

A SOIL-AGGREGATE
CRUSHING-ENERGY METER

by

DAVID WAYNE BOYD
B.S., Kansas State University, 1981

A THESIS

submitted in partial fulfillment of the
requirements for the degree

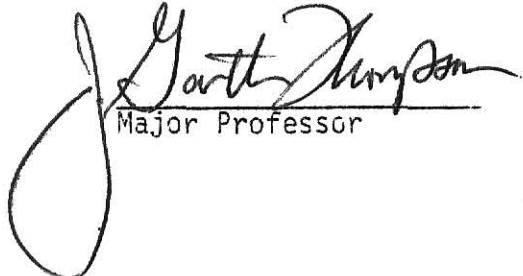
MASTER OF SCIENCE

Department of Mechanical Engineering

KANSAS STATE UNIVERSITY
Manhattan, Kansas

1982

Approved by:


Major Professor

**THIS BOOK
CONTAINS
NUMEROUS PAGES
WITH THE ORIGINAL
PRINTING BEING
SKEWED
DIFFERENTLY FROM
THE TOP OF THE
PAGE TO THE
BOTTOM.**

**THIS IS AS RECEIVED
FROM THE
CUSTOMER.**

Spec.
Coll.
LD
2668
.T4
1982
B69
c.2

A11202 248354

PREFACE

This thesis describes the design, construction, and testing of an instrument to measure the energy required to crush soil aggregates. Chapter I consists of an article submitted for publication describing the purpose of the work and containing brief descriptions of the solution and results. It is self-contained and is presented in the format required for submission to a journal, but later chapters assume that the reader is familiar with the material in Chapter I.

Later chapters, taken with the appropriate appendices, constitute the documentation for the device. Appendix D is a separable operator's manual for the device and is thus presented last. However, familiarity with the material there may help to clarify some other parts of the thesis.

I would here like to acknowledge the contributions of several people who were instrumental in making this work possible. Dr. Garth Thompson has been a continual source of ideas, motivation and energy. Without him, this project may never have come about and certainly would have been more difficult.

I would like to thank Dr. Ed Skidmore for providing the problem to be solved, and his patience, and for his many helpful suggestions.

I would like to thank Mr. Bob Rousser whose expert machining skills and suggestions were vital and much appreciated.

And finally, a special thanks to Mr. Mike Schwartz at KSU Extension Agricultural Engineering for the use of the computer system there, for the considerable amount of time he spent assisting me with the system, and for his many suggestions.

TABLE OF CONTENTS

Chapter

I. A SOIL-AGGREGATE CRUSHING-ENERGY METER	1
Abstract.	1
Introduction.	2
System Design	4
Operation	7
Results and Discussion.	9
Literature Cited.	13
Table Headings and Figure Captions.	14
Table	15
Figures	16
II. HARDWARE DESCRIPTION	21
Crushing Vise	21
Computer Module	23
Accessories	24
III. SOFTWARE DESCRIPTION	26
Overview.	26
SACEM Monitor	26
Subroutine Descriptions	27
RAM Locations	31
IV. CALIBRATION AND TESTING.	34
Displacement Transducer	34
Load Cell	37
System.	40
Conclusions	41
LITERATURE CITED.	43
APPENDIX A Detailed Hardware Explanation	44
APPENDIX B Software Flow Diagrams.	64
APPENDIX C Program Listings.	83
APPENDIX D Operating Instructions.	111

LIST OF TABLES

Table

1. Slopes and Coefficients of Determination of Comparison of Methods for Determining Break Force and Crushing Energy.	15
4.1. Displacement Transducer Calibration Data.	35
4.2. Load Cell Calibration Data.	38
4.3. SACEM and Instron Comparison Data	42

LIST OF FIGURES

Figure

1. Photograph of Soil-Aggregate Crushing Energy-Meter.	16
2. Typical Soil Crushing Curve	17
3. Comparison of Initial Break Force as Determined by Two Different Methods	18
4. Comparison of Crushing Energy as Determined by Two Different Methods. Samples with Energy less than 0.1 Joules	19
5. Comparison of Crushing Energy as Determined by Two Different Methods. Samples with Energy Greater than 0.1 Joules	20
2.1. Parts of the Crushing Vise.	22
2.2. System Circuitry Schematic.	25
4.1. Displacement Transducer Calibration Curve	36
4.2. Load Cell Calibration Curve	39
A.1. Crushing Vise Detail.	45
A.2. Instron Adapter Shaft	46
A.3. SYM Memory Map.	47
A.4. Summary of SYM Port Configuration	49
A.5. SDM856 Power Supply Connections	50
A.6. SDM856 Signal Connections	51
A.7. 3606 Power Supply Connections	55
A.8. 3606 Signal Connections	56
A.9. Power Supply and Input Connector.	60
A.10. Computer Module Front Panel Connector	62
A.11. Transducer and Load Cell Connections.	63

LIST OF FIGURES
(Cont.)

Figure

D.1. Sketch of SACEM System.	112
D.2. Typical Soil Crushing Curve	113
D.3. Keyboard Layout	115
D.4. Running Parallel Tests with the Instron	122

CHAPTER I

A SOIL-AGGREGATE CRUSHING-ENERGY METER

ABSTRACT

Soil aggregate stability is an important measurement in determining soil properties. One current method of evaluating soil aggregate stability involves measuring the energy required to crush a soil aggregate and the new surface area generated. The purpose of this work was to develop a new technique for measuring the energy of crushing. Criteria for the improved system: 1) Energy must be measured quickly and accurately. 2) A digital readout should be provided in convenient units. 3) The system must perform tests both independently and in parallel with the previous method. 4) The force on the sample at its initial fracture should be recorded. And 5) the system must be portable. The system developed consists mainly of two parts. A small crushing vise was constructed that can be hand driven or mounted in existing test equipment. A computer module measures the force on the sample and the displacement of the crushing mechanism using a load cell and a displacement transducer. The force X displacement product is numerically integrated to find the crushing energy. The entire system fits easily into a carrying case about the size of a small suitcase and is powered from a single 110 V electrical outlet. The design criteria were met and measurements taken by the new system showed excellent agreement with previous methods. Coefficients of determination between results found by the new device and those found by previous methods were greater than 0.999.

INTRODUCTION

Dry soil aggregate stability is an important measure in the evaluation of soil properties. It finds application in several areas including tillage and wind erosion research. However current methods of evaluating dry soil aggregate stability are tedious and time consuming.

One common method uses a sieving procedure (Chepil, 1953; Toogood 1978). A sample of aggregates is sieved for a given length of time and the remains are weighed. The remains are then sieved for a given length of time and the remains of that sieving are weighed. The dry soil aggregate stability is expressed as a function of the weights remaining after each sieving.

Aggregate stability has been considered to be a function of the energy required to alter a sample. Some (Marshall and Quirk, 1950; Grossman et al., 1959; Farrell, et al., 1967; Gill and McCreery, 1960) have used a drop-shatter technique. In this method, the aggregate stability is expressed in terms of the height from which the sample must be dropped onto a hard surface in order for the sample to fracture. The energy of impact, and thus the energy imparted to the sample, is proportional to the height from which the sample was dropped.

It has been further suggested that aggregate stability is more precisely defined in terms of the energy required to create new surface area in a sample. This has been the subject of recent research at the Wind Erosion Research Laboratory (Skidmore and Powers, 198_). In this method, a sample is crushed and both the energy imparted to the sample and the surface area after crushing must be measured. The crushing is done on an Instron model 1125 Universal Testing Instrument. The sample is placed on the compression table connected to a 0-200 kg load cell. The crosspiece of the machine then

crushes the sample at a speed of 10 mm/min. The Instron machine is equipped with a chart recorder. The pen of the recorder is driven from the output of the load cell and thus deflects in proportion to the force on the sample. The chart is driven at a rate proportional to the crosspiece speed. The plot generated is then a force vs. displacement record of the test. The energy imparted to the sample is related to the area under this curve. The area is integrated by cutting out the portion of the chart under the curve and weighing it. The weight is compared to the weight of a known area of the same paper. Knowing the calibrations of the load cell and the displacement drive, the energy of crushing is easily figured.

The surface area is found by sieving the crushed sample into 13 size divisions. The average surface area for a particle in each size range is estimated and the total area is calculated as a weighted sum of the areas for all the divisions.

This procedure is obviously tedious and time consuming and the Instron machine is so large that it is essentially a permanent installation. The purpose of this work was to expedite the measurement of dry soil aggregate stability by using a different method of measuring the crushing energy. The criteria for the new measuring device were:

- 1) The device must measure the energy quickly and accurately.
- 2) A digital readout in the proper units should be provided.
- 3) The device should be able to perform tests both independently and in conjunction with the Instron machine, thus enhancing the output capabilities of that instrument.
- 4) The device should record the force on the sample at its initial fracture.
- 5) The device should be portable.

SYSTEM DESIGN

The system consists of two main parts, a crushing vise and a computer module. The system is pictured in Figure 1.

The crushing vise is built of $\frac{1}{4}$ inch aluminum plate with steel supporting rods. The travel of the crushing plate is 2.54 cm and is accomplished with 18-revolutions of the drive shaft.

The platform on which the sample rests is supported by an Interface SSM100 load cell. The load cell contains a strain gage bridge in a sealed aluminum package. It delivers a DC voltage proportional to the force on it. The load cell has a force capacity of 445 N (100 pounds).

The displacement of the crushing plate is measured by a Hewlett-Packard 7D-CDT1000 displacement transducer. This is a linear differential transformer that produces a DC voltage proportional to the displacement of its core.

Since the crushing energy is the integral of the product of the force on the sample and the displacement of the crushing plate, these two instruments provide the necessary information for the computer to calculate the crushing energy.

The vise was designed to mount in the Instron testing machine so that parallel tests can be run. This is desirable both for evaluating the system and for enhancing the information available from the Instron tests.

The computer module contains a single board computer, some interfacing circuitry, and the power supply for all of the devices. The computer is a SYM-1 made by Synertek Systems Corporation. It is built around a 6502 microprocessor. It has on board a 28-key keypad and a six-digit LED display that are accessible from user programs.

The interfacing circuitry consists of a Burr-Brown SDM856 hybrid data acquisition system and a Burr Brown 3606 digitally controlled programmable gain instrument amplifier. The data acquisition system is a single integrated circuit that contains an 8-channel differential input analog multiplexer, a sample/hold amplifier, and a 12-bit successive approximation analog to digital converter. The programmable gain amplifier provides 11 possible gains ranging from 1 to 1024. These are selected by lines from the computer. These devices allow handling of the relatively large (0-5V) displacement signal and the relatively small (0-15mV) force signal with the same system. They are also naturally suited to handling of floating point numbers since the gain of the amplifier is similar to an exponent.

When a test is in progress, the computer reads the force and displacement more than 20 times per second and calculates the energy integral using a trapezoidal algorithm. The computer software is written entirely in machine language and is stored in a 2716 EPROM on the computer board. The monitor program continually scans the keyboard waiting for commands to be entered. When a command is detected, control passes to the routine which processes that particular command. When the function has been performed, control passes back to the monitor and scanning begins again.

All calculations are performed to 16 bits of precision and a limited set of floating point arithmetic routines was written to do the calculation. Numbers are stored internally in a 3-byte floating point format. The software occupies approximately 1500 bytes of memory.

The displacement transducer was calibrated using a machinist's vernier caliper. The caliper was used to measure the overall length of the transducer. At the same time, the displacement reading in its unitless form was read

into the computer and displayed. A scaling factor was calculated by comparing the unitless readings of several points with the known caliper readings. Multiplying the unitless reading by the scaling factor gives the displacement in the desired units. The scaling factor is stored in the computer's memory.

The load cell was calibrated in a similar manner. Weights are placed on the crushing platform of the vise in known increments and the force displayed on the computer module in its unitless form.

The scaling factor for energy values was calculated from the other two factors.

The entire system fits easily into a hard-shelled carrying case about the size of a small suitcase. Power to the system is supplied through a single 110 V standard outlet.

OPERATION

The entire system was designed for easy operation. Each command to the computer consists of a single keystroke. Usually the first command used is one which causes the current displacement of the crushing plate to be continually displayed. This is provided to facilitate adjusting the displacement transducer on the vise. This allows the displacement zero to be easily set.

When the vise and instruments are set up and a sample is in place on the crushing platform, the computer is signalled that a test is beginning. The computer takes about two seconds to initialize its variables and configure the input circuitry and then supplies an audible tone to signal the operator that crushing can begin. While the test is in progress, the force and displacement are read and the energy is integrated. The current force on the platform is displayed during the test. During the first part of the test, the computer monitors the crushing force to detect the initial fracture of the sample. This is defined as the force from which the force first drops 25 percent. This is seen more clearly on the typical crushing curve shown in Figure 2. When the break is detected, a flag is lighted in the computer display to inform the operator.

The endpoint of the test is determined from the break force. The default relation is that the test will be ended when the crushing force reaches 1.5 times the break force. This relation can be changed from the keyboard as described later.

During the part of the test after the break has been detected, the computer quits looking for the initial fracture and begins comparing the current force with the force at which the test is to be ended. The integration, of course, continues as before. When the stop force is reached, the computer

sends out a series of audible tones to tell the operator to stop crushing immediately.

Several important values from the test are stored in the computer's memory and are available through other commands on the keyboard. The values available are the aspects of Figure 2 labelled F_0 , D_0 , F_f , D_f , Break Force, and Energy. The displacements are displayed in units of centimeters, the forces in Newtons, and the energy in Joules.

Another command allows changing the method of calculating the force at which to stop the test. As stated above, the default relation is that the test is stopped when the current force is larger than the break force by a factor of 1.5. Using this command, this factor can be changed to any multiple of .25 between 1.0 and 2.25 inclusive. Obviously, the higher this stopping factor the more energy is imparted to the sample. The stopping factor remains at the new value until the computer is shut off or reset. When either of these happens, the value reverts to 1.5.

One final command passes control from the soil testing software to the monitor program supplied with the computer. This allows all of the capabilities of the computer to be used including machine language and BASIC language programming. An RS-232 connector is provided on the computer module so that a terminal may be connected. These capabilities allow easy testing of the hardware.

RESULTS AND DISCUSSION

To verify the accuracy of the new system (dubbed SACEM for Soil-Aggregate Crushing-Energy Meter), the crushing vise was mounted in the Instron machine and 30 tests were run in parallel. Ten tests were run on each of three different soils. The first ten tests used a relatively soft soil of the Aquic Haploxerolls subgroup (Hot Lake). The second ten tests used a soil of the Typic Argiudolls subgroup (Reading). The final ten tests used a relatively hard soil from the Typic Calciorthids subgroup (Rillito). Soils of varying aggregate stability were used so that the system was tested over a wide segment of its operating range. All of the samples were crushed at 10 mm/min.

During early testing it was discovered that the force measuring system of the Instron machine was prone to drift. To minimize the effect of this, the Instron machine was calibrated frequently during the 30 tests.

The energy was calculated from the Instron chart in two different ways. First, the graph of force vs. displacement was cut out and weighed as described earlier. The weight was compared with the weight of a known area of the paper. From the calibration, it was known what energy the standard area represented. The crushing energy was the ratio of the two areas multiplied by the energy represented by the standard area.

The second method is more convenient when weighing a section of the chart paper. This alternate method involves counting the chart paper divisions enclosed by the crushing curve. The number of divisions was compared to the number of divisions in the standard area. The energy was calculated as the ratio of these two numbers multiplied by the energy represented by the standard area. These two methods should give the same results to within the accuracy of the cutting and counting.

The force at which the sample broke was read from the chart.

The break force and energy readings found by these methods were compared to the readings found by SACEM . The results of these comparisons are shown in figures 3-5. Figure 3 shows the break force read from the Instron chart plotted against the break force as determined by SACEM. Also plotted is a 45° line indicating where ideal results would lie. Figures 4 and 5 show the energy found by both Instron methods plotted against the energy as determined by SACEM. The lines on these figures are also 45° lines. Since a wide range of samples was used, the energy readings are plotted in two figures. Figure 4 shows the results for those samples with crushing energy less than 0.1 J and Figure 5 shows the results for those samples with crushing energy greater than 0.1 J.

Straight lines were fitted to the data using the method of least squares to get a measure of how closely the results match the ideal. The lines were constrained to pass through the origin. The slopes and correlation coefficients found are shown in Table 1. Ideally, each line should have a slope of exactly unity.

The SACEM results for the break force correlated with the Instron results to within 0.6 percent and the SACEM results for the crushing energy to within 0.2 percent with the Instron results found by counting the chart paper divisions. However, the energy measured by weighing the paper shows to be consistently about three percent higher than that found by the other two methods. Ideally, all of the methods should give the same results.

It was first suspected that the standard area being used for the weight comparisons was not representative of the chart paper overall. This could result of nonuniformity of the chart paper. If the standard area were taken from a section of the paper that was three percent lighter than average, this

would account for the discrepancy. However another standard area taken from a different section of the chart paper was not much different in weight than the first and tests done near the sections where the standard areas were taken showed the same discrepancy.

It was then theorized that the difference resulted from incorrectly estimating fractions of divisions on the chart when counting was done. Since the crushing curves are very irregular, fractions of divisions must often be estimated. To test this theory, small rectangular sections of chart paper were taken near the place where one of the standard areas was taken. The number of divisions on a rectangular section can be counted accurately. These samples, though better, still did not show the expected agreement.

It was then noted that handling a chart paper sample could cause its weight to change. To evaluate the extent of this change another sample was cut from the chart paper. This sample was irregular but was composed of rectangular segments. This allowed the number of divisions in the sample to be accurately known but also caused the time required to cut out the sample to be relatively long -- similar to the time required to cut out a soil crushing curve. The longer the cutting time, the more the sample must be handled during cutting.

This sample showed nearly the same discrepancy as shown by the soil crushing curves. Evidently, the act of cutting out the crushing curves significantly affects the results because the moisture and oils from the operator's hands are transferred to the paper sample. The energy values measured from cutting out the chart paper are then apparently about three percent too high.

The time required to make an evaluation by the old methods is much longer than by SACEM. A highly irregular chart of typical size can take as long as 15 minutes to be cut out by a careful operator. The reading made by SACEM is available almost instantaneously.

One minor problem can occur occasionally with the definition of the sample break force. If the initial rise of the crushing curve is not smooth, a false break may be detected by SACEM. A slight shift in the sample position or a small fragment breaking off of the sample may cause the crushing force to drop 25 percent long before the sample actually fractures. This occurred once during the 30 tests used for comparison. To help minimize this problem, the computer is programmed to ignore any break detected when the crushing force is less than 2 Newtons.

It is obvious that the SACEM system gives results that are in excellent agreement with previous work and that the design criteria stated earlier are very well met.

LITERATURE CITED

- Chepil, W.S. 1953. Field Structure of Cultivated Soils with Special Reference to Erodibility by Wind. Soil Sci. Soc. Am. Proc. 17:185-190.
- Farrell, D.A., E.L. Greacen, and W.E. Larson, 1967. The Effect of Water Content on Axial Strain in a Loam Soil Under Tension and Compression. Soil Sci. Soc. Am. Proc. 31:445-450.
- Gill, W.R., and W.F. McCreery. 1960. Relation of Size of Cut to Tillage Tool Efficiency. Agric. Eng. 41:372-374, 381.
- Grossman, R.B., J.B. Fehrenbacher, and A.H. Beavers, 1959. Fragipan Soils of Illinois: I. General Characterization and Field Relationships of Hosmer Silt Loam. Soil Sci. Soc. Am. Proc. 23:65-70.
- Skidmore, E.L. and D.H. Powers. 198_. Dry Soil Aggregate Stability: Energy Based Index. Soil Sci. Soc. Am J. (submitted)
- Toogood, J.A. 1978. Relation of Aggregate Stability to Property of Alberta Soils. IN W.W. Emerson, R.D. Bond, and A.R. Dexter (eds.) Modification of Soil Structure. John Wiley and Sons, pp. 211-215.

Table Headings and Figure Captions

Table 1. Slopes and Coefficients of Determination of Regression Variables of Comparison of Methods for Determining Break Force and Crushing Energy.

Figure 1. Photograph of Soil-Aggregate Crushing-Energy Meter (SACEM).

Figure 2. Typical Soil Crushing Curve

Figure 3. Comparison of Initial Break Force as Determined by Two Different Methods (Instron vs. SACEM).

Figure 4. Comparison of Crushing Energy as Determined by Two Different Methods. Samples with Energy Less than 0.1 Joules.

Figure 5. Comparison of Crushing Energy as Determined by Two Different Methods. Samples with Energy Greater Than 0.1 Joules.

TABLE 1

Regression Variables	Slope	r^2
Instron Break Force vs. SACEM Break Force	.9947	.9996
Instron Energy (Weighing) vs. SACEM Energy	1.0345	.9996
Instron Energy (Counting) vs. SACEM Energy	1.0014	.9997

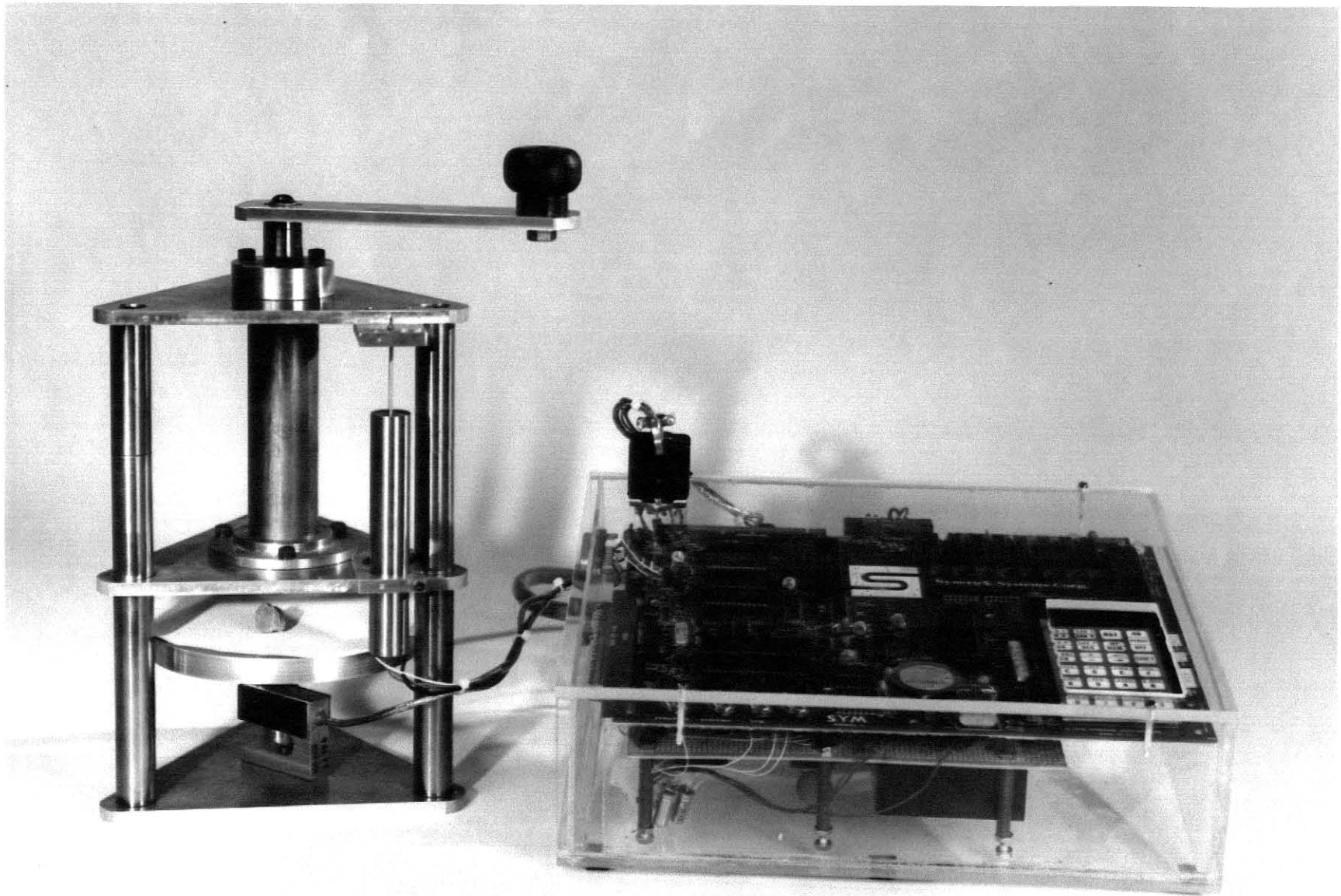


Figure 1

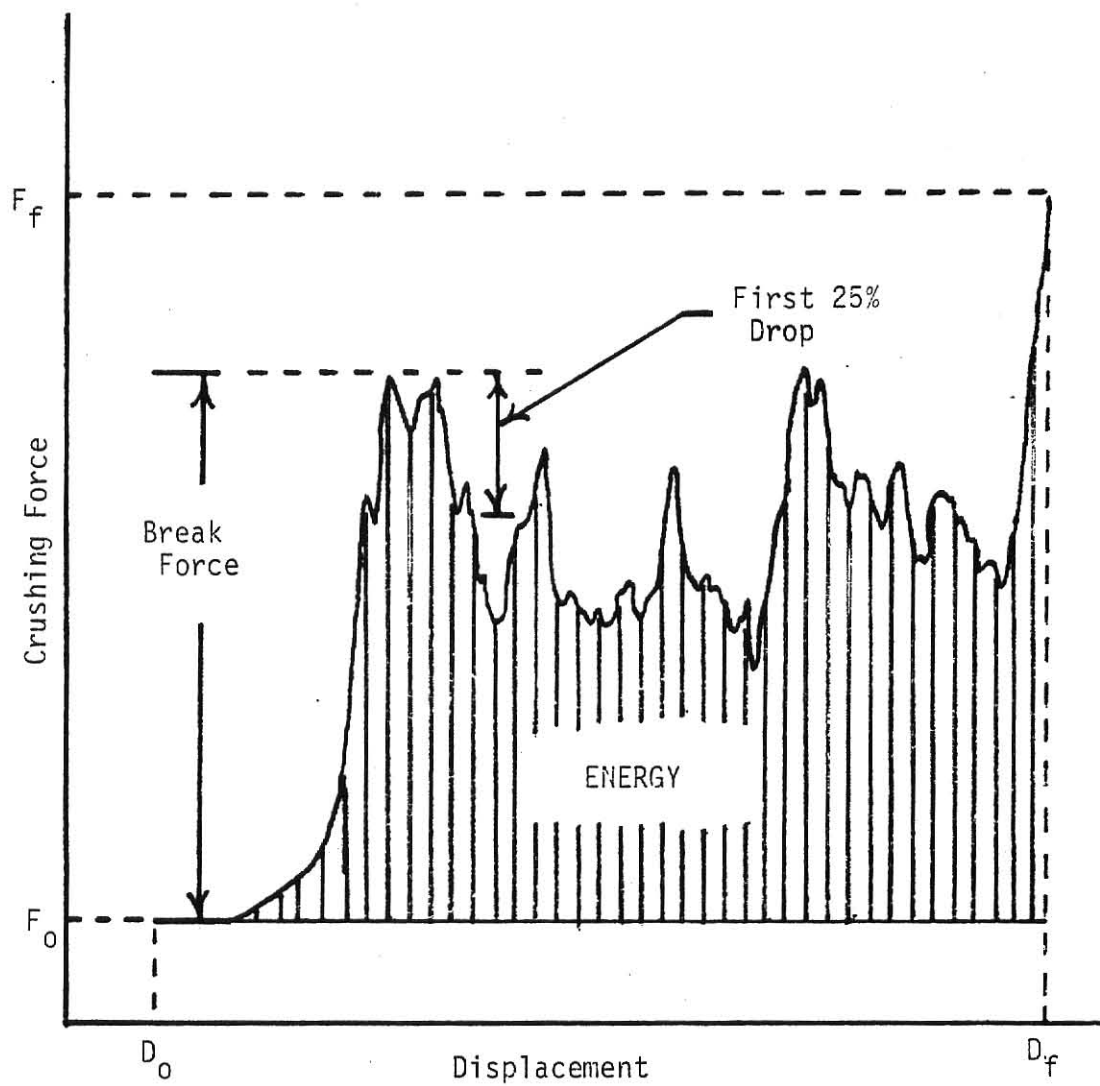


Figure 2.

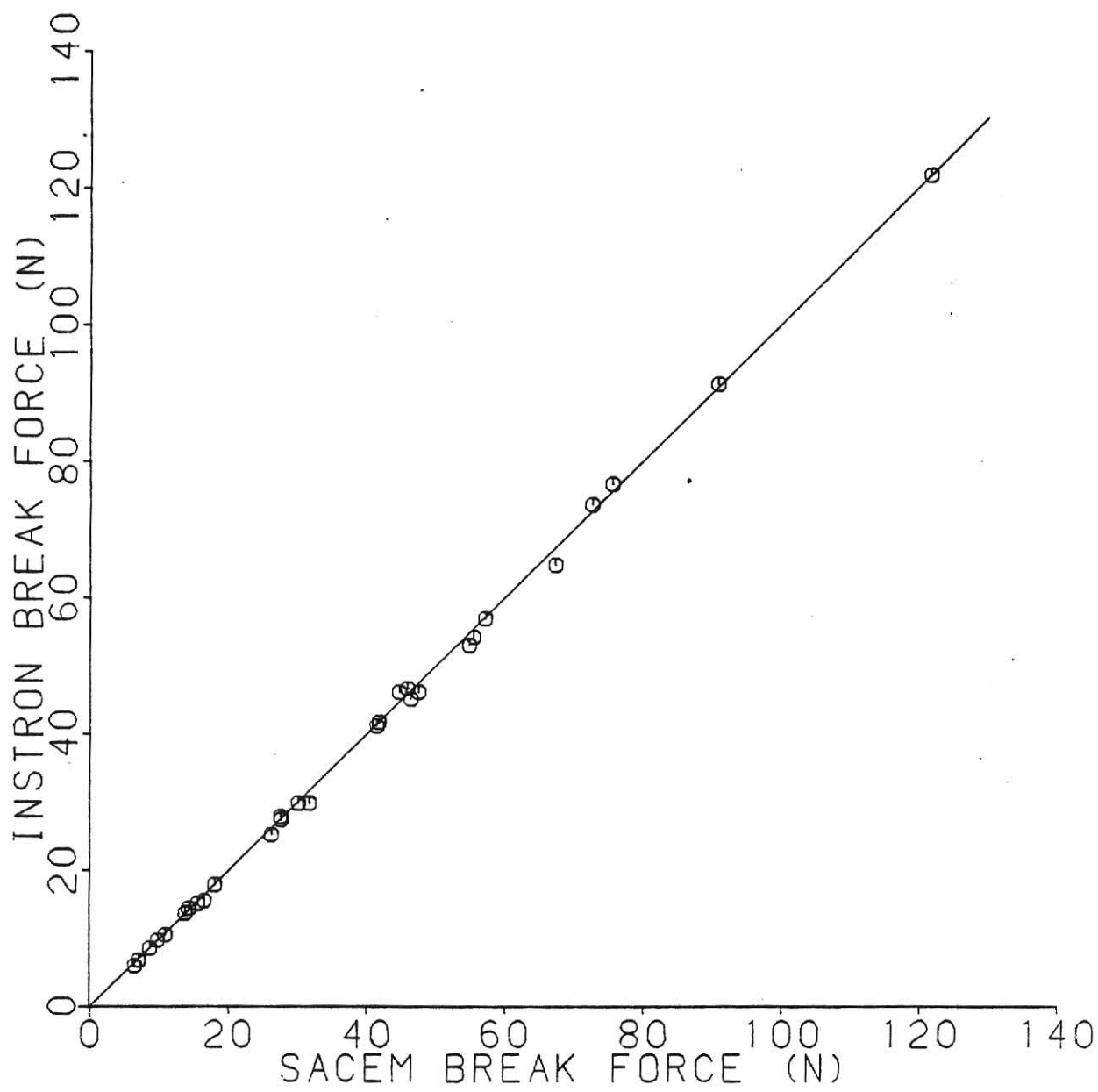


Figure 3

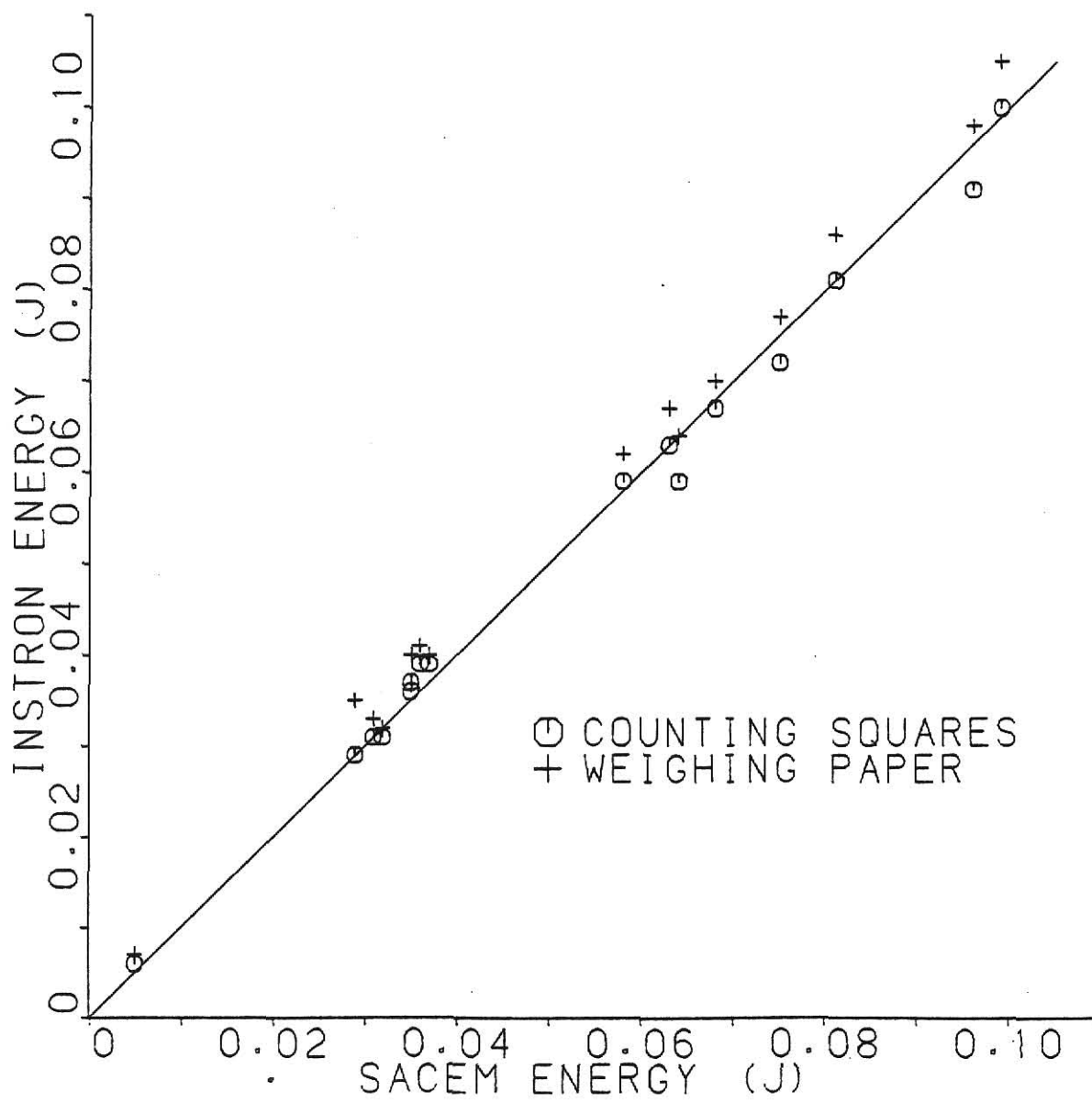


Figure 4.

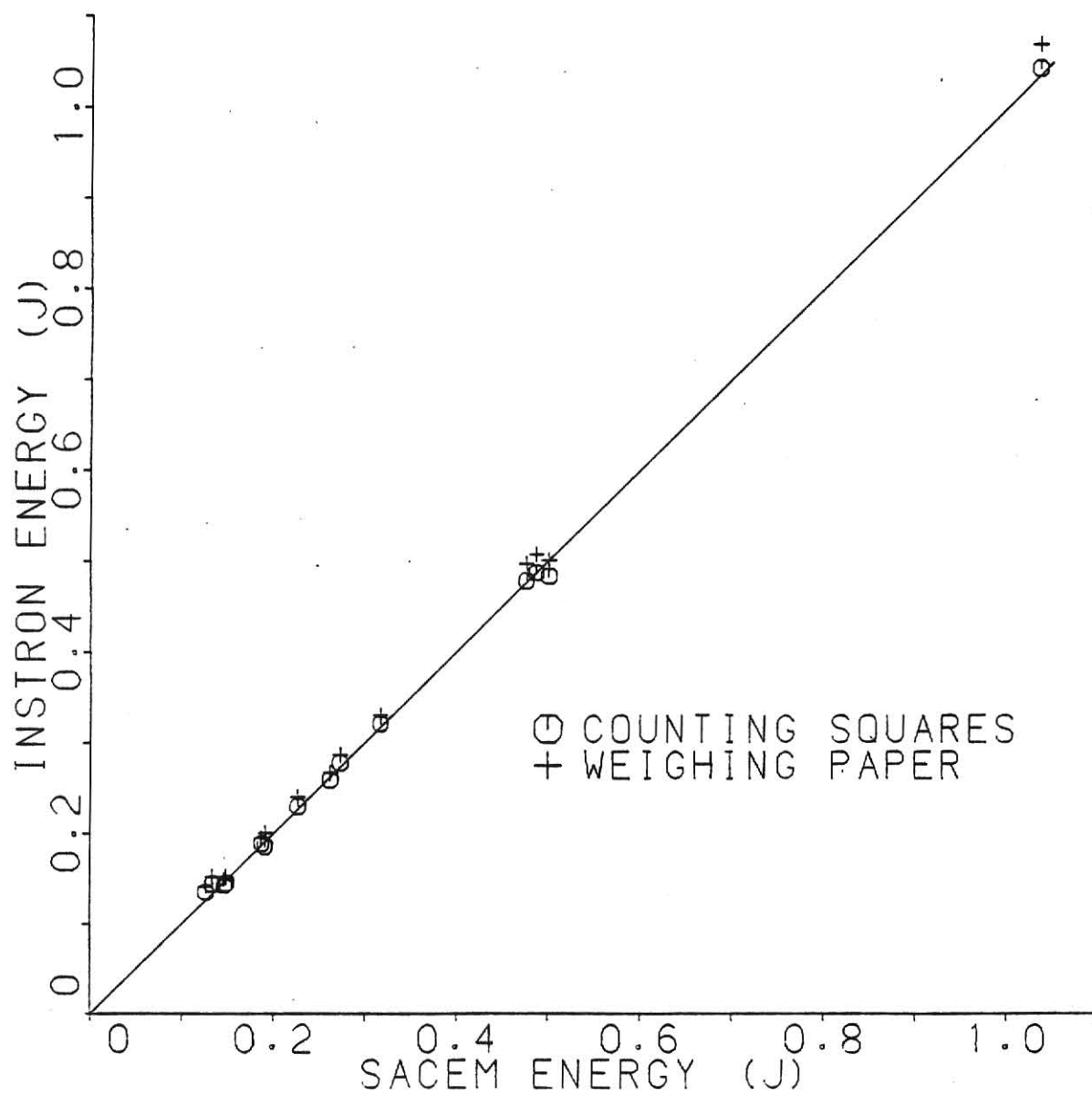


Figure 5.

CHAPTER II

HARDWARE DESCRIPTION

The entire system was pictured in Figure 1.2 and consists of two main parts, the crushing vise and the computer module.

Crushing Vise:

The crushing vise was designed and manufactured specifically for the project. It is shown schematically in Figure 2.1. The crushing plate and end plates are made of $\frac{1}{4}$ inch aluminum plate. The platform is made of $\frac{1}{2}$ inch plate to minimize bending. The support rods are of $\frac{3}{4}$ inch diameter steel rod. The travel of the crushing plate is one inch (2.5 cm) and is accomplished with 18 revolutions of the drive crank. Detailed drawings of the vise and its components are shown in Appendix A.

The displacement of the crushing plate is measured by a Hewlett-Packard 7D-CDT1000 displacement transducer. This is a linear differential transformer. When supplied with a constant excitation voltage, this device puts out a voltage proportional to the displacement of its core.

The force on the sample is measured by an Interface SSM100 load cell which supports the platform. The load cell contains a strain gage bridge in a sealed aluminum package. When supplied with a constant excitation voltage, it delivers a voltage proportional to the force on it.

More detailed information about the load cell and displacement transducer can be found in data sheets supplied by the manufacturers of those devices.

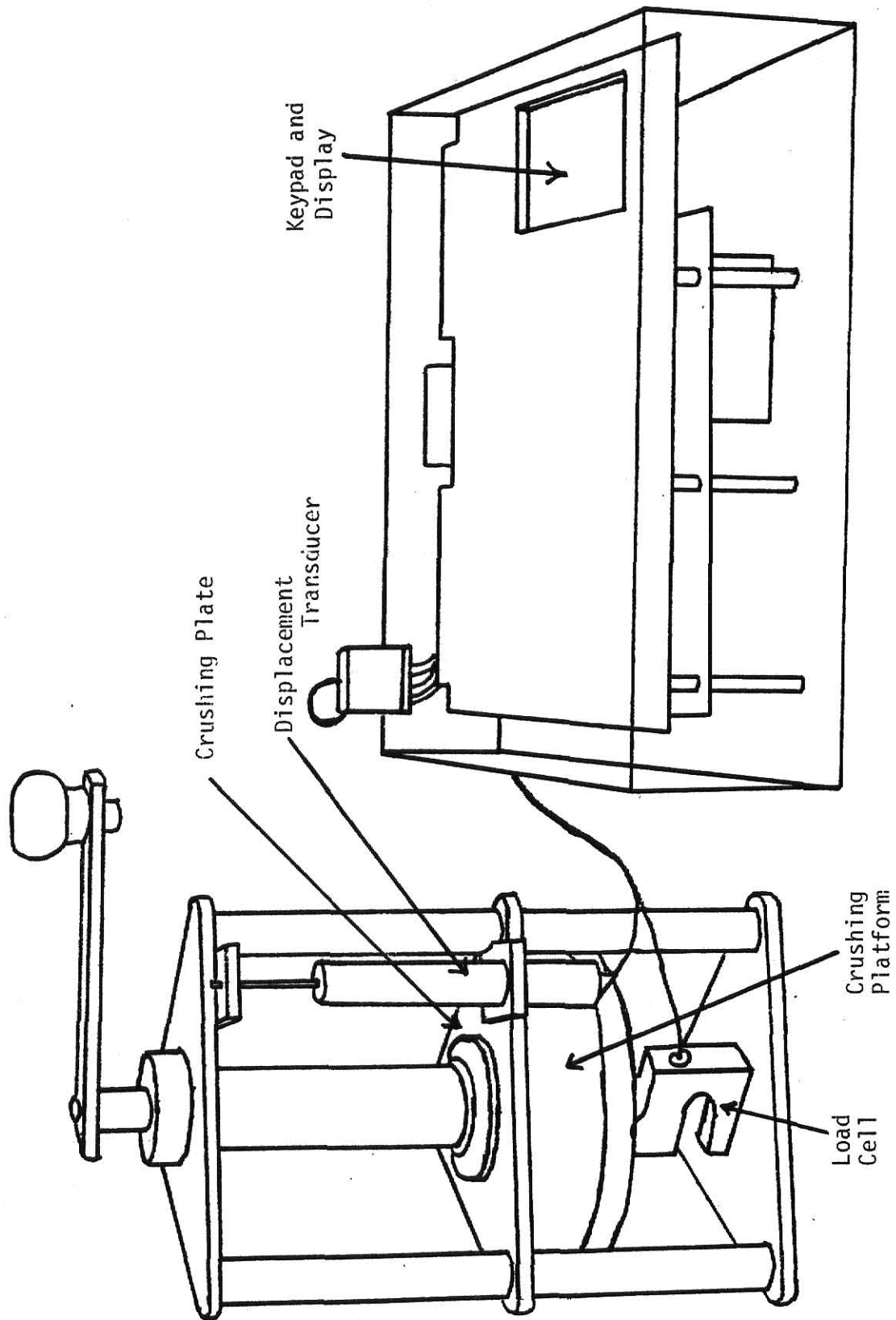


Figure 2.1
Parts of the Crushing Vise

Computer Module:

The computer module contains a single board microcomputer, some interfacing circuitry, and the power supply for all the devices.

The single board computer is a SYM-1 made by Synertek Systems Corporation. It is built around a 6502 microprocessor. It also includes a 28-key keypad, a six-digit LED display, 2½ available input/output ports, and 4K of Random Access Memory. It is provided with a monitor program stored in Read Only Memory. Several of the monitor input/output routines are used in the soil testing software. Though not used in the final implementation, a BASIC language interpreter and an RS-232C terminal connector were added to simplify hardware development and testing. The soil testing software is stored in Read Only Memory on the computer board. More detailed information about the computer can be found in the SYM-1 Reference Manual and the SYM-1 Programming Manual.

The interfacing circuitry consists of a Burr-Brown SDM856 hybrid data acquisition system and a Burr-Brown 3606 digitally controlled programmable gain instrument amplifier. The data acquisition system is a single integrated circuit that contains an 8-channel differential input analog multiplexer, a sample/hold amplifier, and a 12-bit successive approximation analog to digital converter. The programmable gain amplifier provides 11 possible gains ranging from 1 to 1024. These are selected by lines from the computer. These devices used in combination allow handling of the relatively large (0 to 5 V) displacement signal and the relatively small (0 to 15 mV) force signal with the same system. They are also naturally suited to handling floating point numbers since the gain of the amplifier is similar to an exponent.

The power supply is a Power General 326-A triple output switching model. It will supply 4 amperes at 5 volts and 0.2 amperes at both +15 and -15 volts.

More detailed information about the interfacing circuitry components can be found in data sheets supplied by the manufacturer of those devices.

A schematic diagram of the system circuitry is shown in Figure 2.2. When a reading is to be taken, a digital value is put out from the computer which selects both which device is to be read and the gain of the instrument amplifier. The displacement transducer and load cell are selected by different channels of the multiplexer. After a delay of about 300 microseconds to allow the system to settle, the sample/hold amplifier is commanded to hold its value and the A/D converter is commanded to convert the voltage to a digital representation. The digital value is examined to see if all 12 bits are required to represent the voltage. If not, the gain of the amplifier is doubled and the process is repeated until all 12 bits are required. In this manner, each reading can be made to have full precision whether the voltage read was relatively large or small. The amplifier gain required to obtain full precision is recorded by the computer along with the digital value in a floating point number format.

Circuit diagrams and explanations of each pin connection on all the devices can be found in Appendix A.

Accessories:

An adapter shaft was also constructed which allows the crushing vise to be mounted in the Instron testing machine so that parallel tests may be run. The shaft connects to the vise in place of the drive crank which is removed for parallel testing. The shaft also connects directly to the load cell fitting on the Instron machine. This shaft is detailed in Appendix A.

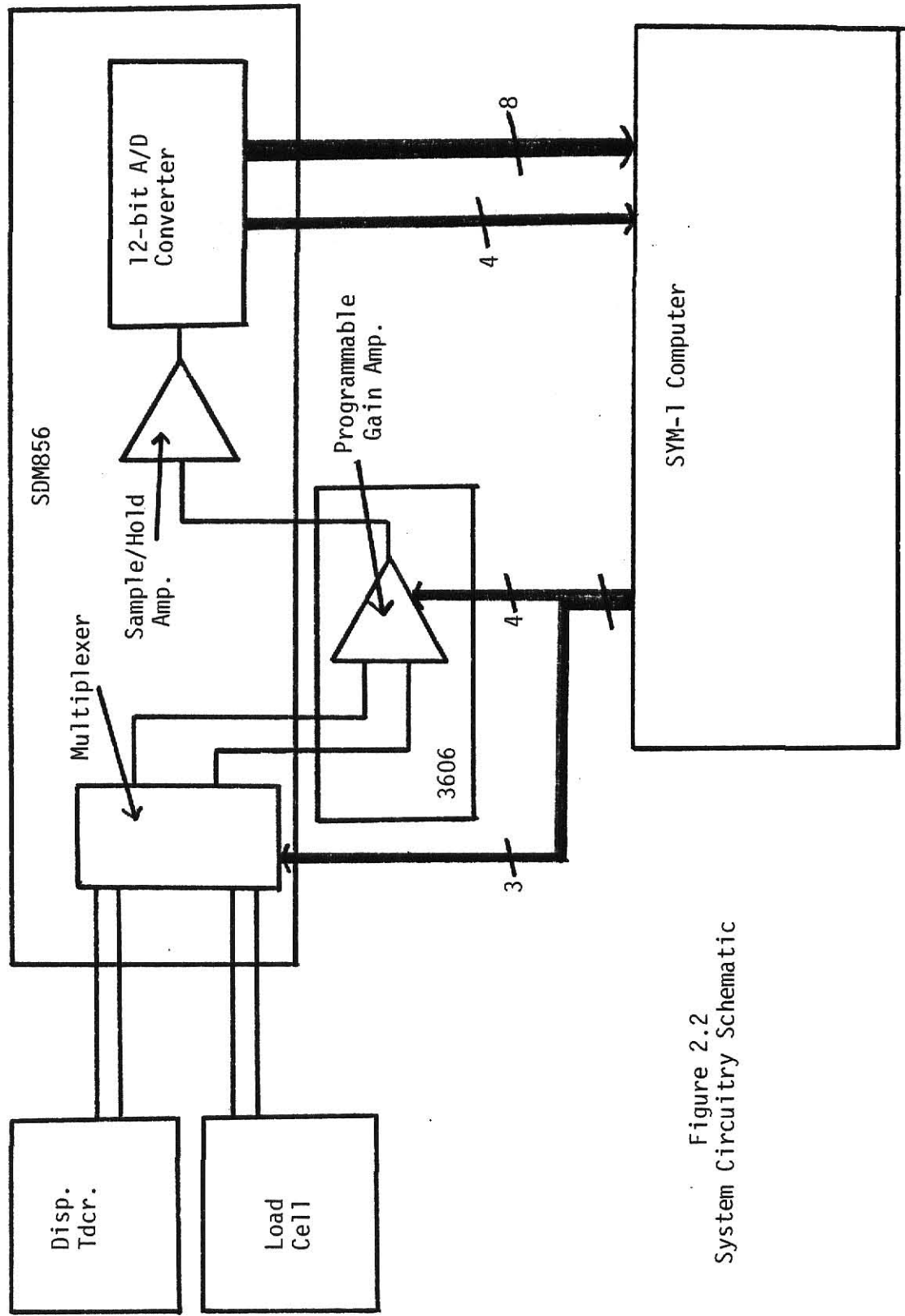


Figure 2.2
System Circuitry Schematic

CHAPTER III

SOFTWARE DESCRIPTION

Overview:

The software of the system consists of two main parts. The SYM monitor and supporting routines were supplied with the computer. The SACEM monitor and command routines were written specifically for this application. The SACEM monitor and command routines use several of the routines within the SYM monitor. The SYM monitor is described fully in the SYM-1 Reference Manual.

SACEM Monitor:

The SACEM monitor begins at memory location E700H. When it is first entered, the system is initialized and the message SOIL 1 is written to the display. The keyboard is then continually polled using a SYM monitor routine. When a keystroke is detected, a unique code identifying the key pressed is placed in the computer accumulator. This code is successively compared to the codes which represent valid commands. When a match is found, control is passed to the routine which processes that particular command. When the command has been executed, control passes back to the monitor and polling resumes. Flow charts for the monitor and the major subroutines used are found in Appendix B.

Several of the monitor functions involve displaying a scaled numeric value. The in-line routine PUTOUT calls the appropriate subroutines to do the scaling and display functions. The addresses of the number to be displayed and the scaling factor are passed to PUTOUT. It assumes a display of three decimal places. This can be altered by loading the computer

accumulator with the desired number places and entering the routine at PUTOUT +2. This is done in the DISPE command.

Subroutine Descriptions:

The following are brief descriptions of all of the subroutines in the SACEM software. Each is headed by its name and the hexadecimal address of its first instruction. It is assumed that the reader is familiar with the architecture of the 6502 microprocessor. In the descriptions, A, X, and Y refer to the accumulator, and X index register, and the Y index register of the microprocessor. Flow charts of all but the simplest routines are found in Appendix B. A complete listing of all of the SACEM software is printed in Appendix C.

TEST E626

The TEST routine is executed during a crushing test. The required variables are initialized upon entry and the crushing energy is continually integrated until the test is ended. The display shows the current force on the crushing plate in kilograms. When the break force is detected, the upper element of the rightmost display digit is lighted as an indicator. The integration is stopped and the beeper is sounded when the current force passes the calculated stop force. If any key is pressed during the test, the test is immediately stopped. If the current force on the platform exceeds about 40 kilograms, the beeper is sounded repeatedly to warn the operator but execution of the TEST routine is continued.

BREAK E52D

The BREAK routine performs several functions and is called by the TEST routine each time through its sample loop. At the beginning of a test

BREAK keeps a running maximum of the crushing force. As soon as the current force drops more than 25 percent below a prior maximum, a flag is set to indicate that the break force has been found. The break force is stored for future reference. If a break force below 0.2 kilograms is detected it is ignored. This is to prevent noise on the force signal from causing false breaks to be registered. Once the break force has been found, BREAK calculates the force at which to stop the test by adding together fourths of the break force. Thereafter, instead of monitoring the force to detect a break, the routine checks to see if the stopping force has been exceeded. The location MAXFLG serves as a flag to indicate the status of the test as determined by BREAK. It is zero initially, is set to one when the break force is detected, and is set to two when the stopping force is exceeded.

INIT E5AF

The INIT routine initializes the variables in RAM. Most variables are initialized by a block move from a table that follows the INIT routine in ROM. Other variables are initialized by taking current readings of the force and displacement through the A/D converter. This routine is called on power up and at the beginning of each test.

DELTA E414

The DELTAE routine calculates the change in crushing energy since the last time it was called. The mathematical expression evaluated by the routine is

$$EDEL = ((\text{Current force} + \text{Past force})/2) * (\text{Current Disp.} - \text{Past disp.})$$

Once the calculation is made, the routine replaces the past values in memory with the current values since these will be the past values on the next call. The value returned is the absolute value of the energy change.

The sign of the result is indicated by the value in location 0. A negative result is indicated by a non-zero value there.

BASE E500

The BASE routine finds the average of eight successive readings of a specified multiplexer channel. The eight readings are added up and the exponent of the sum is decremented three times to get the average. This routine is used to get F_0 and D_0 at the beginning of each test.

READ E000

The READ routine reads a specified channel of the multiplexer and converts the results to the number storage format used by the arithmetic routines. A three-byte floating point format is used. The first byte is the exponent of the number in two's complement form. The next two bytes are the unsigned 16-bit mantissa.

The READ routine selects an amplifier gain of 1 and triggers an A/D conversion. If the result does not have full 12-bit precision the gain is doubled and another conversion is triggered. This continues until either the result has full precision or the highest amplifier gain has been used. Since some gains of the amplifier are selected by more than one combination of control bits, a look-up table is used to determine the proper value to avoid duplication.

CONV E200

The CONV routine converts a three-byte floating point number to a decimal number in the display buffer. The number is separated into integer and fraction parts by shifting it right until the exponent is zero. Each bit is then tested and the equivalent decimal value is added to a running

sum if the bit is a one. When the sum is complete, the result is transferred to the display buffer in the SYM system RAM. If the number is too large to be converted, the display buffer is filled with E's. The largest number that can be converted is about 65,000 in decimal. Decimal equivalents of all the needed powers of two are kept in a table in ROM.

NORM E074

The NORM routine normalizes a floating point number. This is necessary to maintain precision in calculations and to facilitate comparing numbers. The number is shifted left until the most significant bit of the mantissa is a one. The exponent is correspondingly adjusted so that the value represented by the number is unchanged. Zero is represented by a zero mantissa with an exponent of -32. This value was selected so that any finite number generated by the calculations can be found to be greater than zero by comparing only the exponents.

ALIGN E08E

The ALIGN routine aligns two floating point numbers, by shifting the number with the lower exponent to the right and adjusting the exponent until the two numbers have the same exponent. This is necessary before addition or subtraction. This does not change the value represented by either number.

SWAP EOAE

The SWAP routine exchanges the contents of the X and Y registers using the stack. Nothing else is affected.

ADD E0B7

The ADD routine adds two floating point numbers. The numbers are aligned, their mantissas added, and the result is normalized.

SUB E0D5

The SUB routine subtracts one floating point number from another. Since negative numbers are not supported, the result is the absolute value of the difference. If the minuend was larger than the subtrahend, location zero contains a non-zero value on return. This is to indicate a negative result.

MPY E119

The MPY routine multiplies two floating point numbers. A shift and add algorithm is used. The multiplier is shifted right until it becomes zero. If a one is shifted out, the multiplicand is added to a running sum and shifted left. The result is normalized. The exponent of the result is found by adding the exponents of the numbers multiplied.

COMP E400

The COMP routine compares two floating point numbers and sets the flags in the computer's status register accordingly. The routine compares successive bytes of the two numbers until a difference is found. This method relies on the fact that all numbers generated in this application have negative exponents. This routine fails if the exponents of the numbers compared have differing signs.

MOVEM E457

The MOVEM routine moves a floating point number from one specified location to another.

RAM Locations:

All variables used are stored in zero-page RAM so that their addresses can be pointed to by the X and Y registers. The variables used are explained below.

Location	Name	Function
00-0C		Scratch space used by several subroutines. Location 0 is used to pass parameters by SUB, DELTAE, and CONV. Otherwise no meaningful data are here.
0D-1F		Not used
20-22	F0	F_0 in 3-byte floating point form
23-25	PASTF	Force from previous reading used by DELTAE
26-28	PASTD	Displacement from previous reading
29-2B	CURF	Current force reading used temporarily by DELTAE
2C-2E	CURD	Current displacement reading.
2F-31	EDEL	Change in crushing energy returned by DELTAE
32-34	FDIFF	Scratch locations used by BREAK
38	PLIM	Four times the current stopping factor. Initialized to 6 on power on and changed only by monitor command.
39	LIM	Counter value used to figure the stop force. Since this is destroyed during each test, a permanent copy of the value is kept in PLIM. LIM is copied from PLIM by the INIT routine.
3A	MAXFLG	Used by BREAK and TEST to monitor test status.
3B-3D	KG2	Approximately the force reading for a crushing load of 0.2 kg. Used by BREAK to suppress false breaks.
3E-40	FMAX	Used by BREAK for running force maximum. Becomes break force when the break is detected.
41-43	SCR1	Scratch locations
44-46	STOPF	Stop force calculated by BREAK
47-49	ESUM	Running energy integral
4A-4C	KG40	Approximately the force reading for a crushing force of 40 kg. Used to detect too high crushing force so operator can be warned.

4D-4F	FCNV	Unit conversion factor to convert A/D force readings to kg. Determined from load cell calibration. Initialized by INIT each time a test is begun.
50-52	DCNV	Unit conversion factor to convert A/D displacement readings to cm. Determined from displacement transducer calibration. Initialized by INIT each time a test is begun.
53-55	ECNV	Unit conversion factor to convert calculated energies to Joules. Determined from FCNV and DCNV.

CHAPTER IV

CALIBRATION AND TESTING

Displacement Transducer:

The displacement transducer was calibrated using a machinist's vernier caliper. The entire transducer was mounted solidly and the caliper used to measure the overall length. At the same time, the computer was used to read the displacement in its unitless form. The unitless form readings will be referred to in terms of "counts". Comparing the unitless readings with the known caliper measurements allowed calculation of a scaling factor. Multiplying the unitless reading by the scaling factor gives the displacement reading in the proper units.

The actual data points taken are given in Table 4.1. Figure 4.1 shows the calibration curve generated from these points. The data show excellent linearity over the specified range of the transducer. A straight line was fitted to the points using the method of least squares. The resulting relation is

$$\begin{aligned}\text{Unitless Reading} &= -1885.5 * (\text{Caliper Reading}) + 12283 \\ r^2 &= .9999\end{aligned}$$

This gives a relation of 1885.5 counts per inch of displacement. The sign of the coefficient is irrelevant since the polarity of the transducer can be changed. The scaling factor used is calculated as

$$\begin{aligned}\text{DCONV} &= (2.54 \text{ cm/in}) / (1885.5 \text{ counts/in}) \\ \text{DCONV} &= .001347 \text{ cm/count}\end{aligned}$$

Table 4.1
Displacement Transducer Calibration Data

Caliper Reading (inches)	Unitless Computer Reading (counts)
6.489	46.6
6.303	397.3
6.105	777.7
5.900	1161.
5.700	1543.
5.519	1862.
6.479	60.7
6.299	411.6
6.099	787.0
5.899	1165.
5.700	1543.
5.522	1859.
6.500	20.7
6.400	210.9
6.201	589.5
6.005	973.2
5.801	1350.
5.600	1724.
* 5.424	2012.
* 5.302	2128.
* 5.202	2167.

*These points were excluded from the analysis since they are outside the linear range of the transducer.

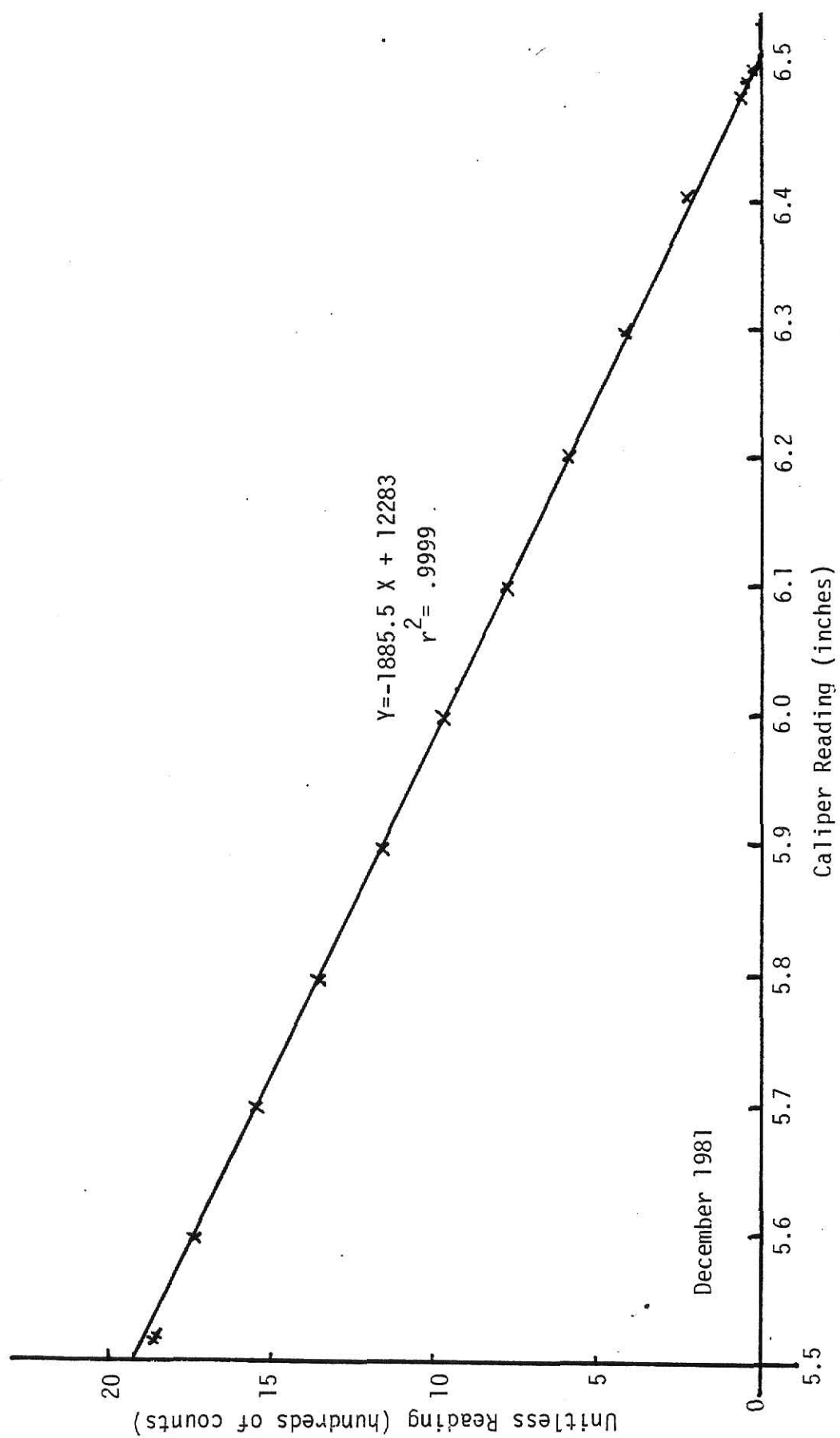


Figure 4.1

Displacement Transducer Calibration Curve

Load Cell:

The load cell was calibrated in a similar manner. Known weights were placed on the crushing platform of the vise and the unitless weight readings displayed on the computer. These readings were compared with the known weights to find a scaling factor in the proper units. A rough two point calibration had already been done while the system was still under development. The rough calibration produced a scaling factor of 2.4066 kg/count. The data points taken for the final calibration are shown in Table 4.2. Figure 4.2 shows the calibration curve generated from these points. The data again showed excellent linearity. A straight line was fitted to the points using the method of least squares. The resulting relation is

$$\begin{aligned} (\text{Unitless Reading}) &= 1.0104 * (\text{Actual Weight}) + 1.329 \\ r^2 &= .999 \end{aligned}$$

The intercept term is due to the weight of the platform of the vise. Using this information and the previous calibration, the new scaling factor is calculated as

$$\text{FCONV} = 2.4066 / 1.0104 = 2.3818 \text{ kg/count}$$

The scaling factor to convert unitless energy results to Joules was calculated as

$$\begin{aligned} \text{ECONV} &= (2.3818 \text{ kg/count}) * (.001347 \text{ cm/count}) * (9.81 \text{ N/kg}) / \\ &\quad (100 \text{ cm/m}) = .0003149 \text{ J/count}^2 \end{aligned}$$

The computer software uses these factors for display purposes only. All calculations are done in unitless form so that time is saved. Whenever a display is required, the number to be displayed is converted to the proper units in scratch memory.

Table 4.2
Load Cell Calibration Data

Known Weight (grams)	Unitless Reading
0	1.32
388	1.75
742	2.07
1264	2.59
1839	3.16
2423	3.81
2954	4.30
3343	4.66
3560	4.91
3780	5.15
4000	5.36
4217	5.56
4746	6.10
5341	6.81
5853	7.21
6237	7.74
6499	7.99
7406	8.87
8315	9.65
8767	10.1

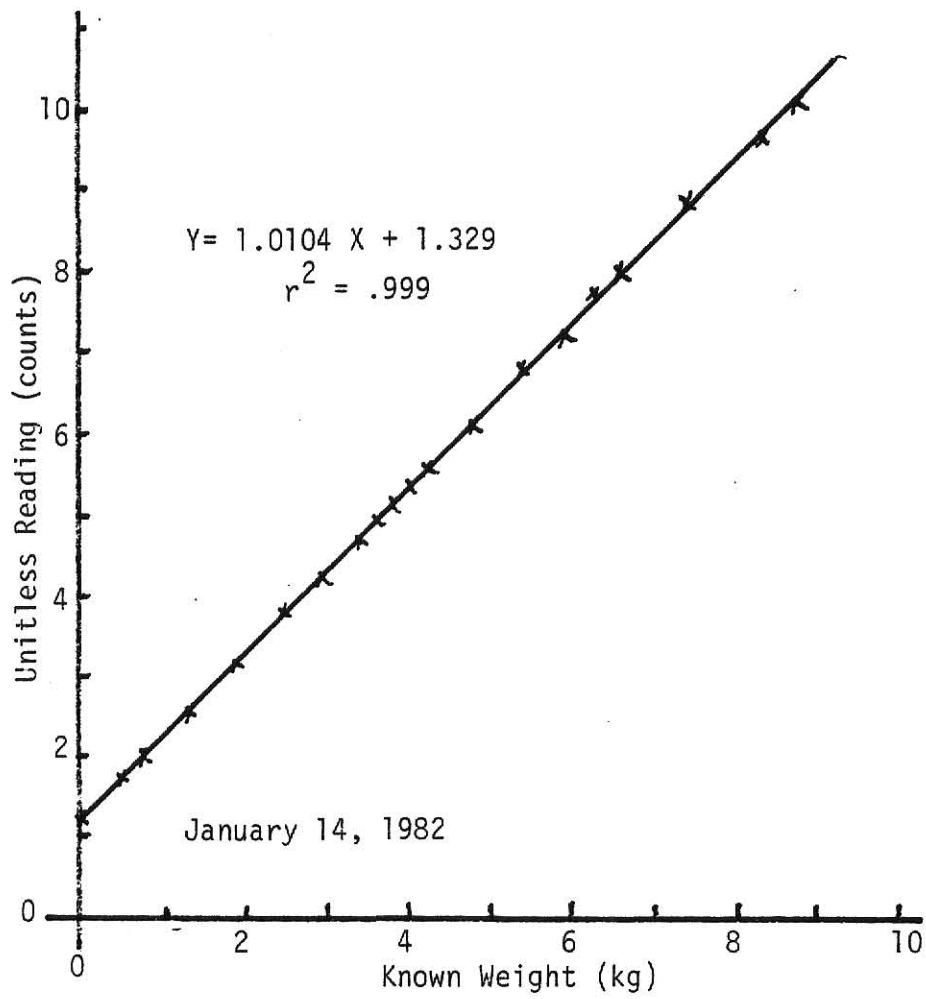


Figure 4.2
Load Cell Calibration Curve

System:

To test the system, the crushing vise was mounted in the Instron machine and crushing tests were run on 30 samples of varying aggregate stability. Ten tests were run on each of three different soils. The first ten tests used a relatively soft soil of the Aquic Haploxerolls subgroup (Hot Lake). The second ten tests used a soil of the Typic Argiudolls subgroup (Reading). The final ten tests used a relatively hard soil from the Typic Calciorthids subgroup (Rillito). Soils of varying aggregate stability were used so that the system was tested over a wide segment of its operating range. All of the samples were crushed at 10 mm/min.

During early testing, it was discovered that the force measuring system on the Instron machine was prone to drift. To minimize this effect, the Instron machine was calibrated frequently during the 30 tests.

The crushing energy was calculated from the Instron chart in two different ways. Each required that a standard sample be taken from the chart paper. A rectangular sample of 5000 chart divisions was taken. Different sensitivities were used for the different groups of ten tests so this standard area represented a different energy for each group. From the calibration of the Instron machine, the standard area represented 0.4905 Joules for the first ten tests, 0.981 Joules for the second ten, and 1.962 for the third ten.

In the first method of finding the crushing energy from the Instron chart, the area enclosed by the force vs. displacement curve is cut out and weighed. This weight is compared with the weight of the standard area. The crushing energy is given by

$$\text{Energy} = \frac{(\text{Weight of Area Under Curve})}{(\text{Weight of Standard Area})} * (\text{Energy Represented by Standard})$$

The charts were weighed using a Mettler AK160 balance. The standard area was weighed each time a crushing plot was weighed to avoid effects of drift in the balance calibration.

In the second method, the number of chart paper divisions enclosed by the force vs. displacement curve are counted. This number is compared with the number of divisions on the standard area. The energy of crushing is given by

$$\text{Energy} = \frac{(\text{No. of Divisions Under Curve})}{(\text{No. of Divisions on Standard})} * (\text{Energy Represented by standard})$$

These methods should give identical results. Table 4.3 lists the data taken during the 30 tests. The SACEM values were read from the SACEM display.

Conclusions:

The SACEM results for the break force correlated with the Instron results to within 0.6%. The SACEM results for crushing energy correlated to within 0.2% with the Instron results found by the counting method and to within 3.5% with the Instron results found by the weighing results.

It was found that the procedure of cutting out and weighing the paper noticeably increased the Instron results found by that method.

These results are shown graphically in Chapter I.

The design criteria were well met. The system measures quickly and accurately and displays its results digitally. It can perform tests independently or in parallel with the Instron machine. It records the break force of the sample, and the entire system can be carried in a suitcase.

INSTRON					ENERGY			SACEM	
RUN NO.	WEIGHT (gm)	STD. WEIGHT (gm)	NO. DIVISIONS	BREAK (kg)	WEIGHING (J)	COUNTING (J)	BREAK (kg)	ENERGY (J)	
1	.1563	1.2347	597	1.41	.062	.059	1.41	.058	
2	.0821	1.2343	314	.70	.033	.031	.73	.031	
3	.1023	1.2360	393	1.55	.041	.039	1.60	.036	
Recalibrated Instron									
4	.1005	1.2364	373	1.48	.040	.037	1.46	.035	
5	.1679	1.2384	647	1.41	.067	.063	1.41	.063	
6	.1777	1.2376	678	3.05	.070	.067	3.08	.068	
7	.1023	1.2400	391	1.83	.040	.039	1.84	.037	
Recalibrated Instron									
8	.0166	1.2398	59	1.00	.007	.006	1.00	.005	
9	.1011	1.2464	371	.88	.040	.036	.89	.035	
10	.2186	1.2455	827	2.84	.086	.081	2.81	.081	
Recalibrated Instron									
11	.2475	1.2458	965	2.80	.195	.189	2.82	.187	
12	.0812	1.2457	303	1.60	.064	.059	1.69	.064	
Recalibrated Instron									
13	.1335	1.2465	509	1.08	.105	.100	1.11	.099	
14	.4190	1.2442	1635	5.52	.330	.321	5.66	.317	
15	.1919	1.2417	739	4.25	.152	.145	4.26	.148	
16	.0406	1.2422	160	.61	.032	.031	.66	.032	
17	.3375	1.2400	1321	5.80	.267	.259	5.83	.262	
18	.0978	1.2401	366	2.58	.077	.072	2.68	.075	
Recalibrated Instron									
19	.3627	1.2390	1417	4.76	.287	.278	4.68	.273	
20	.1237	1.2443	464	3.05	.098	.091	3.24	.096	
Recalibrated Instron									
21	.1520	1.2441	587	4.7	.240	.230	4.85	.227	
22	.6783	1.2442	2660	12.4	1.070	1.044	12.4	1.036	
23	.0962	1.2443	368	7.8	.152	.144	7.70	.133	
24	.3180	1.2447	1230	6.6	.501	.483	6.86	.501	
Recalibrated Instron									
25	.3217	1.2445	1241	7.5	.507	.487	7.40	.487	
26	.3152	1.2446	1219	9.3	.497	.478	9.25	.476	
27	.0900	1.2442	343	4.7	.142	.135	4.56	.126	
28	.0219	1.2390	73	4.6	.035	.029	4.73	.029	
29	.1268	1.2363	474	4.2	.201	.186	4.23	.191	
30	.0939	1.2361	365	5.4	.149	.143	5.59	.146	

Table 4.3

SACEM AND Instron Comparison Data

LITERATURE CITED

SYM-1 Reference Manual, Synertek Systems Corporation, 1981.

SY6500/MCS6500 Microcomputer Family Programming Manual, MOS Technology, Inc., 1975.

Synertek 6500 BASIC Reference Manual, Synertek Systems, 1981.

"3606 Digitally Controlled Programmable Gain Instrumentation Amplifier", PDS-388, Burr-Brown Research Corporation, 1978. Data sheet for amplifier integrated circuit.

"SDM856 Hybrid Data Acquisition System", PDS-402, Burr-Brown Research Corporation, 1978. Data sheet for data acquisition integrated circuit.

"Displacement Transducers, Series 7DCDT & 24DCDT", Hewlett-Packard, 1977. Data sheet for displacement transducer.

"Calibration Certificate, Installation Information", Interface, Inc., 1980. Data sheet for load cell.

APPENDIX A

DETAILED HARDWARE EXPLANATION

Crushing Vise:

Detailed views of the crushing vise are shown in Figure A.1.

The adapter shaft is detailed in Figure A.2.

Computer Module:

It is assumed that the reader has access to the SYM-1 Reference Manual and the SYM BASIC Programming Manual.

Memory locations:

A memory map for the SYM-1 is shown in Figure A.3. Several changes were made to the SYM-1 to achieve this configuration. The BASIC interpreter resides in a single Read Only Memory in U21. The jumper changes necessary to decode this socket as an 8K ROM are detailed in the SYM BASIC Programming Manual.

The soil testing software resides in a 2716 Eraseable Programmable Read Only Memory in U22 and at address E000. The following jumper changes were made to achieve this:

1. Jumper L-12 removed
2. Jumper L-15 placed

The location E000 was chosen to allow the 8K BASIC at Location C000.

In order to have the system power on to the soil testing software, the reset vector was changed. The following were required to have the system

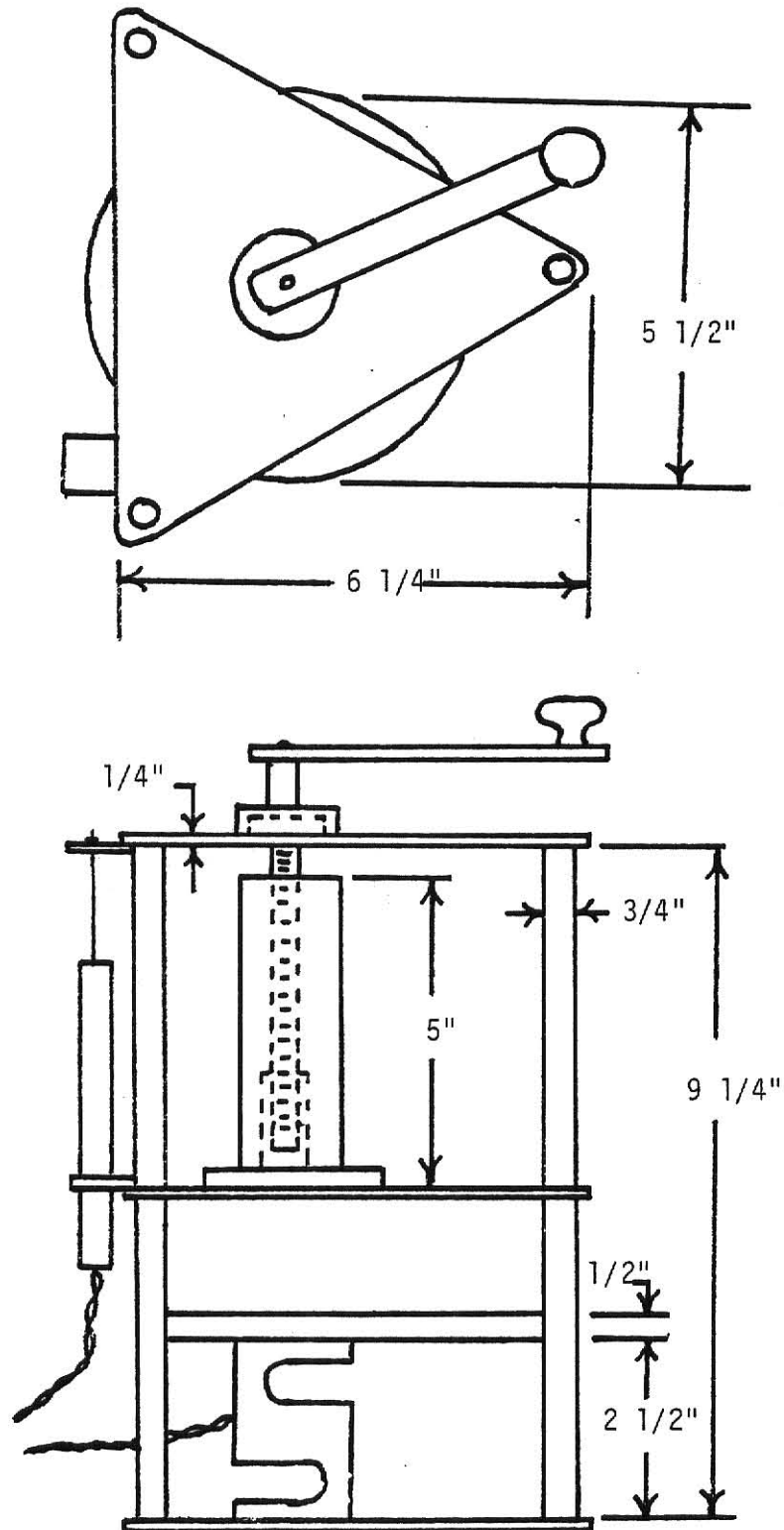


Figure A.1
Crushing Vise Detail

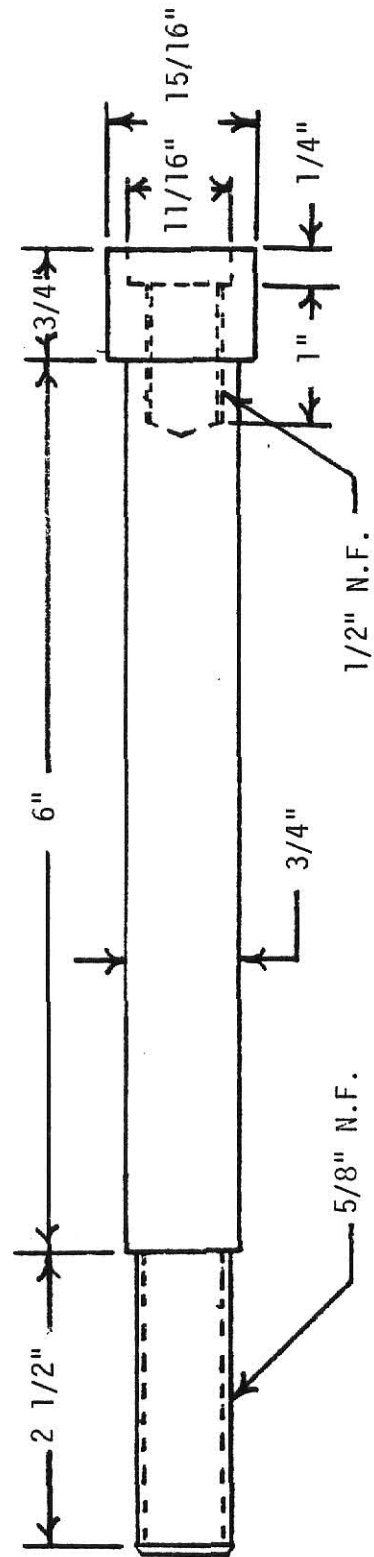


Figure A.2
Instron Adapter Shaft

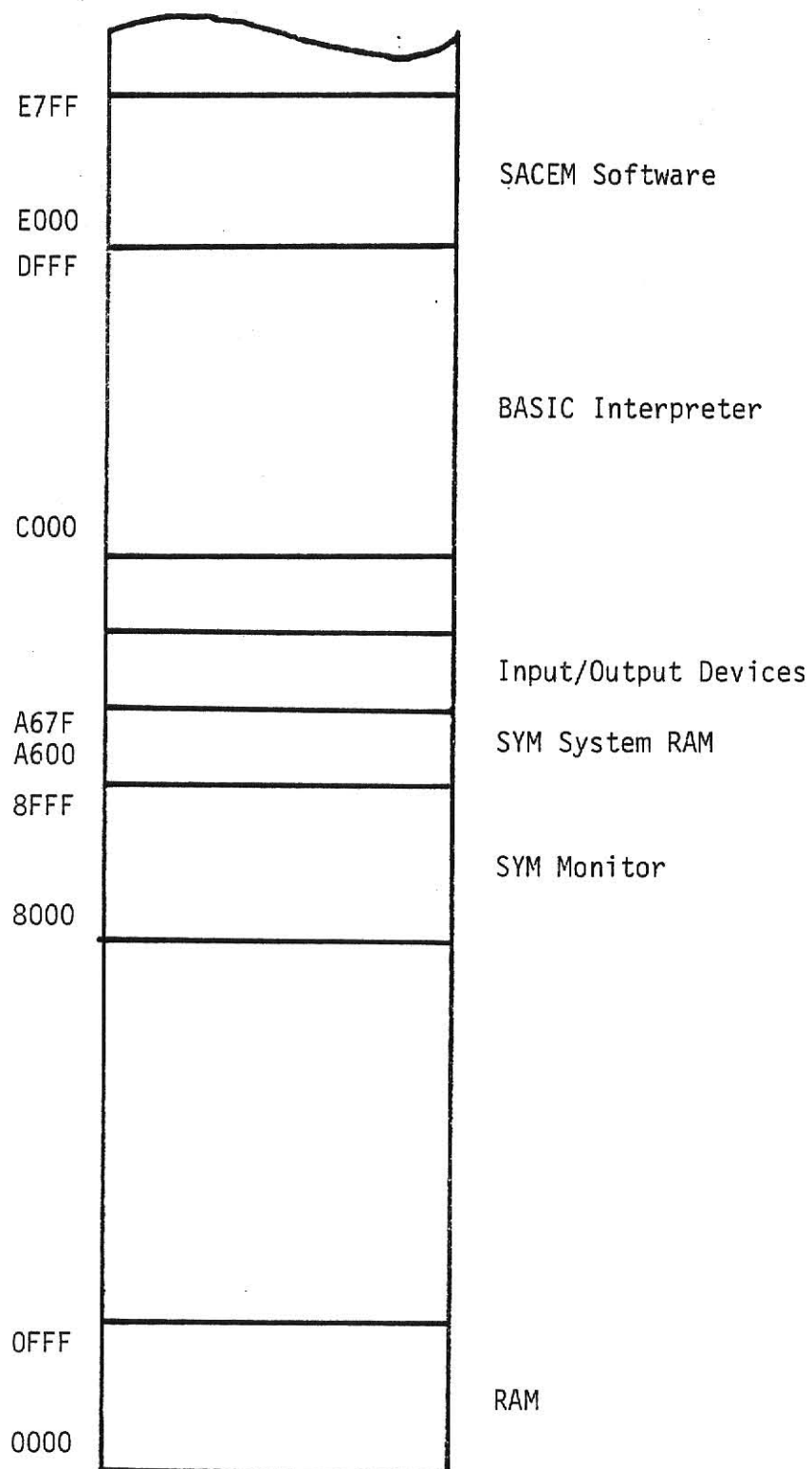


Figure A.3
SYM Memory Map

power on using the reset vector stored at the top of U22:

1. Jumper N-19 moved to N-20
2. Jumper R-20 moved to R-19

The data acquisition system and instrument amplifier appear at memory locations A800, A801, AC00, and A80C. The multiplexer channel and amplifier gain are latched into their respective devices by a transition on SYM control line 2CA2. The analog to digital conversion is triggered by dropping SYM control line 2CB2. A summary of the ports used and their addresses and functions is given in Figure A.4. The specific pin connections required to provide this configuration are given below.

Pin Connections:

The connections for the SDM856 are given first. The connections for involving the power supply are diagrammed in Figure A.5 and the connections involving data, address, and control signals are diagrammed in Figure A.6.

SDM856 Pin Connections

Pin No	Pin Function	Connection
1	Not used	No connection
2	Multiplexer high output.	Connects to pin 29 on 3606
3	Not used	No connection
4	Multiplexer input, high of channel 7	Connects to high output of displacement tdc.
5	Multiplexer input, high of channel 6	Connects to high output of load cell
6-11	Multiplexer inputs, highs of channels 5-0 respectively	No connections
12	Multiplexer #2 enable	Connect to pin 13 for differential operation





<u>SYM Port Name</u>	<u>Function</u>	<u>Address</u>
2PA	 Mux. Amp. Channel Gain	A801
2PB	 Low 8 bits of A/D Result	A800
3PB	 High 4 bits of Result	AC00
2PA Control Register	 2CB2 2CA2 Controls	A80C

Figure A.4
Summary of SYM Port Configuration

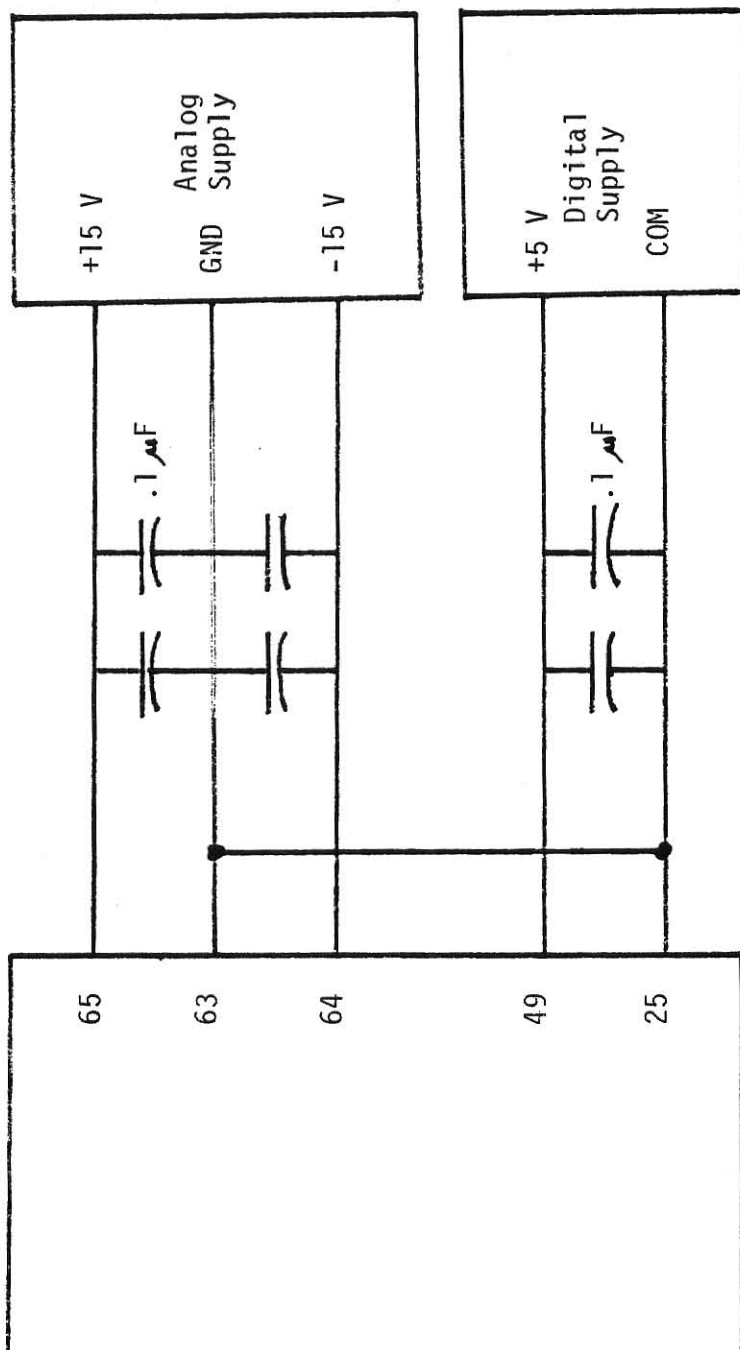


Figure A.5

SDM856 Power Supply Connections

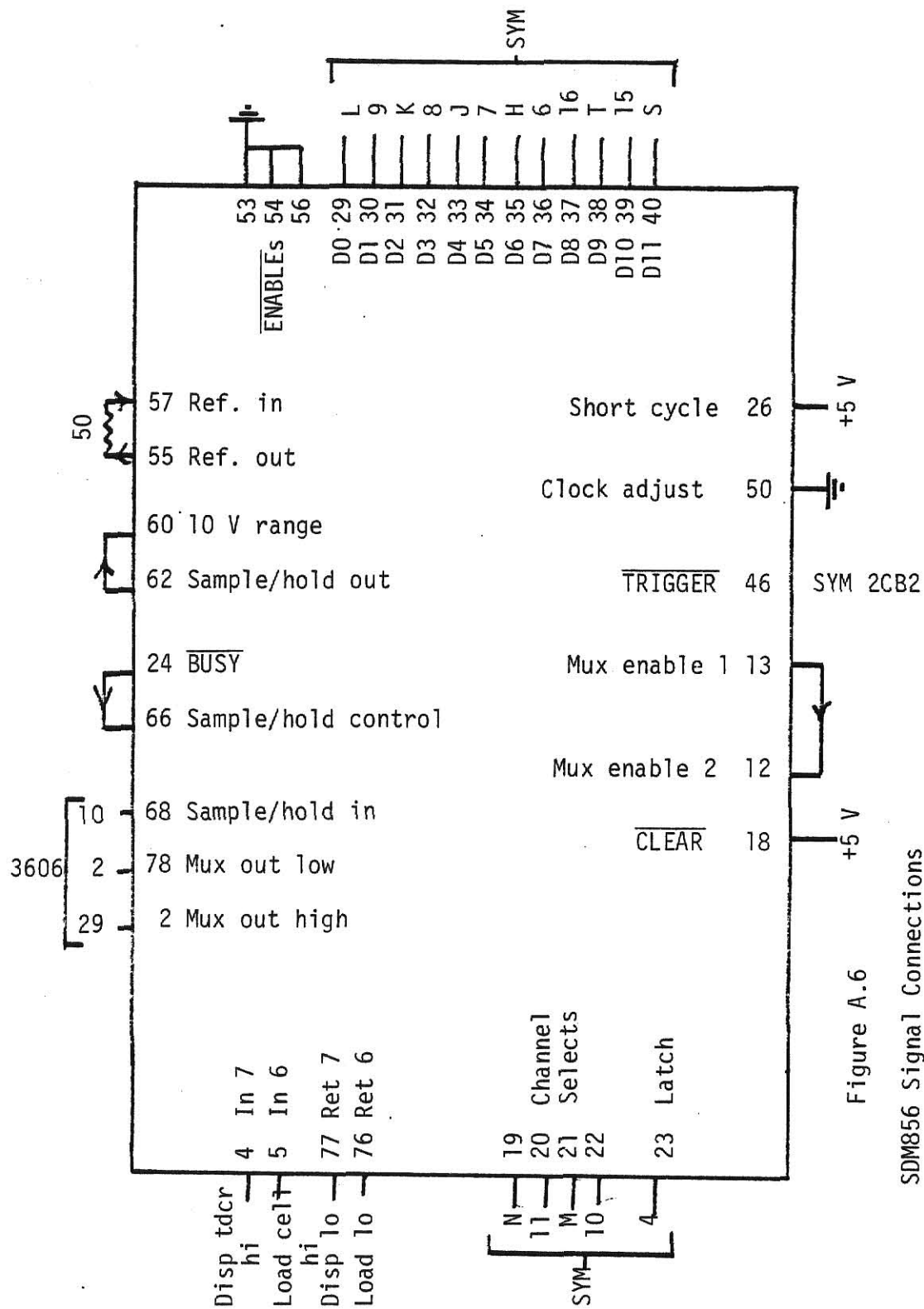


Figure A.6

SDM856 Signal Connections

13	Multiplexer #1 enable	Connect to pin 12
14	Single/differential	No connection
15	A2 out	No connection
16	A1 out	No connection
17	A0 out	No connection
18	$\overline{\text{CLEAR}}$ input	Connect to +5 V.
19-22	Multiplexer channel selects	These come from the upper 4 bits of port 2PA. Connect to SYM application connector respectively pins N,11,M,10.
23	Channel select latch line	Connect to SYM application connector pin 4
24	$\overline{\text{BUSY}}$ output	Connect to pin 66
25	Digital common	Connect to pin 63 and to power supply ground
26	Short cycle input	Connect to +5 V.
27	10 bit resolution	No connection
28	8 bit resolution	No connection
29-36	Low 8 bits of digital output	Connect to SYM application connector respectively pins L,9,K,8,J,7,H,6
37-40	Upper 4 bits of digital output	Connect to SYM application connector respectively pins 16,T,15,S
41	$\overline{\text{D11 ENABLE}}$	No connection
42	$\overline{\text{BUSY ENABLE}}$	No connection
43	$\overline{\text{BUSY}}$ output	No connection
44	$\overline{\text{D11}}$ output	No connection
45	Delay out	No connection
46	$\overline{\text{TRIGGER}}$ input	Connect to SYM application connector pin 5

47	Delay adjust	No connection
48	<u>STROBE</u>	No connection
49	5 volt input	Connect to +5 volt power supply and across capacitance to ground
50	Clock adjust	Connect to ground
51	Clock out	No connection
52	Serial out	No connection
53,54	Output <u>ENABLEs</u>	Connect to ground
55	Reference out	Connect to pin 57 through 50 ohm resistor
56	Output <u>ENABLE</u>	Connect to ground
57	Reference in	Connect to pin 55 through 50 ohm resistor
58	20 V range	No connection
59	Bipolar offset	No connection
60	A/D input resistor	Connect to pin 62
61	-6.4 V ref. out	No connection
62	Sample/hold out	Connect to pin 60
63	Analog common	Connect to pin 25 and to ground
64	-15 Volt input	Connect to -15 Volt power supply and across capacitance to ground
65	+15 Volt input	Connect to +15 Volt power supply and across capacitance to ground
66	Sample/hold control	Connect to pin 24
67	Sample/hold offset adjust	No connection
68	Sample/hold input	Connect to pin 10 of 3606
69	Not used	No connection

70-75	Multiplexer inputs, lows of channels 0 through 5	No connections
76	Multiplexer input, low of channel 6	Connects to low output of load cell
77	Multiplexer input, low of channel 7	Connects to low output of displacement tdc.
78	Multiplexer low output	Connect to pin 2 of 3606
79	Not used	No connection
80	Not used	No connection

The pin connections for the 3606 instrument amplifier are given next. The connections involving the power supply are diagrammed in Figure A.7 and the connections involving data and control signals are diagrammed in Figure A.8.

3606 Pin Connections

Pin no.	Pin Function	Connection
1	-15 V supply	Connect to power supply and across capacitance to ground
2	Low input	Connect to pin 78 of SDM856
3	Input stage output	Connect to pin 8
4	Offset trim	No connection
5	Summing junction	Connect to pin 10 across .0033 μ F to provide output filtering
6	Offset trim	No connection
7	Filter pin	No connection
8	Output stage input	Connect to pin 3
9	Output reference	Connect to ground
10	Output	Connect to pin 5 through .0033 μ F and directly to pins 11, 13, and 13. Connect to ground through 1 Megohm. Also connect to pin 68 on SDM856

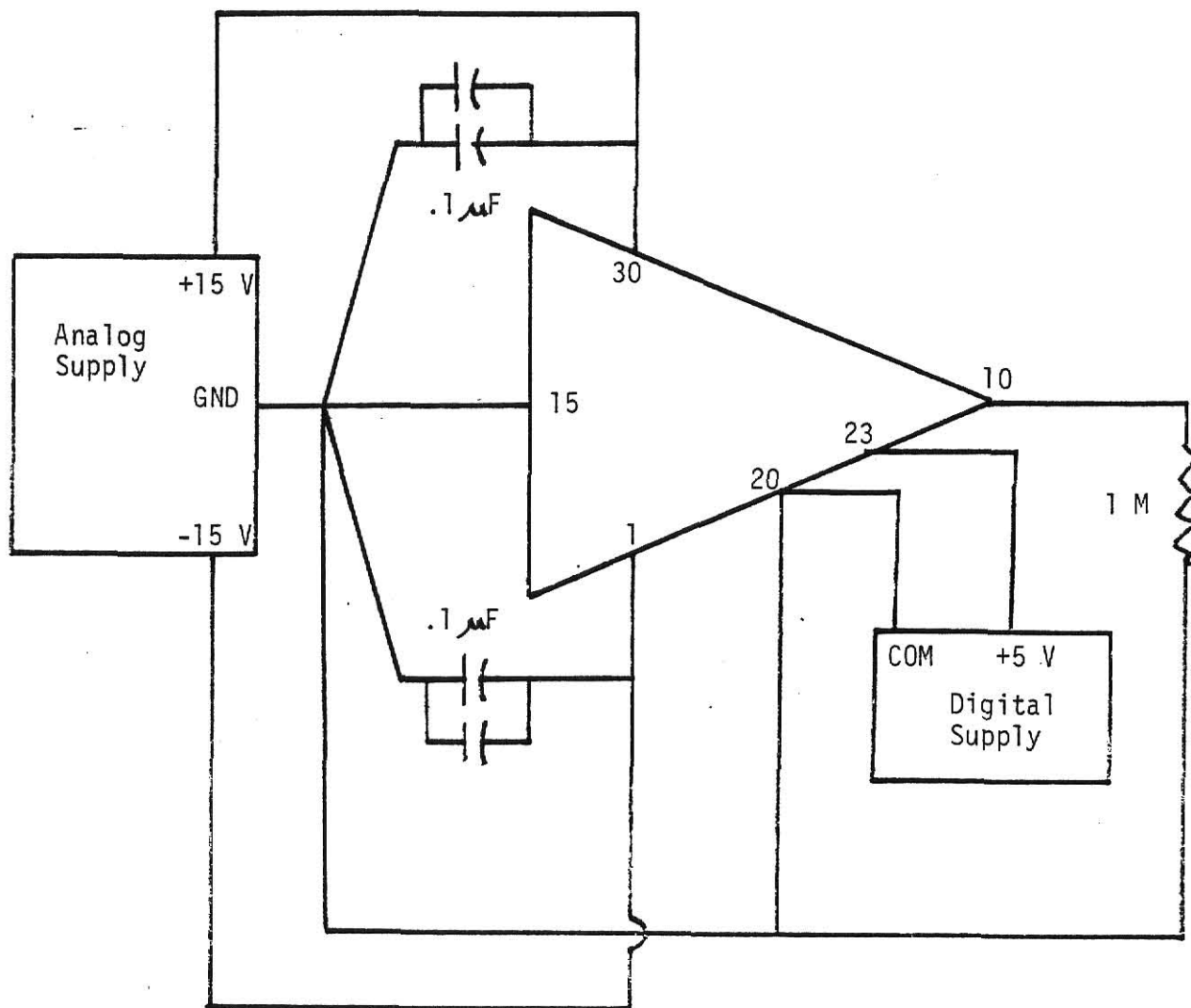


Figure A.7

3606 Power Supply Connections

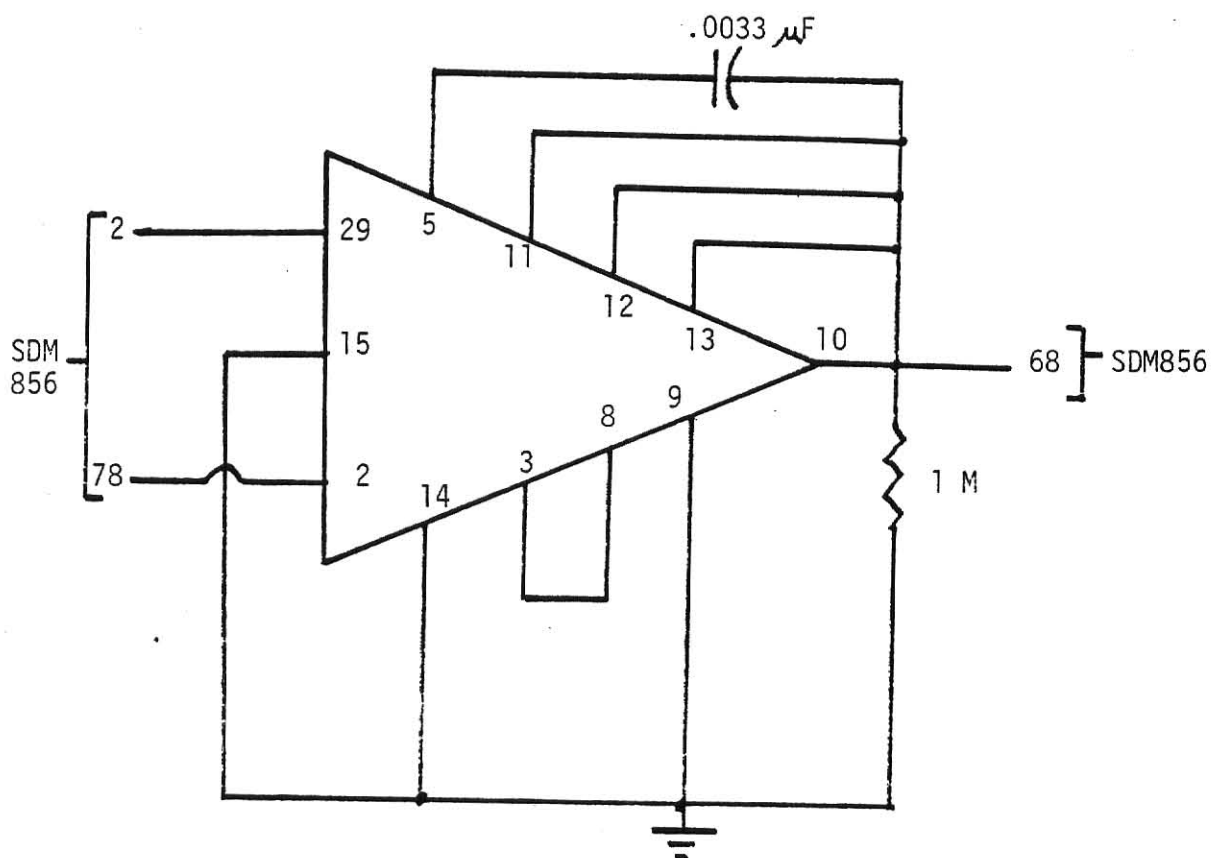


Figure A.8

3606 Signal Connections

11-13	Feedback	Connect each to pin 10
14	Output reference	Connect to ground
15	Analog common	Connect to ground
16	Not used	No connection
17,18	Digital inputs	Connect to SYM application connector respectively pins D,3
19	Latch	Connect to SYM application connector pin 4
20	Digital common	Connect to ground
21,22	Digital inputs	Connect to SYM application connector respectively pins C,12
23	+5 V supply	Connect to power supply
24,25	Not used	No connections
26,27	External gains	No connections
28	Input common mode	No connection
29	High input	Connect to pin 2 on SDM856
30	+15 V supply	Connect to power supply and across capacitance to ground
31,32	Optional input stage offset null	No connections

The pin connections on the SYM-1 are given next. The power supply connector is wired as on page 3-4 of the SYM Reference Manual. V_p is +15 volts and V_n is -15 volts from the power supply.

SYM Application Connector Connections

Pin No.	Pin Function	Connection
1	Ground	Connects directly or indirectly to all grounds on data acquisition chips
2	-15 V (V_n)	Connects to -15V pins on data acquisition chips

3	2PA1	Connects to pin 18 of 3606 as part of gain select
4	2CA2	Connects to pin 23 on SDM856 and to pin 19 on 3606
5	2CB2	Connects to pin 46 on SDM856
6-9	2PB7,5,3,1	Connects respectively to pins 36,34, 32,30 on SDM856
10-11	2PA7,5	Connect respectively to pins 22 and 20 on the SDM856
12	2PA3	Connect to pin 22 of 3606
13	RES	No connection
14	3CB1	No connection
15-16	3PB2,0	Connect respectively to pins 39 and 37 of SDM856
17-20	3PA6,3,4,5	No connections
21-22	3PB5,7	No connections
A	+5 V	Connects directly or indirectly to all pins on data acquisition chips requiring +5 volts
B	+15 V (V_p)	Connects to +15 V pins on data acquisition chips
C-D	2PA2,0	Connect respectively to pins 21 and 17 of 3606
E	2CA1	No connection
F	2CB1	No connection
H-L	2PB6,4,2,0	Connect respectively to pins 35,33,31 and 29 of SDM856
M-N	2PA7,5	Connect to pins 21 and 19 respectively of SDM856
P	3CA1	No connection
R	SCOPE	No connection
S-T	3PB3,1	Connect to pins 40 and 38 respectively of SDM856

U-X	3PA7,0,1,2	No connections
Y-Z	3PB4,6	No connections

All connections to the load cell and displacement transducer are made through a single connector brought out from the data acquisition chip and the power supply. Those connections are then run to another connector in the top panel of the computer module. This allows the module to be completely disassembled. The arrangement of the first connector as viewed from the computer is shown in Figure A.9. The connections are described below.

Connections for Power Supply and Transducers

Pin No.	Pin Function	Connection
1	+15 volts	Connects to power supply +15 volts
2	Not used	No connection
3	Multiplexer input, high of channel 6	Connects to pin 5 of SDM856
4	Multiplexer input, high of channel 7	Connects to pin 4 of SDM856
5	+5 volts	Connects to power supply
6	Not used	No connection
7	Not used	No connection
8	Not used	No connection
9	Ground	Connects to power supply ground
10	Not used	No connection
11	Multiplexer input, low of channel 6	Connects to pin 76 of SDM856
12	Multiplexer input, low of channel 7	Connects to pin 77 of SDM856

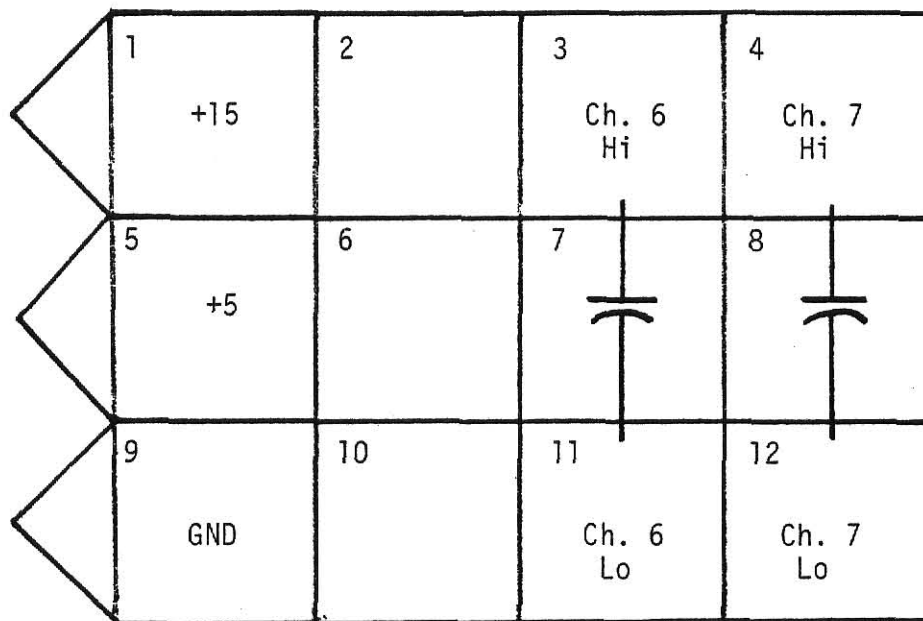


Figure A.9

Power Supply and Input Connector
(Viewed from Computer)

Also note that 10 microfarads of capacitance is connected between pins 3 and 11 and between pins 4 and 12. This is to provide some filtering of the input signals.

The arrangement of the front panel connector on the computer module is shown in Figure A.10. The connections on each pin are detailed below.

Front Panel Pin Connections

Pin No.	Function	Connection
1	+5 volts excitation for displacement transducer	Connects to pin 5 of power supply and input connector
2	High output of displacement transducer	Connects to pin 4 of power supply and input connector
3	+15 volts excitation for load cell	Connects to pin 1 of power supply and input connector
4	Load cell high output	Connects to pin 3 of power supply and input connector
5	Ground	Connects to pin 9 of power supply and input connector and to pins 6 and 7 of this connector
6	Low output of displacement transducer	Connects to pin 12 of power supply and input connector and to ground
7	Ground	Connects to pin 5
8	Low output of load cell	Connects to pin 11 of power supply and input connector

The eight lines from the load cell and displacement transducer are brought into a single connector which mates with the computer module front panel connector. These are diagrammed in Figure A.11. Each line is marked with the corresponding pin on the front panel connector that it mates to.

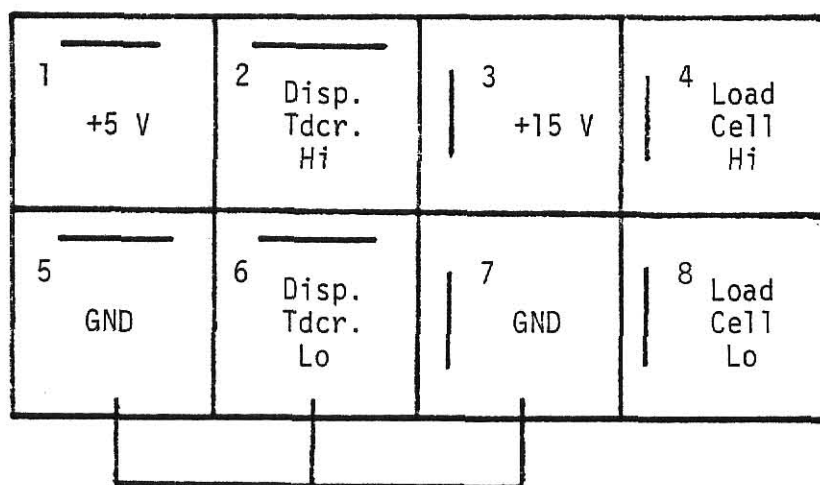


Figure A.10

Computer Module Front Panel Connector
(Viewed from Top of Computer Module)

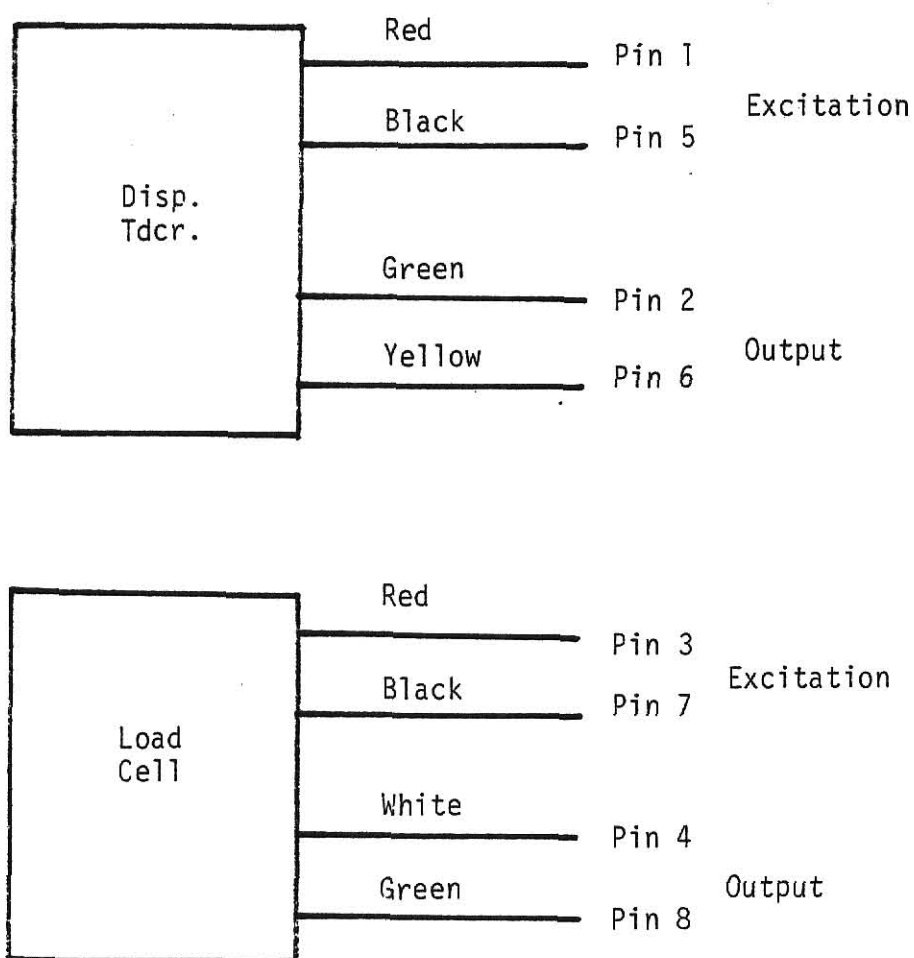


Figure A.11

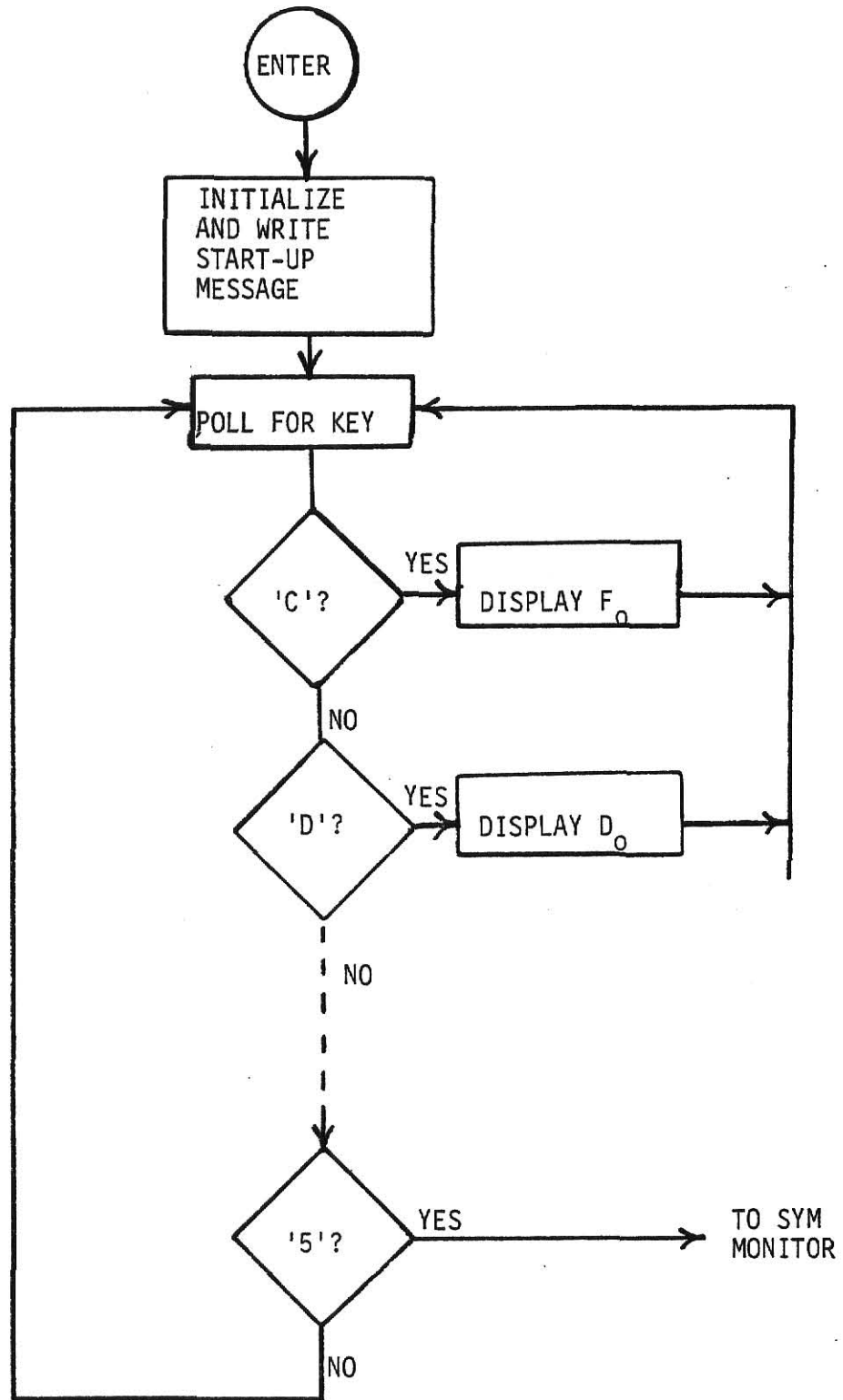
Transducer and Load Cell Connections

APPENDIX B

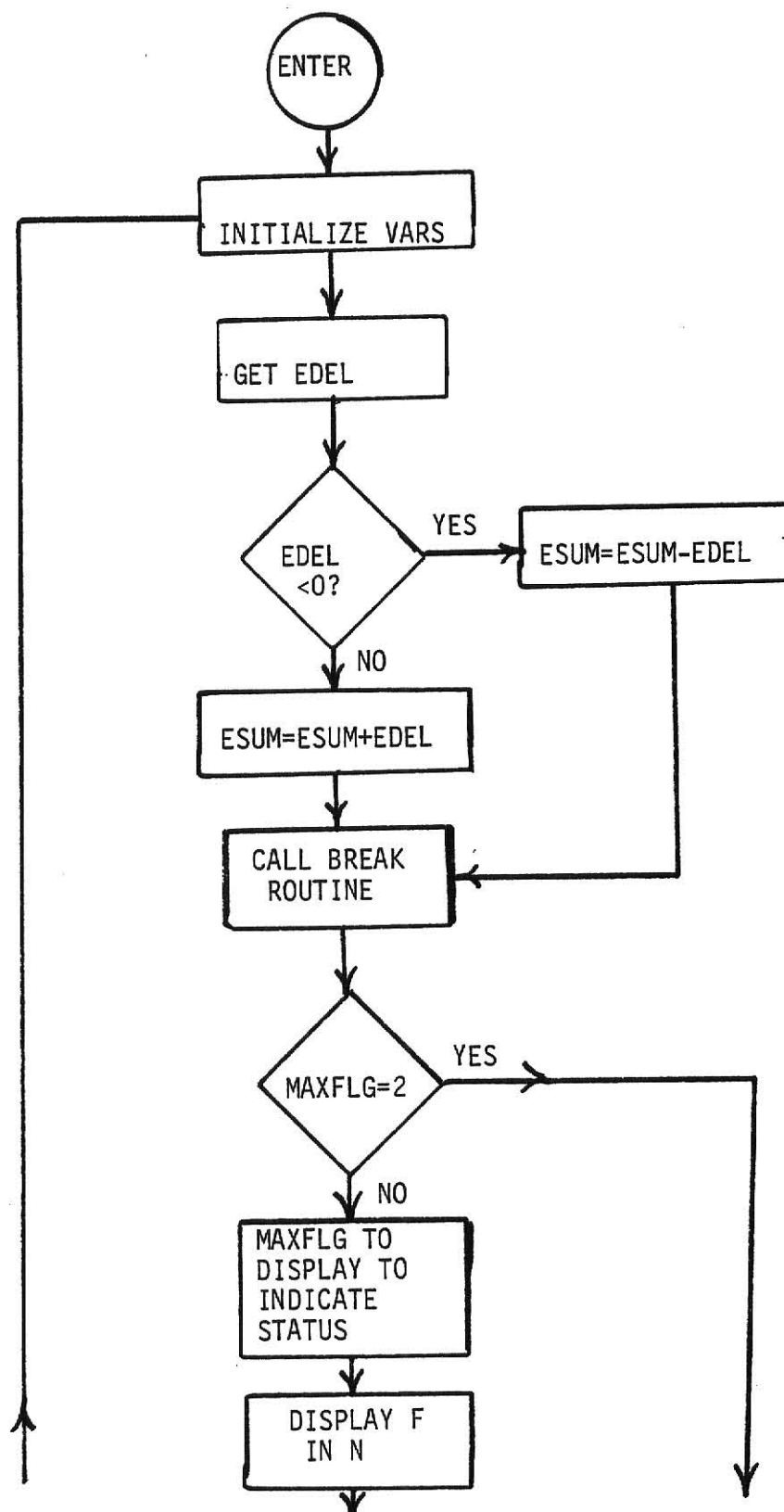
SOFTWARE FLOW DIAGRAMS

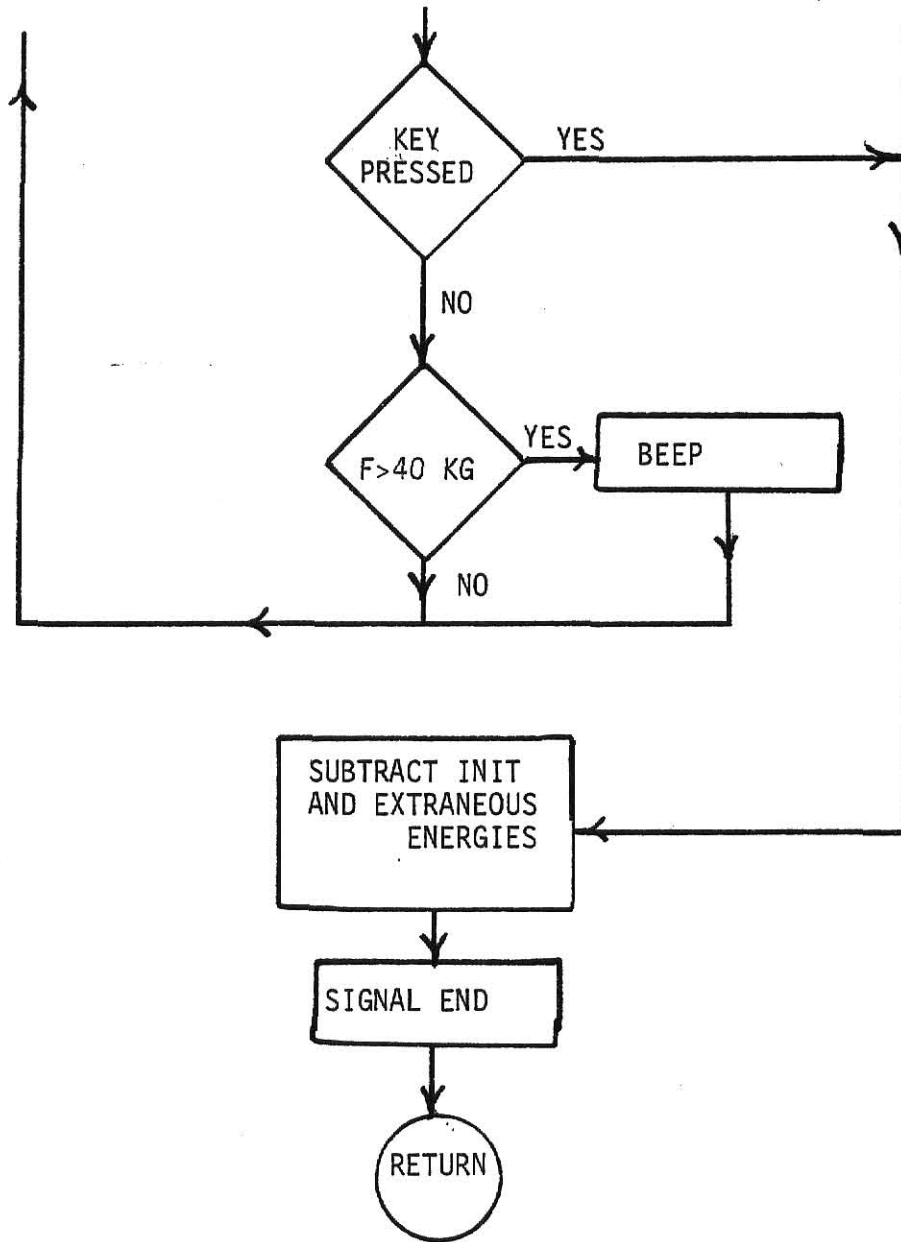
Following is a collection of flow diagrams for the major routines in the SACEM software. Complete assembly language listings of all the software can be found in Appendix C. Each diagram is headed by the name of the routine described. These names match those in the descriptions of chapter 3 and the assembly language labels at the beginning of each routine.

MONITOR

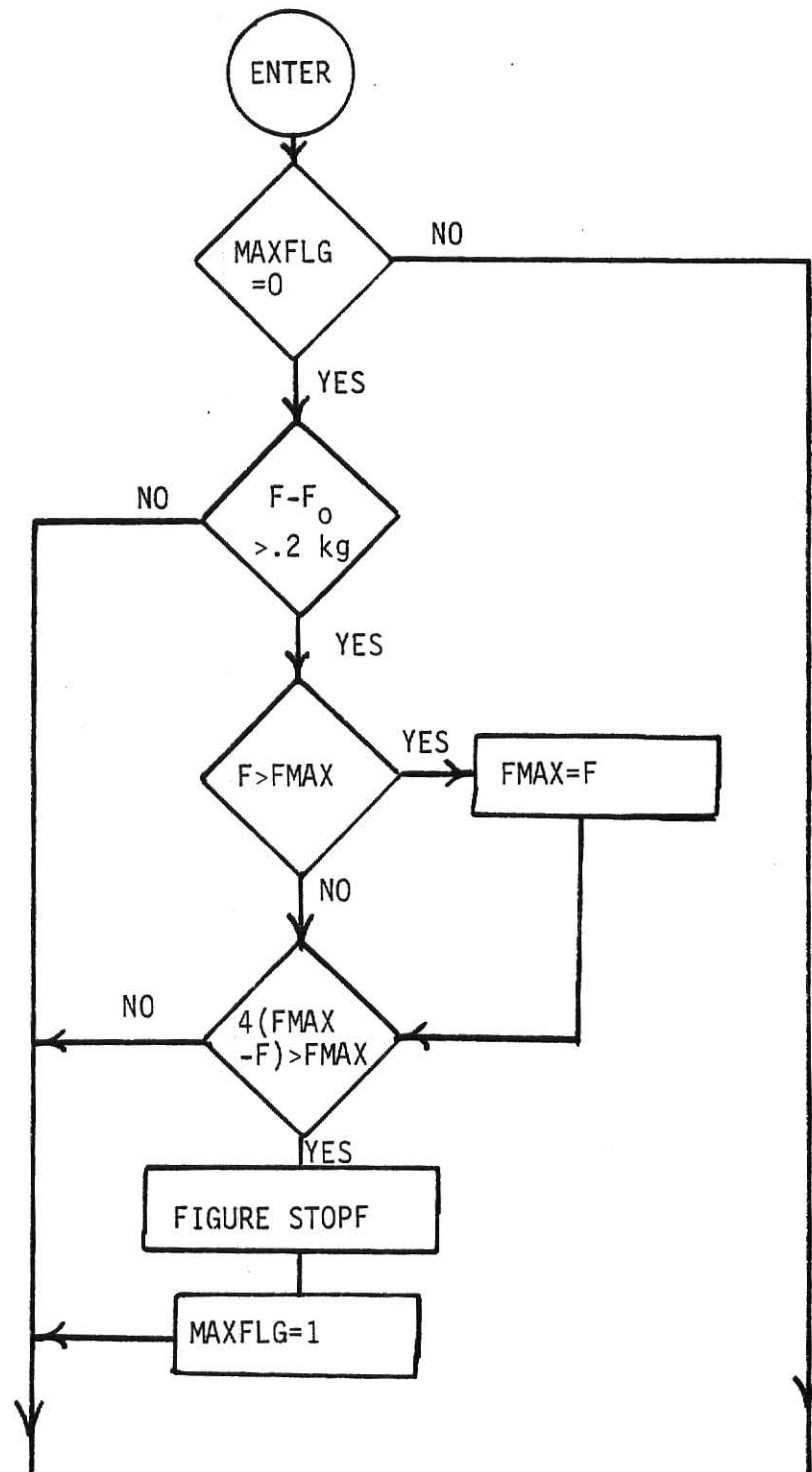


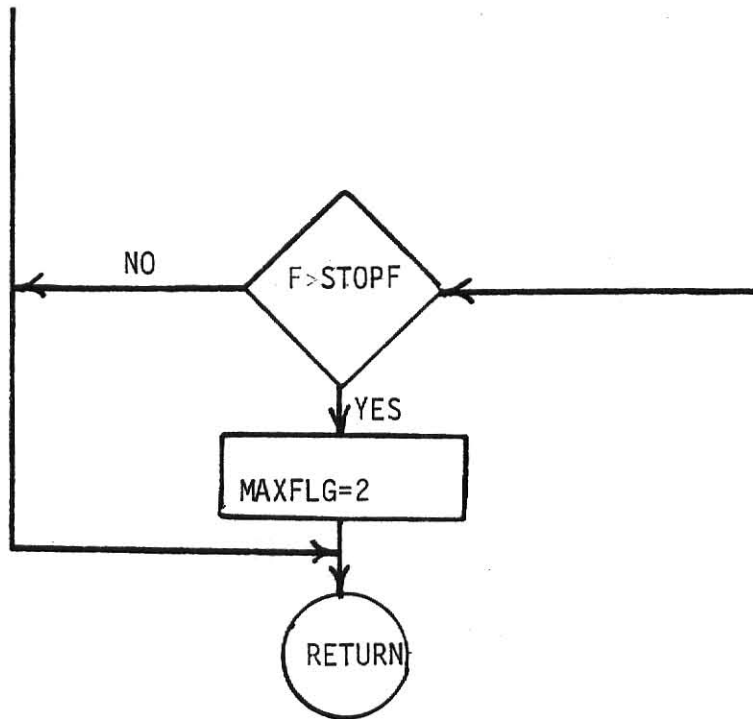
TEST



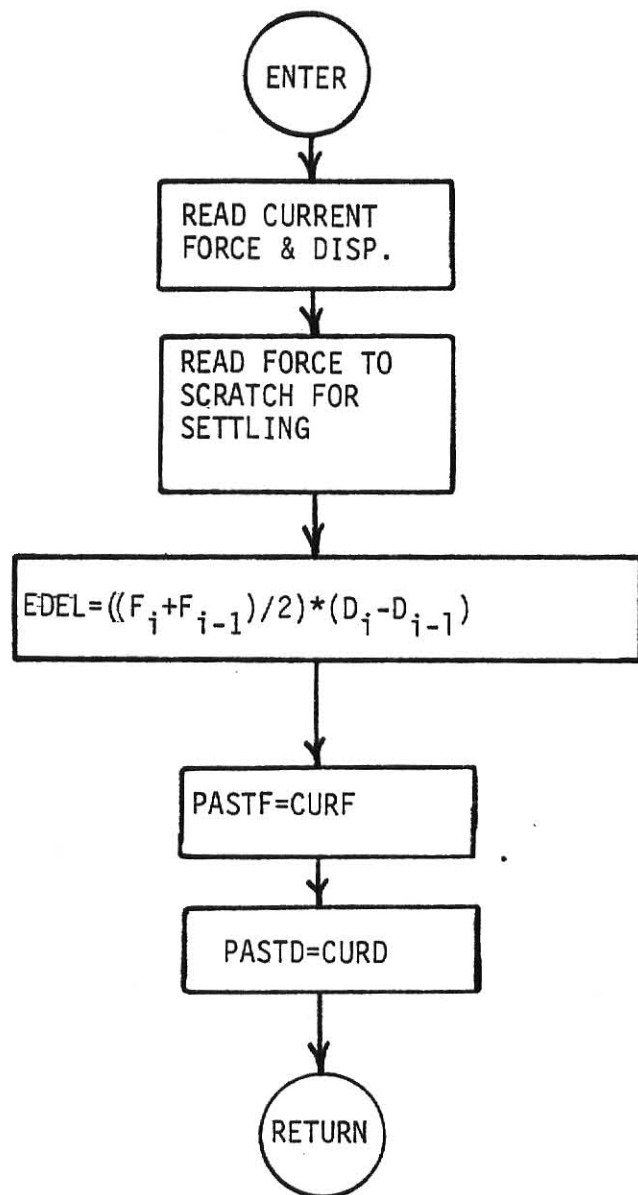


BREAK

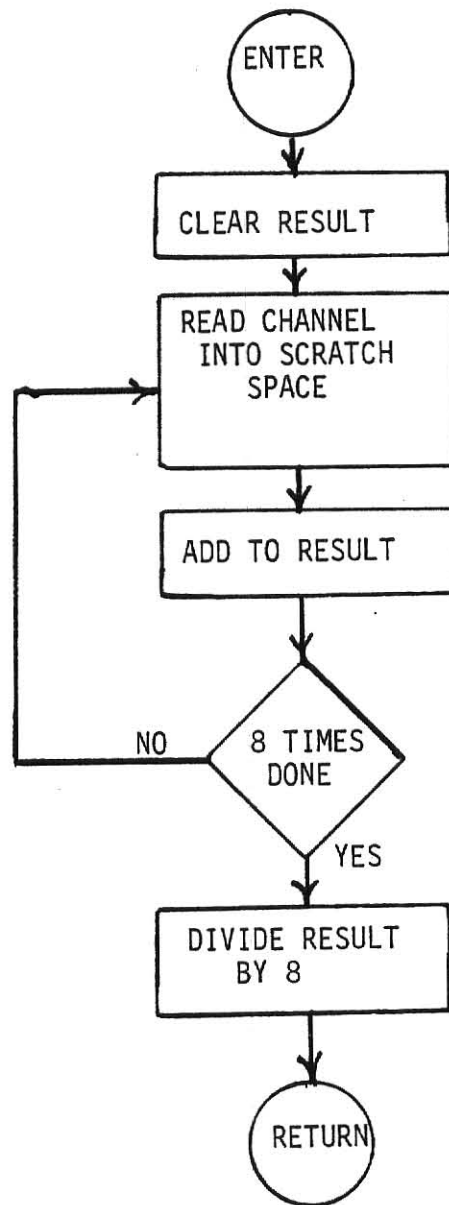




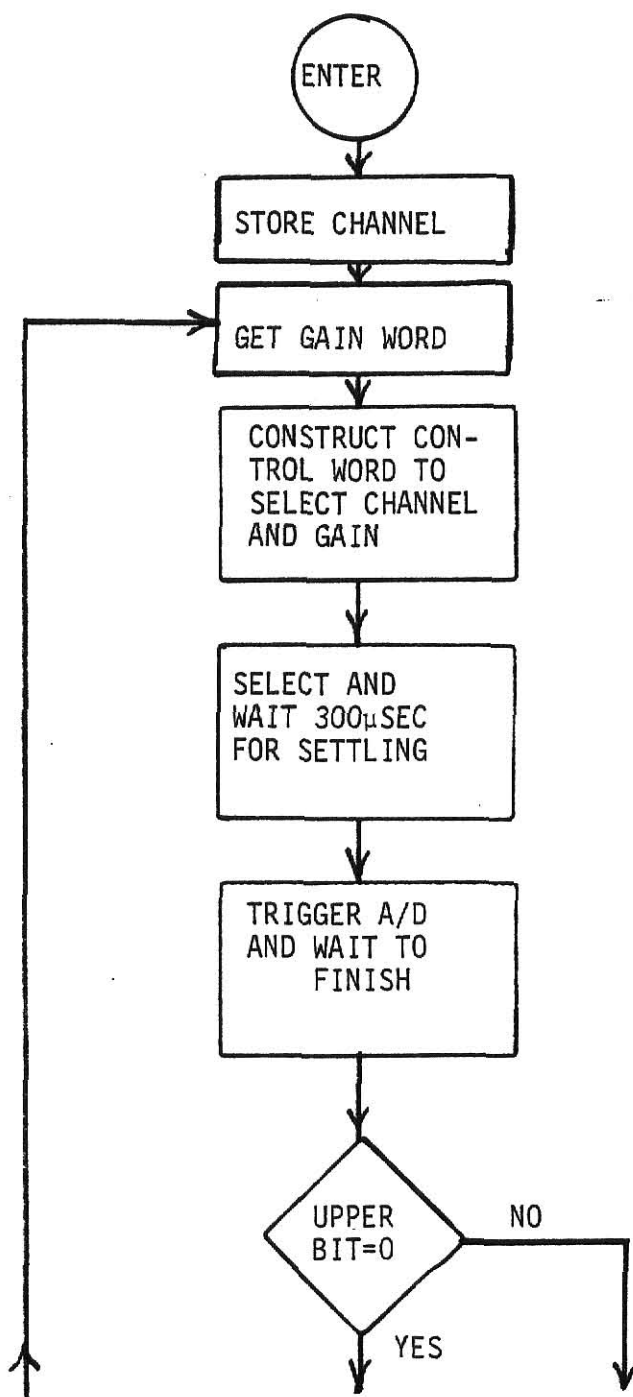
DELTA E

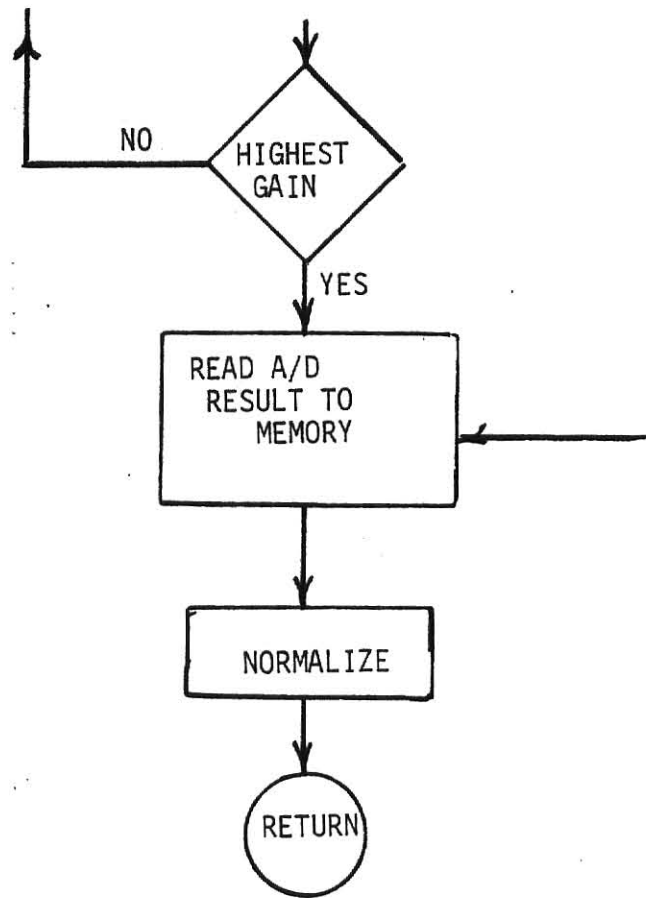


BASE

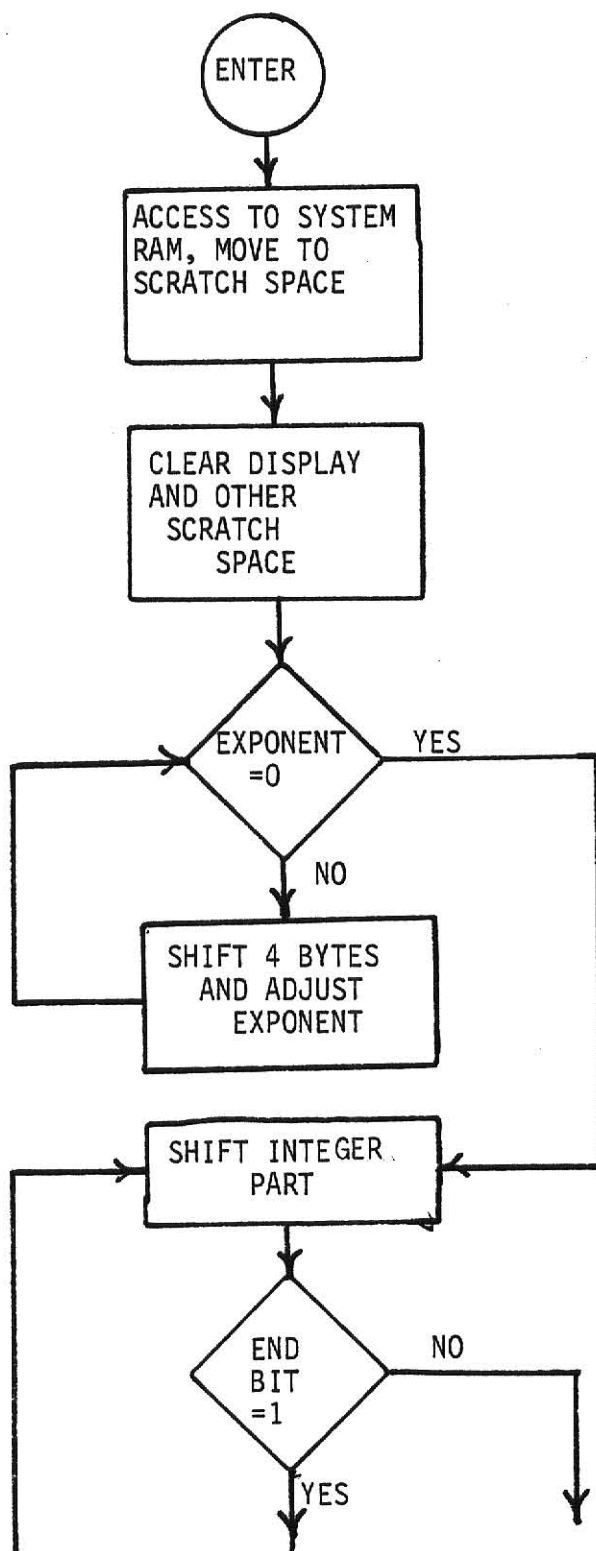


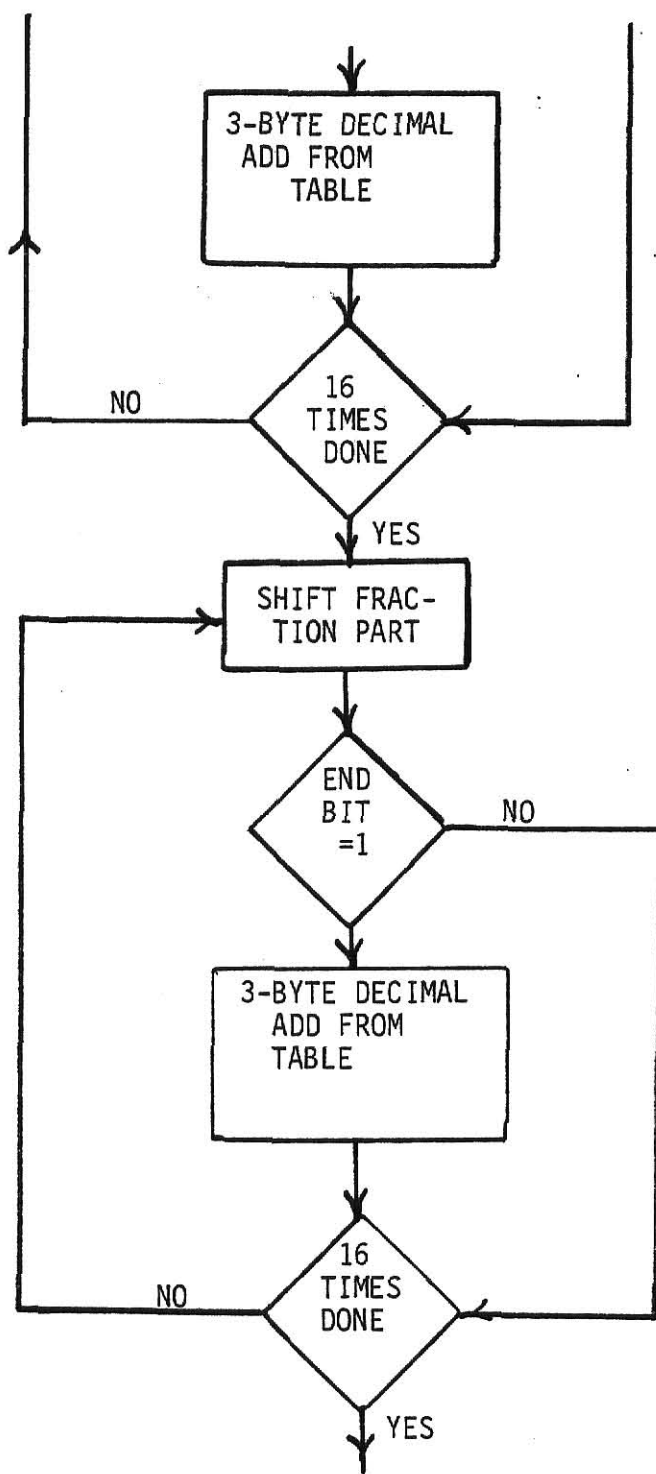
READ

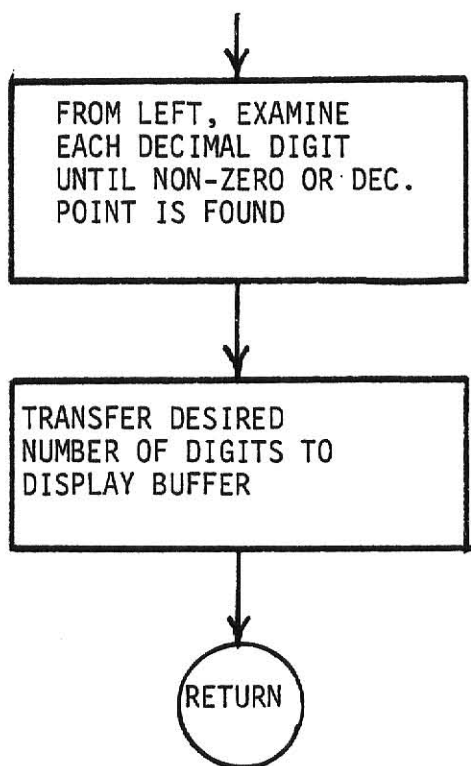




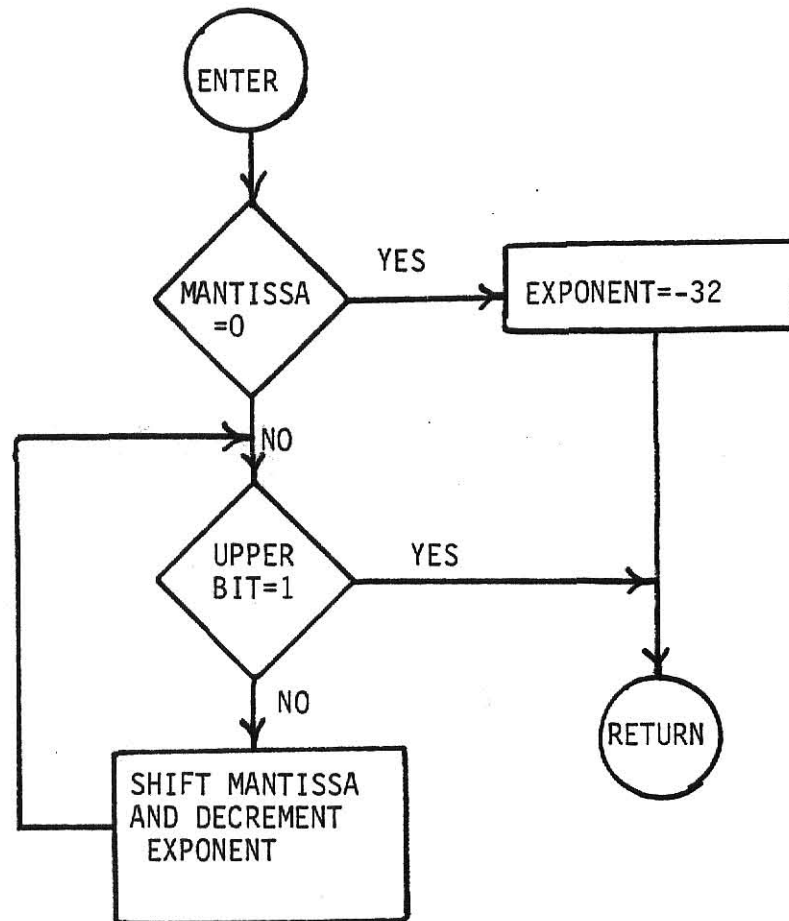
CONV:



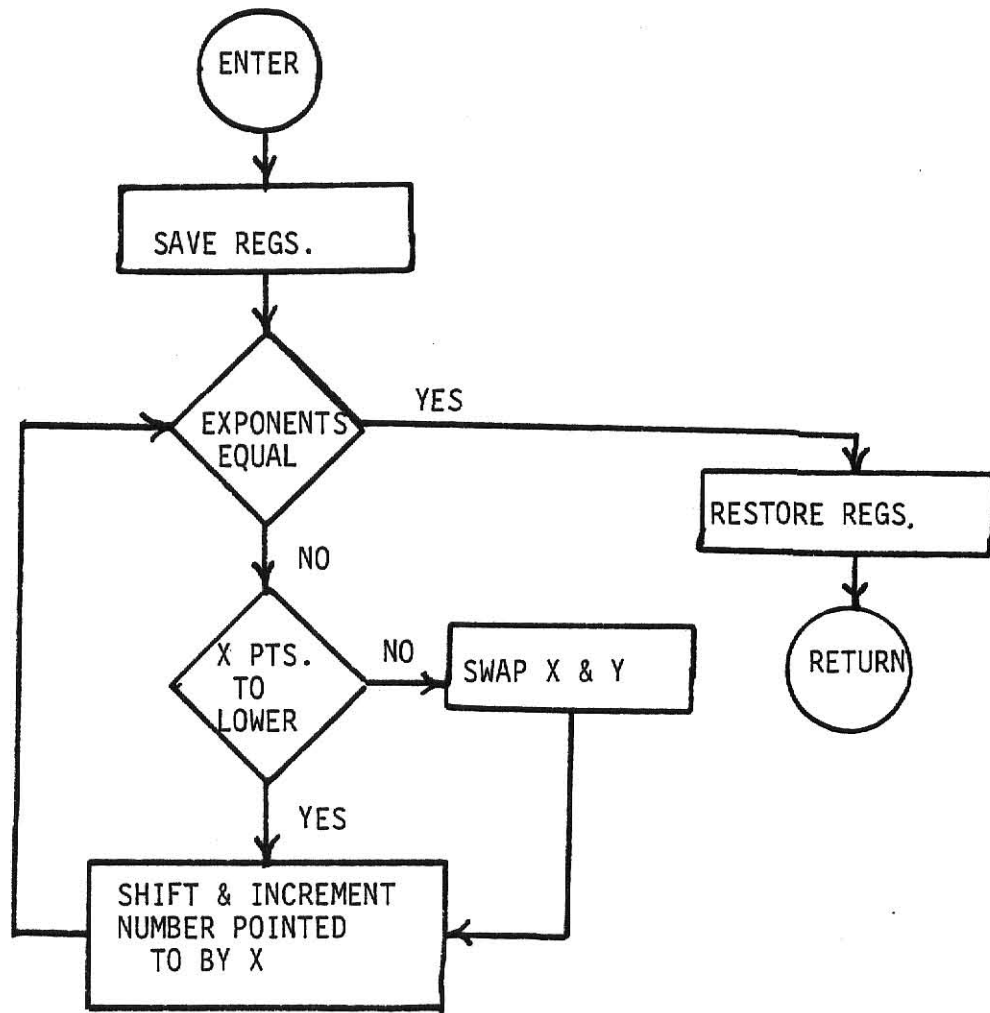




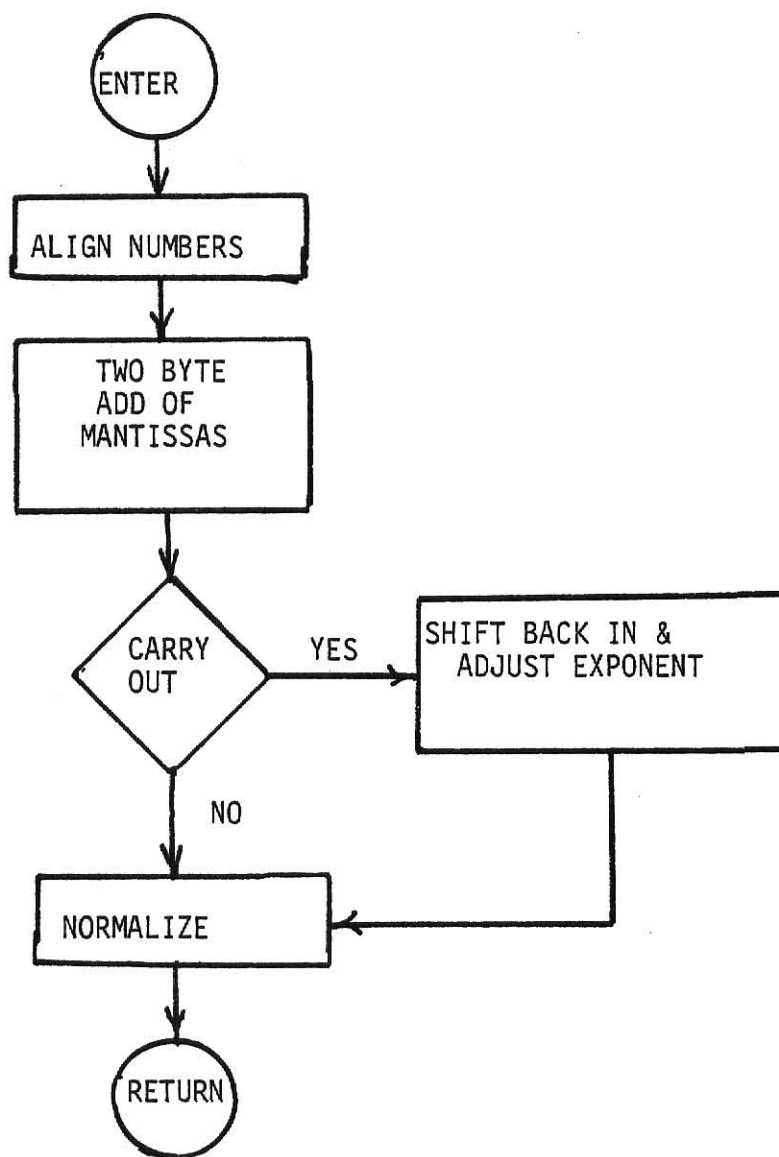
NORM



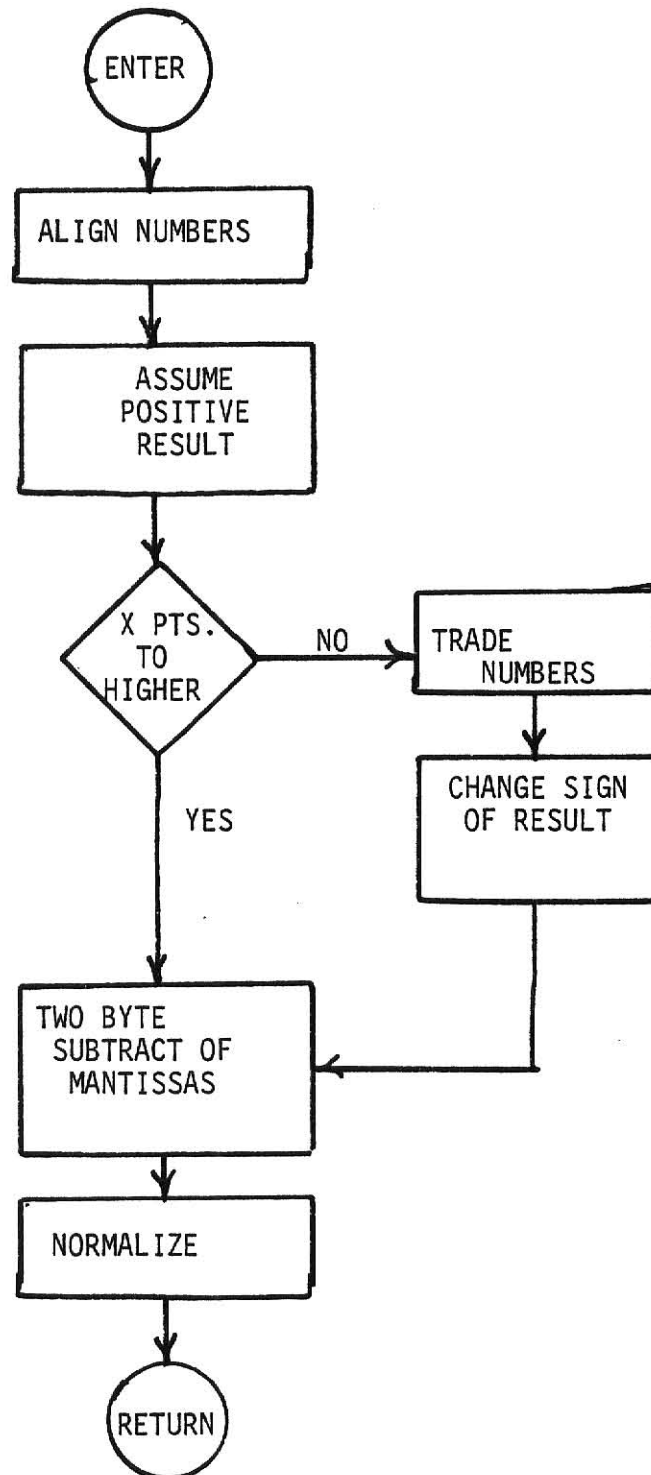
ALIGN



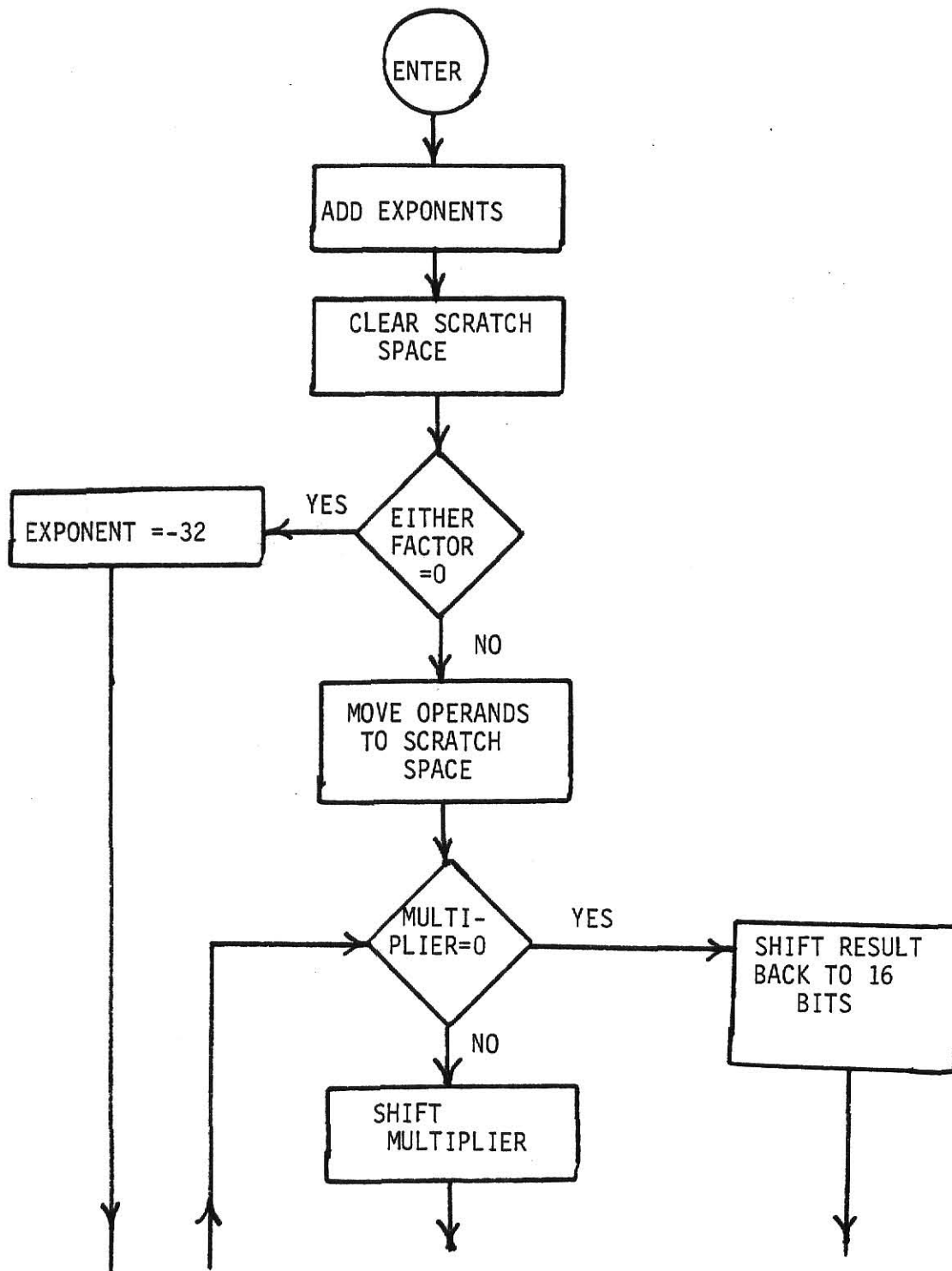
ADD

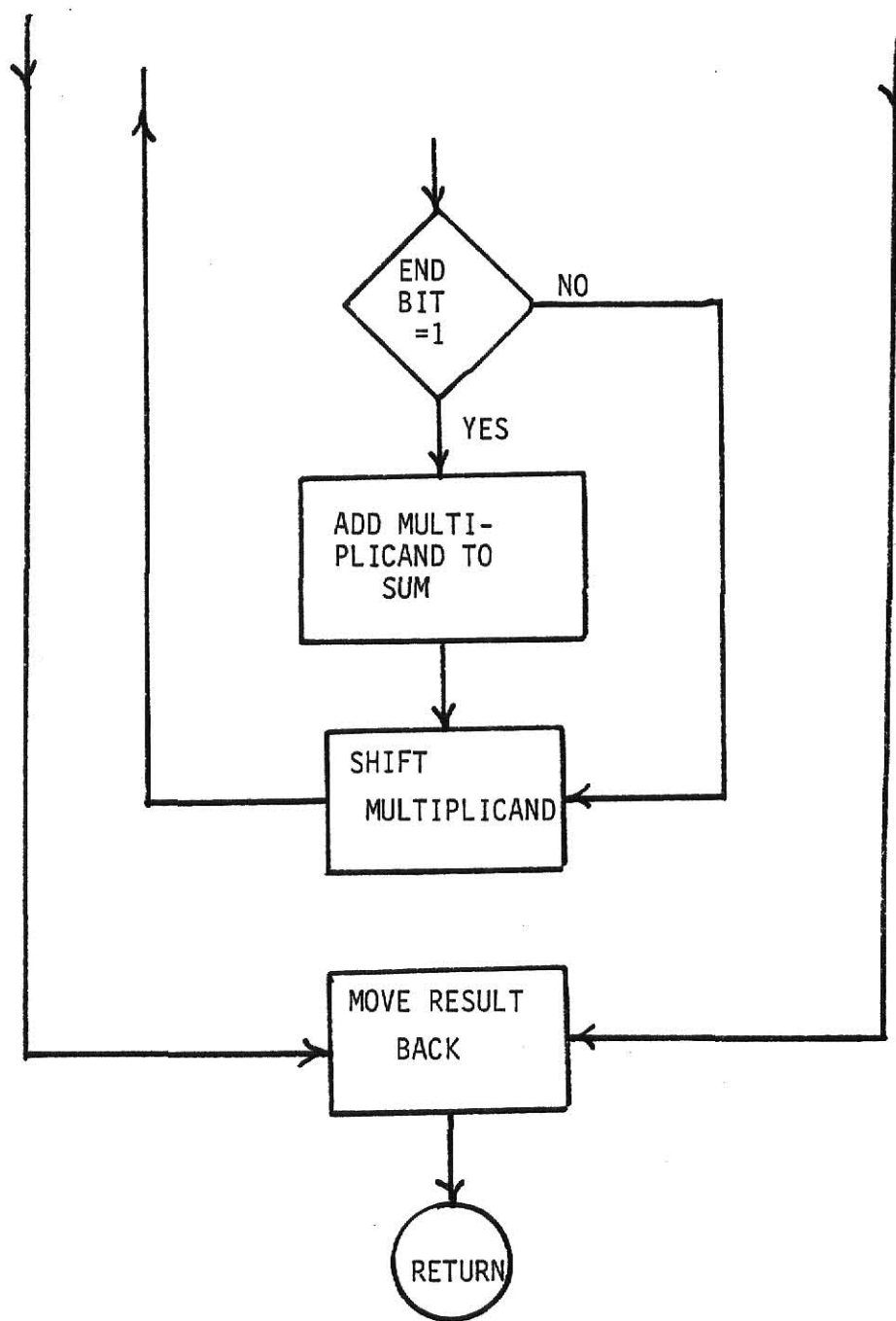


SUB



MPY





APPENDIX C
PROGRAM LISTINGS

Below is a listing of the SACEM computer software in standard 6502 Assembly language.

```

001          .OS
002          .LS
003 ;*****
004 ;
005 ;     SUBROUTINE TO READ THE A/D CONVERTER.  THE CHANNEL
006 ; TO BE READ MUST BE IN REGISTER A ON ENTRY.  THE RESULT
007 ; IS STORED AT THE LOCATION WITH ZERO-PAGE ADDRESS IN X.
008 ; LOCATION 0,X CONTAINS THE EXPONENT AND 1,X TO 2,X
009 ; CONTAIN THE NORMALIZED MANTISSA.  THE ROUTINE IS AUTO-
010 ; RANGING.  VERSION 4.  OCT 16, 1981
011 ;
012 ;-----
013 ;
014 UPPER      .DE $AC00          ;UPPER BITS OF DATA
015 LOWER      .DE $A800          ;LOWER 8 BITS OF DATA
016 CONTR      .DE $A80C          ;CONTROL REGISTER OF VIA
017 DDR        .DE $A803          ;DATA DIRECTION REGISTER
018 SELECT     .DE $A801          ;SELECT CHANNEL AND GAIN
019 TEMP       .DE 00             ;TEMPORARY SCRATCH LOCATIO
020 ;
021          .BA $E000
022          .MC $1000
023
E000- 0A      024 READ          ASL A          ;PUT CHANNEL IN UPPER 4
E001- 0A      025              ASL A
E002- 0A      026              ASL A
E003- 0A      027              ASL A
E004- 85 00    028              STA *TEMP
E006- 8A      029              TXA              ;STORE POINTER
E007- 48      030              PHA
E008- A2 00    031              LDX #0          ;GAIN COUNTER
032 ;
E00A- A9 FF    033              LDA #$FF
E00C- 8D 0C A8 034              STA CONTR          ;CONFIGURE VIA
E00F- 8D 03 A8 035              STA DDR
E012- A9 FD    036 AGAIN        LDA #$FD
E014- 8D 0C A8 037              STA CONTR          ;DROP LATCH LINE
038
E017- A5 00    039              LDA *TEMP          ;SELECT CHANNEL AND GAIN
E019- 8D 01 A8 040              STA SELECT
041
E01C- A9 FF    042              LDA #$FF
E01E- 8D 0C A8 043              STA CONTR          ;RAISE LATCH LINE
044
E021- A0 40    045              LDY #$40
E023- 88      046 DELAY1        DEY              ;ALLOW AMP. SETTling TIME
E024- D0 FD    047              BNE DELAY1
048
E026- A9 DF    049              LDA #$DF
E028- 8D 0C A8 050              STA CONTR          ;TRIGGER A/D CONVERSION
051
E02B- A0 10    052              LDY #$10
E02D- 88      053 DELAY2        DEY              ;ALLOW CONVERT TIME

```

```

E02E- D0 FD      054      BNE DELAY2
                        055
E030- A9 FF      056      LDA #$FF
E032- 8D 0C A8    057      STA CONTR
                        058
E035- AD 00 AC    059      LDA UPPER                ;DONE IF D11 <> 0
E038- 29 08      060      AND #$08
E03A- D0 11      061      BNE GET
                        062
E03C- E0 0A      063      CPX #$0A                ;DONE IF LOG(GAIN)=10
E03E- F0 0D      064      BEQ GET
                        065
E040- E8          066      INX                    ;GET NEXT GAIN AND
E041- A5 00      067      LDA *TEMP                ;TRY AGAIN
E043- 29 F0      068      AND #$F0
E045- 1D 69 E0    069      ORA TABLE,X
E048- 85 00      070      STA *TEMP
E04A- 4C 12 E0    071      JMP AGAIN
                        072
E04D- 8A          073      GET TXA                ;CALCULATE 2'S COMP
E04E- 49 FF      074      EOR #$FF                ;OF GAIN
E050- 18          075      CLC
E051- 69 01      076      ADC #01
E053- A8          077      TAY                    ;PUT IN Y
                        078
E054- 68          079      PLA
E055- AA          080      TAX                    ;RESTORE POINTER
                        081
E056- 98          082      TYA
E057- 95 00      083      STA *0,X                ;STORE EXPONENT
                        084
E059- AD 00 AC    085      LDA UPPER                ;GET UPPER 4
E05C- 29 0F      086      AND #$0F
E05E- 95 01      087      STA *1,X
                        088
E060- AD 00 A8    089      LDA LOWER                ;GET LOW 8 BITS
E063- 95 02      090      STA *2,X
                        091
E065- 20 74 E0    092      JSR NORM                ;NORMALIZE NUMBER
E068- 60          093      RTS
E069- 00 01 02    094      TABLE .BY 0 1 2 5 6 8 9 $A $C $D $E
E06C- 05 06 08
E06F- 09 0A 0C
E072- 0D 0E
                        095
096 ;*****
097
098 ; SUBROUTINE TO NORMALIZE A FLOATING POINT NUMBER.
099 ; THIS IS PERFORMED BY SHIFTING THE NUMBER LEFT UNTIL
100 ; D15=1 AND DECREMENTING THE EXPONENT. A ZERO VALUE
101 ; IS GIVEN THE EXPONENT -32. THE NUMBER TO BE
102 ; NORMALIZED IS FOUND AT THE ZERO PAGE ADDRESS IN X
103 ; AND THE RESULT IS LEFT THERE.

```

```

104
105 ;-----
106
E074- B5 01 107 NORM      LDA *1,X          ;IF THE NUMBER IS ZERO,
E076- 15 02 108          ORA *2,X          ;DON'T TRY TO SHIFT.
E078- F0 0F 109          BEQ ZERO
110
E07A- B5 01 111 LOOPNO    LDA *1,X          ;CHECK FOR D15=1
E07C- 29 80 112          AND #$80
E07E- D0 0D 113          BNE DONENO
114
E080- 16 02 115          ASL *2,X          ;DO SHIFTING AND TRY AGAIN
E082- 36 01 116          ROL *1,X
E084- D6 00 117          DEC *0,X
E086- 4C 7A E0 118         JMP LOOPNO
119
E089- A9 E0 120 ZERO      LDA #$E0          ;EXPONENT = -32
E08B- 95 00 121          STA *0,X
122
E08D- 60 123 DONENO      RTS
124
125 ;*****
126
127 ; SUBROUTINE TO ALIGN THE NUMBERS WITH ZERO-PAGE ADDRES-
128 ; SES IN X AND Y. RESULTS ARE IN THE SAME LOCATIONS.
129 ; ALL REGISTERS ARE PRESERVED. THE ALIGNMENT IS PER-
130 ; FORMED BY SHIFTING THE NUMBER WITH THE LOWER
131 ; EXPONENT AND INCREMENTING ITS EXPONENT.
132
133 ;-----
134
E08E- 48 135 ALIGN      PHA          ;SAVE REGISTERS
E08F- 8A 136          TXA
E090- 48 137          PHA
E091- 98 138          TYA
E092- 48 139          PHA
140
E093- B9 00 00 141 TOP      LDA 0,Y
E096- D5 00 142          CMP *0,X          ;COMPARE EXPONENTS
E098- F0 0E 143          BEQ DONEAL
144
E09A- 10 03 145          BPL SKIP          ;BE SURE X PTS TO LOWER
E09C- 20 AE E0 146          JSR SWAP        ;SWAP X&Y POINTERS
147
E09F- F6 00 148 SKIP      INC *0,X
E0A1- 56 01 149          LSR *1,X          ;DO SHIFTING
E0A3- 76 02 150          ROR *2,X
E0A5- 4C 93 E0 151         JMP TOP
152
E0A8- 68 153 DONEAL      PLA          ;RESTORE REGISTERS
E0A9- A8 154          TAY
E0AA- 68 155          PLA
E0AB- AA 156          TAX

```

```

EOAC- 68      157          PLA
EOAD- 60      158          RTS
159
160 ;*****
161 ;
162 ;   SUBROUTINE TO SWAP X AND Y REGISTERS.
163
164 ;-----
165
EOAE- 48      166 SWAP      PHA
EOAF- 8A      167          TXA
EOB0- 48      168          PHA
EOB1- 98      169          TYA
EOB2- AA      170          TAX
EOB3- 68      171          PLA
EOB4- A8      172          TAY
EOB5- 68      173          PLA
EOB6- 60      174          RTS
175
176 ;*****
177
178 ;   SUBROUTINE TO ADD THE FLOATING POINT NUMBERS WITH ZERO
179 ;   PAGE ADDRESSES IN X AND Y.  THE RESULT IS STORED AT
180 ;   THE ADDRESS IN X.
181
182 ;-----
183
EOB7- 20 8E E0 184 ADD      JSR ALIGN      ;ALIGN NUMBERS
185
EOBA- B5 02    186          LDA *2,X
EOBC- 18       187          CLC              ;ADD LOWS
EOBD- 79 02 00 188          ADC 2,Y
EOC0- 95 02    189          STA *2,X
190
EOC2- B5 01    191          LDA *1,X
EOC4- 79 01 00 192          ADC 1,Y          ;ADD HIGHS
EOC7- 95 01    193          STA *1,X
EOC9- 90 06    194          BCC DONEAD      ;IF NO CARRY, DONE
195
EOCB- 76 01    196          ROR *1,X          ;SHIFT CARRY BACK IN
EOCD- 76 02    197          ROR *2,X
EOCF- F6 00    198          INC *0,X          ;ADJUST EXPONENT
199
EOD1- 20 74 E0 200 DONEAD   JSR NORM        ;NORMALIZE RESULT
EOD4- 60       201          RTS
202
203 ;*****
204
205 ;   SUBROUTINE TO SUBTRACT THE NUMBERS WITH ZERO PAGE
206 ;   ADDRESSES IN X AND Y.  THE ABSOLUTE VALUE OF THE RESULT
207 ;   IS STORED AT THE ADDRESS POINTED TO BY X.  THE RESULT
208 ;   IS NORMALIZED.  THE SMALLER OF THE NUMBERS IS STORED
209 ;   AT THE ADDRESS POINTED TO BY Y.  A NEGATIVE RESULT IS

```

```

210 ; INDICATED BY A NON-ZERO VALUE AT LOCATION ZERO.
211
212 ;-----
213
214 SIGN          .DE 0                ;WHERE TO PUT SIGN
215
E0D5- 20 8E E0 216 SUB          JSR ALIGN          ;ALIGN NUMBERS
217
E0D8- A9 00      218          LDA #0
E0DA- 85 00      219          STA *SIGN          ;ASSUME POSITIVE RESULT
220
E0DC- B5 01      221          LDA *1,X
E0DE- D9 01 00 222          CMP 1,Y
E0E1- 90 09      223          BCC TRADE          ;EXCHANGE NUMBERS IF
E0E3- D0 21      224          BNE OK            ;X PTS TO HIGHER
E0E5- B5 02      225          LDA *2,X
E0E7- D9 02 00 226          CMP 2,Y
E0EA- B0 1A      227          BCS OK
228
E0EC- B9 01 00 229 TRADE      LDA 1,Y
E0EF- 48          230          PHA
E0F0- B5 01      231          LDA *1,X          ;SWAP HIGHS
E0F2- 99 01 00 232          STA 1,Y
E0F5- 68          233          PLA
E0F6- 95 01      234          STA *1,X
235
E0F8- B9 02 00 236          LDA 2,Y
E0FB- 48          237          PHA
E0FC- B5 02      238          LDA *2,X
E0FE- 99 02 00 239          STA 2,Y          ;SWAP LOWS
E101- 68          240          PLA
E102- E6 00      241          INC *SIGN
E104- 95 02      242          STA *2,X
243
E106- B5 02      244 OK      LDA *2,X
E108- 38          245          SEC          ;SUB LOWS
E109- F9 02 00 246          SBC 2,Y
E10C- 95 02      247          STA *2,X
248
E10E- B5 01      249          LDA *1,X          ;SUB HIGHS
E110- F9 01 00 250          SBC 1,Y
E113- 95 01      251          STA *1,X
252
E115- 20 74 E0 253          JSR NORM          ;NORMALIZE NUMBERS
E118- 60          254          RTS
255
256 ;*****
257
258 ; SUBROUTINE TO MULTIPLY THE NUMBERS WITH ZERO-PAGE
259 ; ADDRESSES IN X AND Y. THE PRODUCT IS STORED IN THE
260 ; ADDRESS POINTED TO BY X.
261
262 ;-----

```

		263		
E119-	B5 00	264	MPY	LDA *0,X
E11B-	18	265		CLC
E11C-	79 00 00	266		ADC 0,Y
E11F-	95 00	267		STA *0,X
		268		
E121-	8A	269		TXA
E122-	48	270		PHA
E123-	A2 06	271		LDX #06
E125-	A9 00	272		LDA #0
E127-	95 00	273	CLEAR	STA *0,X
E129-	CA	274		DEX
E12A-	D0 FB	275		BNE CLEAR
E12C-	68	276		PLA
E12D-	AA	277		TAX
		278		
E12E-	B9 01 00	279		LDA 1,Y
E131-	19 02 00	280		ORA 2,Y
E134-	F0 51	281		BEQ ZEROMP
E136-	B5 01	282		LDA *1,X
E138-	15 02	283		ORA *2,X
E13A-	F0 4B	284		BEQ ZEROMP
		285		
E13C-	B5 01	286		LDA *1,X
E13E-	85 07	287		STA *07
E140-	B5 02	288		LDA *2,X
E142-	85 08	289		STA *08
E144-	B9 01 00	290		LDA 1,Y
E147-	85 09	291		STA *09
E149-	B9 02 00	292		LDA 2,Y
E14C-	85 0A	293		STA *\$0A
		294		
E14E-	A5 0A	295	LOOPMP	LDA *\$0A
E150-	05 09	296		ORA *09
E152-	F0 20	297		BEQ OUT
		298		
E154-	46 09	299		LSR *09
E156-	66 0A	300		ROR *\$0A
E158-	90 0F	301		BCC NOADD
		302		
E15A-	A0 04	303		LDY #04
E15C-	18	304		CLC
E15D-	B9 00 00	305	ADD4	LDA 0,Y
E160-	79 04 00	306		ADC 4,Y
E163-	99 00 00	307		STA 0,Y
E166-	88	308		DEY
E167-	D0 F4	309		BNE ADD4
		310		
E169-	06 08	311	NOADD	ASL *08
E16B-	26 07	312		ROL *07
E16D-	26 06	313		ROL *06
E16F-	26 05	314		ROL *05
E171-	4C 4E E1	315		JMP LOOPMP

;ADD EXPONENTS

;CLEAR 6 SPACES
;FOR SCRATCH;TEST FOR ZERO
;MULTIPLIER;TEST FOR ZERO
;MULTIPLICAND;MOVE OPERANDS
;TO SCRATCH SPACE;DONE IF
;MULTIPLIER=0;SHIFT MULTIPLIER
;CHECK END BIT

;FOUR-BYTE ADD ROUTINE

;SHIFT MULTIPLICAND

```

316
E174- A5 01 317 OUT LDA *01
E176- 05 02 318 ORA *02 ;SHIFT BACK UNTIL
E178- F0 11 319 BEQ DONE ;UPPER 16=0
320
E17A- F6 00 321 INC *0,X ;BUMP EXPONENT
E17C- 46 01 322 LSR *01
E17E- 66 02 323 ROR *02
E180- 66 03 324 ROR *03
E182- 66 04 325 ROR *04
E184- 4C 74 E1 326 JMP OUT
327
E187- A9 E0 328 ZEROMP LDA #$E0 ;EXP=-32 IF ZERO
E189- 95 00 329 STA *0,X
330
E18B- A5 03 331 DONE LDA *03 ;PUT RESULT BACK
E18D- 95 01 332 STA *1,X
E18F- A5 04 333 LDA *04
E191- 95 02 334 STA *2,X
E193- 60 335 RTS
336 .EN
END OF MAE PASS!

```

--- LABEL FILE: ---

```

ADD =E0B7 ADD4 =E15D AGAIN =E012
ALIGN =E08E CLEAR =E127 CONTR =A80C
DDR =A803 DELAY1 =E023 DELAY2 =E02D
DONE =E18B DONEAD =E0D1 DONEAL =E0A8
DONENO =E08D GET =E04D LOOPMP =E14E
LOOPNO =E07A LOWER =A800 MPY =E119
NOADD =E169 NORM =E074 OK =E106
OUT =E174 READ =E000 SELECT =A801
SIGN =0000 SKIP =E09F SUB =E0D5
SWAP =E0AE TABLE =E069 TEMP =0000
TOP =E093 TRADE =E0EC UPPER =AC00
ZERO =E089 ZEROMP =E187
//0000,E194,1194

```

```

001          .OS
002 ;*****
003
004 ;      THIS IS A SUBROUTINE TO CONVERT THE FLOATING POINT
005 ; BINARY NUMBER WITH ZERO-PAGE ADDRESS IN X TO A DECIMAL
006 ; NUMBER IN THE DISPLAY BUFFER.  NUMBERS TOO LARGE ARE
007 ; INDICATED BY E'S IN THE DISPLAY.  THE NUMBER OF
008 ; DIGITS TO BE DISPLAYED SHOULD BE IN LOCATION 0.
009
010 ;-----
011
012          .BA $E200
013          .MC $1000
014          .LS
015 ACCESS   .DE $8B86
016 DISBUF   .DE $A640
017
E200- 20 86 8B 018 CONV      JSR ACCESS
E203- B5 00      019      LDA *0,X
E205- F0 05      020      BEQ OK
E207- 30 03      021      BMI OK
E209- 4C B3 E2 022      JMP TOOBIG
023
E20C- 85 02      024 OK      STA *02          ;MOVE NUMBER TO SCRATCH
E20E- B5 01      025      LDA *1,X
E210- 85 03      026      STA *03
E212- B5 02      027      LDA *2,X
E214- 29 F0      028      AND #$F0
E216- 85 04      029      STA *04          ;TRUNCATE TO 12 BITS
030
E218- A2 06      031      LDX #06          ;DISPLAY SPACE
E21A- A9 00      032      LDA #00
E21C- 95 06      033 CLEAR    STA *6,X
E21E- 9D 3F A6 034      STA DISBUF-1,X
E221- CA          035      DEX
E222- D0 F8      036      BNE CLEAR
E224- 85 05      037      STA *05
E226- 85 06      038      STA *06
039
E228- A5 02      040      LDA *02          ;TEST EXPONENT FOR 0
E22A- F0 0C      041      BEQ LINUP
042
E22C- 46 03      043 SLOOP    LSR *03          ; SHIFT RIGHT UNTIL
E22E- 66 04      044      ROR *04          ;EXPONENT=0
E230- 66 05      045      ROR *05
E232- 66 06      046      ROR *06
E234- E6 02      047      INC *02
E236- D0 F4      048      BNE SLOOP
049
E238- A9 0F      050 LINUP    LDA #$0F          ;DECIMAL PT IS AT END
E23A- 85 01      051      STA *01          ;OF $04 HERE
E23C- 06 04      052 ALOOP    ASL *04
E23E- 26 03      053      ROL *03          ;TEST EACH BIT TO

```

E240-	90 1E	054	BCC NOAD	;ADD CORRESPONDING
		055		
E242-	A5 01	056	LDA *01	
E244-	0A	057	ASL A	;3*COUNTER IN X
E245-	65 01	058	ADC *01	
E247-	AA	059	TAX	
		060		
E248-	F8	061	SED	;3-BYTE DECIMAL ADD
E249-	18	062	CLC	
E24A-	A5 09	063	LDA *09	
E24C-	7D C0 E2	064	ADC TAB+2,X	
E24F-	85 09	065	STA *09	
E251-	A5 08	066	LDA *08	
E253-	7D BF E2	067	ADC TAB+1,X	
E256-	85 08	068	STA *08	
E258-	A5 07	069	LDA *07	
E25A-	7D BE E2	070	ADC TAB,X	
E25D-	85 07	071	STA *07	
		072		
E25F-	D8	073	CLD	
E260-	C6 01	074 NOAD	DEC *01	;INTEGR PART DONE HERE
E262-	10 D8	075	BPL ALOOP	
		076		
E264-	A9 0F	077	LDA #\$0F	;16 MORE TIMES
E266-	85 01	078	STA *01	
		079		
E268-	06 06	080 ALOOP2	ASL *06	
E26A-	26 05	081	ROL *05	
E26C-	90 1E	082	BCC NOAD2	;TEST EACH BIT
		083		
E26E-	A5 01	084	LDA *01	
E270-	0A	085	ASL A	
E271-	65 01	086	ADC *01	;3*COUNTER IN X
E273-	AA	087	TAX	
		088		
E274-	F8	089	SED	;3-BYTE DECIMAL ADD
E275-	18	090	CLC	
E276-	A5 0C	091	LDA *\$0C	
E278-	7D F0 E2	092	ADC TAB2+2,X	
E27B-	85 0C	093	STA *\$0C	
E27D-	A5 0B	094	LDA *\$0B	
E27F-	7D EF E2	095	ADC TAB2+1,X	
E282-	85 0B	096	STA *\$0B	
E284-	A5 0A	097	LDA *\$0A	
E286-	7D EE E2	098	ADC TAB2,X	
E289-	85 0A	099	STA *\$0A	
		100		
E28B-	D8	101	CLD	;FRACTION DONE HERE
E28C-	C6 01	102 NOAD2	DEC *01	
E28E-	10 D8	103	BPL ALOOP2	
E290-	A2 0D	104	LDX #\$0D	;12 POSSIBLE DIGITS
		105		
E292-	20 1E E3	106 LOOP	JSR NEXDIG	;LOOK AT LEFT DIGITS

E295- CA	107	DEX	;UNTIL NON-ZERO OR DEC.
E296- E0 07	108	CPX #07	;PT IS FOUND.
E298- F0 04	109	BEQ GO	
	110		
E29A- C9 3F	111	CMP #\$3F	
E29C- F0 F4	112	BEQ LOOP	
	113		
E29E- A0 00	114	LDY #0	
E2A0- E0 07	115	CPX #07	;CHECK FOR PT.
E2A2- D0 02	116	BNE ARND	
E2A4- 09 80	117	ORA #\$80	;PUT ON PT.
	118		
E2A6- 99 40 A6	119	STA DISBUF,Y	
E2A9- 20 1E E3	120	JSR NEXDIG	;GO UNTIL ALL
E2AC- CA	121	DEX	
E2AD- C8	122	INY	
E2AE- C4 00	123	CPY *00	
E2B0- D0 EE	124	BNE LOOP2	
E2B2- 60	125	RTS	
	126		
E2B3- A2 06	127	LDX #06	
E2B5- A9 79	128	LDA #\$79	;DISPLAY E'S
E2B7- 9D 3F A6	129	STA DISBUF-1,X	
E2BA- CA	130	DEX	
E2BB- D0 FA	131	BNE LOOPN	
E2BD- 60	132	RTS	
	133		
E2BE- 00 00 01	134	.BY \$00 \$00 \$01	;TABLE OF DECIMAL EQUIV.
E2C1- 00 00 02	135	.BY \$00 \$00 \$02	;OF POWERS OF 2
E2C4- 00 00 04	136	.BY \$00 \$00 \$04	
E2C7- 00 00 08	137	.BY \$00 \$00 \$08	;2**3
E2CA- 00 00 16	138	.BY \$00 \$00 \$16	;2**4
E2CD- 00 00 32	139	.BY \$00 \$00 \$32	;2**5
E2D0- 00 00 64	140	.BY \$00 \$00 \$64	;ETC.
E2D3- 00 01 28	141	.BY \$00 \$01 \$28	
E2D6- 00 02 56	142	.BY \$00 \$02 \$56	
E2D9- 00 05 12	143	.BY \$00 \$05 \$12	
E2DC- 00 10 24	144	.BY \$00 \$10 \$24	
E2DF- 00 20 48	145	.BY \$00 \$20 \$48	
E2E2- 00 40 96	146	.BY \$00 \$40 \$96	
E2E5- 00 81 92	147	.BY \$00 \$81 \$92	
E2E8- 01 63 84	148	.BY \$01 \$63 \$84	
E2EB- 03 27 68	149	.BY \$03 \$27 \$68	;2**15
E2EE- 00 00 15	150	.BY \$00 \$00 \$15	;TABLE OF NEGATIVE POWERS
E2F1- 00 00 31	151	.BY \$00 \$00 \$31	
E2F4- 00 00 61	152	.BY \$00 \$00 \$61	;2**-14
E2F7- 00 01 22	153	.BY \$00 \$01 \$22	;2**-13
E2FA- 00 02 44	154	.BY \$00 \$02 \$44	;ETC.
E2FD- 00 04 88	155	.BY \$00 \$04 \$88	
E300- 00 09 77	156	.BY \$00 \$09 \$77	
E303- 00 19 53	157	.BY \$00 \$19 \$53	
E306- 00 39 06	158	.BY \$00 \$39 \$06	
E309- 00 78 13	159	.BY \$00 \$78 \$13	

```

E30C- 01 56 25 160      .BY $01 $56 $25
E30F- 03 12 50 161      .BY $03 $12 $50
E312- 06 25 00 162      .BY $06 $25 $00
E315- 12 50 00 163      .BY $12 $50 $00
E318- 25 00 00 164      .BY $25 $00 $00
E31B- 50 00 00 165      .BY $50 $00 $00
166
167 ;-----
168
169 ; SUBROUTINE TO SHIFT LEFT FOUR BITS AND PUT THE
170 ; SEGMENT CODES FOR THE NEXT DIGIT IN A.
171
E31E- 8A      172 NEXDIG      TXA      ;SAVE REGISTERS
E31F- 48      173      PHA
E320- 98      174      TYA
E321- 48      175      PHA
E322- A0 04    176      LDY #04      ;FOUR SHIFTS
E324- A2 06    177 OUTSH      LDX #06      ;SIX BYTES TO SHIFT
E326- 06 0C    178      ASL *$0C
E328- 36 05    179 SHFT      ROL *5,X
E32A- CA      180      DEX
E32B- D0 FB    181      BNE SHFT
E32D- 88      182      DEY
E32E- D0 F4    183      BNE OUTSH      ;SHIFTING DONE
184
E330- A5 06    185      LDA *06      ;LOAD A AND RESTORE X&Y
E332- 29 0F    186      AND #$0F
E334- A8      187      TAY
E335- B9 41 E3 188      LDA DIGIT,Y
E338- 85 05    189      STA *05
E33A- 68      190      PLA
E33B- A8      191      TAY
E33C- 68      192      PLA
E33D- AA      193      TAX
E33E- A5 05    194      LDA *05
E340- 60      195      RTS
E341- 3F 06 5B 196 DIGIT      .BY $3F $06 $5B $4F $66 $6D $7D $07
E344- 4F 66 6D
E347- 7D 07
E349- 7F 67 77 197      .BY $7F $67 $77 $7C $39 $5E $79 $71
E34C- 7C 39 5E
E34F- 79 71
198      .EN
END OF MAE PASS!

```

--- LABEL FILE: ---

ACCESS =8B86
 ARND =E2A6
 DIGIT =E341
 LINUP =E238
 LOOPN =E2B7
 NOAD2 =E28C

ALLOOP =E23C
 CLEAR =E21C
 DISBUF =A640
 LOOP =E292
 NEXDIG =E31E
 OK =E20C

ALLOOP2 =E268
 CONV =E200
 GO =E29E
 LOOP2 =E2A0
 NOAD =E260
 OUTSH =E324

SHFT =E328
TAB2 =E2EE
//0000,E351,1151

SLOOP =E22C
TOOBIG =E2B3

TAB =E2BE

```

001          .LS
002          .OS
003          .BA $E400
004          .MC $1000
005 ;*****
006
007 ; SUBROUTINE TO COMPARE TWO FLOATING POINT NUMBERS
008 ; WITH ZERO-PAGE ADDRESSES IN X AND Y. ON RETURN, THE
009 ; FLAGS ARE SET AS IF TO SINGLE BYTES WERE COMPARED.
010
011 ;-----
012
E400- B5 00 013 COMP      LDA *0,X          ;COMPARE EXPONENT
E402- D9 00 00 014      CMP 0,Y
E405- D0 0C      015      BNE RET
016
E407- B5 01      017      LDA *1,X          ;COMPARE FIRST BYTE
E409- D9 01 00 018      CMP 1,Y
E40C- D0 05      019      BNE RET
020
E40E- B5 02      021      LDA *2,X          ;COMPARE SECOND BYTE
E410- D9 02 00 022      CMP 2,Y
023
E413- 60      024 RET      RTS
025
026 ;*****
027
028 ; SUBROUTINE TO FIND THE CANGE IN CRUSHING ENERGY SINCE
029 ; LAST CALL. THE ABSOLUTE VALUE OF THE CHANGE IS STORED
030 ; AT $2F. AND THE SIGN IS INDICATED BY THE VALUE IN $0.
031 ; A NON-ZERO VALUE IN $0 INDICATES A NEGATIVE RESULT. THE
032 ; ROUTINE ALSO ASSUMES THESE LOCATIONS:
033 ; $23 PAST FORCE          $26 PAST DISPLACEMENT
034 ; LOCATIONS $29 THROUGH $31 ARE ALSO USED.
035
036 ;-----
037
038 READ      .DE $E000          ;ROUTINE TO READ A/D
039 ADD      .DE $E0B7          ;ADDITION ROUTINE
040 SUB      .DE $E0D5          ;SUBTRACTION ROUTINE
041 MPY      .DE $E119          ;MULTIPLICATION ROUTINE
042
E414- A9 06      043 DELTAE      LDA #06          ;CURR F TO $29
E416- A2 29      044          LDX #$29
E418- 20 00 E0 045          JSR READ
046
E41B- A9 07      047          LDA #07          ;DURR D TO $2C
E41D- A2 2C      048          LDX #$2C
E41F- 20 00 E0 049          JSR READ
050
E422- A9 06      051          LDA #06          ;READ F AFTER D
E424- A2 00      052          LDX #0          ;TO LET SETTLE
E426- 20 00 E0 053          JSR READ

```

```

054
E429- A2 03 055      LDX #03          ;COPY CURR D TO $2F
E42B- B5 2B 056 LOOP  LDA *$2B,X
E42D- 95 2E 057      STA *$2E,X
E42F- CA 058      DEX
E430- D0 F9 059      BNE LOOP
060
E432- A2 2F 061      LDX #$2F          ;ABS(DELTA D) IN $2F
E434- A0 26 062      LDY #$26
E436- 20 D5 E0 063     JSR SUB
064
E439- A2 23 065      LDX #$23          ;AVG F IN $23
E43B- A0 29 066      LDY #$29
E43D- 20 B7 E0 067     JSR ADD
E440- C6 23 068      DEC *$23
069
E442- A2 2F 070      LDX #$2F          ;ABS(DELTA E) IN $2F
E444- A0 23 071      LDY #$23
E446- 20 19 E1 072     JSR MPY
073
E449- A2 03 074      LDX #03          ;MOVE CURR F AND D TO PAST
E44B- B5 2B 075 MOVE  LDA *$2B,X
E44D- 95 25 076      STA *$25,X
E44F- B5 28 077      LDA *$28,X
E451- 95 22 078      STA *$22,X
E453- CA 079      DEX
E454- D0 F5 080      BNE MOVE
081
E456- 60 082      RTS
083 ;*****
084
085 ; SUBROUTINE TO MOVE THE NUMBER WITH ZERO-PAGE
086 ; ADDRESS IN X TO THE ZERO-PAGE ADDRESS IN Y.
087
088 ;-----
089
E457- B5 00 090 MOVEM  LDA *0,X
E459- 99 00 00 091      STA 0,Y
E45C- B5 01 092      LDA *1,X
E45E- 99 01 00 093      STA 1,Y
E461- B5 02 094      LDA *2,X
E463- 99 02 00 095      STA 2,Y
E466- 60 096      RTS
097
098 ;*****
099
100 ; CONTROL PASSES TO HERE ON RESET. THIS CODE WAS COPIED
101 ; FROM THE SYM-1 REFERENCE MANUAL. SYSTEM RAM IS INIT-
102 ; IALIZED, THE SYM IS CONFIGURED, AND THE SOIL TESTING
103 ; MONITOR IS INVOKED.
104
105 ;-----
106

```

```

E467- A2 FF    107 RESET    LDX #$FF
E469- 9A      108          TXS                ;INIT STACK
                                           109
E46A- A9 CC    110 POR      LDA #$CC          ;DISABLE POR, TAPE OFF
E46C- 8D 0C A0 111          STA $A00C
E46F- A9 04    112          LDA #04
E471- 48      113          PHA
E472- 28      114          PLP
E473- 20 86 8B 115          JSR $8B86          ;RAM ACCESS
                                           116
E476- A2 5F    117 DFTSR    LDX #$5F
E478- BD A0 8F 118          LDA $8FA0,X        ;INIT SYSTEM RAM
E47B- 9D 20 A6 119          STA $A620,X
E47E- CA      120          DEX
E47F- 10 F7    121          BPL DFTSR+2
                                           122
E481- A9 07    123          LDA #7             ;BEEP
E483- 20 47 8A 124          JSR $8A47          ;OUTCHR
E486- 20 A3 89 125          JSR $89A3          ;KSCONF
E489- 4C 00 E7 126          JMP $E700          ;TO MONITOR
                                           127
                                           128 ;*****
                                           129 .EN

```

END OF MAE PASS!

--- LABEL FILE: ---

ADD =E0B7	COMP =E400	DELTAE =E414
DFTSR =E476	LOOP =E42B	MOVE =E44B
MOVEM =E457	MPY =E119	POR =E46A
READ =E000	RESET =E467	RET =E413
SUB =E0D5		
//0000,E48C,108C		

```

001 ;*****
002
003 ; SUBROUTINE TO TAKE EIGHT READINGS OF THE CHANNEL IN
004 ; A AND AVERAGE THEM INTO THE ADDRESS IN X. LOCATIONS
005 ; 01 THROUGH 06 ARE ALSO USED.
006
007 ;-----
008
009 .OS
010 .LS
011 .BA $E500
012 .MC $1000
013
014 READ .DE $E000
015 ADD .DE $E0B7
016
E500- 85 05 017 BASE STA *05
E502- A9 08 018 LDA #8 ;DO EIGHT TIMES
E504- 85 04 019 STA *04
020
E506- A9 E0 021 LDA #$E0 ;ZERO RESULT
E508- 95 00 022 STA *0,X
E50A- A9 00 023 LDA #00
E50C- 95 01 024 STA *1,X
E50E- 95 02 025 STA *2,X
026
E510- 86 06 027 STX *06
028
E512- A2 01 029 LOOP LDX #01 ;READ INTO SCRATCH
E514- A5 05 030 LDA *05
E516- 20 00 E0 031 JSR READ
032
E519- A6 06 033 LDX *06
E51B- A0 01 034 LDY #01
E51D- 20 B7 E0 035 JSR ADD
036
E520- C6 04 037 DEC *04
E522- D0 EE 038 BNE LOOP
039
E524- A6 06 040 LDX *06
E526- D6 00 041 DEC *0,X
E528- D6 00 042 DEC *0,X
E52A- D6 00 043 DEC *0,X
044
E52C- 60 045 RTS
046
047 ;*****
048
049 ; THIS IS A SUBROUTINE TO FIND THE INITIAL BREAK FORCE.
050 ; A RUNNING MAXIMUM IS KEPT UNTIL THE CURRENT FORCE DROPS
051 ; MORE THAN 25% BELOW THE MAXIMUM. ALL FORCES ARE
052 ; RELATIVE TO AN INITIAL FORCE IN $20. NOTHING IS
053 ; CONSIDERED UNTIL THE RELATIVE FORCE IS >.2 KG.

```

```

054 ; MATHEMATICALLY, THIS DEFINITION IS:
055 ; BREAK=FMAX WHEN  $4((FMAX-F0)-(F-F0)) > (FMAX-F0)$ 
056 ; AND  $(F-F0) > .2 \text{ KG}$ 
057 ; IT IS ASSUMED THAT F0, MAXFLG, FMAX, AND KG2 ARE
058 ; APPROPRIATELY INITIALIZED.
059 ; THE FORCE AT WHICH TO STOP THE TEST IS ALSO
060 ; CALCULATED AS A NUMBER OF FOURTHS OF FMAX
061
062 ;-----
063
064 F0 .DE $20
065 CURF .DE $29
066 FDIFF .DE $35
067 KG2 .DE $3B
068 MAXFLG .DE $3A
069 FMAX .DE $3E
070 SCR1 .DE $41
071 MOVE .DE $E457
072 COMP .DE $E400 ;COMPARE ROUTNE
073 SUB .DE $E0D5
074 STOPF .DE $44
075 LIM .DE $39
076 NORM .DE $E074
077
E52D- A5 3A 078 BREAK LDA *MAXFLG ;SKIP IF ALREADY FOUND
E52F- D0 72 079 BNE CHECK
080
E531- A2 29 081 LDX #CURF
E533- A0 35 082 LDY #FDIFF
E535- 20 57 E4 083 JSR MOVE ;MOVE OPERANDS TO SCRATCH
084
E538- A2 20 085 LDX #F0
E53A- A0 41 086 LDY #SCR1
E53C- 20 57 E4 087 JSR MOVE
088
E53F- A2 35 089 LDX #FDIFF
E541- A0 41 090 LDY #SCR1
E543- 20 D5 E0 091 JSR SUB ;F-F0
092
E546- A2 35 093 LDX #FDIFF
E548- A0 3B 094 LDY #KG2
E54A- 20 00 E4 095 JSR COMP ;IF F-F0<.2 KG
E54D- 90 5F 096 BCC RET ;THEN RETURN
097
E54F- A2 35 098 LDX #FDIFF ;IF F-F0>FMAX-F0
E551- A0 3E 099 LDY #FMAX ;THEN REPLACE FMAX
E553- 20 00 E4 100 JSR COMP
E556- 90 03 101 BCC ARND
102
E558- 20 57 E4 103 JSR MOVE
104
E55B- A2 3E 105 ARND LDX #FMAX
E55D- A0 41 106 LDY #SCR1

```

```

E55F- 20 57 E4 107      JSR MOVE
                        108
E562- A2 35      109      LDX #FDIFF      ;4*ABS(F-FMAX)
E564- A0 41      110      LDY #SCR1
E566- 20 D5 E0 111      JSR SUB
E569- E6 35      112      INC *FDIFF
E56B- E6 35      113      INC *FDIFF
                        114
E56D- A2 35      115      LDX #FDIFF      ;IF >FMAX THEN BREAK FOUND
E56F- A0 3E      116      LDY #FMAX
E571- 20 00 E4 117      JSR COMP
E574- 90 38      118      BCC RET
                        119
E576- E6 3A      120      INC *MAXFLG
E578- C6 3E      121      DEC *FMAX      ;FMAX/4
E57A- C6 3E      122      DEC *FMAX
                        123
E57C- A2 3E      124      LDX #FMAX
E57E- A0 44      125      LDY #STOPF      ;MOVE TO STOPF
E580- 20 57 E4 126      JSR MOVE
E583- C6 39      127      DEC *LIM
                        128
E585- A2 44      129 ADDS      LDX #STOPF      ;ADD LIM-1 TIMES
E587- A0 3E      130      LDY #FMAX
E589- 20 B7 E0 131      JSR ADD
E58C- C6 39      132      DEC *LIM
E58E- D0 F5      133      BNE ADDS
                        134
E590- A2 3E      135      LDX #FMAX      ;RESTORE FMAX
E592- 20 74 E0 136      JSR NORM
E595- E6 3E      137      INC *FMAX
E597- E6 3E      138      INC *FMAX
                        139
E599- A2 44      140      LDX #STOPF      ;BACK TO NON-
E59B- A0 20      141      LDY #F0      ;RELATIVE
E59D- 20 B7 E0 142      JSR ADD
E5A0- 18      143      CLC
E5A1- 90 0B      144      BCC RET
                        145
E5A3- A2 29      146 CHECK      LDX #CURF      ;CHECK FOR STOP FORCE
E5A5- A0 44      147      LDY #STOPF
E5A7- 20 00 E4 148      JSR COMP
E5AA- 90 02      149      BCC RET
                        150
E5AC- E6 3A      151      INC *MAXFLG      ;INCREMENT AGAIN
                        152
E5AE- 60      153 RET      RTS
                        154
155 ;*****
156
157 ; SUBROUTINE TO INITIALIZE THE VARIABLES IS SCRATCHPAD
158 ; RAM. THE A/D CONVERTER IS READ ON BOTH CHANNELS TO ALLOW
159 ; SETTLING. THE VARIABLES INITIALIZED ARE:

```

```

160 ; KG2= ED D8 00          MAXFLG= 00
161 ; FMAX= E0 00 00        F0= AVG. OF 8 READINGS
162 ; D0= AVG OF 8          PASTF= READ FROM A/D
163 ; PASTD= READ FROM A/D  LIM FROM PLIM
164 ; ESUM= F1 80 00        SLIM= F5 80 00
165 ; FCONV= F2 98 70      DCONV= E7 B0 A0
166 ; ECONV= E5 A5 18      ONE= F1 80 00
167
168 ; WHEN THE INITIALIZAION IS COMPLETE, THE BEEPER IS
169 ; SOUNDED FOUR TIMES
170
171 ; -----
172
173 BEEP          .DE $8972
174 SWAP          .DE $EOAE
175 PLIM          .DE $38
176
E5AF- A9 07      177 INIT          LDA #07          ;READ BOTH CHANNELS
E5B1- A2 20      178          LDX #$20
E5B3- 20 00 E5   179          JSR BASE
E5B6- A9 06      180          LDA #06
E5B8- A2 20      181          LDX #$20
E5BA- 20 00 E5   182          JSR BASE
183
E5BD- A2 1F      184          LDX #$1F          ;DO BLOCK MOVE
E5BF- BD 06 E6   185 LP2          LDA TABLE-1,X      ;FROM TABLE
E5C2- 95 39      186          STA *$39,X          ;OF DEFAULT VALUES
E5C4- CA         187          DEX
E5C5- D0 F8      188          BNE LP2
189
E5C7- A0 60      190          LDY #$60          ;DELAY ABOUT 2 SEC
E5C9- A2 00      191 OUTER        LDX #0          ;TO ALLOW SETTLING
E5CB- 20 AE E0   192 INNER        JSR SWAP
E5CE- 20 AE E0   193          JSR SWAP
E5D1- CA         194          DEX
E5D2- D0 F7      195          BNE INNER
E5D4- 88         196          DEY
E5D5- D0 F2      197          BNE OUTER
198
E5D7- A9 06      199          LDA #06
E5D9- A2 20      200          LDX #$20
E5DB- 20 00 E5   201          JSR BASE          ;READ F0
202
E5DE- A9 06      203          LDA #06
E5E0- A2 23      204          LDX #$23
E5E2- 20 00 E0   205          JSR READ          ;GET PASTF
206
E5E5- A9 07      207          LDA #07
E5E7- A2 32      208          LDX #$32
E5E9- 20 00 E5   209          JSR BASE          ; READ D0
210
E5EC- A9 07      211          LDA #07
E5EE- A2 26      212          LDX #$26

```

```

E5F0- 20 00 E0 213      JSR READ          ; READ PASTD
                        214
E5F3- A9 06      215      LDA #06          ;ALWAYS READ F
E5F5- A2 00      216      LDX #0           ;AFTER D
E5F7- 20 00 E0 217      JSR READ
                        218
E5FA- A5 38      219      LDA *PLIM
E5FC- 85 39      220      STA *LIM          ;INITIALIZE LIM
                        221
E5FE- A2 04      222      LDX #04
E600- 20 72 89 223 LPB    JSR BEEP          ;GIVE TONE SIGNAL
E603- CA          224      DEX
E604- D0 FA      225      BNE LPB
                        226
E606- 60          227      RTS
                        228
E607- 00          229 TABLE .BY $00          ;MAXFLG
E608- ED 80 00 230      .BY $ED $80 $00 ;KG2
E60B- E0 00 00 231      .BY $E0 $00 $00 ;FMAX
E60E- 00 00 00 232      .BY $00 $00 $00
E611- E0 00 00 233      .BY $E0 $00 $00 ;STOPF
E614- F1 80 00 234      .BY $F1 $80 $00 ;SUM E
E617- F5 80 00 235      .BY $F5 $80 $00 ;STRESS LIMIT
E61A- F2 98 70 236      .BY $F2 $98 $70 ;FCONV=2.3818 KG/CT
E61D- E7 B0 A0 237      .BY $E7 $B0 $A0 ;DCONV=.0013475 CM/CT
E620- E5 A5 18 238      .BY $E5 $A5 $18 ;ECONV=.0003149 J/CT
E623- F1 80 00 239      .BY $F1 $80 $00 ;ONE=1
                        240
                        241 ;*****
                        242
                        243 ; SUBROUTINE TO DO A COMPRESSION TEST. THE ZERO-
                        244 ; PAGE VARIABLES ARE INITIALIZED AND THE CRUSHING ENERGY
                        245 ; IS INTEGRATED. THE CURRENT FORCE IN KILOGRAMS IS DIS-
                        246 ; PLAYED. WHEN THE BREAK FORCE IS FOUND, THE UPPER SEG-
                        247 ; MENT OF THE RIGHTMOST DISPLAY DIGIT IS LIT. THE TEST
                        248 ; IS ENDED WHEN THE FORCE PASSES THE STOP FORCE.
                        249 ; PRESSING ANY KEY ON THE HEX KEYBOARD ABORTS THE TEST.
                        250 ; IF THE FORCE PASSES ABOUT 40 KG, THE BEEPER IS SOUNDED
                        251 ; EACH TIME THROUGH THE SAMPLE LOOP BUT THE TEST CONTINUES
                        252
                        253 ;-----
                        254
255 EDEL          .DE $2F
256 ESUM          .DE $47
257 DELTAE        .DE $E414
258 FCONV         .DE $4D
259 MPY           .DE $E119
260 SCAND         .DE $8906
261 INSTAT        .DE $8386
262 CONV          .DE $E200
263 PASTF         .DE $23
264 KG40          .DE $4A
265 ONE           .DE $56

```

		266	CURD	.DE \$2C	
		267	D0	.DE \$32	
		268			
E626-	20 AF E5	269	TEST	JSR INIT	; INITIALIZE VARS
E629-	20 14 E4	270	AGN	JSR DELTAE	; GET ENERGY CHANGE
E62C-	A2 47	271		LDX #ESUM	
E62E-	A0 2F	272		LDY #EDEL	
E630-	A5 00	273		LDA *00	
E632-	D0 06	274		BNE NEG	; GO ARND IF NEGATIVE
		275			
E634-	20 B7 E0	276		JSR ADD	; SUM UP
E637-	18	277		CLC	
E638-	90 03	278		BCC OVER	
E63A-	20 D5 E0	279	NEG	JSR SUB	; SUBTRACT NEGATIVE
		280			
E63D-	20 2D E5	281	OVER	JSR BREAK	
		282			
E640-	A2 29	283		LDX #CURF	; CONVERT TO KG
E642-	A0 4D	284		LDY #FCONV	
E644-	20 19 E1	285		JSR MPY	
		286			
E647-	A9 03	287		LDA #03	; DISPLAY CURRENT F
E649-	85 00	288		STA *00	
E64B-	A2 29	289		LDX #CURF	
E64D-	20 00 E2	290		JSR CONV	
		291			
E650-	A5 3A	292		LDA *MAXFLG	
E652-	C9 02	293		CMP #2	; TEST DONE IF BREAK
E654-	F0 22	294		BEQ END	; RETURNS 2 IN MAXFLG
		295			
E656-	8D 45 A6	296		STA \$A645	; INDICATE BREAK FOUND
		297			
E659-	A9 10	298		LDA #\$10	
E65B-	85 FF	299		STA *\$FF	; DISPLAY COUNTER
E65D-	20 06 89	300	DISP	JSR SCAND	
E660-	D0 13	301		BNE ABORT	; GO IF KEY PRESSED
E662-	C6 FF	302		DEC *\$FF	
E664-	D0 F7	303		BNE DISP	
		304			
E666-	A2 23	305		LDX #PASTF	
E668-	A0 4A	306		LDY #KG40	
E66A-	20 00 E4	307		JSR COMP	; FORCE TOO BIG?
E66D-	90 03	308		BCC SKIP	; GO IF OK
E66F-	20 72 89	309		JSR BEEP	; WARN IF BIG
		310			
E672-	18	311	SKIP	CLC	; DO AGAIN
E673-	90 B4	312		BCC AGN	
		313			
E675-	20 86 83	314	ABORT	JSR INSTAT	; DEBOUNCE KEY
E678-	A2 47	315	END	LDX #ESUM	; SUBTRACT INITIAL
E67A-	A0 56	316		LDY #ONE	; ENERGY
E67C-	20 D5 E0	317		JSR SUB	
		318			

E67F-	A2 2C	319	LDX #CURD	;NEED TO SUBTRACT
E681-	A0 32	320	LDY #D0	;F0*(FINALD-D0)
E683-	20 D5 E0	321	JSR SUB	;FINALD-D0
		322		
E686-	A2 2C	323	LDX #CURD	
E688-	A0 20	324	LDY #F0	
E68A-	20 19 E1	325	JSR MPY	;MULTIPLY
		326		
E68D-	A2 47	327	LDX #ESUM	
E68F-	A0 2C	328	LDY #CURD	
E691-	20 D5 E0	329	JSR SUB	;TAKE AWAY
		330		
E694-	A2 03	331	LDX #03	;SIGNAL END
E696-	20 00 E6	332	JSR LPB	
		333		
E699-	60	334	RTS	
		335		
		336	;*****	
		337	.EN	

END OF MAE PASS!

--- LABEL FILE: ---

ABORT =E675	ADD =E0B7	ADDS =E585
AGN =E629	ARND =E55B	BASE =E500
BEEP =8972	BREAK =E52D	CHECK =E5A3
COMP =E400	CONV =E200	CURD =002C
CURF =0029	D0 =0032	DELTAE =E414
DISP =E65D	EDEL =002F	END =E678
ESUM =0047	F0 =0020	FCONV =004D
FDIFF =0035	FMAX =003E	INIT =E5AF
INNER =E5CB	INSTAT =8386	KG2 =003B
KG40 =004A	LIM =0039	LOOP =E512
LP2 =E5BF	LPB =E600	MAXFLG =003A
MOVE =E457	MPY =E119	NEG =E63A
NORM =E074	ONE =0056	OUTER =E5C9
OVER =E63D	PASTF =0023	PLIM =0038
READ =E000	RET =E5AE	SCAND =8906
SCR1 =0041	SKIP =E672	STOPF =0044
SUB =E0D5	SWAP =E0AE	TABLE =E607
TEST =E626		
//0000,E69A,119A		

```

001 ;*****
002
003 ;  MONITOR PROGRAM TO DRIVE SOIL TESTING MACHINE.
004 ;  AFTER INITIALIZATION, THE KEYBOARD IS SCANNED FOR
005 ;  COMMANDS.  THE COMMAND TO BE EXECUTED IS DETERMINED
006 ;  AND THE FUNCTION PERFORMED.  CONTROL IS THEN PASSED
007 ;  BACK TO THE SCAN.  THE SYM MONITOR I/O ROUTINES ARE
008 ;  USED.  THE FUNCTIONS AVAILABLE ARE:
009 ;  DISPLAY INITIAL FORCE
010 ;  DISPLAY INITIAL DISPLACEMENT
011 ;  DISPLAY FINAL FORCE
012 ;  DISPLAY FINAL DISPLACEMENT
013 ;  DISPLAY BREAKING FORCE
014 ;  DISPLAY ENERGY INTEGRAL
015 ;  CHANGE PLIM TO ADJUST STOP FORCE
016 ;  PERFORM COMPRESSION TEST
017 ;  SET THE DISPLACEMENT TRANSDUCER
018 ;  JUMP TO SYM MONITOR
019
020 ;-----
021
022          .OS
023          .LS
024          .BA $E700
025          .MC $1000
026
027 INIT      .DE $E5AF
028 PLIM      .DE $38
029 DISBUF    .DE $A640
030 ACCESS    .DE $8B86
031 GETKEY    .DE $88AF
032 FCONV     .DE $4D
033 DCONV     .DE $50
034 PASTD     .DE $26
035 PASTF     .DE $23
036 FMAX      .DE $3E
037 ESUM      .DE $47
038 ECONV     .DE $53
039 DIGIT     .DE $E341
040 SCR1      .DE $41
041 MPY       .DE $E119
042 CONV      .DE $E200
043 SCAND     .DE $8906
044 F0        .DE $20
045 D0        .DE $32
046 TEST      .DE $E626
047 READ      .DE $E000
048 MOVE      .DE $E457
049 RESET     .DE $E467
050
E700- 20 86 8B 051 SOIL      JSR ACCESS          ;ACCESS TO RAM
E703- A2 06      052          LDX #06             ;WRITE START-UP
E705- BD 42 E7 053 LP3      LDA MESSGE-1,X        ;MESSAGE

```

E708-	9D	3F	A6	054	STA DISBUF-1,X	
E70B-	CA			055	DEX	
E70C-	D0	F7		056	BNE LP3	
				057		
E70E-	A9	06		058	LDA #06	
E710-	85	38		059	STA *PLIM	;INITIALIZE PLIM
E712-	20	AF	E5	060	JSR INIT	;INITIALIZE RAM
				061		
E715-	20	AF	88	062	JSR GETKEY	;SCAN AND POLL
				063		
E718-	C9	43		064	CMP #'C'	;DETERMINE COMMAND
E71A-	F0	2D		065	BEQ DISPF0	;INIT F
				066		
E71C-	C9	44		067	CMP #'D'	
E71E-	F0	30		068	BEQ DISPDO	;INIT D
				069		
E720-	C9	45		070	CMP #'E'	
E722-	F0	33		071	BEQ DISPFF	;FINAL F
				072		
E724-	C9	46		073	CMP #'F'	
E726-	F0	36		074	BEQ DISPFD	;FINAL D
				075		
E728-	C9	38		076	CMP #'8'	
E72A-	F0	39		077	BEQ DISBRK	;BREAK FORCE
				078		
E72C-	C9	39		079	CMP #'9'	
E72E-	F0	3C		080	BEQ DISPE	;ENERGY INTEGRAL
				081		
E730-	C9	41		082	CMP #'A'	
E732-	F0	41		083	BEQ CHANGE	;CHANGE PLIM
				084		
E734-	C9	42		085	CMP #'B'	
E736-	F0	61		086	BEQ SAMPLE	;DO TEST
				087		
E738-	C9	34		088	CMP #'4'	
E73A-	F0	63		089	BEQ SET	;SET TRANSDUCER
				090		
E73C-	C9	35		091	CMP #'5'	
E73E-	D0	D5		092	BNE MAIN	
E740-	4C	4A	8B	093	JMP \$8B4A	;TO SYM MONITOR
				094		
E743-	6D	3F	06	095	MESSGE	.BY \$6D \$3F \$06 \$38 \$00 \$06
E746-	38	00	06			
				096		
E749-	A2	20		097	DISPF0	
E74B-	A0	4D		098	LDX #F0	
E74D-	4C	C9	E7	099	LDY #FCONV	;SET UP TO DISPLAY F0
				100	JMP PUTOUT	;GO DISPLAY AND RETURN
E750-	A2	32		101	DISPDO	
E752-	A0	50		102	LDX #D0	;SETUP TO DISPLAY D0
E754-	4C	C9	E7	103	LDY #DCONV	;IN CM
				104	JMP PUTOUT	
E757-	A2	23		105	DISPFF	
					LDX #PASTF	;END FORCE FOUND HERE

E759-	A0 4D	106		LDY #FCONV	;IN KG
E75B-	4C C9 E7	107		JMP PUTOUT	
		108			
E75E-	A2 26	109	DISPFD	LDX #PASTD	;END DISP
E760-	A0 50	110		LDY #DCONV	;IN CM
E762-	4C C9 E7	111		JMP PUTOUT	
		112			
E765-	A2 3E	113	DISBRK	LDX #FMAX	;BREAK FORCE
E767-	A0 4D	114		LDY #FCONV	;IN KG
E769-	4C C9 E7	115		JMP PUTOUT	
		116			
E76C-	A2 47	117	DISPE	LDX #ESUM	;ENERGY INTEGRAL
E76E-	A0 53	118		LDY #ECONV	;IN JOULES
E770-	A9 04	119		LDA #04	;TO 4 PLACES
E772-	4C CB E7	120		JMP PUTOUT+2	
		121			
E775-	A6 38	122	CHANGE	LDX *PLIM	;DISPLAY OLD
E777-	BD 41 E3	123		LDA DIGIT,X	
E77A-	09 80	124		ORA #\$80	;PUT ON PT.
E77C-	8D 45 A6	125		STA \$A645	
		126			
E77F-	20 AF 88	127		JSR GETKEY	;CHANGE TO WHAT
E782-	38	128		SEC	
E783-	E9 30	129		SBC #\$30	;ASCII CONVERT
		130			
E785-	C9 04	131		CMP #04	;TEST FOR LEGAL RANGE
E787-	30 EC	132		BMI CHANGE	;IGNORE ILLEGAL
E789-	C9 0A	133		CMP #\$0A	;LEGAL= 4 TO 9
E78B-	10 E8	134		BPL CHANGE	
		135			
E78D-	85 38	136		STA *PLIM	;MAKE CHANGE
		137			
E78F-	AA	138		TAX	
E790-	BD 41 E3	139		LDA DIGIT,X	;ECHO IN DISPLAY
E793-	8D 45 A6	140		STA \$A645	
E796-	4C 15 E7	141		JMP MAIN	
		142			
E799-	20 26 E6	143	SAMPLE	JSR TEST	;PERFORM TEST
E79C-	4C 15 E7	144		JMP MAIN	
		145			
E79F-	A9 07	146	SET	LDA #07	;CONTINUOUS DISPLAY
E7A1-	A2 41	147		LDX #SCR1	
E7A3-	20 00 E0	148		JSR READ	;OF DISP
		149			
E7A6-	A2 41	150		LDX #SCR1	;IN CM
E7A8-	A0 50	151		LDY #DCONV	
E7AA-	20 19 E1	152		JSR MPY	
		153			
E7AD-	A9 03	154		LDA #03	;TO 3 PLACES
E7AF-	85 00	155		STA *00	
E7B1-	A2 41	156		LDX #SCR1	
E7B3-	20 00 E2	157		JSR CONV	
		158			

```

E7B6- A9 10      159      LDA #$10                ;DISPLAY DRIVE
E7B8- 85 FF      160      STA *$FF
E7BA- 20 06 89 161 DLOOP  JSR SCAND
E7BD- D0 07      162      BNE ARND                ;KEY PRESSED?
E7BF- C6 FF      163      DEC *$FF
E7C1- D0 F7      164      BNE DLOOP
E7C3- 4C 9F E7 165      JMP SET
                        166
E7C6- 4C 15 E7 167 ARND   JMP MAIN                ;DONE
                        168
E7C9- A9 03      169 PUTOUT LDA #03                ;DEFAULT 3 PLACES
E7CB- 48          170      PHA
E7CC- 98          171      TYA
E7CD- 48          172      PHA
E7CE- A0 41      173      LDY #SCR1                ;MOVE TO SCRATCH
E7D0- 20 57 E4 174      JSR MOVE
                        175
E7D3- 68          176      PLA
E7D4- A8          177      TAY
E7D5- A2 41      178      LDX #SCR1
E7D7- 20 19 E1 179      JSR MPY                ;UNIT CONVERSION
                        180
E7DA- 68          181      PLA
E7DB- 85 00      182      STA *00                ;FILL DISPLAY
E7DD- 20 00 E2 183      JSR CONV
E7E0- 4C 15 E7 184      JMP MAIN
                        185
E7E3- FF FF FF 186      .BY $FF $FF $FF $FF $FF $FF $FF $FF $FF
E7E6- FF FF FF
E7E9- FF FF FF
E7EC- FF FF FF 187      .BY $FF $FF $FF $FF $FF $FF $FF $FF $FF
E7EF- FF FF FF
E7F2- FF FF FF
E7F5- FF FF FF 188      .BY $FF $FF $FF $FF $FF $FF $FF
E7F8- FF FF FF
E7FB- FF
                        189
E7FC- 67 E4      190      .SE RESET                ;CHANGE RESET VECTOR
                        191
                        192 ;*****
                        193 .EN
END OF MAE PASS!

```

--- LABEL FILE: ---

ACCESS =8B86
 CONV =E200
 DIGIT =E341
 DISPDO =E750
 DISPPD =E75E
 ECONV =0053
 FCONV =004D
 INIT =E5AF

ARND =E7C6
 D0 =0032
 DISBRK =E765
 DISPE =E76C
 DISPFF =E757
 ESUM =0047
 FMAX =003E
 LP3 =E705

CHANGE =E775
 DCONV =0050
 DISBUF =A640
 DISPF0 =E749
 DLOOP =E7BA
 F0 =0020
 GETKEY =88AF
 MAIN =E715

MESSGE =E743
PASTD =0026
PUTOUT =E7C9
SAMPLE =E799
SET =E79F

MOVE =E457
PASTF =0023
READ =E000
SCAND =8906
SOIL =E700

MPY =E119
PLIM =0038
RESET =E467
SCR1 =0041
TEST =E626

//0000,E7FE,10FE

APPENDIX D

OPERATING INSTRUCTIONS

INTRODUCTION

This machine measures the energy required to crush soil samples as a first step in evaluating dry soil aggregate stability by an energy method. The system is sketched in Figure D.1.

Once the test is started, the computer periodically measures the force on the crushing platform and the displacement of the crushing plate. The force X displacement product is numerically integrated to find the total crushing energy. Measurements are taken many times per second so even small changes are detected. The force at which the sample first fractures is also recorded.

A typical crushing process plotted on force and displacement axes might look like Figure D.2.

The pertinent features on the graph are defined as follows:

F_0 is the initial force on the platform due to the weights of the platform and sample.

D_0 is the relative displacement of the crushing plate from its zero at the beginning of the test.

F_f is the force on the platform at the end of the test.

D_f is the relative displacement of the crushing plate from its zero at the end of the test.

The break force is defined as the force from which the force on the sample first drops 25 percent. This is shown on figure D.2.

The crushing energy is denoted by the shaded area.

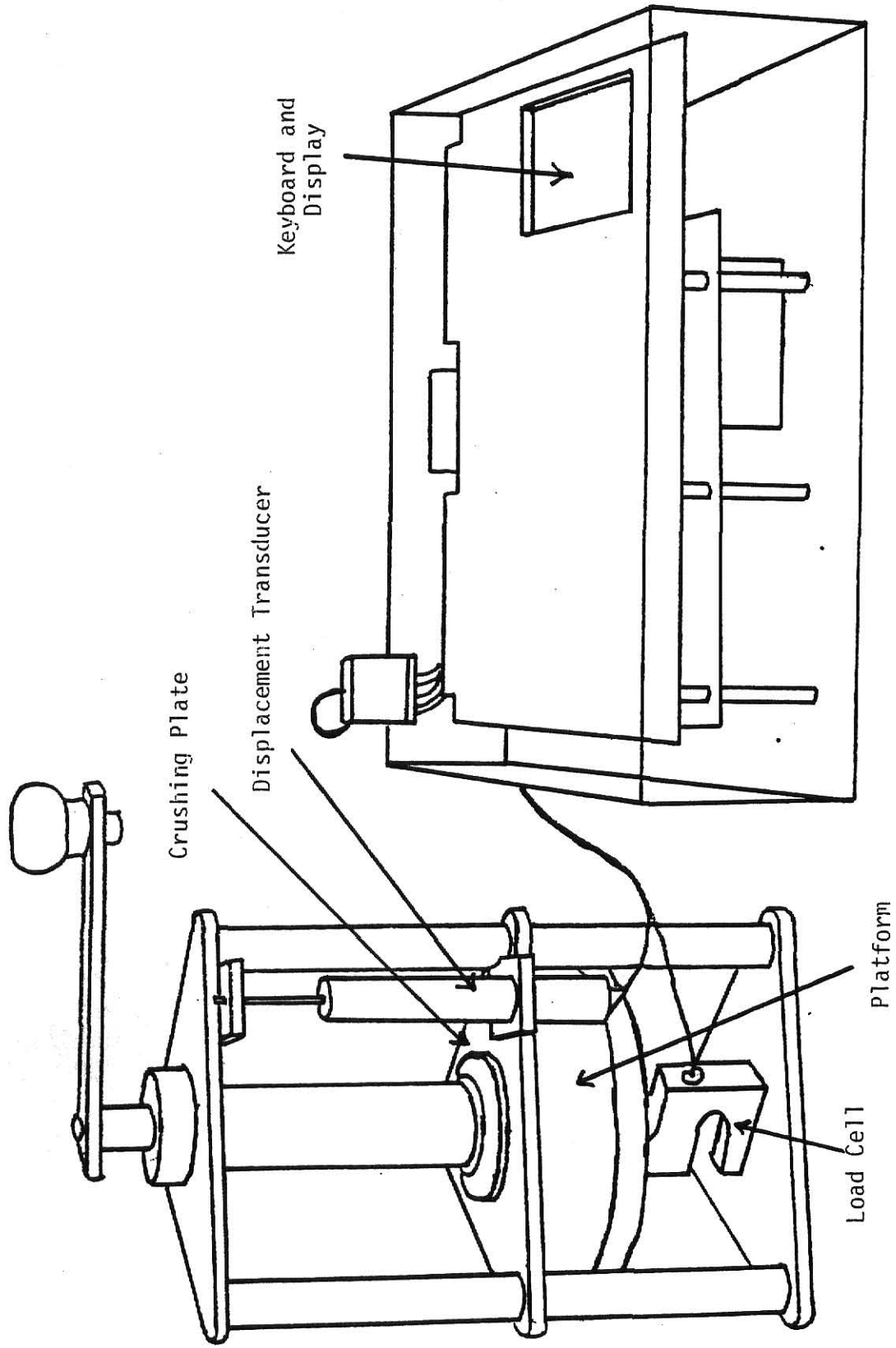


Figure D.1.
Sketch of SACEM System

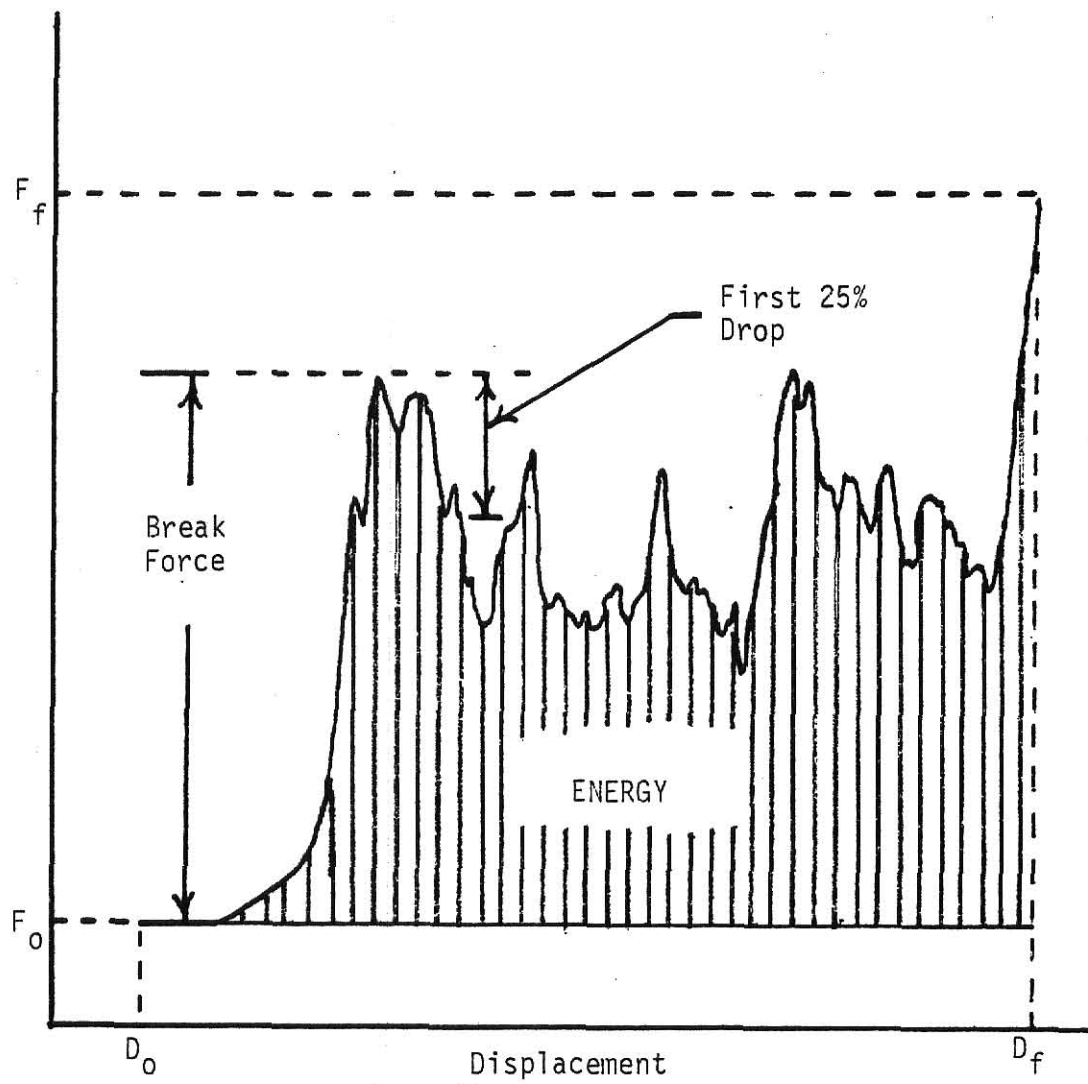


Figure D.2

Typical Soil Crushing Curve

OPERATION

The simplest method of testing is using the hand crank drive on the crushing vise. This is the configuration shown in Figure D.1. The instruments must be connected to the computer module through the connector provided and the computer module must be plugged into a standard 110 V outlet.

When power is supplied to the computer module, a short beep is sounded. After a delay of about two seconds (the computer uses this time for initialization), another tone is heard and the computer displays the message SOIL 1. The system is then ready for commands to be entered. Commands consist of single keystrokes. The computer responds immediately to each. The layout of the keyboard is shown in Figure D.3.

The first command used will probably be the

CURR DISP

 command. This instructs the system to display the current displacement of the crushing plate in centimeters. This function is provided to allow the displacement transducer to be adjusted to its proper position on the vise. To do this, gently close the vise until the crushing plate and the platform touch. There should be nothing between the plates during this procedure. When the plates are touching, press the

CURR DISP

 key. The value displayed should be between 2.40 and 2.50. If the value displayed is between 2.40 and 2.50 no adjustment is required. Pressing any other key will exit the command. If the display is not between 2.40 and 2.50 the displacement transducer must be adjusted as described below.

The displacement transducer can be adjusted in either of two different places. The connection to the top plate of the vise provides some adjustment. If that is not enough, the body of the transducer can be moved in its attachment to the crushing plate. The clamp must be loosened with an Allen wrench.

		RESET	
F_o	D_o	F_f	D_f
8 BREAK FORCE	9 ENERGY	CHANGE STOPF	RUN TEST
4 CURR DISP	5 SYM MON	6	7

Figure D.3
Keyboard Layout

Once the transducer is positioned, the system is ready to perform a test. The sample to be tested should be placed as nearly as possible in the center of the platform. It is important that the sample not be more than 2.4 cm high. If the sample is larger than this, erroneous readings may result.

When the sample is positioned and the vise is ready, press the

RUN TEST

 key. The display will go dark for about two seconds while the system is initialized, and then a tone will be sounded. Once the tone has sounded, the test is underway. The test may be aborted at any time by pressing any key on the keyboard.

The number displayed during the test is the current force on the platform in kilograms. This includes the weights of the platform and sample. Turning the hand crank counterclockwise will cause the crushing to start. The crank should be turned fairly slowly. To obtain a crushing speed of 10 mm/min as has been used in other work, each revolution of the crank must take about eight seconds.

When the initial break of the sample occurs, the upper element of the rightmost display digit is lighted as an indicator. When the break is found, the stop force is calculated as 1.5 times the break force. This relation can be changed.

As crushing continues, the force is compared with the calculated stop force. When the stop force is reached, a tone is sounded and sampling of the force and displacement is halted. Crushing should be stopped immediately.

It is possible that in some cases no break force is detected and thus no stop force is calculated. If this happens, there will be no signal to indicate the end of the test. In this event, crushing should be stopped as soon as it becomes obvious that the test has gone awry. If crushing is not stopped, it is possible that the vise could be damaged due to too high a crushing force. The computer is programmed to warn the operator with a series

of tones when the force gets dangerously high. If this happens, the test should immediately be stopped by pressing a key on the keypad and crushing should be stopped.

Once the test is ended, either by a keypress or because the stop force has been passed, several of the important values from the test can be recalled by commands from the keyboard. The quantities available are those defined on Figure D.2. For example, to find the force at which the sample broke, press the **BREAK FORCE** key. The value is displayed immediately in units of kilograms. When all the desired readings have been recorded, a new test may be started.

CHANGING THE STOP FORCE

A special command is provided to change the method of calculating the stop force. Whenever the computer is powered up or the **RESET** key is pressed, the factor for calculating the stop force from the break force is set to 1.5. This factor can be changed to any multiple of .25 between 1.0 and 2.25. To change it, press the **CHANGE STOPF** key. A number followed by a decimal point will appear in the rightmost digit of the display. This number indicates the current factor for calculating the stop force. The decimal point indicates that the computer is waiting for a new number to be keyed in.

The number is four times the stopping factor. For example, if a 7. appears, the current stopping factor is 1.75. To enter a new factor, press any key marked with a number between four and nine. Since the computer is expecting a number, any command associated with the key will not be executed. When a legal number has been entered, the new number appears in the display and the decimal point disappears to indicate that the change has been made. Any keys other than those marked with numbers four through nine are ignored.

ENTERING THE SYM MONITOR

The one remaining command allows the SYM computer monitor to be invoked. The system powers up to the soil testing monitor, but pressing the SYM
MON key will cause the SYM monitor to be entered. This allows all the capabilities of the SYM to be used. This is useful for testing any suspect hardware or software associated with the soil tester. Short routines may be written in RAM to exercise the section in question.

Anyone interested in using this feature should refer to the SYM-1 Reference Manual and the SYM-1 Programming Manual. An RS-232C connector is provided on the computer module to allow use of a CRT terminal. The computer is also supplied with a BASIC language. This is described fully in the Synertek BASIC Reference Manual.

COMMAND SUMMARY

This is a listing of all the keyboard commands and brief descriptions of their functions.

RESET Resets the computer. This is equivalent to disconnecting the power and powering back up. All data are lost and the system is re-initialized.

**CURR
DISP** Continually displays the current displacement of the crushing plate in centimeters. This is useful for positioning the crushing plate before a test and for adjusting the displacement transducer as described above. Pressing any other key exits the command.

**RUN
TEST** Starts a crushing test. It is assumed that the vise is properly set up. The current platform force in kilograms is displayed continually during the test. If the force gets too high (about 40 kg) the beeper is sounded each time the force and displacement are sampled but the

test continues. When the break force has been detected, the upper element of the rightmost display digit is also lighted. The stop force is calculated from the break force. When the stop force is passed, the beeper is sounded and control passes back to the monitor.

- F_0 Displays the force that was on the platform at the beginning of the last test run. If no test has been run, this is the force at the time the system was powered up. This reading includes the weights of the platform and sample.
- D_0 Displays the displacement of the crushing plate at the beginning of the last test run. If no test has been run, this is the displacement at the time the system was powered up. The units of the reading are centimeters.
- F_f Displays the force on the platform including the weights of the platform and sample, at the end of the past test run. If no test has been run, this is equal to F_0 . The units are kilograms.
- D_f Displays the displacement of the crushing plate at the end of the last test run. If no test has been run, this is equal to D_0 . The units are centimeters.
- BREAK
FORCE** Displays the force in kilograms at which the sample first fractured during the last test run. The weights of the platform and sample are not included. If no test has been run this value is zero. If no break was detected during the last test, this is equal to $F_f - F_0$.

ENERGY Displays the energy integral generated during the last test run. The value is in Joules. The effects of the platform and sample weights have been taken out. If no test has been run, this value is zero.

CHANGE
STOPF Allows changing the method of calculating the force at which to stop the test. The force is determined from the break force. When the force on the sample is large enough relative to the break force, the test is stopped. On power up the relation is set so that the stop force is 1.5 times the break force. This factor can be changed to any multiple of 0.25 between 1.0 and 2.25. When the command is entered, a number equal to four times the current factor appears in the right most digit of the display followed by a decimal point. The decimal point indicates that the computer is waiting for a new number to be entered. A key marked with a number between four and nine must then be pressed. The new number (four times the new stopping factor) then appears in the display and the decimal point disappears to indicate that the change has been made.

SYM
MON Causes a cold start of the SYM monitor. All of the SYM capabilities are available for use. Complete instructions for the SYM computer can be found in the SYM-1 Reference Manual.

RUNNING PARALLEL TESTS WITH THE INSTRON

The crushing vise may be mounted in the Instron testing machine. This allows both machines to measure the same sample for calibration purposes and to enhance the output capabilities of the Instron. One extra fitting is required. The parallel system is sketched in Figure D.4. The crank drive must be removed from the vise and the adapter shaft threaded into its place.

The upper end of the adapter fits into the load cell fitting on the Instron. The crushing motion is generated by the crosspiece of the Instron so it is important that the operator be careful not to exceed the force limit of the vise. A headless bolt may also be threaded into the adapter shaft instead of mounting it on the load cell fitting. This allows the vise to be mounted in a drill press or other machine to generate the crushing motion.

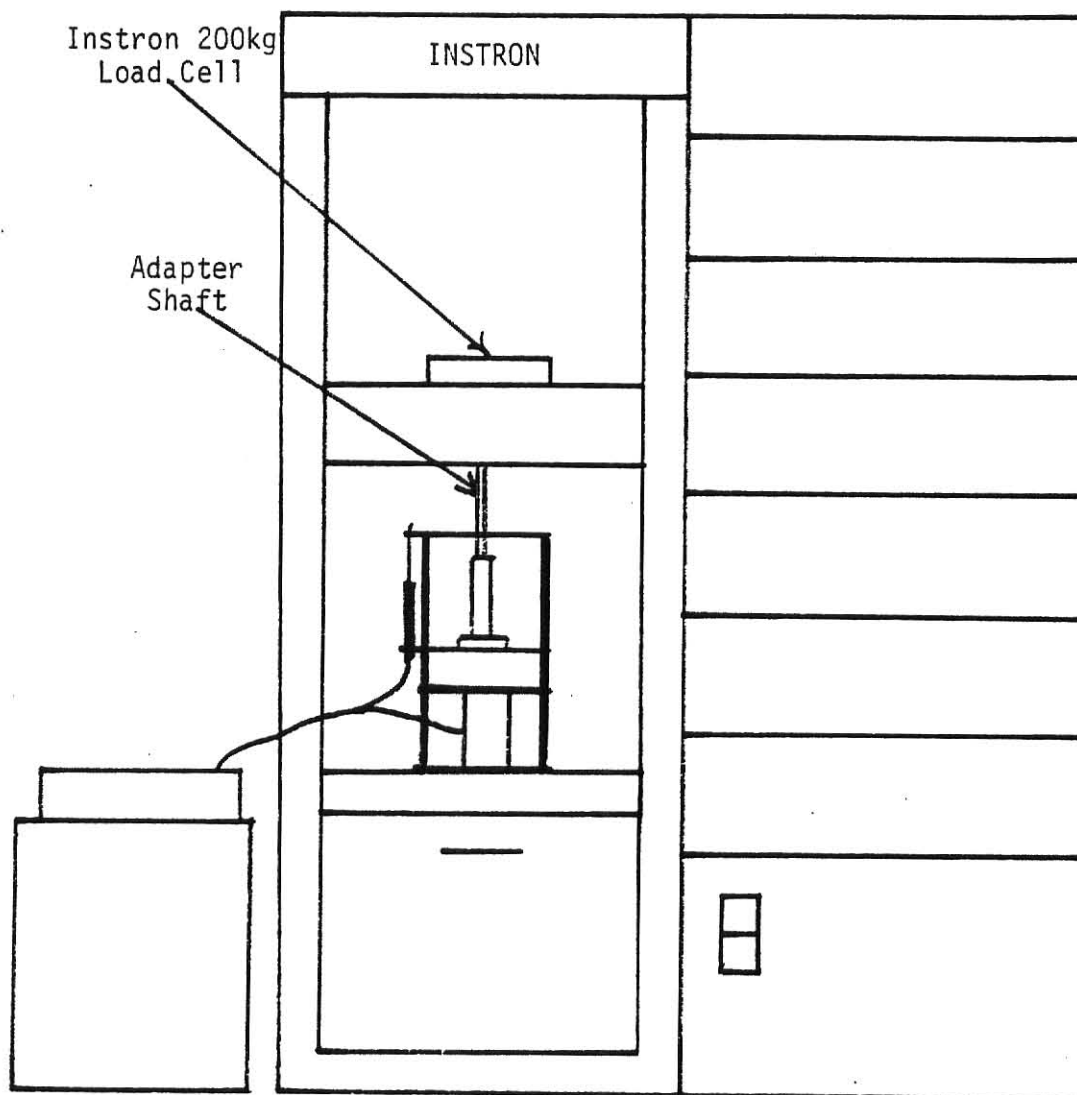


Figure D.4

Running Parallel Tests with the Instron

VITA

David W. Boyd

Candidate for the Degree of

MASTER OF SCIENCE

Thesis: A Soil-Aggregate Crushing-Energy Meter

Major Field: Mechanical Engineering

Biographical:

Personal Data: Born in Belleville, Kansas, February 13, 1959, the son of Mr. & Mrs. Joseph A. Boyd.

Educational: Graduated from Trego Community High School in May, 1977. Received a Bachelor of Science degree in Mechanical Engineering from Kansas State University in May, 1981. Completed the requirements for the Master of Science degree in Mechanical Engineering at Kansas State University in May, 1982.

A SOIL-AGGREGATE
CRUSHING-ENERGY METER

by

DAVID WAYNE BOYD

B.S. Kansas State University, 1981

AN ABSTRACT OF A THESIS

submitted in partial fulfillment of the
requirements for the degree

MASTER OF SCIENCE

Department of Mechanical Engineering
KANSAS STATE UNIVERSITY
Manhattan, Kansas

1982

Soil aggregate stability is an important measurement in determining soil properties. One current method of evaluating soil aggregate stability involves measuring the energy required to crush a soil aggregate and the new surface area generated. The purpose of this work was to develop a new technique for measuring the energy of crushing. Criteria for the improved system were that the system 1) measure the energy quickly and accurately, 2) provide a digital readout in the proper units, 3) perform tests both independently and in parallel with existing equipment, 4) record the force on the sample at its initial fracture, and 5) be portable. The system developed consists of two basic parts. A small crushing vise was constructed which can be hand driven or mounted in existing test equipment. A computer module measures the force on the sample and the displacement more than 20 times per second using a load cell and displacement transducer mounted on the vise. The force-displacement product is numerically integrated using a trapezoidal algorithm to find the crushing energy. The entire system fits easily into a carrying case about the size of a small suitcase. The design criteria were met and measurements taken by the new system showed excellent agreement with previous methods.