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DETERMINATION OF THE TRACKING SIGNAL CONTROL LIMITS

by

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CHAPTER I

INTRODUCTION

Forecasting is a technique of estimating future values if the underlying process continues as it has in the recent past. For any forecasting system the two essential requirements are past data and an adequate forecasting model.

A forecasting model is constructed on the basis of past data. Such a model will provide reasonably accurate forecasts as long as the actual process does not change. However, any process is not static and is liable to change with time. The forecasting system, by some means should be able to detect these changes so that the parameters of the model can be updated to meet the new situation.

A change in the process is immediately reflected in the magnitude of the forecast errors. A forecast error is defined as the difference between the actual observation and its prior forecast. Mathematically;

$$x(t) = \hat{x}_{\tau}(t) + e_{\tau}(t)$$

where

$x(t)$ = the observed value at time t

$\hat{x}_{\tau}(t)$ = the forecast value for time t , which has been made at time $(t-\tau)$, where τ is the forecast horizon.

and

$e_{\tau}(t)$ = error at time t with a horizon of τ .

Unless otherwise stated the forecast horizon τ is one. Whenever a change in the process occurs, the predicted values start lagging the observed values. This results in a change in the error magnitudes which can be used to signal a process change. For this purpose a statistic is necessary. The statistic should be expressed as a function of forecast errors.

The tracking signal is a function of forecast errors and is widely used as a means for detecting process changes. It is a ratio of two smoothed statistics derived from the forecast errors. If the forecasting system is adequate the magnitude of the tracking signal lies close to zero. When the process changes the forecast errors become large and the tracking signal attains large values. To determine whether the process has changed significantly one needs to specify an acceptable limiting value for the tracking signal.

Confidence limits for the tracking signal could be evaluated if the distribution of the tracking signal is known. The present work is an attempt to determine the distribution of the tracking signal and subsequently to propose confidence limits. Two approaches were adopted;

1. Approximating the tracking signal distribution with some known statistical distribution and then imposing confidence limits in terms of the parameters of the approximating distribution.
2. Evaluating confidence limits by computer simulation.

The above approaches deal with a constant model and use single exponential smoothing for predicting future values.

When the forecasting system is making satisfactory forecasts the forecast error magnitude is small and the tracking signal magnitude

is close to zero. When a change takes place in process level, the tracking signal grows larger and sometimes exceeds specified limits depending on the magnitude of the change. At any such time two problems may arise:

1. When should one confirm a change in the process
2. If a change in the process is confirmed how should the forecast system be adjusted to recover rapidly from the change.

The solutions to these problems are not unique. However, a change in the process is usually confirmed when two successive values of the tracking signal exceed a specified limit.

Considering the above problems, the behavior of the tracking signal to a step increase in the process level was studied by simulation. A step increase in the process level was introduced, after the effect of the initial forecast conditions had been discounted to an acceptable value. The magnitude of the step increase varied from 2.5 percent to 25 percent of the process mean. By specifying the limiting value of the tracking signal and using various criteria a change in the process level was confirmed. Various detecting rules were simulated 1000 times and the probability of detecting a process change was obtained. These probabilities were evaluated for smoothing constants ranging from 0.05 to 0.25.

LITERATURE REVIEW

The concept of the tracking signal was first introduced by Brown [1]. If the forecasts are satisfactory, the average forecast error

and the sum of forecast errors will be close to zero. When there is a change in the process, the sum of errors starts drifting away from zero. The problem is to determine when a drift is large enough to imply a process change. For this purpose Brown defined the tracking signal as:

$$\begin{aligned}\text{Tracking Signal} &= \frac{\text{Sum of errors}}{\text{Mean absolute deviation of errors}} \\ &= \frac{\text{S.E.}}{\text{M.A.D.}}\end{aligned}$$

The S.E. is computed by adding the error arising from every new observation to the previous sum of errors. Mathematically

$$Y(t) = Y(t-1) + e(t)$$

where

$$Y(t) = \text{Sum of errors at time } t$$

$$Y(t-1) = \text{Previous sum of errors}$$

and

$$e(t) = \text{Error at time } t.$$

The M.A.D. is a measure of the scatter of the data around the mean.

If $e(t)$ represents the error having a statistical distribution $p(e)$ about the mean μ , then the M.A.D. Δ_e is defined as,

$$\Delta_e = \int_{-\infty}^{\infty} |e - \mu| p(e) de$$

In most cases $\mu = 0$ and the computation is considerably reduced. For a general case, a normalized variable Z may be defined such that

$$Z = \frac{e - \mu}{\sigma_e},$$

where σ_e is standard deviation of errors. The M.A.D. is then

$$\begin{aligned} \Delta_e &= \int_{-\infty}^{\infty} |Z \sigma_e| p(Z) dZ \\ &= \sigma_e \int_{-\infty}^{\infty} |Z| p(Z) dZ \end{aligned}$$

Hence, the M.A.D. is proportional to the standard deviation of the errors.

For normally distributed errors, the constant of proportionality is 0.79788. For detecting a process change, the control limits for the tracking signal are to be evaluated. For this purpose a constant model has been considered. A constant model is one in which the observations are random samples from some distribution whose mean does not change significantly with time. The observations $x(t)$ from such a model can be represented by:

$$x(t) = \xi(t) + \varepsilon(t)$$

where

$$\xi(t) = \text{Process mean}$$

$$\varepsilon(t) = \text{Random noise with } E[\varepsilon(t)] = 0,$$

$$\text{Var}(\varepsilon(t)) = \sigma_\varepsilon^2 \text{ and } \text{cov}(\varepsilon_i, \varepsilon_j) = 0, \text{ for } i \neq j$$

According to Brown pp. 289, the variance of S.E. say σ_Y^2 , for the above model is given by:

$$\sigma_Y^2 = \frac{1}{1-\beta^2} \sigma_\varepsilon^2$$

where β = Discount factor = $(1-\alpha)$, α being smoothing constant. If the errors are normally and independently distributed with mean zero, and the noise samples are serially independent, the M.A.D. Δ_e evaluated by Brown pp. 289 is

$$\Delta_e = \sqrt{2/\pi} \sqrt{\frac{2}{2-\alpha}} \sigma_\varepsilon$$

or

$$\sigma_\varepsilon = \Delta_e \sqrt{\pi/2} \sqrt{\frac{2-\alpha}{2}} \quad (1.1)$$

Expressing σ_ε in terms of Δ_e , the variance of S.E. for a constant model is:

$$\sigma_Y^2 = \frac{1}{1-\beta^2} \pi/2 \frac{2-\alpha}{2} \Delta_e^2$$

$$= \frac{1}{1-(1-\alpha)^2} \pi/2 \frac{2-\alpha}{2} \Delta_e^2$$

$$= \frac{1}{\alpha(2-\alpha)} \pi/2 \frac{2-\alpha}{2} \Delta_e^2$$

$$= \pi/4\alpha \Delta_e^2$$

$$\therefore \sigma_Y = \sqrt{\pi/\alpha} \frac{\Delta_e}{2} \quad (1.2)$$

Since the standard deviation σ_y is proportional to M.A.D., the control limits for S.E. could be obtained in terms of Δ_e . The limiting values of the S.E., if divided by Δ_e , will be limiting values of the tracking signal. These limiting values will be pure numbers.

The definition of the tracking signal by Brown was modified by Trigg [2] of Eastman Kodak. Trigg found that there were two disadvantages with Brown's definition. To quote Trigg pp. 271, the disadvantages are:

"1) once the tracking signal has gone out of limits it will not necessarily return within limits even though the forecasting system itself comes back in control. Consequently, intervention is necessary to set the sum of forecast errors back to zero if future false alarms are to be avoided. Such interventions can be tedious and may tend to be neglected when several hundred items are being forecast.

2) Ironically if the system starts to give exceptionally accurate forecasts the tracking signal may go out of limits. For example, if perfect forecasts begin to occur, the M.A.D. will tend to zero whilst the sum of the errors will remain unaltered. This clearly leads to the tracking signal tending to infinity."

While considering these disadvantages Trigg modified the definition of the tracking signal to:

$$\begin{aligned}\text{Tracking Signal} &= \frac{\text{Smoothed error}}{\text{Smoothed mean absolute dev. of errors}} \\ &= \frac{\text{S.S.E.}}{\text{S.M.A.D.}}\end{aligned}$$

where

$$\text{S.S.E.} = (1-\alpha) \text{ Previous S.S.E.} + \alpha \text{ Latest Error}$$

and

$$\text{S.M.A.D.} = (1-\alpha) \text{ Previous S.M.A.D.} + \alpha \text{ Latest absolute error.}$$

S.S.E. can attain positive or negative values but S.M.A.D. will always be a positive quantity. Further, S.M.A.D. is always greater than S.S.E. However, at times they may be equal. Hence the tracking signal magnitude is bounded by +1 and -1. With this modification the disadvantages were overcome. This modified definition allowed Trigg to find new control limits for the tracking signal. In proposing the control limits he assumed that S.S.E. and S.M.A.D. are independent and the S.M.A.D. a constant. Trigg's approach to control limits was as follows: Let the error i periods in the past be denoted by e_i . Assume they are serially independent and have a standard deviation of σ . The smoothed error is

$$\text{S.S.E.} = \sum_{i=0}^{\infty} \alpha(1-\alpha)^i e_i$$

The smoothed error variance will be

$$\text{Smoothed Error Variance} = \sum_{i=0}^{\infty} [\alpha \sigma (1-\alpha)^i e_i]^2$$

As $0 < \alpha < 1$, $(1-\alpha)$ will be less than unity and the above expression will sum to:

$$\text{Smoothed Error Variance} = \frac{\alpha^2 \sigma^2}{[1 - (1-\alpha)^2]}$$

$$= \frac{\alpha}{2-\alpha} \sigma^2$$

Thus the two Sigma limits for S.S.E. are:

$$\pm 2\sqrt{\frac{\alpha}{2-\alpha}} \sigma$$

Trigg assumed S.M.A.D. to be constant for small values of α . For a wide range of distributions $\sigma \approx 1.2 \cdot \text{S.M.A.D.}$. Hence S.M.A.D. is approximately equal to $\sigma/1.2$. The control limits for the tracking signal thus becomes:

$$\pm 2.4\sqrt{\frac{\alpha}{2-\alpha}}$$

However, Trigg mentions that these limits do not hold good for high values of α . Batty [3] shows these limits in error for $\alpha = 0.1$. For higher values of α , limits were obtained by simulation. For the simulation, the errors were drawn independently and randomly from a normal distribution. A cumulative probability table was obtained which gave the limiting values of the tracking signal. According to Trigg, this table should not be referred to when the forecasting system giving rise to the errors is an adaptive system since this introduces autocorrelation of the errors.

Further, work in this field was carried out by Batty [3]. The cumulative probability table obtained by Trigg [2] was based upon the assumption that the errors are serially independent. Batty obtained a similar cumulative probability table taking into account the correlation between the two smoothed statistics. Moreover, the forecast errors were also correlated since they came from an adaptive forecasting system. A series of data was generated as observations by taking noise samples from a normal distribution. Forecasts were calculated using an appropriate level of smoothing. For each forecast S.S.E. and S.M.A.D. were calculated. The cumulative probability table for the tracking signal was obtained. The values in this table differed from those in Trigg's [2] table by 20% for a smoothing constant equal to 0.1.

CHAPTER II

THE TRACKING SIGNAL DISTRIBUTION APPROXIMATED BY A BETA DISTRIBUTION

2.1 INTRODUCTION

In this approach the tracking signal distribution is approximated with a known statistical distribution. The selection of the approximating distribution depends on the shape of the tracking signal distribution for different values of the smoothing constant. By simulation, tracking signal frequency distributions were obtained for various values of the smoothing constant ranging from 0.05 to 0.9. For small values of α , the distribution is symmetrical and unimodal. For moderate values of α , it becomes flat at the mode and finally becomes bimodal. For high values of α , the distribution is U-shaped. This variability in shape is illustrated in figure (2.1).

The beta family of statistical distribution was considered for approximating the tracking signal distribution. It has a finite range of zero to one. The distributions from this family can adopt various shapes depending upon their parameters. For example, the shape of the beta distribution is:

- a) symmetrical and unimodal when its parameters (m,n) are equal and greater than one. ($m = n > 1$)
- b) rectangular when both parameters are equal to one. ($m = n = 1$)
- c) U-shaped when both parameters are equal and less than one.
($m = n < 1$)
- d) skewed when parameters are unequal. ($m \neq n$)

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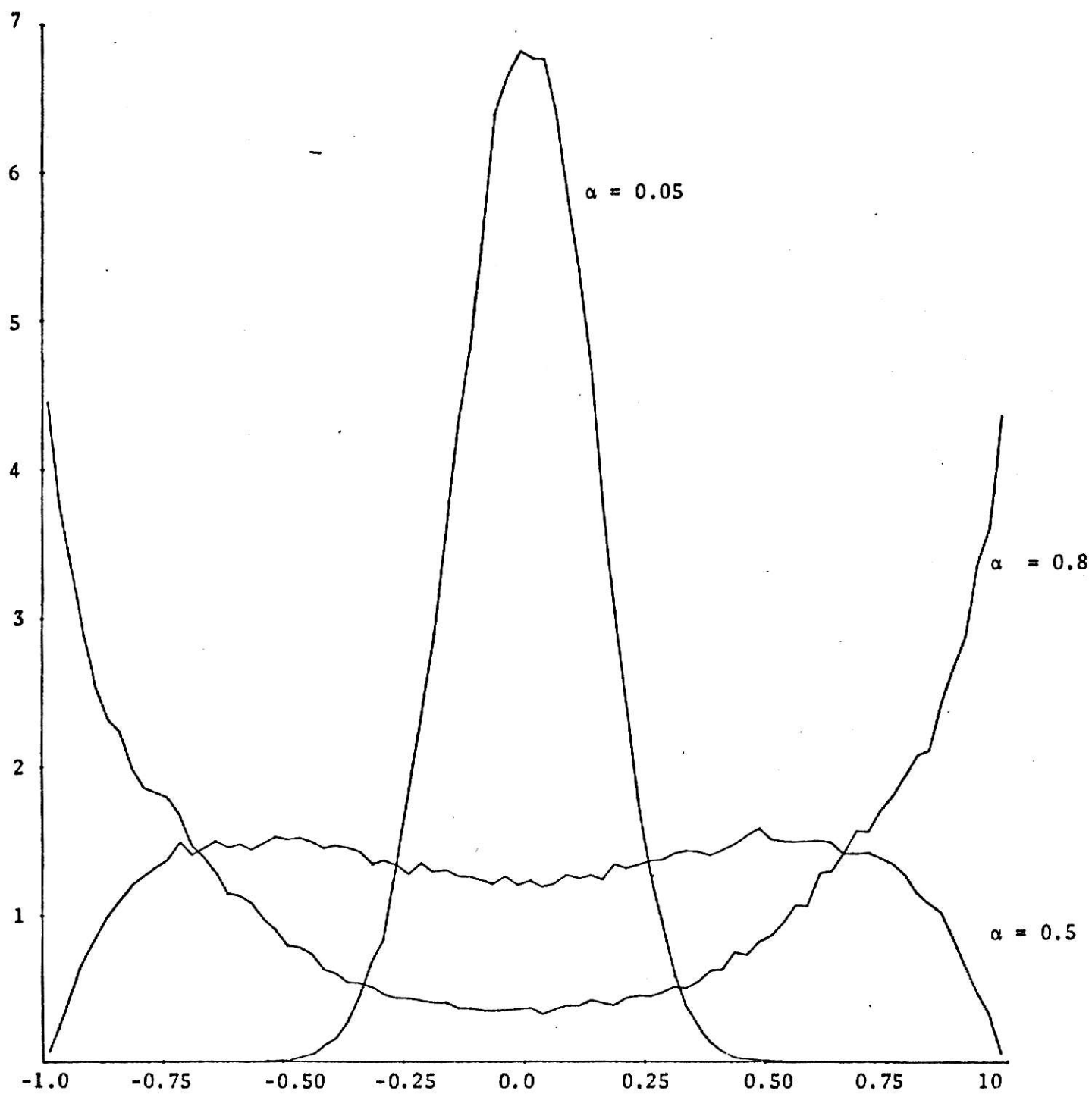


Figure (2.1) Variability in the Shape of the Tracking Signal Distribution

Further, a bimodal distribution could be obtained by combining two beta distributions with appropriate parameters.

2.2 DETAILS OF EXPERIMENTAL WORK

2.2.1 SIMULATION FOR TRACKING SIGNAL DISTRIBUTION

For simulating the tracking signal distribution a constant process has been considered with superimposed normal noise. The noise samples are assumed to be normally and independently distributed with mean zero and standard deviation of 1. Random normal deviates with a mean of 10 were generated as observations. Mathematically, the observations $x(t)$ could be represented as:

$$x(t) = \xi(t) + \epsilon(t)$$

where

$$\xi(t) = \text{process mean}$$

$$\epsilon(t) = \text{noise samples.}$$

These observations of the process were predicted by a forecasting system using single exponential smoothing. Let the predicted values be represented by $\hat{x}(t)$. The forecasting error at any time is given by:

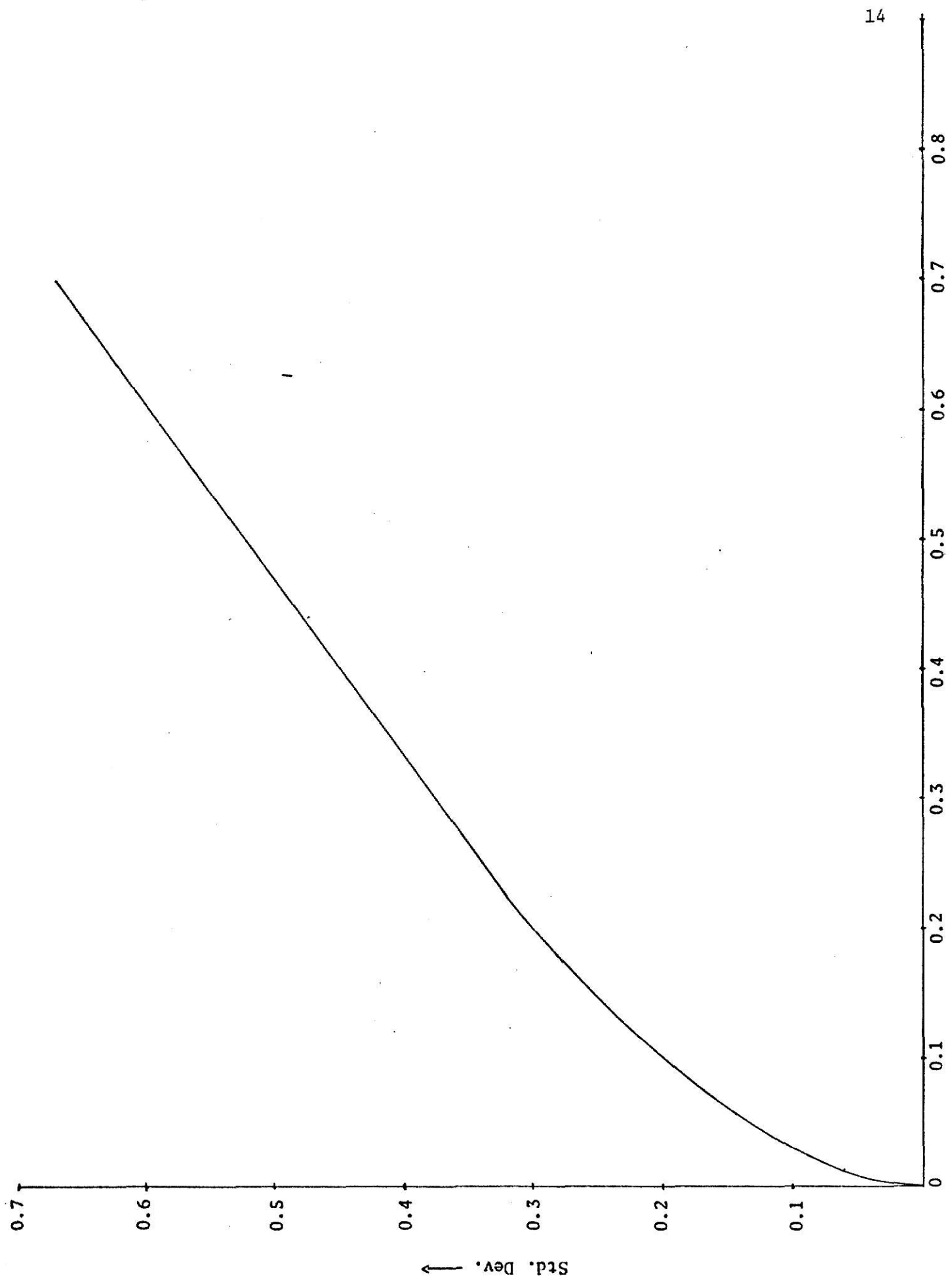
$$\text{ERR}(t) = x(t) - \hat{x}(t)$$

Two smoothed statistics were obtained from this forecast error.

$$\text{Smoothed Error: } \text{S.S.E.}(t) = (1-\alpha) \text{S.S.E.}(t-1) + \alpha \text{ERR}(t)$$

Smoothed Mean Absolute Deviation

$$\text{S.M.A.D.}(t) = (1-\alpha) \text{S.M.A.D.}(t-1) + \alpha |\text{ERR}(t)|$$

Figure (2.2) Variation of Standard Deviation of the Tracking Signal Distribution with α .

From these two statistics the tracking signal was evaluated.

$$\text{Tracking signal} = \frac{\text{S.S.E.}}{\text{S.M.A.D.}}$$

The tracking signal ranges from -1 to +1. This range was divided into 80 equal intervals. 20,000 values of the tracking signal were generated. The frequency plot of the tracking signal revealed a great fluctuation in frequency at the peak of the distribution. The fluctuation in the frequency was smoothed out to a great extent by increasing the number of simulations from 20,000 to 100,000. 20,000 simulations for each of 9 different values of α (a total of 180,000 simulations) took a system time of 0.083 hours in Fortran H level with an optimization level of 2. The cost was \$17.14. For 100,000 simulations with each of 9 different smoothing constants (a total of 900,000) 0.342 hours and \$70.24 were required. If the number of simulations is further increased. The system time will increase accordingly.

The tracking signal mean was approximately zero but the standard deviation varied with the smoothing constant. This variation is illustrated in figure (22). The range of the beta distribution is 0 to 1 and that of the tracking signal distribution is -1 to +1. To map one distribution on the other, a linear transformation is necessary. The transformation is given by:

$$X_{\beta} = \frac{X_T + 1}{2}$$

where X_{β} and X_T are points on the beta and the tracking signal distribution. Experiments were carried out with smoothing constants ranging from 0.1 to

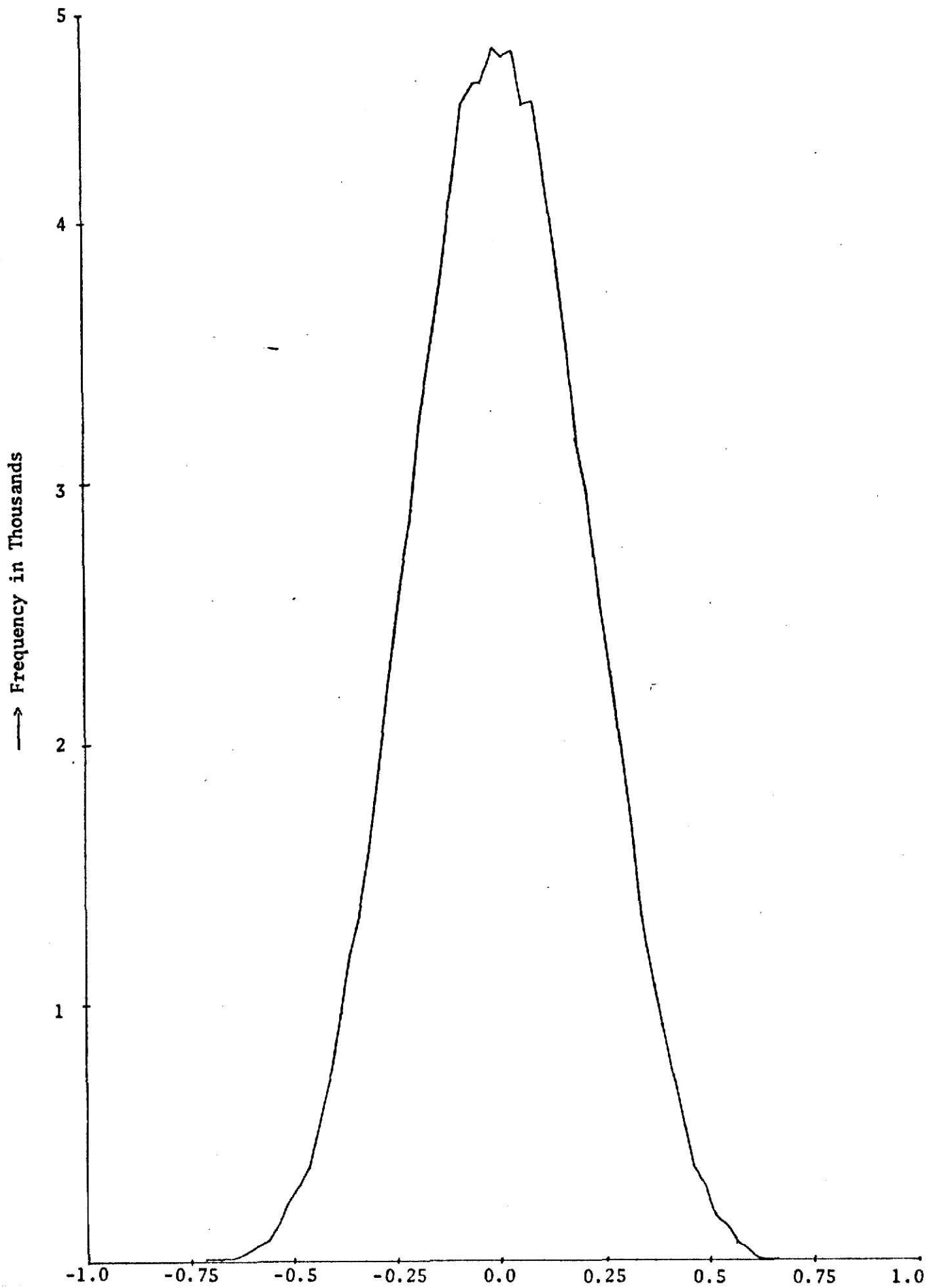


Figure (2.3) The tracking Signal Distribution for an α of 0.1

0.25. This is the usual range of the smoothing constant used in any normal forecasting system.

2.2.2 Details of Experiment with α of 0.1

The tracking signal distribution for α of 0.1 is unimodal and symmetrical. This is depicted in figure [23]. This indicates that for the purpose of approximation, a beta distribution with equal parameters greater than unity should be tried. For a closer approximation, the mean and the standard deviation of the tracking signal distribution should be equal to those of the approximating distribution. Consider a beta distribution $B(m,n)$, with parameters m and n respectively. The mean and variance of this distribution in terms of its parameters is given by [4].

$$\text{Mean} = m / (m+n)$$

$$\text{Variance} = \frac{m \cdot n}{[(m+n+1) \cdot (m+n)^2]}$$

For equal parameters (i.e. $m=n$) the mean of beta distribution is 0.5 and the variance is:

$$\begin{aligned} \text{Variance} &= \frac{m^2}{[(2m+1) \cdot (2m)^2]} \\ &= \frac{1}{4(2m+1)} \end{aligned} \tag{2.1}$$

As the mean of the tracking signal distribution is approximately 0.5 on the transformed scale, only the correspondence of the variance is to be

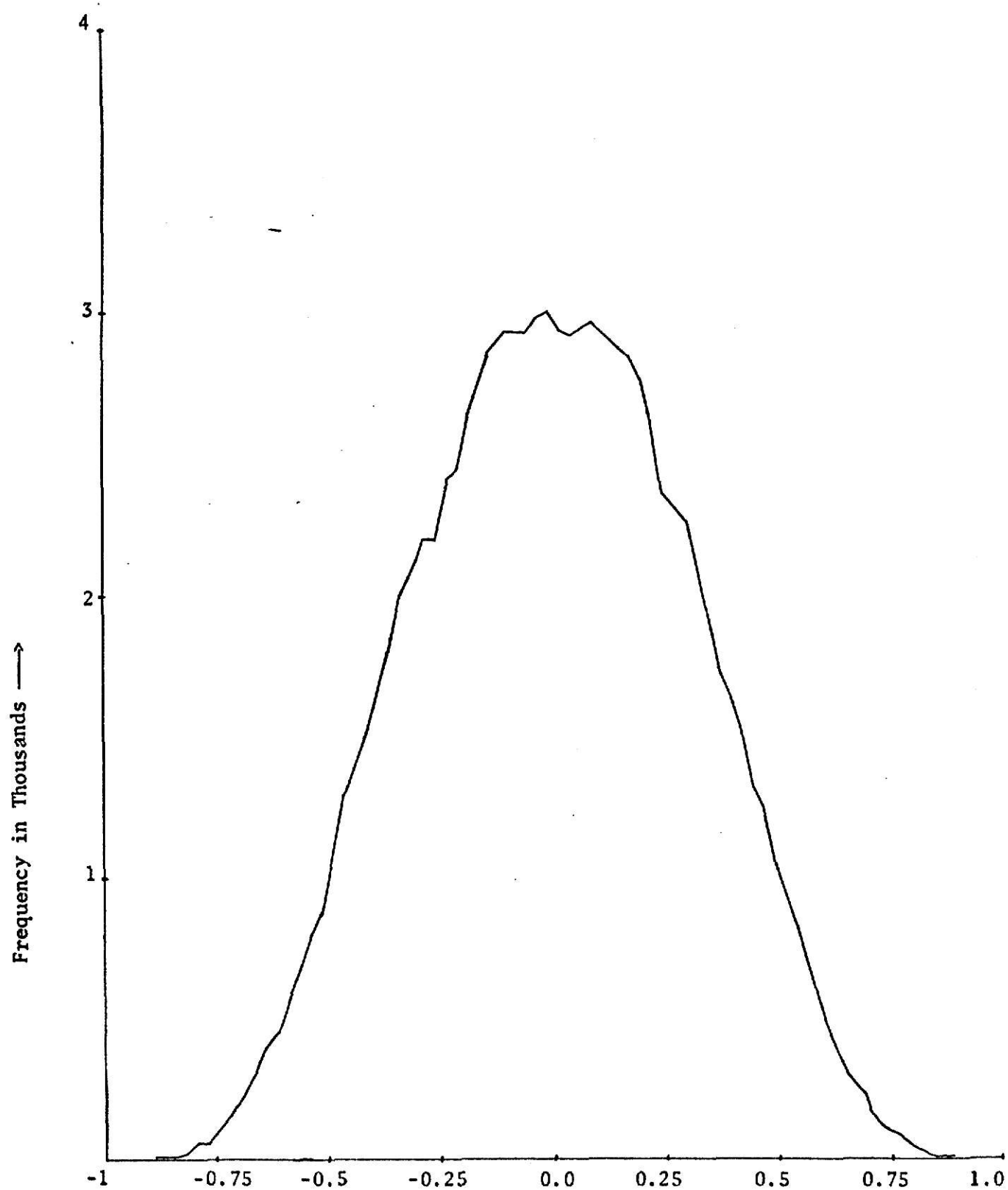


Figure (2.4) The Tracking Signal Distribution for an α of 0.2

considered. The standard deviation of the tracking signal is 0.1027 on the transformed scale. Equating this with the above expression for variance we have:

$$(0.1027)^2 = \frac{1}{4(2m+1)}$$

Solving the above equation, the parameters of the approximating distribution are $m = n = 11.35$. The probabilities of observations falling in 80 equal intervals were obtained for the beta distribution for the I.B.M. scientific subroutine package program NDTR. From these probabilities a theoretical frequency distribution for the tracking signal was derived. Knowing the theoretical and the observed frequencies for the tracking signal, a chi-square test and a Kolmogorov-Smirnov test were applied for the goodness of fit. A chi-square value of 79.44 was obtained which is more than the critical value of 73.3. The fit was inadequate at the 5% significance level. However, the fit was adequate by the Kolmogorov-Smirnov test. The value obtained by this test was 0.00179 which is less than critical value of 0.00430 at the 5% significance level.

As the fit was inadequate by one of the tests, the tracking signal distribution could not be approximated satisfactorily with a single beta distribution. The next step was to investigate other values of α namely .2 and .01.

2.2.3 EXPERIMENT WITH α OF 0.2.

The tracking signal distribution for this value of α was a little flat at the peak as illustrated in figure(2.4). At this stage it was difficult

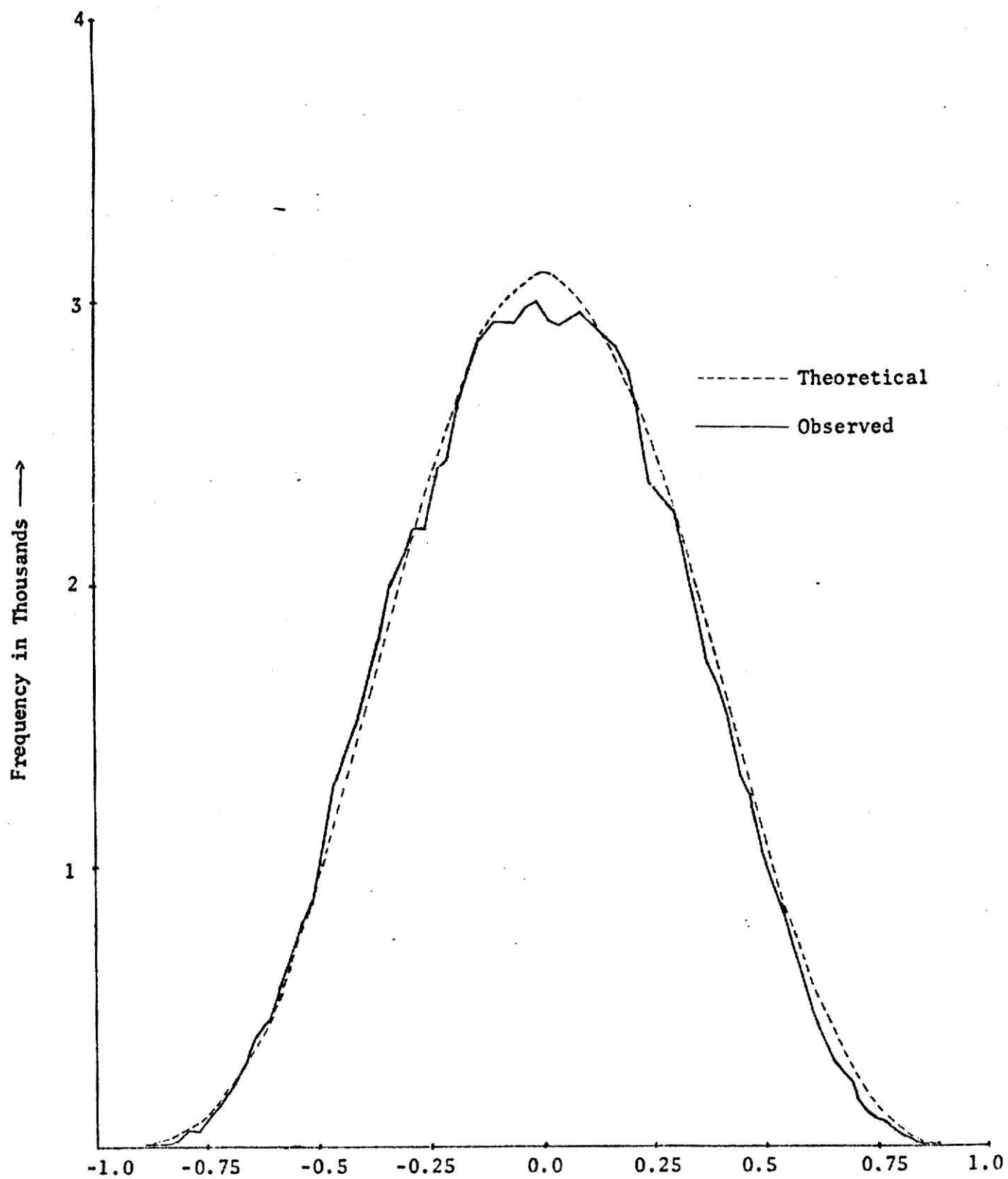


Figure (2.5) Comparison of Observed and Theoretical Tracking Signal Distribution

to say whether this distribution is bimodal. So the first step was to approximate it with a single beta distribution. The frequencies in 80 of the cells were evaluated. These frequencies differed significantly at the peak, from the observed distribution as illustrated in figure (2.5). The next approach was to approximate this tracking signal distribution with some distribution which is flat at peak. This type of distribution could be obtained by combining two beta distributions as illustrated in figure [2.6]. Also, a bimodal distribution could be obtained by such combination of two beta distributions with appropriate parameters.

Consider two beta distributions $B(m,n)$ and $B(n,m)$ with p.d.f's given by:

$$\begin{aligned} B(m,n) &= \frac{\Gamma(m+n)}{\Gamma(m) \Gamma(n)} \cdot x_1^{m-1} (1-x_1)^{n-1} \\ &= f_1(x_1) \end{aligned} \left. \vphantom{\begin{aligned} B(m,n) &= \frac{\Gamma(m+n)}{\Gamma(m) \Gamma(n)} \cdot x_1^{m-1} (1-x_1)^{n-1} \end{aligned}} \right\} , 0 < x_1 < 1$$

and

$$\begin{aligned} B(n,m) &= \frac{\Gamma(n+m)}{\Gamma(n) \Gamma(m)} x_2^{n-1} (1-x_2)^{m-1} \\ &= f_2(x_2) \end{aligned} \left. \vphantom{\begin{aligned} B(n,m) &= \frac{\Gamma(n+m)}{\Gamma(n) \Gamma(m)} x_2^{n-1} (1-x_2)^{m-1} \end{aligned}} \right\} , 0 < x_2 < 1$$

At any point x on the range of these distributions, it is assumed that the ordinate $f(x)$ of the resultant distribution is

$$f(x) = 1/2 [f_1(x) + f_2(x)], \quad 0 < x < 1 \quad (22)$$

or

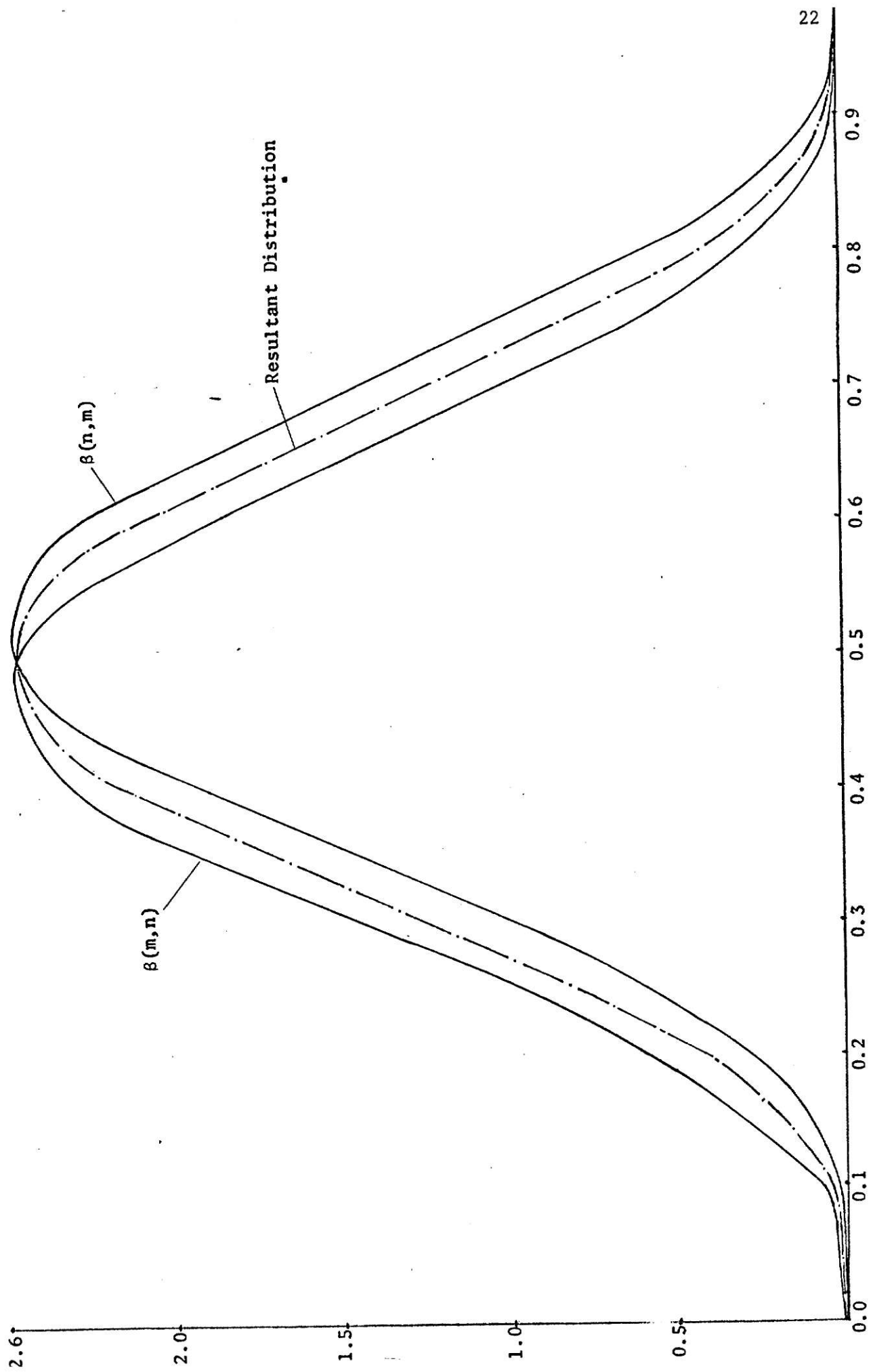


Figure (2.6) Resultant Distribution Obtained by Combining Two Beta Distributions.

$$\int_0^1 f(x) dx = 1/2 \left[\int_0^1 f_1(x) dx + \int_0^1 f_2(x) dx \right], \quad 0 < x < 1.$$

As $\int_0^1 f_1(x) dx = \int_0^1 f_2(x) dx = 1$ the area under the resultant distribution is also equal to one. Further, from equation (2.2),

$$\int_0^1 xf(x) dx = 1/2 \left[\int_0^1 xf_1(x) dx + \int_0^1 xf_2(x) dx \right]$$

The above equation states that the mean of new distribution is half the sum of means of prior beta distributions. If the mean of the resultant distribution is represented by μ , then:

$$\mu = E(x) = 1/2 [E_1(x) + E_2(x)].$$

Representing the means $E_1(x)$ and $E_2(x)$ in terms of parameters:

$$\mu = 1/2 \left[\frac{m}{m+n} + \frac{n}{m+n} \right] = 0.5$$

The variance σ^2 of the resultant distribution is given by:

$$\begin{aligned} \sigma^2 &= E(x^2) - E^2(x) \\ &= 1/2 \left[\int_0^1 x^2 f_1(x) dx + \int_0^1 x^2 f_2(x) dx \right] - \left\{ 1/2 \left[\int_0^1 x f_1(x) dx + \int_0^1 x f_2(x) dx \right] \right\}^2 \\ &= 1/2 E_1(x^2) + 1/2 E_2(x^2) - \{ 1/2 [E_1(x) + E_2(x)] \}^2 \\ &= 1/2 E_1(x^2) + 1/2 E_2(x^2) - 1/4 E_1^2(x) - 1/4 E_2^2(x) - 1/2 E_1(x) E_2(x) \end{aligned}$$

$$\begin{aligned}
&= 1/2 E_1(x^2) - 1/2 E_1^2(x) + 1/2 E_2(x^2) - 1/2 E_2^2(x) + 1/4 E_1^2(x) \\
&\quad + 1/4 E_2^2(x) - 1/2 E_1(x) E_2(x) \\
&= 1/2 E_1(x^2) - 1/2 E_1^2(x) + 1/2 E_2(x^2) - 1/2 E_2^2(x) \\
&\quad + \{1/2 [E_1(x) - E_2(x)]\}^2 \\
&= 1/2 \sigma_1^2 + 1/2 \sigma_2^2 + [1/2(\mu_1 - \mu_2)]^2
\end{aligned}$$

where

μ_1 and σ_1^2 are the mean and variance of first beta distribution $(\beta(m,n))$,

and

μ_2 , σ_2^2 are mean and variance of the second beta distribution. $(\beta(n,m))$.

Substituting the values of means and variances of the two beta distributions in terms of their parameters, the variance of the resultant distribution is given by:

$$\begin{aligned}
\sigma^2 &= 1/2 \left[\frac{mn}{(m+n+1)(m+n)^2} \right] + 1/2 \left[\frac{nm}{(n+m+1)(n+m)^2} \right] + 1/4 \left[\frac{m}{n+m} - \frac{n}{m+n} \right]^2 \\
&= \frac{mn}{(m+n+1)(m+n)^2} + 1/4 \left[\frac{m-n}{m+n} \right]^2
\end{aligned}$$

Rearranging,

$$\sigma^2 = \frac{(m+n) + (m-n)^2}{4(m+n)(m+n+1)} \quad (2.3)$$

After transforming, if the variance of the tracking signal distribution is equated with equation (2.3). The parameters of the approximating distribution could be found. But the above equation contains two unknowns m and n , as such the parameters of the approximating distribution could not be found easily. To obtain the parameters of the approximating distribution the following approach was adopted. Let the variance of the tracking signal distribution be denoted by Y^2 . Then,

$$Y^2 = \frac{(m+n) + (m-n)^2}{4(m+n)(m+n+1)}$$

or

$$(4Y-1)n^2 + (4Y^2+8Y^2m+2m-1)n + 4Y^2m^2 - m^2 + 4mY^2 - m = 0 \quad (2.4)$$

The above equation has the form

$$An^2 + Bn + C = 0$$

where

$$A = 4Y^2 - 1$$

$$B = 4Y^2 + 8Y^2m + 2m - 1$$

and

$$C = 4Y^2m^2 - m^2 + 4mY^2 - m$$

For a particular value of Y and m , n will have two values n_1 and n_2 . The roots of equation (2.4) were evaluated with different values of m and a

m	n_1	n_2	
4.939	5.416	5.416	← Point c
5.000	5.191	5.787	
5.100	5.119	6.097	
5.200	5.099	6.357	
5.300	5.101	6.595	
5.400	5.116	6.820	
5.500	5.139	7.036	
5.600	5.168	7.247	
5.700	5.202	7.452	
5.800	5.239	7.655	
5.900	5.279	7.854	
6.000	5.322	8.050	
6.100	5.367	8.245	

Table (2.1) Two Values of n Corresponding to one Value of m by Solving Quadratic Equation

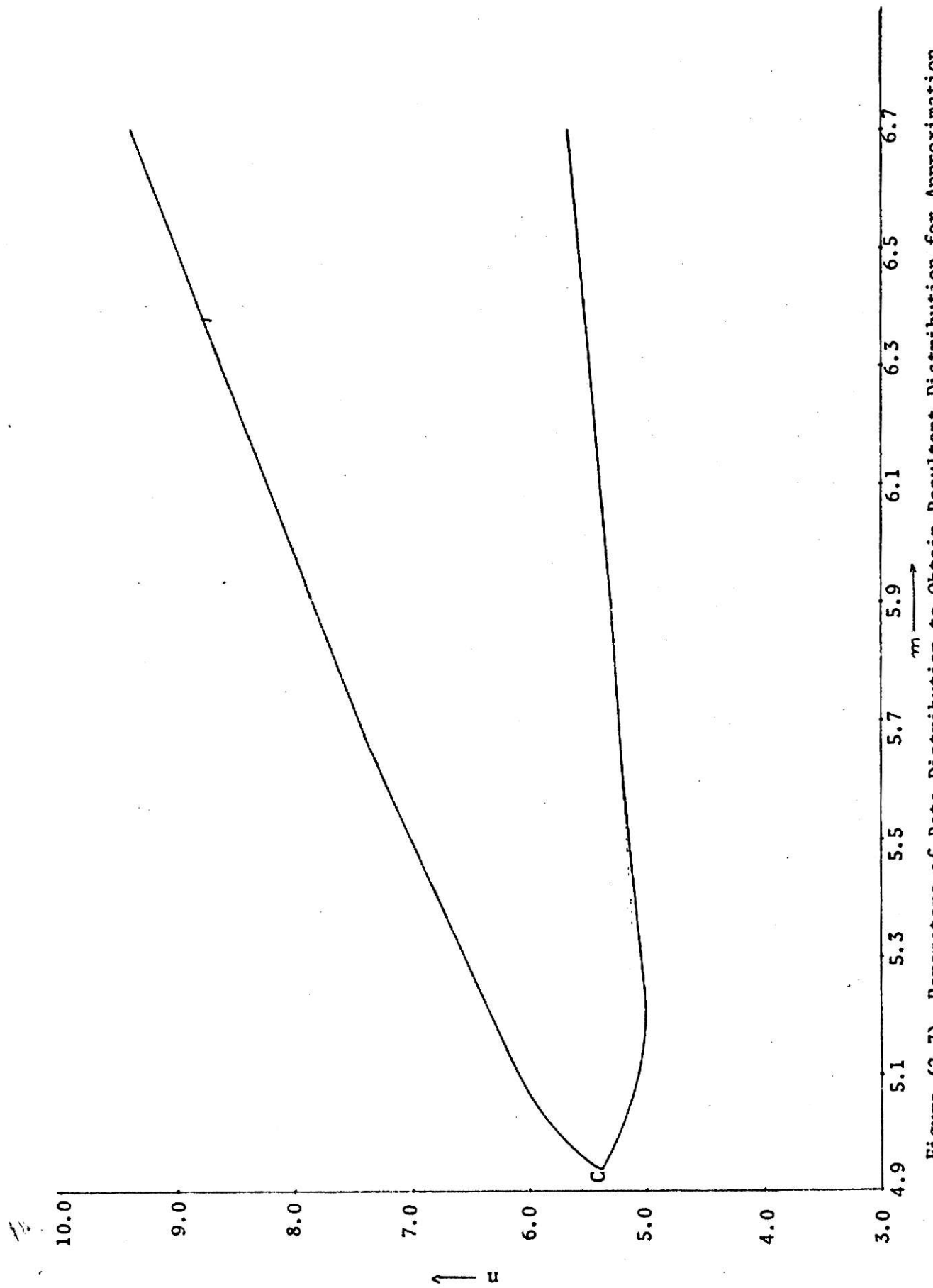


Figure (2.7) Parameters of Beta Distribution to Obtain Resultant Distribution for Approximation

fixed value of Y , the standard deviation of the tracking signal distribution. They are tabulated in Table [2.1]. A graph was plotted between different values of m and the corresponding two values of n . This is illustrated in figure [2.7]. Equation [2.4] is quadratic in n and when $B^2 = 4AC$ the two values n_1 and n_2 for a particular value of m will be equal. This is illustrated by point C in figure (2.7). Theoretical frequency distributions were obtained for various pairs of parameters. These frequencies were compared with the actual frequencies of the tracking signal. A chi-square test was applied to test the goodness of fit. Table (2.2) shows the chi-square values with different pairs of parameters. It could be observed that the chi-square value is a minimum for point C (figure (2.7)). In other words the distribution obtained by combining appropriately two beta distributions corresponding to point C was closest approximating distribution. For the tracking signal distribution. Further, the standard duration of the distribution was 0.150045 as compared with 0.15005 of the observed tracking signal distribution. The standard deviation of the closest simple beta distribution was 0.150119. Even the minimum chi-square value exceeded the critical value of 100.70 at the 5% significance level. This shows that the fit is inadequate and the tracking signal distribution cannot be approximated with the resultant distribution obtained by combining two beta distribution. This was confirmed by the Kolmogorov Smirnov test carried out for point C in figure (2.7). The computed value was .00681 which exceeded the critical value of .0043 at 5% significance level. As this approach failed with higher values of the smoothing constant too, it was tried with smoothing constants lower than 0.1.

m	n	Chi-Square Value	← Point c
4.939	5.416	205.9	
5.00	5.191	213.3	
5.00	5.786	215.23	
5.10	5.119	233.5	
5.10	6.097	227.7	
5.20	5.099	259.1	
5.20	6.357	240.65	
5.30	5.101	290.8	
5.30	6.595	254.6	
5.40	5.116	327.0	
5.40	6.820	270.59	

Table (2.2) Parameters of the Beta Distribution and the Corresponding Chi-Square Values

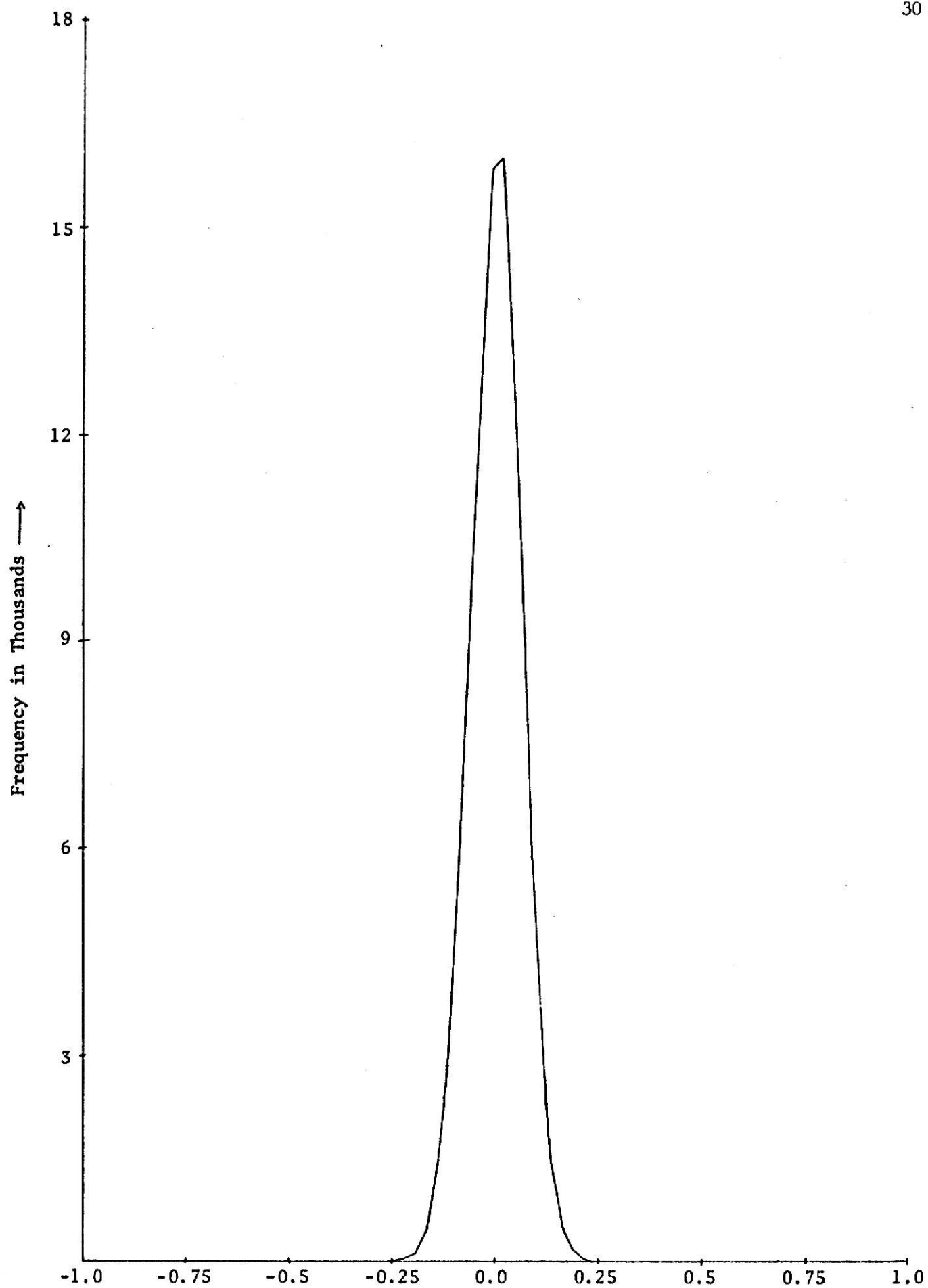


Figure (2.8) The Tracking Signal Distribution for an α of 0.01

2.2.4 EXPERIMENT WITH α OF 0.01

Figure [2.8] illustrates the tracking signal distribution for α of 0.01. It is unimodal and symmetrical with a standard deviation of 0.0306 on the transformed scale. The approach adopted for finding the parameters of the approximating beta distribution, was same as that for 0.1. The parameters of the approximating distribution were obtained from the equation

$$\sigma^2 = \frac{1}{4(2m+1)}$$

with the calculated parameters a theoretical frequency distribution was derived. These frequencies were compared with the observed frequencies for the goodness of fit. The fit was inadequate. The chi-square value was 162.27 as compared with critical value of 32.70 for a 5% significance level. The value obtained by the Kolmogorov Smirnov test was .00479 which exceeded critical value of 0.00473 at the 5% significance level.

2.3 CONCLUSION FROM THE EXPERIMENTAL WORK

From these three experiments it can be concluded that the tracking signal distribution for a normal range of the smoothing constant cannot be approximated adequately with a single beta distribution or a combined beta distribution.

CHAPTER III

THE TRACKING SIGNAL LIMITS BY COMPUTER SIMULATION

When the first approach failed to evaluate the limiting values of the tracking signal, limits were proposed by simulation. Figure [3.1] shows the frequency distribution of the tracking signal for α of 0.1. For illustration let the confidence interval for the tracking signal be 95%. Referring to figure [3.1], one is interested in evaluating values K_1 and K_2 such that 95 percent of the tracking signals lie between K_1 and K_2 . Further, a 95% confidence limits on the tracking signal means that without any significant change in the process level, one value out of 20, may exceed the limiting values K_1 or K_2 . These limiting values may be evaluated separately. To evaluate K_1 the cumulative frequency of the tracking signal for first 40 intervals, corresponding to range of -1 to 0 were plotted against the tracking signal magnitude. This is illustrated in figure [3.2]. 100,000 observations of the tracking signal were simulated. For 95% confidence, 2.5% of the tracking signals will lie between limiting value K_1 and -1. From figure [3.2], the limiting value K_1 is read directly on the X axis. Corresponding to a cumulative frequency of 2500 on Y axis. A similar procedure was carried out to obtain the limiting value K_2 of the tracking signal lying between 0 and 1 from figure [3.3]. It could be observed that the frequency distribution of the tracking signal is approximately symmetrical about zero. The limits K_1 and K_2 , obtained above will be nearly equal in magnitude but opposite in sign. So instead of evaluating two limiting values K_1 and K_2 separately a value K could be evaluated such that the absolute

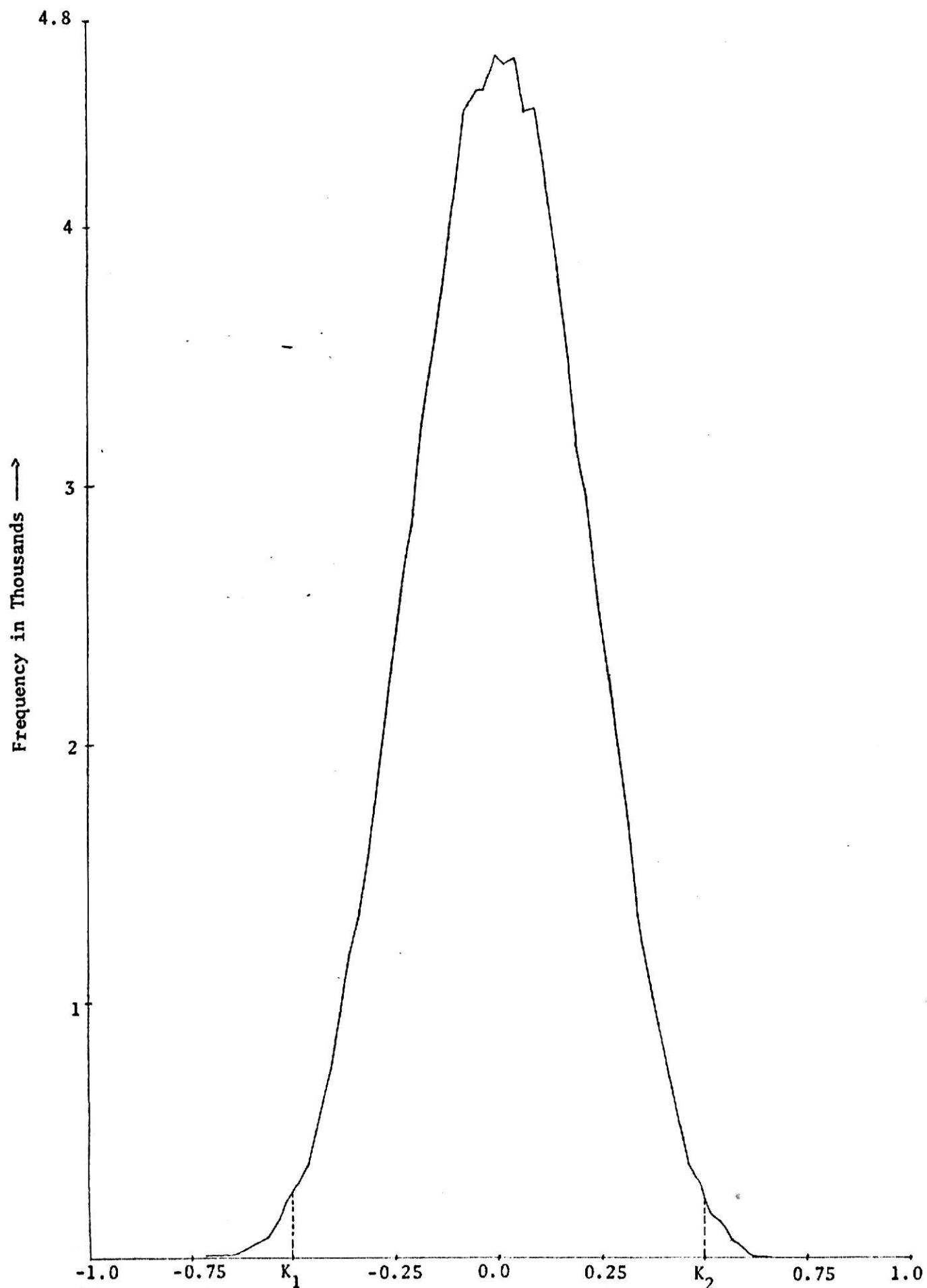


Figure (3.1) The Tracking Signal Distribution from α of 0.1, Depicting Limiting

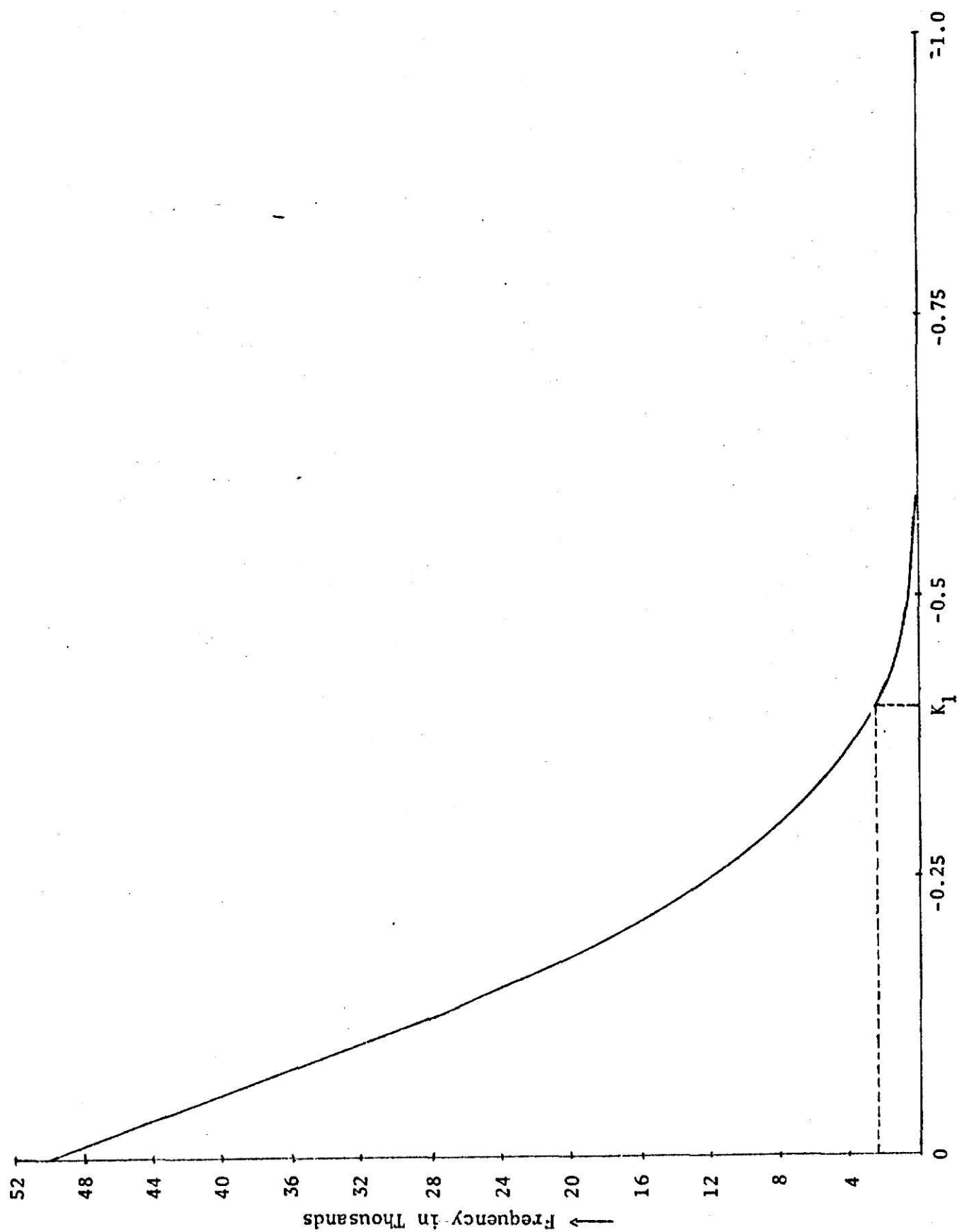


Figure (3.2) Cumulative Frequency Plot for First 40 Cells.

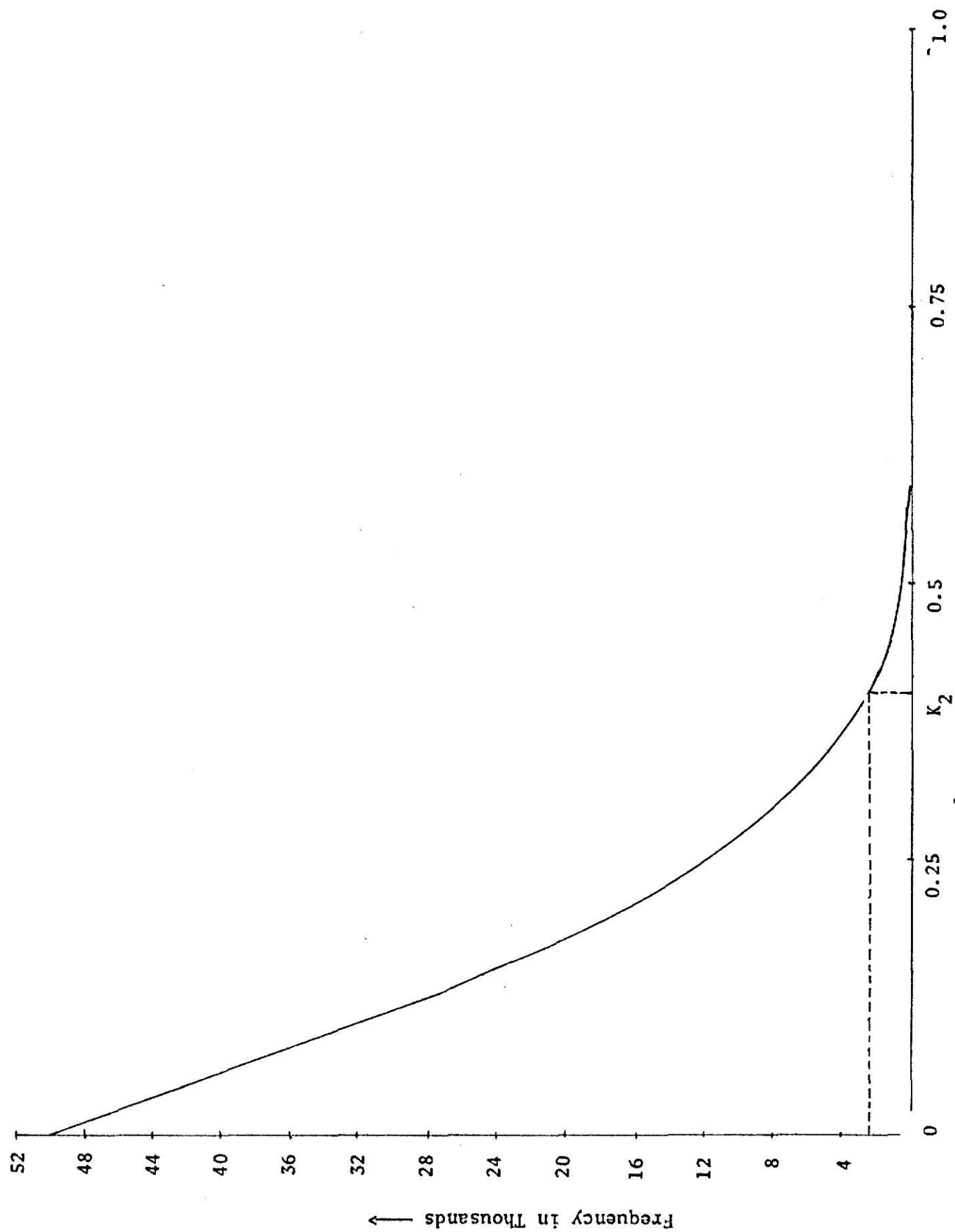


Figure (3.3) Cumulative Frequency Plot for Latter 40 Cells.

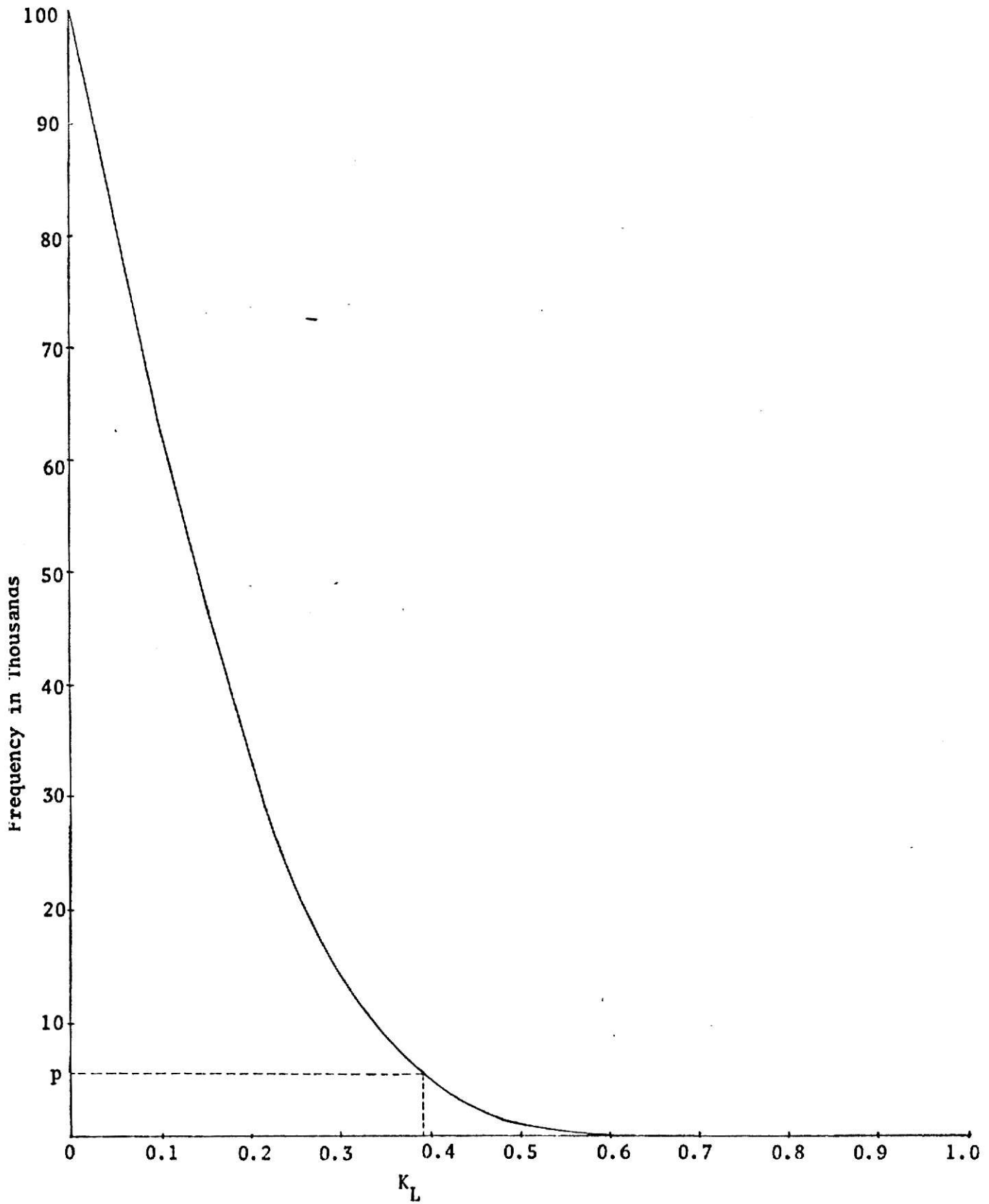


Figure (3.4) Cumulative Frequency Plot for Folded Tracking Signal Distribution

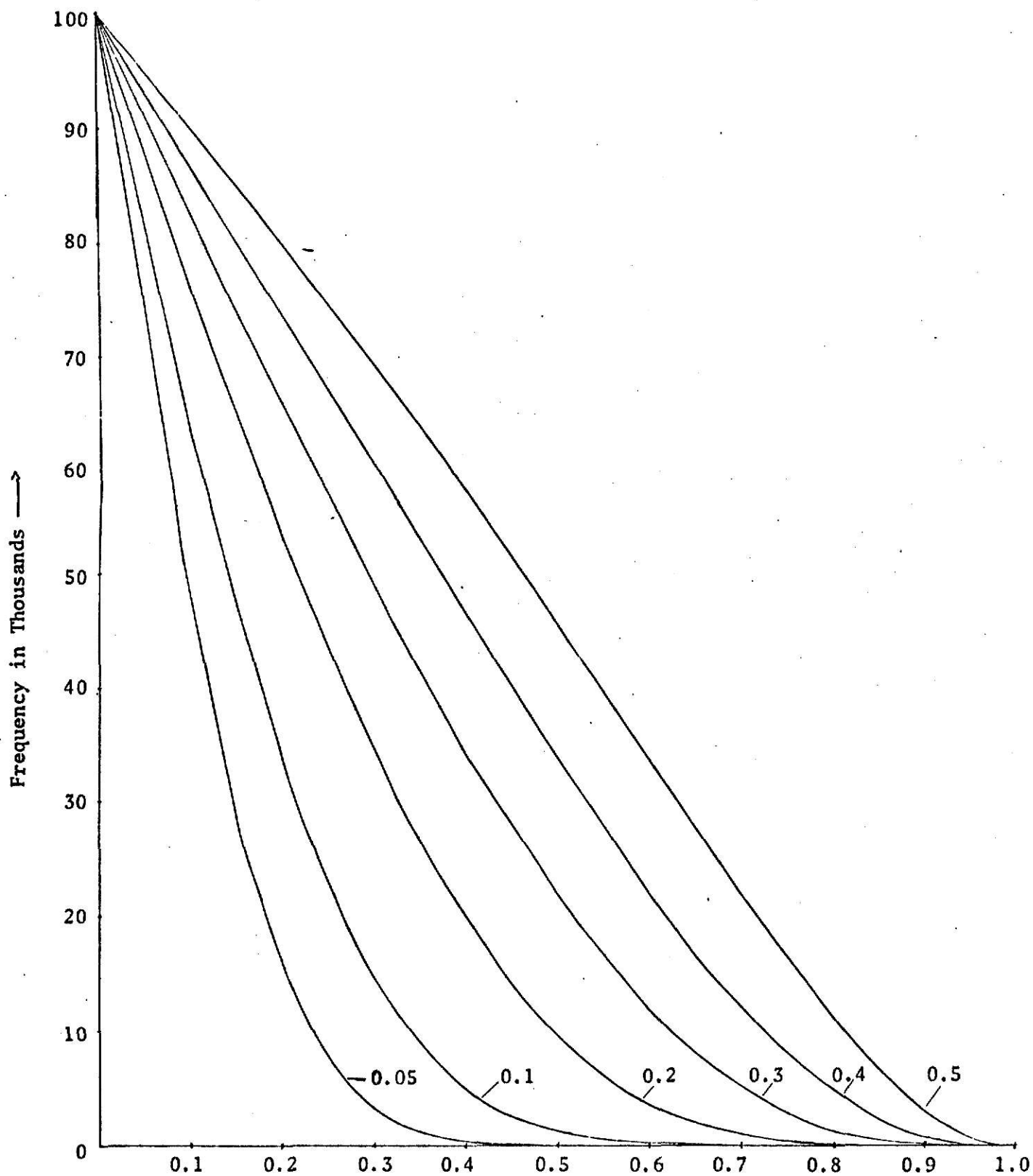


Figure (3.5) Cumulative Frequency Plots for Different Smoothing Constants.

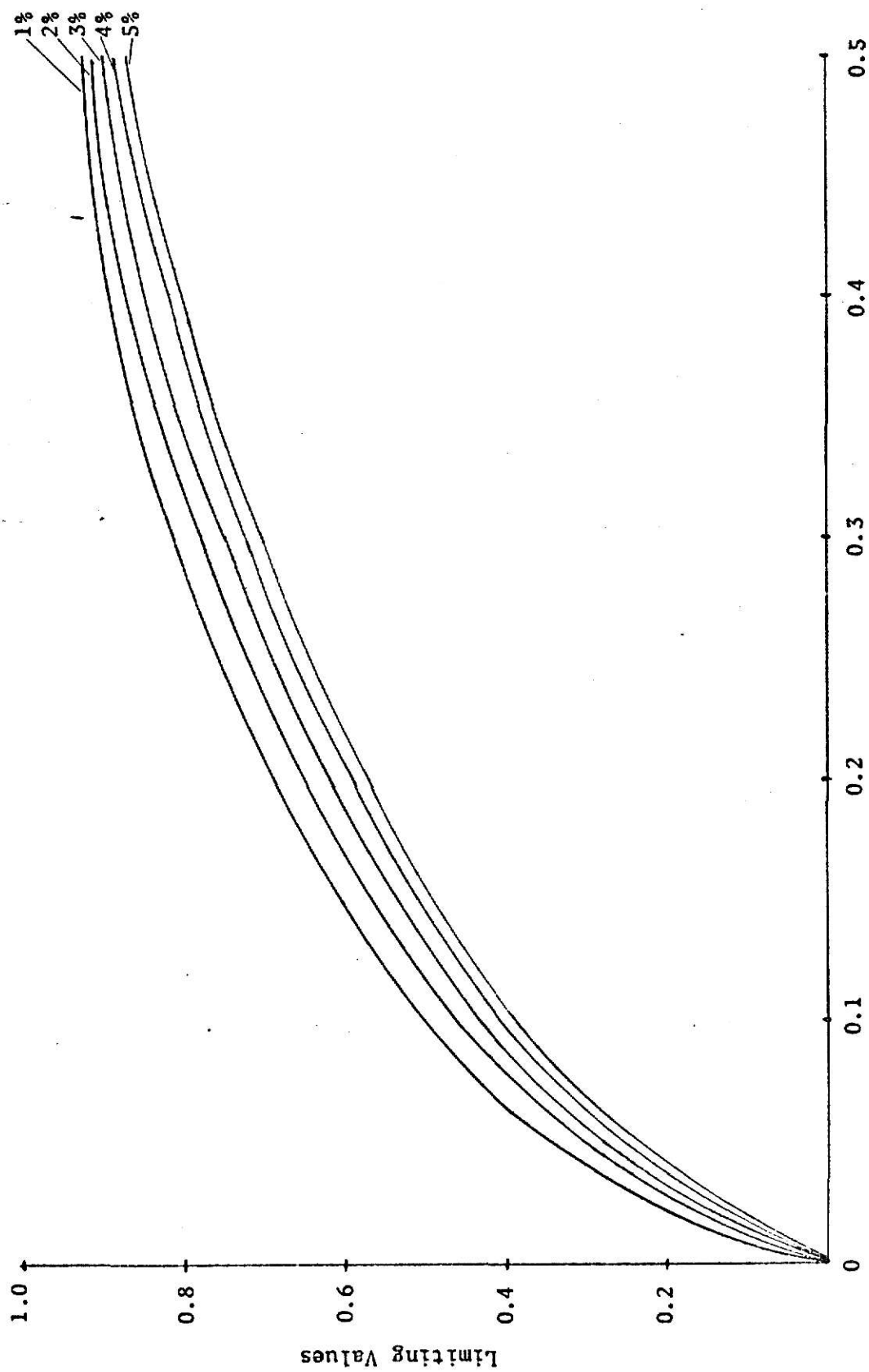


Figure (3.6) Limiting Values of the Tracking Signal for Various Smoothing Constants and Significance Levels.

Significance Level	Smoothing Constant α					
	0.05	0.1	0.2	0.3	0.4	0.5
1	0.360	0.508	0.690	0.810	0.890	0.925
2	0.325	0.468	0.647	0.770	0.864	0.918
3	0.306	0.438	0.618	0.746	0.835	0.900
4	0.290	0.415	0.590	0.724	0.820	0.885
5	0.278	0.400	0.570	0.703	0.800	0.872
10	0.235	0.342	0.497	0.625	0.725	0.815
15	0.205	0.300	0.444	0.570	0.670	0.765
20	0.185	0.270	0.402	0.520	0.620	0.720
30	0.148	0.219	0.330	0.436	0.534	0.634

Table (3.1) Limiting Values of the Tracking Signal

value of K represents the limiting values of the tracking signal. For this purpose, the tracking signal distribution was folded about zero. The tracking signal which was classified into 80 equal intervals previously was reclassified into 40 equal intervals. The frequencies in these 40 intervals were approximately twice as much as those in the unfolded distribution. Cumulative frequencies in each interval were calculated. Effectively, the cumulative frequencies were plotted against the absolute values of the tracking signal. For α of 0.1, this curve is depicted in figure [3.4]. Such plots were obtained for the smoothing constants varying from 0.05 to 0.5. This is depicted in figure [3.5]. From figure [3.5], the limiting values of the tracking signal were evaluated for different smoothing constants and for various levels of significance. These limiting values are tabulated in table [3.1]. For illustration, the frequency corresponding to point P on the Y axis of figure [3.4] is five percent of the total frequency. The corresponding value K_L on the X axis of this graph gives the limiting value of the tracking signal for α of 0.1 and for 5% significance.

A graph was next plotted between the limiting values and the corresponding significance level, for different smoothing constants figure [3.6] from this figure one can find the limiting values of the tracking signal for any level of confidence and for any smoothing constant included in the graph.

The entries of this table are approximately the same as proposed by Batty. However, the details of simulation were not explained explicitly by Batty. In particular there was no indication as to the number of observations generated, hence the reliability of the limits.

CHAPTER IV

RESPONSE OF THE TRACKING SIGNAL TO PROCESS CHANGE

In this section, the behavior of the tracking signal to a process change has been investigated. Consider a constant process, which initially has a mean of a_1 . At a certain time T_1 , let the process level change to a new mean of a_2 . Mathematically, the process can be represented as:

$$\xi_t = a_1 \quad \text{for } t < T_1$$

and

$$\xi_t = a_2 \quad \text{for } t \geq T_1$$

Effectively, at time T_1 a step increase of $(a_2 - a_1)$ has taken place in the process level. Such a situation is illustrated in figure (4.1).

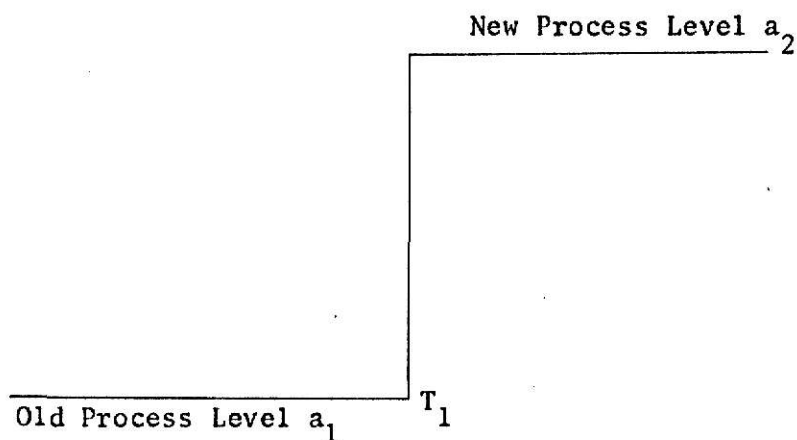


Figure (4.1) Step increase in the process level

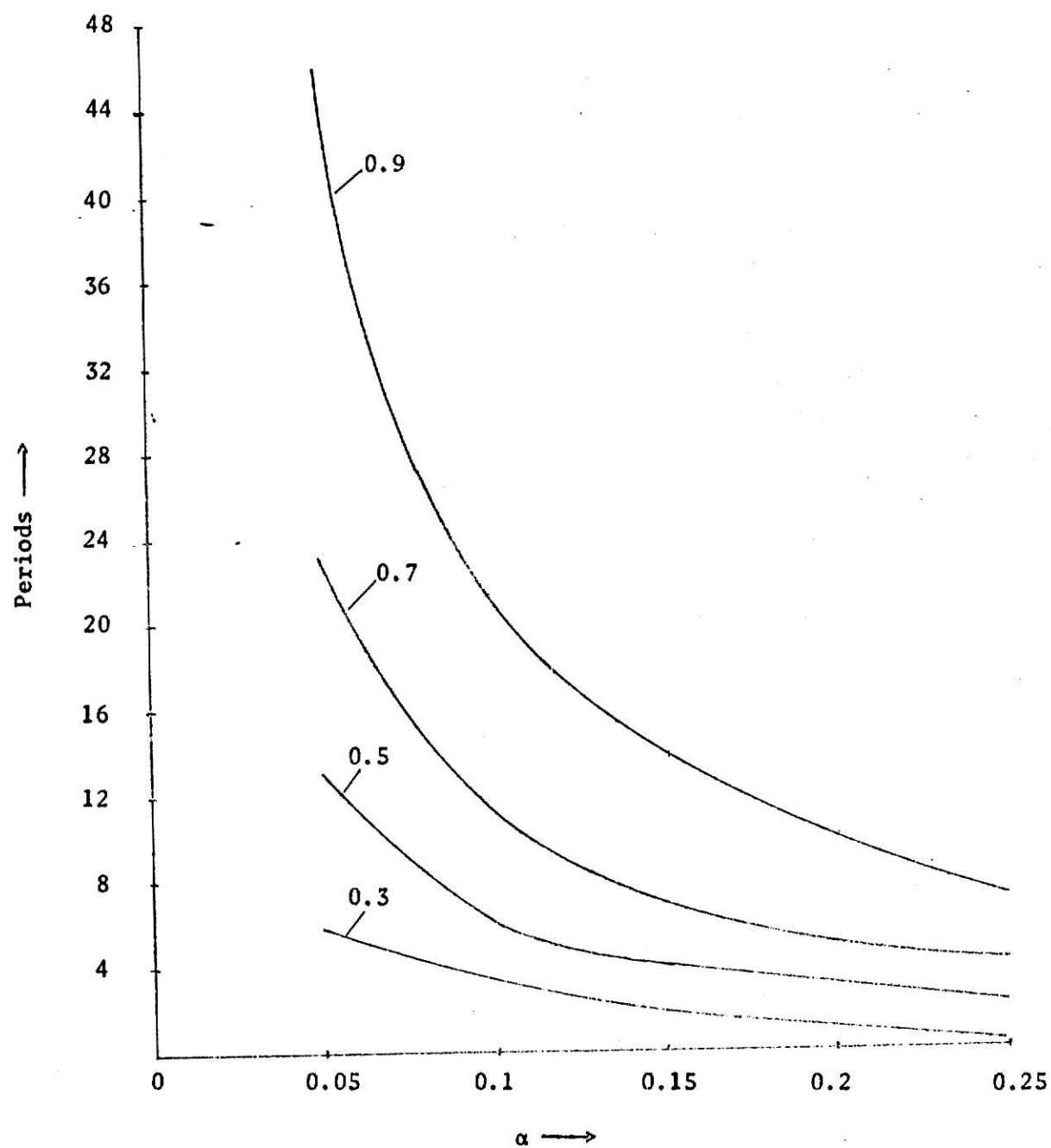
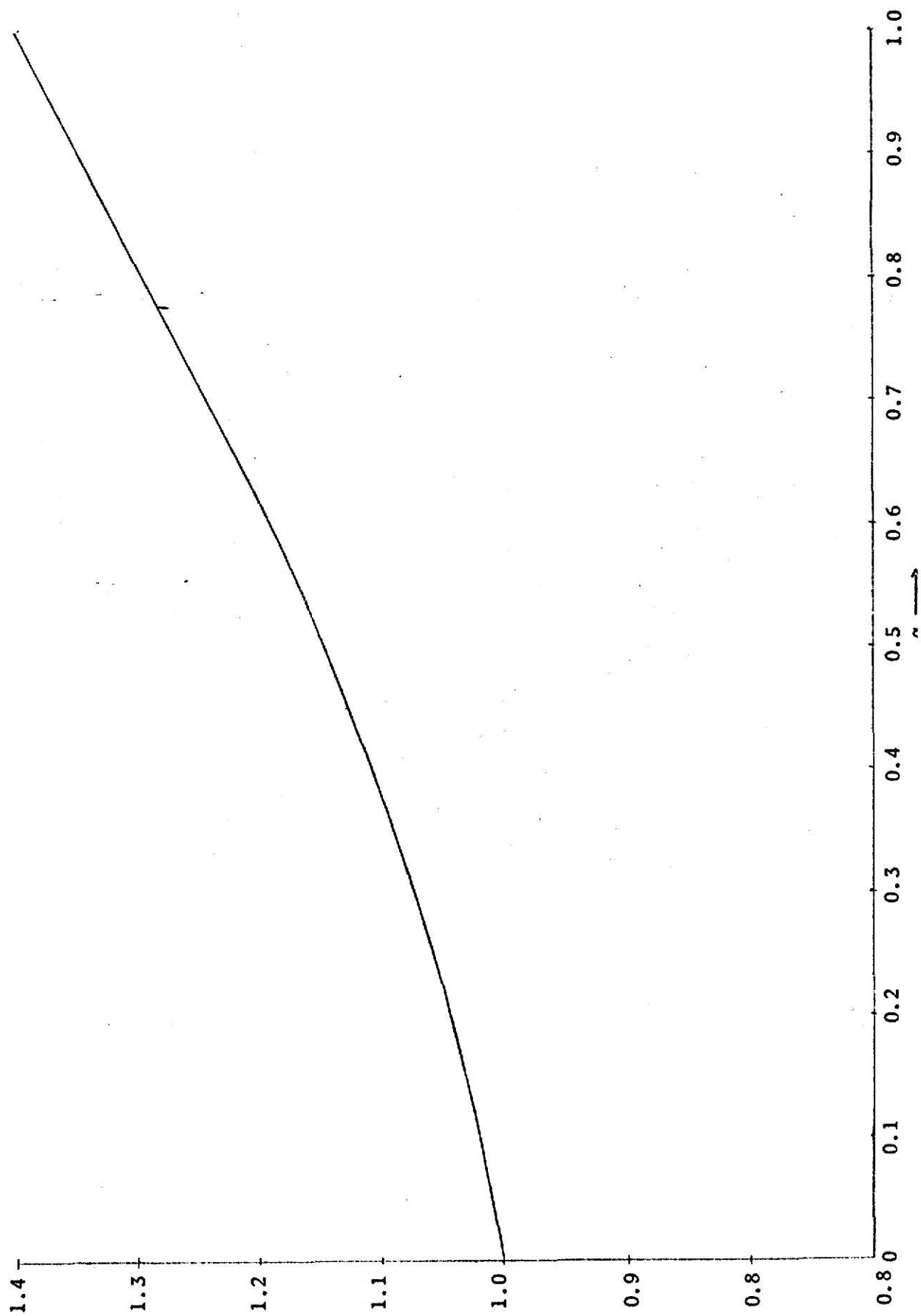


Figure (4.2) Effect of Smoothing Constant on the Time Required to Respond to a Fraction of Step Input.



Fraction of the Step 'f'	Smoothing Constant				
	0.05	0.1	0.15	0.2	0.25
0.1	2	1	-	-	-
0.3	6	3	2	-	-
0.5	13	6	4	3	2
0.7	23	11	7	5	4
0.9	46	21	14	10	8

Table (4.1) No. of Periods Required to Achieve a Fraction 'f' of Step for Various Values of the Smoothing Constants

As the forecasting system uses exponential smoothing to predict future observations, the forecasts will constantly lag the observations. According to Brown [1], using exponential smoothing, the predicted values can never attain the new level in a finite period. However, it can achieve a very high fraction of the step ($a_2 - a_1$) in a finite period. Brown pp. 114, has developed a relation which evaluates the number of periods required to attain any fraction of the step, for various values of the smoothing constant.

$$n = \frac{\log (1-f)}{\log \beta} - 1$$

where n = number of periods required

f = the fraction of the step

β = discount factor = $(1-\alpha)$.

For various values of f and α , the number of periods required, were evaluated using the above relation. The results are tabulated in Table (4.1). Figure (4.2) illustrates relation between α , f and small periods required. From this figure it can be said that a high value of the smoothing constant is desirable for any forecasting system, for a rapid recovery from process changes. Higher values of the smoothing constant will lead to increased magnitude of the forecast errors. Figure (4.3) shows the effect of the smoothing constant on forecast accuracy. Small values of α lead to accurate forecasts but the forecasting system takes a longer time to recover from the process change. Thus, these relative advantages and disadvantages are to be suitably weighed while selecting a smoothing constant. Figure (4.2) also helps in investigating the sensitivity of

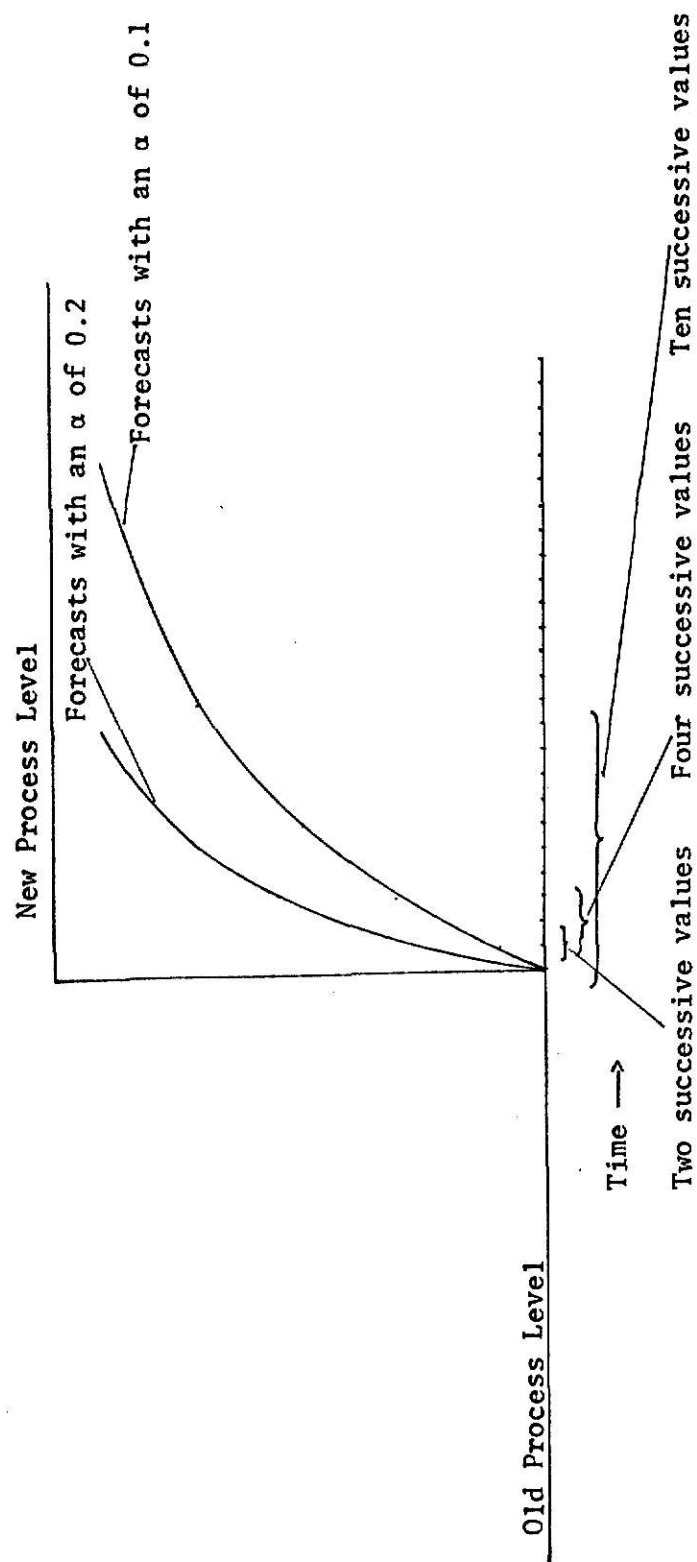


Figure (4.4) Illustration of detection criteria

the tracking signal to process changes. It can be seen from this figure, for an α of 0.1, the number of periods required to achieve 90% of the step is 21. The tracking signal should give an indication of the process change at a very early stage. If it does not give an indication, the system will adjust to the new level by itself. For example after 21 periods the system will more or less achieve the new process level. From the sensitivity point of view this is the maximum period one can allow for the tracking signal to give an indication of the process change. It is desired to detect the process change before the system achieves 20 to 30 percent of the step. The sooner the detection, the more effective the tracking signal.

The sensitivity of the tracking signal was studied by simulation of a constant process. After the starting conditions were discounted, a step in the process level was introduced. The magnitude of the step varied from 2.5 to 25 percent of the process mean of 10. A change in the process was confirmed by formulating different detection criteria. For all criteria and all values of α , the control limits were set at a level corresponding to a 99 per cent confidence. The detection criteria were essentially based on examining a few tracking signals after incorporating a step in the process level. Referring to figure (4.4) the criteria for detecting process change were:

- a) If one value of the tracking signal in two successive values exceeded the limiting value
- b) If one value of the tracking signal in 4 successive values exceeded the limiting value

- c) If one value of the tracking signal in 10 successive values exceeded the limiting values
- d) If any two consecutive values out of ten successive values exceeded the limiting value. These detection systems were simulated 1000 times. The probability of detecting a process change was evaluated. The results are tabulated in Table (4.2 to 4.5). Figures (4.5 to 4.8) depict the relation between step size and probability of detection for various detection criteria.

RESULTS AND DISCUSSION

The results from the first detection system revealed that the probability of detecting a process change is low. Even with a 25 percent change in the process mean, this system gives a 0.171 probability of detecting a process change for an α of 0.05. The probability of detecting increases with the smoothing constant. The probabilities obtained with the second detection system are a little higher than those obtained by first detection system. For an α of 0.05 and for a 25 percent change in the process mean, a detection probability of 0.643 is attained. Based on the second detection system it can be concluded that the first detection system is less effective in detecting process changes.

The third and fourth detection systems have approximately the same probabilities of detection for higher magnitudes of the step. In both systems of an α of 0.05 and a 25 percent change in the process mean, the probability of detection is 1. However, for smaller magnitudes of the step, the third detection system has a higher probability of detection. As compared with first two detection systems, the probability of detection decreased with increased values of α . This reveals that with higher values of α , the forecasting system often adjusts to the new situation by itself. For all values of α and for all detection systems the probability of detection corresponding to a step of zero percent is referred to false alarms given by the tracking signal.

When the adopted detection criteria is one of these four, these probability tables (4.2 to 4.5) will help in deciding whether the system needs updating. However, the decision of updating the system is entirely left to the one in charge of the system. The decision will essentially depend

upon considering the severity of penalties resulting from updating or not updating the system.

The further work in this field can be carried out by investigating various other detection criteria. Another effect which could be studied is the change in detection probabilities that occur when specifying different tracking signal limits at other confidence levels.

Smoothing Constant ' α '	Step Increase in the Process Mean (%)										
	0	2.5	7	7.5	10	1.25	15	17.5	20	22.5	25
0.05	0.012	0.011	0.016	0.025	0.035	0.050	0.057	0.078	0.096	0.126	0.171
0.10	0.019	0.019	0.025	0.025	0.042	0.056	0.081	0.104	0.140	0.189	0.217
0.15	0.015	0.015	0.027	0.036	0.047	0.066	0.103	0.129	0.160	0.211	0.252
0.2	0.022	0.029	0.034	0.046	0.068	0.082	0.112	0.144	0.184	0.236	0.293
0.25	0.021	0.023	0.030	0.043	0.064	0.083	0.117	0.153	0.196	0.242	0.288

Table (4.2) Probabilities of Detecting Process Change by Criteria (a)

Smoothing Constant ' α '	Step Increase in the Process Mean (%)										
	0.0	2.5	5.0	7.5	10.0	12.5	15.0	17.5	20.0	22.5	25.0
0.05	0.015	0.023	0.035	0.062	0.115	0.189	0.271	0.344	0.429	0.537	0.643
0.10	0.026	0.043	0.058	0.098	0.158	0.228	0.338	0.446	0.550	0.666	0.753
0.15	0.031	0.033	0.055	0.093	0.159	0.253	0.358	0.464	0.594	0.704	0.786
0.20	0.040	0.042	0.064	0.112	0.168	0.251	0.353	0.460	0.555	0.651	0.739
0.25	0.026	0.030	0.064	0.102	0.157	0.238	0.321	0.419	0.521	0.614	0.695

Table (4.3) Probability of Detecting A Process Change by Criteria (b)

Smoothing Constant ' α '	Step Increase in the Process Mean (%)										
	0	2.5	5.0	7.5	10.0	12.5	15.0	17.5	20.0	22.5	25.0
0.05	0.044	0.079	0.179	0.372	0.585	0.796	0.923	0.971	0.994	0.999	1.000
0.10	0.056	0.089	0.206	0.391	0.586	0.787	0.906	0.968	0.992	0.999	1.000
0.15	0.069	0.085	0.179	0.343	0.529	0.694	0.834	0.924	0.961	0.987	0.999
0.20	0.074	0.102	0.171	0.300	0.437	0.611	0.742	0.847	0.913	0.952	0.977
0.25	0.082	0.101	0.158	0.260	0.391	0.542	0.673	0.780	0.865	0.905	0.944

Table (4.4) Probability of Detecting a Process Change by Criteria (c)

Smoothing Constant ' α '	Step Increase in the Process Mean (%)										
	0.0	2.5	5.0	7.5	10.0	12.5	15.0	17.5	20.0	22.5	25.0
0.05	0.019	0.042	0.105	0.238	0.462	0.663	0.841	0.935	0.978	0.994	1.000
0.10	0.018	0.040	0.093	0.226	0.408	0.607	0.797	0.914	0.966	0.991	0.998
0.15	0.014	0.043	0.088	0.185	0.337	0.506	0.683	0.806	0.899	0.946	0.983
0.20	0.023	0.039	0.067	0.139	0.248	0.378	0.512	0.662	0.783	0.868	0.923
0.25	0.025	0.027	0.054	0.098	0.179	0.282	0.403	0.542	0.652	0.756	0.827

Table (4.5) Probability of Detecting a Process Change by Criteria (d)

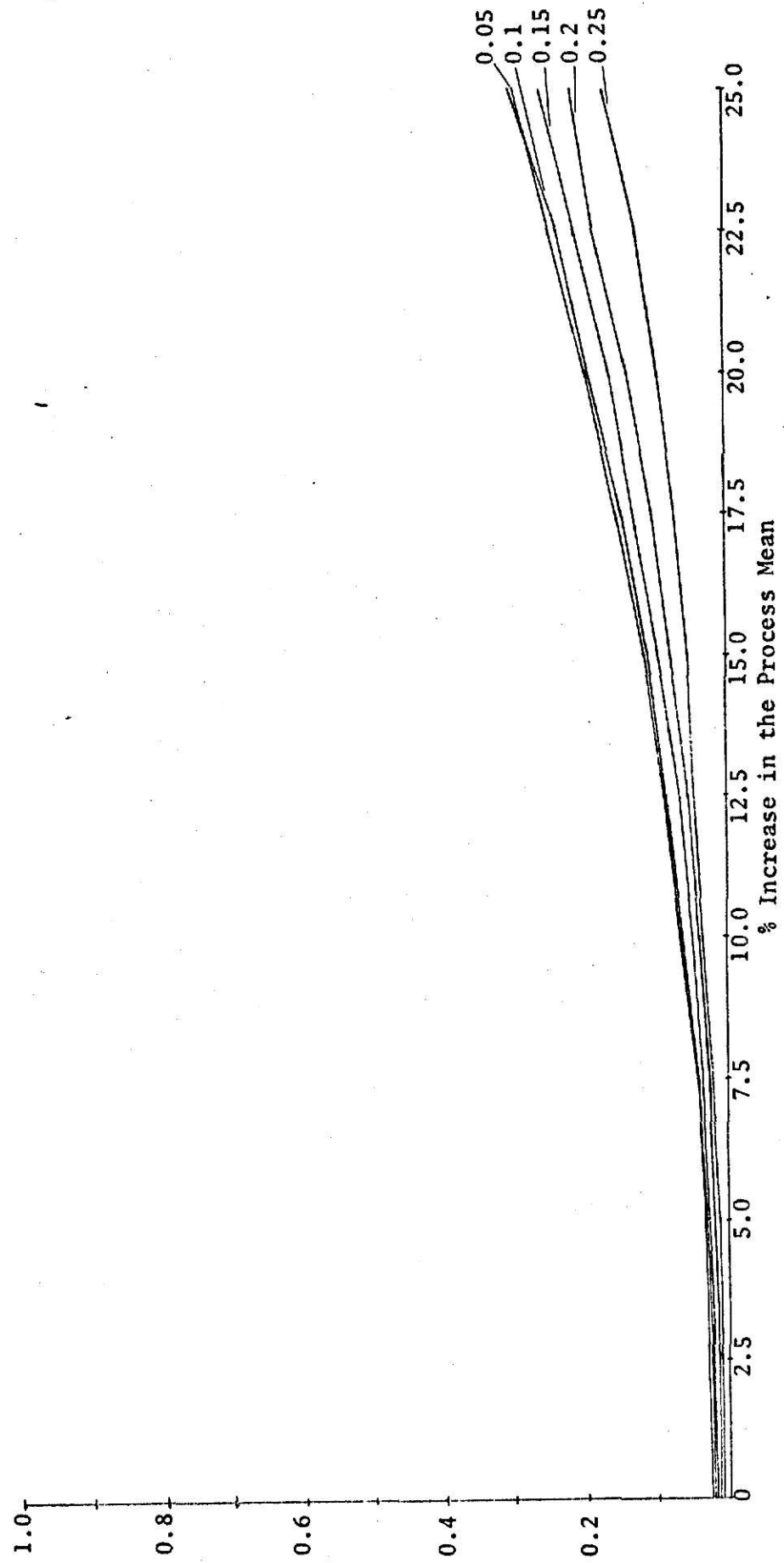


Figure (4.5) Probability Curve for Detection Criterion (a)

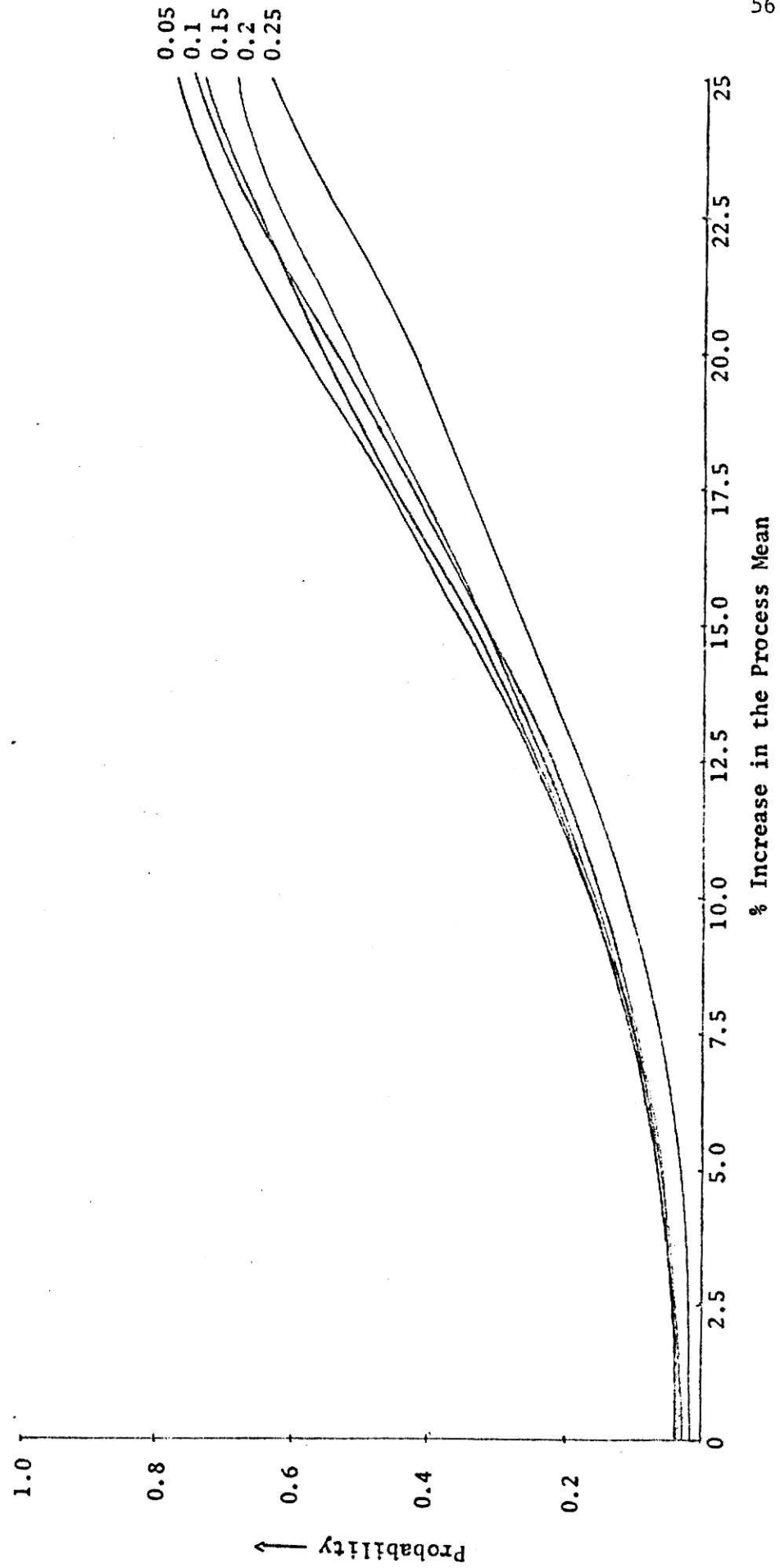


Figure (4.6) Probability Curve for Detection Criterion (b)

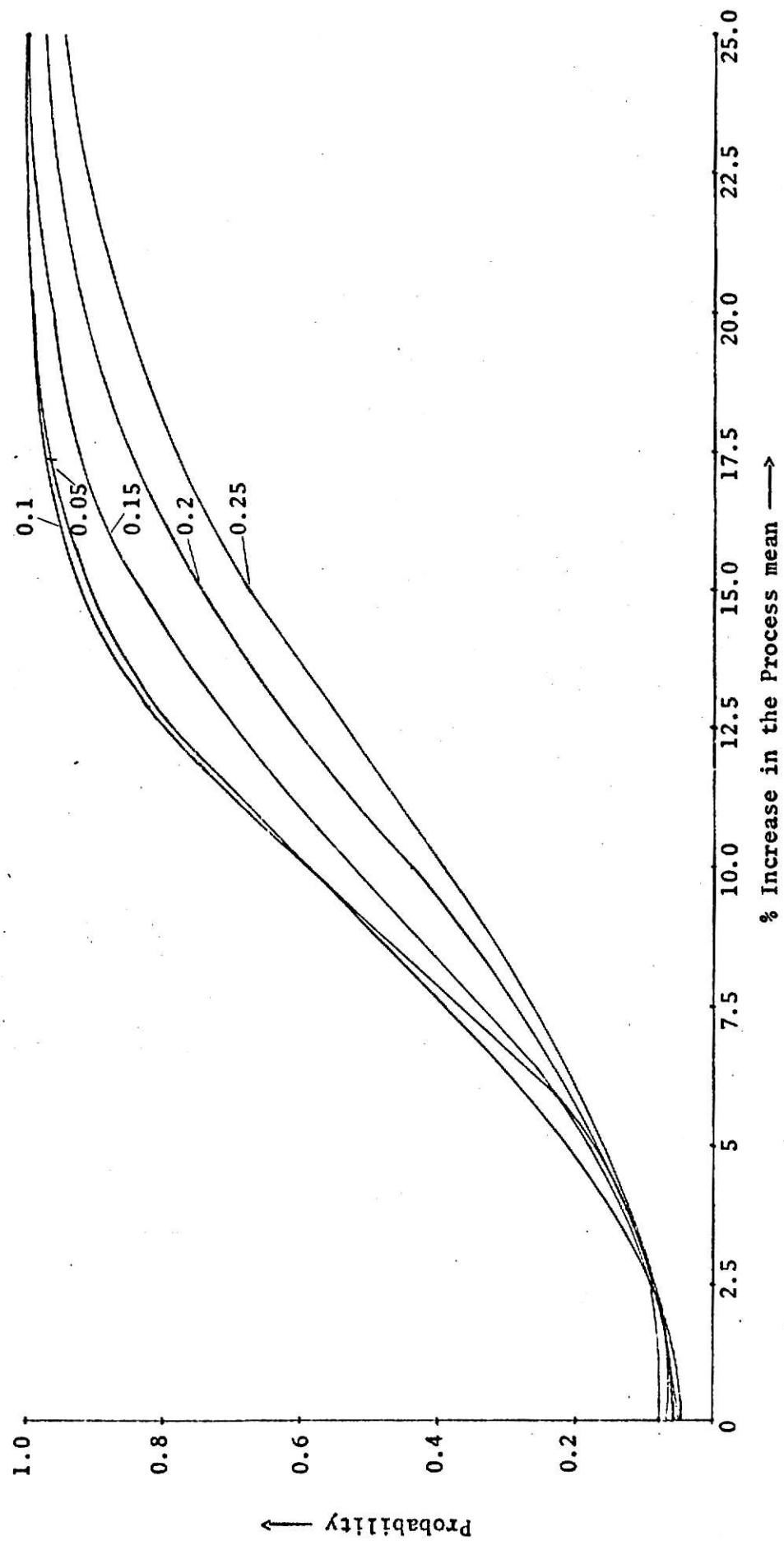
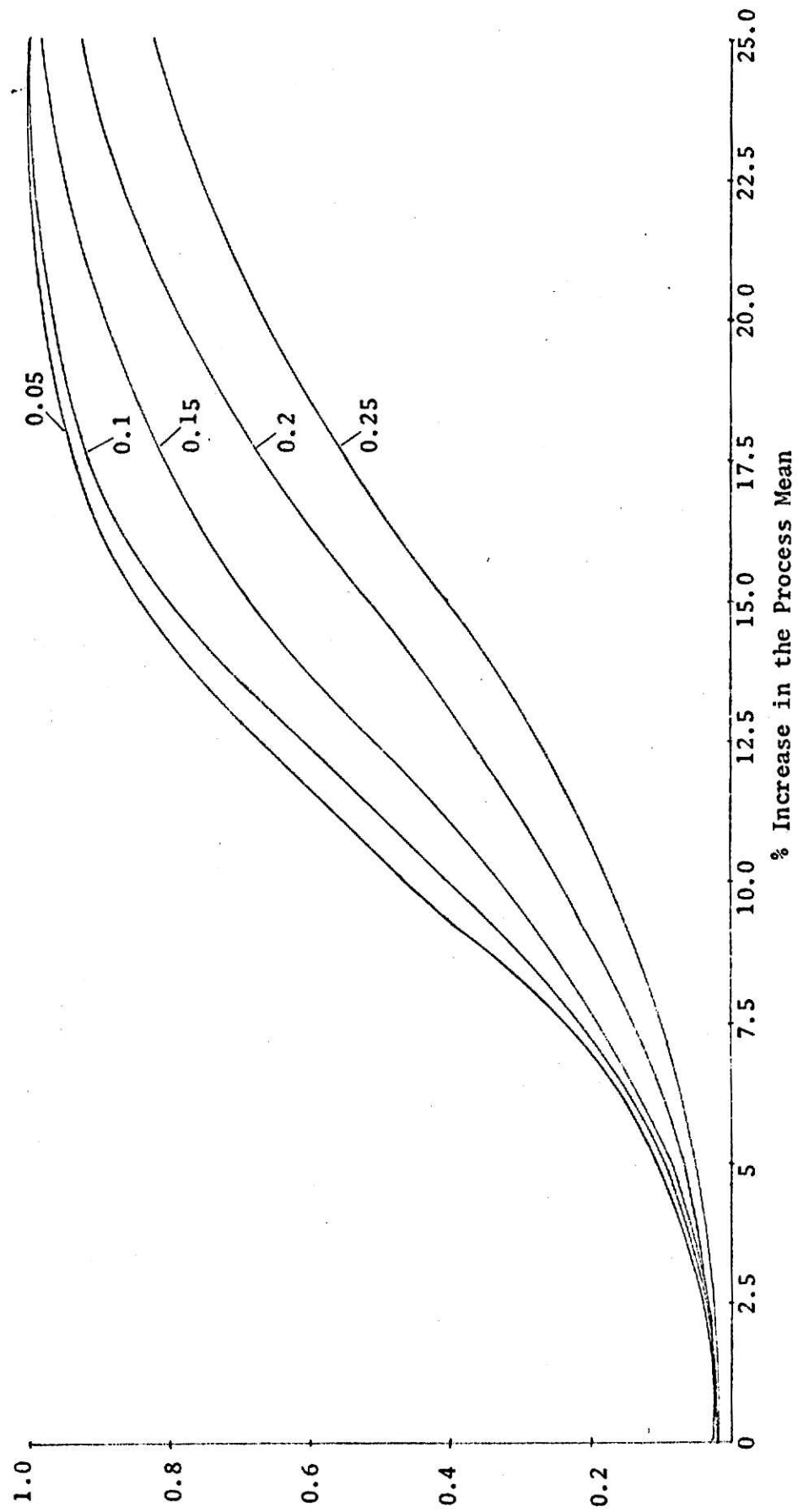


Figure (4.7) Probability Curves for Detection Criterion (c)



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APPENDIX A

Comparison of Frequencies for Chi-Square and
Kolmogorov Smirnov Tests for Goodness of Fit

Smoothing Constant = 0.1

Approximating Distribution = Beta Distribution with Parameters $m = n = 11.35$

Comparison of Frequencies for Chi-Square Test

CELL NO.	OBSERVED FREQUENCY	THEORETICAL FREQUENCY	CELL NO.	OBSERVED FREQUENCY	THEORETICAL FREQUENCY
1	0	0	21	304	284.33
2	0	0	22	372	390.35
3	0	0	23	531	522.50
4	0	0	24	685	683.11
5	0	0	25	919	873.73
6	0	0	26	1215	1094.78
7	0	0.02	27	1343	1345.45
8	0	0.07	28	1616	1623.48
9	0	0.22	29	1915	1925.15
10	0	0.59	30	2260	2245.22
11	0	1.43	31	2576	2577.13
12	2	3.13	32	2850	2913.08
13	3	6.35	33	3257	3244.40
14	10	12.03	34	3511	3561.83
15	17	21.49	35	3787	3855.96
16	40	36.49	36	4079	4117.64
17	52	59.19	37	4445	4338.43
18	80	92.23	38	4528	4510.98
19	137	138.58	39	4512	4629.43
20	230	201.50	40	4557	4689.70

CELL NO.	OBSERVED FREQUENCY	THEORETICAL FREQUENCY	CELL NO.	OBSERVED FREQUENCY	THEORETICAL FREQUENCY
41	4633	4689.70	61	183	201.50
42	4644	4629.43	62	150	138.58
43	4441	4510.98	63	76	92.23
44	4456	4338.43	64	56	59.19
45	4164	4117.64	65	35	36.49
46	3850	3855.96	66	11	21.49
47	3526	3561.83	67	10	12.03
48	3149	3244.40	68	4	9.48
49	2953	2913.08	69	7	2.02
50	2561	2577.13	70	4	0.22
51	2308	2245.22	71	2	0.07
52	1977	1925.15	72	0	0.02
53	1706	1623.48	73	0	0
54	1295	1345.45	74	0	0
55	1094	1094.78	75	0	0
56	893	873.73	76	0	0
57	696	683.11	77	0	0
58	524	522.50	78	0	0
59	368	390.35	79	0	0
60	291	284.33	80	0	0

The Obtained Chi-Square Value = 79.44

The Critical Chi-Square Value = 73.30, for 55 degrees of freedom and 5% significance level.

Smoothing Constant = 0.1

Approximating Distribution = Beta Distribution with Parameters $m=n=11.35$.

Comparison of Cumulative Frequencies for Kolmogorov Smirnov Test

CELL NUMBER	OBSERVED CUMULATIVE FREQUENCY 'f ₀ '	THEORETICAL CUMULATIVE FREQUENCY 'f _t '	CELL NUMBER	OBSERVED CUMULATIVE FREQUENCY 'f ₀ '	THEORETICAL CUMULATIVE FREQUENCY 'f _t '
1	0	0.0	21	875	857.65
2	0	0.0	22	1247	1248.00
3	0	0.0	23	1778	1770.00
4	0	0.0	24	2463	2453.61
5	0	0.0	25	3382	3327.34
7	0	0.02	27	5940	5767.57
8	0	0.09	28	7556	7391.05
9	0	0.31	29	9471	9316.20
10	0	0.90	30	11731	11561.42
11	0	2.33	31	14307	14138.55
12	2	5.46	32	17157	17051.63
13	5	11.81	33	20414	20296.03
14	15	23.84	34	23925	23857.86
15	32	45.33	35	27712	27713.82
16	72	81.82	36	31791	31831.46
17	124	141.01	37	36236	36169.89
18	204	233.24	38	40764	40680.87
19	341	371.82	39	45276	45310.30
20	571	573.32	40	49933	50000.00

CELL NUMBER	OBSERVED CUMULATIVE FREQUENCY 'f ₀ '	THEORETICAL CUMULATIVE FREQUENCY 'f _t '	CELL NUMBER	OBSERVED CUMULATIVE FREQUENCY 'f ₀ '	THEORETICAL CUMULATIVE FREQUENCY 'f _t '
41	54566	54689.70	61	99645	99628.18
42	59210	59319.13	62	99795	99766.76
43	63651	63830.11	63	99871	99858.99
44	68107	68168.54	64	99927	99918.18
45	72271	72286.18	65	99962	99954.67
47	79647	79703.97	67	99983	99988.19
48	82796	82948.37	68	99987	99994.54
49	85749	85861.45	69	99994	99997.67
50	88310	88438.58	70	99998	99999.10
51	90618	90683.80	71	100,000	99999.69
52	92595	92608.95	72	100,000	99999.91
53	94301	94232.43	73	100,000	99999.98
54	95596	95577.88	74	100,000	100,000.00
55	96690	96672.66	75	100,000	100,000.00
56	97583	97546.39	76	100,000	100,000.00
57	98279	98229.50	77	100,000	100,000.00
58	98803	98752.00	78	100,000	100,000.00
59	99171	99142.35	79	100,000	100,000.00
60	99462	99426.68	80	100,000	100,000.00

Maximum difference $|f_0 - f_t| = 179$

The obtained Kolmogorov Smirnov Value = $\frac{179}{100,000} = .00179$

The Critical Value" = $\frac{1.36}{\sqrt{n}} = \frac{1.36}{\sqrt{100,000}} = .00430$ for 5% Significance level.

Smoothing Constant = 0.2

Approximating Distribution = Resultant distribution obtained by combining
two beta distribution $\beta(4.939, 5.416)$ and
 $\beta(5.416, 4.939)$.

Comparison of Frequencies for Chi-Square Test

CELL NUMBER	OBSERVED FREQUENCY	THEORETICAL FREQUENCY	CELL NUMBER	OBSERVED FREQUENCY	THEORETICAL FREQUENCY
1	0	0.01	21	1094	1028.86
2	0	0.10	22	1291	1165.12
3	0	0.67	23	1391	1306.37
4	0	2.35	24	1508	1451.31
5	2	6.03	25	1654	1598.53
6	5	12.71	26	1809	1746.53
7	14	23.48	27	1997	1893.80
8	24	39.46	28	2111	2038.77
9	61	61.71	29	2216	2179.90
10	69	91.24	30	2206	2315.63
11	115	128.92	31	2394	2444.48
12	174	175.51	32	2441	2565.02
13	233	231.59	33	2642	2675.88
14	311	297.55	34	2738	2775.82
15	398	373.61	35	2864	2863.71
16	459	459.78	36	2914	2938.55
17	574	555.86	37	2925	2999.47
18	675	661.47	38	2932	3045.78
19	814	776.04	39	2981	3076.96
20	876	898.81	40	2992	3092.64

CELL NUMBER	OBSERVED FREQUENCY	THEORETICAL FREQUENCY	CELL NUMBER	OBSERVED FREQUENCY	THEORETICAL FREQUENCY
41	2960	3092.64	61	918	898.81
42	2939	3076.96	62	836	776.04
43	2968	3045.78	63	708	661.47
44	2860	2999.47	64	572	555.86
45	2896	2938.55	65	450	459.78
46	2809	2863.71	66	363	373.61
47	2851	2775.82	67	274	297.55
48	2764	2675.88	68	236	231.59
49	2609	2565.02	69	154	175.51
50	2364	2444.48	70	100	128.92
51	2322	2315.63	71	85	91.24
52	2277	2179.90	72	56	61.71
53	2131	2038.77	73	35	39.46
54	1968	1893.88	74	11	23.48
55	1745	1746.53	75	2	12.71
56	1655	1598.53	76	5	6.03
57	1528	1451.31	77	1	2.35
58	1334	1306.37	78	0	0.67
59	1260	1165.12	79	0	0.10
60	1050	1028.86	80	0	0.01

The obtained Chi-Square Value = 205.977

The critical chi-square value = 88.3, for 68 degrees of freedom and 5% significance level.

Smoothing Constant = 0.2

Approximating Distribution = Resultant Distribution Obtained by Combining
Two Beta Distributions, $\beta(4.939, 5.416)$ and
 $\beta(5.416, 4.939)$.

Comparison of Cumulative Frequencies for Kolmogorov Smirnov Test

CELL NUMBER	OBSERVED CUMULATIVE FREQUENCY 'f ₀ '	THEORETICAL CUMULATIVE FREQUENCY 'f _t '	CELL NUMBER	OBSERVED CUMULATIVE FREQUENCY 'f ₀ '	THEORETICAL CUMULATIVE FREQUENCY 'f _t '
1	0	.02	21	5898	5825.77
2	0	.12	22	7189	6990.89
3	0	.79	23	8580	8297.26
4	0	3.14	24	10058	9748.57
5	2	9.17	25	11742	11347.10
6	7	21.88	26	13551	13093.63
7	21	45.36	27	15548	14987.43
8	45	84.82	28	17659	17026.20
9	106	146.53	29	19875	19206.10
10	175	237.77	30	22081	21521.73
11	290	366.69	31	24475	23966.21
12	464	542.20	32	26916	26531.23
13	697	773.79	33	29558	29207.11
14	1008	1073.04	34	32296	31982.93
15	1406	1444.95	35	35160	34846.64
16	1865	1904.73	36	38074	37785.16
17	2478	2460.59	37	409999	40784.66
18	3114	3122.06	38	43931	43830.44
19	3928	3898.10	39	46912	46907.40
20	4804	4796.91	40	49904	50000.00

CELL NUMBER	OBSERVED CUMULATIVE FREQUENCY 'f ₀ '	THEORETICAL CUMULATIVE FREQUENCY 'f _t '	CELL NUMBER	OBSERVED CUMULATIVE FREQUENCY 'f ₀ '	THEORETICAL CUMULATIVE FREQUENCY 'f _t '
41	52864	53092.68	61	96112	96101.98
42	55803	56169.64	62	96948	96878.02
43	58771	59215.42	63	97656	97539.49
44	61631	62214.89	64	98228	98095.35
45	64527	65153.44	65	98678	98555.13
46	67336	68017.15	66	99041	98928.74
47	70187	70792.97	67	99315	99226.29
48	72951	73468.85	68	99551	99457.88
49	75560	76033.87	69	99715	99633.39
50	77924	78478.35	70	99805	99762.31
51	80246	80793.98	71	99890	99853.55
52	82523	82973.88	72	99946	99915.26
53	84654	85012.65	73	99981	99954.72
54	86622	86906.45	74	99992	99978.20
55	88367	88652.98	75	99994	99990.91
56	90022	90251.51	76	99999	99996.94
57	91550	91702.82	77	100,000	99999.29
58	92884	93009.19	78	100,000	100,000.00
59	94144	94174.31	79	100,000	100,000.00
60	95194	95203.17	80	100,000	100,000.00

Maximum Difference $|f_0 - f_t| = 681$

The Obtained Kolmogorov Smirnov Value = $\frac{681}{100,000} = 0.00681$

The Critical Kolmogorov Smirnov Value = $\frac{1.36}{\sqrt{n}} = \frac{1.36}{\sqrt{100,000}} = 0.00430$
for 5% Significance Level.

Smoothing Constant = 0.01

Approximating Distribution = Beta distribution with parameter $m=n=132.5$.

Comparison of Frequencies for a Chi-Square Test.

CELL NUMBER	OBSERVED FREQUENCY	THEORETICAL FREQUENCY	CELL NUMBER	OBSERVED FREQUENCY	THEORETICAL FREQUENCY
1	0	0.0	21	0	0.0
2	0	0.0	22	0	0.0
3	0	0.0	23	0	0.0
4	0	0.0	24	0	0.0
5	0	0.0	25	0	0.0
6	0	0.0	26	0	0.0
7	0	0.0	27	0	0.0
8	0	0.0	28	2.1	0.05
9	0	0.0	29	6.1	0.34
10	0	0.0	30	9	2.15
11	0	0.0	31	14	11.31
12	0	0.0	32	40	49.54
13	0	0.0	33	122	181.63
14	0	0.0	34	489	560.11
15	0	0.0	35	1340	1459.17
16	0	0.0	36	3138	3223.22
17	0	0.0	37	6101	6055.08
18	0	0.0	38	9656	9696.51
19	0	0.0	39	13146	13259.65
20	0	0.0	40	15801	15501.23

CELL NUMBER	OBSERVED FREQUENCY	THEORETICAL FREQUENCY	CELL NUMBER	OBSERVED FREQUENCY	THEORETICAL FREQUENCY
41	15977	15501.23	61	0	0.0
42	13394	13259.65	62	0	0.0
43	9604	9696.51	63	0	0.0
44	5891	6055.08	64	0	0.0
45	3082	3223.22	65	0	0.0
46	1459	1459.17	66	0	0.0
47	512	560.11	67	0	0.0
48	169	181.63	68	0	0.0
49	41	49.54	69	0	0.0
50	7	11.31	70	0	0.0
51	0	2.15	71	0	0.0
52	0	0.34	72	0	0.0
53	0	0.05	73	0	0.0
54	0	0.0	74	0	0.0
55	0	0.0	75	0	0.0
56	0	0.0	76	0	0.0
57	0	0.0	77	0	0.0
58	0	0.0	78	0	0.0
59	0	0.0	79	0	0.0
60	0	0.0	80	0	0.0

The obtained chi-square value = 162.27

The critical chi-square value = 327, for 21 degrees of freedom and at 5% significance level.

Smoothing Constant = 0.01

Approximating Distribution = Beta distribution with parameters $m=n=132.5$

Comparison of Cumulative Frequencies for Kolmogorov Smirnov Test.

CELL NUMBER	OBSERVED CUMULATIVE FREQUENCY 'f ₀ '	THEORETICAL CUMULATIVE FREQUENCY 'f _t '	CELL NUMBER	OBSERVED CUMULATIVE FREQUENCY 'f ₀ '	THEORETICAL CUMULATIVE FREQUENCY 'f _t '
1	0	0	21	0	0
2	0	0	22	0	0
3	0	0	23	0	0
4	0	0	24	0	0
5	0	0	25	0	0
6	0	0	26	0	0
7	0	0	27	0	0
8	0	0	28	2	0
9	0	0	29	8	0
10	0	0	30	17	2
11	0	0	31	31	13
12	0	0	32	71	62
13	0	0	33	193	243
14	0	0	34	682	803
15	0	0	35	2022	2262
16	0	0	36	5160	5485
17	0	0	37	11261	11540
18	0	0	38	20917	21236
19	0	0	39	34063	34495
20	0	0	90	49864	49996

CELL NUMBER	OBSERVED CUMULATIVE FREQUENCY 'f ₀ '	THEORETICAL CUMULATIVE FREQUENCY 'f _t '	CELL NUMBER	OBSERVED CUMULATIVE FREQUENCY 'f ₀ '	THEORETICAL CUMULATIVE FREQUENCY 'f _t '
41	65841	65497	61	100,000	100,000
42	79235	78756	62	100,000	100,000
43	88839	88452	63	100,000	100,000
44	94730	94507	64	100,000	100,000
45	97812	97730	65	100,000	100,000
46	99271	99189	66	100,000	100,000
47	99783	99749	67	100,000	100,000
48	99952	99930	68	100,000	100,000
49	99993	99979	69	100,000	100,000
50	100,000	99989	70	100,000	100,000
51	100,000	100,000	71	100,000	100,000
52	100,000	100,000	72	100,000	100,000
53	100,000	100,000	73	100,000	100,000
54	100,000	100,000	74	100,000	100,000
55	100,000	100,000	75	100,000	100,000
56	100,000	100,000	76	100,000	100,000
57	100,000	100,000	77	100,000	100,000
58	100,000	100,000	78	100,000	100,000
59	100,000	100,000	79	100,000	100,000
60	100,000	100,000	80	100,000	100,000

Maximum Difference $|f_0 - f_t| = 479$

The obtained Kolmogorov Smirnov Value = $\frac{479}{100,000} = 0.00479$

The critical Kolmogorov Smirnov Value = $\frac{1.36}{\sqrt{n}} = \frac{1.36}{\sqrt{100,000}} = 0.00473$

APPENDIX B

COMPUTER PROGRAMS

ILLEGIBLE DOCUMENT

**THE FOLLOWING
DOCUMENT(S) IS OF
POOR LEGIBILITY IN
THE ORIGINAL**

**THIS IS THE BEST
COPY AVAILABLE**

FORTRAN IV G LEVEL 18

MAIN

DATE = 71095

17/17/35

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CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C
C      PURPOSE
C
C      THE PURPOSE OF THIS PROGRAMME IS TO SIMULATE TRACKING SIGNAL
C      DISTRIBUTION USING SINGLE EXPONENTIAL SMOOTHING
C
C      DESCRIPTION OF PARAMETERS
C
C      ALPHA-THE VALUE OF SMOOTHING CONSTANT ,WHICH VARIES FROM 0 TO 1
C
C      STEP-THE DESIRED INCREMENT IN THE VALUE OF SMOOTHING CONSTANT.
C
C      LIMIT-STOPPING CRITERIA FOR THE PROGRAMME OR THE LAST VALUE OF
C      SMOOTHING CONSTANT FOR WHICH SIMULATION IS CARRIED OUT
C
C      XEAN-THE MEAN OF THE PROCESS
C
C      STDDEV-THE STANDARD DEVIATION OF ASSUMED NORMAL DISTRIBUTION
C      OF NOISE
C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
0001      DIMENSION MT(80)
0002      1 FORMAT(3I10,2F10.4)
0003      2 FORMAT (' ',I10,' IY',I10,' IX',I10,' NCOUNT',F10.4,' MEAN',F10.4,
0004      1' STDDEV',F10.4,' ALPHA')
0005      10 FORMAT (3F8.4,I3)
0006      120 FORMAT(10X,'MEAN',10X,'STDDEV')
0007      121 FORMAT(5X,F8.4,10X,F8.4)
0008      123 FORMAT('1 I TSIG')
0009      124 FORMAT(I3,10X,I6)
0010      READ 10,ALPHA,STEP,XLIMIT,N
0011      DO 200 NRUN =1,N
0012      READ(1,1) IY,IX,NCOUNT,XEAN,STDDEV
0013      13 WRITE(3,2) IY,IX,NCOUNT,XEAN,STDDEV,ALPHA
0014      DO 3 I=1,80
0015      MT(I)=0
0016      3 CONTINUE
0017      FACT=SQRT(2./(2.-ALPHA))
0018      SMAD=.79788*FACT*STDDEV
0019      XHAT=XEAN
0020      SSE=0.
0021      BETA=1.-ALPHA
0022      STRSIG=0.0
0023      SOTSIG=0.0
C
C      GENERATION OF UNIFORM RANDOM NUMBER
C
0023      DO 101 I=1,NCOUNT
0024      IY=IY+IX
0025      IF(IY.LT.0) IY=IY+2147483647+1
0026      RA=IY*.4656613E-9
0027      IY=IY+IX
0028      IF(IY.LT.0) IY=IY+2147483647+1
0029      RB=IY*.4656613E-9
C
C      GENERATION OF TWO RANDOM NORMAL DEVIATES
C

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0030      LA=SQRT(-2.0*ALOG(RA))
0031      UB=6.2832*RB
0032      XA=UA*COS(UB)
0033      XB=UA*SIN(UB)
0034      X=XA*STDDEV+XEAN
0035      RD=XB*STDDEV+XEAN

      C
      C      EVALUATION OF TRACKING SIGNAL
      C

0036      DO 101 II=1,2
0037      ERR=X-XHAT
0038      SSE=ALPHA*ERR+BETA*SSE
0039      SMAD=ALPHA*ABS(ERR)+BETA*SMAD
0040      TRSIG=SSE/SMAD
0041      XHAT=ALPHA*X+BETA*XHAT
0042      STRSIG=STRSIG+TRSIG
0043      SOTSIG=SOTSIG+TRSIG*TRSIG

      C
      C      CLASSIFICATION OF TRACKING SIGNAL INTO 80 CELLS
      C

0044      NT=TRSIG*40.+41.
0045      IF (NT. GT. 80 ) NT=80
0046      IF(NT.LT.1 ) NT=1
0047      MT(NT)=MT(NT)+1
0048      X=RD
0049      101 CONTINUE

      C
      C      OBTAIN MEAN AND STANDARD DEVIATION OF TRACKING SIGNAL
      C

0050      CMEAN=STRSIG/(2*NCOUNT)
0051      STDEV=(SOTSIG/(2*NCOUNT))-(CMEAN)**2)**0.5
0052      DO 122 J=1,41,40
0053      JJ=J+39
0054      PRINT 123
0055      DO 122 I=J,JJ
0056      PRINT 124,I,MT(I)
0057      122 CONTINUE
0058      PRINT 120
0059      PRINT 121,CMEAN,STDEV

      C
      C      INCREMENT IN THE VALUE OF ALPHA FOR NEXT SIMULATION
      C

0060      ALPHA=ALPHA+STEP
0061      IF (ALPHA-XLIMIT) 11,12,12
0062      11 GO TO 13

      C
      C      RESET VALUE OF ALPHA FOR SIMULATION WITH A NEW SET OF DATA
      C

0063      12 ALPHA=0.1
0064      200 CONTINUE
0065      STOP
0066      END

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C .....CDTR 10
C .....CDTR 20
C .....CDTR 30
C SUBROUTINE CDTRCDTR 40
C .....CDTR 50
C PURPOSECDTR 60
C COMPUTES P(X) = PROBABILITY THAT THE RANDOM VARIABLE U,CDTR 70
C DISTRIBUTED ACCORDING TO THE CHI-SQUARE DISTRIBUTION WITH G CDTR 80
C DEGREES OF FREEDOM, IS LESS THAN OR EQUAL TO X. F(G,X), THECDTR 90
C ORDINATE OF THE CHI-SQUARE DENSITY AT X, IS ALSO COMPUTED.CDTR 100
C .....CDTR 110
C USAGECDTR 120
C CALL CDTR(X,G,P,C,IER)CDTR 130
C .....CDTR 140
C DESCRIPTION OF PARAMETERSCDTR 150
C X - INPUT SCALAR FOR WHICH P(X) IS COMPUTED.CDTR 160
C G - NUMBER OF DEGREES OF FREEDOM OF THE CHI-SQUARECDTR 170
C DISTRIBUTION. G IS A CONTINUOUS PARAMETER.CDTR 180
C P - OUTPUT PROBABILITY.CDTR 190
C D - OUTPUT DENSITY.CDTR 200
C IER - RESULTANT ERROR CODE WHERECDTR 210
C IER= 0 --- NO ERRORCDTR 220
C IER=-1 --- AN INPUT PARAMETER IS INVALID. X IS LESSCDTR 230
C THAN 0.0, OR G IS LESS THAN 0.5 OR GREATERCDTR 240
C THAN 2*10**(15). P AND D ARE SET TO -1.E75.CDTR 250
C IER=+1 --- INVALID OUTPUT. P IS LESS THAN ZERO ORCDTR 260
C GREATER THAN ONE, OR SERIES FOR T1 (SEECDTR 270
C MATHEMATICAL DESCRIPTION) HAS FAILED TOCDTR 280
C CONVERGE. P IS SET TO 1.E75.CDTR 290
C .....CDTR 300
C REMARKSCDTR 310
C SEE MATHEMATICAL DESCRIPTION.CDTR 320
C .....CDTR 330
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIREDCDTR 340
C DLGAMCDTR 350
C NDTRCDTR 360
C .....CDTR 370
C METHODCDTR 380
C REFER TO R.E. BARGMANN AND S.P. GHOSH, STATISTICALCDTR 390
C DISTRIBUTION PROGRAMS FOR A COMPUTER LANGUAGE,CDTR 400
C IBM RESEARCH REPORT RC-1094, 1963.CDTR 410
C .....CDTR 420
C .....CDTR 430
C .....CDTR 440
C0001 SUBROUTINE CDTR(X,G,P,C,IER)CDTR 460
C0002 DOUBLE PRECISION XX,DLXX,X2,DLX2,GG,G2,DLT3,THETA,THP1,CDTR 470
C1GLG2,DD,T11,SER,CC,XI,FAC,TLOG,TERM,GTH,A2,A,B,C,DT2,DT3,THP1CDTR 480
C .....CDTR 490
C TEST FOR VALID INPUT DATACDTR 500
C .....CDTR 510
C0003 IF(G-(.5-1.E-5)) 590,10,10CDTR 520
C0004 10 IF(G-2.E+5) 20,20,590CDTR 530
C0005 20 IF(X) 590,30,30CDTR 540
C .....CDTR 550
C TEST FOR X NEAR 0.0CDTR 560
C .....CDTR 570
C0006 30 IF(X-1.E-8) 40,40,80CDTR 580
C0007 40 P=0.0CDTR 590

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CDTR

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CCC8	IF(G-2.) 50,60,70	CDTR 590
CC09	50 C=1.E75	CDTR 600
CC10	GO TO 610	CDTR 610
CC11	60 C=0.5	CDTR 620
CC12	GO TO 610	CDTR 630
CC13	70 C=0.0	CDTR 640
CC14	GO TO 610	CDTR 650
C		CDTR 660
C	TEST FOR X GREATER THAN 1.E+6	CDTR 670
C		CDTR 680
CC15	80 IF(X-1.E+6) 100,100,90	CDTR 690
CC16	90 C=C-0	CDTR 700
CC17	P=1.0	CDTR 710
CC18	GO TO 610	CDTR 720
C		CDTR 730
C	SET PROGRAM PARAMETERS	CDTR 740
C		CDTR 750
CC19	100 XX=DBLE(X)	CDTR 760
CC20	CLXX=DLOG(XX)	CDTR 770
CC21	X2=XX/2.00	CDTR 780
CC22	CLX2=DLOG(X2)	CDTR 790
CC23	GG=DBLE(G)	CDTR 800
CC24	G2=GG/2.00	CDTR 810
C		CDTR 820
C	COMPUTE ORDINATE	CDTR 830
C		CDTR 840
CC25	CALL DLGAM(G2,GLG2,ICK)	CDTR 850
CC26	CD=(G2-1.00)*CLXX-X2-G2*.6931471805599453 -GLG2	CDTR 860
CC27	IF(CD-1.68002) 110,110,120	CDTR 870
CC28	110 IF(CD+1.68002) 130,130,140	CDTR 880
CC29	120 C=1.E75	CDTR 890
CC30	GO TO 150	CDTR 900
CC31	130 C=0.0	CDTR 910
CC32	GO TO 150	CDTR 920
CC33	140 CD=DEXP(CD)	CDTR 930
CC34	C=SNGL(CD)	CDTR 940
C		CDTR 950
C	TEST FOR G GREATER THAN 1000.0	CDTR 960
C	TEST FOR X GREATER THAN 2000.0	CDTR 970
C		CDTR 980
CC35	150 IF(G-1000.) 160,160,180	CDTR 990
CC36	160 IF(X-2000.) 190,190,170	CDTR1000
CC37	170 P=1.0	CDTR1010
CC38	GO TO 610	CDTR1020
CC39	180 A=DLOG(XX/GG)/3.00	CDTR1030
CC40	A=DEXP(A)	CDTR1040
CC41	B=2.00/(9.00*GG)	CDTR1050
CC42	C=(A-1.00+B)/DSQRT(B)	CDTR1060
CC43	SC=SNGL(C)	CDTR1070
CC44	CALL NDTR(SC,P,DUMMY)	CDTR1080
CC45	GO TO 490	CDTR1090
C		CDTR1100
C	COMPUTE THETA	CDTR1110
C		CDTR1120
CC46	190 K= IDINT(G2)	CDTR1130
CC47	THETA=G2-DFLOAT(K)	CDTR1140
CC48	IF(THETA-1.0-8) 200,200,210	CDTR1150
CC49	200 THETA=0.00	CDTR1160

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CC50	210	THP1=THETA+1.D0	CDTR1170
	C		CDTR1180
	C	SELECT METHOD OF COMPUTING T1	CDTR1190
	C		CDTR1200
CC51		IF(THETA) 230,230,220	CDTR1210
CC52	220	IF(XX-10.D0) 260,260,320	CDTR1220
	C		CDTR1230
	C	COMPUTE T1 FOR THETA EQUALS 0.0	CDTR1240
	C		CDTR1250
CC53	230	IF(X2-1.68D02) 250,240,240	CDTR1260
CC54	240	T1=1.0	CDTR1270
CC55		GO TO 400	CDTR1280
CC56	250	T11=1.D0-DEXP(-X2)	CDTR1290
CC57		T1=SNGL(T11)	CDTR1300
CC58		GO TO 400	CDTR1310
	C		CDTR1320
	C	COMPUTE T1 FOR THETA GREATER THAN 0.0 AND	CDTR1330
	C	X LESS THAN OR EQUAL TO 10.0	CDTR1340
	C		CDTR1350
CC59	260	SER=X2*(1.D0/THP1 -X2/(THP1+1.D0))	CDTR1360
CC60		J=+1	CDTR1370
CC61		CC=DFLOAT(J)	CDTR1380
CC62		DO 270 IT1=3,30	CDTR1390
CC63		XI=DFLOAT(IT1)	CDTR1400
CC64		CALL DLGAM(XI,FAC,IOK)	CDTR1410
CC65		TLOG= XI*DLX2-FAC-DLOG(XI+THETA)	CDTR1420
CC66		TERM=DEXP(TLOG)	CDTR1430
CC67		TERM=DSIGN(TERM,CC)	CDTR1440
CC68		SER=SER+TERM	CDTR1450
CC69		CC=-CC	CDTR1460
CC70		IF(DABS(TERM)-1.D-9) 280,270,270	CDTR1470
CC71	270	CONTINUE	CDTR1480
CC72		GO TO 600	CDTR1490
CC73	280	IF(SER) 600,600,290	CDTR1500
CC74	290	CALL DLGAM(THP1,GTH,IOK)	CDTR1510
CC75		TLOG=THETA*DLX2+DLOG(SER)-GTH	CDTR1520
CC76		IF(TLOG+1.68D02) 300,300,310	CDTR1530
CC77	300	T1=0.0	CDTR1540
CC78		GO TO 400	CDTR1550
CC79	310	T11=DEXP(TLOG)	CDTR1560
CC80		T1=SNGL(T11)	CDTR1570
CC81		GO TO 400	CDTR1580
	C		CDTR1590
	C	COMPUTE T1 FOR THETA GREATER THAN 0.0 AND	CDTR1600
	C	X GREATER THAN 10.0 AND LESS THAN 2000.0	CDTR1610
	C		CDTR1620
CC82	320	A2=0.D0	CDTR1630
CC83		DO 340 I=1,25	CDTR1640
CC84		XI=DFLOAT(I)	CDTR1650
CC85		CALL DLGAM(THP1,GTH,IOK)	CDTR1660
CC86		T11=- (13.D0*XX)/XI +THP1*DLOG(13.D0*XX/XI) -GTH-DLOG(XI)	CDTR1670
CC87		IF(T11+1.68D02) 340,340,330	CDTR1680
CC88	330	T11=DEXP(T11)	CDTR1690
CC89		A2=A2+T11	CDTR1700
CC90	340	CONTINUE	CDTR1710
CC91		A=1.01282051+THETA/156.D0-XX/312.D0	CDTR1720
CC92		E=DABS(A)	CDTR1730
CC93		C= -X2+THP1*DLX2+DLOG(E)-GTH-3.951243718581427	CDTR1740

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0094	IF(C+1.68D02) 370,370,350	CDTR1750
0095	350 IF (A) 360,370,380	CDTR1760
0096	360 C=-DEXP(C)	CDTR1770
0097	GO TO 390	CDTR1780
0098	370 C=0.D0	CDTR1790
0099	GO TO 390	CDTR1800
0100	380 C=DEXP(C)	CDTR1810
0101	390 C=A2+C	CDTR1820
0102	T11=1.D0-C	CDTR1830
0103	T1=SNGL(T11)	CDTR1840
	C	CDTR1850
	C	CDTR1860
	C	CDTR1870
0104	400 IF(G-2.) 420,410,410	CDTR1880
0105	410 IF(G-4.) 450,460,460	CDTR1890
	C	CDTR1900
	C	CDTR1910
	C	CDTR1920
0106	420 CALL DLGAM(THPI,GTH,ICK)	CDTR1930
0107	CT2=THETA*DLXX-X2-THPI*.6931471805599453 -GTH	CDTR1940
0108	IF(DT2+1.68D02) 430,430,440	CDTR1950
0109	430 P=T1	CDTR1960
0110	GO TO 490	CDTR1970
0111	440 CT2=DEXP(DT2)	CDTR1980
0112	T2=SNGL(DT2)	CDTR1990
0113	P=T1+T2+T2	CDTR2000
0114	GO TO 490	CDTR2010
	C	CDTR2020
	C	CDTR2030
	C	CDTR2040
	C	CDTR2050
0115	450 P=T1	CDTR2060
0116	GO TO 490	CDTR2070
	C	CDTR2080
	C	CDTR2090
	C	CDTR2100
	C	CDTR2110
0117	460 DT3=0.D0	CDTR2120
0118	DO 480 I3=2,K	CDTR2130
0119	THPI=DFLOAT(I3)+THETA	CDTR2140
0120	CALL DLGAM(THPI,GTH,ICK)	CDTR2150
0121	CLT3=THPI*DLX2-DLXX-X2-GTH	CDTR2160
0122	IF(DLT3+1.68D02) 480,480,470	CDTR2170
0123	470 CT3=DT3+DEXP(DLT3)	CDTR2180
0124	480 CONTINUE	CDTR2190
0125	T3=SNGL(DT3)	CDTR2200
0126	P=T1-T3-T3	CDTR2210
	C	CDTR2220
	C	CDTR2230
	C	CDTR2240
0127	490 IF(P) 500,520,520	CDTR2250
0128	500 IF(ABS(P)-1.E-7) 510,510,600	CDTR2260
0129	510 P=0.0	CDTR2270
0130	GO TO 610	CDTR2280
0131	520 IF(1.-P) 530,550,550	CDTR2290
0132	530 IF(ABS(1.-P)-1.E-7) 540,540,600	CDTR2300
0133	540 P=1.0	CDTR2310
0134	GO TO 610	CDTR2320

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0135	550	IF(P-1.E-8) 560,560,570	CDTR2330
0136	560	P=0.0	CDTR2340
0137		GO TO 610	CDTR2350
0138	570	IF((1.0-P)-1.E-8) 580,580,610	CDTR2360
0139	580	P=1.0	CDTR2370
0140		GO TO 610	CDTR2380
0141	590	IER=-1	CDTR2390
0142		C=-1.E75	CDTR2400
0143		P=-1.E75	CDTR2410
0144		GO TO 620	CDTR2420
0145	600	IER=+1	CDTR2430
0146		P= 1.E75	CDTR2440
0147		GO TO 620	CDTR2450
0148	610	IER=0	CDTR2460
0149	620	RETURN	CDTR2470
0150		END	CDTR2480

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C		NDTR	10
C		NDTR	20
C		NDTR	30
C	SUBROUTINE NDTR	NDTR	40
C		NDTR	50
C	PURPOSE	NDTR	60
C	COMPUTES Y = P(X) = PROBABILITY THAT THE RANDOM VARIABLE U,	NDTR	70
C	DISTRIBUTED NORMALLY(0,1), IS LESS THAN OR EQUAL TO X.	NDTR	80
C	F(X), THE ORDINATE OF THE NORMAL DENSITY AT X, IS ALSO	NDTR	90
C	COMPUTED.	NDTR	100
C		NDTR	110
C	-USAGE	NDTR	120
C	CALL NDTR(X,P,D)	NDTR	130
C		NDTR	140
C	DESCRIPTION OF PARAMETERS	NDTR	150
C	X--INPUT SCALAR FOR WHICH P(X) IS COMPUTED.	NDTR	160
C	P--OUTPUT PROBABILITY.	NDTR	170
C	D--OUTPUT DENSITY.	NDTR	180
C		NDTR	190
C	REMARKS	NDTR	200
C	MAXIMUM ERROR IS 0.0000007.	NDTR	210
C		NDTR	220
C	SUBROUTINES AND SUBPROGRAMS REQUIRED	NDTR	230
C	NONE	NDTR	240
C		NDTR	250
C	METHOD	NDTR	260
C	BASED ON APPROXIMATIONS IN C. HASTINGS, APPROXIMATIONS FOR	NDTR	270
C	DIGITAL COMPUTERS, PRINCETON UNIV. PRESS, PRINCETON, N.J.,	NDTR	280
C	1955. SEE EQUATION 26.2.17, HANDBOOK OF MATHEMATICAL	NDTR	290
C	FUNCTIONS, ABRAMOWITZ AND STEGUN, DOVER PUBLICATIONS, INC.,	NDTR	300
C	NEW YORK.	NDTR	310
C		NDTR	320
C		NDTR	330
C		NDTR	340
CCC1	SUBROUTINE NDTR(X,P,D)		
C		NDTR	360
CCC2	AX=ABS(X)	NDTR	370
CCC3	T=1.0/(1.0+.2316419*AX)	NDTR	380
CCC4	C=0.3989423*EXP(-X*X/2.0)	NDTR	390
CCC5	P = 1.0 - D*T*(((1.330274*T - 1.821256)*T + 1.781478)*T -	NDTR	400
	1 0.3565638)*T + 0.3193815)	NDTR	410
CCC6	IF(X)1,2,2	NDTR	420
CCC7	1 P=1.0-P	NDTR	430
CCC8	2 RETURN	NDTR	440
CCC9	END	NDTR	450

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C		DLGA 10
C		DLGA 20
C		DLGA 30
C	SUBROUTINE DLGAM	DLGA 40
C		DLGA 50
C	PURPOSE	DLGA 60
C	COMPUTES THE DOUBLE PRECISION NATURAL LOGARITHM OF THE	DLGA 70
C	GAMMA FUNCTION OF A GIVEN DOUBLE PRECISION ARGUMENT.	DLGA 80
C		DLGA 90
C	USAGE	DLGA 100
C	CALL DLGAM(XX,DLNG,IER)	DLGA 110
C		DLGA 120
C	DESCRIPTION OF PARAMETERS	DLGA 130
C	XX - THE DOUBLE PRECISION ARGUMENT FOR THE LOG GAMMA	DLGA 140
C	FUNCTION.	DLGA 150
C	DLNG - THE RESULTANT DOUBLE PRECISION LOG GAMMA FUNCTION	DLGA 160
C	VALUE.	DLGA 170
C	IER - RESULTANT ERROR CODE WHERE	DLGA 180
C	IER= 0----NO ERROR.	DLGA 190
C	IER=-1----XX IS WITHIN 10**(-9) OF BEING ZERO OR XX	DLGA 200
C	IS NEGATIVE. DLNG IS SET TO -1.0075.	DLGA 210
C	IER=+1----XX IS GREATER THAN 10**70. DLNG IS SET TO	DLGA 220
C	+1.0075.	DLGA 230
C		DLGA 240
C	REMARKS	DLGA 250
C	NONE	DLGA 260
C		DLGA 270
C	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	DLGA 280
C	NONE	DLGA 290
C		DLGA 300
C	METHOD	DLGA 310
C	THE EULER-MCLAURIN EXPANSION TO THE SEVENTH DERIVATIVE TERM	DLGA 320
C	IS USED, AS GIVEN BY M. ABRAMOWITZ AND I.A. STEGUN,	DLGA 330
C	'HANDBOOK OF MATHEMATICAL FUNCTIONS', U. S. DEPARTMENT OF	DLGA 340
C	COMMERCE, NATIONAL BUREAU OF STANDARDS APPLIED MATHEMATICS	DLGA 350
C	SERIES, 1966, EQUATION 6.1.41.	DLGA 360
C		DLGA 370
C		DLGA 380
C		DLGA 390
CCC1	SUBROUTINE DLGAM(XX,DLNG,IER)	DLGA 400
CC02	DOUBLE PRECISION XX,ZZ,TERM,RZZ,DLNG	DLGA 410
CC03	IER=0	DLGA 420
CC04	ZZ=XX	DLGA 430
CC05	IF(XX-1.D10) 2,2,1	DLGA 440
CC06	1 IF(XX-1.D70) 8,9,9	DLGA 450
C		DLGA 460
C	SEE IF XX IS NEAR ZERO OR NEGATIVE	DLGA 470
C		DLGA 480
CC07	2 IF(XX-1.D-9) 3,3,4	DLGA 490
CC08	3 IER=-1	DLGA 500
CC09	DLNG=-1.075	DLGA 510
CC10	GO TO 10	DLGA 520
C		DLGA 530
C	XX GREATER THAN ZERO AND LESS THAN OR EQUAL TO 1.D+10	DLGA 540
C		DLGA 550
CC11	4 TERM=1.D0	DLGA 560
CC12	5 IF(ZZ-18.D0) 6,6,7	DLGA 570
CC13	6 TERM=TERM*ZZ	DLGA 580

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CC14	ZZ=ZZ+1.00	DLGA 590
CC15	GO TO 5	DLGA 600
CC16	7 RZ2=1.00/ZZ**2	DLGA 610
CC17	CLNG=(ZZ-0.500)*DLOG(ZZ)-ZZ +0.9189385332046727 -DLOG(TERM)+	DLGA 620
	1(1.00/ZZ)*(.8333333333333333D-1 -(RZ2*(.2777777777777777D-2 +(RZ2*DLGA 630	
	2(.7936507936507936D-3 -(RZ2*(.5952380952380952D-3))))))	DLGA 640
CC18	GO TO 10	DLGA 650
	C	DLGA 660
	C XX GREATER THAN 1.0+10 AND LESS THAN 1.0+70	DLGA 670
	C	DLGA 680
CC19	8 CLNG=ZZ*(DLOG(ZZ)-1.00)	DLGA 690
CC20	GO-TO 10	DLGA 700
	C	DLGA 710
	C XX GREATER THAN OR EQUAL TO 1.0+70	DLGA 720
	C	DLGA 730
CC21	9 IER=+1	DLGA 740
CC22	CLNG=1.075	DLGA 750
CC23	10 RETURN	DLGA 760
CC24	END	DLGA 770

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C ..... BDTR 10
C ..... BDTR 20
C ..... BDTR 30
C SUBROUTINE BDTR BDTR 40
C ..... BDTR 50
C PURPOSE BDTR 60
C COMPUTES P(X) = PROBABILITY THAT THE RANDOM VARIABLE U, BDTR 70
C DISTRIBUTED ACCORDING TO THE BETA DISTRIBUTION WITH BDTR 80
C PARAMETERS A AND B, IS LESS THAN OR EQUAL TO X. F(A,B,X), BDTR 90
C THE ORDINATE OF THE BETA DENSITY AT X, IS ALSO COMPUTED. BDTR 100
C ..... BDTR 110
C -USAGE BDTR 120
C CALL BDTR(X,A,B,P,D,IER) BDTR 130
C ..... BDTR 140
C DESCRIPTION OF PARAMETERS BDTR 150
C X - INPUT SCALAR FOR WHICH P(X) IS COMPUTED. BDTR 160
C A - BETA DISTRIBUTION PARAMETER (CONTINUOUS). BDTR 170
C B - BETA DISTRIBUTION PARAMETER (CONTINUOUS). BDTR 180
C P - OUTPUT PROBABILITY. BDTR 190
C D - OUTPUT DENSITY. BDTR 200
C IER - RESULTANT ERROR CODE WHERE BDTR 210
C IER= 0 --- NO ERROR BDTR 220
C IER=-1,+1 CCTR HAS BEEN CALLED AND AN ERROR HAS BDTR 230
C OCCURRED. SEE CCTR. BDTR 240
C IER=-2 --- AN INPUT PARAMETER IS INVALID. X IS LESS BDTR 250
C THAN 0.5 OR GREATER THAN 1.0, OR EITHER A OR BDTR 260
C B IS LESS THAN 0.5 OR GREATER THAN 10*(1+5). BDTR 270
C P AND D ARE SET TO -1.E75. BDTR 280
C IER=+2 --- INVALID OUTPUT. P IS LESS THAN ZERO OR BDTR 290
C GREATER THAN ONE. P IS SET TO 1.E75. BDTR 300
C ..... BDTR 310
C REMARKS BDTR 320
C SEE MATHEMATICAL DESCRIPTION. BDTR 330
C ..... BDTR 340
C SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED BDTR 350
C DLGAM BDTR 360
C NDTR BDTR 370
C CCTR BDTR 380
C ..... BDTR 390
C METHOD BDTR 400
C REFER TO R.E. BARGMANN AND S.P. GHOSH, STATISTICAL BDTR 410
C DISTRIBUTION PROGRAMS FOR A COMPUTER LANGUAGE, BDTR 420
C IBM RESEARCH REPORT RC-1094, 1963. BDTR 430
C ..... BDTR 440
C ..... BDTR 450
C ..... BDTR 460
0001 SUBROUTINE BDTR(X,A,B,P,D,IER) BDTR 480
0002 DOUBLE PRECISION XX,DLXX,DL1X,AA,BB,G1,G2,G3,G4,DD,PP,XD,FF,FN, BDTR 490
IXI,SS,CC,RR,DLBETA BDTR 500
C TEST FOR VALID INPUT DATA BDTR 510
C ..... BDTR 520
0003 IF(A-(.5-1.E-5)) 640,10,10 BDTR 530
0004 10 IF(B-(.5-1.E-5)) 640,20,20 BDTR 540
0005 20 IF(A-1.E+5) 30,30,640 BDTR 550
0006 30 IF(B-1.E+5) 40,40,640 BDTR 560
0007 40 IF(X) 640,50,50 BDTR 570
0008 50 IF(1.-X) 640,60,60 BDTR 580

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	C		BDTR 590
	C	COMPUTE LOG(BETA(A,B))	BDTR 600
	C		BDTR 610
0009		60 AA=DBLE(A)	BDTR 620
0010		BB=DBLE(B)	BDTR 630
0011		CALL DLGAM(AA,G1,I0K)	BDTR 640
0012		CALL DLGAM(BB,G2,I0K)	BDTR 650
0013		CALL DLGAM(AA+BB,G3,I0K)	BDTR 660
0014		DLBETA=G1+G2-G3	BDTR 670
	C		BDTR 680
	C	TEST FOR X NEAR 0.0 OR 1.0	BDTR 690
	C		BDTR 700
0015		IF(X-1.E-8) 80,80,70	BDTR 710
0016		70 IF((1.-X)-1.E-8) 130,130,140	BDTR 720
0017		80 P=0.0	BDTR 730
0018		IF(A-1.) 90,100,120	BDTR 740
0019		90 D=1.E+75	BDTR 750
0020		GO TO 660	BDTR 760
0021		100 DD=-DLBETA	BDTR 770
0022		IF(DD+1.68002) 120,120,110	BDTR 780
0023		110 DD=DEXP(DD)	BDTR 790
0024		D=SNGL(DD)	BDTR 800
0025		GO TO 660	BDTR 810
0026		120 D=0.0	BDTR 820
0027		GO TO 660	BDTR 830
0028		130 P=1.0	BDTR 840
0029		IF(B-1.) 90,100,120	BDTR 850
	C		BDTR 860
	C	SET PROGRAM PARAMETERS	BDTR 870
	C		BDTR 880
0030		140 XX=DBLE(X)	BDTR 890
0031		DLXX=DLOG(XX)	BDTR 900
0032		DL1X=DLOG(1.D0-XX)	BDTR 910
0033		XO=XX/(1.D0-XX)	BDTR 920
0034		ID=0	BDTR 930
	C		BDTR 940
	C	COMPUTE ORDINATE	BDTR 950
	C		BDTR 960
0035		DD=(AA-1.D0)*DLXX+(BB-1.D0)*DL1X-DLBETA	BDTR 970
0036		IF(DD-1.68002) 150,150,160	BDTR 980
0037		150 IF(DD+1.68002) 170,170,180	BDTR 990
0038		160 D=1.E75	BDTR1000
0039		GO TO 190	BDTR1010
0040		170 C=0.0	BDTR1020
0041		GO TO 190	BDTR1030
0042		180 DD=DEXP(DD)	BDTR1040
0043		C=SNGL(DD)	BDTR1050
	C		BDTR1060
	C	A OR B OR BOTH WITHIN 1.E-8 OF 1.0	BDTR1070
	C		BDTR1080
0044		190 IF(ABS(A-1.)-1.E-8) 200,200,210	BDTR1090
0045		200 IF(ABS(B-1.)-1.E-8) 220,220,230	BDTR1100
0046		210 IF(ABS(B-1.)-1.E-8) 260,260,290	BDTR1110
0047		220 P=X	BDTR1120
0048		GO TO 660	BDTR1130
0049		230 PP=BB*DL1X	BDTR1140
0050		IF(PP+1.68002) 240,240,250	BDTR1150
0051		240 P=1.0	BDTR1160

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0052	GO TO 660	BDTR1170
0053	250 PP=DEXP(PP)	BDTR1180
0054	PP=1.00-PP	BDTR1190
0055	P=SNGL(PP)	BDTR1200
0056	GO TO 600	BDTR1210
0057	260 FP=AA*DLXX	BDTR1220
0058	IF(PP+1.68D02) 270,270,280	BDTR1230
0059	270 P=0.0	BDTR1240
0060	GO TO 660	BDTR1250
0061	280 PP=DEXP(PP)	BDTR1260
0062	P=SNGL(PP)	BDTR1270
0063	GO TO 600	BDTR1280
C		BDTR1290
C	TEST FOR A OR B GREATER THAN 1000.0	BDTR1300
C		BDTR1310
0064	290 IF(A-1000.) 300,300,310	BDTR1320
0065	300 IF(B-1000.) 330,330,320	BDTR1330
0066	310 XX=2.00*AA/X0	BDTR1340
0067	XS=SNGL(XX)	BDTR1350
0068	AA=2.00*BB	BDTR1360
0069	CF=SNGL(AA)	BDTR1370
0070	CALL CDTR(XS,DF,P,DUMMY,IER)	BDTR1380
0071	P=1.0-P	BDTR1390
0072	GO TO 670	BDTR1400
0073	320 XX=2.00*BB*X0	BDTR1410
0074	XS=SNGL(XX)	BDTR1420
0075	AA=2.00*AA	BDTR1430
0076	CF=SNGL(AA)	BDTR1440
0077	CALL CDTR(XS,DF,P,DUMMY,IER)	BDTR1450
0078	GO TO 670	BDTR1460
C		BDTR1470
C	SELECT PARAMETERS FOR CONTINUED FRACTION COMPUTATION	BDTR1480
C		BDTR1490
0079	330 IF(X-.5) 340,340,380	BDTR1500
0080	340 IF(AA-1.00) 350,350,360	BDTR1510
0081	350 RR=AA+1.00	BDTR1520
0082	GO TO 370	BDTR1530
0083	360 RR=AA	BDTR1540
0084	370 CD=DLXX/5.00	BDTR1550
0085	CD=DEXP(CD)	BDTR1560
0086	CD=(RR-1.00)-(RR+BB-1.00)*XX*CD +2.00	BDTR1570
0087	IF(CD) 420,420,430	BDTR1580
0088	380 IF(BB-1.00) 390,390,400	BDTR1590
0089	390 RR=BB+1.00	BDTR1600
0090	GO TO 410	BDTR1610
0091	400 RR=BB	BDTR1620
0092	410 CD=DLXX/5.00	BDTR1630
0093	CD=DEXP(CD)	BDTR1640
0094	CD=(RR-1.00)-(AA+RR-1.00)*(1.00-XX)*CD +2.00	BDTR1650
0095	IF(CD) 430,430,420	BDTR1660
0096	420 ID=1	BDTR1670
0097	FF=DLXX	BDTR1680
0098	CLXX=DLXX	BDTR1690
0099	CLXX=FF	BDTR1700
0100	X0=1.00/X0	BDTR1710
0101	FF=AA	BDTR1720
0102	AA=BB	BDTR1730
0103	BB=FF	BDTR1740

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C104	G2=G1	BDTR1750
C		BDTR1760
C	TEST FOR A LESS THAN 1.0	BDTR1770
C		BDTR1780
C105	430 FF=0.00	BDTR1790
C106	IF(AA-1.00) 440,440,470	BDTR1800
C107	440 CALL DLGAM(AA+1.00,G4,IOK)	BDTR1810
C108	ED=AA*DLXX+BB*DL1X+G3-G2-G4	BDTR1820
C109	IF(DD+1.68D02) 460,460,450	BDTR1830
C110	450 FF=FF+DEXP(DD)	BDTR1840
C111	460 AA=AA+1.00	BDTR1850
C		BDTR1860
C	COMPUTE P USING CONTINUED FRACTION EXPANSION	BDTR1870
C		BDTR1880
C112	470 FN=AA+BB-1.00	BDTR1890
C113	RR=AA-1.00	BDTR1900
C114	II=80	BDTR1910
C115	XI=DFLOAT(II)	BDTR1920
C116	SS=((BB-XI)*(RR+XI))/((RR+2.00*XI-1.00)*(RR+2.00*XI))	BDTR1930
C117	SS=SS*X0	BDTR1940
C118	DO 480 I=1,79	BDTR1950
C119	II=80-I	BDTR1960
C120	XI=DFLOAT(II)	BDTR1970
C121	ED=(XI*(FN+XI))/((RR+2.00*XI+1.00)*(RR+2.00*XI))	BDTR1980
C122	ED=ED*X0	BDTR1990
C123	CC=((BB-XI)*(RR+XI))/((RR+2.00*XI-1.00)*(RR+2.00*XI))	BDTR2000
C124	CC=CC*X0	BDTR2010
C125	SS=CC/(1.00+ED/(1.00-SS))	BDTR2020
C126	480 CONTINUE	BDTR2030
C127	SS=1.00/(1.00-SS)	BDTR2040
C128	IF(SS) 650,650,490	BDTR2050
C129	490 CALL DLGAM(AA+BB,G1,ICK)	BDTR2060
C130	CALL DLGAM(AA+1.00,G4,IOK)	BDTR2070
C131	CC=G1-G2-G4+AA*DLXX+(BB-1.00)*DL1X	BDTR2080
C132	PP=CC+DLOG(SS)	BDTR2090
C133	IF(PP+1.68D02) 500,500,510	BDTR2100
C134	500 PP=FF	BDTR2110
C135	GO TO 520	BDTR2120
C136	510 PP=DEXP(PP)+FF	BDTR2130
C137	520 IF(ID) 540,540,530	BDTR2140
C138	530 PP=1.00-PP	BDTR2150
C139	540 P=SNGL(PP)	BDTR2160
C		BDTR2170
C	SET ERROR INDICATOR	BDTR2180
C		BDTR2190
C140	IF(P) 550,570,570	BDTR2200
C141	550 IF(ABS(P)-1.E-7) 560,560,650	BDTR2210
C142	560 P=0.0	BDTR2220
C143	GO TO 660	BDTR2230
C144	570 IF(1.-P) 580,600,600	BDTR2240
C145	580 IF(ABS(1.-P)-1.E-7) 590,590,650	BDTR2250
C146	590 P=1.0	BDTR2260
C147	GO TO 660	BDTR2270
C148	600 IF(P-1.E-8) 610,610,620	BDTR2280
C149	610 P=0.0	BDTR2290
C150	GO TO 660	BDTR2300
C151	620 IF((1.0-P)-1.E-8) 630,630,660	BDTR2310
C152	630 P=1.0	BDTR2320

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```
C153      GO TO 660
C154      640 IER=-2
C155      C=-1.E75
C156      P=-1.E75
C157      GO TO 670
C158      650 IER=+2
C159      P= 1.E75
C160      GO TO 670
C161      660 IER=0
C162      670 RETURN
C163      END
```

```
BDTR2330
BDTR2340
BDTR2350
BDTR2360
BDTR2370
BDTR2380
BDTR2390
BDTR2400
BDTR2410
BDTR2420
BDTR2430
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CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C
C   THE PURPOSE OF THIS PROGRAM IS TO OBTAIN THE PROBABILITIES
C   UNDER A RESULTANT DISTRIBUTION BY COMBINING TWO BETA
C   UNDER A RESULTANT DISTRIBUTION BY COMBINING TWO BETA DISTRIBUTIONS
C   TIONS  $B(M,N)$  AND  $B(N,M)$ , M AND N BEING THE PARAMETERS. WHEN N AND
C   M ARE EQUAL THE RESULTANT DISTRIBUTION IS ALSO A BETA DISTRIBUTION
C   WITH PARAMETERS M AND N, BOTH BEING EQUAL
C
C   DESCRIPTION OF PARAMETERS---
C
C   RESP= PROBABILITY OF EQUAL INTERVALS ON THE RANGE OF BETA DISTRIBUTION
C
C   FINP=PROBABILITY OF EQUAL INTERVALS ON THE RANGE OF THE RESULTANT
C   DISTRIBUTION
C
C   FRECY=THEORETICAL FREQUENCY OF THE TRACKING SIGNAL
C
C   NTRSIG=OBSERVED FREQUENCY OF THE TRACKING SIGNAL
C
C   NCELL= NUMBER OF POINTS ON THE RANGE OF THE BETA DISTRIBUTION
C   AT WHICH THE PROBABILITIES ARE TO BE EVALUATED.THIS INCLUDES
C   END POINT ZERO ALSO.
C
C   NCELLL=NUMBER OF INTERVALS ON THE RANGE OF THE BETA DISTRIBUTION.
C
C   NTIME= NUMBER OF TIMES THE PROGRAM IS USED TO COMPARE THE TRACKING
C   SIGNAL FREQUENCIES WITH DIFFERENT RESULTANT DISTRIBUTIONS
C
C   NRUN=NUMBER OF RUNS TO BE MADE WITH DIFFERENT VALUES OF SMOOTHING
C   CONSTANTS.
C
C   STEP1= INCREMENT IN THE VALUE OF X.THIS INCREMENT DEPENDS ON THE
C   NUMBER OF INTERVALS.
C
C   NUMBER=MULTIPLYING FACTOR,WHICH IS THE SAME AS NUMBER OF TRACKING
C   SIGNALS GENERATED TO OBTAIN THE ACTUAL FREQUENCY OF THE TRACKING
C   SIGNAL.WHEN THE PROBABILITY FINP(I) IS MULTIPLIED BY THIS NUMBER
C   THE THEORETICAL FREQUENCY OF THE TRACKING SIGNAL IS OBTAINED.
C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C
C001   DIMENSION P(90),RESP(80),FINP(80),FRECY(80),NTRSIG(80)
C002   1 FORMAT (4I8)
C003   11 FORMAT (4F9.5)
C004   12 FORMAT(5F9.6,I5)
C005   18 FORMAT(3X,'(X)',7X,'(M)',6X,'(N)',5X,'P(X)',6X,'D',5X,'IER')
C006   28 FORMAT (2F11.6,F11.2)
C007   50 FORMAT (1H-,16X,'MEAN',15X,'ST.DEV.')
C008   60 FORMAT (2(10X,E14.6))
C009   80 FORMAT (20I4)
C010   90 FORMAT (1H-,'THE CHI-SQUARE VALUE IS =',E14.6)
C011   98 FORMAT (1H-,3X,'RESP(I)',5X,'FINP(I)',3X,'FRECY(I)')
C012   99 FORMAT ('1','OBSERVED FREQUENCY OF THE TRACKING SIGNAL')
C013   100 FORMAT(1H-,20I6)
C014   READ 1,NCELL,NTIME,NRUN,NUMBER
C015   NCELLL=NCELL-1
C016   DO 70 JJ=1,NRUN

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C
C   READ THE OBSERVED FREQUENCIES OF THE TRACKING SIGNAL TO CALCULATE
C   THE CHI-SQUARE VALUE.
C
CC17   READ 80,(NTRSIG(I),I=1,NCELLL)
CC18   PRINT 99
CC19   PRINT 100,(NTRSIG(I),I=1,NCELLL)
CC20   DO 40 J=1,NTIME
CC21   READ 11,X,A,B,STEP1
CC22   PRINT 18
CC23   DO 26 J=1,NCELL

C
C   CALCULATE PROBABILITY AT THE EQUIDISTANT POINTS ON THE RANGE OF
C   THE BETA DISTRIBUTION.THIS IS CUMULATIVE PROBABILITY.
C
CC24   CALL BDTR(X,A,B,PR,D,IER)
CC25   P(I)=PR
CC26   PRINT 12,X,A,B,P(I),D,IER

C
C   CHECK WHETHER PROBABILITY AT THE LAST POINT ON THE RANGE IS
C   EVALUATED.
CC27   IF (X-1.0) 13,14,14

C
C   IF NOT GIVE AN INCREMENT IN THE VALUE OF X.
C
CC28   13 X=X+STEP1
CC29   26 CONTINUE
CC30   14 DO 10 I=2,NCELL
CC31   IF (I-2) 10,31,31

C
C   OBTAIN PROBABILITY OF INDIVIDUAL INTERVAL FROM CUMULATIVE
C   PROBABILITY BY SUBTRACTION
CC32   31 RESP(I-1)=P(I)-P(I-1)
CC33   10 CONTINUE
CC34   CHISQ=0.0
CC35   DO 33 I=1,NCELLL

C
C   CALCULATE THE PROBABILITIES OF THESE INTERVALS UNDER THE RESULTANT
C   DISTRIBUTION.
CC36   FINP(I)=(RESP(I)+RESP(NCELL-I))/2.0

C
C   OBTAIN THE THEORETICAL FREQUENCIES.
C
CC37   FREQCY(I)=FINP(I)*NUMBER

C
C   CALCULATE THE CHI-SQUARE VALUE.
C
CC38   CHISQ=CHISQ+((NTRSIG(I)-FREQCY(I))**2)/FREQCY(I)
CC39   33 CONTINUE
CC40   DO 27 I=1,NCELLL
CC41   PRINT 98
CC42   PRINT 28,RESP(I),FINP(I),FREQCY(I)
CC43   27 CONTINUE
CC44   SUMX=0.0
CC45   SSUMX=0.0
CC46   X=STEP1
CC47   DO 45 I=1,NCELLL
CC48   SUMX=SUMX+X*FINP(I)

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0049      SSUMX=SSUMX+X**2*FINP(I)
0050      X=X+STEP1
0051      45 CONTINUE

      C
      C      CALCULATE THE MEAN AND STANDARD DEVIATION OF THE RESULTANT
      C      DISTRIBUTION.
0052      XMEAN=SUMX
0053      XSTDEV=(SSUMX-SUMX**2)**0.5
0054      PRINT 50
0055      PRINT 60,XMEAN,XSTDEV
0056      PRINT 90,CHISQ
0057      40 CONTINUE
0058      70 CONTINUE
0059      STOP
0060      END
```

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CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C
C   THIS PROGRAM CALCULATES THE PROBABILITY OF DETECTING A PROCESS
C   CHANGE, WHEN THE PROCESS LEVEL IS SUBJECTED TO A STEP. THIS PROGRAM
C   CAN BE USED ONLY WHEN THE DETECTION CRITERIA IS--ONE VALUE OF
C   THE TRACKING SIGNAL AMONG ANY NUMBER OF SUCCEEDING VALUES ,
C   EXCEEDS THE LIMITING VALUE AFTER STEP IS INCORPORATED.
C
C   DESCRIPTION OF THE PARAMETERS---
C
C   NALPHA=NUMBER OF SMOOTHING CONSTANTS FOR WHICH SIMULATION IS TO
C   BE CARRIED OUT
C
C   NSIMU=NUMBER OF SIMULATIONS TO BE CARRIED OUT.
C
C   NSTEP=NUMBER OF STEPS OF DIFFERENT MAGNITUDE INCORPORATED IN THE
C   PROCESS LEVEL.
C
C   NUMBER=PERIOD AT WHICH THE STEP IS TO BE INCORPORATED
C
C   ALPHA=SMOOTHING CONSTANT
C
C   XEAN=PROCESS MEAN
C
C   STDDEV=STANDARD DEVIATION OF RANDOM NOISE
C
C   XINC=A MULTIPLIER WHICH ALTERS THE MAGNITUDE OF STEP TO BE
C   INCORPORATED IN THE PROCESS MEAN
C
C   XLIMIT=LIMITING VALUE OF THE TRACKING SIGNAL TO BE SPECIFIED BY
C   THE USER
C
C   NCOUNT=NUMBER TO BE SPECIFIED WHICH IS HALF THE NUMBER OF THE
C   TRACKING SIGNALS TO BE GENERATED.
C
C   BY PROPERLY SELECTING VALUES FOR NCOUNT AND NUMBER THE CRITERIA
C   FOR DETECTING THE PROCESS CHANGE CAN BE VARIED. FOR EXAMPLE, WHEN
C   NCOUNT IS 30 AND NUMBER IS 26, 10 SUCCEEDING VALUES OF THE TRACKING
C   SIGNAL WILL BE TESTED FOR CONFIRMING A CHANGE IN THE PROCESS
C   AFTER STEP IS INCORPORATED.
C
0001   DIMENSION ICOUNT(20), KCOUNT(20), SMAD(20), SSE(20), XD(20), TRSIG(20), X
      1FAT(20), PROB(20), ERR(20), XKOUNT(20)
0002   1 FORMAT(4I4, 5F8.4)
0003   2 FORMAT('1', 'NSIMU', 5X, 'NSTEP', 5X, 'NCOUNT', 5X, 'NUMBER', 6X, 'ALPHA',
      16X, 'XEAN', 5X, 'STDDEV', 6X, 'XINC', 6X, 'XLIMIT')
0004   3 FORMAT('16, 7X, 12, 8X, 12, 9X, 12, 8X, F5.3, 5X, F5.2, 7X, F3.1, 7X, F5.3, 5X
      1, F5.3)
0005   6 FORMAT (3I8)
0006   140 FORMAT (1H-, 11F8.4)
0007   READ 6, IY, IX, NALPHA
0008   DO 5 IJ = 1, NALPHA
0009   READ 1, NSIMU, NSTEP, NCOUNT, NUMBER, ALPHA, XEAN, STDDEV, XINC, XLIMIT
0010   PRINT 2
0011   PRINT 3, NSIMU, NSTEP, NCOUNT, NUMBER, ALPHA, XEAN, STDDEV, XINC, XLIMIT
0012   FACT=2./(2.-ALPHA)
0013   DO 8 I=1, NSTEP
0014   8 KOUNT(I)=0

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CC15      DO 10 L=1,NSIMU
CC16      DO 20 I=1,NSTEP
CC17      ICOUNT(I)=0
CC18      SMAD(I)=0.79788*FACT*STDDEV
CC19      SSE(I)=0.0
CC20      XHAT(I)=XEAN
CC21      20 CONTINUE
CC22      BETA=1.-ALPHA

C
C      GENERATE RANDOM NUMBER BETWEEN ZERO AND ONE
C
CC23      DO 30 I=1,NCOUNT
CC24      IY=IY*IX
CC25      IF(IY.LT.0) IY=IY+2147483647+1
CC26      RA=IY*.4656613E-9
CC27      IY=IY*IX
CC28      IF(IY.LT.0) IY=IY+2147483647+1
CC29      RB=IY*.4656613E-9
CC30      LA=SQRT(-2.0*ALOG(RA))
CC31      UB=6.2832*RB

C
C      CALCULATE TWO RANDOM NORMAL DEVIATES
C
CC32      XA=UA*COS(UB)
CC33      XB=UA*SIN(UB)

C
C      CHECK IF TIME HAS REACHED TO INCORPORATE THE STEP
C
CC34      IF ((I-NUMBER) 40,50,50
CC35      40 X=XA*STDDEV+XEAN
CC36      RD=XB*STDDEV+XEAN

C
C      CARRY OUT SMOOTHING PROCESS
C
CC37      DO 45 II=1,2
CC38      DO 46 J=1,NSTEP
CC39      XD(J)=X
CC40      ERR(J)=XD(J)-XHAT(J)
CC41      SSE(J)=ALPHA*ERR(J)+BETA*SSE(J)
CC42      SMAD(J)=ALPHA*ABS(ERR(J))+BETA*SMAD(J)
CC43      TRSIG(J)=SSE(J)/SMAD(J)

C
C      SMOOTHING CARRIED OUT ON THE OBSERVED VALUE OF THE PROCES TO
C      EVALUATE THE NEXT FORECAST
C
CC44      XHAT(J)=ALPHA*XD(J)+BETA*XHAT(J)
CC45      46 CONTINUE
CC46      X=RD
CC47      45 CONTINUE
CC48      GO TO 30
CC49      50 X=XA*STDDEV+XEAN
CC50      RD=XB*STDDEV+XEAN
CC51      DO 70 K=1,2

C
C      INCORPORATE STEP OF DIFFERENT MAGNITUDE IN THE OBSERVATIONS OF
C      THE PROCESS
C
CC52      DO 80 J=1,NSTEP

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0053      XD(J)=X+(J-1)*XINC
0054      ERR(J)=XD(J)-XHAT(J)
0055      SSE(J)=ALPHA*ERR(J)+BETA*SSE(J)
0056      SMAD(J)=ALPHA*ABS(ERR(J))+BETA*SMAD(J)

      C
      C      EVALUATE THE TRACKING SIGNAL
      C
0057      TRSIG(J)=SSE(J)/SMAD(J)

      C
      C      CHECK IF THE TRACKING SIGNAL HAS EXCEEDED THE LIMITING VALUE
      C
0058      IF (ABS(TRSIG(J))-XLIMIT) 65,75,75

      C
      C      IF IT HAS EXCEEDED DETECT A CHANGE IN THE PROCESS BY MOVING THE
      C      DETECTION COUNTER ICOUNT. ICOUNT WILL HAVE A VALUE 0 OR 1.
      C      0 FOR NO CHANGE IN THE PROCESS AND 1 FOR CHNAGE IN THE PROCESS
      C
0059      75 ICOUNT(J)=1
0060      65 XHAT(J)=ALPHA*XD(J)+BETA*XHAT(J)
0061      80 CONTINUE
0062      X=RD
0063      70 CONTINUE
0064      30 CONTINUE

      C
      C      COUNT THE NUMBER OF TIMES A CHANGE HAS BEEN DETECTED IN THE TOTAL
      C      NUMBER OF SIMULATIONS CARRIED OUT
      C
0065      DO 90 J=1,NSTEP
0066      KOUNT(J)=KOUNT(J)+ICOUNT(J)
0067      90 CONTINUE
0068      10 CONTINUE
0069      XNSIMU=NSIMU

      C
      C      CALCULATE PROBABILITY CF DETECTING A CHANGE WITH DIFFERENT
      C      MAGNITUDE OF STEP INCREASE IN THE PROCESS LEVEL
      C
0070      DO 120 I=1,NSTEP
0071      XKOUNT(I)=KOUNT(I)
0072      120 PROB(I)=XKOUNT(I)/XNSIMU
0073      PRINT 140,(PROB(I),I=1,NSTEP)
0074      5 CONTINUE
0075      STOP
0076      END

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CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
C
C   THIS PROGRAM CALCULATES THE PROBABILITY OF DETECTING A PROCESS C
C   CHANGE, WHEN THE PROCESS LEVEL IS SUBJECTED TO A STEP. THE PRO- C
C   GRAM CAN BE USED ONLY WHEN THE CRITERIA FOR DETECTION IS BASED C
C   ON A SUCCESSIVE NUMBER OF THE TRACKING SIGNALS EXCEEDING THE C
C   LIMITING VALUE AMONG ANY NUMBER OF SUCCEEDING VALUES, AFTER A C
C   STEP IN THE LEVEL OF THE PROCESS IS INCORPORATED. C
C
C   DESCRIPTION OF THE PARAMETERS--- C
C
C   NALPHA=NUMBER OF SMOOTHING CONSTANTS FOR WHICH SIMULATION IS TO C
C   BE CARRIED OUT C
C
C   NSIMU=NUMBER OF SIMULATIONS TO BE CARRIED OUT. C
C
C   NSTEP=NUMBER OF STEPS OF DIFFERENT MAGNITUDE INCORPORATED IN THE C
C   PROCESS LEVEL. C
C
C   NUMBER=PERIOD AT WHICH THE STEP IS TO BE INCORPORATED C
C
C   ALPHA=SMOOTHING CONSTANT C
C
C   XEAN=PROCESS MEAN C
C
C   STDDEV=STANDARD DEVIATION OF RANDOM NOISE C
C
C   XINC=A MULTIPLIER WHICH ALTERS THE MAGNITUDE OF STEP TO BE C
C   INCORPORATED IN THE PROCESS MEAN C
C
C   XLIMIT=LIMITING VALUE OF THE TRACKING SIGNAL TO BE SPECIFIED BY C
C   THE USER C
C
C   NCOUNT=NUMBER TO BE SPECIFIED WHICH IS HALF THE NUMBER OF THE C
C   TRACKING SIGNALS TO BE GENERATED. C
C
CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
0001  DIMENSION ICOUNT(20), KCUNT(20), SMAD(20), SSE(20), XD(20), TRSIG(20), X
      I-AT(20), PROB(20), ERR(20), XKOUNT(20), IDETECT(20)
0002  1 FORMAT(4I4, 5F8.4)
0003  2 FORMAT('1', 'NSIMU', 5X, 'NSTEP', 5X, 'NCOUNT', 5X, 'NUMBER', 6X, 'ALPHA',
      16X, 'XEAN', 5X, 'STDDEV', 6X, 'XINC', 6X, 'XLIMIT')
0004  3 FORMAT('16, 7X, I2, 8X, I2, 9X, I2, 8X, F5.3, 5X, F5.2, 7X, F3.1, 7X, F5.3, 6X
      1, F5.3)
0005  6 FORMAT(3I8)
0006  140 FORMAT(1H-, 11F8.4)
0007  READ 6, IY, IX, NALPHA
0008  DO 5 IJ = 1, NALPHA
0009  READ 1, NSIMU, NSTEP, NCOUNT, NUMBER, ALPHA, XEAN, STDDEV, XINC, XLIMIT
0010  PRINT 2
0011  PRINT 3, NSIMU, NSTEP, NCOUNT, NUMBER, ALPHA, XEAN, STDDEV, XINC, XLIMIT
0012  FACT = 2. / (2. - ALPHA)
0013  DO 8 I = 1, NSTEP
0014  8 KOUNT(I) = 0
0015  DO 10 L = 1, NSIMU
0016  DO 20 I = 1, NSTEP
0017  ICOUNT(I) = 0
0018  SMAD(I) = 0.79788 * FACT * STDDEV

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CC19      SSE(I)=0.0
CC20      XHAT(I)=XEAN
CC21      20 CONTINUE
CC22      BETA=1.-ALPHA

      C
      C      GENERATE RANDOM NUMBER BETWEEN ZERO AND ONE
      C

0023      DO 30 I=1,NCOUNT
CC24      IY=IY*IX
CC25      IF(IY.LT.0) IY=IY+2147483647+1
CC26      RA=IY*.4656613E-9
CC27      IY=IY*IX
CC28      IF(IY.LT.0) IY=IY+2147483647+1
CC29      RB=IY*.4656613E-9
CC30      LA=SQRT(-2.0*ALOG(RA))
CC31      LB=6.2832*RB

      C
      C      CALCULATE TWO RANDOM NORMAL DEVIATES
      C

0032      XA=UA*COS(UB)
0033      XB=UA*SIN(UB)

      C
      C      CHECK IF TIME HAS REACHED TO INCORPORATE THE STEP
      C

0034      IF (I-NUMBER) 40,50,50
CC35      40 X=XA*STODEV+XEAN
CC36      RD=XB*STODEV+XEAN

      C
      C      CARRY OUT SMOOTHING PROCESS
      C

0037      DO 45 II=1,2
0038      DO 46 J=1,NSTEP
CC39      XD(J)=X
0040      ERR(J)=XD(J)-XHAT(J)
0041      SSE(J)=ALPHA*ERR(J)+BETA*SSE(J)
CC42      SMAD(J)=ALPHA*ABS(ERR(J))+BETA*SMAD(J)
0043      TRSIG(J)=SSE(J)/SMAD(J)

      C
      C      SMOOTHING CARRIED OUT ON THE OBSERVED VALUE OF THE PROCES TO
      C      EVALUATE THE NEXT FORECAST
      C

0044      XHAT(J)=ALPHA*XD(J)+BETA*XHAT(J)
CC45      46 CONTINUE
CC46      X=RD
0047      45 CONTINUE
CC48      GO TO 30
0049      50 X=XA*STODEV+XEAN
0050      RD=XB*STODEV+XEAN
0051      DO 70 K=1,2

      C
      C      INCORPORATE STEP OF DIFFERENT MAGNITUDE IN THE OBSERVATIONS OF
      C      THE PROCESS
      C

CC52      DO 80 J=1,NSTEP
CC53      XD(J)=X+(J-1)*XINC
CC54      ERR(J)=XD(J)-XHAT(J)
CC55      SSE(J)=ALPHA*ERR(J)+BETA*SSE(J)
0056      SMAD(J)=ALPHA*ABS(ERR(J))+BETA*SMAD(J)

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      C
      C      EVALUATE THE TRACKING SIGNAL
      C
0057      TRSIG(J)=SSE(J)/SMAD(J)
      C
      C      CHECK IF THE TRACKING SIGNAL HAS EXCEEDED THE LIMITING VALUE
      C
0058      IF (ABS(TRSIG(J))-XLIMIT) 65,75,75
      C
      C      IF YES COUNT THE NUMBER OF TIMES THE TRACKING SIGNAL EXCEEDS THE
      C      LIMITING VALUE SUCCESSIVELY.
      C
0059      75 ICOUNT(J)=ICOUNT(J)+1
      C
      C      DETECT ACHANGE IN THE PROCESS IF TWO OR MORE SUCCESSIVE VALUES
      C      OF THE TRACKING SIGNAL EXCEED THE LIMITING VALUE.
      C
0060      IF (ICOUNT(J).GE.2) IDTECT(J)=1
0061      GO TO 200
0062      65 ICOUNT(J)=0
0063      200 XHAT(J)=ALPHA*XD(J)+BETA*XHAT(J)
0064      80 CONTINUE
0065      X=RD
0066      70 CONTINUE
0067      30 CONTINUE
      C
      C      COUNT THE NUMBER OF TIMES A CHANGE HAS BEEN DETECTED IN THE TOTAL
      C      NUMBER OF SIMULATIONS CARRIED OUT
      C
0068      DO 90 J=1,NSTEP
0069      KOUNT(J)=KOUNT(J)+IDTECT(J)
0070      90 CONTINUE
0071      10 CONTINUE
0072      XNSIMU=NSIMU
      C
      C      CALCULATE PROBABILITY OF DETECTING A CHANGE WITH DIFFERENT
      C      MAGNITUDE OF STEP INCREASE IN THE PROCESS LEVEL
      C
0073      DO 120 I=1,NSTEP
0074      XKOUNT(I)=KOUNT(I)
0075      120 PROB(I)=XKOUNT(I)/XNSIMU
0076      PRINT 140,(PROB(I),I=1,NSTEP)
0077      5 CONTINUE
0078      STOP
0079      END

```

DETERMINATION OF THE TRACKING SIGNAL CONTROL LIMITS

by

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ABSTRACT

The purpose of this thesis is twofold:

- 1) To approximate the tracking signal distribution with some known statistical distribution.
- 2) To evaluate the limiting values of the tracking signal.

Attempts were made to approximate the tracking signal distribution for three different values of α (0.01, 0.1, 0.2). For an α of 0.01 and 0.1, the approximating distribution was a single beta distribution. Whereas for an α of 0.2, the approximating distribution was a resultant distribution obtained by combining two beta distributions appropriately. The procedure essentially involved generation of the tracking signal distribution and the approximating distribution and their comparison. The goodness of fit was tested by a chi-square test and a Kolmogorov Smirnov test. The results obtained are tabulated below:

ALPHA	CHI-SQUARE TEST	KOLMOGOROV SMIRNOV TEST
0.01	Inadequate	Inadequate
0.1	Inadequate	Adequate
0.2	Inadequate	Inadequate

These results lead to a conclusion that the tracking signal distribution cannot be adequately approximated with a beta or combined beta distribution. Thus, it was not possible to evaluate the tracking signal limits by the above procedure. The limits were then evaluated by simulation.

In the latter phase of this thesis, the effectiveness of the tracking signal in detecting a process change was studied by simulation. For detecting a process change various criteria were formulated. Essentially, all the criteria were based on testing a few tracking signal values after a step increase is incorporated in the process mean. For the first three criteria, the number of the tracking signals tested were 2, 4 and 10 respectively. A change in the process was detected when one value among these tested values exceeded the specified limit. In the fourth criterion, 10 values were tested but a change was detected when any two successive values among these 10, exceeded the specified limit. Theoretically, the first detection criterion is the best one as it gives an indication of a process change at a very early stage. However, the results revealed that the tracking signal is very insensitive to process changes, with first detection criterion. As compared with other criteria, the first criterion registered a low probability of detecting process changes. Based on the probabilities from third and fourth criterion, the tracking signal was comparatively effective in detecting process changes. However, with these two criteria, a corrective action to be undertaken is delayed.