APPLICATIONS OF NONPARAMETRIC STATISTICS TO MULTICOMPONENT SOLIDS MIXING

by

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I. INTRODUCTION

Solids mixing or blending is an operation by which two or more particulate solid materials are scattered randomly in a mixer by the random movement of the particles. Solids mixing tends to eliminate existing inhomogeneities, or to reduce gradients. Although it is one of the oldest industrial operations, it is still one of the most widely employed. For example, it is essential in plastic processing, ore smelting, pharmaceutical preparation, fertilizer production, food manufacture, and catalytic synthesis of chemicals. Generally, solids mixing operations are often multicomponent in nature in that each of such operations involves blending of more than two ingredients. Thus, the study of solids mixing for multicomponent mixtures is of practical importance.

Statistical analysis has been a major tool in solids mixing investigations because of the stochastic nature of mixing processes. The statistical properties of a multicomponent heterogeneous solids mixture have been of intense interest to researchers in the field of solids mixing, yet a systematic approach to this problem is still lacking.

The theory of nonparametric methods is essentially concerned with the development of statistical inference procedures without the explicit assumptions regarding the functional form of the probability distribution of the sample observations. Since the distributions of the components during mixing are usually unknown, nonparametric statistical methods should provide a class of appropriate and effective techniques for the analysis of mixing systems. The applications of certain nonparametric tests for solids mixing for binary mixtures has been previously demonstrated by Lai, Wang and Fan [1].

The object of this study is to demonstrate the applicability of nonparametric statistics to the analysis of mixing processes of multicomponent
mixtures and the characterization of such mixtures. As specific examples, the
mixing processes carried out in a drum mixer and several mixtures generated
by the processes are considered.

II. NONPARAMETRIC STATISTICS

In most statistical problems, a class of distributions or states of nature assumed as possible models is defined by a probability density function of given form, which depends on a finite number of real parameters. In other words, if the basic distribution is known, one may be able to derive optimal tests of hypotheses and confidence intervals based on the distribution. In many case an experimenter does not know the form of the basic distribution and is in need of statistical techniques which are applicable regardless of the form of the density. These techniques are called nonparametric or distribution-free methods.

The term "distribution free" refers to the fact that no assumptions are made about the underlying distribution except that the distribution function being sampled is absolutely continuous or purely discrete. The term "nonparametric" refers to the fact that there are no parameters involved in the traditional sense. The restriction to absolutely continuous distribution function is a simplifying assumption that allows us to use the fact that ties occur with probability 0. They apply to very wide families of distributions rather than only to families specified by a particular functional form.

In nonparametric statistics, the measurement scale need not be numerical.

Usually measurements can be classified as one of four levels depending on the precision represented by the measurement procedure. They are

(1). Nominal scale: In nominal (scale) measurements no physical meaning is attached to the values of the numbers. We simply assign numerical names to the types of outcomes, however the principle of order in real number system is not relevant. Of the four measurement scales, nominal is the least precise.

- (2). Ordinal or ranking scale: When measurements are made on an ordinal scale, the elements can be arranged in a meaningful order, which corresponds to their relative positions or sizes. In a taste test for five different brands of beer, the tasters may rank beers as 1, 2, 3, 4, and 5 according to their preferences. Note that the rank does not indicate how much better one beer is preferred.
- (3). Interval scale: When the elements can be ordered and the arithmetic difference between the elements is meaningful, the data are measured on an interval scale. Thus, we can say not only that one element is larger than or smaller than another, but also by how much. This scale of measurement is much more informative than either of the scales above, since the fact that the distance between elements can be determined implies that there is a fixed unit of measurement and a zero point, the latter being arbitrary. Thus, interval scale data are quantitative in the sense, that the numbers have a true meaning.
- (4). Ratio scale: For ratio scale measurements we have not only the order property, a unit of measurement and a meaningful arithmetic difference between elements, but also a fixed origin or zero point as opposed to an arbitrary origin. The term "ratio scale" is used because the ratio of two measurements on this highest scale is meaningful.

The validity of the nonparametric statistical inference does not rest on a specific probability model in the population. Nonparametric procedures exist for data from all four scales of measurements. Such procedures are very useful in many different areas of application. Nonparametric methods can be applied to test a variety of hypotheses. According to types of inferences, the major nonparametric statistical tests are summarized below:

- Goodness-of-Fit Tests
 Chi-square test, Kolmogorov-Smirnov test
- Tests of Location or Central Tendency
 Sign test, Wilcoxon signed rank test, Mann-Whitney-Wilcoxon test,
 Normal scores Van der Waerden test, Kruskal-Wallis test, Friedman test.
- Tests of Scale or Dispersion
 Siegel-Tukey test, Klotz test, Ansari-Bradley test, Mood test.
- 4. General Distribution Tests
 Equality of k proportions test, Chi-square test, Kolmogorov-Smirnov
 test.
- Association Analysis
 Spearman test, Kendall Tau test, Chi-square test.
- Tests for Randomness or Trend
 Ordinary runs test, Runs up and down test.

Table 1 gives some available nonparametric tests depending on types of samples obtained and types of measurements involved. For further details, we may be referred to some nonparametric statistics texts such as Gibbons [2,3], Conover [4], Lehmann [5], Hájek [6] or Hollander and Wolfe [7]. Note that we may be referred to Puri and Sen [8] for nonparametric multivariate methods.

Besides the advantage of robustness against distributional assumptions, nonparametric statistical methods often involve less computational work, and therefore, are easier and quicker to apply than other statistical methods. Another advantage of nonparametric statistical techniques is that much of their theory may be developed rigorously using elementary combinatorial mathematics.

THIS BOOK CONTAINS NUMEROUS PAGES WITH DIAGRAMS THAT ARE CROOKED COMPARED TO THE REST OF THE INFORMATION ON THE PAGE. THIS IS AS RECEIVED FROM

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Table 1. A brief chart for testing hypotheses and the appropriate nonparametric test

		Type of measurement involved	pa	
Type of sample obtained	Hypothesis test involving	Nominal (observations may be separated according to categories)	Ordinal* (observations may be arranged from smallest to largest)	Interval (the numerical value of the observation has meaning)
One random sample Means (medians)	Means (medians)	Binomial test	Quantile test	Wilcoxon test
$^{\Lambda_1, \Lambda_2, \ldots, \Lambda_n}$	(Conf.int. for means)	Conf. int, for p	Conf. int. for x	Conf. int. for mean
	Nonrandomness	Wald-Wolfowitz test	Cox and Stuart test Spearman's rho	
	Goodness-of-fit	Chi-square test	Kolmogorov test Cramer-von Mises test Lilliefors test	
	Cond. band for F(x)		Cond. band for F(x)	
Paired observa- tions, or two	Means (medians)	McNemar test	Sign test	Wilcoxon test Randomization test
matched samples $(X_1, Y_1), \ldots, (X_n, Y_n)$	(Conf. int. for diff. between means)	Conf. int. for p	Conf. int. for x	Conf. int, for diff.
=	Independence	Chi-sauare test Fisher's test	Sign test Bell-Doksum test Olmstead-Tukey test	
	•			

Table 1---continued

	Randomization test	
Friedman test Bell-Doksum test	Mann-Whitney test Tukey's quick test Mann-Whitney Conf. int. Tukey's conf. int. Siegel-Tukey test Smirnov test Cramer-von Mises test Wald-Wolfwitz test Kruskal-Wallis test Bell-Doksum test Slippage test Birnbaum-Hall test	Median test extended Durbin test for BIBD
Cochran test	Chi-square test	Many-way contingency table
Means	Means (medians) (Conf. int. for diff. between means) Variances Identical distributions Means (medians)	Means (medians)
Multivariate observa- tions, or the random- ized complete block design	Two random samples, X ₁ ,X ₂ ,,X _n and Y ₁ ,Y ₂ ,,Y _m . (see also tests for several random samples) Several random samples	Other types

* The methods listed under Nominal may also be used here.

 ** The methods listed under Nominal and Ordinal may also be used here.

III. THEORY

Consider a mixture which has (m+1) components. For the trivial case (m=1), the mixture is called binary. In this paper, we are particularly interested in the nontrivial case where m>1. Let X_{ij} be a random variable denoting the weight fraction of the i-th component in the j-th spot sample $(i=1, 2, \ldots, m+1; j=1, 2, \ldots, n)$. Since

only m of (m+1) weight fractions need to be determined. Thus,

$$\underline{X}_{i} = [X_{1i} \ X_{2i} \ . \ . \ X_{mi}]', \qquad j = 1, 2, ..., n$$
 (1)

will denote an arbitrary selection of m weight fractions for a given sample. Several nonparametric statistical methods, which can be applied in analyzing a variety of sampling results of multicomponent solids mixing, are presented in this section.

1. One-Sample Location Problem

In many mixing problems, the true component proportions in a mixture are known. The problem of interest then becomes a test of the sampling procedure. If sampling is random throughout the mixture, the sample mean vector should be representative of the population and the sample mean vector should not be significantly different from the specified component proportions. Multivariate rank tests for the one-sample location problem [8] are thus appropriate for a test of the sampling procedure.

Suppose that n spot samples are taken from a mixture. Let \underline{x}_j (j = 1, 2, ..., n) be a random sample (vector-valued) with a continuous cumulative distribution $F(\underline{x})$, $\underline{x} \in \mathbb{R}^m$, where \mathbb{R}^m is the set of all m-tuples $\underline{x} = [x_1 \ x_2 \dots x_m]'$. $F(\underline{x})$ may be written as

$$F(x) = F(x, \mu) \tag{2}$$

where $\underline{\mu} = \begin{bmatrix} \mu_1 & \mu_2 & \dots & \mu_m \end{bmatrix}$ is a location (vector) parameter. The random (mxn) matrix takes the form

$$[\underline{x}_1 \quad \underline{x}_2 \quad \cdots \quad \underline{x}_n]$$

$$= \begin{bmatrix} x_{11} & x_{12} & \dots & x_{1n} \\ x_{21} & x_{22} & \dots & x_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ \vdots & \vdots & \ddots & \vdots \\ x_{m1} & x_{m2} & \dots & x_{mn} \end{bmatrix}$$
(3)

We now derive a test of the null hypothesis

$$H_0: \quad \underline{\mu} = \underline{\mu}_0 \tag{4}$$

against the alternative hypothesis

$$H_1: \underline{\mu} \neq \underline{\mu}_0$$

where $\underline{\mu}_0 = [\mu_{10} \ \mu_{20} \ \dots \ \mu_{m0}]$ ' is a specified vector. Let

$$Y_{ij} = X_{ij} - \mu_{i0}$$
 (5)

denote the adjusted sample values, then the random sample matrix becomes

$$\underline{z}_{n} = \begin{bmatrix}
Y_{11} & Y_{12} & \dots & Y_{1n} \\
Y_{21} & Y_{22} & \dots & Y_{2n} \\
\vdots & \vdots & \ddots & \vdots \\
Y_{m1} & Y_{m2} & \dots & Y_{mn}
\end{bmatrix}$$
(6)

Ranking the n elements in each row of $\frac{Z}{n}$ in increasing order of their absolute value, we obtain an $(m \times n)$ rank matrix

$$\frac{R}{n} = \begin{bmatrix}
R_{11} & R_{12} & \cdots & R_{1n} \\
R_{21} & R_{22} & \cdots & R_{2n} \\
\vdots & \vdots & \ddots & \vdots \\
R_{m1} & R_{m2} & \cdots & R_{mn}
\end{bmatrix} (7)$$

where R_{ij} is the rank of $|Y_{ij}|$ (j = 1, 2, ..., n) among the set $\{|Y_{i1}|, |Y_{i2}|, \ldots, |Y_{in}|\}$. Since the populations are assumed continuous, the probability of a tie is zero. Then for each i (i = 1, 2, ..., m), we replace the ranks 1, 2, ..., n in the i-th row of $\frac{R}{n}$ by a set of general scores denoted by

$$\{E_{j}^{(i)}, j = 1, 2, ..., n\}$$

Hence, we obtain an $(m \times n)$ matrix of general scores $\frac{E}{n}$ corresponding to $\frac{R}{n}$:

$$\underline{E}_{n} = \begin{bmatrix} E_{R_{11}}^{(1)} & E_{R_{12}}^{(1)} & \cdots & E_{R_{1n}}^{(1)} \\ E_{R_{21}}^{(2)} & E_{R_{22}}^{(2)} & \cdots & E_{R_{2n}}^{(2)} \\ \vdots & \vdots & \ddots & \vdots \\ \vdots & \vdots & \ddots & \vdots \\ E_{R_{m1}}^{(m)} & E_{R_{m2}}^{(m)} & \cdots & E_{R_{mn}}^{(m)} \end{bmatrix}$$

$$(8)$$

We refer the reader to Chapter 4 of Puri and Sen [8] for a detailed discussion of the regularity conditions on a score generating function which determines the constants $E_{j}^{(i)}$.

We now consider a univariate rank order statistic for each coordinate (component) of the form

$$T^{(i)} = \sum_{j=1}^{n} E_{R_{ij}}^{(i)} C_{ij}$$
(9)

where C_{ij} = 1 or -1 according as Y_{ij} > 0 or Y_{ij} < 0, respectively. Therefore, $T^{(i)}$ is the difference of the sum of the scores $E_{j}^{(i)}$ for which Y_{ij} > 0 and the sum of those for which Y_{ij} < 0.

Let

$$T = [T^{(1)} T^{(2)} ... T^{(m)}]$$
 (10)

Under the null hypothesis, eqn. (4), the mean and dispersion matrix of \underline{T} are

$$E[T] = 0 \tag{11}$$

and

$$E[\underline{T'T}] = n\underline{V} = n[v_{\underline{i}\,\ell}]_{m\times m} \tag{12}$$

where

$$\mathbf{v}_{i\ell} = \frac{1}{n} \sum_{j=1}^{n} E_{R_{ij}}^{(i)} E_{R_{\ell j}}^{(\ell)} C_{ij} C_{\ell j},$$

$$i, \ell = 1, 2, ..., m$$
(13)

Note that

$$\mathbf{v}_{ii} = \frac{1}{n} \sum_{j=1}^{n} [E_{R_{ij}}^{(i)}]^2, \qquad i = 1, 2, ..., m$$
 (14)

The test statistic, S, formed by

$$S = \frac{1}{n} \left[\underline{T} \ \underline{V}^{-1} \ \underline{T}' \right] \tag{15}$$

is asymptotically distributed as a chi-square random variable with m degrees of freedom for large samples. If \underline{T} is stochastically different from $\underline{0}$, S will be large which will lead us to reject the null hypothesis. The appropriate P-value [see Appendix A] is the probability that a chi-square variable is greater than or equal to the observed value of S, that is, a right tail probability.

Two special cases are considered in this paper for the one-sample location problem. First, setting

$$E_{j}^{(i)} = 1, \qquad i = 1, 2, ..., n; \quad j = 1, 2, ..., n$$
 (16)

the test statistic, S, is the multivariate sign test. Second, if

$$E_{j}^{(i)} = \frac{j}{n+1}, \quad i = 1, 2, ..., m; \quad 1 \le j \le n$$
 (17)

then S reduces to the multivariate generalization of the one sample Wilcoxon signed rank statistic.

2. Test of Homogeneity of Dispersion Matrices

The degree of mixedness is used to judge the difference between various experimental situations (treatments). For example, we may be interested in comparing different types of mixers, mixing speeds or mixing times.

The covariance (dispersion) matrix characterizes the degree of dispersion of each component proportion. Therefore in testing for the homogeneity (or equality) of several dispersion matrices, we may be able to judge whether their degrees of mixedness are significantly different. In other words, we may determine if the variation in composition among spot samples of each treatment is identical. A multivariate nonparametric test of the equality of dispersion matrices discussed in [8] is used to assess treatment effects.

Suppose that we wish to compare the effects among t treatments. All t treatments are assumed to be mutually independent. The number of spot samples for the treatment k is denoted by n_k . Let $X_{ij}^{(k)}$ be a random variable representing the weight fraction of the i-th component in the j-th sample for the treatment k. Also let

$$\underline{x}_{j}^{(k)} = [x_{1j}^{(k)} \ x_{2j}^{(k)} \ \dots \ x_{mj}^{(k)}]', \quad j = 1, 2, \dots, n_{k}$$
 (18)

be n_k independent and identically distributed (vector-valued) random variables having a m-variate absolutely continuous cumulative distribution function (c.d.f.) $F^{(k)}(\underline{x})$ for k = 1, 2, ..., t.

Assuming the identity of locations, we test the hypothesis of the equality of dispersion matrices, i.e.

$$H_0: \underline{\Sigma}^{(1)} = \underline{\Sigma}^{(2)} = \dots = \underline{\Sigma}^{(t)}$$
 (20)

against the alternative hypothesis

$$H_1: \underline{\Sigma}^{(1)}, \underline{\Sigma}^{(2)}, \ldots, \underline{\Sigma}^{(t)}$$
 are not all identical.

Let

$$\begin{array}{ccc}
 & t \\
 & N = \sum n \\
 & k=1
\end{array}$$

denote the total number of observations

$$\underline{X}_{j}^{(k)}$$
, $j = 1, 2, ..., n_{k}$; $k = 1, 2, ..., t$

and define

$$\underline{Z}_{N} = \begin{bmatrix} x_{11}^{(1)} & x_{12}^{(1)} & \dots & x_{1n_{1}}^{(1)} & x_{12}^{(2)} & \dots & x_{1n_{2}}^{(2)} & \dots & x_{11}^{(t)} & x_{12}^{(t)} & \dots & x_{1n_{t}}^{(t)} \\ x_{21}^{(1)} & x_{22}^{(1)} & \dots & x_{2n_{1}}^{(1)} & x_{22}^{(2)} & \dots & x_{2n_{2}}^{(2)} & \dots & x_{21}^{(t)} & x_{22}^{(t)} & \dots & x_{2n_{t}}^{(t)} \\ \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots & \vdots & \vdots \\ x_{m1}^{(1)} & x_{m2}^{(1)} & \dots & x_{m1_{1}}^{(1)} & x_{m1}^{(2)} & x_{m2}^{(2)} & \dots & x_{mn_{2}}^{(2)} & \dots & x_{m1}^{(t)} & x_{m2}^{(t)} & \dots & x_{mn_{t}}^{(t)} \end{bmatrix}$$

$$(21)$$

a random matrix of dimension (mxN). Ranking the N elements in each row of \underline{z}_N in increasing order of magnitude, we obtain an (mxN) rank matrix

$$\underline{R}_{N} = \begin{bmatrix} R_{11}^{(1)} & R_{12}^{(1)} & \dots & R_{1n_{1}}^{(1)} & R_{12}^{(2)} & \dots & R_{1n_{2}}^{(2)} & \dots & R_{11}^{(t)} & R_{12}^{(t)} & \dots & R_{1n_{t}}^{(t)} \\ R_{21}^{(1)} & R_{22}^{(1)} & \dots & R_{2n_{1}}^{(1)} & R_{21}^{(2)} & R_{22}^{(2)} & \dots & R_{2n_{2}}^{(2)} & \dots & R_{21}^{(t)} & R_{22}^{(t)} & \dots & R_{2n_{t}}^{(t)} \\ \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots & \vdots & \vdots \\ R_{m1}^{(1)} & R_{m2}^{(1)} & \dots & R_{mn_{1}}^{(1)} & R_{m2}^{(2)} & \dots & R_{mn_{2}}^{(2)} & \dots & R_{m1}^{(t)} & R_{m2}^{(t)} & \dots & R_{mn_{t}}^{(t)} \end{bmatrix}$$

$$(22)$$

where the possibility of ties may be ignored in probability by virtue of the continuity of the c.d.f.'s. For each i (i = 1, 2, ..., m), we replace the ranks in the i-th row of \underline{R}_N by a set of general scores

$$E_{j}^{(1)} = \sqrt{12} \left(\frac{j}{N+1} - \frac{1}{2} \right), \quad j = 1, 2, ..., N$$
 (23)

and obtain the corresponding score matrix

Now, let us define

$$U_{i\ell}^{(k)} = \frac{1}{n_{k}-1} \left\{ \begin{array}{l} n_{k} \\ \sum E_{(k)}^{(1)} E_{(k)}^{(\ell)} - \frac{1}{n_{k}} \begin{bmatrix} n_{k} \\ \sum E_{(k)}^{(1)} \end{bmatrix} \begin{bmatrix} n_{k} \\ \sum E_{(k)}^{(\ell)} \end{bmatrix} \begin{bmatrix} n_{k} \\ \sum E_{(k)}^{(\ell)} \end{bmatrix} \right\}$$
(25)

$$i \le k = 1, 2, ..., m;$$
 $k = 1, 2, ..., t$

and

$$U_{i\ell}^{*} = \frac{1}{N-1} \left\{ \begin{array}{ccc} t & n_{k} & & \\ \Sigma & \Sigma & E^{(i)} & E^{(\ell)} & - & N & \overline{E}^{(i)} & \overline{E}^{(\ell)} \\ k=1 & j=1 & R_{ij}^{(k)} & R_{\ell j}^{(k)} & & \end{array} \right\}$$
(26)

where

$$\bar{E}^{(i)} = \frac{1}{N} \sum_{k=1}^{T} \sum_{j=1}^{n_k} E^{(i)}_{(k)}$$
(27)

Furthermore, let

$$v_{i\ell,i'\ell'}(\underline{R}_{N}) = \frac{1}{N} \sum_{k=1}^{t} \sum_{j=1}^{n_{k}} E_{(k)}^{(i)} E_{(k)}^{(\ell)} E_{(k)}^{(\ell)} E_{(k)}^{(\ell')} E_{(k)}^{(\ell')}$$

$$- v_{i\ell}^{*} v_{i'\ell'}^{*}, \quad i, i', \ell, \ell' = 1, 2, ..., m \quad (28)$$

Setting

$$r = \frac{1}{2}$$
 (i-1) (2m-i) + l for $i \le l = 1, 2, ..., m$

we rewrite

$$\{U_{i,\ell}^{(k)}, i \le \ell = 1, 2, ..., m\}$$

F		THE CONTRACT WATER AND THE CONTRACT OF THE CON		- Personal	-,	AND THE PERSON NAMED AND ADDRESS OF THE PERSON NAMED AND ADDRE							
ı	E(1) R(t) R _{1nt}	E(2) R(t) R _{2n₂}	•	•	•	$\mathbf{E}_{\mathbf{R}}^{(\mathbf{m})}$							
	•	•			•	•							
	$E_{12}^{(1)}$	$\mathbf{E}_{\mathbf{R}(\mathbf{t})}^{(2)}$			•	$\mathbf{E}_{\mathbf{R}}^{(m)}$							
	$\mathbf{E}_{\mathbf{R}_{11}}^{(1)}$	$E_{R(t)}^{(2)}$				$\frac{\mathrm{E}^{(\mathrm{m})}}{\mathrm{R}^{(\mathrm{t})}}$							
		•	: • :		•	•							
	$\frac{E}{R_{1n_2}^{(1)}}$	$E_{\rm R(t)}^{(2)}$:••		•	$E_{R(2)}^{(m)}$ $E_{R(2)}$							
	•	:	•	*	•								
	E(1) R ₁₂	$\frac{E}{R_{22}^{(2)}}$	•	•		E(m) R(2) m2							
	(1) R(2) F11	$\frac{{ m E}(2)}{{ m R}(2)}$	•	~		E(m) R(2) m1							-
	$\frac{E}{R_{1n_1}}^{(1)}$	$\frac{E(2)}{R_{2n_1}}$				$\mathbf{E}_{\mathbf{R}}^{(\mathbf{m})}$			todana v _{odan} t				N × G
	•	:		•	•	•	$\frac{1}{2} \frac{1}{2N}$. 1	. 1 1	•	•	•	. 1 1
	$\binom{(1)}{R_{12}^{(1)}}$	$\frac{\mathrm{E}^{(2)}}{\mathrm{R}^{(1)}_{22}}$				$\frac{\mathrm{E}(\mathrm{m})}{\mathrm{R}_{\mathrm{m}2}}$	Z.		•		•		
1	$E_{(1)}^{(1)}$ $E_{(1)}^{(1)}$ $E_{11}^{(1)}$ $E_{12}^{(1)}$	E(2) E R(1) E	*	***		$\begin{bmatrix} \mathbf{E}^{(\mathbf{m})} \\ \mathbf{E}^{(1)} \\ \mathbf{m} \end{bmatrix}$	T T T T T T T T T T T T T T T T T T T	1	1	•	•	•	1 1
L	<u>ы</u>			•	•	<u> </u>	= 112			•		•	二
		₩. "						,	N N				

as

$$\underline{\underline{U}}^{(k)} = \{\underline{U}_r^{(k)}, \quad r = 1, 2, ..., \frac{1}{2} m (m+1)\}$$
 (29)

and

$$\{U_{i,\ell}^*, i \leq \ell = 1, 2, ..., m\}$$

as

$$\underline{\underline{U}}^* = \{\underline{U}_r^*, \qquad r = 1, 2, ..., \frac{1}{2} m (m+1)\}$$
 (30)

and

$$\underline{\mathbf{v}}_{\mathbf{N}}(\underline{\mathbf{R}}_{\mathbf{N}}) = [\mathbf{v}_{\mathbf{r}s} \ (\underline{\mathbf{R}}_{\mathbf{N}})], \ \mathbf{r}, \mathbf{s} = 1, \ 2, \ \dots, \ \frac{1}{2} \mathbf{m} \ (\mathbf{m}+1)$$
 (31)

Thus, the test statistic can be expressed as

$$L = \sum_{k=1}^{t} n_{k} \left[\underline{\underline{u}}^{(k)} - \underline{\underline{u}}^{*} \right] \underline{\underline{v}}_{N}^{-1} \left(\underline{\underline{R}}_{N} \right) \left[\underline{\underline{u}}^{(k)} - \underline{\underline{u}}^{*} \right], \tag{32}$$

Under the null hypothesis, eqn. (20), the test statistic L (for large samples) is asymptotically distributed as a chi-square random variable with ν degrees of freedom, where

$$v = \frac{1}{2} m(m+1) (t-1)$$
 (33)

The P-value for this test is a right tail probability from a chi-square distribution table with the appropriate degrees of freedom.

Distribution-free Tests of Fit

Besides testing hypotheses concerning parameters of location and dispersion we are often interested in the validation of a specified distribution.

The goodness-of-fit problem in this multivariate setting may be described as follows:

Let \underline{x}_1 , \underline{x}_2 , ..., \underline{x}_n be independent multivariate random variables with the distribution function F(x). We wish to test the hypothesis

$$H_{0}: F(\underline{x}) = F_{0}(\underline{x}) \tag{34}$$

against the alternative

$$H_1: F(\underline{x}) \neq F_0(\underline{x})$$

where $F_0(\underline{x})$ is some particular distribution function (either continuous or discrete). We can distinguish two special cases for tests of fit:

(i) Simple null hypotheses

Under a simple null hypothesis, the distribution of the random variable is completely specified by $F_0(\underline{x})$.

(ii) Composite null hypotheses

Under a composite null hypothesis, the distribution of the random variable is not completely determined by $F_0(\underline{x})$. If a composite null hypothesis depends upon unknown parameters, their maximum likelihood estimators [9] are usually used to derive the appropriate test.

When samples are obtained in a multicomponent solids mixing problem, the data can be expressed as

component sample	1	2		_•_	•	m	m+1
1	f 11	f ₁₂	•	() • (f _{lm}	f _{1(m+1)}
2	f ₂₁	f ₂₂	•	•	•	f _{2m}	f _{2(m+1)}
•	•	•	•			•	
•	•	•		٠			•
•	•	•			•	•	•
n	f _{nl}	f_{n2}	16 8	٠		f _{nm}	f n(m+1)

where f_{ij} (i = 1, 2, ..., (m+1); j = 1, 2, ..., n) denotes the number of particles of the i-th component in the j-th spot sample. If the samples are taken from a specified distribution, the expected number of particles of the i-th component in the j-th sample will be known and denoted by e_{ij} .

Furthermore, under the null hypothesis, eqn. (34), there should be close agreement between these corresponding frequencies. The deviations $(f_{ij} - e_{ij})$ measure lack of agreement. We eliminate the signs by squaring each difference, and reduce that value to original units by dividing by the respective e_{ij} . Thus

$$(f_{ij} - e_{ij})^2/e_{ij}$$

measures lack of agreement for the i-th component in the j-th sample. An overall measure of the lack of agreement is the sum of these individual measures. Thus, the test statistic Q is defined as

$$Q = \sum_{i=1}^{m+1} \sum_{j=1}^{n} \frac{(f_{ij} - e_{ij})^{2}}{e_{ij}}$$
(35)

A small value of Q supports the null hypothesis H_0 , whereas a large value reflects a general incompatibility between the frequencies observed and those expected under H_0 .

The asymptotic distribution (large n) of Q is independent of the underlying distribution. For a simple null hypothesis, Q is asymptotically distributed as a chi-square random variable with mn degrees of freedom under H_{Ω} .

As mentioned earlier, it is sometimes necessary to estimate some parameter values before the test can be performed. Once the parameters are estimated and subsequently used to estimate e_{ij} , Q is calculated according to eqn. (35) as before. For a composite null hypothesis, again the distribution of Q is approximately chi-square but with n(m-w) degrees of freedom, where w denotes the number of independent unspecified parameters. Reduction of the number of degrees of freedom shifts the boundary of the critical region so that Q has to be smaller for acceptance at a given level.

4. Binomial Test

A common problem in solids mixing involves the blending of an active ingredient with several diluents. The homogeneity of this active ingredient in the entire mixture is of primary importance. Given a prescribed quality standard we are interested in testing the hypothesis that the proportion of mixture which meets the quality standard exceeds a fixed level.

In general, the hypothesis may take one of the following forms for some specified value of θ_0 (0 < θ_0 <1)

(1) One-sided alternatives

(a)
$$H_{01}$$
: $\theta \le \theta_0$ versus H_+ : $\theta > \theta_0$ (36)

(b)
$$H_{02}$$
: $\theta \ge \theta_0$ versus $H_{\underline{}}$: $\theta < \theta_0$ (37)

(2) Two-sided alternative

$$H_{03}: \theta = \theta_0 \quad \text{versus } H_a: \theta \neq \theta_0$$
 (38)

We first consider a test of the hypothesis (la). Suppose that n spot samples are drawn from the mixture with each spot sample being classified as satisfactory or unsatisfactory. Denote the numbers of satisfactory and unsatisfactory samples by S_+ and S_- , respectively. The hypothesis H_{01} is rejected at the α level whenever

$$s_{+} > c_{\alpha 1}$$

where the critical value $C_{\alpha 1}$ is determined such that

$$Pr_{\theta_0}[S_+ > C_{\alpha_1}] = \alpha$$

Note that the distribution of S_+ , when θ = θ_0 , is binomial with parameters n and θ_0 , hence

$$E_{\theta_0}[S_+] = n\theta_0$$

Similarly, we reject the hypothesis ${\rm H}_{\rm 02}$ at the $^{\rm c}$ level whenever

$$s_{-} > c_{\alpha 2}$$

where

$$Pr_{\theta_0}[S_+ > C_{\alpha 2}] = \alpha$$

Here the distribution of S_ , when $\theta=\theta_0$, is binomial with parameters n and $(1-\theta_0)$, hence

$$E_{\theta_0}[S_1] = n (1 - \theta_0)$$

Since

$$S_{+} + S_{-} = n$$

the rejection region of an α level tests of the hypothesis H_{03} is determined by

$$S_{+} < C_{\alpha 1}$$
 or $S_{+} > C_{\alpha 2}$

where

$$\Pr_{\theta_0}[S_+ < C_{\alpha 1}] + \Pr_{\theta_0}[S_+ > C_{\alpha 2}] = \alpha$$

An equal tails test selects critical values ${
m C}_{lpha 1}$ and ${
m C}_{lpha 2}$ such that

$$\Pr_{\theta_0}[S_+ < C_{\alpha 1}]$$

and

$$Pr_{\theta_0}[s_+ > c_{\alpha 2}]$$

are approximately equal.

For large samples, we define the standardized variables (with a continuity correction of 0.5) to be

$$\dot{z}_{+} = \frac{S_{+} - n\dot{\theta}_{0} - 0.5}{n\theta_{0} (1 - \theta_{0})} \tag{39}$$

and

$$z = \frac{S_{.} - n(1-\theta_{0}) - 0.5}{n\theta_{0} (1-\theta_{0})}$$
(40)

The P-value associated with the tests of the above three hypotheses

are obtained from the standard normal table[2] as:

Hypothesis	P-value
H ₀₁ vs H ₊	Pr[Z > z ₊]
H ₀₂ vs H_	Pr[Z > z_]
H ₀₃ vs H _a	2 (max (Pr[Z > z ₊] , Pr[Z > z ₋]))

where Z has a standard normal distribution.

IV. EXPERIMENT

The experimental apparatus, materials and procedures employed are described in this section. To minimize experimental and computational effort, ternary particles systems were chosen to demonstrate the analysis of multicomponent solids mixing by nonparametric statistical methods.

1. Apparatus and Materials

The apparatus used in this experiment was a cylindrical plexiglass mixer of the following dimensions: internal length 38.1 cm (15 in), diameter 14.0 cm (5.5 in) and end flanges diameter 25.4 cm (10 in). The tube was split axially so that the upper portion could be removed for loading and sampling. The end flanges were accurately made to insure that during mixing the axis of rotation coincided with the geometric axis of the mixer. The plexiglass cylinder was set horizontally on a jar mill whose rotational speed was accurately maintained at a speed between 10 and 50 r.p.m.. Particles used in this experiment were Lucite spheres with an average diameter of 0.16 cm (small), 0.32 cm (medium) and 0.48 cm (large) with an average density of 1.156 g/cm³.

2. Procedure

Prior to mixing, two thin semi-circular partitions were placed between the two ends of mixer normal to the mixer axis dividing it into three equal compartments. One hundred and seventy grams each of 3 types of particles were loaded in each compartment, respectively. Approximately 30% of the overall volume of the mixer was occupied by the particles. The bed was then leveled, the partitions were removed, the cover was put in place, and the mixer was rotated. Two types of systems were created:

(1) Heterogeneous

Three types of particles of different sizes (small, medium and large) were employed in this system.

(2) Homogeneous

Three types of (large) particles, which had identical properties except color, were used in this system.

Table 2 summarizes the experimental conditions of each run. After a predetermined mixing time, twelve spot samples were randomly drawn from the mixture for each experimental run and the weight fractions of three types of particles in the sample were recorded. For the homogeneous system, the number of particles of each type in the sample was also counted.

Table 2. Summary of particle system and experimental conditions

(1) Heterogeneous sy	stem (small, medium and l	arge particles)
experimental run	rotating speed (r.p.m.)	mixing time (min.)
1	30	2
2	30	10
3	30	30
4	20	10
5	45	10
(2) Homogeneous syst	em (large particles)	**
experimental run	rotating speed (r.p.m.)	mixing time (min.)
6 ,	30	30
7	45	30
8	45	60
9	45	150

V. RESULTS AND DISCUSSION

The theories and procedures presented in Section III. are employed to analyze the experimental data obtained. Implications of various tests are explained.

1. Test of sampling techniques

In a multicomponent solids mixing problem, the sample mean vector should not deviate greatly from its known population mean vector. On the other hand, the mean vector by itself should not be used as a measure of the degree of mixedness, since, if the batch is properly sampled, the only variation between sample mean vectors should be the sampling variation, regardless of how well mixed the batch is. If the mean vector $\underline{\mu}$ differs significantly from the population mean vector $\underline{\mu}_0$, the sampling may have been biased due to location or method [10]. If so, this bias should be eliminated before further sampling.

To accomplish this, we have to test the hypothesis that the mean vector is specified, e.g., to test the null hypothesis

$$H_0: \ \mu = \mu_0 = \left[\frac{1}{3} \quad \frac{1}{3} \right]'$$
 (41)

against the alternative hypothesis

$$H_1: \mu \neq [\frac{1}{3}, \frac{1}{3}]'$$

An example of this calculation is shown below for the first experimental run. The experimental data for the 3 particle sizes (small, medium and large) in 12 random spot samples are tabulated in Table 3. By selecting the small and medium sized particles, we express the sample data matrix, \underline{x} , as

Table 3 Experimental data expressed in Weight fraction for experimental runs 1 through 3.

-				haragaya saran.		water states	-	- Charles and Assess		والمواركين	unari wa	
3 .m.) large	.539	000.	.477	.951	607.	.408	.792	.473	.353	.336	777	.476
experimantal run 3 (30 min, 30 r.p.m.) mall medium larg	.426	000	.493	. 049	.482	. 507	. 200	.463	. 583	. 529	. 504	. 474.
experi (30 m smæ11	.035	1.000	.029	000.	.109	.085	.008	.064	790.	.136	.052	.050
un 2 .p.m.) large	.729	000.	.279	.212	.118	.017	.661	000.	. 211	.175	.731	.150
experimental run 2 (10 min, 30 r.p.m.) mall medium larg	.259	.565	909.	.771	.611	.836	.250	.071	.517	.225	.202	.419
exper (10 ms 11)	.012	.435	.115	.017	.271	.146	680.	.929	.272	009.	190.	.431
run 1 .p.m.) large	920.	000	.626	.590	.283	000.	800.	.007	1.000	.324	000.	000.
experimental run (2 min, 30 r.p. all medium l	797.	.032	.370	.410	569.	800.	,123	.752	000	859.	.013	.031
exper (2 n small	.127	896.	,004	000	.022	.992	698.	. 241	000.	.018	.987	696°
spot sample	 -1	2	m	7	5	9	7	∞	6	10	 1	12

which, after adjustment for $\underline{\mu}_0$, yields

ch, after adjustment for
$$\underline{\mu}_0$$
, yields
$$y = \underline{x} - \underline{\mu}_0 = \begin{bmatrix}
0.969 & 0.031 \\
-0.206 & 0.464 \\
0.635 & -0.301 \\
-0.329 & 0.037 \\
-0.333 & 0.077 \\
-0.311 & 0.362 \\
0.659 & -0.325 \\
0.536 & -0.210 \\
-0.092 & 0.419 \\
-0.333 & -0.333 \\
-0.315 & 0.325 \\
0.654 & -0.320 \\
0.636 & -0.302
\end{bmatrix}$$

Since ties occur in the application of rank tests, we use a midrank procedure that assigns the simple average of the ranks which would have been assigned to the observations if they were not tied. Thus, ranking the elements of each row of y in increasing order of their absolute values, we obtain

$$\frac{R}{n} = \begin{bmatrix}
2 & 9 & 5 & 6.5 & 3 & 12 & 8 & 1 & 6.5 & 4 & 11 & 10 \\
12 & 4 & 1 & 2 & 10 & 7.5 & 3 & 11 & 9 & 7.5 & 6 & 5
\end{bmatrix}$$

Two multivariate rank tests were developed to test the hypothesis of a prescribed mean vector:

(1) A multivariate sign test

The score matrix takes the form

According to eqn. (9), we have

$$T^{(1)} = -2, T^{(2)} = 0$$

and,

$$T = [-2 \ 0]$$

Thus, from eqns. (13) and (14), we have

$$\underline{V} = \begin{bmatrix}
1 & -\frac{10}{12} \\
-\frac{10}{12} & 1
\end{bmatrix}$$

and

$$\underline{v}^{-1} = \begin{bmatrix} \frac{36}{11} & \frac{30}{11} \\ \frac{30}{11} & \frac{36}{11} \end{bmatrix}$$

Therefore, the test statistic is calculated as

$$S = \frac{1}{n} \left[\underline{T} \underline{V}^{-1} \underline{T}' \right]$$

$$= \frac{1}{12} \begin{bmatrix} -2 & 0 \end{bmatrix} \begin{bmatrix} \frac{36}{11} & \frac{30}{11} \\ \frac{30}{11} & \frac{36}{11} \end{bmatrix} \begin{bmatrix} -2 \\ 0 \end{bmatrix}$$

Since S is asymptotically distributed as a chi-square random variable with 2 degrees of freedom, we can calculate the P-value as

$$P = 0.5796$$

Such a large P-value supports H_0 ; hence, the sampling technique is judged to be representative of the mixture.

(2) A multivariate generalization of the Wilcoxon signed-rank test
In this case, the score matrix

$$\underline{\mathbf{E}}_{\mathbf{n}} = \frac{1}{13} \, \underline{\mathbf{R}}_{\mathbf{n}}$$

By eqn. (9),

$$T^{(1)} = 1.692, T^{(2)} = 0.692$$

and

$$\underline{\mathbf{T}} = [1.692 \quad 0.692]$$

According to eqns. (13) and (14), we have

$$\underline{V} = \begin{bmatrix} 0.320 & -0.158 \\ -0.158 & 0.320 \end{bmatrix}$$

Thus, the test statistic, eqn. (15), is

$$S = \frac{1}{n} \left[\underline{T} \underline{V}^{-1} \underline{T}^{-1} \right]$$
$$= 1.5476$$

The associated P-value is

$$P = 0.4613$$

Therefore, use of the multivariate Wilcoxon signed-rank procedure leads to the same conclusion as the multivariate sign test and the sampling technique is judged to be representative of the mixture.

Table 4 lists the P-values for all pairs of particles considered and the two multivariate rank tests. Calculations have been carried out for experimental runs 2 through 5. The results from these runs are also shown in Table 4.

2. Test of Treatment Effects

The data from the first three experimental runs are used to illustrate a test of significance of treatment effects. This is accomplished by testing the homogeneity of their covariance matrices. Thus, we test the hypothesis

Table 4. Results of testing the sampling technique

	Experimental run	Calaulati (small, medium)	Calaulation based on the pair of (small, medium) (medium, large) (small, large)	air of (small, large)	Inference:H ₀ , eqn.(41), is rejected
	1	0.5796	0.2138	0.1054	ou
	2	0.1653	0.4758	0.0765	ou
multivariate sign test	m	0.1054	0.1054	0.2231	ou
)	4	0.2231	0.1353	0.1353	ou
	2	0.1653	0.7788	0.1653	ou
		0.4613	0.3285	0.2712	оп
;	2	0.3293	0.3196	0.2366	ou
multivariate Wilcoxon signed-	£	0.3392	0.3443	0.7649	ou
rank test	7	0,3013	0.2808	0.3488	ou
	ĸ	0.5732	0.6985	0.8583	ou

$$H_0: \underline{\Sigma}^{(1)} = \underline{\Sigma}^{(2)} = \underline{\Sigma}^{(3)} \tag{42}$$

against the alternative

$$H_1: \underline{\Sigma}^{(1)}, \underline{\Sigma}^{(2)}$$
 and $\underline{\Sigma}^{(3)}$ are not identical

In other words, H_0 hypothesizes no significant difference in dispersion for mixing times of 2, 10 and 30 minutes.

The experimental data are listed in Table 3. Using the small and medium sized particles for illustration, we define

$$\underline{\mathbf{x}}_{\mathbb{N}} = \left(\underline{\mathbf{x}}^{(1)} \quad \underline{\mathbf{x}}^{(2)} \quad \underline{\mathbf{x}}^{(3)}\right) \quad \underline{\mathbf{2}}_{\mathbf{x}36}$$

where -

	\$5 30		,			,
	0.127	0.797		0.012	0.259	
	0.968	0.032		0.435	0.565	
	0.004	0.370		0.115	0.606	
	0.000	0.410		0.017	0.771	
	0.022	0.695		0.271	0.611	
v ⁽¹⁾ =	0.992	0.008	<u>x</u> ⁽²⁾ =	0.146	0.836	
X m	0.869	0.123	<u> </u>	0.089	0.250	
	0.241	0.752		0.929	0.071	
	0.000	0.000		0.272	0.517	
	0.018	0.658		0.600	0.225	
	0.987	0.013		0.067	0.202	
	0.969	0.031	, j	0.431	0.419	

and

$$\mathbf{x}^{(3)} = \begin{bmatrix} 0.035 & 0.426 \\ 1.000 & 0.000 \\ 0.029 & 0.493 \\ 0.000 & 0.049 \\ 0.109 & 0.482 \\ 0.085 & 0.507 \\ 0.008 & 0.200 \\ 0.064 & 0.463 \\ 0.064 & 0.583 \end{bmatrix}$$

Ranking the 36 elements of each row of the matrix \underline{x}_N in increasing order of magnitude, we obtain the rank matrix

$$\underline{R}_{N} = \left[\underline{R}^{(1)} \underline{R}^{(2)} \underline{R}^{(3)} \right]_{2\times 36}$$

where

$$\underline{R}^{(1)} = \begin{bmatrix}
16 & 31 & 3 & 1.5 & 7 & 36 & 29 & 21 & 1.5 & 6 & 35 & 32 \\
35 & 7 & 16 & 20 & 32 & 2 & 9 & 33 & 1 & 31 & 3 & 6
\end{bmatrix}$$

$$\underline{R}^{(2)} = \begin{bmatrix}
4 & 26 & 15 & 5 & 22 & 17 & 12 & 30 & 23 & 27 & 10.5 & 25 \\
13 & 28 & 29 & 34 & 30 & 36 & 12 & 8 & 27 & 11 & 10 & 22
\end{bmatrix}$$

and

$$\underline{R}^{(3)} = \begin{bmatrix} 33 & 13 & 20 & 14 & 18 & 10.5 & 8 & 19 & 9 & 34 & 28 & 24 \\ 5 & 23 & 17 & 26 & 21 & 18 & 19 & 25 & 24 & 4 & 15 & 14 \end{bmatrix}$$

According to eqn. (24), the general score matrix is of the form

$$\underline{\mathbf{E}}_{\mathrm{N}} = \sqrt{12} \left(\frac{1}{\mathrm{N}+1} \, \underline{\mathbf{R}}_{\mathrm{N}} - \frac{1}{2} \, \underline{\mathbf{J}}_{\mathrm{N}} \right)$$

where

$$\underline{J}_{N} = \begin{bmatrix} 1 & 1 & \dots & 1 \\ 1 & 1 & \dots & 1 \end{bmatrix}_{2\times 36}$$

Thus, in our example,

$$\underline{E}_{N} = \sqrt{12} \left(\frac{1}{37} \, \underline{R}_{N} - \frac{1}{2} \, \underline{J}_{N} \right)$$

Using eqns. (25) through (31), (see Appedix B for a list of computer program)

$$\underline{\mathbf{U}}^{(1)} = [1.7099 -0.7724 \ 1.5668]$$

$$\underline{\mathbf{U}}^{(2)} = [0.6743 -0.0612 \ 0.9201]$$

$$\underline{\mathbf{U}}^{(3)} = [0.7034 -0.4645 \ 0.4565]$$

$$\underline{v}_{N}(\underline{R}_{N}) = \begin{bmatrix} 0.6606 & -0.2705 & -0.3515 \\ -0.2705 & 0.9632 & -0.2442 \\ 0.1870 & -0.2442 & 0.6623 \end{bmatrix}$$

and

$$\underline{\underline{V}}_{N}^{-1}(\underline{\underline{R}}_{N}) = \begin{bmatrix} 1.7878 & 0.4113 & -0.3515 \\ 0.4113 & 1.2402 & 0.3411 \\ -0.3515 & 0.3411 & 1.7348 \end{bmatrix}$$

According to eqn. (32), the test statistic is

$$L = \frac{3}{\Sigma} n_k \left[\underline{\underline{U}}^{(k)} - \underline{\underline{U}}^* \right] \underline{\underline{V}}_N^{-1} (\underline{\underline{R}}_N) \left[\underline{\underline{U}}^{(k)} - \underline{\underline{U}}^* \right]$$
$$= 21.6334$$

Since L is asymptotically distributed as a chi-square random variable with six degrees of freedom, the associated P-value is

$$P = 0.001$$

Therefore, the null hypothesis H_0 , eqn. (43), is rejected, and we conclude that there exists a significant difference in dispersion between the mixing times of 2, 10 and 30 minutes. The P-value based on small and large sized particles and that based on medium and large sized particles are 0.001 and 0.006 respectively.

In the second experiment, we test the effect of rotating speeds (20, 30 and 45 r.p.m.) on dispersion for a fixed mixing time of 10 minutes (Experimental runs 2, 4, and 5). The P-values corresponding to test statistics for pairs (small, medium), (small, large) and (medium, large) are 0.720, 0.360 and 0.753 respectively. Because, the P-values are quite large, we conclude that the difference in dispersion among rotating speeds of 20, 30 and 45 r.p.m. is not significant.

3. Test of the Completely Mixed State

In solids mixing, the completely random (or mixed) state is characterized by the property that the probability of selecting a particle of a given component from anywhere in the mixture is identical. When the population proportions are known for the components of a mixture, the chi-square goodness-of-fit test can be used to test the hypothesis that the mixture is in the completely mixed state. In other words, we test

 H_0 : the mixture is in the completely mixed state (44) against the alternative

 H_1 : H_0 is not true The data generated in run 6 of the experiments is shown below.

spot sample	color Green	distril Red	bution [*] White	total number of particles	expected number of particles for each color
1	47	34	22	103	34.33
2	39	28	31	98	32.6
3	26	16	42	84	28
4	24	10	50	84	28
5	38	42	17	97	32.33
6	33	39	35	107	35.67
7	35	47	9	91	30.33
8	31	26	54	111	37
9	32	39	31	102	34
10	36	20	27	83	27.67
11	33	76	11	120	40
12	40	43	37	120	40

^{*} The ratio is 1 : 1 : 1 for categories Green : Red : White, respectively.

From eqn. (35), the test statistic is computed as

$$Q = \sum_{i=1}^{3} \sum_{j=1}^{12} \frac{f_{ij} - e_{ij}^{2}}{e_{ij}^{2}}$$

$$= \frac{(47 - 34.33)^{2} + \frac{(34 - 34.33)^{2} + \frac{(22 - 34.33)^{2}}{34.33} + \cdots + \frac{(40 - 40)^{2}}{40}}{\frac{(43 - 40)^{2} + \frac{(37 - 40)^{2}}{40}}{40}}$$

= 162.68

Under the null hypothesis, eqn. (44), Q is asymptotically distributed as the chi-square random variable with 24 degrees of freedom. Since

the null hypothesis is rejected (at the usual levels); we conclude that mixture has not reached the completely mixed state. The following table summarizes the results of tests of completely mixed state for experimental runs 6 through 9:

experimental run	mixing time (min)	rotating speed (r.p.m.)	expected distribution	Test statistic Q	associated probability P	inference about H _O , eqn. (44)
6	30	30	$\frac{1}{3}:\frac{1}{3}:\frac{1}{3}$	162.28	<< 0.001	rejected
7	30	45	$\frac{1}{3}:\frac{1}{3}:\frac{1}{3}$	56.25	<0.001	rejected
8	60	45	$\frac{1}{3}:\frac{1}{3}:\frac{1}{3}$	43.43	0.009	rejected
9	150	45	$\frac{1}{3}:\frac{1}{3}:\frac{1}{3}$	13.20	0.963	accepted

4. Test of a Quality Standard

In quality control involving multicomponent solids mixing, we may be concerned with the fraction of a population which meets a quality criterion. The binomial test can be used to solve this multicomponent solids mixing problem. Again let x_{ij} denote the weight fraction of the i-th component in the j-th sample and μ_{i0} the population weight fraction of i-th component. We may set the criterion as

$$\sum_{i=1}^{m+1} \lambda_i \left(x_{ij} - \mu_{i0} \right)^2 \leq \varepsilon$$
 (45)

where

 λ_{i} = arbitrary positive constant which might reflect the relative importance of the i-th component being mixed.

and

ε = pre-selected positive real number.

We say that a spot sample is satisfactory, if it satisfies this criterion; otherwise, it is unsatisfactory.

Assume that three components are equally important. Hence, let

$$\lambda_1 = \lambda_2 = \lambda_3 = 1$$

We wish to test that the satisfactory proportion of a mixture has reached 95% for a pre-selected value of 0.015 for £. In the following examples, we test the null hypothesis

$$H_0: \theta \ge .95 \tag{46}$$

against the alternative hypothesis

The calculation for run 7 of the experiments is shown in Table 5. The results are

$$S_{+} = 7$$
, $S_{-} = 5$, $n = 12$

The guide indicates that the appropriate P-value is left-tail probability for $S_{+} = 7$ with a parameter of .95, which from a binomial table is

$$P = .0002$$

Since this P-value is so small, we conclude that the data reject H_0 in favor

Table 5. The calculation for experimental run 7 for testing the quality standard as defined in eqn. (45)

spot sample	×ij	* _{2j}	×3j	$\sum_{i=1}^{3} (x_{i} - \mu_{i0})^{2^{**}}$	is it satisfactory?
1	0.3333	0.2564	0.4103	0.0018	yes
2	0.3537	0.4146	0.2317	0.0174	no
3	0.2941	0.3765	0.3294	0.0034	yes
4	0.3196	0.2474	0.4330	0.0175	no
5	0.3113	0.4811	0.2075	0.0382	no
6	0.2857	0.3286	0.3587	0.0050	yes
7	0.2785	0.2405	0.4810	0.0334	no
8	0.3678	0.3908	0.2414	0.0129	yes
9	0.3229	0.2917	0.3854	0.0046	yes
10	0.3182	0.3636	0.3182	0.0014	yes
11	0.3367	0.5000	0.1633	0.0567	no
12	0.3636	0.2987	0.3377	0.0021	yes

^{**} $\mu_{10} = \mu_{20} = \mu_{30} = 0.3333$

of H. Hence, we conclude that mixing is not adequate. The results of runs 6 through 9 are summarized in the following table.

experimental run	s+	s_	n	Р	Inference concerning H _O , eqn. (46).
6	5	7	12	0.0000	rejected
7	7	5	12	0.0002	rejected
8	10	2	12	0.1184	accepted
9	12	0	12	1.0000	accepted

Note that this test may also be used in the analysis of a continuous mixing process.

VI. CONCLUSIONS

Statistical analysis is recognized as a major tool in solids mixing investigations. Traditionally, results of sampling have been analyzed using normal theory statistical techniques [10, 12].

This study proposes the applicability of several nonparametric statistical techniques to problems in multicomponent solids mixing. The most important feature of a nonparametric procedure is its lack of dependence on a particular distribution type, e.g., normal. Since the distributions of components during mixing are usually unknown, nonparametric procedures comprise a substantial collection of alternatives to the classical parametric procedures.

Recently, the extension of nonparametric techniques from the univariate to the multivariate case has been pursued in [8]. The present study demonstrate the applicability of multivariate tests of location and dispersion to test the hypotheses concerning a sampling technique and the significance of treatment effects in multicomponent solids mixing problems.

The proposed nonparametric procedures were tested with actual homogeneous and heterogeneous ternary mixtures generated by a drum mixer. In spite of the small number (n=12) of the sample obtained, the results tend to support the practical significance of nonparametric statistics in the evaluation of mixing systems.

Besides the robustness of the nonparametric methods against the assumption of a specified distributional form, it is important to note their simplicity in application. An effort will be made in the future to study the performance of the proposed nonparametric methods for larger sample sizes.

NOTATIONS

```
critical value at the significance level a
C_{\alpha}
           sign indicator of Y
Cii
E(X)
           expected value of random variable X
           score matrix as defined in eqn. (24)
E_{N}
\frac{\mathbf{E}_{\mathbf{n}}}{\mathbf{E}_{\mathbf{n}}}
           score matrix as defined in eqn. (8)
<sub>臣</sub>(i)
           mean score of the i-th variate
           expected number of particles of the i-th component in the j-th
e<sub>ij</sub>
           sample
F(x)
           cumulative distribution function (c.d.f.) of X
           number of particles of the i-th component in the j-th sample
fit
           null hypothesis
H_{0}
Ha
           two-sided alternative
           one-sided alternative with positive direction
H^{T}
           one-sided alternative with negative direction*
H
           test statistic for testing homogeneity of dispersion matrices
L
           number of variates
m
N
           total number of spot samples for t treatments
           number of spot samples
n
           number of samples of treatment k
nk
P
           associated probability
Q
           test statistic for goodness of fit test
           (m x N) rank matrix as defined in eqn. (22)
\frac{R}{N}
           (m x n) rank matrix as defined in eqn. (7)
\frac{R}{n}
R_{ij}
          rank of Y_{ij} among (Y_{i1}, ..., Y_{in})
R<sup>TTI</sup>
          set of all order m-tuples (x_1 x_2 \dots x_m)
R_{ij}^{(k)}
           rank of X_{ij}^{(k)} among (X_{i1}^{(k)}, ..., X_{in_{+}}^{(k)}) for k = 1, 2, ..., t
```

number of unsatifactory samples

S

```
S
            number of unsatisfactory samples
             test statistic for testing equality of mean vectors
S
T<sup>(1)</sup>
             univariate rank order statistic as defined in eqn. (9)
             row vector as defined in eqn. (10)
I
t
             number of treatments
U(k)

*
Uil
Uil
Uil
             row vector as defined in eqn. (29)
             row vector as defined in eqn. (30)
             as defined in eqn. (25)
U*
             as defined in eqn. (26)
             as defined in eqn. (13)
v 12
             as defined in eqn. (12)
V
             as defined in eqn. (31)
\frac{\mathbf{v}_{\mathbf{N}}}{\mathbf{v}_{\mathbf{N}}}
             number of unspecified parameters estimated from data
- W
             row vector = [X_{ij} X_{2j} ... X_{mj}], j = 1, 2, ..., n
\frac{\mathbf{x}}{1}
             row vector = [X_{ij}^{(k)} \ X_{2j}^{(k)} \dots X_{mj}^{(k)}], \quad j = 1, 2, \dots, n
             row vector = [X_{ij}^{(k)} \ X_{2j}^{(k)} ... X_{mj}^{(k)}], \quad j = 1, 2, ..., n
             a random variable representing the weight fraction of the i-th
             component in the j-th sample for the k-th treatment
             realization of X_i
\frac{\mathbf{x}}{1}
             = x_{ij} - \mu_{i0}
Y
             (m x n) random matrix
\frac{Z}{n}
             (m x N) pooled random matrix
 \frac{Z_{N}}{}
             standardized variable as defined in eqn. (39)
 z_{\perp}
             standardized variable as defined in eqn. (40)
 Z_
              a parameter representing the probability of satisfaction
 θ
              location vector parameter
 <u>1</u>
```

 μ_{10} weight proportion of the 1-th component in the population ν degrees of freedom as defined in eqn. (33) χ^2 chi-square distribution $\underline{\Sigma}^{(k)}$ dispersion matrix of treatment k

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9

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APPENDIX A. On the Use of P-values in Hypothesis Testing

The traditional method of testing a hypothesis is the determination of a rejection region and a corresponding rejection rule for which the probability of making a Type I error does not exceed some preselected value called the level of the test. In many cases, the choice of the level of the test is arbitrary and in some testing situations the chosen level may not even be attainable. These problems are circumvented by the reporting of P-values.

The P-value is defined as the probability under the null hypothesis of a sample outcome equal to or more extreme than that observed. The reporting of P-values clearly contains more information than merely reporting the decision made on a hypothesis at a possibly arbitrary level.

The use of P-value is clear for those tests in which the outcomes can be ordered according to how extreme they are relative to the expected outcome under the null hypothesis. In those unambiguous cases the P-value is the probability associated with a corresponding right or left tail probability. In the more complex situations where "more extreme" is an ambiguous relation, conventions must be defined for the reporting of P-values.

APPENDIX B List of a Computer Program for Calculating the Test Statistic L

A computer program for calcuting the test statistic L in eqn. (32) is developed and listed in the following pages. The input data are the elements of the rank matrix, eqn. (22). The symbols used in this program are listed as below.

M: m; number of variates

NT : T; number of treatments

N(K): n_k ; number of spot samples for treatment k.

E(K,I,J): $E_{R(k)}^{(i)}$; general score of the i-th component in the j-th spot sample for treatment k.

NTT: N; total number of observations.

 $S(K,I,J): U_{ij}^{(k)}$ as defined in eqn. (25).

SS(I,J) : U as defined in eqn. (26).

 $G(I) = \overline{E}^{(i)}$ as defined in eqn. (27).

V(I,J,II,JJ): $V_{ij,i'j'}$ as defined in eqn. (28)

L : L; test statistic as defined in eqn. (32)

Note that two subroutines are used. Subroutine MINV is used to obtain the inverse matrix of a non-singular matrix. Subroutine GMPRD is used to get the product of two general matrices. The result of calculation of the test statistic for comparison among the first three runs is also shown in page 56.

```
THIS PACKAGE IS USED TO CALCULATE THE TEST STATISTIC L, EQN. (32)
                                                                              E(K,1,J) = GENEKAL SCORE OF THE I-TH COMPONENT IN THE J-TH SPOT SAMPLE FOR TREATMENT K
                                                                                                                                15(31, 16(3,31,T(3,31,55(2,21,A(91,L1(3),L2(3),B(3),R(3)
                                                                                                               DIMENSION E(3,2,12), S(3,2,2),N(3),D(3,2),G(2),V(2,2,2),
                                                                                                                                                                                                                                                                               MAIRIX RI . 11, . 1.
                                                                                                                                                                                                                I = I = I * M ! K= I , NI )
                                               NIK) = NUMBER OF SPOT SAMPLES FCR TREATMENT K
                                                                                                                                                                                                                                                                                                                                                                                                                                                E(K, I, J)=(E(K, I, J)/(NTT+1)-.5)*(12**.5)
                                                                                                                                                                                                                                                                                                HRITE (0,11) ((L(K,1,1),J=1,12),I=1,M)
                                                               NII = TOTAL NUMBER OF OBSERVATIONS
                                                                                                                                                                                                              READ (5,2) (((E(K,1,J),J=1,12
                                                                                                                                                                                                                                                                               THE INPUT DATA,
                               NT = NUMBER OF TREATMENTS
                                                                                                                                                                              KEAD (5,1) (N(I), I=1,NI)
               M = NUMBER OF VARIATES
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                D(K, I)=D(K, I)+E(K, I, J)
                                                                                                                                                                                                                               FORMAT (12F6.0)
                                                                                                                                                                                                                                                                                                               FURMAT (12F7.1)
                                                                                                                                                                                                                                                               WRITE (6,12) K
                                                                                                                                                                                                FCHMAT (3110)
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 21'15 7=1'17
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 DO 25 K=1,NT
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V[[,J,][,JJ)=V(],J,][,J,][+,JJ)+E(K,],J])+E(K,J,J])*E(n,][,J])*E(K,JJ,J]
                                                                                                                                                                                                                                                                                                                                                                                                                    SIK, I, J)=E(K, I, JI) *E(K, J, JI) + S(K, I, J)
                                           S(K, I, J)=S(K, I, J)-D(K, I) +D(K, J)/N(K)
                                                                                                                                                                                                                                    SS(1, J)=SS(1, J)+E(K, 1, J1)*E(K, J, J1)
                                                                                                                                                                                                                                                               SS(I, J)=SS(I, J)-NTT*G(I)*G(J)
SS(I, J)=SS(I, J)/(NTT-I)
                                                       S(K,1,1)=S(K,1,1)/(h(K)-1)
                                                                                                                            G(1)=G(1)+E(K,1,J1)
                                                                                                                                                                                                                                                                                                                                               .U=(LL, 11, L, 1)
                                                                                                                                                                                                                        21,1=1t 25 0U
                     00 30 31=1,12
                                                                                                                 00 21 11=1,12
                                                                                                                                                    G(1)=G(1)/NIT
                                                                                                                                                                                                                                                                                                                                                                      00 50 JI=1,12
                                                                                                                                                                                                                                                                                                                                    00 45 JJ=1, M
                                                                                                                                                                                                                                                                                                                                                           DU 50 K=1,NI
                                                                                                                                                                                                             00 35 K=1,NT
                                                                                                                                                                                                                                                                                                                        No 45 II=1,M
                                                                                                     00 27 K=1,N1
                                                                                                                                                                                                                                                                                                             00 45 J=1,M
                                                                              DU 26 I=1 M
                                                                                                                                                                           DU 40 I=1,M
                                                                                                                                                                                      DO 40 J=1,M
                                                                                                                                                                                                                                                                                                  DO 45 1=1 M
00 25 J=1,M
           S (K, 1, 1)=0.
                                                                                                                                                                                                 .0=(f'1)5S
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MATRIX V(A), ECN. (31).../1
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                                                                                                                                                                                                                                                                                                                           (15(1),1=1,3)
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                                                                                                                                                                                              W (3,2)=V(2,2,1,2)
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                                                                                                                                                                                 W (3, 1)=V(2,2,1,1)
                                                                                                                                                                                                         W(3,3)=V(2,2,2,2)
                                                                                                                 W(1,2)=V(1,1,1,1,2)
                                                                                                                              W(1,3)=V(1,1,2,2)
                                                                                                                                          W(2,1)=V(1,2,1,1)
                                                                                                    W(1,1)=V(1,1,1,1,1)
                                                                                                                                                      W(2,2)=V(1,2,1,2
           I(K, 1)=S(K, 1,1)
                        I (K,2)=S(K,1,2)
                                     T(K, 3) = S(K, 2, 2)
                                                                                                                                                                                                                                  WRITE (6,6) K
                                                                                      15(3)=55(2,2)
                                                              15(1)=55(1,1)
                                                                          15(2)=55(1,2)
UU 55 K=1,NT
                                                                                                                                                                                                                      DO 80 K=1,NY
                                                                                                                                                                                                                                                                                                                            WKITE (6,3)
                                                                                                                                                                                                                                                                                                                                                                  WRITE (6,3)
                                                                                                                                                                                                                                                                                                                7 FURMAT (/,
                                                                                                                                                                                                                                                                                                                                                    8 FURMAT (/,
                                                                                                                                                                                                                                                                                                  WRITE (6,7)
                                                                                                                                                                                                                                                                                                                                       WRITE (6,8)
                                                                                                                                                                                                                                                                                                                                                                                            A(1)= M(1,1)
                                                                                                                                                                                                                                                                                                                                                                                                         A(2)=H(2,1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                        A(7)=W(1,3)
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                                                          00 65 K=1,NT
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A (8)= W (2,3)
       A(9)=W(3,3)
                        WRITE (6,9)
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                                                                                    131
                                                                                          130
                                                                                                                                           143
                                                                                                                                                447
                                                                                                                                                       571
                                                                                                                                                             740
                                                                                                                                                                         140
                                                                                                                                                                                                                   152
153
154
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MINV 940 MINV 950 MINV 950 MINV 950	98 99 100 100 100 100 100 100 100 100 100	MINVIOSO MINVIOSO MINVIOSO MINVIOSO MINVIIOS	MINVI 12 C MINVI 13 O MINVI 14 C MINVI 15 O MINVI 17 O MINVI 19 O MINVI 20 C MINVI 20 C	MINV1220 MINV1230 MINV1250 MINV1250 MINV1250 MINV1280 MINV1290
	US PIVOT (VALUE OF PIVOT ELEMENT IS			
J1=JP+J HGLD=-A(JK) A(JK)=A(JI) 40 A(JI) =HGLD	C CONTAINED IN BIGA) C CONTAINED IN BIGA) C 45 IF(BIGA) 48,46,48 46 D=0.0 RETURN 48 DO 55 I=1,N IF(I-K) 50,55,50	ACIK): CONTI	00 65 1=1,N IK=NK+I HULD=A(IK) IJ=I-N 00 65 J=1,N IJ=IJ+N IF(I-K) 60,65,60 60 IF(J-K) 62,65,62 62 KJ=IJ-I+K A(IJ)=HULD*A(KJ)+A(IJ)	
155 156 157 158		65	167 168 169 170 171 172 173 175	77 78 79 60 60 81 82

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MINV1320
                   MINV 1330
                             MINV1340
                                      MINVI350
                                                MINV1360
                                                         MINV1370
                                                                   MINVI380
                                                                             MINV 1390
                                                                                                MINVIALC
                                                                                                         MINV1 42 0
                                                                                                                   MINVI430
                                                                                                                             MINVIGO
                                                                                                                                      MINVL450
                                                                                                                                               MINV1460
                                                                                                                                                         MINV1470
                                                                                                                                                                   MINV1480
                                                                                                                                                                            MINV 149C
                                                                                                                                                                                      MINV1500
                                                                                                                                                                                                MINV151C
                                                                                                                                                                                                         MINV1520
                                                                                                                                                                                                                   MINV1530
                                                                                                                                                                                                                            MINV1540
                                                                                                                                                                                                                                      MINV1550
                                                                                                                                                                                                                                                MINV1560
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                                                                                                                                                                                                                                                                   MINV1580
                                                                                                                                                                                                                                                                             DOSTANIE
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                                                                                                                                                                                                                                                                                                MINVI61C
                                                                                                                                                                                                                                                                                                         MINV 1620
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                                                                                                                                                                                                                                                                                                                            MINVI64C
                                                                                                                                                                                                                                                                                                                                      MINVIOSO
                                                                                                                                                                                                                                                                                                                                                MINV1660
                                                                                                                                                                                                                                                                                                                                                          MINVI67C
                                                                                       MINVI 400
                                                                                                                                                                                                                                                                                                                                                                    MINV 1630
                                                                                                          FINAL ROW AND COLUMN INTERCHANGE
                                                         REPLACE PIVOT BY RECIPRUCAL
                   PRUDUCT OF PLYOTS
                                                                                                                                                                   (FII-K) 120,129,138
                                                                                                                                                                                                                                                                    IF(J-K) 100, 100, 125
                                                                                                                                                IF (K) 150,150,105
                                                                             A (KK)=1.0/B 1GA
                                                                                                                                                                                                N41=C 011 00
                                                                                                                                                                                                                                                                                      Nº1=1 001 00
                                                                                                                                                                                                                                                                                                                            A(K1)=-A(J1)
                                                                                                                                                                                                                                       A(JK)=-A(JI)
                                                                                                                                                                                                                                                A(JI) = HCLD
                                                                                                                                                                                                                                                                                                                                      4(11) =Hulb
                                                                                                                                                                                                                   HULD=A(JK)
                                                                                                                                                                                       「1-1)*ペーとつ
                                                                                                                                                                                                                                                                                                         HULD=A(KI)
                                                                                                                                                                            10=N# (K-1)
                                                                                                                                                                                                                                                                                                                   J 1=K 1-K+J
                                                                                                                                                                                                                                                                                                                                                CC 10 100
                                                                                       BO CUNTINUE
75 CONTINUE
                                      D=U*BIGA
                                                                                                                                                                                                                                                                                                KI=KI+N
                                                                                                                                                                                                           フャプフェソフ
                                                                                                                                                                                                                             し + とし = 10
                                                                                                                                       X=(X-1)
                                                                                                                                                                                                                                                                             KI=K-N
                                                                                                                                                                                                                                                                                                                                                         RE TURN
                                                                                                                                                          (=(K)
                                                                                                                                                                                                                                                          J=X(X)
                                                                                                                              XII
                                                                                                                                                         105
                                                                                                                                                                            108
                                                                                                                                                                                                                                                110
                                                                                                                                       100
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                                                                                                                                                                                                                                                                             571
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                                                                                                 J
                                                                                                          J
                             C
                                                                             185
                                                                                       1 86
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183
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                                       184
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رر		GMPR GMPR	202
ن		GMPR	30
Ç	SUBRUUTINE GMPRU	GMPR	40
၁		GMPR	20
ر		CMPR	60
ာ	AULTIPLY THO GENERAL MATRICES TO FORM A RESULTANT GENERAL	GMPR	J/
J	MAIRIX	GMPR	80
၁		GMPR	3
၁	USAGE	GMTK	100
ر	CALL GMPRD(A, B, R, M, M, L)	GMPR	017
J		GMPR	120
J	OF PARAMETERS	GMPR	130
ں	- NAME OF FIRST INPUT M	CMPR	140
ں	UF SECUND	GMPR	150
ر	0 -	GMPR	16.0
د	ů.	GMPR	176
၁	CULUMNS IN	GMPR	190
J	1	SAPR	190
ر		CMPR	20 C
ن		GMPR	210
ر	INICES MUST BE STORED AS GENERAL I	GMPR	220
J	R CANNUT BE IN THE SAME LUCATION AS MATRIX	CMPR	230
J	R CANNOT BE IN THE SAME LUCA	CAPR	0 47
ن	MER OF COLUMNS OF MATRIX A MUST BE EQUAL TO NUMBER OF	RUNGERTR	250
ں	OF MAIRIX B	CMPR	200
ر		GMPR	270
ں	SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED	CMPR	20 C
ن	NONE	CMPR	29.0
ں		GMPR	30 C
ب		GMPR	31 C
. د	M BY L MAINIX B IS PREMULTIPLIED BY THE N		320
، ر	AND THE RESULT IS STURED IN THE N BY L MATRIX K.	CMPK	330
. ن		GMPR	340
ر ر		GMPR	350
د		という	000

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SUBROUTINE GMPRD(A,B,R,N,M,L)
DIMENSION A(1), B(1),R(1)
                                                                                                 K(1R)=K(1R)+A(J1)*B(1B)
                                                                              N.1=1 C1 UU
                                            N' 1= F 01 00
                               UO 10 K=1,L
                                      IK=IK+M
                                                                                     N+IC=IC
                                                   IK=IK+I
                                                                       R(IK)=0
                                                                                           13=18+1
                                                         N-C=IC
                                                                                                        RETURN
                                                                1 B=1K
                         IK=-M
                  I R=0
                                                                                                  )
|
            S
                                             214
215
216
216
217
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370 380 390 400 410 420 430

GMPR

GMPR GMPR

GMPR GMPR GMPR 440 450 470 480 490 510

GMPR

GMPR GMPR GMPR GMPR

GMPR

GMPR

GMPR

520 530 540

CMPR

GMPR

32.0	25.0	24.0	য়							
35.0	10.5	28.0					2			
6.0	27.0	34.0					29			
4.5 1.0	23.0	9.0								
21.0	30.0	19.0								
29.0	12.0 12.0	19.0	2	~ 1	9	3		430		en avan
36.0	17.0	10.5	1.506832	0.920113	0.456536	0.972960		0.137034 -0.244185 0.062332		-0.351543 0.341079 1.734835
7.0	22.0 30.0	16.0 21.0						1		
1.5 1.5 20.0	1X R(2) 5.0 34.0	IX R(3) 14.0 26.0	.772361	.061226	464538	-0.412605	<u>.</u>	-0.270491 0.963211 -0.244185	OF V(K)	0.411252 1.240149 0.341079
3.0 16.0 2	15.0 29.0	MATR 20.0 17.0	-0-7	0-0-	-0.4	0-	N. (31).	022		ં ને છે
31.0 7.0	JT UATA, 26.0 28.0	11 DATA. 13.0 23.0	к U(1) 1.709870	IR U(2) 0.674330	R U(3) 0.703415	k U(*) 0.972715	(K), EL	0.660559 -0.276491 0.187034	INVERSE MATRIX	1.781810 0.411252 -0.351543
THE INPUT DATA, 16.0 31.0 35.0 7.0 L	THE INPUT DATA, MATRIX 74.0 26.0 15.0 13.0 28.0 29.0 3	1HE INPUT DATA, MATRIX 33.0 13.0 20.0 1 5.0 23.0 17.0 2	VEC 10K U(1) 1.7098	VECTUR U(2)	VEC TOR U(3)	VEC TUR U(*) 0.9727	MAIRIX V(R), EUN.	0.0	THE INVE	0.4

THE TEST STATISTIC L = 21.033430

ACKNOWLEGMENTS

The author wishes to express his sincere gratitude to Dr. R. M. Rubison for his excellent guidance and creative advice in directing this work. To Dr. L. T. Fan goes a special debt of gratitude for his constant encouragement and financial support during the course of this study. Appreciation is also extended to Dr. R. F. Nassar and Dr. F. S. Lai for serving on the author's graduate comittee and for reviewing this report. Special gratitude is extended to his wife, Bernice M. Y. Wu, and his parents for their steady encouragement.

APPLICATIONS OF NONPARAMETRIC STATISTICS TO MULTICOMPONENT SOLIDS MIXING

by

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AN ABSTRACT OF A MASTER'S REPORT

submitted in partial fulfillment of the

requirements for the degree

MASTER OF SCIENCE

Department of Statistics

KANSAS STATE UNIVERSITY

Manhattan, Kansas

1979

ABSTRACT

This study demonstrates the applicability of nonparametric procedures to the analysis of mixing processes. In particular, multivariate nonparametric methods are used to evaluate the properties of a multicomponent solids mixture. Specific problems considered are:

- (1) test of sampling techniques,
- (2) a test of treatment effects,
- (3) a test of the completely mixed state, and
- (4) a test of a quality standard.

The usefulness of the proposed nonparametric techniques is amply demonstrated with both homogeneous and heterogeneous mixtures generated by a drum mixer. The techniques presented in this paper are also applicable to any other mixers.