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MULTIPLE ELECTRON CAPTURE AT HIGH VELOCITIES USING THE BATES POTENTIAL IN THE INDEPENDENT ELECTRON APPROXIMATION

by

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CHAPTER 1

INTRODUCTION

Since the atom is a microscopic quantity, its properties cannot be determined using macroscopic measuring devices directly. One way to investigate the atom is to probe it with a particle that is of the same relative size. In an atom-ion collision, this particle is a fast moving ionic projectile. It is incident upon the target atom to be investigated, usually at some known energy, trajectory and charge state. As the projectile passes near the atom, it is deflected from its original path. At the same time some of the electronic properties of the atom and the ion may be altered. Studying the results of the collision reveals information about the structure of the target and the forces of interaction between the two systems.

The quantity that is measured in an atom-ion collision is the total cross section. It is proportional to the probability that if the projectile is in a particular initial state, its interaction with the target will cause a transition into a particular final state. Two transitions of interest are excitation of a projectile electron into a higher energy level, and ionization of a projectile electron into the continuum. Extensive work has been done in the calculation of both excitation and ionization cross sections. It has been shown that there is another type of transition that occurs. This is known as electron capture or charge transfer.

Electron capture is a rearrangement collision in which one or more electrons initially bound to the target atom are, upon collision, transferred to the projectile. This process is believed to be significant in many aspects of physical research as well as in the study of the structure of the atom. One such aspect is astrophysics. Since multiply charged ions are present in the interstellar medium, along with neutral hydrogen and helium atoms, if charge capture reactions are rapid at the thermal energies of the medium, they play an important role in reducing the fractional abundance of such ions. Then charge capture must be included in calculations of models to be compared with observed physical conditions of the interstellar medium.

Louisell et. al. have applied charge transfer to the development of an x-ray laser. The process they propose invloves passing a beam of bare nuclei through a target and capturing electrons into a particular excited state. Then population inversion will cause the stimulated emission of x-rays of a particular wavelength. Sweeping the ions along a foil at speeds near that of light will cause the radiation emitted from the first ions to stimulate radiation from the inverted ions arriving along the foil later. Hence charge transfer could provide a mechanism for pumping of the required excited-state population.

The role of charge exchange in nuclear fusion studies is discussed by Crandall et. al.³ It is significant in such properties as charge-state distribution, resistivity and energy transfer. It is believed that charge transfer

between multicharged impurities and neutral particles injected into a plasma may be instrumental in stopping the injected beam at the outer edge of the plasma, thus destroying the needed plasma heating. Klinger et. al. emphasize the need for the charge transfer process in the ion source extraction region of heavy-ion accelerators. This process, in which atoms are repeatedly stripped of electrons while being accelerated, has opened new possibilities in the design of high energy, heavy-ion accelerators.

Since the range of application of multiple charge capture is so broad, it is important to develop a suitable formalism for the collision process. Much work has been done in the calculation of first order single charge capture cross sections. Since the transition matrix is too complicated to solve exactly, one must approximate the initial and final wave functions and the perturbing potential used. Several attempts have been made to calculate single capture cross sections that closely agree with those experimentally measured.

Oppenheimer⁵, in 1928, and Brinkman and Kramers⁶, in 1930, calculated cross sections for a single K-shell electron of hydrogen captured into the K-shell of a proton. They used the product of a plane wave and a bound state hydrogen wave function for their initial and final wave functions. This is the first Born approximation. They argued that the internuclear potential should not have an appreciable effect on the probability of charge capture since its only effect seems to be a slight deflection of the projectile. Their total interaction potential, then, is the Coulomb

attraction between the projectile ion and the electron to be captured. When compared to experiment, their results seem to have the right shape, but are too large by a factor of four near incident energies of 100 KeV, and even larger at smaller energies.

Jackson and Schiff, in 1953, and Bates and Dalgarno, and 1952, used the sum of the projectile-electron and the projectile-target nucleus potentials as the perturbing potential in their calculations. They argued that since charge capture is a three body problem involving non-orthogonal initial and final states, the internuclear term is not negligible.

Combining this with the first Born wave functions, they obtained cross sections for protons on hydrogen that were in better agreement with experiment than those of Oppenheimer and Brinkman and Kramers.

A distorted wave Born approximation is used by Bassel and Gerjuoy in an attempt to reconcile the problem of whether or not to include the internuclear potential. The result of their use of the total interaction potential (electron-projectile and nuclear-nuclear interactions) and the plane wave limit to the distorted wave Born approximation in the transition matrix turns out to be the same as using the plane wave Born approximation wave functions combined with the difference between the instantaneous and average interaction potentials. This does not depend on the internuclear term directly. Their total cross sections for charge capture of a single electron from the ground state of the hydrogen atom to the ground state of the incident

proton is in best agreement with experiment of the three procedures presented.

Bates 11, in 1958, approaches the problem from a different point of view. He recognizes that the inclusion of the dubious internuclear potential does in fact improve agreement with experiment, but explains that the reason for the inclusion is unsatisfactory. The internuclear potential should have little effect on the total cross section especially for fast moving projectiles. He shows that one needs rather to be concerned with the problems of the non-orthogonality of the initial and final states and with the incongruous fact that the choice of the zero point potential alters the total cross sections. His final results are very similar to those of Bassel and Gerjuoy but the physical interpretation for his calculations is a bit more palatable.

First order calculations have been extended to single capture involving arbitrary projectile and target charge states as well as capture into higher energy levels for a wide variety of incident energies. A summary of these results for hydrogen targets has been compiled by Tawara and Russek. More general results are reviewed by Betz. 13

Only recently has any attempt been made to develop a formalism to calculate multiple capture cross sections. It is known that double charge capture is the dominant process for resonant systems at low energies. In the case of alpha particles on helium, double capture cross sections are almost an order of magnitude larger than single capture cross sections at energies of about 10 KeV. 14 Crandall et. al. 3 have shown

that in this energy range, double capture is also the dominant process for C^{+l_1} on helium.

Even though multiple charge transfer is accepted as an important process, and a great deal of experimental data for multiple capture is available, few theoretical calculations have been attempted because the interaction is too complicated to be dealt with using previously developed techniques. Gerasimenko 15 has calculated double capture cross sections by protons from helium using the first Born approximation. His results are two orders of magnitude higher than experimental values. Roy et. al. 16 used an impact parameter formalism 17 to calculate the same cross sections. They too get poor agreement with experiment. Biswas et. al. 18 investigate an integral approximation to the three state close-coupling formalism for protons on helium. They get excellent agreement with experiment for incident energies from 5 KeV to 1 MeV. This agreement is not well understood, however, since their method is the wave treatment counterpart to the impact treatment of Roy et. al. and one would expect similar results. C. D. Lin¹⁹ uses a three state close-coupling formalism too, and replaces the interelectron Coulomb interaction by a monopole term with a screening charge. He extends the calculation to higher charge states, and gets good agreement with experiment.

It is the purpose of this thesis to present a different approach to the calculation of multiple charge transfer cross sections. The independent electron approximation developed by Mc Guire and Weaver²⁰ for atomic scattering by

heavy particles will be applied to the case of charge transfer. In this approximation, the full wave function for the scattering system is expressed as a product of single electron wave functions, and the cross sections for multiple electron transfer are expressed as products of single electron probabilities. This approximation is independent of the perturbation theory one chooses to use. This means that all the techniques considered when dealing with single charge capture are applicable to the problem of multiple charge transfer in this independent electron approximation.

The Bates-Born approximation is used to calculate cross sections for single charge capture from the ground state of helium atoms to the ground state of alpha particles in the incident energy range of 0 to 1000 KeV. This calculation is compared to experiment and the discrepancies noted. Then charge capture cross sections are calculated for the same system. The discrepancies here are compared to those for single capture in order to test the validity of the independent electron approximation.

CHAPTER 2

CROSS SECTIONS

In a scattering experiment, a target is bombarded by a monoenergetic beam of particles of known incident flux. A detector with a finite detecting area is placed at a particular angle with respect to the direction of the incident beam. It counts the number of particles deflected into that angle per unit time. This number normalized by the incident flux, I, is known as the differential cross section. Symbolically,

$$\frac{d\Omega}{d\Omega} = \frac{dN(\theta, \phi)}{I}.$$

Classically, the particles approach the scattering center at a distance b from its center, and are scattered through an angle, θ . The distance, b, is known as the impact parameter, and θ is referred to as the scattering angle. Since the detector has a finite area, particles scattered into angles from θ to θ + $d\theta$ will be detected. The total number of particles counted per second is then,

and the classical differential cross section is

$$\frac{d\sigma}{d\Omega} = \frac{d\Delta\Omega}{d\phi} = b \frac{d\phi}{d\phi}$$

The particles of concern here can be thought of quantum

mechanically as waves. In order to define a quantum mechanical differential cross section, one assumes that the motion of the particles involved in the scattering process may be described by the Hamiltonian

$$H = H_o + V_i$$

where V_i is effective over only a finite range. The incident partical flux may be visualized as the superposition of plane waves. The scattering center may be regarded as the source of spherical waves. The simplest expression for the incident wave is a normalized plane wave

where \vec{k}_i is the initial momentum of the system, \vec{r} is the position vector of the incident beam, μ_i is the reduced mass of the initial system, and A is the normalizing amplitude such that the intensity of the incident beam is

Asymptotically, the final wave function may be expressed as the superposition of the incident plane wave and some angular dependent amplitude times a spherical wave.

The intensity of the beam scattered at an angle θ is

$$N(\theta) = \left| f(\theta) \frac{e^{i \vec{k} \cdot \vec{r}}}{r} \right|^2 \cdot \frac{\hbar k_i}{\mu_i} = \left| f(\theta) \right|^2 \frac{\hbar k_i}{\mu_i r^2}.$$

Then the number of particles scattered into the detector

of area, $r^2 d\Omega$ is

Hence the quantum mechanical differential cross section is

$$\frac{d\Omega}{d\alpha} = |f(\theta)|^2,$$

and $f(\theta)$ is known as the scattering amplitude.

If the perturbation, V_i , is effective over only a finite range, one may assume it is small in comparison with H_0 and may solve the Schrödinger equation for the system

using time-dependent perturbation theory. ^21 The resulting transition rate from an initial state Ψ_i to a final state Ψ_f is

For a system with final momentum \vec{k}_f , and final reduced mass μ_f in a volume L^3 , the density of final states is

$$\rho_{f} = \frac{\mu_{c} k_{c} L^{3}}{8\pi^{3} h^{2}} d\Omega.$$

The quantity $\langle \psi_i | \psi_i \rangle$ will be referred to as the transition matrix element or transition matrix and will be denoted by T_{if} . Then

Since the transition rate is equivalent to the number of particles detected per unit time, the differential cross

section may be expressed as

Since the incident flux was shown above to be

the differential cross section may be expressed in terms of the transition matrix as follows

$$\frac{d\sigma}{d\Omega} = |f(\theta)|^2 = \mu_{i,MF} \left(\frac{k_F}{k_i}\right) \left(\frac{L^2}{2\pi h^2}\right)^2 |T_{if}|^2.$$

In order to simplify the coefficient of the differential scattering cross section, atomic units will be adopted here and will be used throughout the rest of the paper unless otherwise specified. In atomic units, e, the charge on the electron, is taken to be one unit of charge. The mass of the electron, m_e , is one unit of mass. Plancks constant divided by 2π , \hbar , is one unit of energy times time. In this system, the differential cross section is

A total cross section may be obtained by integration of the differential cross section over all possible scattering angles.

$$T = \int \frac{d\sigma}{d\Omega} d\Omega = \int \int \frac{d\sigma}{d\Omega} d(\cos\theta) d\phi.$$

Classically, the total cross section is

where P(b) is the probability that a particle incident at an impact parameter b will be scattered into an angle e.

For transition matrix elements independent of the azimuthal angle ϕ .

$$\sigma = \frac{\mathcal{H}: \mathcal{H}_{\theta}}{2\pi} \left(\frac{k_{\theta}}{k_{i}}\right) \int \left|T_{i, \theta}\left(\theta\right)\right|^{2} d\left(\cos\theta\right) \qquad \text{in units of } a_{\theta}^{2}.$$

Two other common forms in which the total scattering cross section is given are

$$\sigma = \frac{\mu_i \, \mu_f}{2 \, \pi^2} \left(\frac{\kappa_f}{\kappa_i} \right) \int \left| T_{if} \left(\theta \right) \right|^2 d \left(\cos \theta \right) \qquad \text{in units of } \pi a^2.$$

and

It has proved useful 22,23 to obtain an expression for total cross sections that depends quantum mechanically on impact parameter rather than scattering angle. This is accomplished by expanding the transition matrix in partial waves. That is,

Tif (0) =
$$\left(\frac{\pi^2}{\mu_i \mu_f k_i k_f}\right)^{\gamma_2} \sum_{\ell=0}^{\infty} (2\ell+1) \alpha_{\ell} P_{\ell}(\cos \theta)$$
.

Then

$$\sigma = \frac{\pi}{k_i k_i} \sum_{k=0}^{\infty} (2\ell+1) |a_k|^2,$$

where a_1 is the 1th probability amplitude and P_1 (cos θ) is the 1th order Legendre polynomial. Multiplying both sides of the above expression for T_{if} by P_{1} (cos θ) and integrating over all angles, one finds that

$$a_e = \left(\frac{\mu_i \, \mu_e \, k_i \, k_e}{4 \pi^a}\right)^{1/2} \int_{-1}^{1} T_{if}(\theta) P_e(\cos \theta) \, d(\cos \theta).$$

For heavy projectiles, large values of 1 dominate, and the only non-zero probability amplitudes are those for 1 on the order of k_i times b. Also for large 1, $P_1(\cos\theta)$ may be approximated as the zeroth order Bessel function with argument 1 times θ . Then P(b) becomes

One may now compute cross sections by integration over impact parameter or scattering angle provided the transition matrix element can be evaluated for the system of interest.

CHAPTER 3

APPROXIMATIONS

3.1 The Independent Electron Approximation.

In the independent electron approximation 20 to be described below, the target atom is treated as a collection of electrons which independently interact with the projectile. During the time of collision, the interaction between the projectile and a given electron neither affects nor depends on the other target electrons. The non-participating electronic wave functions are not used in the calculation. One approach to multi-electron transitions is to calculate single transition probabilities then to use the product of these single probabilities to calculate multiple transition probabilities.

Consider a particle of charge Z_1 , incident on a target with Z_2 electrons. The wave function for the full system, $\Psi(\vec{R}, \vec{r}_1, \vec{r}_2, \dots \vec{r}_{Z_2})$, is a solution of the Schrödinger equation

Here, \vec{R} is the projectile position vector and $\vec{r_1}$, $\vec{r_2}$,... $\vec{r_Z}_2$ are the target electron coordinates. The full Hamiltonian is

$$H = \frac{p^{2}}{a_{jki}} + \frac{2}{R^{2}} - \sum_{j=1}^{2} \frac{2}{(R-r_{j})} + \sum_{j=1}^{2} \left\{ \frac{p_{j}^{2}}{Q} - \frac{2}{r_{j}} + \sum_{k=1}^{2} \frac{1}{(r_{j}^{2} - r_{k})} \right\}$$

$$= KE + V_{c} + \sum_{j=1}^{2} V_{e_{j}}^{2} + H_{T},$$

where $KE = \frac{p^2}{2 / r^2}$, is the initial kinetic energy of the system,

 $V_c = \frac{Z_1 Z_2}{R}$, is the Coulomb attraction between the projectile and the target nucleus,

 $v_{ej}^{i} = \frac{-\overline{z}_{i}}{|\vec{R} - \vec{r}_{j}|}$, is the Coulomb repulsion between the projectile and the target electrons,

and $H_T = \sum_{j=1}^{\frac{7}{2}} \left\{ \frac{p_j^2}{2} - \frac{7}{r_j} + \sum_{k \neq j}^{\frac{7}{2}} \frac{1}{|\vec{r}_j - \vec{r}_k|} \right\}$, is the Hamiltonian of the unperturbed target atom.

The perturbing potential, then, is

$$v_{i} = \frac{z_{i} z_{a}}{R} - \sum_{i=1}^{2a} \frac{z_{i}}{|\vec{R} - \vec{x}_{i}|} = v_{c} - \sum_{j=1}^{2a} v_{ej}^{i}.$$

In order that the electrons be uncorrelated, the full wave function must reduce to a product wave function. This is done by making two assumptions. First assume that the total asymptotic wave functions, initially and finally, are product wave functions. That is

and

For this to be true, correlations in the target wave function are ignored. This corresponds to the replacement of the term $\sum_{j=1}^{2n} \frac{1}{|\vec{r}_j - \vec{r}_k|} \quad \text{by an effective potential } \sum_{j=1}^{2n} V_j(r_j), \text{ so that } H_T$ is the sum of single electron terms.

The second approximation is that $\frac{\rho}{2\mu_i}$ commutes with all other terms in the full Hamiltonian, H. This treats the projectile motion classically. It also guarantees that Υ_i evolves as a product wave function because the evolution operator, $\Omega(t_1,t_2)$, 24 factors into a product of single particle terms. For example, in the Heisenberg picture, with T the time ordering operator,

$$\Omega(t, t_{2}) = \text{Texp} \left\{ -i \int_{t_{1}}^{t_{2}} H(t) dt \right\}$$

$$= \text{Texp} \left\{ -i \int_{t_{2}}^{t_{2}} \left(\frac{\partial^{2}}{\partial \mu_{i}} + V_{c}(R) + \sum_{j=1}^{2} \left(V_{e_{j}}^{2} + H_{jT} \right) \right) dt \right\}$$

$$= \text{Texp} \left\{ -i \int_{t_{1}}^{t_{2}} \left(\frac{\partial^{2}}{\partial \mu_{i}} + V_{c} \right) dt \right\} \prod_{j=1}^{2} \text{Texp} \left\{ -i \int_{t_{1}}^{t_{2}} V_{e_{j}}^{2} dt \right\}$$

$$= \Omega_{p} \left(t_{1}, t_{2} \right) \prod_{j=1}^{2} \Omega_{j} \left(t_{1}, t_{2} \right).$$

This is due to the fact that $\exp(A+B+C+...) = e^A e^B e^C...$ if and only if the commutation relations, [A,B], [B,C], [A,C] etc. are zero.

The probability amplitude, A^{if} , corresponds to the projection of the vector $\Lambda(-\infty,\infty)|Y_i\rangle$ representing the full state evolved from $|Y_i\rangle$, onto a particular final state $\langle Y_f|$. This becomes a product of single electron probability amplitudes, a^{if}_j , in the independent electron approximation provided Y_f and Y_i are orthogonal. That is

$$A^{if} = \langle \Psi_{F}(\vec{R}) \frac{1}{i!} \Phi_{F}^{f}(\vec{r}_{i}) | \Omega_{F}(---,--) | \Psi_{F}(\vec{R}) \frac{1}{i!} \Phi_{F}^{f}(\vec{r}_{i}) \rangle$$

$$= \langle \Psi_{F}(\vec{R}) | \Omega_{F} | \Psi_{F}(\vec{R}) \frac{1}{i!} \langle \Phi_{F}^{f}(\vec{r}_{i}) | \Omega_{F} | \Phi_{F}^{f}(\vec{r}_{i}) \rangle$$

$$= \int_{-\infty}^{\infty} \alpha_{F}^{f}(\vec{r}_{i}) | \Omega_{F}^{f}(\vec{r}_{i}) | \Omega_{F}^{f}(\vec{r}_{i}) | \Omega_{F}^{f}(\vec{r}_{i}) \rangle$$

$$= \int_{-\infty}^{\infty} \alpha_{F}^{f}(\vec{r}_{i}) | \Omega_{F}^{f}(\vec{r}_{i}) | \Omega_{F}^{f}(\vec{r}_{i}) | \Omega_{F}^{f}(\vec{r}_{i}) | \Omega_{F}^{f}(\vec{r}_{i}) | \Omega_{F}^{f}(\vec{r}_{i}) \rangle$$

where j = 0 corresponds to the internuclear term.

If one isolates a particular transition, s, and sums over other electron activity, the total cross section is

$$\sigma = 2\pi \int_{0}^{\pi} |a_{s}|^{2} \int_{0}^{\pi} \sum_{j \neq s} |a_{j}|^{2} |a_{j}|^{2} db$$

$$= 2\pi \int_{0}^{\pi} |a_{s}|^{2} |a_{j}|^{2} |a_{j}|^{2} db,$$

since $\sum_{\mathbf{f}} |\mathbf{a}_{\mathbf{j}}^{\mathbf{if}}|^2 = 1$, according to conservation of electron probability.

3.2 The Bates-Born Approximation.

The next step in the calculation of multi-electron capture cross sections is to find an appropriate method for calculating single electron probability amplitudes.

If one were to follow the accepted procedure for calculating the transition matrix in the wave picture and the first Born approximation, when dealing with ionization or excitation, one would choose the initial wave function to be the product of the unperturbed bound state wave function of the target and a plane wave dependent on the initial relative momentum of the system and its corresponding relative position vector. That is

$$\Psi_i = \Phi_i(\vec{r}_{ae})e^{i\vec{k}_i \cdot \vec{R}_i}$$
.

Similarly one would choose the fianl wave function of the system to be the asymptotic final wave function which is the product of the final bound state wave function and a plane wave dependent upon the final relative momentum and its corresponding relative position vector. Hence

$$\Psi_{f} = \phi_{f}(\vec{r}_{ie}) e^{i \vec{k}_{f} \cdot \vec{R}_{f}}.$$

In both Ψ_i and Ψ_f , the translational motion of the electron is neglected because it is attached to a moving nucleus. These wave functions along with V_i , when inserted into the transition matrix, should lead to cross sections for single electron capture.

Bates 11 points out, however, that if one were to add to V_i , any constant function of R, the transition matrix,

hence the cross section, would be altered. This is not acceptable since the choice of the zero point potential should not affect the outcome of the calculation. This ambiguity arises because, using the above method, one has ignored the fact that in charge capture, ϕ_1 and ϕ_f are not orthogonal. This non-orthogonality would also rule out the application of this independent electron approximation to charge transfer.

Bates accounts for the non-orthogonality of the initial and final states by expressing his full wave function as the sum of $\Psi_{\bf i}$, $\Psi_{\bf f}$ and a term, T, orthogonal to both $\varphi_{\bf i}$ and $\varphi_{\bf f}$. This is equivalent to a Gram-Schmidt orthogonalization of the initial state vector $\langle \Psi_{\bf i} |$ to the final state vector $|\Psi_{\bf f}\rangle$ at each internuclear separation $\vec{\bf R}$. That is

$$|\Psi_{\epsilon}\rangle \rightarrow |O\Psi_{\epsilon}\rangle = \frac{|\Psi_{\epsilon}\rangle - |\Psi_{\epsilon}\rangle |\Psi_{\epsilon}\rangle |\Psi_{\epsilon}\rangle}{1 - |\Psi_{\epsilon}\rangle |\Psi_{\epsilon}\rangle|^{2}}$$
.

Implicit in this expression for $|O\Psi_f\rangle$ is the neglection of all terms not involving the initial and final bound states. Backcoupling is neglected. This assumes that the amplitude of the scattered wave is much much smaller than the amplitude of the initial wave. Bates also assumes that for sufficiently high velocities the perturbation of the atomic eigen-energies, δ , is small.

Having made these assumptions, $|\Psi_f\rangle$ is replaced in the transition matrix by $|O\Psi_f\rangle$, and one obtains the result

$$T_{if} = \left\langle \Psi_i \middle| \frac{V_i - U_i}{1 - |S|^2} \middle| \Psi_f \right\rangle,$$

where

is the average interaction potential, and

$$|S|^2 = |\langle \Psi_{\epsilon} | \Psi_{\epsilon} \rangle|^2$$
.

Since $|S|^2 \ll 1$ for high velocities²⁵, it will be neglected in this calculation. The transition matrix that will be evaluated is

This approximation will be referred to as the Bates-Born version of first order perturbation theory. It is equivalent to the expression used by Bassel and Gerjuoy 10 in their plane wave limit to the distorted wave Born approximation. Note that since the effective perturbing potential is now the difference between the instantaneous and average interaction potentials, there is no longer any dependence of the transition matrix on the choice of the zero point potential.

3.3 Application to Multiple Electron Capture.

Combining the Bates-Born approximation with the independent electron approximation, one may now deal with the problem of multiple charge capture. Without them the initial and final asymptotic wave functions are not orthogonal and the evolution of the initial system does not remain an uncorrelated product of single electron wave functions. Since one expresses $|\Psi_{\pm}\rangle$ as $|O\Psi_{\pm}\rangle$, such that

all assumptions made in Section 3.1 are true and the probability amplitude does reduce to the product of single electron probability amplitudes.

$$A^{if} = \prod_{j=0}^{\frac{n}{2}} a_j^{if}.$$

Since $P_j(b) = |a_j^{if}|^2$, the probability for charge capture of the jth electron is $P_j(b)$, and the probability of not capturing the kth electron is $1 - P_k(b)$. The cross section for capture of the sth electron is

$$\sigma = 2\pi \int_{0}^{\infty} P_{s}(b) \prod_{i=1}^{\frac{3}{2}} (1-P_{j}(b))bdb.$$

As an example, let $P_1 = P_2 = P$ be the probability of the capture of a single electron from a helium atom. Then the single capture cross section is

$$\sigma_{1} = 2\pi \int_{0}^{\infty} \{P_{1}(b)(1-P_{2}(b))+P_{2}(b)(1-P_{1}(b))\} bdb$$

$$= 4\pi \int_{0}^{\infty} P(b)(1-P(b))bdb.$$

The cross section for double capture from helium is

$$\sigma_2 = 2\pi \int_{0}^{\infty} P_1(b) P_2(b) b db$$

= $2\pi \int_{0}^{\infty} P^2(b) b db$.

CHAPTER 4

CALCULATION OF SINGLE TRANSITION PROBABILITIES

In order to calculate multiple charge capture cross sections, from the ground state of the target into the ground state of the projectile in the Bates-Born and independent electron approximations, one needs to evaluate the transition matrix for single charge capture. This was shown in Section 3.2 to be

Before this can be solved, the system must be defined and some relationships developed. Assume the incident projectile has mass M_1 , charge Z_1 and incident velocity \vec{v}_1 . The target has mass M_2 and effective charge Z_2 . The electron is initially bound to the target and has mass 1 and charge 1 in accordance with atomic units.

The initial reduced mass of the system is μ_i and the final reduced mass of the system is μ_f where

$$\mu_{i} = \frac{M_{1}(M_{2}+1)}{M_{1}+M_{2}+1}$$
 and $\mu_{f} = \frac{M_{2}(M_{1}+1)}{M_{1}+M_{2}+1}.$

The reduced mass of the target initially is a. The final reduced mass of the projectile is b, where

$$a = \frac{M_1}{M_1 + 1}$$
 and $b = \frac{M_2}{M_2 + 1}$.

The coordinate system chosen to describe the interaction is

shown in Figure 1. Here \vec{R} is the vector from the projectile to the target nucleus. The coordinates from the projectile to the electron and from the target to the electron are \vec{r}_{1e} and \vec{r}_{2e} respectively. The coordinate from the center of mass of the initial target atom to the projectile is \vec{R}_{i} , and the coordinate from the center of mass of the final projectile atom to the target nucleus is \vec{R}_{f} . Then

$$\vec{R}_i = \vec{br}_{2e} - \vec{r}_{1e}$$
 and $\vec{R}_f = \vec{ar}_{1e} - \vec{r}_{2e}$.

The initial relative momentum of the system is \vec{k}_i . $\vec{k}_i = \mu_i \vec{v}_{relative}$ but $\vec{v}_{relative} = \vec{v}_i$ since initially the target nucleus is assumed stationary. The final relative momentum of the stsrem is \vec{k}_f . Let the initial and final binding energies of the system be BE_i amd BE_f respectively. Then since the energy of the system must be conserved,

$$k_f = \left\{ \mu_f \left[k_i^2 / \mu_i + 2(BE_f - BE_i) \right] \right\}^{1/2}$$

The center of mass scattering angle, θ , defined as the angle between the initial and final center of mass momenta, is the same angle as that between the initial and final relative momenta, hence, one may define θ as

$$\theta = \cos^{-1} \left\{ \frac{\vec{k}_i \cdot \vec{k}_f}{k_i k_f} \right\}.$$

A normalized hydrogenic wave function for an atom of charge Z and electron positioned a distance r from the nucleus is

$$u(r) = \left(\frac{z^3}{\pi}\right)^{1/2} e^{-zr}.$$

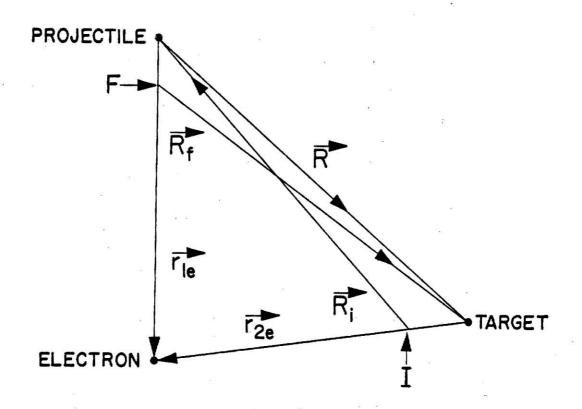


FIGURE 1.
The coordinates for charge capture.

I is the center of mass of the target and electron.

F is the center of mass of the projectile and electron.

The initial wave function of the system is then

$$\Psi_{i} = e^{i\vec{k}_{i} \cdot \vec{R}_{i}} u(r_{2e}) = \left[\frac{z_{2}^{3}}{\pi}\right]^{1/2} e^{i\vec{k}_{i} \cdot \vec{R}_{i}} e^{-z_{2}r_{2e}}.$$

The final wave function is

= IBK + IJS + IBG.

$$\Psi_{f} = e^{-i\vec{k}_{f} \cdot \vec{R}_{f}} u(r_{1e}) = \left[\frac{z_{1}^{3}}{\pi}\right]^{1/2} e^{-i\vec{k}_{f} \cdot \vec{R}_{f}} e^{-z_{1}r_{1e}} .$$

The difference between the instantaneous and average potentials in terms of the system defined above is

$$v_{i} - v_{i} = v_{i} - \int d\vec{r}_{2e} u(r_{2e}) v_{i} u(r_{2e})$$
.

This has been evaluated in Appendix 1. To order of M_2^{-1} , the resulting potential is

$$V_{i} - U_{i} = Z_{1} \left\{ \frac{1}{R} - \frac{1}{r_{1e}} - \left[\frac{1}{R} + Z_{2} \right] e^{-2Z_{2}R} \right\}$$
.

Then

$$\begin{split} & \text{T}_{\text{if}} = \int \!\! d\vec{r}_{1\text{e}} \int \!\! d\vec{r}_{2\text{e}} \, \stackrel{\text{#}}{\text{u}}(\mathbf{r}_{1\text{e}}) \, e^{i\vec{k}_{\text{f}} \cdot \vec{R}_{\text{f}}} \, (\mathbf{V}_{\text{i}} - \mathbf{U}_{\text{i}}) \, e^{i\vec{k}_{\text{i}} \cdot \vec{R}_{\text{i}}} \, \mathbf{u} \, (\mathbf{r}_{2\text{e}}) \\ & = \int \!\! d\vec{r}_{1\text{e}} \int \!\! d\vec{r}_{2\text{e}} \, \stackrel{\text{#}}{\text{u}}(\mathbf{r}_{1\text{e}}) e^{-i(\vec{k}_{\text{i}} - \vec{a}\vec{k}_{\text{f}}) \cdot \vec{r}_{1\text{e}}} (\mathbf{V}_{\text{i}} - \mathbf{U}_{\text{i}}) \mathbf{u}(\mathbf{r}_{2\text{e}}) e^{i(\vec{b}\vec{k}_{\text{i}} - \vec{k}_{\text{f}}) \cdot \vec{r}_{2\text{e}}} \\ & \text{Let } \vec{A} = \vec{k}_{\text{i}} - a\vec{k}_{\text{f}} \, \text{ and } \vec{B} = b\vec{k}_{\text{i}} - \vec{k}_{\text{f}} \, . \quad \text{Then} \\ & \\ T_{\text{if}} = \int \!\! d\vec{r}_{1\text{e}} \! \int \!\! d\vec{r}_{2\text{e}} \, \stackrel{\text{#}}{\text{u}}(\mathbf{r}_{1\text{e}}) \, e^{-i\vec{A} \cdot \vec{r}_{1\text{e}}} \, (\mathbf{V}_{\text{i}} - \mathbf{U}_{\text{i}}) \, \mathbf{u}(\mathbf{r}_{2\text{e}}) \, e^{i\vec{B} \cdot \vec{r}_{2\text{e}}} \\ & \cdot \end{split}$$

IBK is the transition matrix used by Brinkman and Kramers in their single capture cross section calculation.

IBK =
$$-Z_1 \int d\vec{r}_{1e} \int d\vec{r}_{2e} u^*(r_{1e}) e^{-i\vec{A}\cdot\vec{r}_{1e}} \frac{1}{r_{1e}} u(r_{2e}) e^{i\vec{B}\cdot\vec{r}_{2e}}$$
.

This has been evaluated by many authors^{6,23,26} and is found to be

IBK =
$$-32\pi(z_1z_2)^{5/2}(z_1^2 + A^2)^{-1}(z_2^2 + B^2)^{-2}$$
,

where $A^2 = |\vec{A}|^2$ and $B^2 = |\vec{B}|^2$. Jackson and Schiff use the sum of IBK and IJS in their transition matrix, where

IJS =
$$Z_1 \int d\vec{r}_{1e} \int d\vec{r}_{2e} u^*(r_{1e}) e^{-i\vec{A}\cdot\vec{r}_{1e}} \frac{1}{R} u(r_{2e}) e^{i\vec{B}\cdot\vec{r}_{2e}}$$

The transition matrix used in the approximation of Bassel and Gerjuoy is the sum of IBK, IJS and IBG, where

IBG =
$$-z_1 \int d\vec{r}_{1e} \int d\vec{r}_{2e} \vec{u}(r_{1e}) e^{-\vec{A} \cdot \vec{r}_{1e}} \left[\frac{1}{R} + z_2 \right] e^{-2z_2 R} u(r_{2e}) e^{i\vec{B} \cdot \vec{r}_{2e}}$$

IBG and IJS will be evaluated in Appendix 2. Due to the complexity of their results, they will not be repeated in the text of this thesis.

CHAPTER 5

RESULTS

Since the calculation of double electron capture cross sections, in the independent electron approximation used, is explicitly dependent on the scattering amplitudes used when calculating single capture cross sections, it is imperative that one verify that these amplitudes are correct. Hence, the first calculation made was an attempt to reproduce the differential cross sections computed by Bassel and Gerjuoy for single capture from hydrogen into protons incident at an energy of 25 KeV. Agreement would guarantee the correct expressions for IBK, IJS and IBG, except for the charge dependence. One could then assume the algebra that is included in Appendix 2 but omitted from the Bassel and Gerjuoy paper is accurate. The computer program used in the calculation is presented in Appendix 4. The comparison to the results of Bassel and Gerjuoy is shown in Figure 2.

Unfortunately, the comparison was not successful. The differential cross sections for the Jackson and Schiff approximation is identical to present results. The Bassel and Gerjuoy curve, however, differs appreciably as Λ increases. The algebra has been rechecked a number of times, and the computer program has been carefully reexamined. The final conclusion reached is that the results presented by Bassel and Gerjuoy differ from present results.

Luckily, the discrepancies in the angular distributions do not affect the total cross sections appreciably. This

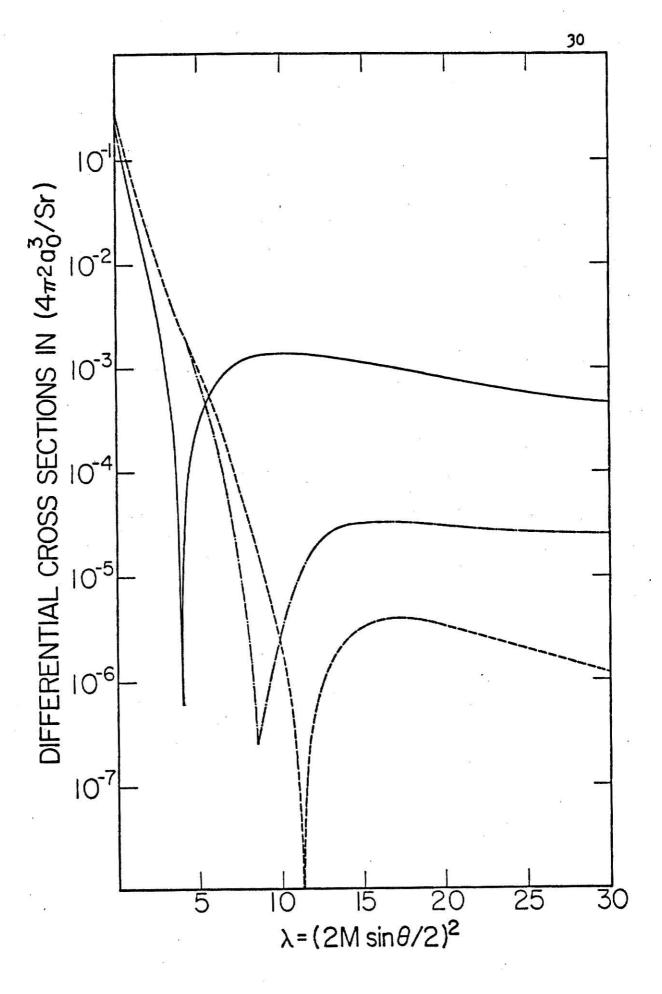
FIGURE 2

Differential electron capture cross sections for protons on hydrogen at 25 KeV.

- in the Jackson and Schiff approximation.

 -----, present calculation in the Bassel and
- -----. Bassel and Gerjuoy calculation in the Bassel and Gerjuoy approximation.

Gerjuoy approximation.



is due to the fact that the error occurs after the differential cross section has fallen off more than two orders of magnitude. This causes error of less than one per cent in their total cross section calculation. This can be seen in Figure 3. Here the total cross sections for 25 KeV protons incident on hydrogen are presented for the Brinkman and Kramers, the Jackson and Schiff and the Bassel and Gerjuoy approximations as calculated by both the author and by Bassel and Gerjuoy. Only three curves are shown because these results are identical to one another.

After a careful check of the charge dependence of the transition matrix, single charge capture cross sections were computed for the capture of electrons from the ground state of helium to the ground state of alpha particles. This calculation was made for incident energies from 0 to 1,000 KeV. The masses used are $M_1 = M_2 = 7344.0$, which is four times the mass of a proton in atomic units. The charge on the projectile is $Z_1 = 2.0$. The effective charge on the target due to screening of the nucleus by the electrons present is $Z_2 = 1.618$. The initial and final binding energies used are the ionization energies for a helium atom, 24.587, and for He^+ , 54.4, respectively.

These resulting cross sections are presented in Figure 4 where they are compared to the experimental results compiled by Barnett et. al. 14 for capture to all energy levels. At high velocities, when the projectile electron velocity is much greater than the velocity of the orbiting electron, the capture cross sections are inversely proportional to n³

FIGURE 3

Total single capture cross sections for protons on hydrogen.

	Brinkman and Kramers approximation.
,	Jackson and Schiff approximation.
-,	Bassel and Gerjuoy approximation.

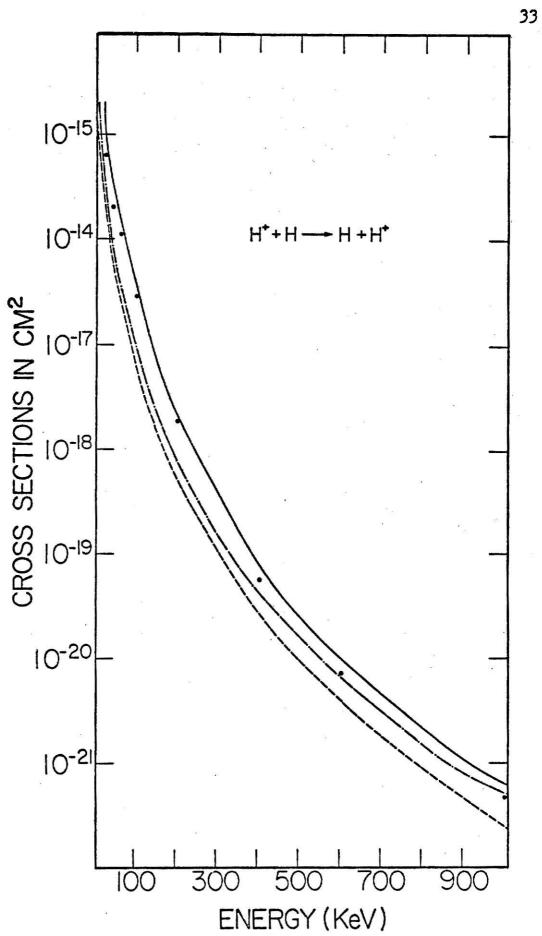
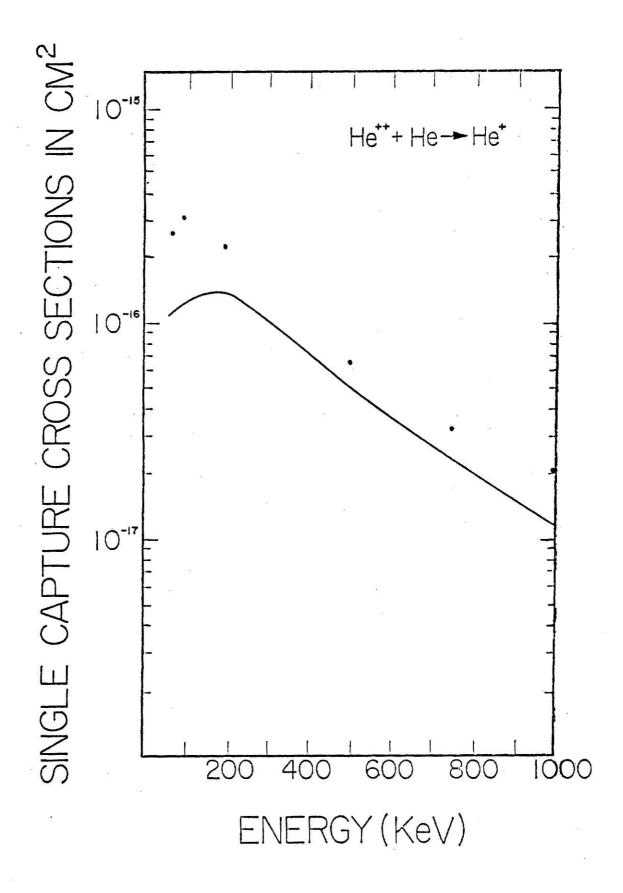


FIGURE 4

Total single electron capture cross sections from helium atoms by alpha particle projectiles.

- , Experimental data of Barnett et. al.
- -----, Theoretical results from present calculation.



where n is the principle quantum number. ²⁶ Then one expects that twenty per cent of the experimental result is due to capture into higher energy levels. Multiplying the present result by 1.2 would result in excellent agreement with experiment for higher energies.

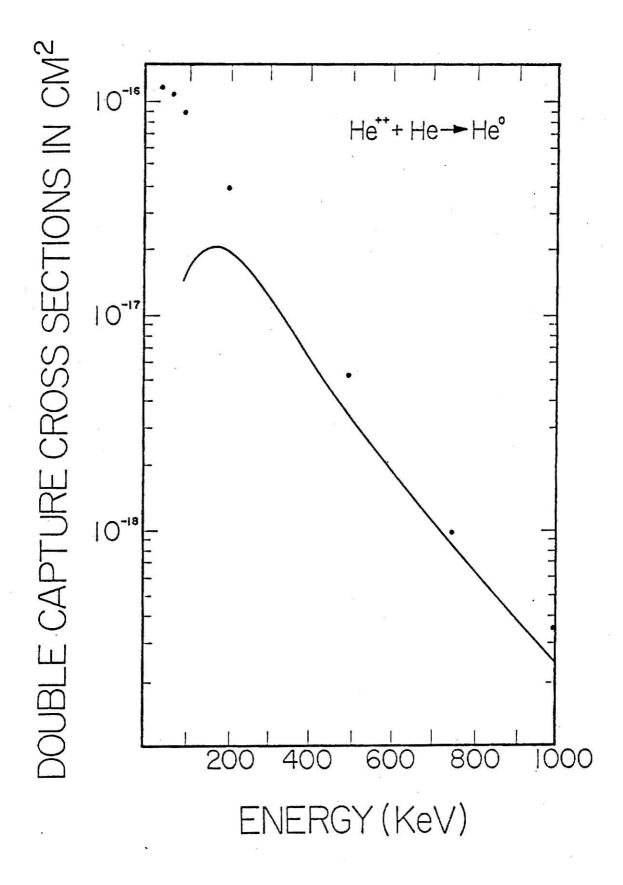
For smaller incident energies the comparison becomes less and less agreeable. This is expected for any number of reasons. First the percentage of higher level transitions increases. The significance of the omitted backcoupling and $|S|^2$ term becomes larger and larger as the energy decreases. Finally, there is persuasive evidence that the second order Born calculation becomes appreciable and may even dominate as the energy becomes small. 28,29

The computer program used to compute both the single and double capture cross sections is presented in Appendix 3. The square of the probability amplitude for single capture is the basis for double capture in accordance with the independent electron approximation. The results of this calculation, in which the same parameters were used, is shown in Figure 5. The experimental data to which it is compared is also a composit by Barnett et. al. 14 A comparison shows the theoretical calculation falls farther below the data than for the case of single capture. This is expected since the percentage of higher level transitions is twice as large for this case. That is only 60% of the total transitions are attributed to 1s to 1s capture. Also some disagreement may be due to the use of the single capture binding energy. This corresponds to the assumption that the collision process

FIGURE 5

Total double electron capture cross sections from helium atoms by alpha particle projectiles.

- , Experimental data of Barnett et. al.
- ______, Theoretical results from present calculation.



occurs too quickly to allow the target atom to readjust after the first electron has been captured.

Then the agreement with experiment achieved for the double charge capture process does follow the same pattern as that for single capture. It is good at high energies and falls farther below the data as the energy decreases.

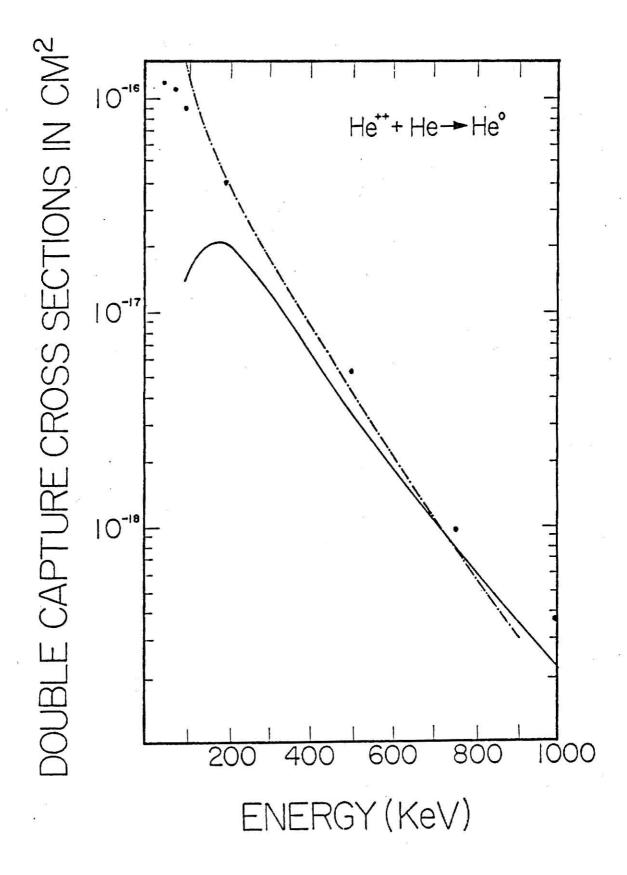
One may then conclude that the independent electron approximation used is a valid one.

Several calculations have been made for K-shell to K-shell capture for this system using the close-coupling technique. The results of one approximation using three state, two center atomic expansion are compared to the present results in Figure 6. Here it can be seen that agreement with experiment is comparable or even better than the close-coupling calculation at energies above 600 KeV, but worse for low energies. This is attributed to an inadequacy in the single capture calculation rather than the breakdown of the independent electron approximation.

FIGURE 6

Total double electron capture cross sections from helium atoms by alpha particles.

- , Experimental data of Barnett et. al.
- _____, Theoretical results from present calculation.
- -----, Theoretical results from Lin.



CHAPTER 6

CONCLUSION

The independent electron approximation of McGuire and Weaver has been tested for double charge capture from the ground state of a helium atom into the ground state of an alpha particle of high incident energy. The difference between the instantaneous and the average interaction potential was used as the perturbing potential as in the approximation of Bates. The wave functions used were those dictated by the first Born approximation.

The resulting cross sections for double capture were compared to experimental results and the discrepancies were noted. These differences turned out to follow the same trend as the comparison made for single capture. This led to the conclusion that the discrepancies were due to the weaknesses in the probability amplitude computed. Then the independent electron approximation has passed the test and has been deemed a worthwhile approximation to use when dealing with the complicated reaction of multiple charge transfer.

Since it has proven to be worthwhile, a thorough investigation into the limitations of the approximation would be advantageous. For example, the comutator terms that were neglected could be evaluated to see if they are truly as small as rough estimates indicate. The choice of

the effective inter-electron interaction potential could be investigated to see if there is a better way of expressing it than the one used.

The applications of the approximation are numerous.

Cross sections for higher target and projectile charge states are a minor perturbation of the calculation already done.

Capture of more than two electrons is obtainable. Capture into higher energy levels could be computed as well for multiple charge transfer. Computations could be made combining multiple charge capture and multiple ionization cross sections. The second Born terms could be computed for multiple charge transfer as well.

These calculations among others are now conceivable in a simple way since this independent electron approximation has been shown to give results that are in reasonable agreement with experiment and with theoretical results that are much more complicated to compute.

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APPENDIX 1

THE DIFFERENCE BETWEEN THE INSTANTANEOUS AND AVERAGE POTENTIALS

In order to arrive at the form of the Bates potential used in this calculation, the exact form of the interaction potential is evaluated here. The result is then approximated to order M_2^{-1} , where M_2 is the target mass, in order that its use may be facilitated.

$$\begin{aligned} v_{i} &= \frac{z_{1}z_{2}}{R} - \frac{z_{1}}{r_{1e}} \,. \\ v_{i} &= \left\langle u(r_{2e}) \mid v_{i} \mid u(r_{2e}) \right\rangle \\ &= \left\langle u(r_{2e}) \middle| - \frac{z_{1}}{r_{1e}} \middle| u(r_{2e}) \right\rangle + \left\langle u(r_{2e}) \middle| \frac{z_{1}z_{2}}{R} \middle| u(r_{2e}) \right\rangle \\ &= v_{i1} + v_{i2} \,. \end{aligned}$$

$$u(r_{2e}) &= \left(\frac{z_{2}^{3}}{\pi} \right)^{1/2} e^{-z_{2}r_{2e}} \,. \end{aligned}$$

Generally, using a standard expansion in terms of Spherical Harmonics, $Y_{lm}(\theta,\phi)$,

$$|\vec{r} - \vec{R}|^{-1} = \sum_{l,m} \frac{\mu_{lm}}{2l+1} \frac{r_c^{l}}{r_c^{l+1}} Y_{lm}^{*}(\theta', \phi') Y_{lm}(\theta, \phi).$$

where r is the lesser of r and R and r, is the greater of r and R.

Since only 1s to 1s transitions are of concern, 1 = m = 0, and $Y_{00}(\theta, \phi) = 1/\sqrt{4\pi}$,

$$|\vec{r} - \vec{R}|^{-1} = \frac{\mu_{\pi}}{r_{3}} Y_{00}^{*}(\theta', \phi') Y_{00}(\theta, \phi) = \frac{1}{r_{3}}$$

Then specifically, $|\vec{r}_{1e}|^{-1} = |\vec{R}_i - b\vec{r}_{2e}|^{-1} = 1/r$, where $b = M_2/(M_2 + 1)$ and r, is the greater of R and br_{2e} . Then

$$U_{11} = -Z_1 \iiint_{0}^{2\pi} \frac{r_{2e}^2}{r_{1}} \left(\frac{Z_2^3}{\pi}\right) e^{-2Z_2 r_{2e}} dr_{2e} d(\cos \theta) d\phi$$

$$= -4Z_1 Z_2^3 \iint_{0}^{2\pi} \frac{r_{2e}^2}{r_{1}} e^{-2Z_2 r_{2e}} dr_{2e}.$$

where

or

Let $2Z_2r_{2e} = x$. Then

$$r_{2e} = \frac{x}{2Z_2}$$
, $dr_{2e} = \frac{dx}{2Z_2}$

and

$$x_i = R_i \text{ if } \frac{bx}{2Z_2} < R_i \text{ or } x_i = \frac{bx}{2Z_2} \text{ if } \frac{bx}{2Z_2} > R_i$$
.

Then

$$U_{i} = -4Z_{1}Z_{2}^{3} \int_{a}^{\infty} (\frac{1}{2Z_{2}})^{2} \frac{x^{2}}{x_{2}} e^{-x} (\frac{1}{2Z_{2}}) dx$$

$$= -\frac{Z_{1}}{2} \left\{ \int_{a}^{(\frac{2Z_{2}}{b})^{2}} \frac{x^{2}}{R_{i}} e^{-x} dx + \int_{(\frac{2Z_{2}}{b})^{2}}^{\infty} \frac{2Z_{2}}{b} xe^{-x} dx \right\}$$

$$= -Z_{1} \left\{ \frac{1}{R_{i}} - e^{-(2Z_{2}R_{i})/b} \left(\frac{Z_{2}}{b} + \frac{1}{R_{i}} \right) \right\}.$$

Similarly $|\vec{R}|^{-1} = |\vec{R}_1 + gr_{2e}|^{-1} = 1/r$, where $g = 1/(M_2 + 1)$ and r, is the greater of R and gr_{2e} .

Then
$$U_{12} = Z_1 Z_2 \iiint_{0.10}^{2\pi} \frac{r_{2e}^2}{r_{2e}} \left(\frac{Z_2^3}{\pi}\right) e^{-2Z_2 r_{2e}} dr_{2e} d(\cos \theta) d\phi$$

$$= 4Z_1 Z_2 4 \int_{0.10}^{\infty} \frac{r_{2e}^2}{r_{2e}^2} e^{-2Z_2 r_{2e}} dr_{2e}$$

This is the same integral as evaluated in U_{i1} except for the constant $-Z_2$, and now

$$r_i = R_i \text{ if } gr_{2e} \langle R_i \text{ or } r_i = gr_{2e} \text{ if } gr_{2e} \rangle R_i$$
.

So that with b replaced by g,

$$U_{i2} = Z_1 Z_2 \left\{ \frac{1}{R_i} - e^{-(2Z_2 R_i)/g} \left(\frac{1}{R_i} + \frac{Z_2}{g} \right) \right\}$$

Then the average interaction potential is

$$v_i = v_{i1} + v_{i2}$$

$$= z_1 z_2 \left\{ \frac{1}{R_i} - e^{-2z_2(M_2+1)R_i} \left(\frac{1}{R_i} + z_2(M_2+1) \right) \right\}$$

$$-z_1 \left\{ \frac{1}{R_i} - e^{-2z_2R_i(M_2+1)/M_2} \left(\frac{1}{R_i} + \frac{z_2(M_2+1)}{M_2} \right) \right\}.$$

Now, since $M_2 \gg 1$, the exponential, $\exp\left[-Z_2(M_2+1)R_1\right]$ is very small and the term containing it may be neglected altogether from the expression for U_1 . To order of M_2^{-1} , the quantity $(M_2+1)/M_2$ is approximately equal to one. For large M_2 , R_1 is approximately equal to R. With these three approximates all on the order of M_2^{-1} included, the expression for U_1 becomes

$$U_{i} = \frac{Z_{1}Z_{2}}{R} - \frac{Z_{1}}{R} + Z_{1} e^{-2Z_{2}R} \left[\frac{1}{R} + Z_{2} \right].$$

Then the instantaneous minus the average potential is

$$\begin{aligned} \mathbf{v_{i}} - \mathbf{u_{i}} &= \frac{\mathbf{z_{1}} \mathbf{z_{2}}}{\mathbf{R}} - \frac{\mathbf{z_{1}}}{\mathbf{r_{1e}}} - \frac{\mathbf{z_{1}} \mathbf{z_{2}}}{\mathbf{R}} + \frac{\mathbf{z_{1}}}{\mathbf{R}} - \mathbf{z_{1}} e^{-2\mathbf{z_{2}}\mathbf{R}} \left(\frac{1}{\mathbf{R}} + \mathbf{z_{2}} \right) \\ &= \mathbf{z_{1}} \left\{ \frac{1}{\mathbf{R}} - \frac{1}{\mathbf{r_{1e}}} - e^{-2\mathbf{z_{2}}\mathbf{R}} \left(\frac{1}{\mathbf{R}} + \mathbf{z_{2}} \right) \right\}. \end{aligned}$$

This is indeed the potential given as the Bates potential in Chapter 3.

APPENDIX 2

CALCULATION OF THE PIECES OF THE TRANSITION MATRIX CALLED IJS AND IBG

In this appendix the integral forms of IJS and IBG will be reduced to closed form expressions. In their integral form they are

IJS =
$$Z_1 \int d\vec{r}_{1e} \int d\vec{r}_{2e} u^*(r_{1e}) e^{-i\vec{A}\cdot\vec{r}_{1e}} \frac{1}{R} u(r_{2e}) e^{+i\vec{B}\cdot\vec{r}_{2e}}$$

and

$$IBG = -Z_1 \int_{\vec{r}_{1e}} \vec{r}_{1e} \int_{\vec{r}_{2e}} \vec{u}(\vec{r}_{1e}) e^{-i\vec{A}\cdot\vec{r}_{1e}} \left(\frac{1}{R} + Z_2\right) e^{-2Z_2R} u(\vec{r}_{2e}) e^{i\vec{B}\cdot\vec{r}_{2e}}.$$

Note that

$$\left(\frac{1}{R} + Z_2\right) e^{-2Z_2R} = \left(1 - Z_2 \frac{\partial}{\partial(2Z_2)}\right) \frac{1}{R} e^{-2Z_2R}$$

Let $2Z_2 = y$. Then

$$IBG = -Z_1 \left(1 - Z_2 \frac{\partial}{\partial y}\right) \int_{d\mathbf{r}_{1e}}^{+} \int_{d\mathbf{r}_{2e}}^{+} \frac{\pi}{u(\mathbf{r}_{1e})} e^{-i\mathbf{A}\cdot\mathbf{r}_{1e}} \frac{1}{\mathbf{R}} e^{-y\mathbf{R}} u(\mathbf{r}_{2e}) e^{i\mathbf{B}\cdot\mathbf{r}_{2e}}$$

and IJS is a special case of IBG. That is

$$IJS = \lim_{y \to 0} -IBG.$$

Hence evaluation of the integral

$$I = \int d\vec{r}_{1e} \int d\vec{r}_{2e} \ u^{*}(r_{1e}) \ e^{-i\vec{A}\cdot\vec{r}_{1e}} \frac{1}{R} \ e^{-yR} \ u(r_{2e}) \ e^{i\vec{B}\cdot\vec{r}_{2e}}$$

gives both closed form expressions sought.

The Fourier transform of e^{-yR}/R is 30

$$F\left(\frac{e^{-yR}}{R}\right) = \frac{1}{2\pi^2} \int d\vec{p} \ (p^2 + y^2)^{-1} \ e^{i\vec{p}\cdot\vec{R}}$$

$$= \frac{1}{2\pi^2} \int d\vec{p} \ (p^2 + y^2)^{-1} \ e^{i\vec{p}\cdot\vec{r}} 2e \ e^{-i\vec{p}\cdot\vec{r}} 1e$$

since $\vec{R} = \vec{r}_{2e} - \vec{r}_{1e}$. Then

$$I = \frac{1}{2\pi^2} \int_{\vec{q}} d\vec{p} (p^2 + y^2)^{-1} \int_{\vec{q}} d\vec{r}_{1e} u(r_{1e}) e^{-i(\vec{A} + \vec{p}) \cdot \vec{r}_{1e}} \int_{\vec{q}} d\vec{r}_{2e} u(r_{2e}) e^{i(\vec{B} + \vec{p}) \cdot \vec{r}_{2e}}$$

The Fourier transform of the wave function u(r) is

$$\phi_o(\vec{K}) = \int e^{i\vec{K}\cdot\vec{r}} u(r)d\vec{r}.$$

For a ground state hydrogenic bound state wave function of charge z, 7

$$\phi_0(\vec{K}) = 8 \pi^{1/2} z^{5/2} \left[z^2 + K^2 \right]^{-2}$$

so that

$$I = \frac{1}{2\pi^2} \int d\vec{p} (p^2 + y^2)^{-1} \phi_0^* (\vec{A} + \vec{p}) \phi_0 (\vec{B} + \vec{p})$$

$$= \frac{32}{\pi} (z_1 z_2)^{5/2} \int_{\mathbf{dp}}^{3} (p^2 + y^2)^{-1} \left[z_1^2 + (A+p)^2 \right]^{-2} \left[z_2^2 + (B+p)^2 \right]^{-2}.$$

Let $a = Z_1$, $b = Z_2$ and recall $y = 2Z_2$. Then

$$I = \frac{8}{\pi} (Z_1 Z_2)^{5/2} \frac{1}{ab} \frac{\partial}{\partial a} \frac{\partial}{\partial b} \int dp^{2} \left\{ (p^{2} + y^{2}) \left[a^{2} + (A+p)^{2} \right] \left[b^{2} + (B+p)^{2} \right] \right\}^{-1}.$$

The integral

$$I' = \int d\vec{p} \left\{ (p^2 + y^2) \left[a^2 + (A+p)^2 \right] \left[b^2 + (B+p)^2 \right] \right\} -1$$
has been evaluated by Lewis³¹ to be

$$I' = \pi^{2} (\beta - \alpha \delta)^{-1/2} \ln \left\{ \frac{\beta + (\beta^{2} - \alpha \delta)^{1/2}}{\beta - (\beta^{2} - \alpha \delta)^{1/2}} \right\},$$

where

$$\alpha = [(A-B)^2 + (a+b)^2][(a+y)^2 + A^2][(b+y)^2 + B^2]$$

and

$$\beta = y[(A-B)^2 + (a+b)^2] + b(A^2+a^2+y^2) + a(B^2+b^2+y^2).$$

For the calculation of interest, $\mbox{\ensuremath{\mbox{\ensuremath}\ensuremath{\mbox{\ensuremath{\mbox{\ensuremath{\mbox{\ensuremath}\ensuremath{\mbox{\ensuremath}\$

$$\begin{split} \text{I}' &= \mathrm{i} \pi^2 (\alpha x - \beta^2)^{-1/2} \text{ In } \frac{1 + \frac{\mathrm{i}}{\beta} (\alpha x - \beta^2)^{1/2}}{1 - \frac{\mathrm{i}}{\beta} (\alpha x - \beta^2)^{1/2}} \quad . \end{split}$$
 Let $x = \frac{1}{\beta} (\alpha x - \beta^2)^{1/2}$.

$$I = \frac{i \pi^2}{x} \ln \left\{ \frac{1+ix}{1-ix} \right\}.$$

Using the identities 32

$$tanh^{-1}(ix) = -itan^{-1}(x)$$

and

$$\tanh^{-1}(ix) = \frac{1}{2} \ln \left\{ \frac{1+ix}{1-ix} \right\},$$

$$\ln \left\{ \frac{1+ix}{1-ix} \right\} = -2i \tan^{-1}(x).$$

Then

$$I' = \frac{i\pi^2}{x} (-2i\tan^{-1}(x))$$

$$= \frac{2\pi^2}{x} \tan^{-1}(x)$$

$$= 2\pi^2 (\lambda x - \beta^2)^{-1/2} \tan^{-1} \left\{ \frac{(\lambda x - \beta^2)^{1/2}}{\beta} \right\}.$$

and
$$I = 16\pi (z, z_a)^{5/2} \frac{1}{ab} \frac{3}{3a} \frac{3}{3b} (a8 - \beta^2)^{-1/2} tan^{-1} \left(\frac{(a8 - \beta^2)^{-1/2}}{\beta} \right)$$
.

Let
$$t = dN - \beta^2$$
 and $\xi = \tan^{-1}(t^{\frac{1}{2}}/\beta)$

Then

$$\frac{\partial}{\partial a} \frac{\partial}{\partial b} \left(t^{-\frac{1}{2}} \overline{Z} \right) = \frac{\partial}{\partial a} t^{-\frac{1}{2}} \frac{\partial}{\partial b} \overline{Z} + t^{-\frac{1}{2}} \frac{\partial^2 \overline{Z}}{\partial a \partial b} + \frac{\partial \overline{Z}}{\partial a} \frac{\partial t^{-\frac{1}{2}}}{\partial b} + \frac{\partial^2}{\partial a \partial b} t^{-\frac{1}{2}}.$$

$$= -\frac{1}{2} t^{-\frac{1}{2} a} \frac{\partial t}{\partial a} \frac{\partial \overline{Z}}{\partial b} + t^{-\frac{1}{2}} \frac{\partial^2 \overline{Z}}{\partial a \partial b} - \frac{1}{2} t^{-\frac{1}{2}} \frac{\partial \overline{Z}}{\partial a} \frac{\partial t}{\partial b} + \frac{\partial^2}{\partial a \partial b} t^{-\frac{1}{2}}.$$

$$\frac{\partial z}{\partial \alpha} = \frac{(1 + t/\beta^{2})^{-1} \left[\frac{t^{-1/2}}{2\beta} \frac{\partial t}{\partial \alpha} - \frac{t}{\beta^{2}} \frac{\partial \beta}{\partial \alpha} \right]}{\frac{\partial^{2}}{\partial \alpha^{2} + \alpha x^{2} - \beta^{2}} \left[\frac{1}{2\beta t^{2}} \frac{\partial t}{\partial \alpha} - \frac{t}{t^{2}} \frac{\partial \beta}{\partial \alpha} - \frac{t^{2}}{\beta^{2}} \frac{\partial \beta}{\partial \alpha} \right]}$$

$$= \frac{\beta^{2}}{\alpha^{2}} \left[\frac{1}{2\beta t^{2}} \frac{\partial t}{\partial \alpha} - \frac{1}{t^{2}} \frac{\partial \beta}{\partial \alpha} - \frac{t^{2}}{\beta^{2}} \frac{\partial \beta}{\partial \alpha} \right]$$

$$= \frac{\beta^{2}}{\alpha^{2}} \left[\frac{1}{2\beta t^{2}} \frac{\partial t}{\partial \alpha} - \frac{1}{t^{2}} \frac{\partial \beta}{\partial \alpha} - \frac{t^{2}}{\beta^{2}} \frac{\partial \beta}{\partial \alpha} \right]$$

$$= \frac{\beta}{\alpha^{2}} \frac{\partial t}{\partial \alpha^{2}} - \frac{\partial t}{\alpha^{2}} \frac{\partial \beta}{\partial \alpha} - \frac{t^{2}}{\alpha^{2}} \frac{\partial \beta}{\partial \alpha} - \frac{t^{2}}{\alpha^{2}} \frac{\partial \beta}{\partial \alpha} \right]$$

$$= \frac{\beta}{\alpha^{2}} \frac{\partial t}{\partial \alpha^{2}} - \frac{\partial t}{\partial \alpha^{2}} \frac{\partial \beta}{\partial \alpha^{2}} - \frac{t^{2}}{\alpha^{2}} \frac{\partial \beta}{\partial \alpha} - \frac{t^{2}}{\alpha^{2}} \frac{\partial \beta}{\partial \alpha} \right]$$

$$= \frac{\beta^{2}}{\alpha^{2}} \frac{\partial t}{\partial \alpha^{2}} - \frac{\beta^{2}}{\alpha^{2}} \frac{\partial \beta}{\partial \alpha^{2}} - \frac{t^{2}}{\alpha^{2}} \frac{\partial \beta}{\partial \alpha^{2}} - \frac{t^{2}}{\alpha^{2}} \frac{\partial \beta}{\partial \alpha^{2}}$$

$$= \frac{\beta^{2}}{\alpha^{2}} \frac{\partial t}{\partial \alpha^{2}} - \frac{\beta^{2}}{\alpha^{2}} \frac{\partial \beta}{\partial \alpha^{2}} - \frac{t^{2}}{\alpha^{2}} \frac{\partial$$

$$+ \frac{3b}{3b} \left[-\frac{2b}{4b^{2}} \frac{3b}{3b} + \frac{2b}{8a^{2}} \frac{3b}{3ab} + \frac{1}{4b^{2}} \frac{3b}{3a} \right] + \frac{2a}{4b^{2}} \frac{3b}{3a} - \frac{1}{4b^{2}} \frac{3b}{3a}$$

$$+ \frac{3b}{3b} \left[\frac{1}{4b^{2}} \frac{3b}{3a} + \frac{2b}{8a^{2}} \frac{3b}{3a} + \frac{2b}{4b^{2}} \frac{3b}{3a} + \frac{2b}{4b^{2}} \frac{3b}{3a} \right] + \frac{2b}{4b^{2}} \frac{3b}{3a} - \frac{2b}{4b^{2}} \frac{3b}{3a}$$

$$+ \frac{3b}{3b} \left[\frac{1}{4a^{2}} \frac{3b}{3a} + \frac{1}{4b^{2}} \frac{3a}{3a} - \frac{2b}{4b^{2}} \frac{3b}{3a} + \frac{2a}{4b^{2}} \frac{3b}{3a} \right] + \frac{2a}{4b^{2}} \frac{3a}{3a} \left(\frac{3b}{3b} \right)$$

$$+ \frac{3b}{3b} \left[\frac{1}{4a^{2}} \frac{3b}{3a} + \frac{1}{4b^{2}} \frac{3a}{3a} + \frac{2a}{4b^{2}} \frac{3b}{3a} \right] + \frac{a}{4b^{2}} \frac{3a}{3a} \left(\frac{3b}{3b} \right) - \frac{a}{4b^{2}} \frac{3a}{3a} \left(\frac{3b}{3b} \right)$$

$$+ \frac{3b}{3b} \left[-\frac{1}{4b^{2}} \frac{3b}{3a} + \frac{2a}{4b^{2}} \frac{3a}{3a} + \frac{2a}{4b^{2}} \frac{3b}{3a} \right] + \frac{a}{4b^{2}} \frac{3a}{3a} \left(\frac{3b}{3b} \right) - \frac{a}{4b^{2}} \frac{3a}{3a} \left(\frac{3b}{3b} \right)$$

$$+ \frac{3b}{3b} \left[-\frac{1}{4b^{2}} \frac{3b}{3a} + \frac{2a}{4b^{2}} \frac{3a}{3a} + \frac{a}{4b^{2}} \frac{3b}{3a} \right] + \frac{a}{4b^{2}} \frac{3a}{3a} \frac{3b}{3a}$$

$$= \frac{2}{30} \left(\frac{34x}{36x} \right) \left[-\frac{2}{2t^{3/2}} + \frac{3}{24xt} \right] + \frac{2}{30} \left(\frac{38}{36} \right) \left[\frac{82}{t^{3/2}} - \frac{6^2}{48t} - \frac{1}{4x} \right] + \frac{1}{4x^2} \frac{34x}{3a} \frac{38}{3a} \frac{38}{3b}$$

$$+ \frac{34x}{3b} \left[-\frac{1}{44x^2} + \frac{3}{2a} + \frac{3}{24x^2} + \frac{3}{2a} +$$

$$= \frac{3}{3a} \left(\frac{38}{3b} \right) \left[-\frac{1}{4b} - \frac{8^{2}}{4b^{2}} + \frac{62}{t^{3/2}} \right] + \frac{3}{3a} \left(\frac{34b}{3b} \right) \left[\frac{8}{24b^{2}} - \frac{2}{2t^{3/2}} \right]$$

$$+ \frac{38}{3a} \frac{38}{3b} \left[-\frac{38^{3}}{4b^{2}t^{2}} - \frac{38}{4b^{2}t} + \frac{38^{2}}{t^{3/2}} + \frac{7}{t^{3/2}} \right]$$

$$+ \frac{34b}{3a} \frac{34b}{3b} \left[-\frac{38}{4b^{2}t^{2}} - \frac{8}{24b^{2}t} + \frac{32}{4t^{5/2}} \right]$$

$$+ \frac{34b}{3a} \frac{36}{3b} \left[\frac{1}{4b^{2}t^{2}} + \frac{8^{2}}{4b^{2}t} + \frac{38^{2}}{4t^{5/2}} - \frac{362}{4t^{5/2}} \right]$$

$$+ \frac{34b}{3a} \frac{36}{3b} \left[\frac{1}{4b^{2}t^{2}} + \frac{8^{2}}{4b^{2}t} + \frac{38^{2}}{4b^{2}t^{2}} - \frac{362}{4t^{5/2}} \right]$$

Since they will be used repeatedly, the following quantities will be represented by symbols:

$$rp = -\frac{1}{a^{3}} - \frac{\beta^{2}}{a^{3}t} + \frac{\beta^{2}}{t^{2}a^{2}},$$

$$ap = \frac{\beta}{2a^{3}t} - \frac{2}{2t^{2}a},$$

$$gp = -\frac{3\beta^{3}}{a^{3}t^{2}} - \frac{3\beta}{a^{3}t} + \frac{3\beta^{2}}{t^{2}5a^{2}} + \frac{2}{t^{2}a^{2}},$$

$$pp = -\frac{3\beta}{4a^{3}t^{2}} - \frac{\beta}{2a^{3}t^{2}} + \frac{32}{4t^{2}5a^{2}},$$

$$op = \frac{3\beta^{2}}{2a^{3}t^{2}} + \frac{1}{a^{3}t} - \frac{3\beta^{2}}{2t^{2}a^{2}}$$

and bp =
$$\frac{1}{dy^2} + \frac{8^2}{dy^2t} + \frac{38^2}{2dyt^2} - \frac{382}{2t^{5/2}}$$
.

Note that
$$\frac{1}{dx^2} + \frac{R^2}{dx^2t} = \frac{t+R^2}{dx^2t} = \frac{dx^2+R^2}{dx^2t} = \frac{dx}{dx^2t} = \frac{1}{dx^2t}$$
, so that bp = op, and

$$I = 16 \pi (Z_1 Z_2)^{5/2} \frac{1}{ab} \left\{ \frac{\partial}{\partial a} \left(\frac{\partial \beta}{\partial b} \right) (rp) + \frac{\partial}{\partial a} \left(\frac{\partial \kappa k}{\partial b} \right) (ap) + \frac{\partial \beta}{\partial a} \frac{\partial \beta}{\partial b} (gp) + \frac{\partial \kappa k}{\partial a} \frac{\partial \kappa k}{\partial b} (pp) + \left(\frac{\partial \kappa k}{\partial a} \frac{\partial \beta}{\partial b} + \frac{\partial \kappa k}{\partial b} \frac{\partial \beta}{\partial a} \right) (op) \right\}.$$

Here the calculations of IJS and IBG must part company, since the definitions of $\alpha \%$ and β are different in the two cases. The term IJS will be completed first. It has the same form as I above except that the expressions for $\alpha \%$ and β are in the limit where y=0. That is

$$d\delta' = \left[(A^{-B})^{2} + (a+b)^{2} \right] \left[A^{2} + a^{2} \right] \left[B^{2} + b^{2} \right]$$
 and
$$\beta' = b(A^{2} + a^{2}) + a(B^{2} + b^{2}) .$$

The partial derivatives of these with respect to a and b needed for the equation for I are:

$$\frac{\partial X'}{\partial a} = 2a \left[(\vec{A} - \vec{B})^2 + (a + b)^2 \right] \left[B^2 + b^2 \right] + 2(a + b) \left[A^2 + a^2 \right] \left[B^2 + b^2 \right]$$

$$\frac{\partial X'}{\partial b} = 2b \left[(A - B)^2 + (a + b)^2 \right] \left[A^2 + a^2 \right] + 2(a + b) \left[A^2 + a^2 \right] \left[B^2 + b^2 \right]$$

$$\frac{\partial B'}{\partial a} = 2ab + B^2 + b^2$$

$$\frac{\partial 8'}{\partial b} = 2ab + A^2 + a^2$$

$$\frac{\partial}{\partial a} \left(\frac{\partial \beta}{\partial b} \right) = 2(a+b)$$

$$\frac{\partial}{\partial a} \left(\frac{\partial a x}{\partial b} \right) = 4ab \left[(\mathring{A} - \mathring{B})^2 + (a+b)^2 \right] + 4b(a+b) \left[A^2 + a^2 \right] + 4a(a+b) \left[B^2 + b^2 \right].$$

Also for the term IJS, with

$$t' = ax' - \beta'^{2} \quad \text{and} \quad Z' = \tan^{-1} \left(t'^{2} / \beta' \right)_{1}$$

$$rp' = -\frac{1}{ax'} - \frac{g'^{2}}{ax''t'} + \frac{g'^{2}}{t'^{6/2}},$$

$$ap' = \frac{g'}{aax''t'} - \frac{Z'}{at'^{3/2}},$$

$$gp' = -\frac{3g'^{3}}{ax''t'^{2}} - \frac{3g'}{ax''t'} + \frac{3g'^{2}}{t'^{5/2}} + \frac{Z}{t'^{3/2}},$$

$$pp' = -\frac{3g'}{4ax''t'^{2}} - \frac{g'}{2ax''^{2}t'} + \frac{3Z'}{4t'^{5/2}}$$
and $op' = \frac{3g'^{2}}{2ax''t'^{2}} + \frac{3g'^{2}}{ax''^{2}t'} - \frac{3g'^{2}}{3t'^{5/2}}$

Then with the quantities defined as above,

IJS =
$$1b \pi \xi' (\xi' \xi'') + \frac{3p}{3a'} \frac{3p}{3b'} (bb') + \frac{3a}{3a'} (\frac{3p}{3b'}) (bb') + \frac{3a}{3a'} (\frac{3p}{3b'}) (ab')$$

$$+ (\frac{3a}{3a'} \frac{3p}{3b'} (gb') + \frac{3a'}{3a'} \frac{3p}{3a'} (ob') \}.$$

The expression for IBG is a great deal more complicated due to the presence of the partial with respect to y.

$$IBG = -16 \text{ m } \vec{z}. (\vec{z}.\vec{z}_2)^{5/2} \frac{1}{ab} (1 - \vec{z}_2 \frac{3}{3y}) \left\{ \frac{3}{ab} (\frac{3}{3b}) (rp) + \frac{3}{ab} (\frac{3}{3b}) (ap) + \frac{3}{ab} (\frac{3}{3b}) (pp) + \left[(\frac{3}{3a} \frac{3}{3b}) + (\frac{3}{3b} \frac{3}{3b}) (op) \right] + \frac{3}{ab} (\frac{3}{3b} \frac{3}{3b}) (ap) - \frac{1}{2a} (ap) + (ap) \frac{3}{3y} (\frac{3}{3a} \frac{3}{3b}) + (rp) \frac{3}{3y} ($$

Recall that

$$d\delta = \left[(\vec{A} - \vec{B})^2 + (a+b)^2 \right] \left[A^2 + (a+y)^2 \right] \left[B^2 + (b+y)^2 \right]$$

and

The partial derivatives needed above are given below.

$$\frac{\partial AB}{\partial a} = 2(a+y) \left[(\vec{A} - \vec{B})^2 + (a+b)^2 \right] \left[B^2 + b^2 + y^2 \right] + 2(a+b) \left[A^2 + (a+y)^2 \right] \left[B^2 + (b+y)^2 \right]$$

$$\frac{\partial}{\partial b} \left(\frac{\partial a y}{\partial b} \right) = 4 (a+y)(b+y) \left[(\vec{A} - \vec{B})^2 + (a+b)^2 \right] + 4 (a+b)(b+y) \left[\vec{A}^2 + (a+y)^2 \right] + 4 (a+y)(a+b) \left[\vec{B}^2 + (b+y)^2 \right] + 2 \left[\vec{A}^2 + (a+y)^2 \right] \left[\vec{B}^2 + (b+y)^2 \right].$$

$$\frac{2}{2y}\left(\frac{2a}{2a}\frac{3ax^4}{3b}\right)^2 + \left[a+b+2y\right]\left[(\vec{A}-\vec{B})^2 + (a+b)^2\right] + \left[b(a+b)(a+y)(b+y)\right] + 4\left[a+2b+y\right]\left[A^2 + (a+y)^2\right] + 4\left[2a+b+y\right]\left[A^2 + (a+y)^2\right]$$

$$\frac{2}{3y}\left(\frac{3dx}{3a}\right) = 4(a+y)(b+y)\left[(\vec{A}-\vec{B})^2 + (a+b)^2\right] + 2\left[(\vec{A}-\vec{B})^2 + (a+b)^2\right]\left[B^2 + (b+y)^2\right] + 4(a+b)(a+y)\left[B^2 + (b+y)^2\right] + 4(a+b)(b+y)\left[A^2 + (a+y)^2\right]$$

$$\frac{2}{2y}\left(\frac{24b}{2b}\right) = 4(a+y)(b+y)\left[(\vec{A}-\vec{B})^2 + (a+b)^2\right] + 2\left[(\vec{A}-\vec{B})^2 + (a+b)^2\right]\left[\dot{A}^2 + (a+y)^2\right] + 4(a+b)(a+y)\left[B^2 + (b+y)^2\right] + 4(a+b)(b+y)\left[A^2 + (a+y)^2\right]$$

$$\frac{\partial t}{\partial y} = \frac{\partial}{\partial y} (4y - \beta^2) = \frac{\partial 4y}{\partial y} - 2\beta \frac{\partial \beta}{\partial y}$$

$$\frac{\partial \overline{z}}{\partial y} = \frac{B^2}{\lambda x} \left[\frac{1}{a\beta t^{2}} \frac{\partial t}{\partial y} - \frac{t^{2}}{\beta} \frac{\partial \beta}{\partial y} \right] = \frac{B^2}{adx^{2}} \frac{\partial dx}{\partial y} - \frac{B^2}{ax^{2}} \frac{\partial \beta}{\partial y} - \frac{t^{2}}{ax^{2}} \frac{\partial \beta}{\partial y}$$

$$\frac{\partial}{\partial y}(rp) = \frac{\partial dy}{\partial y} \left[\frac{1}{dy^2} + \frac{8^2}{dy^2t} + \frac{38^2}{2dy^2t^2} - \frac{38^2}{2t^{442}} \right] + \frac{28}{2y} \left[-\frac{38}{dyt} - \frac{38^3}{dyt^2} + \frac{2}{t^{442}} + \frac{38^2}{t^{5/2}} \right].$$

$$\frac{\partial}{\partial y} (ap) = \frac{\partial ay}{\partial y} \left[-\frac{\beta}{2ay^2t} - \frac{3\beta}{4xyt^2} + \frac{3\xi}{4t^{5/2}} \right] + \frac{\partial \beta}{\partial y} \left[\frac{1}{ayt} + \frac{3\beta^2}{2ay^2t^2} - \frac{3\beta\xi}{2t^{5/2}} \right]$$

$$\frac{\partial}{\partial y} \left(gp \right) = \frac{\partial x^{N}}{\partial y} \left[\frac{3\beta^{3}}{x^{N}^{2}t^{2}} + \frac{3\beta}{d3^{2}t} - \frac{15\beta^{2}z}{2t^{7/2}} + \frac{15\beta^{3}}{24^{N}t^{3}} - \frac{3z}{2t^{5/2}} + \frac{7\beta}{24^{N}t^{2}} \right] + \frac{\partial}{\partial y} \left[-\frac{19\beta^{2}}{4^{N}t^{2}} - \frac{15\beta^{N}}{4^{N}t^{2}} + \frac{9\beta^{N}z}{t^{5/2}} + \frac{15\beta^{N}z}{t^{7/2}} - \frac{4}{4^{N}t} \right]$$

$$\frac{\partial}{\partial y} \left(pp \right) = \frac{3ax}{3y} \left[\frac{5\beta}{4ax^2t^2} + \frac{\beta}{ax^3t} + \frac{15\beta}{8ax^3t^3} - \frac{15z}{8t^{712}} \right] + \frac{3\beta}{3y} \left[-\frac{3}{2ax^2t^2} - \frac{15\beta^2}{4ax^2t^3} - \frac{15\beta^2}{2ax^2t} - \frac{\beta^2}{ax^2t^2} + \frac{15\beta^2}{4t^{712}} \right]$$

$$\frac{\partial}{\partial y} \left(\text{ op} \right) = \frac{\partial x^8}{\partial y} \left[-\frac{3\beta^2}{2x^8 z^2} - \frac{1}{x^8 z^2} - \frac{1}{x^8 z^2} + \frac{15\beta^2}{4t^{1/2}} - \frac{15\beta^2}{4x^8 t^2} \right] + \frac{\partial \beta}{\partial y} \left[\frac{13\beta}{2x^8 t^2} - \frac{3\xi}{2t^{5/2}} - \frac{15\beta^2 \xi}{2t^{5/2}} + \frac{15\beta^3}{2x^8 t^2} \right].$$

APPENDIX 3

A computer program that calculates single and double charge capture cross sections from the ground state of a target atom into the ground state of a projectile. These are given in units of a_0^2 , πa_0^2 and cm^2 , in the approximations of Brinkman and Kramers, Jackson and Schiff, and Bassel and Gerjuoy.

COMPUTATION OF SINGLE AND COUBLE ELECTRON CAPTURE CROSS SECTIONS IN THE BRINKMAN AND KRAMERS, THE JACKSON AND SCHIFF AND THE PREGRAM BY TERRY C. THEISEN, KANSAS STATE UNIVERSITY, NCV. 1978. BASSEL AND CERJUCY APPRCXIMATIONS.

CHARGE OF THE PRCJECTILE IN ATCMIC UNITS MASS OF THE PROJECTIVE IN ATCMIC UNITS IS THE

MASS OF THE TARGET IN ATOMIC UNITS M2 IS THE

22 IS THE CHARGE OF THE TARGET IN ATCMIC UNITS BEI IS THE BINDING ENERGY OF THE INITIAL SYSTEM.

BEF IS THE BINDING ENERGY OF THE FINAL SYSTEM.

BIA IS THE INITIAL BINDING ENERGY IN ATCMIC UNITS.

ENERGY IS THE ENERGY OF THE INCIDENT PARTICLE IN ELECTFON VOLTS. BFA IS THE FINAL BINDING ENERGY IN ATCMIC UNITS.

V IS THE VELOCITY OF THE INCIDENT PARTICLE

KI IS THE MCMENTUM OF THE INCIDENT PARTICLE.

THE INITIAL AND FINAL RECUCED MASSES ARE MUI AND MUF RESPECTIVELY. KF IS THE MCMENTUM OF THE TARGET AFTER CAPTURE.

THETA IS THE SCATTERING ANGLE

TIMETA IS THE SCATTERING AMPLITUDE

B IS THE IMPACT PARAMETER

BJ IS THE VALUE OF THE ZERCTH CROER BESSEL FUNCTION WHOSE

ARGUMENT IS: K#B#THETA

PRCBABILITY AMPLITUDE SQUARED IS THE PRCEABILITY ANFLITUDE IS THE ٦r

SUM GF THE JACKSON AND SHIFF AND THE DENCTES THE PRINKMAN KRAMERS APPROXIMATION.

APFRCXIMATICNS. DENCTES THE

DENOTES THE SUM OF THE JS AND THE BASSEL AND GERJUCY APPRCXIMATICNS. BG

INPLICIT REAL#8 (A-H,O-Z)

```
FCRMAT ('1',7X,'CALCULATION OF TOTAL CROSS SECTIONS',
1///8X,'Ml=',F11.5,10X,'Zl=',F8.5//8X,'R2=',F11.5,10X,'Z2=',F8.5//)
                                                                                                                                                                                                                                                                              FCRMAT (/'0',5X,'B',10X,'P(B)BK',11X,'P(B)JS',11X,'P(B)BG')
                                                                                                                                                                                                                                      FORMATIC/101, THE INCIDENT ENERGY IN EV IS: 1, FIG. 1//)
REAL*8 KI, KF, MUI, MUF, MI, N2, 18K, IJS, 18G
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     CTF ET 1= (THET 2-TF ET 1) /25.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        DTH ET2=(THET3-THET2)/25.
                                                                                                                                      IF (ENERGY.LE.O) STOP
                                                                                                                                                         PRINT. 15,41,21,42,22
                   REAU 10,M1,Z1,M2,Z2
                                                                                                                                                                                                                                                                                                                                                                                EI A=RE 1/ (2.0*RYCB)
                                                                                                                                                                                                                                                                                                                                                                                                  BFA=BEF/(2.0*RYCE)
                                                                                                                                                                                                                    PRINT 50, ENERGY
                                                                                                                                                                                                                                                                                                                      A0=5.25177150-9
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   IHET4=3.1405526
                                                         READ 12, BEI, BEF
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            THET2=3.0*22/M2
                                      FCRMAT (4F10.0)
                                                                             FORMAT (2F10.0)
                                                                                               REAC 20, ENERGY
                                                                                                                  20 FCRMAT (F15.0)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              TheT3=27.5/M2
                                                                                                                                                                                                                                                                                                                                                            E=ENFRGY/RYDB
                                                                                                                                                                                                                                                                                                                                         RYDE=13.6058
                                                                                                                                                                                                                                                                                                 PI=3,1415926
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 CO 40 J=1,50
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        THET1=C.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          E=-0.0499
                                                                                                                                                                                                                                                           PRINT 23
                                                                                                                                                                                                                                                                                                                                                                                                                                           SJS1=0.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                              SBG1=C.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 SEK 4=0.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    0.0=4202
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       5864=0.0
                                                                                                                                                                                                                                                                                                                                                                                                                      SEK 1=0.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              CP = 0.C5
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      E= E+CB
                                                                                                                                                                              15
                                                                             5.5
                                                                                                                                                                                                                                        5 C
                                                                                                                                                                                                                                                                              23
                                       10
```

SINGLE CAPTURE', 10x, 'IN', 15x, 'IN', 15x, 'IN')

FCKMAT (//'C', 'TOTAL

80

```
CALL AL(M1, M2, Z1, Z2, E, BIA, BFA, THET1, DTHET1, B, ALEK1, ALJS1, ALBG1)
CALL AL(M1, N2, Z1, Z2, E, BIA, BFA, THET2, GTFET2, B, ALEK2, ALJS2, ALBG2)
                                                                   AL(M1, M2, Z1, Z2, E, BIA, BFA, THET3, DTHET3, B, ALEK3, AL JS3, ALBG3)
                                                                                                                                                                                                                                                   FCRMAT ('0', 1PD10.3, 1P3D17.7)
                                                                                                                                                                                                                              PRINT 25,8, PBBK, FBJS, PBBC
DIHET3=(THET4-ThET3)/25.
                                                                                        ALBK=ALBK1+ALBK2+ALBK3
                                                                                                                                    AL 8G= AI BG1 + AL BG2 + ALBG3
                                                                                                                AL JS=ALJS1+ALJS2+ALJS3
                                                                                                                                                                                                                                                                                                                                                                   SBK4= SBK4+CC*PBBK**2
                                                                                                                                                                                                                                                                                                                                                                                         SJS4=SJS4+CC*PBJS**2
                                                                                                                                                                                                                                                                                                                                                                                                                SBG4= SBG4+CC*PBBG**2
                                                                                                                                                                                                                                                                                                                       SJS1=5JS1+CC *PBJS
                                                                                                                                                                                                                                                                                                                                               SPG1=SEG1+CC*PBBG
                                                                                                                                                                                                                                                                                                 SBK1=SBK1+CC*PBBK
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   SBK3=SBK2*A0**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         SJS3=5JS2*A0**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 SBG3=SBG2*A0**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       SBK 6= SBK 5*AC**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              SJS6=SJS5*A0**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     SEG6= SEG5*A0**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                             SBK1=SBK1*2.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     SJS1=SJS1*2.0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          SBG1= SBG1*2.0
                                                                                                                                                           PBBK=ALRK**2
                                                                                                                                                                                   PBJS=A1JS**2
                                                                                                                                                                                                         PBBG=ALBG*#2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            SEG2=SEG1*PI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  SBG5=SBG4*PI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     SBK5=SBK4*PI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               SBK2=SBK1*PI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      SJ 52= 5J51*PI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            SJS5=5JS4*PI
                                                                                                                                                                                                                                                                            CC=8*CB*2.0
                                                                                                                                                                                                                                                                                                                                                                                                                                       CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           PRINT 80
                                                                    CALL
                                                                                                                                                                                                                                                      25
                                                                                                                                                                                                                                                                                                                                                                                                                                       4)
```

- FORMAT ('0', 4X, 'CROSS SECTIONS', 10X, 'PI*A0**2', 10X, 'A0**2', 11X,
- PRINT 84, SBK1, SBK2, SBK3

84

- FCRAAT (/'0',1X, BRINKMAN KRAMERS',5X,1P3E17.7)
 - PRINT 86,5351,5352,5353
- FGRMAT (/'0',1X,'JACKSCN AND SCHIFF',3X,1P3D17.7) 86
 - PRINT 88, SBC1, SEG2, SEG3

88

- FCRMAI (/'0',1X,'EASSEL ANE GERJUDY',3X,1P3D17.7)
- PRINT 50
- FCRMAT (//'O','TGTAL GCUBLE CAPTURE',10X,'IN',15X,'IN',15X,'IN') PRINT 52 06
 - FORMAT ('0', 4X, 'CROSS SECTIONS', 10X, 'PI*AC**2', 1CX, 'AC**2', 11X, 1 · C / * * 2 ·) 6
- PRINT 94, SBK4, SBK5, SBK6
- FCHMAT (/'0', 1X, 'BRINKMAN KRAMERS', 5X, 1P3D17.7) PRINT 56,5354,5355,5356 76
- FCRMAT (/'0',1X,'JACKSCN AND SCHIFF',3X,1F3017.7) 96
 - PRINT 58, SBC4, SBC5, SBC6
- FORMAT (/'0',1X,'BASSEL AND GERJUDY',3X,1P3C17.7) 5 01 39 58

AMPLITUDE WHICH IS THE INTEGRAL OF THE PROCUCT OF THE SCATTERING AMPLITUDE. THE JO BESSEL FUNCTION. SIN(THETA), AND A CONSTANT CVER AND THE TARGET, RESPECTIVELY. E IS THE ENERGY OF THE PROJECTILE MI, M2, ZI, ANC ZZ ARE THE MASSES AND CHARGES OF THE PROJECTILE SUBRGUTINE AL CALCULATES THE SGUARE RUCT OF THE PROBABILITY A GIVEN THETA INTERVAL.

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SUERCUTINE AL(M1, M2, Z1, Z2, E, B1 A, BFA, THETA, CTFETA, B, ALBK, ALJS, ALBG) IMPLICIT REAL#8 (A-H,C-Z)

```
GRJS=3.*BTAJS**2/(2.*AGJS*1JS**2) +1./(AGJS*TJS) -3.*BTAJS*2JS/
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             FNKJS=-3.*ETAJS/(4.*AGJS*IJS**2) -8TAJS/(2.*AGJS**2*1JS)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            REDJS=-1./AGJS -BTAJS**2/(AGJS*TJS) +BTAJS*ZJS/TJS**1.5
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       GRJS=-(3.*BTAJS**3)/(AGJS*TJS**2)-3.*BTAJS/(AGJS*TJS)
+(3.*BTAJS**2*ZJS)/TJS**2.5 +ZJS/TJS**1.5
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             AMNBSC=ASQ+BSC+2.*KI*KF*CCCS(TFETA)*(W*X A+1.0)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                BSG=KF**2+(XA*KI)**2-2.0*KI*KF*XA*DCCS(THE1A)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         AGUAJS=8TAJS/(2.*AGJS*TJS) -ZJS/(2.*TJS**1.5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  ASD=KI **2+( W*KF) **2-2.0*KI *KF* W*DCOS (TheIA)
                                                                                                                                                                                                                                                               KF=(MUF*(KI**2/MUI-2.0*(BII-EFA)))**0.5
REAL * B KI, KF, MUI, MUF, MI, W2, I BK, IJS, IBG
                                                                                                                                                                                                                                                                                                                                                       (3= (MUI * MUF * KI * KF) * * G.5/(2.*PI)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             +3. #7 J5/(4. # TJ5 # #2.51
                                                                                                                                              MUF=(M2*(M1+1.))/(M1+M2+1.)
                                                                                                                NLI=(N1*(M2+1.))/(N1+N2+1.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           -2 ** (N*KF**2+XA*KI**2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    ZJS=EATAN(TJS**.5/ETAJS)
                                                                                                                                                                                                                                                                                                                         C=16.*PI*(21*Z2)**2.5
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       F=AMNBSO+(21+22)**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         BIAJS=22*0JS+21*RJS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        THETA=THETA+CTHETA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       JS=AGJS-BTAJS**2
                          A0=5.2917715C-9
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             AGJS=P*0JS*RJS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     6.JS=ASC+Z1**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 RJS=850+22**2
                                                                                                                                                                                                         XA=M2/(M2+1.)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                            CC 30 J=1,25
                                                          PI=3.1415926
                                                                                      V=(E/N1)**.5
                                                                                                                                                                            W= M1/(M1+1.)
                                                                                                                                                                                                                                                                                                                                                                                                                                                ALBG=0.00
                                                                                                                                                                                                                                                                                                                                                                                       AL BK=0.00
                                                                                                                                                                                                                                                                                                                                                                                                                  00.0=SL 1A
                                                                                                                                                                                                                                     K I = MU I *V
                                                                                                                                                                                                                                                                                                 Y=2.*Z2
```

```
AAGJSB=4.#21#22#P+4.#22#(21+22)#4JS+2.#4JS*RJS+4.#21#(21+22)#RJS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     +BY*(-(15.*ETA**2/(AG*T))*(ETA**2/T**2)+(5.*ETA/T**1.5)*(Z/T)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          PNKY=AGY*((5.*BTA/AG**2)/(4.*T**2)+(BTA/AG**2)/(AG*T)-(15./T**2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    +BY*(-(3./AG)/12.*T**2)-1./(2.*AG**2*1)-(BIA**2/AG**2)/T**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     -(15.*BIA**2/1**2)*(2/(2.*T**1.5))+(15.*BIA**2/(2.*AG*I))*
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          GR=-3. *BIA**3/(AG*T**2) -3. *BIA/(AG*I) + (3. *EIA**2*2)/ T**2.5
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         +3. +81 A * *2/(2. * A G * I * *2)) +8 Y * (-3. * B I A / ( A G * I ) -3. * E I A * * 3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       PNK=-3 **BIA/(4.*AG*T**2) -ETA/(2.*AG**2*T) +3.*I/(4.*T**2.5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  (BTA/T**2)-(3./(2.*T))*(2/T**1.5)+(7.*ETA/(2.*T**2))/AG)
                                                                                                                                                                                                  IJS=(C/22)*(2.*(21+22)*REDJS +AAGJSB*AGUAJS +BJSA*BJSB*GRJS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               ACUAY=AGY+(-BIA/(2.*AG**2*I) +3.*Z/(4.*T**2.5) -3.*BIA/(4.*
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  AG*T**21) +8Y*(1./(AE*T) +3.*BTA**2/(2.*AE*1**2) -3.*
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          OR=3.*BIA**2/12.*AG*T**2) +1./(AG*T) -3.*ETA*2/12.*T**2.5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                REDY=AGY*(1./AG**2 +BTA**2/(AG**2*T) -3.*BTA*2/(2.*T**2.5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  +(15. *BIA**2/1**2)*(BIA*2/1**1.5)-(19.*ETA**2/T**2)/AG
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  GRY=AGY*((3.*BTA**2/AG**2)*(BTA/T**2)+(3.*BTA/AG**2)/T
                                                                                                                                                                                                                                                  +ACJSA*AGJSB*FNKJS +(AGJSA*EJSB+AGJSB*BJSA)*CRJS)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    *[2/(8.*1**1.5))+(15./(8.*AG*T))*(ETA/T**2))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               /(AG*1**2) +2/1**1.5 +3 .*ETA**2*2/T**2.5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       REC=-1./AG -BIA**2/(AG*T) +BIA*2/1**1.5
                                                                                                                                                  INK=(-32,*PI*(21*22)**2,5)/(6JS**2*RJS)
                                               AGJSB=2. *22*QJS*P+2. *(21+22) *QJS*RJS
AGJSA=2.*21*RJS*P+2.*(21+22)*QJS*RJS
                                                                                                                                                                                                                                                                                                                                                                                                                                                        BIA=Y*P+22*(GJS+Y**2)+21*(RJS+Y**2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       AGUA=BIA/(2.*AG*I) -2/(2.*1**1.5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             AGY=2.*(Z2+Y)*P #Q +2.*(Z1+Y) #P #R
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  BTA+2/(2. + T + + 2.51)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          Z=CAIAN( T** . 5/8TA)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                BY=P+2.*Y*(21+22)
                                                                                                                                                                                                                                                                                                        G=ASO+(Z1+Y)**2
                                                                                                                                                                                                                                                                                                                                                     R= ESG+ (22+Y) **2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             42/1**1.5
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        1=4G-81A**2
```

8JSA=2.*Z1*Z2+RJS 8JSB=2.*Z1*Z2+CJS

```
+(15.*BTA/T**2)*(2/(4.*T**1.5))-(15.*BTA**2/(4.*T**2))/(AG*T))
                                                                                                    +BY*(-(3./(2.*T))*(2/1**1.5)-(15.*BTA**2/1**2)*(2/(2.*T**1.5))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  YAAGB=4.*ABB*(0+P+R)+4.*(22*C+21*R+Y*P)+16.*(21+22)*(21+Y)*(22+Y)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       IBG=C*12.*ABB*(REDY-RED/22) +AAGB*(AQUAY-ACUA/22) +BA#EB*(GRY-GR/
                            ORY=AGY*(-(3.*BIA**2/(2.*AG**2))/T**2-1./(AG**2*1)-1./(AG*T**2)
                                                                                                                                         +(15. +8T A*#2/(2. * T * * 2)) *(BTA/(AG * 1)) + (13. *BTA/T * # 2) /(2. * AG))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             AAGB=4.#(21+22)#(22+Y)#Q+4.#(21+Y)#(22+Y)#F+4.#(21+22)#(21+Y)#R
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             +2.*RED +YAAGB*AGUA +2.*ABB*(BA+BB)*GR +(AGA*YAGE+AGB*YAGA)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    EQUATICNS
                                                                                                                                                                                                                                                                                                                                                               YAGA=4.*(21+Y)*(22+Y)*P+2.*P*R+4.*(21+Y)*(21+Z2)*R+4.*(21+Z2)*
+(15. *PTA/T**2)*(2/(4. *T**1.5))-(15. *ETA**2/T**3)/(4. *AG))
                                                                                                                                                                                                                                                                                                                                                                                                                                     YACB=4.*(Z1+Y)*(Z2+Y)*P+2.*P*Q+4.*(Z1+Y)*(Z1+Z2)*R+4.*(Z1+Z2)*
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          22) +AGA*ACE*(PNKY-FNK/22) +(AGA*EB+ACE*EA)*(ORY-OR/22)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    CALCULATION OF THE ZEROTH CROER RESSEL FUNCTION USING THE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         FCRMULAS OF ABRAMOWITZ AND STEGUN, PAGES 369 ANE 370,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  *FNK + (2. * ARB * ( AGA + AGH ) + BA * YAGB + BB * YAGA ) *CR)
                                                                                                                                                                            BA=2.*Y*(21+221+2.*Z1*22+RJS+Y**2
                                                                                                                                                                                                                   8B=2.*Y*(Z1+72)+2.*Z1*Z2+QJS+Y**2
                                                                                                                                                                                                                                                                                                                          AGB=2.*(22+Y)*P*0+2.*(21+22)*0*R
                                                                                                                                                                                                                                                                                       AGA=2.*(21+Y)*P*R+2.*(21+22)*0*R
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               IF (X+3.) 50,100,100
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             TTBG=18K+1JS+18G
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              9.4.1 AND9.4.3.
                                                                                                                                                                                                                                                                                                                                                                                                      (22+Y) *C
                                                                                                                                                                                                                                                                                                                                                                                                                                                                              (22+1)*C
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  +2.*0*R
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          ITJS=IEK+IJS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  X=KI*IHETA*B
                                                                                                                                                                                                                                                        ABB=Y+21+22
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         VAL 1= X/3.00
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          VAL2=3.00/X
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       11
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     DL 09
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  IER=1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       100 1ER=0
```

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THETA0=X -.7853581600 -.0416635700*(VAL2) -. COCC395400*[VAL2]**2
                                                                                                                                                                    200 FO=.7578845600 -.000CCC77DC*(VAL2) -.0C55274CDC*(VAL2)**2
                                                                                                                                                                                                                                                                                                   +.0026257300*(VAL2) **3 -.00054125E0*(VAL2) **4
                                                                                                                                                                                                                                                                                                                                      -.00029333D0*(VAL2)**5 +.CCC13558D0*(VAL2)**6
                                150 BJ=1.00-2.249999700*(VAL1)**2 +1.2656208C0*(VAL1)**4
                                                                                                                                                                                              -.0C005512D0*(VAL2)**3 +.00137237E0*(VAL2)**4-.000728C5D0*(VAL2)**5 +.C0014476D0*(VAL2)**6
                                                                                               -.0039444D0*(VAL1)**10 +.C0C2100D0*(VAL1)**12
                                                              -.3163866DC*(VAL1)**6 +.0444479DO*(VAL1)**8
                                                                                                                                                                                                                                                                                                                                                                                                                                           CTHET A=C3*BJ*DSIN(THETA)*DTHETA
                                                                                                                                                                                                                                                                                                                                                                      BJ=F0*DCCS(THETA01/X**.5E0
IF (X-3.) 150,150,200
                                                                                                                                                                                                                                                                                                                                                                                                                                                                           AL BK=ALBK+TIBK*CTHETA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            AL JS=ALJS+TTJS*CTHETA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              ALBG=ALBG+TTBG*CT+ ET A
                                                                                                                                                                                                                                                                                                                                                                                                        17 CCNTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   RETURN
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     SENTRY
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                30
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APPENDIX 4

This computer program computes single charge capture differential cross sections in πa_0^2 for the approximations of Brinkman and Kramers, Jackson and Schiff, and Bassel and Gerjuoy.

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1///8X, 'Ml=',F11.5,10X,'21=',F8.5//3X,'M2=',F11.5,10X,'22=',F8.5//
                                                                                                                                                                                                                                                                                                                                                                                                                            1 10X, '(DSIGMA/CCMEGA)BK', 1X, '(CSIGMA/CCMEGA)JS', 1X, '(DSIGMA/CCMEGA
CALCULATION OF DSIGMA/DOMEGA IN THE BRINKPAN KRAPERS, JACKSON AND
                                                                                                                                                                                                                                                                                                                                                                                               32 FCRMAT ('0',2X,'THETA',6X,'LAMECA',10X,'IBK',14X,'IJS',14X,'IBG',
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              CALL DIFCS(M1,M2,Z1,Z2,E,THETZ,DTHETZ,CSCEKZ,CSCJSZ,CSCBG2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              CALL DIFCS(M1.M2,Z1,Z2,E,THET1,DTHET1,CSOBK1,USCJS1,CSCBG1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             CALL DIFCS(M1, M2, Z1, Z2, E, THET3, DTHET3, DSCBK3, DSCJS3, CSCBG3)
                                                                                                                                                                                                                                                                                             15 FCRMAT ('1',8X,'DIFFERENTIAL CROSS SECTIONS IN PI*A0**2.",
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                FORMAT(/'0'.'THE INCIDENT ENERGY IN EV IS: ',FIG.1//)
                             SHIFF, AND THE BASSEL AND CERJUDY APPROXIMATIONS.
                                                                                                                                                               REAL *8 K.MUI, MUF, MI, MZ, IBK, IJS, IBG
                                                                                                                                 IMPLICIT REAL*8 (A-H,C-Z)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              DTFET1=(THET2-TFET1)/30.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               DIHETZ=(IhET3-1hET2)/30.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               CTF ET3= (THET4-TFET3) /30.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                IF (FNERCY.LE.O) STOP
                                                                                                                                                                                                                                                               PRINT 15,M1,Z1,M2,Z2
                                                                                                                                                                                              READ 10, M1, Z1, N2, Z2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              PRINT 50, ENERGY
                                                                                                                                                                                                                                FCRMAT (4F10.0)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               Th ET2= .0029832
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               5 READ 20, ENERGY
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               20 FCRMAT (F15.C)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                THET4=PI-.001
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               E= ENER CY/RYCB
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                RYDB=13.6058
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              PI=3,1415926
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 THET3=P1/2.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  THET1=0.0
                                                                                                                                                                                                                                                                                                                                                               PRINT 32
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                50
   \circ \circ \circ \circ
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SUBRCUTINE CIFCS(MI, M2, Z1, Z2, E, THETA, CTHETA, CSCCRK, DSCCJS, DSCDBG)
                                                                                          THE JACKSON AND SCHIFF DIFF CROSS SECTION IS DENCTED BY DSDOJS.

THE BASSEL AND GERJUOY DIFF CROSS SECTION IS DENCTED BY DSDOJS.

MI. M2. ZI. AND ZZ ARE THE MASSES AND CHARGES OF THE PROJECTILE
                                                                                                                                                                                              AND TARGET, RESPECTIVELY. E IS THE ENERGY OF THE PROJECTILE IN
SUBRCUTINE CIFCS CALCULATES THE DIFFERENTIAL CRESS SECTION IN
                                                            THE BRINKMAN KRAMERS DIFF CRGSS SECTION IS DENCIED BY DSDCBK.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              AMNBSO=K**2*([W-1.)**2+(X-1.)**2+2.*(W*X-W-X+1.)*DCOS(THETA))
                               PI*AO**2 FCR A GIVEN THETA AND A GIVEN DIPETA.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               450=K**2*(1.+W*#2-2.*W*CCOS(ThETA))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                BSC=K**2*(1.+X**2-2.*X*CCOS(THETA))
                                                                                                                                                                                                                                                                                                                                                               REAL*8 K, MUI, MUF, MI, MZ, 18K, IJS, 18G
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             AL AMBD=(2.* NI* DSIN(THETA/2.))**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                NU I= [ N L* (M2+1.) ) / (M1+M2+1.)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 MUF=(M2*(M1+1.))/(M1+M2+1.)
                                                                                                                                                                                                                                                                                                                              IMPLICIT REAL *8 (A-H,0-Z)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                C=16.*PI*(21*22)**2.5
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               C2=MUI*MUF/ (4.*PI**3)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             P= AMNBSO+(21+22) **2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               BIAJS=12*6JS+21*FJS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                THETA= THETA +DTHETA
                                                                                                                                                                                                                                                                                                                                                                                                                                  A0=5.29177156-9
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               AGJS=P*CJS*RJS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              CJS=ASC+Z1**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                RJS=BS0+Z2**2
                                                                                                                                                                                                                                                                                                                                                                                                 PI=3.1415926
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              V=(E/N1) **.5
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                DO 30 J=1,3C
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               W=M1/(N1+1.)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 X=M2/(N2+1.)
                                                                                                                                                                                                                                RYCBERGS.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                K = MUI # V
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  Y=2.422
```

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IJS=C*(2*(Z1+Z2)*REDJS +AAGJSB*AQUAJS +BJSA*EJSE*GFJS +AGJSA*ACJSB
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                AAGJSB=4.*21*22*P+4.*22*(21+221*QJS+2.*GJS*RJS+4.*21*(21+22)*RJS
                                                                                                                                                                                                                                                       ORJS=3.*BTAJS**2/(2.*AGJS*1JS**2) +1./(AGJS*1JS) -3.*ETAJS*2JS/
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            GR =-3. *BIA**3/(AG*I**2) -3.*BIA/(AG*I) +(3.*BIA**2*2)/1**2.5
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        +3.*HTA**2/(2.*AG*T**2)) +BY*(-3.*BIA/(AG*I) -3.*BTA**3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   FNK=-3.4BTA/(4.4AG*T**2) -ETA/(2.*AG**2*1) +3.4Z/(4.*T**2.5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 AQUAY=ACY*(-BTA/(2.*A6**2*T) +3.*Z/(4.*1**2.5) -3.*BTA/(4.*
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     AG*T**2)) +BY*(1./(AG*T) +3.*BTA**2/(2.*AG*T**2) -3.*
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         OR=3.*BIA**2/(2.*AG*T**2) +1./(AG*T) -3.*ETA*2/(2.*T**2.5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     REDY=AGY*(1./AG**2 +BIA**2/(AG**2*1) -3.*EIA*2/(2.*1**2.5)
                                                                                                                                                                              PNKJS=-3.*ETAJS/(4.*AGJS*TJS**2) -8TAJS/(2.*AGJS**2*TJS)
                                 REDJS=-1./AGJS -BTAJS**2/(AGJS*TJS) +BTAJS*ZJS/TJS**1.5
                                                                                                   GRJS=-(3.*BIAJS**3)/(AGJS*TJS**2)-3.*BTAJS/(AGJS*TJS)
                                                                                                                                           +(3. *BIAJS**2*2JS1/TJS**2.5 +2JS/TJS**1.5
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              /(AG*T**2) +2/T**1.5 +3.*ETA**2*2/T**2.5)
                                                                  AQUAJS=8TAJS/(2.*AGJS*TJS) -ZJS/(2.*TJS**1.5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            *PNKJS + (AGJSA*BJSB+AGJSB*EJSA)*CRJS)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     IBK=(-32.*PI*(21*22)**2.5)/(6JS**2*RJS)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      RED=-1./AG -81A**2/1AG*I) +81A*2/1**1.5
                                                                                                                                                                                                                                                                                                                                                                                                       AGJSA=2. #Z1# FJS #P+2. # (Z1+Z2) #GJS #RJS
                                                                                                                                                                                                                                                                                                                                                                                                                                            AGJSH=2. #Z2#QJS#P+2. #(Z1+Z2)#QJS#RJS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              BIA=Y *P+ 22* (QJS+Y**2)+21* (RJS+Y**2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       AQUA=BIA/(2.*AG*I) -2/(2.*I**1.5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              AGY=2.*(Z2+Y)*P*Q +2.*(Z1+Y) *P*R
                                                                                                                                                                                                                    +3.*235/14.*135**2.51
ZJS=CATAN(TJS**.5/ETAJS)
                                                                                                                                                                                                                                                                                               (2. *TJS **2.5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       Z-DATAN(T**.5/ETA)
                                                                                                                                                                                                                                                                                                                                                                      BJSB=2. *Z1*Z2+QJS
                                                                                                                                                                                                                                                                                                                                BJSA=2.*21*22+RJS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      BY=P+2. * Y* (21+22)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               G=ASO+(21+Y)**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     R=BSO+(Z2+Y)**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    +2/1**1.5
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 T=AG-BIA**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          AG=P*C*R
```

1JS=AGJS-BTAJS**2

FORMAT ('0', F11.7, F11.4, 1P £017.7)

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+15.*BTA/(8.*AG*1**3)) +BY*(-3./(2.*AC*1**2) -1./(2.*AG**2*T)
                                                                                                                                                                                                                PAKY=AGY*(5. *BTA/(4. *AG**2*T**2) *BTA/(AG**3*T) -15. *2/(8. *T**3.5)
                                                                                                                                                                      T**2.5 +15.*BTA**3*Z/T**3.5 -19.*BTA**2/(AG*T**2) -4./(AG*T))
                                                                                                                                                                                                                                                                                                                                                                                                                                +15. #BI A*2/(4. #T*#3.5) -15. #BTA*#2/(4. #AG*T*#3)) +BY*(-3. #2/(
                                                                                                                                                                                                                                                                                                                                                                                                                                                                               2. *T **2.51 -15. * ET A**2 * Z / (2. *T **3.5) + 15. * BI A * 3 / (2. * AG * T * # 3)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   YAAGB=4.*ABB#(G+P+R)+4.*(Z2*G+Z1*R+Y*P)+16.*(Z1122)*(Z1+Y)*(Z2+Y)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          IBG=C*(2.*ABB*(REDY-RED/22) +AAGB*(AQUAY-ACUA/22) +BA*BB*(GRY-GR/
                                                                                                                            +7.*BIA/(2.*AG*T**2)) +8Y*(-15.*BIA**4/(AG*T**3) +9.*EIA*2/
                                                                                                                                                                                                                                                                                                                                                                                      ORY=AGY+(-3. +BIA++2/(2. +AG++2+I++2) -1./(AC++2+1) -1./(AG+T++2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              AAGB=4.*(21+22)*(22+Y)*G+4.*(21+Y)*(22+Y)*F+4.*(21+22)*(21+Y)*R
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     +2.*RED +YAAGB*AQUA +2.*ABB*(BA+EB)*CR +(AGA*YAGE+AGB*YAGA)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       YAGA=4.*(21+Y)*(22+Y)*P+2.*P*R+4.*(21+Y)*(21+Z2)*R+4.*(21+Z2)*
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          YAGB=4.*(21+Y)*(22+Y)*p+2.*P*Q+4.*(21+Y)*(21+Z2)4R+4.*(21+Z2)*
                                                                                                                                                                                                                                                                                                   -EIA**2/(AG**2*T**2) +15. *BIA*2/(4.*T**3.5) -15.*EIA**2,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         Z2) +AGA*AGB*(PNKY-PNK/Z2) +(AGA*BB+AGB*EA)*(ORY-OK/Z2)
                                                                                (2.*T**3.5) +15. *BIA**3/(2,*AG*T**3) -3.*2/(2.*T**2.5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     PRINT 40, THE TA, ALAMBD, IBK, 1JS, IBG, DSCCEK, CSCCJS, CSCOEG
                                       GRY=AGY*(3.*81A**3/(AG**2*1**2) +3.*81A/(AG**2*1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             *PNK + (2 * * ABB * (AGA + AGB )+ BA * YAGB + BB * YACA) *CR)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    BA=2.*Y*(21+22)+2.*Z1*22+RJS+Y**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 BB=2.*Y*(21+22)+2.*21*22+6J5+Y**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            AGA=2.*(21+Y)*P*R+2.*(21+22)*Q*R
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        AGB=2.*(22+Y)*P*Q+2.*(21+22)*Q*R
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        +13.*BTA/(2.*AG*T**2))
BTA*Z/(2.*T**2.51)
                                                                                                                                                                                                                                                                                                                                                    [4.*AG*T**3]]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        DSDCBK=C2*TTEK**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    CSC0JS=C2*T1JS**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              OSCORG=C2*118G**2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               [TBG=IBK+1JS+IEG
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   (ZZ+X)*C
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         3 × ( X + Z Z )
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          +2. #0*R
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     11 JS=1 BK+1 JS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        AEB=Y+21+22
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1836.0 30 CCNTINLE RETURN END \$ENTRY 1836.0 25000. 0.0

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MULTIPLE ELECTRON CAPTURE AT HIGH VELOCITIES USING THE BATES POTENTIAL IN THE INDEPENDENT ELECTRON APPROXIMATION

by

TERRY CAGNEY THEISEN

B.A., Colorado State University, 1976

AN ABSTRACT OF A MASTER'S THESIS

submitted in partial fulfillment of the

requirements for the degree

MASTER OF SCIENCE

Department of Physics

KANSAS STATE UNIVERSITY

Manhattan, Kansas

Cross sections are calculated in the independent electron approximation using the Bates-Born approximation. Based on the independent electron approximation, where electrons in a multi-electron atom are uncorrelated, the probability for capture of two electrons is the product of the probabilities of capture of two single electrons. Probability amplitudes for single electron capture are computed using the difference between the instantaneous and average interaction potentials. This choice has been made because it eliminates the dependence of the probability amplitude on the choice of the zero point potential and it effectively orthogonalizes the initial and final wave functions used in the transition matrix.

Agreement with the literature is obtained for capture of a single electron for protons incident on hydrogen. The technique is then used to calculate single and double charge capture cross sections from the K-shell of helium atoms to the K-shell of alpha particles for incident energies of 0 to 1,000 KeV. These results are compared to experiment and previous calculations and reasonable agreement is obtained.