUBLE CROPPING
0030      READ PLANTINGS AND HARVESTING DATES FOR WHEAT SHOULD BE READ
          ACCORDING TO THE PLAN OF DOUBLE CROPPING IF ANY I.E. IF TWO PLOTS
          CONSIDERED TO BE DOUBLE CROPPED. TWO CARDS OF SAME DATA SHOULD BE
          INPUT
0031      DO 100 IW=1,NPLOTS
          IF(IW=1) IW=NE-2, GO TO 100
0032      READ(5,35),MGSB,MGSE,MGSE,MGSE
0033      35 FORMAT(5X,4I2)
0034      MGSB=MGSB
          MGSE=MGSB
0035      MGSB=MGSB
          MGSE=MGSE
0036      MGSE=DGSEW
0037      DGSE=DGSEW
0038      CRUP=1
0039      CALL CROP.COTCRUP,MGSB,DGSB,MGSE,DGSEW,MGSE,MGSE,MU1H,MU1H
0040      100 CONTINUE
0041      110 CONTINUE
0042      C*** ESTABLISH CROP ROTATION SYSTEM FOR MODEL TWO
0043      120 DO 250 I=1,NPLOTS
          MAM=RCYCLE(I)
          SINGLE CROP EACH YEAR
0044      240 DO 240 J=1,NAM
          IF(NY*CE-MM+1)=NRCROP(I,NY)
          LTEMP(I,MM,MM)=NRCROP(I,NY)
          GOTOD 130
          120 LTEMP(I,MM,MM)=LTEMP(I,MM,MM,NY-MM)
          GOTOD 130
0045      130 IF(DOUBLELLNE+2) GO TO 230
          NNN=1FALWT(I)
          GO TO 1150,190,NNN
0046      150 BEGINNING WITH WHEAT
          IF(NY-EQ-1) GO TO 160
          IF(NY-EQ-2) GO TO 170
          IF(NY-EQ-3) GO TO 180
0047      160 IWT((1-NY)=1
          IWT((1-NY)=7
          GU TO 220
0048      170 IWT((1-NY)=7
          IWT((1-NY)=1
          GU TO 220
0049      180 IWT((1-NY)=1WHT((1-NY-2)
          IWT((1-NY)=1WHT((1-NY-2)
0050      190 BEGINNING WITH FALLUM
          IF(NY-EQ-1) GO TO 200
          IF(NY-EQ-2) GO TO 210
          IF(NY-EQ-3) GO TO 215
          IWT((1-NY)=1
          IWT((1-NY)=1

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ORTIRAN IV G LEVEL	ROTATION	DATE = 8046	22/25/31
0124	320 FORMATTED (J) FOR 21 HECTARES (6.320) 1EEH KOPS REINFORCED IN PART (B) 1EQUONI E (J) TO 2 AND ITALI (J) EQ. 1) WRITIE (E. 360) 1FDBOURT (J) TO 2 AND ITALI (J) EQ. 1) WRITIE (E. 370)		
0125			
0126	370 FORMATTED (25X) (1) STUDENCE OF DOUBLE-CROPPING : FALLOW--SUMMER CROP		
0127	1--WINTER WHEAT--SUMMER CROP--AGAIN FALLOW		
0128	360 FORMATTED (25X) (1) STUDENCE OF DOUBLE-CROPPING : WINTER WHEAT--SUMMER CROP--AGAIN WHEAT		
0129	325 FORMATTED (25X) (1) SINGLE CROPPING MANAGEMENT (1)		
0130	PAV U-KPAVLU		
0131	CONTINUE		
0132	340 CONTINUE		
0133	350 FORMATTED (1.46X, * * * ANNUAL SUMMARY * * * *) RETURN		
0134			
0135			
0136			

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FORTRAN IV G LEVEL 21 DATE = 80016 PAGE 0001
      C SNOWMEL DATE = 80016
      C SURROUNDING SNOWMEL PRECIP, WATER, PACK, PET, TEMP, SNOWAV
      C **** CALCULATION OF MOISTURE ADDED TO DISPSAL AREA DUE TO
      C SNOWMEL IN THE AREA **** 22/25/77

      REAL M, MA, MR
      M=0.0
      10 IF(PACK.GT.D11) SNOWAV=PEI
      10 IF(SNOWAV.GT.0.0) PEI=0.0
      10 IF(TEMPAV<-32.) 10,10,20
      10 IF(PRECIP>70.) 70,70,30
      20 IF(PACK)>90.90,40
      30 PACK=PACK+PRECIP
      30 WATER=0.0
      40 GO TO 90
      C **** MA IS SNOWMEL DUE TO ATMOSPHERIC CONDENSATION
      40 MA=0.05*(TEMPAV-34.)
      40 IF(MA.LT.0.0) MA=0.0
      40 IF(PACK-MA)>60.60,50
      40 MA=0.05*(SNOWMEL/DUE TO MAIN)
      50 MR=(PRECIP*(TEMPAV-32.))/14.4
      50 M=MR+MA
      50 IF(PACK-M)>60.70,70
      60 M=PACK
      60 PACK=0.0
      60 GO TO 80
      70 PACK=PACK-M
      70 WATER=M+PRECIP
      80 RETURN
      90 END
      0002
      0003
      0004
      0005
      0006
      0007
      0008
      0009
      0010
      0011
      0012
      0013
      0014
      0015
      0016
      0017
      0018
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      0021
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      0023
      0024
      0025

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FORTRAN IV LEVEL 21          DARCY I          DATE = 00036          22/25/37          PAGE 0061

0.001      SUBROUTINE DARCY(I,PERC,SLUZ,FLG,SMULZ,FLGM,SMGWZ,DLRRC,CONDIZ,C
0.002      TONDIZ,CONDIZ,HUZ,HLZ,IGW,PUZ,DIMENSION H(1),H(1),SND(1),F(1),COND(1),DEP(1),31.0(2)
0.003      DATA DEP,KINGS,EXCESS,RCHGR/30.48,91.46,60.96,34.0(2)

C***  DISTRIBUTION OF WATER ADDED TO EACH PLOT

0.004      EXCESS=0.0
0.005      IF(IPERC.EQ.0.0) GO TO 10
0.006      SMAVZ=SLUZ-SMULZ
0.007      IF(SMAVZ.LT.0.0) SMAVZ=0.0
0.008      EXCESS=PERL-SMAVZ
0.009      IF(EXCESS.LT.0.0) EXCESS=0.0
0.010      SMULZ=SMULZ+PERC-EXCESS
0.011      SMAVLZ=FLCL-SMULZ
0.012      IF(SMAVLZ.LT.0.0) SMAVLZ=0.0
0.013      EXTRA=EXCESS
0.014      EXCESS=EXCESS-SMAVLZ
0.015      IF(EXCESS.LT.0.0) EXCESS=0.0
0.016      SMULZ=SMULZ+EXTRA-EXCESS
0.017      SMAVGW=FLGM-SMGW
0.018      IF(SMAVGW.LT.0.0) SMAVGW=0.0
0.019      EXTRA=EXCESS
0.020      EXCESS=EXCESS-SMAVGW
0.021      IF(EXCESS.LT.0.0) EXCESS=0.0
0.022      SMGWZ=SMGWZ+EXTRA-EXCESS
0.023      RCHGR=EXTRA-EXCESS
0.024      IF(RCHGR.LT.0.0) RCHGR=0.0

C***  MOISTURE REAISRATION USING THE ONE-DIMENSIONAL DARCY EQUATION
C***  FOR UNSATURATED FLOW

C   10  LCOUNT=1
0.025      UTIME=0.1667
0.026      IF(PERC.LE.0.0) UTIME=1.0
0.027      LCOUNT=1
0.028      IF(PERC.LE.0.0) LCOUNT=6
0.029      PERC=EXCESS
0.030      HF(1)=HU/12.
0.031      HF(2)=PW/36.
0.032      HF(3)=PW/24.
0.033      SND(1)=SMULZ/12.
0.034      SND(2)=SMULZ/36.
0.035      SND(3)=SMGWZ/24.
0.036      DO 20 K=1,3
0.037      IF(SND(K).GT.1.0) SND(K)=1.

C   20  IF(SND(K).GT.1.0) SND(K)=1.

C***  CALCULATE SOIL MOISTURE TENSION IN CM
0.038      H(1)=SMULZ-HUZ
0.039      H(2)=SMULZ-HUZ
0.040      H(3)=SMGWZ-HUZ
0.041      DO 30 K=1,3
0.042      H(K)=EXP(H(1)(K))
0.043      IF(H(K).GT.1500.) H(K)=1500.
0.044      IF(H(K).LT.-0.0) H(K)=0.0
0.045      XXX=SMULZ-HUZ
0.046      IF(XXX.LT.0.0) SMULZ=HUZ

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PAGT G002
DATE = 00036 22/25/31

WIRTRAN IV G LEVEL 21 DARLR1
IF(K-EU-1) CONDUZ=CONDULZ*EXP((5.039*SMC(K))/((SMO(K)-WF(K)))
IF(K-EU-2) CONDZ=CONDULZ*EXP((5.595*SMO(K))/((SMO(K)-WF(K)))
IF(K-EU-3) CONDZ=CONDULZ*EXP((70.588*SMO(K))/((SMO(K)-WF(K)))
IF(CND(k).GT.10.0) CUND(k)=10.0
30 IF(COND(k).LT.1.0E-07) CUND(k)=1.0E-07

C*** CALCULATE MOISTURE FLOW. IN INCHES
40 DO 50 K=L_2
50 Q(k)=(COND(k)+COND(k+1))/2*DIMEN*(H(k+1)-H(k))/DEP(k)
SMUZ=SMUZ-Q(1)
SMLZ=SMLZ+Q(1)
SML2=SML2-Q(2)
SMQWZ=SMLZ+Q(2)
RCHGS=RCHGS+Q(2),
LCOUNT=LCOUNT+1
IF(LCOUNT.LE.6 GO TO 40
OPRC=OPRC+RCHGS+RCHGR
RETURN
END

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FORTAN IV G LEVEL 21          STORAG           DATE = 00036        22/25/JI
0001      1F.WINP 1NE.STURAG(P1,P2,P3,PRECIP,SNOW,FRZL,MONTH,GROW,MONTH,KUNUT
C
C   *** CALCULATION OF FETDLOT RUNOFF ***
C
C   IF(BYPASS.EQ.3) GO TO 60
C   CALCULATE 3 DAY ANTECEDENT MOISTURE
C   AM=P1+P2+P3
C   P1=P2
C   P2=P3
C   P3=PRECIP
C   IF(SNOW.GT.0.0.AND.FRZL.EQ.0) GO TO 10
C   IF(PRECIP.LE.0.0) GO TO 50
C   IF(FRZL.EQ.1) GO TO 40
C   IF(AM.LE.0.5.AND.PRECIP.LE.0.5) GO TO 50
C   CALCULATE FETDLOT RUNOFF USING 3 DAY ANTECEDENT MOISTURE CONDITIONS
C
C   MODIFICATION OF THE SCS METHOD
C   10 AM=AM+PRECIP
C   PRESIP=PRECIP+SNOW
C   RC=97
C   IF(MONTH.LT.4.UK.MONTH.GT.-10) GO TO 20
C   IF(AM.LT.0.75) RC=91.0
C   IF(AM.GT.0.75) RC=GROW
C   GO TO 30
C   20 IF(AM.LT.0.50) RC=91.0
C   IF(SNOW.GT.0.0) RC=97.0
C   IF(AM.GT.DORM.AND.PRECIP.GT.DORM) PRESIP=DORM
C   30 CS=1000.0/RC-10.0
C   RUNOFF=(PRECIP-0.2*CS)*2/(PRESIP+0.8*CS)
C   SNOW=0.0
C   IF(RUNOFF.GT.0.06) RUNOFF=RUNOFF-0.06
C   IF(PRESIP-0.2*CS.LT.0.0) GO TO 50
C   GO TO 60
C   40 SNOW=SNOW+PRECIP
C   50 RUNOFF=0.0
C   IF(BYPASS.EQ.2) GO TO 70
C   60 KUNUT=WINP/(3630*7.48)
C   70 RETURN
C
0002
0003
0004
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0008
0009
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0012
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0018
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FORTRAN IV G LEVEL 21 WIRMOD DATE = 80036
 0001 SUBROUTINE WIRMOD PRECIP, MONTH, MODEL, WPCNT
 C***
 C*** SEEDING CLOUDS
 C*** NO PRECIPITATION MODIFICATION DURING MARCH THROUGH SEPTEMBER
 C*** MODEL 2: INCREASE PRECIPITATION DURING MARCH THROUGH SEPTEMBER BY
 C*** THE FOLLOWING PERCENTAGES - 75% FOR RAINFALLS < 0.10 IN.
 C*** 30% FOR RAINFALLS < 0.50 IN. 10% FOR RAINFALLS < 1.0 IN.
 C*** 10% FOR RAINFALLS > 1.0 IN.
 C*** MODEL 3: INCREASE ALL RAINFALLS DURING EVERY MONTH BY A SPECIFIED
 C*** PERCENTAGE, WPCNT
 C*** MODEL 4: INCREASE PRECIPITATION DURING MARCH THROUGH SEPTEMBER BY
 C*** THE FOLLOWING PERCENTAGES - 75% FOR RAINFALLS < 0.10 IN.
 C*** 30% FOR RAINFALLS < 0.50 IN. 10% FOR RAINFALLS < 1.0 IN.
 C*** NO ADJUSTMENT FOR RAINFALLS > 1.0 IN

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0002 IF(MODEL.EQ.1) GO TO 40
0003 IF(MONTH.EQ.3) GO TO 10
0004 IF(MONTH.EQ.9) GO TO 10
0005 ADJ=1.75
0006 IF(PRECIP.GT.0.10) ADJ=1.10
0007 IF(PRECIP.GT.0.50) ADJ=1.30
0008 IF(MODEL.EQ.4) GO TO 20
0009 IF(PRECIP.GT.1.0) ADJ=0.90
0010 GO TO 30
0011 ADJ=1.0
0012 IF(MODEL.EQ.3) ADJ=WPCNT
0013 GO TO 20
0014 IF(PRECIP.GT.1.0) ADJ=1.0
0015 30
0016 PRECIP=PRECIP*ADJ
0017 RETURN
  
```

STATION : FT. SCOTT, KANSAS

1948 TO 1970

MODEL : NO MUNICIPAL INP
 INFLOW TO STORAGE POND
 FEEDOUT AREA = 0.0 ACRES

SIZE OF CRITICAL EVENT : 6.60

POND VARIABLES:

- (A) BASE DIMENSION-- 65.00 FEET BY 65.00 FEET
- (B) SIDE SLOPE-- RUN:RISE = 30. : 1
- (C) MAXIMUM DEPTH-- 14.00 FEET
- (D) MAXIMUM POND VOLUME-- 1133.98 ACRE-INCHES
- (E) DIRECT RECEIVING AREA (FOR PRECIPITATION) -- 18.80 ACRES

AREA VARIABLES:

PLOT 1

- (A) AREA-- 85.00 ACRES
- (B) CROP-- CORN SOY BEANS
- (C) SOIL TYPE-- 1 (SCS SOIL TYPE)
- (D) IRRIGATION RATE-- 0.10 INCHES/DAY
- (E) IRRIGATION MANAGEMENT-- IRRIGATION BELOW 0.50 FIELD CAPACITY
- (F) PLAN IMPLEMENTED-- IRRIGATION
- (G) CROP MANAGEMENT-- CROP ROTATION WITH ** 2 YEAR REPETITION
- (H) DOUBLE CROPPING MANAGEMENT WITH WINTER WHEAT BETWEEN CROPS MENTIONED IN PART (B)
- (I) SEQUENCE OF DOUBLE-CROPPING : FALLOW--SUMMER CROP--WINTER WHEAT--SUMMER CROP--AGAIN FALLOW

PL OT 2

(A) AREA-- 30.00 ACRES
 (B) CROP-- CORN
 (C) SOIL TYPE-- 1 (SCS SOIL TYPE)
 (D) IRRIGATION RATE-- 0.10 INCHES/DAY
 (E) IRRIGATION MANAGEMENT-- IRRIGATION BELOW 0.50 FIELD CAPACITY
 (F) PLAN IMPLEMENTED-- RUNOFF AND IRRIGATION
 (G) CROP MANAGEMENT-- CROP ROTATION WITH ** 2 YEAR REPETITION
 (H) SINGLE CROPPING MANAGEMENT

PL OT 3

(A) AREA-- 30.00 ACRES
 (B) CROP-- SOY BEANS
 (C) SOIL TYPE-- 1 (SCS SOIL TYPE)
 (D) IRRIGATION RATE-- 0.10 INCHES/DAY
 (E) IRRIGATION MANAGEMENT-- IRRIGATION BELOW 0.50 FIELD CAPACITY
 (F) PLAN IMPLEMENTED-- RUNOFF AND IRRIGATION
 (G) CROP MANAGEMENT-- NO CROP ROTATION
 (H) SINGLE CROPPING MANAGEMENT

PL OT 4

(A) AREA-- 190.00 ACRES
 (B) CROP-- PASTURE
 (C) SOIL TYPE-- 1 (SCS SOIL TYPE)
 (D) IRRIGATION RATE-- 0.10 INCHES/DAY
 (E) IRRIGATION MANAGEMENT-- IRRIGATION BELOW 0.0 FIELD CAPACITY
 (F) PLAN IMPLEMENTED-- RUNOFF
 (G) CROP MANAGEMENT-- NO CROP ROTATION
 (H) SINGLE CROPPING MANAGEMENT

PLOT 5

(A) AREA-- 120.00 ACRES
 (B) CROP-- CORN
 (C) SOIL TYPE-- 1 ISCS SOIL TYPE!
 (D) IRRIGATION RATE-- 0.10 INCHES/DAY
 (E) IRRIGATION MANAGEMENT-- IRRIGATION BELOW 0.0 FIELD CAPACITY
 (F) PLAN IMPLEMENTED-- RUNOFF F
 (G) CROP MANAGEMENT-- NO CROP ROTATION
 (H) SINGLE CROPPING MANAGEMENT

PLOT 6

(A) AREA-- 40.00 ACRES
 (B) CROP-- SORGUM
 (C) SOIL TYPE-- 1 ISCS SOIL TYPE!
 (D) IRRIGATION RATE-- 0.10 INCHES/DAY
 (E) IRRIGATION MANAGEMENT-- IRRIGATION BELOW 0.0 FIELD CAPACITY
 (F) PLAN IMPLEMENTED-- RUNOFF F
 (G) CROP MANAGEMENT-- NO CROP ROTATION
 (H) SINGLE CROPPING MANAGEMENT

*** ANNUAL SUMMARY ***

	DISCHARGE OF	33.25 ACRE-IN REQUIRES VOLUME OF	1167.23 ACRE-IN FOR 100.00 % CONTROL WHERE L = W = 271.26
1/ 5/63 - DISCHARGE OF	2.65 ACRE-IN REQUIRES VOLUME OF	1169.88 ACRE-IN FOR 100.00 % CONTROL WHERE L = W = 271.76	
1/20/63 - DISCHARGE OF	2.82 ACRE-IN REQUIRES VOLUME OF	1172.10 ACRE-IN FOR 100.00 % CONTROL WHERE L = W = 272.29	
1/23/63 - DISCHARGE OF	0.94 ACRE-IN REQUIRES VOLUME OF	1173.64 ACRE-IN FOR 100.00 % CONTROL WHERE L = W = 272.47	
1/26/63 - DISCHARGE OF	20.66 ACRE-IN REQUIRES VOLUME OF	1194.30 ACRE-IN FOR 100.00 % CONTROL WHERE L = W = 276.32	
2/ 4/63 - DISCHARGE OF	95.92 ACRE-IN REQUIRES VOLUME OF	1290.23 ACRE-IN FOR 100.00 % CONTROL WHERE L = W = 293.96	
3/ 5/63 - DISCHARGE OF	84.28 ACRE-IN REQUIRES VOLUME OF	1374.51 ACRE-IN FOR 100.00 % CONTROL WHERE L = W = 309.10	
3/ 9/63 - DISCHARGE OF	8.39 ACRE-IN REQUIRES VOLUME OF	1382.89 ACRE-IN FOR 100.00 % CONTROL WHERE L = W = 310.59	
3/11/63 - DISCHARGE OF	682.22 ACRE-IN REQUIRES VOLUME OF	2065.11 ACRE-IN FOR 100.00 % CONTROL WHERE L = W = 423.00	
8/13/63 - DISCHARGE OF	WATER ACCOUNT FOR STORAGE FACILITY (IN ACRE-INCHES)	- 1963	

INFLOWS

MONTH	PRECIP.	MUNICIPAL	FEEDOUT	RUNOFF	IRR. DAYS	DISPOSAL VOL.	SURFACE EVAP.	DISCHARGE	VOL. CHANGE
JAN.	25.6	0.0	0.0	27.2	0.	0.0	0.0	39.7	5.1
FEB.	0.4	0.0	0.0	20.7	0.	0.0	0.1	20.7	-7.5
MAR.	51.5	0.0	0.0	171.6	0.	60.8	188.6	0.0	13.87
APR.	14.1	0.0	0.0	0.0	22.	82.2	0.0	0.0	-25.1
MAY	76.5	0.0	0.0	210.0	25.	187.0	93.2	0.0	12.66
JUNE	60.4	0.0	0.0	99.6	212.5	10.4	10.4	49.2	-12.56
JULY	65.1	0.0	0.0	122.0	10.	30.0	121.4	0.0	49.7
AUG	112.2	0.0	0.0	889.3	18.	54.0	119.1	682.2	32.1
SEPT	26.7	0.0	0.0	0.0	30.	320.0	80.0	0.0	126.2
OCT.	12.2	0.0	0.0	0.0	31.	449.5	35.3	0.0	11.61
NOV.	44.7	0.0	0.0	7.6	0.	10.3	0.0	-472.6	-7.49
DEC.	10.2	0.0	0.0	1527.9	136.	0.0	10.3	42.4	7.95
TOT.	499.6	0.0	0.0	1527.9	136.	1253.0	122.5	6.5	8.03
							931.1	-879.2	-0.99

PLCT NO. 1

CRUP--SOY BEANS DOUBLE CRUPPING WITH WHEAT

SOIL TYPE-- 1 DISPOSAL AREA-- 85.00 ACRES

WATER BALANCE (INCHES) IN THE DISPOSAL AREA - 1963

INPUTS

MONTH	PRECIPITATION	IRRIGATION	INTERCEPTION	SURFACE RUNOFF	PERCOLATION	AET	CHANGE IN SH
JAN.	1.36	0.0	0.10	0.32	0.0	0.26	0.18
FEB.	0.02	0.0	0.18	0.05	0.0	0.52	-0.13
MAR.	2.74	0.0	0.71	0.88	0.0	1.42	-0.27
APR.	0.75	2.20	2.20	0.0	0.0	2.74	-2.02
MAY	4.07	2.50	2.70	0.50	0.0	2.26	1.21
JUNE	3.21	0.0	0.69	0.94	0.0	2.18	-0.30
JULY	3.46	0.0	0.30	1.13	0.0	1.12	-1.12
AUG	5.47	0.0	0.50	1.63	0.0	2.82	-0.98
SEPT	1.44	2.00	2.10	0.0	0.0	2.53	-1.31
OCT.	0.65	3.10	3.03	0.0	0.0	0.57	0.15
NOV.	2.38	0.0	0.52	0.08	0.0	0.52	1.37
DEC.	0.54	0.0	0.12	0.0	0.0	0.25	0.17
TOT.	26.57	9.30	13.15	7.01	0.0	17.19	-0.99

PLCT NO. 2

CROP--SORGHUM

SOIL TYPE-- 1

DISPENSAL AREA-- 30.00 ACRES

WATER BALANCE (INCHES) IN THE DISPOSAL AREA - 1963					
MONTH	INPUTS			OUTPUTS	
	PRECIPITATION	IRRIGATION	INTERCEPTION	SURFACE RUNOFF	PERCOLATION
JAN.	1.39	0.00	0.10	0.10	0.27
FEB.	0.32	0.00	0.18	0.07	0.51
MAR.	2.74	0.00	0.71	0.54	-0.03
APR.	0.75	0.00	0.32	0.00	-0.21
MAY	4.07	0.00	0.76	1.31	-1.01
JUNE	3.21	0.00	0.49	0.84	0.24
JULY	3.49	1.00	1.20	0.91	-2.33
AUG.	5.97	1.80	1.90	2.42	-1.24
SEP.	1.42	3.30	3.00	0.30	-0.24
OCT.	0.45	3.10	3.03	0.00	0.57
NOV.	2.36	0.00	0.52	0.11	-1.25
DEC.	0.57	0.00	0.12	0.00	0.01
TOT.	26.57	0.00	12.53	6.38	-0.42

PLCT NO. 3

CROP--SWEET BEANS

SOIL TYPE-- 1

DISPENSAL AREA-- 30.00 ACRES

WATER BALANCE (INCHES) IN THE DISPOSAL AREA - 1963					
MONTH	INPUTS			OUTPUTS	
	PRECIPITATION	IRRIGATION	INTERCEPTION	SURFACE RUNOFF	PERCOLATION
JAN.	1.38	0.00	0.10	0.10	0.27
FEB.	0.02	0.00	0.18	0.07	0.81
MAR.	2.74	0.00	0.71	0.54	-0.54
APR.	0.75	0.00	0.32	0.00	-0.03
MAY	4.07	0.00	0.76	1.31	-0.21
JUNE	3.21	0.00	0.49	0.64	-1.03
JULY	3.46	0.00	0.30	0.90	-0.39
AUG.	5.97	0.00	2.00	3.63	-0.69
SEP.	1.42	2.00	2.10	0.00	-1.14
OCT.	0.65	3.10	3.03	0.00	-0.12
NOV.	2.30	0.00	0.52	0.11	0.33
DEC.	0.57	0.00	0.12	0.00	0.17
TOT.	26.57	5.10	9.33	7.32	-0.37

PLOT NO. 4

CROP--PASTURE SOIL TYPE-- 1 DISPOSAL AREA--190.00 ACRES

WATER BALANCE (INCHES) IN THE DISPOSAL AREA - 1963							
MONTH	INPUTS			OUTPUTS			
	PRECIPITATION	IRRIGATION	INTERCEPTION	SURFACE RUNOFF	POROSITY		
JAN.	1.14	0.0	0.10	0.93	0.0	0.31	0.42
FEB.	0.02	0.0	0.14	0.23	0.0	0.81	-0.50
MAR.	2.74	0.0	0.71	0.28	0.2	1.54	-0.03
APR.	0.75	0.0	0.32	0.0	0.0	2.28	-1.45
MAY	4.07	0.0	0.76	0.04	0.0	3.34	0.92
JUNE	3.21	0.0	0.49	0.02	0.0	3.93	-1.40
JULY	3.46	0.0	0.30	0.03	0.0	2.94	-0.9
AUG.	5.57	0.0	0.50	1.65	0.0	4.05	-0.72
SEPT	1.42	0.0	0.50	0.0	0.0	0.44	-0.72
OCT.	0.45	0.0	0.28	0.11	0.0	0.33	-0.04
NOV.	2.34	0.0	0.46	0.0	0.0	0.52	-1.49
DEC.	0.54	0.0	0.12	0.0	0.0	0.25	-0.47
TOT.	26.57	0.0	4.93	2.07	0.0	20.91	-1.56

PLOT NO. 5

CROP--CORN SOIL TYPE-- 1 DISPOSAL AREA--120.00 ACRES

WATER BALANCE (INCHES) IN THE DISPOSAL AREA - 1963							
MONTH	INPUTS			OUTPUTS			
	PRECIPITATION	IRRIGATION	INTERCEPTION	SURFACE RUNOFF	POROSITY		
JAN.	1.36	0.0	0.10	0.10	0.0	0.27	0.39
FEB.	0.02	0.0	0.18	0.97	0.0	0.74	-0.51
MAR.	2.74	0.0	0.71	0.54	0.0	1.51	-0.03
APR.	0.75	0.0	0.32	0.0	0.0	0.85	-0.42
MAY	4.07	0.0	0.76	0.39	0.0	3.35	-0.37
JUNE	3.21	0.0	0.49	0.15	0.0	4.10	-1.44
JULY	3.46	0.0	0.30	0.19	0.0	3.03	-0.50
AUG	5.97	0.0	0.30	2.34	0.0	3.66	-0.20
SEPT	1.42	0.0	0.50	0.0	0.0	1.12	-0.17
OCT.	0.45	0.0	0.24	0.0	0.0	0.34	-0.04
NOV.	2.34	0.0	0.46	0.0	0.0	0.33	-1.56
DEC.	0.54	0.0	0.12	0.0	0.0	0.20	-0.24
TOT.	26.57	0.0	4.93	3.98	0.0	16.72	-1.06

PLOT NO. 4

CHURCH—SUGARLOAF
SOIL TYPE-- I
DISPOSAL AREA-- 40.00 ACRES

WATER BALANCE (INCHES) IN THE DISPOSAL AREA - 1963

MONTH	INPUTS		OUTPUTS		CHANGE IN SM
	PRECIPITATION	IRRIGATION	INTERCEPTION	SURFACE RUNOFF	
JAN.	1.36	0.0	0.10	0.10	0.30
FEB.	0.92	0.0	0.18	0.07	-0.54
MAR.	2.74	0.0	0.71	0.54	-0.06
APR.	0.75	0.0	0.32	0.00	-0.21
MAY	4.07	0.0	0.76	1.31	-1.03
JUNE	3.21	0.0	0.69	0.84	0.53
JULY	3.44	0.0	0.30	0.74	-2.30
AUG.	5.97	0.0	0.50	2.34	-1.40
SEP.	1.42	0.0	0.50	0.00	-0.30
OCT.	0.65	0.0	0.28	0.00	0.24
NOV.	2.30	0.0	0.44	0.00	1.24
DEC.	0.54	0.0	0.12	0.00	0.21
TOT.	26.57	0.0	4.93	6.15	-1.10
PERCENT OF WASTEWATER CONTROLLED=		54.07			
POTENTIAL DISPOSAL DAYS= 136					
PACK ON DECEMBER 31 = 0.0					
INPUTS-OUTPUTS-CHANGE IN SNOW STOREAGE= CHANGE IN SOIL MOISTURE					
PERCENT OF MAXIMUM POND VOLUME REQUIRED = 100.00					
ESTIMATED LAKE EVAPORATION. INCHES = 47.03					

***** FINAL SUMMARY *****

METEOROLOGICAL SUMMARY

AVERAGE ANNUAL LAKE EVAPORATION= 45.31 INCHES

AVERAGE ANNUAL PRECIPITATION= 38.45 INCHES

PRECIPITATION RANGE= 34.01 INCHES (FROM A LOW OF 26.35 INCHES TO A HIGH OF 60.36 INCHES)

AVERAGE ANNUAL MOISTURE DEFICIT= 6.86 INCHES

SUMMARY OF POND OPERATIONS

NO. OF YEARS HAVING A DISCHARGE= 23

AVERAGE NO. OF DISCHARGES / YEAR HAVING A DISCHARGE= 29.04

AVERAGE DISCHARGE=115.75 ACRE-INCHES

AVERAGE PERCENT OF DISCHARGE CONTROLLED BY EVAPORATION AND IRRIGATION= 36.71

TOTAL DISCHARGE VOLUME= 77320.19 ACRE-INCHES

TOTAL NO. OF DISCHARGES=660.

MAXIMUM DISCHARGE=***** ACRE-INCHES

AVERAGE ANNUAL VOLUME OF IRRIGATED WATER TO THE FIELD= 625.30 ACRE-INCHES

SUMMARY OF DISPOSAL PLOTS

PLOT 1

AVERAGE ANNUAL DISPOSAL AREA RUNOFF= 11.01 INCHES

AVERAGE ANNUAL DISPOSAL AREA PERCOLATION= 1.03 INCHES

AVERAGE ANNUAL NO. OF DISPOSAL DAYS= 46.2

AVERAGE ANNUAL DISPOSAL AREA INTERCEPTION= 10.49 INCHES

AVERAGE ANNUAL DISPOSAL AREA EVAPOTRANSPIRATION= 20.60 INCHES

AVERAGE ANNUAL DISPOSAL AREA CHANGE IN SOIL MOISTURE= -0.06 INCHES

PLOT 2

AVERAGE ANNUAL DISPOSAL AREA RUNOFF= 11.98 INCHES

AVERAGE ANNUAL DISPOSAL AREA PERCOLATION= 1.33 INCHES

AVERAGE ANNUAL NO. OF DISPOSAL DAYS= 53.7

AVERAGE ANNUAL DISPOSAL AREA INTERCEPTION= 11.21 INCHES

AVERAGE ANNUAL DISPOSAL AREA EVAPOTRANSPIRATION= 19.34 INCHES

AVERAGE ANNUAL DISPOSAL AREA CHANGE IN SOIL MOISTURE= -0.05 INCHES

PLOT 3

AVERAGE ANNUAL DISPOSAL AREA RUNOFF= 12.60 INCHES
 AVERAGE ANNUAL DISPOSAL AREA PERCOLATION= 1.29 INCHES
 AVERAGE ANNUAL NO. OF DISPOSAL DAYS= 24.0
 AVERAGE ANNUAL DISPOSAL AREA INTERCEPTION= 0.00 INCHES
 AVERAGE ANNUAL DISPOSAL AREA EVAPORATION= 18.06 INCHES
 AVERAGE ANNUAL DISPOSAL AREA CHANGE IN SOIL MOISTURE= -0.04 INCHES

PLOT 4

AVERAGE ANNUAL DISPOSAL AREA RUNOFF= 7.73 INCHES
 AVERAGE ANNUAL DISPOSAL AREA PERCOLATION= 1.59 INCHES
 AVERAGE ANNUAL NO. OF DISPOSAL DAYS= 3.0
 AVERAGE ANNUAL DISPOSAL AREA INTERCEPTION= 0.00 INCHES
 AVERAGE ANNUAL DISPOSAL AREA EVAPORATION= 22.27 INCHES
 AVERAGE ANNUAL DISPOSAL AREA CHANGE IN SOIL MOISTURE= -0.03 INCHES

PLOT 5

AVERAGE ANNUAL DISPOSAL AREA RUNOFF= 11.34 INCHES
 AVERAGE ANNUAL DISPOSAL AREA PERCOLATION= 0.80 INCHES
 AVERAGE ANNUAL NO. OF DISPOSAL DAYS= 0.0
 AVERAGE ANNUAL DISPOSAL AREA INTERCEPTION= 6.00 INCHES
 AVERAGE ANNUAL DISPOSAL AREA EVAPORATION= 19.48 INCHES
 AVERAGE ANNUAL DISPOSAL AREA CHANGE IN SOIL MOISTURE= -0.05 INCHES

PLOT 6

AVERAGE ANNUAL DISPOSAL AREA RUNOFF= 12.12 INCHES
 AVERAGE ANNUAL DISPOSAL AREA PERCOLATION= 1.37 INCHES
 AVERAGE ANNUAL NO. OF DISPOSAL DAYS= 0.0
 AVERAGE ANNUAL DISPOSAL AREA INTERCEPTION= 0.00 INCHES
 AVERAGE ANNUAL DISPOSAL AREA EVAPORATION= 18.14 INCHES
 AVERAGE ANNUAL DISPOSAL AREA CHANGE IN SOIL MOISTURE= -0.06 INCHES

SUMMARY OF STATISTICAL DATA

INTENSITY (IN.)	PRECIPITATION FREQUENCY DATA		
	FREQUENCY (4)	FREQUENCY (DAYS)	RUNOFF FREQ. (DAYS)
>0.0	100.00	1970.00	1074.00
>0.1	71.27	1404.00	1065.00
>0.2	54.01	1064.00	874.00
>0.3	42.99	847.00	759.00
>0.4	34.72	684.00	624.00
>0.5	29.29	577.00	539.00
>0.6	23.05	454.00	432.00
>0.7	19.59	386.00	369.00
>0.8	16.55	326.00	312.00
>0.9	14.57	287.00	274.00
>1.0	12.20	242.00	231.00
>1.1	10.46	204.00	197.00
>1.2	9.19	181.00	175.00
>1.3	7.97	157.00	154.00
>1.4	7.16	141.00	136.00
>1.5	6.29	124.00	119.00
>1.6	5.23	103.00	98.00
>1.7	4.26	84.00	82.00
>1.8	3.81	75.00	73.00
>1.9	2.99	59.00	57.00
>2.0	2.34	50.00	50.00
>2.5	0.56	11.00	11.00
>3.0	0.20	4.00	4.00
>5.0	0.10	2.00	2.00
>10.	0.0	0.0	0.0

DEVELOPMENT OF SUPPLEMENTAL IRRIGATION
SYSTEM MODEL FOR A FARM IN
SOUTHEASTERN KANSAS

by

JONG SEONG IM

B.S., Seoul National University, 1974

AN ABSTRACT OF A MASTER'S THESIS

submitted in partial fulfillment of the
requirements for the degree

MASTER OF SCIENCE

Department of Civil Engineering

KANSAS STATE UNIVERSITY
Manhattan, Kansas

1980

ABSTRACT

Supplemental irrigation has been increasingly popular in the eastern half of the United States. In an area where a crop can be grown by natural rainfall alone, but additional water produces improved yields, irrigation is defined as supplemental.

The aim of this research is to study the feasibility of supplemental irrigation in subhumid regions by developing a general hydrologic crop management model. This purpose can be achieved by testing a continuous watershed hydrologic model, which can estimate the effect of each hydrologic component on a specified site. The actual site used to test the model is owned by Ronnie Felt, located near Uniontown, Kansas, in Bourbon County. The Felt site consists of a $11.66 \times 10^4 \text{ m}^3$ (94.5 ac-ft) storage pond, and a 166 ha (410 acres) watershed, of which 57 ha (145 acres) are irrigated with three center pivot sprinklers. To examine the performance of a pond water supply for irrigation, meteorological data (1948-1970) and various geographic input variables were used in the simulation. The variability of surface runoff in response to precipitation, and irrigation demand are important factors to analyze the reliability of a pond. A general method of crop management system is capable of simulating any typical cropping schedule for Southeastern Kansas.

According to this simulation, the annual irrigation demand was estimated to be about 110 mm (4.3 inches) on the average. The precipitation produces sufficient runoff to the pond for use as supplemental irrigation water. The storage pond can meet the irrigation needs at the probability level of 91 percent.