DIFFERENTIAL CROSS SECTIONS FOR CHARGE TRANSFER USING SCREENED COULOMB POTENTIALS IN THE EIKONAL APPROXIMATION

by

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I would like to dedicate this work to my mother who has labored to provide me with my education. And most importantly, I would like to thank my loving wife who has provided for my health and emotional well being and shares with me in a dream.

CHAPTER 1

INTRODUCTION

Charge transfer or, sometimes, electron capture is a type of rearrangement collision. This is depicted in the reaction,

$$A + (e + B) \rightarrow (A + e) + B$$
,

where A represents the projectile system, B the target system, and e the transferred electron. Due to the Coulomb interactions influencing the projectile's path, the projectile will scatter at various angles depending on the impact parameter, see Figure 1. Looking at many scattering events corresponding to various impact parameters, an angular distribution will arise. Calculation of the charge transfer angular distributions from the K shell by proton impact is presented in this thesis.

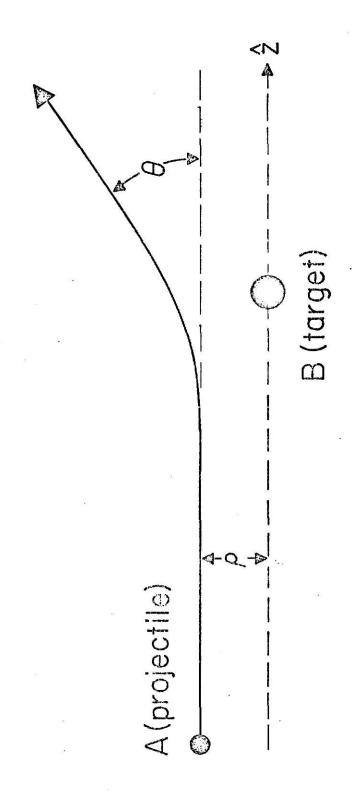
Thus far, charge transfer calculations yield non rigorous total cross sections for K shell capture. The most extensively used method for determining electron capture cross sections is the first Born approximation or, simply, the Born approximation. This method is used for its simplicity and not necessarily for its validity. It is known that the second Born term dominates at very high energies and second order calculations are now being pursued. In this presentation, the simplicity of the first order calculation is retained while viewing the differential cross section for charge transfer.

Examination of the differential cross section can give a deeper understanding of the charge transfer process. The perturbing potential for charge transfer is still somewhat unclear. Since the differential

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Figure 1. Scattering of an ion from an atomic target, where ρ is the impact parameter and θ is the scattering angle.



cross section is sensitive to how the Hamiltonian is broken up, detailed information of the charge transfer process is possible. Thus, calculations of angular distributions could lend credance to ideas as to how the Hamiltonian for charge transfer should be broken up in first order perturbation theory.

One of the first charge transfer calculations was done by Brinkman and Kramers² in 1930. Their calculation was performed adhering to the point of view that the relevant interaction potential was between the projectile and (captured) electron. It is argued that the internuclear interaction, which is largely responsible for the path of the projectile, contributes little to the total capture cross section for heavy particles. For most capture cross sections, the resulting BK total cross sections were typically too large by a factor of 2 to 10.

Another first order calculation was performed by Jackson and Schiff⁵ in 1953 for the special case of protons incident upon hydrogen. The potential used in the JS calculation was the full interaction, that is, the BK potential and the internuclear (or core) potential. Including the "core" term had the effect of reducing the total cross section over a range of energies thus giving much better agreement with experiment. However, when the JS method was applied to other systems of higher nuclear charge, total calculated cross sections were found to disagree with experiment by as much as several orders of magnitude.^{6,7}

The success of the JS approach was later partially explained by Bates in 1958. Taking into account the nonorthogonality of the initial and final state wave functions, Bates was able to demonstrate that a JS like core term with unit nuclear charge originates from the average electron interaction. This tends to account for the relative success of the

JS method for protons on hydrogen, and suggests an alternate method for targets of nuclear charge greater than one.

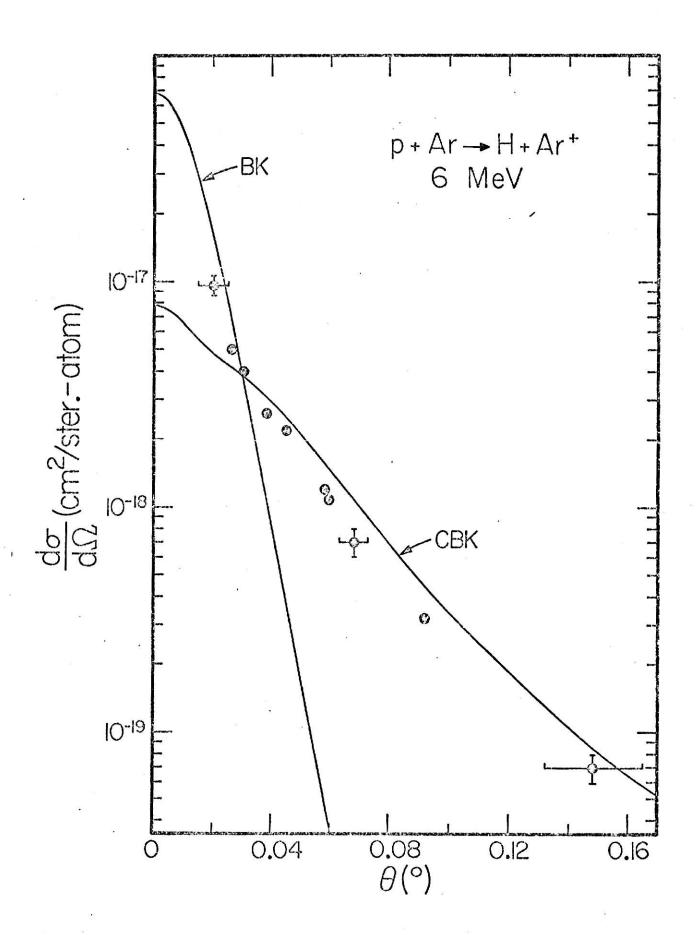
At the present time, some believe that the Bates calculation offers the most complete picture for viewing charge transfer to first order. Nevertheless, only various approximations for the Bates method of charge exchange have been used resulting in total cross sections that tend to agree with experiment. The success of these approximations in predicting total cross sections tend to indicate that the Bates approach is superior to that of BK or JS.

Taking advantage of the heavy projectile mass, it is often useful to study the charge transfer process by means of the impact parameter treatment. A transformation from the wave picture over to an impact parameter picture is presented in appendix 1. This impact parameter formalism was used by Belkic and Salin¹¹in 1976 for the angular distributions for charge transfer.

The impact parameter formalism used in Belkic and Salin's calculation employs an eikonal phase so as to include the internuclear potential together with the Brinkman-Kramers method. Justification for the use of the eikonal phase within the impact parameter treatment is made in Chapter 2. By including the internuclear potential in the eikonal phase, Belkic and Salin were able to get improved agreement at wide angles with the differential cross section for electron capture from argon by 6 MeV protons observed by Cocke, et al., in 1976, see Figure 2. Using the BK probability amplitude for capture which is calculated in a straight-line impact-parameter version of the BK approximation Belkic and Salin were able to obtain a better angular distribution than the BK calculation which took into account no contributions of the internuclear repulsion.

Figure 2. Differential cross section in laboratory system for capture of K-shell electrons from argon by 6 MeV protons. The curve marked BK represents the Brinkman-Kramers approximation; and CBK, the Coulomb Brinkman-Kramers approximation. Experimental data are those of Cocke, et al., (1976). Figure taken from Belkic and Salin, J. Phys. B: Atom. Molec. Phys. 9, L397 (1976).

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Note that their results are in good agreement at large angles (i.e. small impact parameters) but may give poor agreement at the forward angles (i.e. large impact parameters). Data for protons on helium support this trend, suggesting that the scattering potential is too strong at large impact parameters.

One of the limitations of the Belkic and Salin calculation is the omission of the screening effects by the electrons at large impact parameters. We include the effects of screening by the electrons in an approximate manner. For p + H and p + He, the internuclear potential is represented by the static potential (cf. Chapter 2) which is introduced into the eikonal phase within the BK method. Hence, it will be referred to as the Static Brinkman-Kramers (SBK) approximation. For p + Ar which is mathematically more complex, a screened Coulomb potential is incorporated in the eikonal phase as an approximation for the static potential. This Screened Coulomb Brinkman-Kramers calculation will be referred to as the SCBK approximation.

Application of the eikonal impact parameter treatment of charge transfer is made for three specific cases. The relatively simple system of protons incident upon hydrogen is presented first. This is followed by protons incident on helium. Then finally, the more complex system of protons on argon is examined. The two later cases are compared with recently gathered experimental differential cross sections for charge transfer.

CHAPTER 2

THEORY

2.1 The Differential Cross Section

The differential cross section is defined as

 $\frac{d\sigma}{d\Omega} \equiv \begin{array}{c} \text{Number of particles per unit time scattered} \\ \frac{d\sigma}{d\Omega} \equiv \begin{array}{c} \text{Into a solid angle} \\ \text{Number of particles incident on the} \\ \text{target per unit area per unit time} \end{array}$

This can be written symbolically as,

$$\frac{d\sigma}{d\Omega} = \frac{\omega/d\Omega}{I}$$
 (2.1)

The incident flux, I, can be given as,

$$I = \frac{\text{velocity of incident particle}}{\text{unit volume}}$$

$$=\frac{k_1 \tilde{h}}{\mu_1 L^3} \tag{2.2}$$

where $\hbar k_i$ is the magnitude of the relative initial momentum, μ_i is the initial reduced mass of the system, and L^3 is the volume of a cube of length, L. The transition probability per unit time, ω , is given by,

$$\omega = \frac{2\pi}{\hbar} \rho_{\mathbf{f}} |\langle \phi_{\mathbf{f}} | \mathbf{H'} | \Psi \rangle|^2, \qquad (2.3)$$

where ρ_f is the density of final states and $\langle \phi_f | H^* | \Psi \rangle$ is the transition matrix element for a transition from all possible states, Ψ , into the

final state, $\phi_{\mathbf{f}}$, under the perturbing Hamiltonian, H'. The density of final states, $\rho_{\mathbf{f}}$, is given by,

$$\rho_{f} = \frac{\mu_{f} k_{f} d\Omega_{f} L^{3}}{(2\pi)^{3} h^{2}},$$
(2.4)

where μ_f is the reduced mass of the final system, $\hbar k_f$ is the magnitude of the final relative momentum, $d\Omega_f$ is the solid angle subtended by the detector, and L 3 is the volume. Combining eq. 2.1, 2.2, 2.3 and 2.4, the differential cross section becomes,

$$\frac{\mathrm{d}\sigma}{\mathrm{d}\Omega} = \frac{\mu_{\mathbf{i}}\mu_{\mathbf{f}}L}{(2\pi)^{2}h^{4}} \left(\frac{k_{\mathbf{f}}}{k_{\mathbf{i}}}\right) \left| \langle \phi_{\mathbf{f}} | H' | \Psi \rangle \right|^{2}$$
 (2.5)

It is now convenient to introduce atomic units ($e^2 = \pi = m_e = 1$), where e is the electron charge and m_e is the electron mass. A few basic units are given below;

unit length =
$$a_0 = \frac{\chi^2}{m_e e^2} = 5.29 \cdot 10^{-9}$$
 cm

unit energy =
$$\frac{m_e^4}{\hbar^2}$$
 = 27.2 eV

unit time =
$$\frac{h^3}{m_e e^4}$$
 = 2.42·10⁻¹⁷ sec.

Atomic units will be used unless stated otherwise.

The differential cross section given in atomic units is,

$$\frac{\mathrm{d}\sigma}{\mathrm{d}\Omega} = \frac{\mu_{\mathbf{i}} \mu_{\mathbf{f}}}{(2\pi)^2} \left(\frac{k_{\mathbf{f}}}{k_{\mathbf{i}}}\right) \left| \langle \phi_{\mathbf{f}} | \mathbf{H}' | \Psi \rangle \right|^2, \qquad (2.6)$$

where the wave functions are normalized to the unit volume, L^3 . As yet, all we have done is to have re-written the definition of differential cross section into a form that can be used for calculation.

2.2 The Hamiltonian

Charge transfer is not a well understood atomic process. In our quest toward understanding the charge transfer process, approximations for both the wave functions and the perturbing Hamiltonian are made. However, in making approximations for the wave functions, difficulties arise from the fact that the wave functions are not described in the same basis set (i.e., nonorthogonal wave functions are used). In addition, it is a general practice to consider only one electron target atoms in charge transfer.

The Hamiltonian for a charged projectile incident upon a multielectron target (assuming two body interactions) is given by,

H = Total Kinetic Energy + Total Potential Energy

$$= \frac{P^{2}}{2M_{a}} + \frac{Z_{a}Z_{b}e^{2}}{R} - \frac{Z_{b}}{j=1} \frac{Z_{a}e^{2}}{|\vec{r}_{c}-\vec{r}_{j}|}$$

$$+ \frac{Z_{b}}{j=1} \left(\frac{P_{j}^{2}}{2m_{e}} - \frac{Z_{b}e^{2}}{r_{i}} \right) + \frac{Z_{b}}{k>j} \frac{e^{2}}{|\vec{r}_{k}-\vec{r}_{j}|}$$
(2.7)

where Z_a and M_a are the charge and mass of the incident projectile with momentum P, Z_b is the charge of the target nucleus, R represents the projectile coordinate and \vec{r}_1 \vec{r}_{Z_b} the set of coordinates of the target electrons measured from the target nucleus, and P_j is the momentum of the jth electron. By adding then subtracting the average projectile electron potential (i.e.,

$$\vec{\mathbf{V}}_{\mathbf{e}}^{\mathbf{j}} \equiv \langle \phi_{\mathbf{i}} \mid \frac{-\mathbf{Z}_{\mathbf{e}}^{\mathbf{e}^{2}}}{|\vec{\mathbf{R}} - \vec{\mathbf{r}}_{\mathbf{j}}|} \mid \phi_{\mathbf{i}} \rangle$$
 (2.8)

where ϕ_{i} is the initial bound state wave function for the jth electron), the Hamiltonian in eq. 2.7 takes the form,

$$H = \frac{P^2}{2M_a} + V_s(R) + H' + H_o' + H_o', \qquad (2.9)$$

where $V_{S}(R)$ is the static potential 15 given by

$$V_{s}(R) = \frac{Z_{a}Z_{b}e^{2}}{R} + \frac{Z_{b}}{j=1}V_{e}^{j}$$
 (2.10)

or

$$V_{s}(R) = Z_{a} \begin{bmatrix} \frac{Z_{b}e^{2}}{R} & \frac{Z_{b}}{|\vec{x}-\vec{r_{j}}|} & \frac{\rho(\vec{r_{j}})}{|\vec{x}-\vec{r_{j}}|} & \vec{r_{j}} \end{bmatrix}$$

where (r_j) is the charge density for the jth electron H' is the electron capture potential prescribed by Bates, i.e.,

$$H' \equiv \frac{-Z_a e^2}{\left|\overrightarrow{R} - \overrightarrow{x}\right|} + \langle \phi_i \mid \frac{Z_a e^2}{\left|\overrightarrow{R} - \overrightarrow{x}\right|} \mid \phi_i \rangle \qquad (2.11)$$

where \vec{x} is the coordinate of the captured electron measured from the target nucleus; H' is the Hamiltonian that describes the initial bound state of the electron to be captured, i.e.,

$$H_0' = \frac{P_e^2}{2m_e} - \frac{Z_b e^2}{x} + V(\vec{x}),$$
 (2.11A)

where P_e is the momentum of the captured electron and V(x) is the effective potential between the captured electron and the spectator electrons, i.e.,

$$V(\overrightarrow{x}) \simeq \sum_{k=1}^{Z_b} \frac{e^2}{|\overrightarrow{r}_k - \overrightarrow{x}|}, \qquad (2.11B)$$

where the prime indicates the restricted sum $r_k \neq x$; and H is the Hamiltonian for the spectator electrons which is given by

$$H_{o} = \sum_{j=1}^{Z_{b}-1} \left[\frac{P_{j}^{2}}{2m_{e}} - \frac{Z_{b}e^{2}}{r_{j}} + V(\vec{r}_{j}) - \vec{V}_{e}^{j} \right], \qquad (2.11c)$$

where the summation is over all the spectator electrons and $V(\overset{\rightarrow}{r_j})$ is the effective potential between the spectator electrons (cf. eq. 2.11B). To retain the simplicity of the one electron atom, the effects due to the spectator electrons, eq. 2.11C, are ignored in the development to follow. This is done so that simple hydrogenic wave functions can be used to describe the bound state of the captured electron. Note that in this fashion of breaking up the Hamiltonian, both the static potential and the electron capture potential of Bates are directly related.

The perturbation to the one electron Hamiltonian is separable into two categories: the perturbation for electron capture and the perturbation responsible for scattering of the projectile. Both are needed for the differential cross section. The perturbation for the capture process is the Bates potential, eq. 2.11. The "scattering" perturbation is the static potential given by eq. 2.10. We choose to treat these two processes separately.

2.3 The Eikonal Phase

We can treat the scattering process within the eikonal approximation. As an introduction to the eikonal approximation, let us consider the scattering of a particle from the central potential, V(R). The time

independent Schrödinger equation for such a process is

$$\left(-\frac{\nabla^2}{2\mu} + V(R)\right)\psi = \frac{k^2}{2\mu}\psi, \qquad (2.12)$$

where μ is the reduced mass and k is the momentum of the projectile.

Assuming our wave function to be of the form,

$$\psi = e^{i\vec{k}\cdot\vec{R}} \Phi(R)$$
 (2.13)

and substituting into eq. 2.12 we get

$$\left[\frac{k^2}{2\mu} \Phi(R) - \frac{\nabla^2}{2\mu} \Phi(R) - \frac{2i\vec{k} \cdot \vec{\nabla} \Phi(R)}{2\mu} + V(R)\Phi(R)\right]$$

$$X e^{i\vec{k} \cdot \vec{R}} = \frac{k^2}{2\mu} \tilde{\psi}(R) e^{i\vec{k} \cdot \vec{R}} .$$
(2.14)

Equation 2.14 reduces to

$$-\frac{\nabla^2}{2\mu} \Phi(R) - \frac{i \vec{k} \cdot \vec{\nabla} \Phi(R)}{\mu} + V(R) \Phi(R) = 0. \qquad (2.15)$$

Assuming $\Phi(R)$ to vary slowly over many wavelengths of the incident projectile, i.e.

$$\nabla^2 \Phi(R) \ll \vec{k} \cdot \vec{\nabla} \Phi(R), \qquad (2.16)$$

choosing \vec{k} along the 2 direction, and solving eq. 2.15 for $\Phi(R)$ we get

$$\Phi(R) = \left(\exp \frac{-\mu i}{k} \int_{-\infty}^{\infty} V(R) dz\right). \tag{2.17}$$

Noting that $R = \sqrt{\rho^2 + z^2}$ where ρ is the impact parameter, our projectile

wave function (eq. 2.13) is

$$\psi \approx \exp(i\vec{k}_i \cdot \vec{R}_i + 2i\delta(\rho)), \qquad (2.18)$$

where

$$\delta(\rho) = \frac{-1}{v} \int_{0}^{\infty} V(R) dz, \qquad (2.19)$$

and $\mu v = k$.

2.4 The Eikonal Impact Parameter Method

McCarroll and Salin ¹⁷ (1968) present a method for evaluation of the differential cross section (Appendix 1) where the wave picture is formally transformed into an impact parameter picture. The results of this method were then modified by Belkic and Salin (1976) so as to include scattering from the internuclear potential in an eikonal phase. The internuclear potential used by Belkic and Salin appears to be too strong at the large impact parameters which suggests that screening of the electrons is important for angular distributions. Here the eikonal impact parameter method used by Belkic and Salin is presented in a general form so that the screening effects are properly taken into account.

The differential cross section (eq. A1. 38) is obtained by McCarroll and Salin by evaluating the transition matrix. The transition matrix, T_{if} , is given by either of the two equivalent expressions, 18

$$T_{if} = \langle \phi_f | \Psi_f | \Psi_i \rangle \qquad (2.20)$$

or

$$T_{if} = \langle \phi_i | V_i | \Psi_f \rangle, \qquad (2.21)$$

where the subscripts i and f are used to denote initial and final conditions. The first of the two expressions for the transition matrix is evaluated in Appendix 1. Since the single electron charge transfer process is time reversible, the perturbation is given by some appropriate interaction potential between the captured electron and the projectile either before or after the collision indicated by $V_{\bf i}$ and $V_{\bf f}$ respectively.

It has already been mentioned that the choice of the static potential in the eikonal phase corresponds to use of the Bates potential, i.e.

$$V_{f} \approx \frac{Z_{b}e^{2}}{x} - \langle \phi_{i} | \frac{Z_{b}e^{2}}{x} | \phi_{i} \rangle.$$
 (2.22)

The Bates potential has two desirable features that the BK and JS potentials lack. First, the orthogonality of the wave functions ϕ_i and ϕ_f are maintained. Second, the choice of a zero point energy has no effect on the total or differential cross sections as it should. However, the Bates calculation is difficult computationally. For this reason, the BK potential is adopted at this point for computational convenience, i.e.

$$V_{f} = \frac{Z_{b}e^{2}}{x}$$
 (2.23)

One consequence of using the BK potential is failure of our calculation to produce correctly normalized distributions. It is well known that the BK results generally lie above observed results for total cross sections.

The general form for the eikonal impact parameter method used by Belkic and Salin is presented. Using the BK potential in the evaluation of the probability amplitude (cf. Appendix 2), the differential cross section (eq. Al.38) takes the form,

$$\frac{d\sigma}{d\Omega} = \left| i\mu v \right|_{0}^{\infty} \rho d\rho J_{0}(n\rho) \exp(2i\delta(\rho)) b_{BK}(\rho) \left|^{2}, \right|$$
 (2.24)

where μ is the reduced mass, v is the velocity of the incident projectile, η is the momentum transfer, J_o is the zero order Bessel function of the first kind, $\delta(\rho)$ is the eikonal phase (eq. 2.19) for the static potential, and $b_{BK}(\rho)$ is the Brinkman-Kramers probability amplitude (eq. A2.30) for the capture of an electron at the impact parameter, ρ . In eq. 2.24, the probability amplitude (eq. A1.37) is separable into the BK probability amplitude times an overall phase (eq. A2.8). The BK probability amplitude given by McGuire and Cocke¹⁹ is

$$b_{BK}(\rho) = \left(\frac{2in_a}{v}\right) \left(\frac{z_a z_b}{n_a n_b}\right)^{5/2} \left(\frac{\rho^2}{\gamma}\right) K_2\left(\gamma^{\frac{1}{2}}\rho\right), \qquad (2.25)$$

where \mathbf{Z}_a and \mathbf{Z}_b are the charges of the respective nuclei A and B, \mathbf{n}_a and \mathbf{n}_b are the principle quantum numbers of the bound electron to the respective nuclei A and B, \mathbf{K}_2 is the second order Bessel function of the third kind, and

$$\gamma = \frac{z_b^2}{n_b^2} + \left(\frac{v}{2} + \frac{1}{2v} \left(\frac{z_a^2}{n_a^2} - \frac{z_b^2}{n_b^2}\right)\right)^2.$$
 (2.26)

Upon specification of the eikonal phase, the integration over impact parameters gives the differential cross section for charge transfer of an electron from the state \mathbf{n}_b to state \mathbf{n}_a .

CHAPTER 3

APPLICATIONS AND RESULTS

3.1 The Static Brinkman-Kramers Approximation

Use of the Static potential (eq. 2.10) in the calculation of the eikonal phase (eq. 2.19) with the BK probability amplitude (eq. 2.25) defines the Static Brinkman-Kramers (SBK) approximation. The static potential for hydrogen and helium like targets is easily evaluated in the independent electron approximation. The form of the eikonal phase using the static potential is now presented.

The average electron-projectile interaction potential (eq. 2.8) using hydrogenic wave functions is readily evaluated for the K shell. The initial wave function 20 is

$$\phi_{i} = \left(\frac{z^{*}}{a_{o}}\right)^{3/2} 2 \exp\left(-\frac{z^{*}r}{a_{o}}\right) \frac{1}{2\sqrt{\pi}} P_{o}(\cos\theta), \qquad (3.1)$$

where Z^* ($Z^* = Z_b$ for a one electron atom) is the effective nuclear charge seen by the bound electrons, and P_o is the Legendre polynomial. The projectile-electron interaction potential²¹ is

$$-\frac{z_{a}}{|\vec{R} - \vec{r}|} = \frac{-z_{a}}{r_{>}} \sum_{\ell=0}^{\infty} \left(\frac{r_{<}}{r_{>}}\right)^{\ell} P_{\ell}(\cos\theta), \qquad (3.2)$$

where R is the internuclear separation distance and r is the electron target separation distance ($r_{<}$ and $r_{>}$ refer to the lesser and greater of the two distances). From eq. 3.1 and eq. 3.2, the average projectile - 1s electron interaction potential is

$$\overline{V}_{e} = \frac{-Z_{a}}{\pi} \left[\frac{Z^{*}}{a_{o}} \right]^{3} \int_{0}^{\infty} r^{2} dr \exp \left[-\frac{2Z^{*}r}{a_{o}} \right] \frac{1}{r_{>}}$$

$$X \int_{-\infty}^{\infty} \left[\frac{r_{<}}{r_{>}} \right]^{1} \int_{-1}^{1} P_{o}(\cos\theta) P_{o}(\cos\theta) P_{o}(\cos\theta) d(\cos\theta) \int_{0}^{2\pi} d\phi.$$
 (3.3)

Upon integration over ϕ and noting that $P_o(\cos\theta)$ = 1, eq. 3.3 reads

$$\overline{V}_{e} = -2Z_{a} \left(\frac{Z^{*}}{a_{o}}\right)^{3} \int_{0}^{\infty} r^{2} dr \exp \left(-\frac{2Z^{*}r}{a_{o}}\right) \frac{1}{r_{>}}$$

$$X = \sum_{r=0}^{\infty} \left(\frac{r}{r}\right)^{r} \int_{-1}^{1} P_{r}(\cos\theta) P_{o}(\cos\theta) d(\cos\theta). \tag{3.4}$$

Using the orthogonality of Legendre polynomials,22

$$\int_{-1}^{1} P_{\rho}(x) P_{\rho}(x) dx = 2\delta_{\rho}, \qquad (3.5)$$

the summation vanished except for the I = 0 term. This reduces eq. 3.4 to,

$$\overline{V}_{e} = -\frac{Z_{a}}{2} \int_{0}^{\infty} \frac{x^{2}e^{-x}}{x_{>}} dx,$$
 (3.6)

where $x = 2Z^* \frac{r}{a}$ and

$$x_{>} = \begin{cases} R & \text{if } x < \frac{2Z^{*}R}{a_{0}} \\ r & \text{if } x > \frac{2Z^{*}R}{a_{0}} \end{cases}$$
 (3.7)

Since 23

$$\int_{t}^{\infty} xe^{-x} dx = e^{-t}(t+1)$$
 (3.8)

and

$$\int x^2 e^{-x} dx = e^{-x} (-x^2 - 2x - 2), \qquad (3.9)$$

eq. 3.6 is evaluated as

$$\overline{V}_{e} = -\frac{Z_{a}}{R} + Z_{a} \left(\frac{1}{R} + \frac{Z^{*}}{a_{o}} \right) \exp \left(-\frac{2Z^{*}R}{a_{o}} \right). \tag{3.10}$$

This is precisely the expression that Bassel and Gerjouy $^9(1960)$ obtained for the average electron interaction for protons on hydrogen ($\text{Z}^* = \text{Z}_a = 1$). Hence, the static potential (eq. 2.10) for $\text{Z}_b \leq 2$ is

$$Z_{a}Z_{b}\left[\frac{1}{R}-\frac{1}{R}+\left(\frac{1}{R}+\frac{Z^{*}}{a_{o}}\right)\exp\left(-\frac{2Z^{*}R}{a_{o}}\right)\right]. \tag{3.11}$$

The eikonal phase for the static potential in eq. 3.11 is

$$\delta(\rho) = -\frac{Z_a Z_b}{v} \int_0^\infty \left(\frac{1}{R} + \frac{Z^*}{a_o} \right) \exp \left(-\frac{2Z^*R}{a_o} \right) dz.$$
 (3.12)

Letting $q = \frac{2Z^*}{a_0}$ and noting $R = \sqrt{\rho^2 + z^2}$, we have

$$\int_{0}^{\infty} (\rho^{2} + z^{2})^{-\frac{1}{2}} \exp(-q(\rho^{2} + z^{2})^{\frac{1}{2}}) dz$$
 (3.13)

which is evaluated to be K_0 (pq) which is the zero-order modified Bessel function of the third kind. Since

$$\frac{\partial}{\partial q} \frac{e^{-qR}}{R} = -e^{-qR} , \qquad (3.14)$$

we have

$$\int_{0}^{\infty} \exp(-q(\rho^{2} + z^{2})^{\frac{1}{2}}) dz = -\frac{\partial}{\partial q} K_{o}(\rho q).$$
 (3.15)

Letting $p = \rho q$, we have ²⁵

$$-\rho \frac{\partial}{\partial p} K_{o}(p) = \rho K_{1}(p), \qquad (3.16)$$

where K_1 is the first order Bessel function of the third kind. The eikonal phase for the static potential is,

$$\delta(\rho) = -\frac{Z_a Z_b}{v} \left[K_o \left(\frac{2Z^* \rho}{a_o} \right) + \frac{Z^* \rho}{a_o} K_1 \left(\frac{2Z^* \rho}{a_o} \right) \right] . \tag{3.17}$$

Appendix 3 contains a computer program for the calculation of the differential cross section (eq. 2.24) for the static potential in the eikonal phase (eq. 3.17)

3.2 Screened Coulomb Brinkman-Kramers Approximation

For targets with more than two electrons, the static potential contains terms that arise from electrons in shells and subshells other than the K shell. For this reason, there are a multitude of additional terms to be evaluated to obtain the total static potential. To simplify matters, we can approximate the screening of the electrons by the screened Coulomb potential,

$$V(R) = \frac{Z_a Z_b}{R} \exp \left(-\frac{R}{r_o}\right), \qquad (3.18)$$

where r_o is an appropriate screening radius. For atom-atom collisions, an expression for the screening radius exists in the literature, given by, 26,27

$$r_o = a_o / (Z_a^{2/3} + Z_b^{2/3})^{\frac{1}{2}}.$$
 (3.19)

Making use of eq. 3.13, the eikonal phase (eq. 2.10) for a screened Coulomb potential (eq. 3.18) is

$$\delta(\rho) = -\frac{z_a z_b}{v} \quad \kappa_o \left[\frac{\rho}{r_o}\right] . \tag{3.20}$$

Use of the screened Coulomb potential in the eikonal phase with the BK probability amplitude defines the Screened Coulomb Brinkman-Kramers (SCBK) approximation.

The limiting cases for screening give the results of Brinkman and Kramers and the results of Belkic and Salin. When the screening radius is zero the screened Coulomb potential vanishes, i.e.

$$\frac{Z_a Z_b}{R} \exp \left(-\frac{R}{r_o}\right) \xrightarrow[r_o \to o]{} 0. \tag{3.21}$$

This corresponds to the calculation of Brinkman and Kramers. When the screening radius is infinite the screened Coulomb potential reduces to the Coulomb potential, i.e.

$$\frac{Z_a Z_b}{R} \exp \left(-\frac{R}{r_o}\right) \xrightarrow[r_o \to \infty]{} \frac{Z_a Z_b}{R} . \tag{3.22}$$

This is the potential used by Belkic and Salin to obtain the Coulomb Brinkman-Kramers (CBK) approximation.

Appendix 4 contains a program for the calculation of the differential cross section (eq. 2.24) using the screened Coulomb potential in the eikonal phase (eq. 3.20).

3.3 Protons on Hydrogen

We can now test the effects of screening of the internuclear poten-

tial by the target electrons in the charge transfer process. Consider the simplest possible system of a proton incident upon atomic hydrogen, i.e.

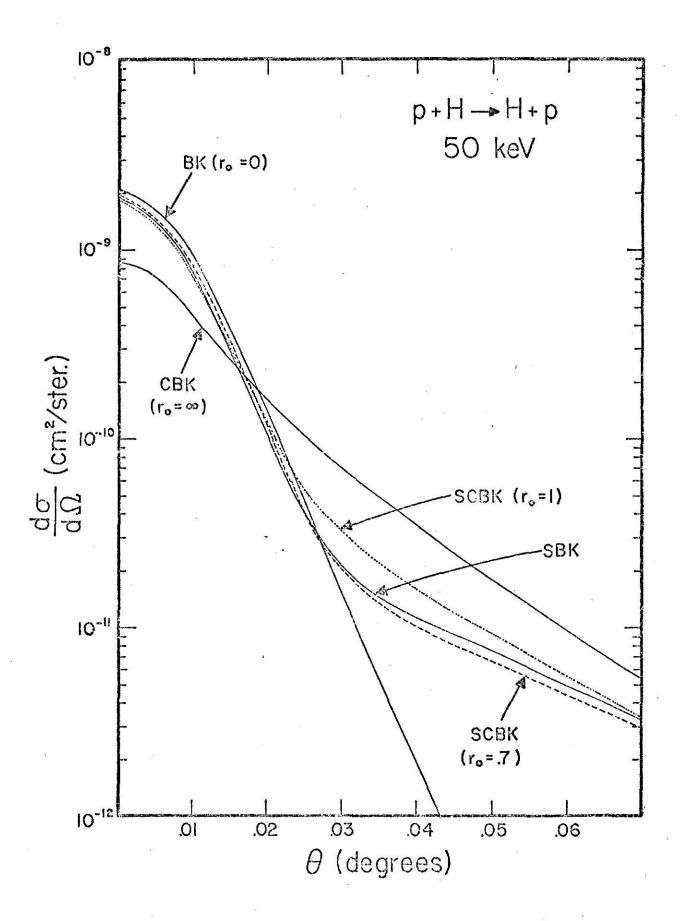
$$p + H \rightarrow H + p$$
.

In viewing this reaction, we compare the differential cross section of SCBK, for several screening radii, with SBK.

There are several interesting features of SCBK and SBK. In figure 3, a comparison of the differential cross sections versus angle is presented for protons incident upon atomic hydrogen at 50 keV. There are three distinct curve shapes (solid lines). The screened Coulomb Brinkman-Kramers calculation reduces to the Brinkman-Kramers calculation and the Coulomb Brinkman-Kramers calculation of Belkic and Salin in the limiting cases of screening parameters. The total cross sections from all the differential cross sections in figure 3 are identical. Finally, the shape of SCBK is not sensitive to reasonable choices of the screening parameter.

There are three distinct shapes for the differential cross section indicated by the solid curves in figure 3. The BK angular distribution is peaked in the forward direction and falls off rapidly at the larger angles, for the BK calculation takes into account no internuclear interaction. On the other hand, the CBK calculation takes into account the full internuclear interaction i.e. $V(R) = \frac{1}{R}$, where R is the internuclear separation distance. As a result, the curve marked CBK shows that the capture process at the larger angles is orders of magnitude above the BK results due to inclusion of the internuclear repulsion within the eikonal phase. Recalling the discussion of figure 2, the SBK calculation gives the desired results of following BK at the forward angles (0 < $\frac{m}{m_D}$) and CBK at large

Figure 3. The differential cross section for electron capture by 50 keV protons incident on atomic hydrogen is shown. The curve marked BK is the Brinkman-Kramers approximation, CBK is the Coulomb Brinkman-Kramers approximation, SBK is the Static Brinkman-Kramers approximation, and SCBK the Screened Coulomb Brinkman-Kramers approximation.



angles ($\theta > \frac{m_e}{m}$, where m_e is the mass of the electron and m_p is the projectile mass). The charge parameters used are $Z_a = Z_b = Z^* = 1$.

The SCBK calculation reduces to BK and CBK in the limiting cases for screening parameters. The BK curve in figure 3 is obtained by choosing the screening radius in SCBK to be 10^{-2} , cf. eq. 3.21. The CBK curve is obtained by choosing the screening radius in SCBK to be 10^{2} , cf. eq. 3.22. There were difficulties in choosing extreme values for the screening parameter due to the Bessel function subroutines. However, it is noted that in atomic dimensions $10^{-2} \approx 0$ and $10^{2} \approx \infty$. This serves as a check on the SCBK program.

The total integrated cross sections for BK, CBK, and SBK are identical. This is because the eikonal phase appears as an overall phase in the probability amplitude (eq. A2.8), i.e.

$$\sigma_{\text{Total}} = 2\pi \int |b(\rho)|^2 \rho d\rho$$

$$= 2\pi \int |b_{\text{BK}}(\rho)|^2 \rho d\rho$$

$$= \sigma_{\text{BK}},$$
(3.23)

where b(ρ) is the probability amplitude (eq. A2.8), b_{BK}(ρ) is the BK probability amplitude (eq. 2.9), ρ is the impact parameter, σ_{Total} is the total cross section, and σ_{BK} is the BK total cross section. The total integrated cross sections BK, SBK, and CBK are in agreement with the closed form expression for the total BK cross section of 2.96 \cdot 10⁻¹⁶ cm². This serves as a check on the various integration techniques used in the SBK and SCBK computer programs.

The shape of SCBK is not sensitive to reasonable choices of the

screening parameter. That is, the SCBK calculation for screening radii on the order the K shell radius (dotted and dashed curves in figure 3) retains the two region shape of the SBK calculation. For the Bohr screening radius (eq. 3.19), the SCBK calculation (dashed line) closely follows that of SBK. This indicates that the screened Coulomb potential with Bohr screening is a good approximation to the static potential.

3.4 Protons on Helium

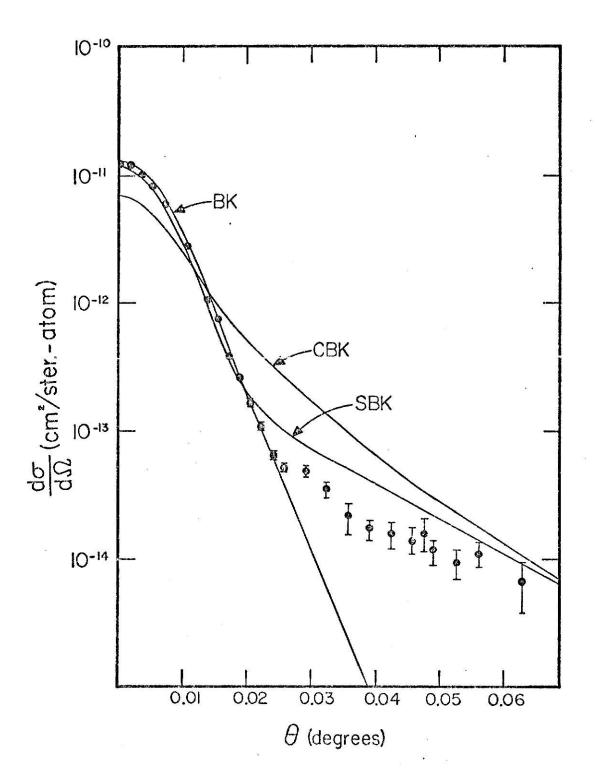
Although the angular distribution for protons incident on atomic hydrogen is easiest to treat theoretically, it is difficult to measure experimentally simply because hydrogen is diatomic. A comparison with observed differential cross sections is necessary to check the screening effects of the electrons on the internuclear potential in the SBK approximation. For these reasons we choose to consider the charge transfer process,

$$p + He \rightarrow H + He^+$$
.

Data for this reaction exists at 293 keV observed by Bratton, et al., (1977).

The differential cross section for 293 keV protons incident on helium is compared with the normalized theoretical predictions of BK, CBK, and SBK (cf. figure 4). The fact that the theoretical predictions must be reduced by a factor of 3.55 to agree with the observed cross section of $9.4 \cdot 10^{-19} \text{ cm}^2/\text{atom}$ indicates a poor asumption has been made. The charge parameters used in the SBK calculation are $Z_a = 1$, $Z_b = 2$ and $Z^* = 1.618$. We believe the weakest assumption made is use of the BK probability amplitude in our calculation, for it is well known that the BK results generally lie above the observed total cross sections. Nevertheless, we are testing

Figure 4. Differential cross section in laboratory system for capture of K-shell electrons from helium by 293 keV protons. The curve marked BK represents the normalized Brinkman-Kramers approximation; CBK, the normalized Coulomb Brinkman-Kramers approximation, and SBK, the normalized Static Brinkman-Kramers approximation. Each theoretical curve has been reduced by a factor of 3.55 normalizing total cross sections to observed results of $9.4 \cdot 10^{-19} \, \mathrm{cm}^2/\mathrm{atom}$. Experimental data are those of Bratton, et al., (1977).

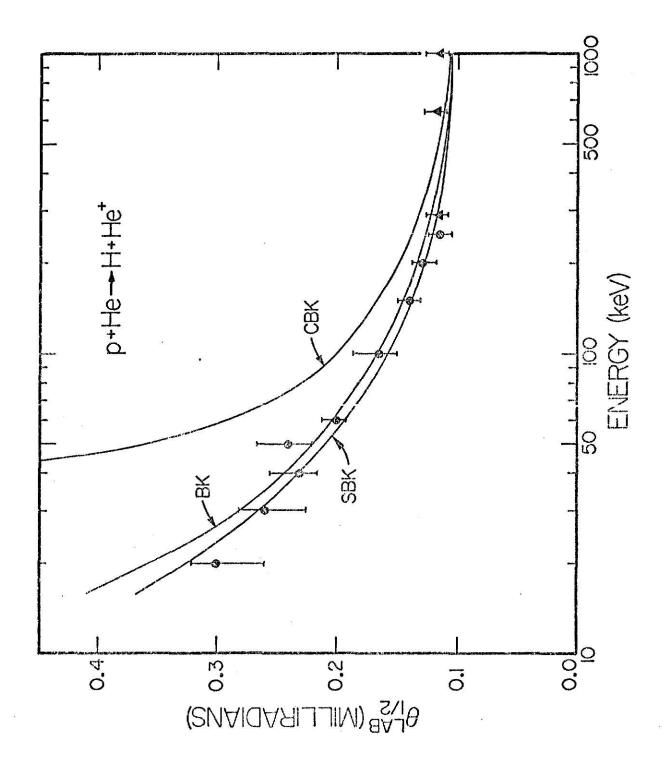


the screening effects on the differential cross section and not the BK approximation. Hence, when comparing our predictions with data, normalization is unavoidable when the BK probability amplitude is used.

There is evidence that a normalization factor is justified for bringing the SBK approximation into close agreement with observation. A recent close coupling calculation of the Bates probability amplitude by Lin^{10} indicates the Bates probability amplitude exhibits the same impact parameter dependence as the BK probability amplitude times a constant factor. In addition, the total cross section from this calculation is in agreement with that observed by Bratton, et al., (1977). Another justification of the normalization of SBK is witnessed in a plot of the laboratory angle θ_{l_2} where the scattering distribution falls to half the maximum intensity as a function of the projectile energy, cf. figure 5. A normalization factor is not an issue in the calculation of θ_{l_2} since we are considering a ratio of intensities.

SBK gives a better fit to the data than CBK or BK. Referring to figure 4, it is seen that the SBK calculation features two regions, the forward angle region where BK gives a reasonable fit to the data and the large angle region where CBK gives reasonable fit to the data. Referring to figure 5, it is seen that the SBK approximation is superior to CBK in its agreement with data. This is because CBK follows the angular distribution at large angles whereas $\theta_{1/2}$ is calculated at the forward angle region where CBK is in poor agreement. A similar argument can be given as to why BK and SBK agree in the calculation of $\theta_{1/2}$. However, it should be noted that the BK approximation does not give good agreement for large angle capture as witnessed in the angular distribution in figure 4.

Figure 5. The laboratory angle $\theta_{1/2}$ where the scattering distribution falls to half the maximum intensity as a function of the projectile energy. The curve marked BK represents results using the Brinkman-Kramers approximation; SBK using the Static Brinkman-Kramers approximation; and CBK the Coulomb Brinkman-Kramers approximation. Experimental data are due to (o) Wittkower and Gilbody³⁰(1967), and (Δ) Bratton, (1977).



3.5 Protons on Argon

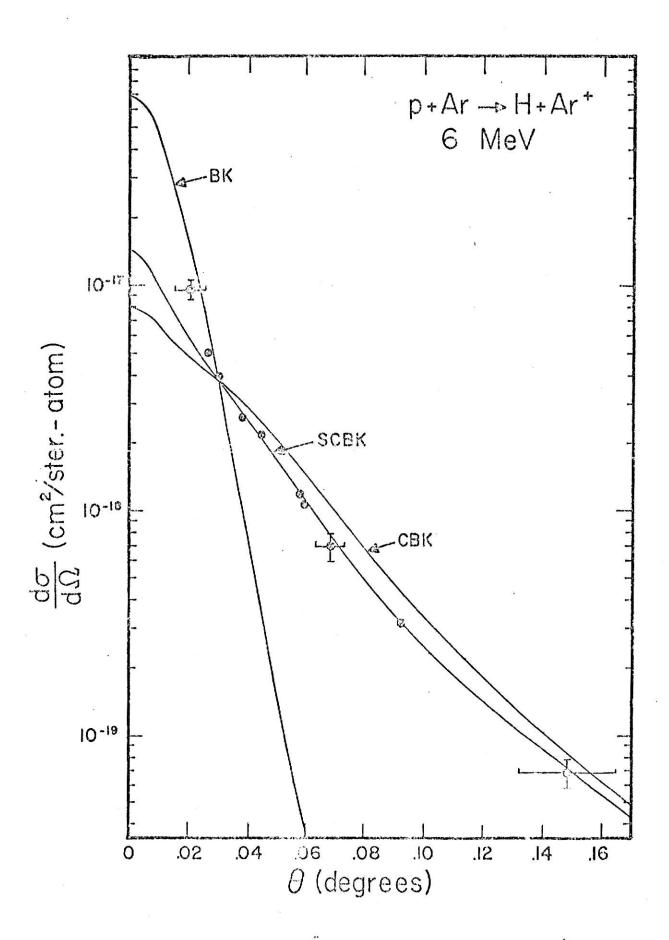
In considering the reaction of protons incident on helium, a normalization factor was introduced to bring the BK, CBK, and SBK calculations into agreement with the experimental total cross section. For the
reaction

$$p + Ar \rightarrow H + Ar^{\dagger}$$

the BK total cross section is in close agreement with the data at a projectile energy of 6 MeV. For this reaction, we compare the SCBK approximation to the data without normalization.

Using hydrogenic wave functions as before and charge parameters $Z_a = 1$ and $Z_b = Z^* = 18$, we calculate BK, CBK and SCBK, cf. figure 6. These are precisely the results obtained by Belkic and Salin for the BK and CBK approximations in figure 2. The SCBK results are obtained for Bohr screening which corresponds to the SBK approximation. The total cross section for BK (i.e. all curves) is $1.78 \cdot 10^{-23} \, \mathrm{cm}^2/\mathrm{atom}$ which compares with the experimental results of (1.68 ± 0.9) x $10^{-23} \, \mathrm{cm}^2/\mathrm{atom}$. Again the screened Coulomb Brinkman-Kramers approximation is in better agreement with the data than either BK or CBK at both the large and small angles.

Figure 6. Differential cross section in laboratory system for the capture of K-shell electrons from argon by 6 MeV protons. The curve marked BK is the Brinkman-Kramers approximation; CBK, the Coulomb Brinkman-Kramers approximation, and SCBK the Screened Coulomb Brinkman-Kramers approximation. Experimental data are those of Cocke, et al., (1976).



CHAPTER 4

CONCLUSION

The role of the internuclear potential in angular distributions has been examined. Using the eikonal method of McCarroll and Salin, the effective internuclear potential is represented by the static potential. The shape of the angular distribution using this static potential gives improved agreement with observed results of Bratton, et al., over that obtained by Belkic and Salin using an unscreened Coulomb potential and much better agreement than Brinkman and Kramers which takes into account no internuclear repulsion.

As a consequence of choosing the static potential to represent the effective internuclear potential, the electron capture potential is found to be the potential prescribed by Bates. Although the Brinkman-Kramers potential is used to approximate the Bates electron capture potential, the shape of the differential cross section in the Static Brinkman-Kramers (SBK) approximation exhibits two distinct regions in the differential cross section corresponding to observation by Bratton, et al. In contrast to other methods, the SBK approximation has no node in the differential cross section. Since the static potential and the Bates potential are intimately related, the SBK results reinforce use of the Bates potential.

However, our SBK approximation suffers from various limitations.

Possible improvements in our calculation include:

- i) use of the Bates potential in calculating the electron capture probability amplitude,
- ii) use of better wave functions to describe the bound electron, and

iii) taking into account second order effects.
Other effects are probably less important than these although they may contribute to a total understanding of charge transfer.

REFERENCES

- 1. R. Shakeshaft, J. Phys. B 7, 1059 (1974).
- H. C. Brinkman and H. A. Kramers, Proc. Acad. Sci. Amst. 33, 973 (1930).
- 3. J. R. Oppenheimer, Phys. Rev. 31, 349 (1928).
- V. S. Nikolaev, Zh. Eskp. Teor. Fiz. <u>51</u>, 1263 (1966), Sov. Phys. JETP 24, 847 (1967).
- 5. J. D. Jackson and H. Schiff, Phys. Rev. 89, 359 (1953).
- R. A. Mapleton, J. Phys. B 1, 529 (1968).
- A. M. Halpern and J. Law, Bull. Am. Phys. Soc. <u>19</u>, 561 (1974); Phys. Rev. A 12, 1776 (1975).
- 8. D. R. Bates, Proc. Roy. Soc. (London) A247, 294(1958).
- 9. R. H. Bassel and E. Gerjuoy, Phys. Rev. 117, 749 (1960).
- 10. C. D. Lin, S. C. Soong, and L. Tunnell, private communication (1977).
- 11. Dz. Belkic and A. Salin, J. Phys. B 9, L397 (1976).
- 12. C. L. Cocke, J. R. Macdonald, B. Curnutte, S. L. Varghese, and P. Randall, Phys. Rev. Lett. 36, 782 (1976).
- 13. L. I. Schiff, Quantum Mechanics (McGraw-Hill, New York, 1968) 3rd ed., pp. 314-315. Eq. 2.3-2.5 are presented in Schiff as well as other texts.
- J. H. McGuire and L. Weaver, Phys. Rev. A 16, to be published (1977).
- 15. J. R. Taylor, Scattering Theory: The Quantum Theory on Nonrelativistic

 Collisions (Wiley and Sons, New York, 1972), p. 153.
- 16. Reference 13, pp. 339-341.
- 17. R. McCarroll and A. Salin, J. Phys. B 1, 163 (1968).
- M. R. C. McDowell and J. P. Coleman, <u>Introduction to the Theory of</u> <u>Ion-Atom Collisions</u> (American Elsevier Publishing Company, New York, 1970), p. 279.

- 19. L. H. McGuire and C. L. Cocke, "BK Probabilities for Electron Capture", Kansas State University, unpublished (1977).
- A. Messiah, Quantum Mechanics (Wiley and Sons, New York, 1958) Vol. I,
 p. 484.
- 21. Reference 20, p. 497.
- 22. Reference 20, p. 493.
- 23. S. M. Selby, <u>Standard Mathematical Tables</u> (CRC Press, Cleveland, 1973) 23rd ed., p. 453.
- 24. I. S. Gradshteyn and I. M. Ryzhik, <u>Table of Integrals</u>, <u>Series</u>, and <u>Products</u> (Academic Press, New York, 1965), p. 959.
- 25. Reference 24, p. 970.
- 26. N. Bohr, Kgl. Danske Videnskab. Selskab, Mat-fys. Medd. 18, 8 (1948).
- 27. E. Everhart, G. Stone, and R. J. Carbone, Phys. Rev. 99, 1287 (1955).
- 28. T. Bratton, C. L. Cocke, and J. R. Macdonald, J. Phys. B, (to be published).
- 29. S. R. Rogers and J. H. McGuire, J. Phys. B, (to be published).
- 30. A. B. Wittkower and H. B. Gilbody, Proc. Phys. Soc. 90, 343 (1967).
- 31. T. R. Bratton, Master's Thesis Kansas State University (1977), (unpublished).
- 32. J. R. Macdonald, C. L. Cocke, and W. W. Eidson, Phys. Rev. Lett. <u>32</u>, 648 (1974).
- 33. H. Schiff, Can. J. Phys. 32, 393 (1954).
- 34. R. J. Glauber, <u>Lectures in Theoretical Physics</u> (Interscience, New York, 1958) Vol. 1, pp. 315-424.
- 35. M. Abramowitz and I. A. Stegun, <u>Handbook of Mathematical Functions</u>
 with Formulas, Graphs, and Mathematical Tables (Dover Publications,
 New York, 1972), p. 360.
- 36. Reference 18, pp. 212-215.

APPENDIX 1

The Transition Matrix

The form of the transition matrix developed in this section closely follows that outlined by McCarroll and Salin (1968). Related results have previously been given by Schiff³³(1954) and Glauber³⁴(1958). From this development the validity of the expressions for the transition matrix, and hence the differential cross section, is clearly shown.

Consider the charge transfer process,

$$A + (e + B) \rightarrow (A + e) + B$$
.

A diagram of the position vectors for this reaction is given in Figure 7.

This diagram is used extensively in the steps to follow. In addition,

some vector relations corresponding to the diagram are used:

$$\vec{x} = \vec{r}_2 - \vec{r}_1 \tag{A1.1}$$

$$\vec{s} = \vec{r}_2 - \vec{r}_3 \tag{A1.2}$$

$$\vec{R} = \vec{r}_3 - \vec{r}_1 = \vec{x} - \vec{s}$$
 (A1.3)

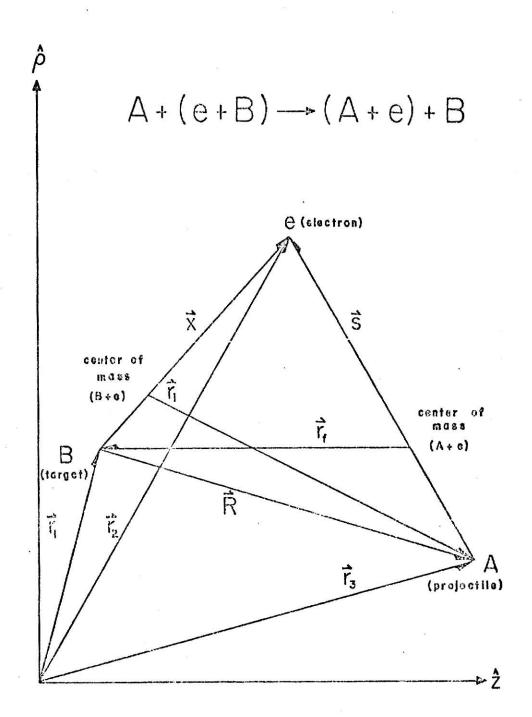
$$\vec{r} = \frac{1}{2} \left(\vec{x} + \vec{s} \right).$$
(A1.4)

Letting \mathbf{m}_a be the mass of the projectile and \mathbf{m}_b be the mass of the target, the following vector quantities are defined from the reduced mass relations for the respective electron-nucleus systems:

$$\vec{r}_1 + \vec{s} = \frac{m_b}{m_b + 1} \vec{x}$$
 (A1.5)

and

Figure 7. The coordinates for the charge transfer process $A + (e + B) \rightarrow (A + e) + B$.



$$\vec{r}_f + \vec{x} = \frac{m_a}{m_a + 1} \vec{s}. \tag{A1.6}$$

Upon substitution for \vec{x} and \vec{s} (eq. Al.i and eq. Al.2) eq. Al.5 and Al.6 become,

$$\vec{r}_1 = \vec{r}_3 - \frac{m_b \vec{r}_1 + \vec{r}_2}{m_b + 1}$$
 (A1.7)

$$\vec{r}_f = \vec{r}_1 - \frac{m_a \vec{r}_3 + \vec{r}_2}{m_a + 1}$$
 (A1.8)

A two state wave expansion of the total wave function within the independent electron model is

$$\Psi = \phi_b(\vec{x}) F(\vec{r}_i) + \phi_a(\vec{s}) G(\vec{r}_f), \qquad (A1.9)$$

where $\phi_a(\vec{s})$ and $\phi_b(\vec{x})$ are the bound state functions of the active electron around nuclei A and B, respectively. The asymptotic conditions on Ψ are

$$F(\overrightarrow{r_i}) \xrightarrow{\overrightarrow{r_i} \to \infty} \exp(i\overrightarrow{k_i} \cdot \overrightarrow{r_i}) + O(\frac{1}{r_i})$$

and

$$G(\overset{\rightarrow}{r_f}) \xrightarrow{\overset{\rightarrow}{r_i} \to \infty} O(\frac{1}{r_f}).$$
 (A1.11)

The scattered waves are shown to fall off as $\exp(ikr)/r$, i.e. $\mathcal{O}(\frac{1}{r})$.

It is now of relative importance to introduce the quantities,

$$F(\vec{r}_i) = \exp(-i\vec{k}_i \cdot \vec{r}_i) F(\vec{r}_i)$$
 (A1.12)

and

$$G(\vec{r}_f) \equiv \exp(i\vec{k}_f \cdot \vec{r}_f)G(\vec{r}_f).$$
 (A1.13)

This phase transformation is made for later simplification in the transition matrix.

The transition matrix (eq. 2.18) is now given by,

$$T_{if} = \langle \phi_f | V_f | \Psi_i \rangle$$

$$= \langle \phi_2 (\overrightarrow{s}) \exp(-i\overrightarrow{k}_f \cdot \overrightarrow{r}_f) | V_f | \Psi_i \rangle, \qquad (A1.14)$$

where Ψ is given by eq. Al.9. Substitution of $F(\vec{r}_i)$ and $G(\vec{r}_f)$ from eqs. Al.12 and Al.13 gives,

$$\Psi = \exp(i\vec{k}_i \cdot \vec{r}_i) L(\vec{x}, \vec{r}_i), \qquad (A1.15)$$

where

$$L(\vec{x}, \vec{r}_i) = \phi_b(\vec{x})F(\vec{r}_i) + \phi_b(\vec{s})G(\vec{r}_f)\exp\left(-i\vec{k}_i \cdot (\vec{r}_f + r_i)\right). \quad (A1.16)$$

It then follows that the transition matrix is given by,

$$T_{if} = \int d\vec{R} \int d\vec{r} \phi_a^*(\vec{s}) \exp\left(i(\vec{k}_f \cdot \vec{r}_f + \vec{k}_i \cdot \vec{r}_i)\right) V_f L(\vec{x}, \vec{r}_i)$$
(A1.17)

Modification of the exponential phase in eq. Al.17 is needed. Consider,

$$\vec{k}_{f} \cdot \vec{r}_{f} + \vec{k}_{i} \cdot \vec{r}_{i} = \vec{k}_{i} \cdot \vec{r}_{f} - \vec{k}_{i} \cdot \vec{r}_{f} + \vec{k}_{f} \cdot \vec{r}_{f} + \vec{k}_{i} \cdot \vec{r}_{i}$$

$$= (\vec{k}_{f} - \vec{k}_{i}) \cdot \vec{r}_{f} + \vec{k}_{i} \cdot (\vec{r}_{i} + \vec{r}_{f}) \qquad (A1.18)$$

$$= -\vec{\eta} \cdot \vec{r}_{f} + \vec{k}_{i} \cdot (\vec{r}_{i} + \vec{r}_{f}), \qquad (A1.19)$$

where the definition,

$$\overrightarrow{\eta} \equiv \overrightarrow{k}_{i} - \overrightarrow{k}_{f},$$
(A1.20)

is used. Utilizing eq. Al.3 and eq. Al.6 (also see diagram) it follows

$$-\vec{r}_{f} \approx \vec{R},$$
 (A1.21)

since $m_a >> 1$. Combining eq. A1.19 and eq. A1.21, the phase is

$$\vec{k}_{f} \cdot \vec{r}_{f} + \vec{k}_{i} \cdot \vec{r}_{i} \approx \vec{n} \cdot \vec{R} + \vec{k}_{i} \cdot (\vec{r}_{i} + \vec{r}_{f}). \tag{A1.22}$$

Noting that

$$\vec{R} = z\hat{z} + \vec{\rho}, \tag{A1.23}$$

where \hat{z} is chosen to be $(2k_i)^{-1}(\vec{k_i} + \vec{k_f})$ and $\vec{\rho}$ is the plane of impact parameters perpendicular to \vec{z} , eq. Al.22 becomes

$$\vec{k}_f \cdot \vec{r}_f + \vec{k}_f \cdot \vec{r}_i \approx \vec{n} \cdot \vec{z} + \vec{n} \cdot \vec{\rho} + \vec{k}_f \cdot (\vec{r}_i + \vec{r}_f). \tag{A1.24}$$

However, it is observed

$$\vec{\eta} \cdot \vec{z} = \frac{k_i^2 - k_f^2}{2k_i} z.$$
 (A1.25)

From conservation of energy, we have

$$\frac{k_{i}^{2}}{2\mu_{i}} + \varepsilon_{i} = \frac{k_{f}^{2}}{2\mu_{f}} + \varepsilon_{f}, \qquad (A1.26)$$

where ϵ_i and ϵ_f are the initial and final binding energies of the electrons to the respective nuclei B and A. Combining eq. Al.25 with eq.

A1.26 and noting that

$$\mu = \mu_{1} = \frac{(m_{b} + 1)m_{a}}{m_{a} + m_{b} + 1} \approx \frac{(m_{a} + 1)m_{b}}{m_{a} + m_{b} + 1} = \mu_{f},$$
(A1.27)

we get

$$\overrightarrow{\eta} \cdot \overrightarrow{z} = \frac{\varepsilon_{\mathbf{f}} - \varepsilon_{\mathbf{i}}}{\mathbf{v}} z, \qquad (A1.28)$$

where $\mu v = k_i$ is used. Defining $\Delta E = \epsilon_f - \epsilon_i$ and substituting eq. Al.28 into eq. Al.24, the phase takes the form

$$\vec{k}_{f} \cdot \vec{r}_{f} + \vec{k}_{i} \cdot \vec{r}_{i} \approx \vec{n} \cdot \vec{p} + \vec{k}_{i} \cdot (\vec{r}_{i} \cdot \vec{r}_{f}) + \frac{\Delta E}{v} z.$$
 (A1.29)

Replacing the phase in the transition matrix (eq. Al.17) by eq. Al.29, we obtain

$$T_{if} \approx \int \exp(i \vec{n} \cdot \vec{\rho}) d\vec{\rho} \int_{-\infty}^{\infty} dz \int d\vec{r} \phi_a^*(\vec{s}) \exp(i \xi) V_f L(\vec{x}, \vec{r}_i), \qquad (A1.30)$$

where

$$\xi = \vec{k}_i \cdot (\vec{r}_i + \vec{r}_f) + \frac{\Delta E}{v} z.$$
 (A1.31)

Considering only s state to s state electron capture gives our system cylindrical symmetry. Hence, the integration over the plane of impact parameters becomes

$$d\vec{p} = \rho d\rho d\alpha$$
 (A1.32)

and

$$\overrightarrow{\eta} \cdot \overrightarrow{\rho} = \eta \rho \cos \alpha,$$
(A1.33)

where a is the azmuthal angle. The integral,

$$\int_{0}^{2\pi} \exp(in\rho\cos\alpha) d\alpha$$
 (A1.34)

is the evaluated 35 to be,

$$2\pi J_{o}(\eta \rho)$$
, (A1.35)

where J_{o} is the zero order Bessel function of the first kind. Using the result of eq. Al.35, the transition matrix (eq. Al.30) becomes

$$T_{if} \approx -i2\pi v \int_{0}^{\infty} \rho d\rho J_{o}(\eta \rho) b(\rho),$$
 (A1.36)

where

$$b(\rho) = \frac{i}{v} \int_{\infty}^{\infty} dz \int_{\infty}^{\infty} dz \int_{\infty}^{\infty} dz \int_{\alpha}^{\infty} dz \int$$

It follows immediately (eq. Al.36 and eq. 2.6) that the differential cross section is given by,

$$\frac{\mathrm{d}\sigma}{\mathrm{d}\Omega} \approx \left| -\mathrm{i}\mu v \right|_{0}^{\infty} \rho \, \mathrm{d}\rho \, \mathrm{J}_{0}(\eta \rho) \, \mathrm{b}(\rho) \, \left|^{2}.$$
 (A1.38)

In arriving at eq. A1.38 near elastic scattering, i.e. k \equiv k_f, is assumed.

APPENDIX 2

The Brinkman Kramers Probability Amplitude

The probability that a projectile will capture an electron at a given impact parameter, ρ , is

Probability =
$$|b(\rho)|^2$$
, (A2.1)

where $b(\rho)$ is the probability amplitude. From appendix 1, the probability amplitude is given by

$$b(\rho) = \frac{-i}{v} \exp(2i\delta(\rho)) \int_{-\infty}^{\infty} dz \int d\vec{r} \phi_a^*(\vec{s}) \exp(i\xi) \frac{Z_b}{x} \phi_b(\vec{x}), \qquad (A2.2)$$

where the BK potential (eq. 2.23) and the projectile wave function (eq. 2.18) are used. Note in the eikonal phase, we have $\vec{k}_i | |\hat{z}|$. In the probability amplitude (eq. Al.37), we have $\vec{k}_i + \vec{k}_f | |\hat{z}|$. For small angle scattering, \vec{k}_i is approximately parallel to $\vec{k}_i + \vec{k}_f$.

Using the definitions of the reduced mass (eq. A1.27) and the vector relations (eq. A1.3 - eq. A1.6), the phase (eq. A1.31) becomes

$$\xi = (f + g) \overrightarrow{v} \cdot \overrightarrow{r} + \frac{1}{2} (g - f) \overrightarrow{v} \cdot \overrightarrow{R} + \frac{\Delta E}{v} z, \qquad (A2.3)$$

where

$$f = -\frac{m_a}{(m_a + 1)} \frac{(m_b + 1)}{(m_a + m_b + 1)}$$
 (A2.4)

and

$$g = -\frac{m_a}{m_a + m_b + 1}$$
 (A2.5)

Noting that

$$\mathbf{v}_{\mathbf{z}} \hat{\mathbf{z}} \approx \hat{\mathbf{v}}$$
 (A2.6)

and that within $\mathcal{O}(\frac{1}{\mu})$

$$f + g \approx -1,$$
 (A2.7)

the probability amplitude (eq. A2.2) becomes

$$b(\rho) = -b_{BK}(\rho) \exp(2i\delta(\rho)),$$
 (A2.8)

where

$$b_{BK}(\rho) = \frac{i}{v} \int_{-\infty}^{\infty} dz \, \exp(i(\frac{v}{2}(g - f) z + \frac{\Delta E}{v} z))$$

$$X \left[d\vec{r} \phi_a^{\ k}(\vec{s}) \frac{z_b}{x} \phi_b(\vec{x}) \exp(-i\vec{v} \cdot \vec{r}) \right] \tag{A2.9}$$

Following the Fourier transform method of McDowell and Coleman, the probability amplitude for symmetric charge capture ($Z_a = Z_b \equiv Z$ and $m_a = m_b \equiv M$) is

$$b_{BK}(\rho) = \frac{i}{v} \int_{-\infty}^{\infty} dz \exp(i\frac{\Delta E}{v} z) \int d\vec{r} \phi_a^*(\vec{s}) \frac{Z_b}{x} \phi_b(\vec{x}) \exp(-i\vec{v} \cdot \vec{r}). \quad (A2.10)$$

By performing the Fourier transforms on

$$f_a(\vec{k}) = \int \phi_a(\vec{s}) \exp(-i\vec{k} \cdot \vec{s}) d\vec{s}$$
 (A2.11)

and

$$g_{b}(\vec{K}) \equiv \int \phi_{b}(\vec{x}) \frac{Z_{b}}{x} \exp(-i\vec{K} \cdot \vec{x}) d\vec{x}$$
 (A2.12)

to give

$$\phi_{\mathbf{a}}(\vec{\mathbf{s}}) = (2\pi)^{-3} \int f_{\mathbf{a}}(\vec{\mathbf{k}}) \exp(i\vec{\mathbf{k}} \cdot \vec{\mathbf{s}}) d\vec{\mathbf{k}}$$
 (A2.13)

and

$$\frac{z_b}{x} \phi_b(\vec{x}) = (2\pi)^{-3} \int g_b(\vec{K}) \exp(i\vec{K} \cdot \vec{x}) d\vec{K}, \qquad (A2.14)$$

eq. A2.10 is

$$b_{BK}(\rho) = \frac{i}{v} (2\pi)^{-6} \int_{-\infty}^{\infty} dz \exp(i\frac{\Delta E}{v}z) \int d\vec{k} \int d\vec{k} f_{a}(\vec{k})^{*} g_{b}(\vec{k})$$

$$\times \int d\vec{r} \exp(i(\vec{k} \cdot \vec{x} - \vec{k} \cdot \vec{s} - \vec{v} \cdot \vec{r})). \tag{A2.15}$$

From eq. Al.3 and eq. Al.4,

$$\overrightarrow{x} = \overrightarrow{r} + \frac{1}{2} \overrightarrow{R}$$
 (A2.16)

and

$$\vec{s} = \vec{r} - \frac{1}{2} \vec{R}, \qquad (A2.17)$$

the integration over r reduces eq. A2.15 to

$$b_{BK}(\rho) = \frac{i}{v} (2\pi)^{-3} \int_{-\infty}^{\infty} dz \exp(i \frac{\Delta E}{v} z) \exp(\frac{i}{2} \vec{v} \cdot \vec{R})$$

$$\times \int d\vec{k} f_{a}(\vec{k}) g_{b}(\vec{k} + \vec{v}) \exp(i \vec{k} \cdot \vec{R}). \tag{A2.18}$$

Recalling that

$$\vec{R} = \rho \hat{\rho} + z \hat{z}$$
 (A2.19)

and choosing

$$\vec{k} = k_x \hat{x} + k_y \hat{y} + k_z \hat{z}$$
 (A2.20)

such that $\hat{x} | | \hat{\rho}$, the BK probability amplitude (eq. A2.18) is

$$b_{BK}(\rho) = \frac{i}{v} (2\pi)^{-3} \int_{-\infty}^{\infty} dk_{x} \int_{-\infty}^{\infty} dk_{y} \int_{-\infty}^{\infty} dk_{z} f_{a}(k_{x}, k_{y}, k_{z})^{*}$$

$$\times g_{b}(k_{x}, k_{y}, k_{z} + v) \exp(i\rho k_{x}) \int_{-\infty}^{\infty} dz \exp(iz(\frac{v}{2} + k_{z})). \tag{A2.21}$$

At this time, we further limit our development of the BK probability amplitude to consider K shell to K shell capture. The 1s wave function in momentum space is

$$f_a(k) = \frac{8\pi^2 Z_a^{5/2}}{(k^2 + Z_a^2)^2}$$
 (A2.22)

which gives

$$g_{b}(\vec{k} + \vec{v}) = \frac{4\pi^{\frac{1}{2}}Z_{b}^{5/2}}{((\vec{k} + \vec{v})^{2} + Z_{b}^{2})}.$$
 (A2.23)

Completing the integration over \vec{z} and substituting eq. A2.22 and eq. A2.23, eq. A2.21 is

$$b_{BK}(\rho) = \frac{i3Z^5}{\pi v} \int_{-\infty}^{\infty} dk_x \int_{-\infty}^{\infty} dk_y \exp(i\rho k_x) (k_x^2 + k_y^2 + \beta)^{-3},$$
 (A2.24)

where

$$\beta = \frac{v^2}{4} + z^2.$$
 (A2.25)

Integrating over k_{v} , eq. A2.24 reduces to

$$b_{BK}(\rho) = \frac{16Z^5}{v} \int_0^{\infty} \frac{\cos(\rho k_x)}{(k_x^2 + \beta)^{5/2}} dk_x$$
 (A2.26)

The last integration, eq. A2.26 is

$$b_{BK}(\rho) = \left(\frac{2i}{v}\right) z^5 \left(\frac{\rho^2}{\beta}\right) K_2 \left(\beta^{\frac{1}{2}}\rho\right), \qquad (A2.27)$$

where K₂ is the second-order modified Bessel function of the third kind. This corresponds to the transition probability amplitude calculated in a straight-line impact parameter method given by Belkic and Salin as,

$$b_{BK}(\rho) = \left(\frac{2i}{v}\right) \left(z_a z_b\right)^{5/2} \left(\frac{\rho^2}{\gamma_o}\right) K_2 \left(\gamma_o^{\frac{1}{2}}\rho\right), \qquad (A2.28)$$

where

$$\gamma_{o} = Z_{b}^{2} + \left(\frac{v}{2} + \frac{\Delta E}{v}\right)^{2}$$
 (A2.29)

An even more general expression given by McGuire and Cocke is given as,

$$b_{BK}(\rho) = \left(\frac{2 \operatorname{in}}{v}\right) \left(\frac{Z \operatorname{a}^{Z} b}{n_{a} n_{b}}\right)^{5/2} \left(\frac{\rho^{2}}{\gamma}\right) \kappa_{2} \left(\frac{1}{\gamma^{2} \rho}\right), \qquad (A2.30)$$

where

$$\gamma = \frac{Z_b^2}{n_b^2} + \left(\frac{v}{2} + \frac{1}{2v} \left(\frac{Z_a^2}{n_a^2} - \frac{Z_b^2}{n_b^2} \right) \right)^2$$
 (A2.31)

and

$$\Delta E = \frac{1}{2} \left[\frac{Z_a^2}{n_a^2} - \frac{Z_b^2}{n_b^2} \right]. \tag{A2.32}$$

The principal quantum numbers are indicated by n_a and n_b for the respective nuclei A and B. The probability amplitude in eq. A2.30 is justified 19

only when there is a one-to-one correspondence between the angle and impact parameter, in contrast to eq. A2.28.

APPENDIX 3

The computer program for the calculation of the differential cross section for the static potential in the eikonal phase, cf. Section 3.1, is listed.

BRINKMAN KRAMERS APPROXIMATION. JOB TIME=(,59), PAGES=15 COMPUTES DIFFERENTIAL CRGSS SECTION FOR SCREENED COULDMB BRINKMAN PHASE AND CAPTURE PROBABILITY WORKED OUT IN THEORY BY STEVEN R. READ IN PROJECTILE(A)-TARGET(B) CHARGE AND MASS (ELECTRON MASS KRAMER'S APPROXIMATION FOR ELECTRON CAPTURE. INCLUDES EIKONAL ELECTRON VOLTS) = ', 1PD11.4/ JOH (522804028, DMB0S4N8), 'S.R. ROGERS', TIME=(,59) READ IN GAUSS LEGENDRE WEIGHTS AND ABCISSA ARRAY, XW READ IN INCIDENT ENERGY OF PROJECTILE IN ELECTRON VOLTS ROGERS AND JAMES H. MC GUIRE, KANSAS STATE UNIVERSITY. CCMMON CUEF, XBAR, KC, THETA, RO, THETAD, ETA READ 10, ((XW(I,J),J=1,4),I=1,NUMBER) 3 FORMAT ('1', 20X, 'SCREENED COULCMB
1 //21X, 'ENERGY (IN ELECTRON C HYDROGEN (1S) TC HYDROGEN (1S) STATES C IMPLICIT REAL *8 (A-H, 0-Z) REAL* 8. MA, MB, NA, NB, KC, MU DIMENSION XW(100,10) PI=3.1415926535898 FURMAT (4020.14) NUMBER = I CRDER /4 FURWAT (020.14) EXTERNAL FOFY EXTERNAL GOFY PRINT 3, EINC REAU 1, EINC REAL#8 LAB ICRDER=12 // EXEC WATFIV //WATFIV NISKS// 0 \$ JOB U U $\circ \circ \circ$ $\circ \circ \circ$

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PRINCIPLE QUANTUM NUMBERS OF PROJECTILE-ELECTRON SYSTEM (NA) AND TARGET-
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C LIMITS OF INTEGRATION FOR DIFFERENTIAL CROSS SECTIONS
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              C1=NA*32*PI*(ZBBAR*ZABAR)**2.500
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            COEF=KO*C1/(16×VO*PI*XBAR**2)
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READ 2, ZA, ZB, MA, MB

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IF (THETAD-2.0-2) 75,76,76

R.O=A0/2/28

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LAB=(1.+2.*TAU*DCOS(THETA)+TAU**2)**1.500/DABS(1.+TAU*DCOS(THETA))
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DIFCRS=(FOFYI**2+GOFY2**2)*2
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                                                                                                                                                                                                                                                                                                                                  HIHETA=C1*MU/(2.00**.500*PI*(ZBBAR**2+42) **3)
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IF (IERO.NE.O) PRINT 7, IERO

CALL BESK (B/RC, 0, BKO, IERO)

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                    SERIES APPROXIMATIONS AND THEN COMPUTES N TH ORDER FUNCTION
                                            RECURRENCE RELATION AND POLYNOMIAL APPROXIMATION TECHNIQUE
                                                      AS DESCRIPED BY A.J.M.HITCHCOCK, "POLYNOMIAL APPROXIMATIONS
           BESSEL FUNCTIONS USING
                                                                             FUNCTIENS*, M.T.A.C., V.11,1957,PP.86-88, AND G.N. WATSON,
                                                                                        'A TREATISE ON THE THEORY OF BESSEL FUNCTIONS", CAMBRIDGE
                                                                  BESSEL FUNCTIONS OF CROER ZERC AND ONE AND TO RELATED
                                                                                                                              AND FIRST DRUER
                                                                                                                                                                                 CCMMON COEF, XBAR, KO, THETA, RO, THETAD, ETA DIMENSION T(12)
                                                                                                   UNIVERSITY PRESS, 1958, P. 62
                                USING RECURRENCE RELATION.
                                                                                                                                               SUBROUTINE BESK(X,N,BK,IER)
           COMPUTES ZERO ORDER
                                                                                                                                                          IMPLICIT REAL #8(A-H, 0-Z)
                                                                                                                                                                                                                                                                                      IF(X-170.0)22,22,21
                                                                                                                                                                                                                                                                                                                                   IF(X-1,136,36,25
                                                                                                                                                                                                                                                                                                                                                                                                                  IF(N-1)27,29,27
                                                                                                                                                                                                                                                                                                                                                                                                     T(L)=T(L-1)*B
                                                                                                                                                                                                                                                     IF(X)12,12,20
                                                                                                                                                                                                                   IF(N)10,11,11
                                                                                                                                                                                                                                                                                                                                                                                           DC 26 L=2,12
                                                                                                                                                                                                                                                                                                                                               A = D \in XP(-X)
                                                                                                                                                                                                                                                                                                                                                                     C=DSORT(B)
                                                                                                                                                                     REAL - 8 KC
METHOD
                                                                                                                                                                                                                                         RETURN
                                                                                                                                                                                                                                                                          RETURN
                                                                                                                                                                                                                                                                                                                                                          B=1./X
                                                                                                                                                                                                                                                                                                                                                                                T(1) = 8
                                                                                                                                                                                                                                                                                                             RETURN
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COMPOUND AC COLDS FOLYNCE AFFROATABLION	0
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1566642%T(1)+-08811128%T(2	BESK
368*T(8)-*4262633*T(9)+*2184518*T(10)-*0680977	S
85383*T(12))*C	S
3,28,	S
	S
CRN	5
	S
MPUTE KI LSING POLYNOMIAL APPROXIMATION	BESK ARSK
A*(1.2533141+.4699927*I(1)1468583#I(2)+.1283	1 11
1736432*T(4)+.2847618*T(5)4594342*T(6)+.6283381*T(7	E CO
6632295%T(8)+.5050239%T(9)2581304*T(10)+.07880001*	11:
.01082418#T(12))*C	S
(N-1)20,3	U)
11	S)
-	SU
	7) U
E AN USING PECONCENCE NEEDIN	J W
35 J=2,N	ES
=2.*(DFLOAT(J)-1.)*G1/X+60	S
GJ-1.0E70133,3	ES
11	ES
-	ES
=61	ES
1=C)	S
	S
TURN .	S
: X/2.	ES
.5772157+DLCG(8)	ES
E T	ES
(N-1)37,43,37	BESK

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G1=G1+X2J*FACT*(.5+(A-HJ)*DFLDAT(J))
CCMPITE KO USING SERIES EXPANSION
                                                                                                                                                                                               CCMPUTE KI USING SERIES EXPANSION
                                                                                                                                                                                                                                                                                                                                                                                                SUBROLTINE BESJO (X,BJ,IER)
COMPUTES THE J-ZERO BESSEL FUNCTION
                                                                                                                                                                                                                                                                                                                                                                                                                                    BESJO (X, BJ, 1ER)
                                                                                                                                                                                                                                                           G1=1./X+X2J*(.5+A-HJ)
                                                                                                                                   60=60+X20*FACT*(HJ-A)
                                                                                                           FACT=FACT*RJ*RJ
                                                                                                                                                                                                                                                                                                           FACT=FACT*R J*RJ
                                                                                                                                                                                                                                                                                                                                                IF (N-1)31,52,31
                                                                                                                                                                                                                                                                                               RJ=1./DFLOAT(J)
                                                                                   RJ=1./DFLOAT(J)
                                                                                                                                               IF(N)43,42,43
                                                                                                                                                                                                                                                                      DC 50 J=2,8
                                                                       CO 40 J=1,6
                                                                                               X2J=X2J*C
                                                                                                                                                                                                                                                                                   X2J=X2J#C
                                                                                                                       FJ=FJ+RJ
                                                                                                                                                                                                                                                                                                                       FU=FU+RU
                                                                                                                                                                                                                                                                                                                                                                                                                                   USAGE: CALL
                                                                                                                                                                                                                                   FACT=1.
                                                FACT=1.
                                                                                                                                                                       RETURN
                                                                                                                                                                                                                                                                                                                                                                       RETURN
                                    x2J=1.
                                                                                                                                                           BK=60
                                                                                                                                                                                                                                                FJ=1.
                                                            HJ= 0
                                                                                                                                                                                                                        X2J=R
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                        G 0 = -A
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BESK1170 BESK1180 BESK1190

BESK1000 **BESK1010** BESK1020 **BESK1030** RESK1040 **BESK1050** BESK 1060 **BESK1070** RESK1080 BESK1090 BESK1100 BESK1110 BESK1120 BESK1130 BESK1140 **BESK1150** BESK1160 BESK1210

8ESK1220

BESK1200

BESK1230

BESK1240 BESK1250 BESK1270 BESK1280 BESK1290 **BESK1300**

BESK1260

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.3163866DO*(VALUE1)**6+.0444479DO*(VALUE1)**8-.3039444DO*(VALUE1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             TFETA0=X-.7853581600-.0416639700*(VALUE2)-.0000395400*(VALUE2)**2
                                                                                                                                                                                                                                                   APPROXIMATION ASCRIBED IN "HANDBOOK OF MATHEMATICAL FUNCTIONS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         1-.00309512D0*(VALUE2)**3+.00137237D0*(VALUE2)**4-.00072805D0*
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               FG=.75788456D0-.6C600677D0*(VALUE2)-.06552740D0*(VALUE2)**2
                                                                                                                                                                                                                                                                           WITH FORMULAS, GRAPHS, AND MATHEMATICAL TABLES", EDITED BY
                                                                                                                                                                                                                                                                                                       M. ABRAMOWITZ AND I. A. STEGUN, 1972, N.Y., PAGE 369-370,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    150 BJ=1.DO-2.249999700%(VALUE1)**2+1.265620800%(VALUE1)**4-
                                                                                                                                                                                                                        JO BESSEL FUNCTION IS CALCULATED BY THE POLYNOMIAL
X - ARGUEMENT OF THE JO BESSEL FUNCTION
BJ - VALUE OF THE JO BESSEL FUNCTION
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             CCMMCN COEF, XBAR, KO, THETA, RO, THETAD, ETA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   2(VALUE2) **5+.00014476D0*(VALUE2) **5
                                                       IER - ERRCR COCE FOR THE FUNCTION
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        2 **10+.0062100DC*(VALUE1)**12
                                                                                  NC ERRCR
                                                                                                          X.LT.-3
                                                                                                                                                                                                                                                                                                                                                                                                                                              SUBROUTINE BESJO (X, BJ, IER)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                      IMPLICIT REAL*8 (A-H,C-Z)
                                                                                                                                                                                                                                                                                                                                   EQUATIONS 9.41 AND 9.43.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           IF (X-3.) 150,150,200
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             IF (X+3.) 50,100,100
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       VALUE1=X/3.D0
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                                                                                   INAU
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    REAL*8 KO
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        RETURN
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PARAMETERS:

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257 2)* 000	NE SSIGMA	UTE THE INTEGRAL OF	GRATICN		SSIGMA (FOFY, A, B, C, D, E, F, N, XW, NUMBER, INVE		N OF PARANE	ARE POINTS OF INTEGRATION	MBER OF INTERVALS TO INTEGRATE	GAUSS LEGENDRE WEIGHTS AND ABCISSA AR	- CRDER OF THE LEGENDRE PCLYNCMIAL USED	RT - SWITCHES THE FUNCTION IN THE INTEGRAT	FCM FOFY (1) TO GDFY (2)	SULTING INTEGR			ER MUST BE DIVISIBLE BY 4		ES AND FUNCTION SUB	LE PRECISION FUNCTION FOFY (Y	ICIT REAL *8 (A-H, 0-Z)	= FUNCTION 1	URE			AIN PROGRAM	CIT REAL # 8(A	SICN XW (100,1	NAL FOF

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SIGMA47R
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                                           SIGMA34A
                                                      SIGMA34B
                                                                 SIGMA34C
                                                                            SIGMA34D
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                                                                                            SUBROUTINE SSIGMA (FOFY, AA, BB, C, D, E, F, N, XW, NUMBER, INVERT, SSUM)
                                 READ IN GAUSS LEGENDRE WEIGHTS AND ABCISSA ARRAY, XW
                                                                                                                                   CCMMON COEF, XBAR, KC, THETA, RO, THETAD, ETA
                                                      READ 10, ((XW(I,J),J=1,4),I=1,NUMBER)
FCRMAT (4D20.14)
                                                                                                                                                                                                                                                                                                         Y=(B-A)/2.D0*XW(I,J)*NEG+(B+A)/2.D0
                                                                                                                                                                                                                                                                                                                                                                            SCM=(B-A)/2.DO*XW(I,K)*TOFY
SSIGMA
                                                                                                              IMPLICIT REAL*8(A-H, 0-Z)
                                                                                                                                                                                                                                                                                                                                                                                                  IF (NEG) 200,200,150
                                                                                                                                              DIMENSION XW(100,10)
PRECEDE SUBROUTINE
                                                                                                                                                                                                                                                                                                                    IF (INVERT-1) 1,1,2
                                                                                                                                                                                                                                       DO 100 IX=1,NUMBER
          A-F, N, AND NUMBER
                                                                                                                                                                                                                                                                                                                                                                                       SSUM=SSUM+SCM
                                                                                                                                                                                                                                                                         JX=1,2
                                                                                                                                                                                                                                                                                                                                TOFY=FOFY(Y)
                                                                                                                                                                                                                                                                                                                                                      TOFY=GOFY(Y)
                                                                                                                         REAL*8 KO
                                                                                                                                                                                                                                                                                                                                                                                                             NEG-NEG-2
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                                                                                                                                                                                                                                                                                               K= J+1
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                                                                                                                                                                                                                                                               3.67831498958180E-012.33492536538355E-011.25233408511469E-012.49147045813403E-01
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APPENDIX 4

The main program for the Screened Coulomb Brinkman-Kramers approximation is listed, cf. Section 3.2. The three subroutines not listed are identical to those used in Appendix 3.

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FORMAT ('1',20X,'SCREENED COULCMB BRINKMAN KRAMERS APPROXIMATION'
                                                                                                      C CCMPUTES DIFFERENTIAL CROSS SECTION FOR SCREENED COULDMB BRINKMAN
                                                                                                                                                     PHASE AND CAPTURE PROBABILITY WORKED OUT IN THEORY BY STEVEN R.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        C READ IN PROJECTILE(A)-TARGET(B) CHARGE AND MASS (ELECTRON MASS C
                                                                                                                             KRAMER'S APPROXIMATION FOR ELECTRON CAPTURE. INCLUDES EIKONAL
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      //21X, "ENERGY (IN ELECTRON YOLTS) = ", IPDII.4/ )
JOB (522304028, DMB0S4N8), 'S. R. RUGERS', TIME=(,59)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               READ IN GAUSS LEGENDRE WEIGHTS AND ABCISSA ARRAY, XW
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            C READ IN INCIDENT ENERGY OF PROJECTILE IN ELECTRON VOLTS C
                                                                                                                                                                                 STATE UNIVERSITY.
                                                                                                                                                                                                                                                                                                                                                                    CCMMON COEF, XBAR, KD, THETA, RD, THETAD, ETA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 READ 10, ((XW(I,J),J=1,4),I=1,NUMBER)
                                                                                                                                                                                 ROGERS AND JAMES H. MC GUIRE, KANSAS
                                                                                                                                                                                                                                   ARGEN (1S) TO PYDREGEN (1S) STATES
                                                                            ,TIME=(,59),PAGES=15
                                                                                                                                                                                                                                                                                                                SEAL*8 MA, MB, NA, NB, KO, MU
                                                                                                                                                                                                                                                                                         IMPLICIT REAL*8(A-H;0-Z)
                                                                                                                                                                                                                                                                                                                                                                                            DIMENSION XM(100,10)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                          PI=3.1415926535898
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OF PROJECTILE-ELECTRON SYSTEM (NA) AND TARGET-
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   RO IS SCREENING PARAMETER
                                                                                                                                                                                                                                                                                           DIFFERENTIAL CRCSS SECTIONS
                                                                                                                                                                                                                                                                                                                                                                                                                             SBAR=VO/ ZBBAR*(1.-(ZBBAR**2-ZABAR**2)/VO**2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   IS THE RADIUS OF THE FIRST BOHR DRBIT,
                                                                                                                                                                                                                                                                                                                                                                                                                                          XBAR= ZBBAR* (1.+5848**2/4.)**.500
                                                                                                                                                                                                                                                                                                                                                                                                                                                         C1=NA *32*PI*(ZBBAR *ZABAR) **2.500
                                                                                                                                                                                                                                                                                                                                                                                                                                                                       COEF=KO*C1/(16*VO*PI*XEAR**2)
                                          PRINCIPLE QUANTUM NUMBERS
                                                                                                                                                                                                                                                                                            LIMITS OF INTEGRATION FOR
                                                                                                                                                                                                      VO=(EINC/MA)**0.500
PEAL 2, ZA, ZB, MA, MB
                                                                                                                                                                                                                                                                                                                                                    /ZEBAR
                                                                                                                                                                                                                                                                                                                                                                                 /ZEBAR
                                                                                                                                                                                                                                                                                                                        AA=1.D-10 /ZEBAR
BB=.100 /ZBBAR
              FORMAT (4D20.14)
                                                        ELECTRON SYSTEM (NB)
                                                                                                                                                                                                                    MU=NA *NB/ (NA+NB)
                                                                                                                                                                                                                                                                                                                                                                  /ZBBAR
                                                                                                                                                                          EINC=EINC/RYDB
                                                                                                                               ENERGY IN RYDBERGS
                                                                                                                                                                                                                                                                                                                                                                                               /ZBRAR
                                                                                                                                                            RYDB=13.6DU
                                                                                                                                                                                                                                                 ZABAR=ZA/NA
                                                                                                                                                                                                                                                               28848=Z8/NB
                                                                                                                                                                                                                                   KC=VC*MC
                                                                                                                                                                                                                                                                                                                                                                                                FF=10.
                                                                                                                                                                                                                                                                                                                                                     CC=1.
                                                                                                  NA=1.
                                                                                                                                                                                                                                                                                                                                                                   00=2.
                                                                                                                                                                                                                                                                                                                                                                                  EE=5.
                                                                                     NE=1.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                AC=1.
               N
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     OA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   ں ب
                                                                                                                                                                                                                                                                              000
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8x, THETA", 20X, THETA", 21X, DIFFER ENTIAL CROSS SECTIO
                                                                                                                                                                                                                                               FORMAT (* ',15x, 'CHARGE',13X, 'MASS (ELECTRON MASS = 1)',5X, 'PRINCI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      353X, BPINKMAN KRAMERS', 9X, 'SCREENED CCULJPB', 9X, '8.K.', 9X, 'SCBK'//
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         2'(IN DEGREES)', 21X, '(IN PIMAG**2/RADIAN)', 21X, '(IN PIMAN)*2)'/
                                                                                                                                                                                                                                                                                                                                                                                       BET 1= (V0**4+2*V0**2#(ZBBAR**2+ZABAR**2)+(ZBBAR**2-ZABAR**2)**2)
                                                                                                                                                                                                                                                                                                                 2F10.0,14X, "NA = ",F10.0//1X, "TARGET",9X, 'ZB = ",F10.4,4X, "MB
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   INS', 9X, 'RUNNING TOTAL CROSS SECTIONS' /6X, '(IN RADIANS)', 13X,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 57X, ( [ AB) ", 7X, " (C.M.) ", 7X, " (LAB) ", 7X, " (C.M.) ", 7X, " (C.M.) "//)
                                                                                                                                                                                                                                                                               IPLE OUANTUM NO. 1/1X, PROJECTILE", 5X, 2A = ', FIO. 0, 4X, MA =
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             42X, "(C.M.)",7X,"(LAB)",7X,"(C.M.)",7X,"(LAB)",7X,"(C.M.)",
                                                                                                                                                                         = ',1P011.4//)
                                                                                                                                                                                                                                                                                                                                                                                                                                                             C L O S E D = 2 × × 8 × ( Z A × Z B ) × × 5 / (5 × V O × × 2 × N A × × 3 × N B × × 5 × 8 E T A × × 5 )
                                                                                                     RC=A0/(ZA**(2.00/3.00)+ZB**(2.00/3.00))**.500
                                                                                                                                                                   FORMAT (' ', 20x, 'SCREENING RACIUS (IN AO) PRINT II, ZA, MA, NA, ZB, MB, NB
                                                                                                                                                                                                                                                                                                                                                   3F10.0,14X,'N3 = ',F10.0/)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               ETA=2 . *ZA *ZB/VO
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   DO 50 ITER=1,50
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     THETAS=PI/1.06
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     FURMAT ( . . .
                                                                                                                                     PRINT 21, RC
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           THE TAM = THETA
                                                                                                                                                                                                                                                                                                                                                                                                                           /(4*VO4-x2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 TAU=MA/MB
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 THETAM=0.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     THETAD=0.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               PRINT 101
                                 RO=1.0-2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   HETA=0.
                                                                   RC=1.02
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         SCBK=0.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           CEK=0.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             7 AU=0.
RO=1.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       101
                                                                                                                                                                         21
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C DUTPUT SCALING TO COVER WIDEST RANGE OF VALUES C

OF ANGLE

1F (THETAD-2.D-2) 75,76,76 75 THETA=(THETA+THETAS)*1.3D0

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LAB=(1.+2.*TAU*DCOS(THETA)+TAU**2)**1.500/CABS(1.+TAU*DCOS(THETA))
                                                                                                                                                                                                                                                          A2=VD%+2%((1.60-(288A3=*2-Z48AR**2)/VC4=2)**2+4*MU**2*THETA**2)/4
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       PRINT 22, THETA, THETA1, THETAD, THETD1, DQOBK, DQOBKL, DIFCRS, DIFCRL,
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           CALL SSIGMA (FOFY, AA, RB, CC, DC, EE, FF, 5, XW, NUMBER, 1, FUFY1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        CALL SSIGMA (GDFY, AA, BB, CC, DD, EE, FF, 5, XW, NUMBER, 2, GOFY2)
DIFCES=(FDFY1**2+GDFY2**2)*2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              22 FORMAT (' ', IPD11.4,4(2X, IPD1C.4,2X, IFD11.5),2X,1PD11.5)
                                                                                                                                      THETA1=DARCOS((DCOS(THETA)+TAU)/(1.+2.*TAU*DCOS(THETA)+
                                                                                                                                                                                                                                                                                    HTHETA=C1*MU/(2.D0**.5D0*P1*(288AR**2+A2)**3)
                           IF (THETAD.GT.6.D-2) THETAS=THETAS#4.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                GOFY IS THE IMAGINARY PART OF F(THETA)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  FOFY IS THE REAL PART OF F(THETA)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           F (THETAD.GT.0.3) GO TO 86
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                SCREEN=DIFCRS*THETA*DTFETA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          IF (THETAD.GE.2.) GO TO 51
                                                                                                                                                                                                                                                                                                                                                                            QUBK=DQUBK*THETA*DTHETA
                                                                                    THETAC=THETA*18C.DO/PI
                                                                                                                                                                                                 HET01=THETA1*180./PI
                                                                                                                                                                                                                              DTHETA=THETA-THETAM
                                                       THE TA = THE TA + THE TAS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  CIFCRL=DIFCRS*LAB
                                                                                                                                                                                                                                                                                                                                               DOCRKL=DOCBK*LAB
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           SCBK=SCBK+SCFEEN
                                                                                                                                                                                                                                                                                                                   DGODK=HTFETA**2
                                                                                                                                                                         TAU# 2 ) * 4.500)
THETAS=5.0-5
                                                                                                                                                                                                                                                                                                                                                                                                        OPK=OBK+CCBK
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      50 CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    1CBK, SCBK
                                                                                                                                                                                                                                                                                                                                                                                                                                   FOFY1 = 0.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                 GDFY2=0.
 16
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        86
                                                                                    11
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          \circ \circ \circ
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                UU
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FORMAT (' ', 'CLOSED FORM BK = ', IPD20.13, '; INTEGRAL VALUE 11PD20.13, '; SCREENED CCULGMB BK = ', IPD20.13)
                                                                                                                                         C
C SUBROUTINE FOR GETTING FÜNCTION INTO INTEGRATION ROUTINE
C
                                                                                                                                                                                                                                                                                                         COMMON COEF, XBAR, KO, THETA, RO, THETAD, ETA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 COMMON COEF, XBAR, KO, THETA, RO, THETAU, ETA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      *8K0)*8K2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         FCRMAT (' ', 'IER FUR BESJ IS ', IZ)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   COFY (8)
                                                                                                                                                                                                                       8
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    FCRMAT ( * *, * IER FOR BESK 0 IS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             (KO*THETA*B, BJ, IER)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                      FORMAT (* *, * IER FOR BESK 0 IS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      IF (IER2.NE.J) PRINT 6, IER2
FCPMAT (' ','IER FOR BESK 2 IS
                                                                                                                                                                                                                       FOFY
                                                                                                                                                                                                                                                                                                                                                                                       FURMAT (* ', 'IER FOR BESK 2 IS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      (KO*THETA*B, BJ, IER
                                                                                                                                                                                                                                                                                                                                   CALL BESK (XBAR*B,2,BK2, IER2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             CALL BESK (XPAR* B, 2, BK2, IEK2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        IF (IERO.NE.O) PRINT 7, IERO
                                                                                                                                                                                                                                                                                                                                                          IF (IERZ.NE.O) PRINT 6, IERZ
                                                                                                                                                                                                                                                                                                                                                                                                                                              IF (IERO.NE.O) PRINT 7, IERO
                                                                                                                                                                                                                                                                                                                                                                                                                   CALL RESK (B/RG,0,8K0, IERO)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               CALL BESK (B/RO,0,BKO,IERO)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 IF (IER.NE.D) PPINT 8, IER
                                                                                                                                                                                                                    DOUBLE PRECISION FUNCTION
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  DOUBLE PRECISION FUNCTION
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          IMPLICIT REAL#8 (A-H, G-Z)
CLCSED, OBK, SCBK
                                                                                                                                                                                                                                                    INPLICIT REAL *8 (A-H, U-Z)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    FOFY=COEF#8**3*DSIN (ETA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      CALL BESJO
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       PEALT8 KO
                                                                                                                                                                                                                                                                              REAL#8 KO
```

P [* A O * * 2 .]

('0', 'TOTAL CROSS SECTIONS IN UNITS OF

FURMAT

O) PRINT 8, IER ','IER FOR BESJ IS ',12) 8**3*DCCS (ETA *BKO)*BK2 *8J	INE BESK BESK	820634246719E-014.71753363865118E-029.04117256370475E-011.06939325995318E- 502674154305E-011.60078328543346E-015.87317554286617E-012.03157426723066E- 831498998180E-012.3349253653858E-011.25233408511469E-012.49147045813403E- E 6 000000 E 00 18.00 E 00
	N E	719E-014.7 305E-011.6 130E-012.3 E 6 E 00 18.
IF (IER.NE. 3 FORMAT (' ' GOFY=COEF¥B RETURN END	C SUBROUTI	\$ENTRY 9.81560634246719E 7.69502674194305E 3.67831498998130E 6.0 1.00000000 E 0 /*

DIFFERENTIAL CROSS SECTIONS FOR CHARGE TRANSFER USING SCREENED COULOMB POTENTIALS IN THE EIKONAL APPROXIMATION

by

STEVEN RAY ROGERS

B.A., University of Northern Colorado, 1975

AN ABSTRACT OF A MASTER'S THESIS

submitted in partial fulfillment of the

requirements for the degree

MASTER OF SCIENCE

Department of Physics

KANSAS STATE UNIVERSITY

Manhattan, Kansas

The effects of electronic screening of the internuclear potential in charge transfer is considered. By studying the differential cross section, the role of the internuclear potential is examined. Using the eikonal method of McCarroll and Salin (1968), the effective internuclear potential is represented by the static potential. The differential cross section for capture of K-shell electrons from helium by 293 keV protons observed by Bratton, et al., (1977), are compared with the theoretical predictions of Brinkman and Kramers (BK), Belkic and Salin (CBK), and myself (SBK). The shape of the observed differential cross section is in closer agreement to SBK, which uses the static potential, than BK, which uses no potential, or CBK, which uses the full Coulomb potential. The SBK differential cross section yields an improvement over CBK for the capture of K-shell electrons from argon by 6 MeV protons observed by Cocke, et al., (1976). Both CBK and SBK show marked improvements over BK.