

THE USE OF A DYNAMIC DIGRAPH STRUCTURE  
IN A POPULATION SIMULATION MODEL  
FOR GRAIN SORGHUM

By

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Major Professor

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The Use of a Dynamic Digraph Structure in a Population  
Simulation Model for Grain Sorghum

I. INTRODUCTION

Sorghum (often referred to as milo) has, through successful research efforts, grown to be one of the leading world crops both in production area and in food value. As of 1969, sorghum ranked fifth in acreage of crops in the world, being exceeded only by wheat, rice, corn, and barley. Perhaps of greater importance is the fact that it is a major food crop in the most heavily populated regions of the world. The three top producers of sorghum in 1970 were the United States, Mainland China, and India.

Because of its resistance to drought and heat, sorghum has been a prominent crop in the southern half of the Great Plains area since the early 19th Century. It was a highly successful livestock food for the early pioneer farmers especially in the semi-arid regions. Also, due primarily to research, sorghum production grew seven-fold between 1940 and 1968 alone, and as a result, it has become an important cash crop for the American farmer. The development of early maturing varieties allowed expansion to the higher altitudes to the west and cooler areas to the north. Shorter varieties allowed automation of harvesting while development of insect and disease resistant hybrids have increased per acre production considerably.

Kansas ranks second only to Texas in total sorghum production and has played a key role in the continued improvement of sorghum. Significant contributions have been made and are presently being made by the agricultural experiment stations of Texas and Kansas. One such contribution was the development in 1975 of the first computer simulation model for grain sorghum by Drs. G. F. Arkin and J. T. Ritchie of the Blacklands Conservation Research Center, Temple, Texas and Dr. R. L. Vanderlip of the Agronomy Department at Kansas State University <1>. This model was developed primarily as a tool for improving management decisions for increased sorghum crop production.

The Arkin, Ritchie, Vanderlip model was based upon simulating a single sorghum plant from emergence to maturity under the weather and soil conditions given for the sorghum field under consideration. A per acre production figure was derived by multiplying the production of the single plant by the number of sorghum plants per acre. This model, which will be referred to as the Single Plant Model, was a fairly sophisticated model with a good degree of accuracy. However, a detailed study of the Single Plant Model showed a complete lack of program structuring and internal documentation. More importantly, the study raised the question as to the accuracy of modeling an entire field based upon the output of one single plant. For example, in the original simulation model, no consideration was given to field variables such as soil variability, seed distribution, emergence date variance, and plant leaf area and tillering.

The current project was instigated to design a field level simulation model which: 1) would have a modular structure, 2) would have sufficient internal documentation, and 3) would expand the model developed by Drs. Arkin, Ritchie, and Vanderlip to include simulation of the variability within a field of sorghum. The new simulation model developed during this project will be referred to as the Field Level Model. The basis of this model is a data structure representing a directed graph (digraph). Each node in the data structure will represent a portion of the field which has some significant difference from the rest of the model. The digraph is the result of plotting the nodes from day to day as they diverge and converge (see figure 3). For example, if half of the field holds water very well while the remainder can not, then the model would be split (the graph will diverge) into two equal parts (or nodes) each of which will be simulated based upon its separate characteristics. The nodes will also be allowed to merge (or converge) if the difference between the two parts is eliminated. If in the above example it rains enough to allow sufficient water for the entire field then the nodes would converge. The converging and diverging of nodes will be based upon internal policies programmed into the model at a later date. It is the objective of the current project to develop the data structure and prove that it is applicable and useful.

## II. The Single Plant Model

It is difficult to present the workings of the Single Plant Model because of the initial lack of modularity and program structure. To overcome this problem the model will be presented in a more logical format with proper modularization and program flow. This represents the state of the model after it was reorganized for use in the Field Level Model but before any new modules were added.

Figure 1. gives a high level diagram for the Single Plant Model showing the various subroutines in the order that they are called. Figure 2. shows a hierarchy diagram of the model before modularization was undertaken. The main routine initializes the critical variables to zero and reads the remaining constant variables from cards. These variables represent plant data, soil data, planting data and location data, all of which remain unchanged throughout the simulation. Table 1 gives a breakdown of the information used in each data type.

After the constant data has been read, up to one year's climatic data is read. This data gives the maximum and minimum temperatures, solar radiation, and rainfall. As each day's climatic data is read, the day's evaporation is calculated by the subroutine EVAP. This value is subtracted from the available water content of the soil by a second subroutine called SOLWAT. SOLWAT also adds rainfall amounts to the soil contents when applicable and then calculates the moisture limiting factor for photosynthesis. Both of these

**TABLE****Plant Data**

Leaf number -- total number of leaves produced

Leaf area -- maximum area of each individual leaf, cm<sup>2</sup>

**Planting Data**

Planting date

Plant population

Row width

Row direction

**Climatic Data (daily from planting to maturity)**

Maximum temperature, C

Minimum temperature, C

Solar radiation, langleys per day

Rainfall, cm

**Location Data**

Extractable soil water capacity, cm

Initial extractable soil water content, cm

Latitude

**Table 1. Input data required.**

The Single Plant Model  
(After Modularization)

6

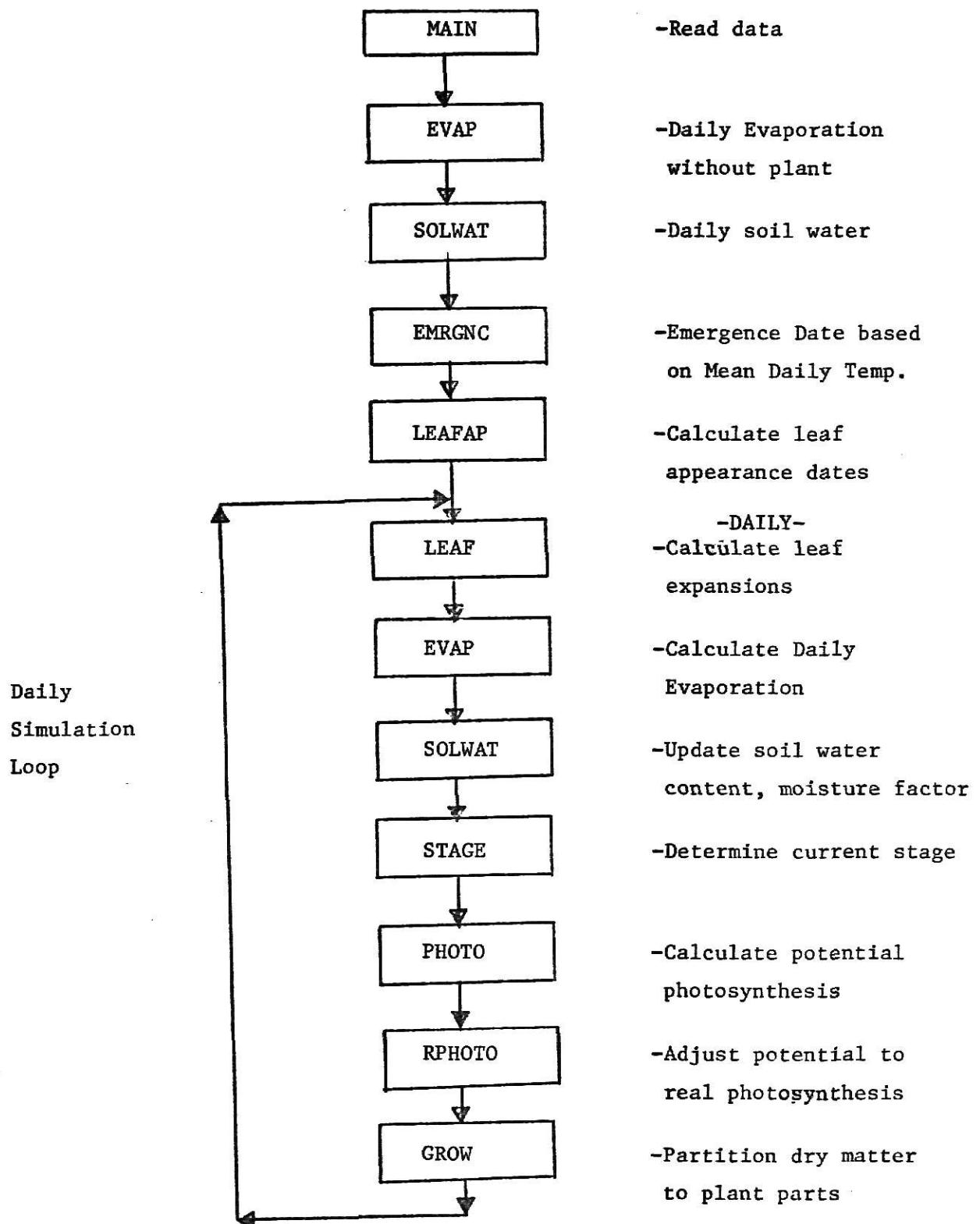


FIGURE 1.

Single Plant Model's Hierarchy Diagram\*

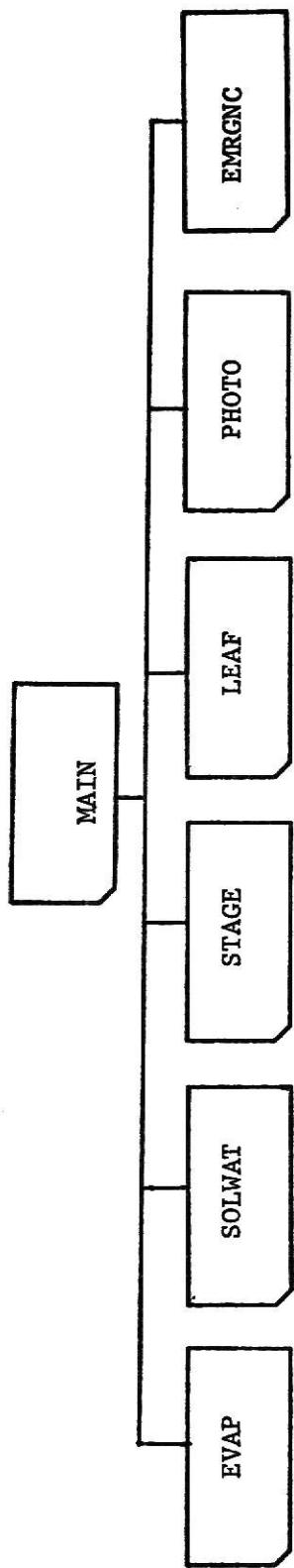


FIGURE 2.

subroutines will be used again when growth simulation begins. After all the climatic data has been read, the emergence module (EMRGNC) is called to calculate emergence date of the single plant based upon mean daily temperature.

Each sorghum hybrid has a maximum number of leaves which will develop and a maximum leaf area for each leaf. The model is heavily based upon the amount of light intercepted by the plant. Therefore, the leaf area per plant must be known. Field and phytotron studies have shown that the rate leaves appear on grain sorghum is directly related to mean daily temperature. The next step is to call the leaf appearance module to calculate the date each leaf appears (subroutine LEAFAP) based on mean daily temperature.

These first three stages are completed in preparation for the actual daily growth simulation. A large loop is established beginning on the date of emergence and ending either at plant maturity or the last date climatic data was supplied, whichever comes first. Within this loop there are seven stages or modules (1).

The first stage calls the module LEAF which calculates the expansion of each leaf and adds this amount to the area of that particular leaf. This figure will then be used to

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(1) This loop with some modifications will later be referred to as the Daily Simulation Control Routine or DSCR.

calculate the amount of light intercepted by the plant. Leaf senescence (death due to aging) is accounted for by subtracting the maximum leaf area of the first leaf from the total leaf area at the time the twelfth leaf has reached its maximum area. This process then continues for each successive leaf which appears after the twelfth leaf. Once all the leaves have appeared the modeling of senescence continues by subtracting 0.4 percent of the total leaf area from the total area each day until maturity.

In the second and third stages, the EVAP and SOLWAT routines are called again to give the daily water evaporation and to update the soil water content, respectively. During initialization these routines were called to establish the soil condition for each day under the assumption that no plant was present. This data is now used as input on a daily basis and new figures are calculated based upon the presence of the sorghum plant. Although this seems to be a fine point on the differences between the initialization calls to EVAP and SOLWAT and the simulation calls, it is an important point. This is especially true for SOLWAT which takes the evaporation figures from EVAP and separates them into soil evaporation and plant evaporation both of which are taken from the soil content figure. The division is important from two standpoints; first in the initial calls no plant evaporation occurs, thus affecting the soil content in a different manner, and secondly in the simulation calls the moisture limiting factor for photosynthesis which is derived

in SOLWAT is a major factor on plant growth.

The fourth stage is for the simulation model to determine the stage of plant development. There are three important stages in the development of grain sorghum and the model must identify the current stage in order to apply certain important growth factors. The subroutine STAGE does this based upon the date that certain leaves reach their maximum leaf area which is an output from the LEAF routine. STAGE sets a common variable representing the plants development stage which is then referenced by the final three stages.

Stage five of the plant simulation is the most sophisticated and technically based portion of the model. In this stage the PHOTO subroutine is called to calculate the potential photosynthesis of the plant under each day's conditions. Since light interception is the most critical element in the model, the shading of leaves both from the plant itself and from neighboring plants becomes a critical factor. Complicating the problem is the fact that shading within the plant's canopy is dynamic, that is, it changes with the sun's altitude and azimuth and with plant's size. To account for these dynamic interactions the PHOTO routine applies a mathematical model developed by Arkin and Ritchie <2> to simulate the light interception in the grain sorghum plant canopy.

Using this model, PHOTO estimates the net potential

photosynthesis in terms of the amount of carbon dioxide fixed during daylight hours under certain common conditions. The calculations are made and summed for each hour of the daylight portion of the day. The result is a daily figure representing potential photosynthesis.

In stage six the potential photosynthesis is passed to the RPHOTO routine where a series of efficiency functions are applied to the data. These functions modify the potential photosynthesis to reflect a more realistic value based upon non-optimum temperatures and soil water conditions. There is an efficiency parameter for each environmental constraint on the photosynthetic rate. Examples of these would be night-time respiration loss, temperature conditions and soil water conditions. As an example of their effect, all photosynthesis stops below the temperature of minus five degrees C; thus all potential photosynthesis calculated below that temperature would be subtracted to give a zero rate for each hour the temperature was below minus five degrees C. Similarly, reduction in photosynthesis due to limiting soil moisture has been shown to be proportionate to the reduction in plant evaporation resulting from the limited water availability <7>. There is a threshold of extractable soil moisture below which plant evaporation is affected. This threshold is dependent upon the particular soil and enters the model as a single soil water holding capacity variable. The extractable soil water is determined daily by the model using a modified soil water balance routine developed by Ritchie <6>. Once the water

available has been reduced to 25% of the soil holding capability an effect upon net photosynthesis is seen.

The seventh and final stage of the Single Plant Model is the GROW routine. It is within this routine that all dry matter is partitioned between the various plant parts (root, leaf, culm, head, and grain). The basis of the distribution is the stage of development which is an output from the STAGE routine. The plant's growth is broken into three major phases and each phase gives a different dry matter distribution. Each part's weight is kept on an accumulative basis from day to day until maturity.

After the GROW routine has calculated the day's growth factors and they have been added to the plant's development, the model loops back to stage one and begins simulating the next day's growth. Final maturity is based upon 1.6 times the number of days to half-bloom (anthesis) which, in turn, is based upon leaf development.

In summary, the model goes through seven stages each day with each stage applying critical factors progressively until the final stage where the day's growth estimates are partitioned into the various plant parts. The plant's maturity date is calculated as a function of leaf development. These steps are summarized in Figures 1 and 2.

### III. OBJECTIVES AND APPROACHES

The following are the four main objectives of this project.

1. To add internal documentation to the main routines of the Single Plant Model.
2. To modularize the model into logical units in preparation for later updates and replacements.
3. To develop an acceptable approach to extending the Single Plant Model to a field population model.
4. To prove the validity of the approach by implementing divergence due to variations in emergence dates.

The first two objectives were to represent only about five percent of the project effort. The development of the field model was expected to account for approximately 40% of the project effort, while the remaining 55% was dedicated to converting the Single Plant Model into a field model in accordance with objective four.

A limited literature search was undertaken to study some of the more widely used plant simulation models. Included in the study was a cotton model developed at

Mississippi State <5>, a vegetative plant growth model <8>, a sugar beet model <4>, and a distribution model of organism Development times <3>. Although several of the models studied presented alternate approaches, the result of the study was that no new approach would be undertaken and the project would be oriented toward the Single Plant Model because of the large amount of local time and effort already committed to the Single Plant Model and the successes seen in its development.

Because of the already large size of the program that simulates the Single Plant Model (86K-bytes), the problem was to develop an approach which would not greatly increase the model's core requirements or run time.

The first serious approach considered was to partition the sorghum field into a variable number of segments, each of which would represent a specified combination of field variables. For example, a field consisting of two basic soil types, 60% of one and 40% of another would be split into two partitions representing 60% and 40% of the field, respectively. These partitions would then be sub-partitioned based upon a second variable, for example, there might be three separate emergence dates representing 30% emergence on day one, 40% on day two, and 30% on day three (2). This results in six partitions representing 18%,

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(2) That is 30% of all the plants which will emerge do so on the same day the first plant emerges while 40% emerge on the next day and all remaining plants emerge on day three.

12%, 24%, 16%, 18%, and 12% of the field. The process would continue for each field variable applicable to the model. The Single Plant Model would then be called to simulate each partition and a total field production would be estimated by weighting each partition based upon the percent of the entire field it represented.

There were several major difficulties with this approach. The number of simulations, and thus the run time required, appeared to grow exponentially with the number of field variables added to the model. Secondly, several of the crucial field variables do not become critical until later into the simulation itself. Since these variables could not be ignored, a modification was considered which would allow the model to dynamically add additional partitions during the simulation of any partition. These partitions would then be added to the list of partitions to be simulated. Although, the new approach cut down the initial number of partitions required, it allowed each partition to create new partitions which in turn could create still more partitions, etc. The approach was theoretically desirable but since there appeared to be no limit to the number of partitions which could be created, it was not considered realistically applicable.

An alternative solution was to apply the same theoretical approach, but in a more manageable structure. The idea was to build a dynamic tree structure which would allow the concurrent simulation of the various partitions on

a daily basis. The tree would grow dynamically each day with each leaf (3) representing a field partition. When a new field variable becomes critical at one of the leaves then that leaf would diverge into one or more additional leaves in preparation for the next day's simulation.

At first, a tree search routine was considered for limiting the number of nodes. With this approach partitioning or branching would be unlimited. At simulation time each branch would be searched to see if its simulation would be critical based upon policies which would have to be written into the program. Figure 4. demonstrates how this approach would have worked. In the beginning each branch is considered and only those nodes considered critical would be simulated (nodes 1,2,4, and 6). On the next day only those branches and their potential diverging (sons) branches would be considered. At day two nodes 1, 2, 7, 8, and 6 are simulated. This procedure would continue until all paths reach maturity.

Theoretically this approach also seemed acceptable because there are several known algorithms for tree searching and dynamic divergence would be allowed. However, some major difficulties arose. First allowing the creation of branches which may never be used increases storage requirements unnecessarily. Even if such unused branches were ignored and never stored in memory there would be no

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(3) The word 'leaf' or 'leaves' here represents leaves in the tree structure not leaves on the Sorghum plant.

limitations on the number of branch nodes which would have to be kept. The second major problem was that tree searching is a very time consuming process. It was felt that as much time would be used searching as simulating and if possible this should be eliminated. Therefore a modification was considered which would limit the number of partitions the tree structure would be allowed to diverge into by requiring that any new partition represent five percent or more of the entire field. Once a leaf matured its daily simulation would be discontinued, but the remaining leaves would be simulated on a daily basis until all leaves reached maturity.

This approach seemed to overcome all of the major objections to the previous alternatives considered. The maximum number of leaves which would have to be simulated on any given day would be twenty (4). This limited run time to an acceptable level. Secondly, the critical variables would be able to enter the system when they became critical without requiring any form of catch-up simulation time. However, if a variable which became critical represented less than 5% of the field, then it would not be considered crucial to the model as a whole and divergence would not be allowed. The only remaining concern was the amount of core that would be required to simultaneously simulate twenty plants. Since this approach had generated a considerable

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(4) There are at most twenty nodes representing 5% or more of a field. However, as will be seen later a twenty-first node is used for data accumulation after maturity.

amount of excitement, this concern was ruled secondary to the potential of the proposed data structure. It was hoped that the tree structure would lend itself to better memory management and that the core requirements could be reduced in the Single Plant Model itself.

Although the tree structure approach had several desirable characteristics, one additional modification was made to take advantage of the fact that with grain sorghum, it is quite common for a field variable which has become critical and has caused a slow-down in the plant's growth, to be eliminated before it causes too much damage. In this case, the plant could 'catch up' to its normal growth level. For example, a lack of available soil water in one area of the field might cause a slow-down in the growth rate in that partition (simulated by a divergence at that point). However, if rain comes, the plants in the partition may speed up growth until they reach the growth level of the rest of the field. To allow for this possibility the proposed data structure was modified from a tree structure with only divergence to a directed graph structure with divergence and convergence.

Convergence in the model is a unique concept that is expected to increase the accuracy of the model. Once a node matures it will be possible to merge the associated data and to free the node space for other uses. This concept of convergence add tremendous potential to the model from the stand point of the Agronomist, and it is perhaps as unique

as the proposed data structure itself.

The final conclusion was that a graph structure which allowed dynamic divergence and convergence of nodes would best serve the objectives of the project.

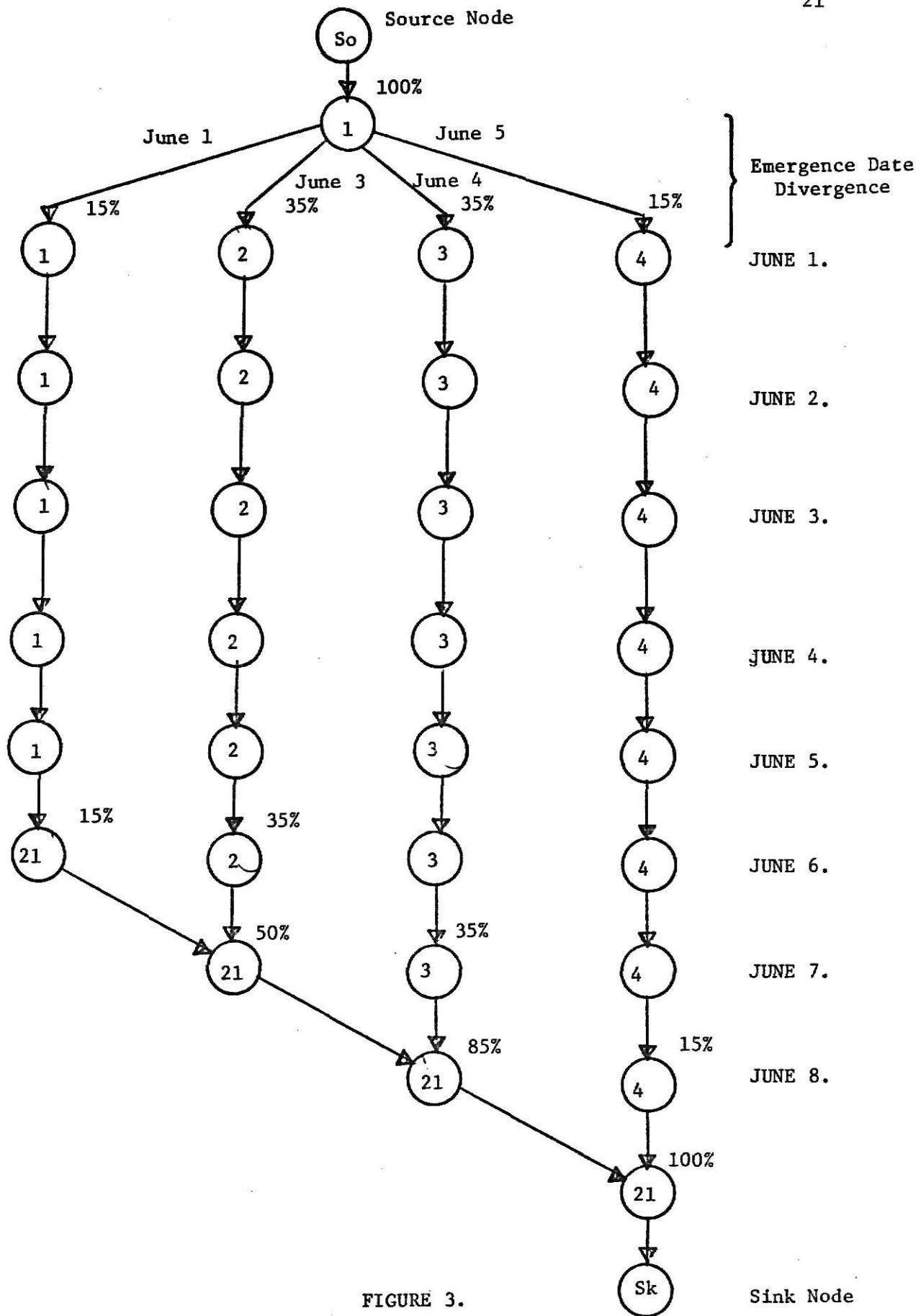
#### IV. THE PROPOSED DATA STRUCTURE

The core of the Field Level Model is its data structure. Figure 3 illustrates the gradual development of the model's digraph structure. The Source Node represents the field prior to entering the simulation model. The Sink Node at the bottom of the graph is a special node, where all simulation nodes are merged at maturity. It is represented in the program as the twenty-first element of each of the dimensioned variables in the NODBLK COMMON block. Node 1 represents the field as initialized from the reading of global and field variables; that is, one full set of data is read in and stored in the first of the twenty available nodes. At this point the weighting factor for the node is 100%. Immediately following the input of both the global and field data, the emergence routine is called to calculate the days and percent per day that emergence occurs. The Emergence Routine in turn calls the CREATE routine for each additional day emergence occurs. Each call to the CREATE routine represents a divergence of the node presently being processed.

For the example shown in Figure 3, four emergence days are shown (June 1, 3, 4, and 5). Therefore, CREATE must be called three times. The weighting factor for each node is calculated by the Emergence Routine; for our example, 15%, 35%, 35%, and 15% respectively. (Note that node one simply has had its emergence date established and its weighting factor changed.) After the necessary divergence has occurred

The Digraph Structure

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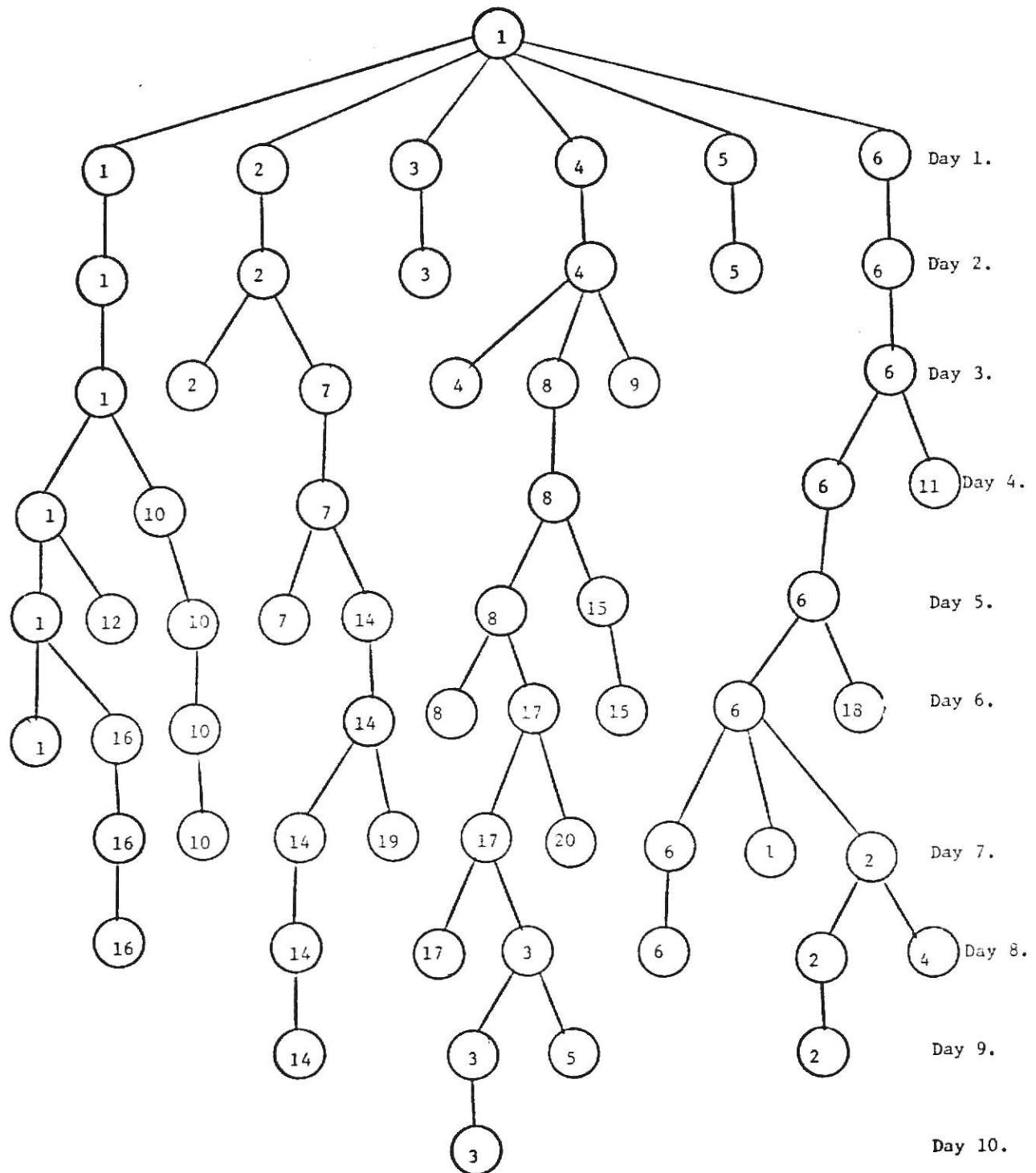
**Tree Search Approach**

FIGURE 4.

the main routine enters the Daily Simulation Control Routine. At this point the earliest emergence date is located and the daily simulation begins (in the above example June 1).

To simulate a node for a particular day, the Single Plant Model routine (SPMDOL) is called, which in turn follows the previously described procedure for the Single Plant Model (see section II). Once the simulation is completed control passes back to the Daily Simulation Control Routine in the main routine which checks to see if that node has reached maturity. If so, a flag is set which will allow that particular branch to be bypassed from the next day on. The control routine then uses the memory management scheme illustrated in Figure 5 (and described in the next section) to scan each of the remaining active nodes to see if its emergence date has been reached. If it has, then a check is made as to whether or not the node has already reached maturity. If the emergence date has not been reached or if maturity has already occurred then the node is bypassed. Otherwise, the SPMDOL is called for each active node. This process continues until all the nodes in the INUSE list (5) have been tested. At that point the date counters are incremented to the next day and the procedure is repeated.

In the example in Figure 3, the SPMDOL routine is

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(5) The INUSE list will be covered in the next section.

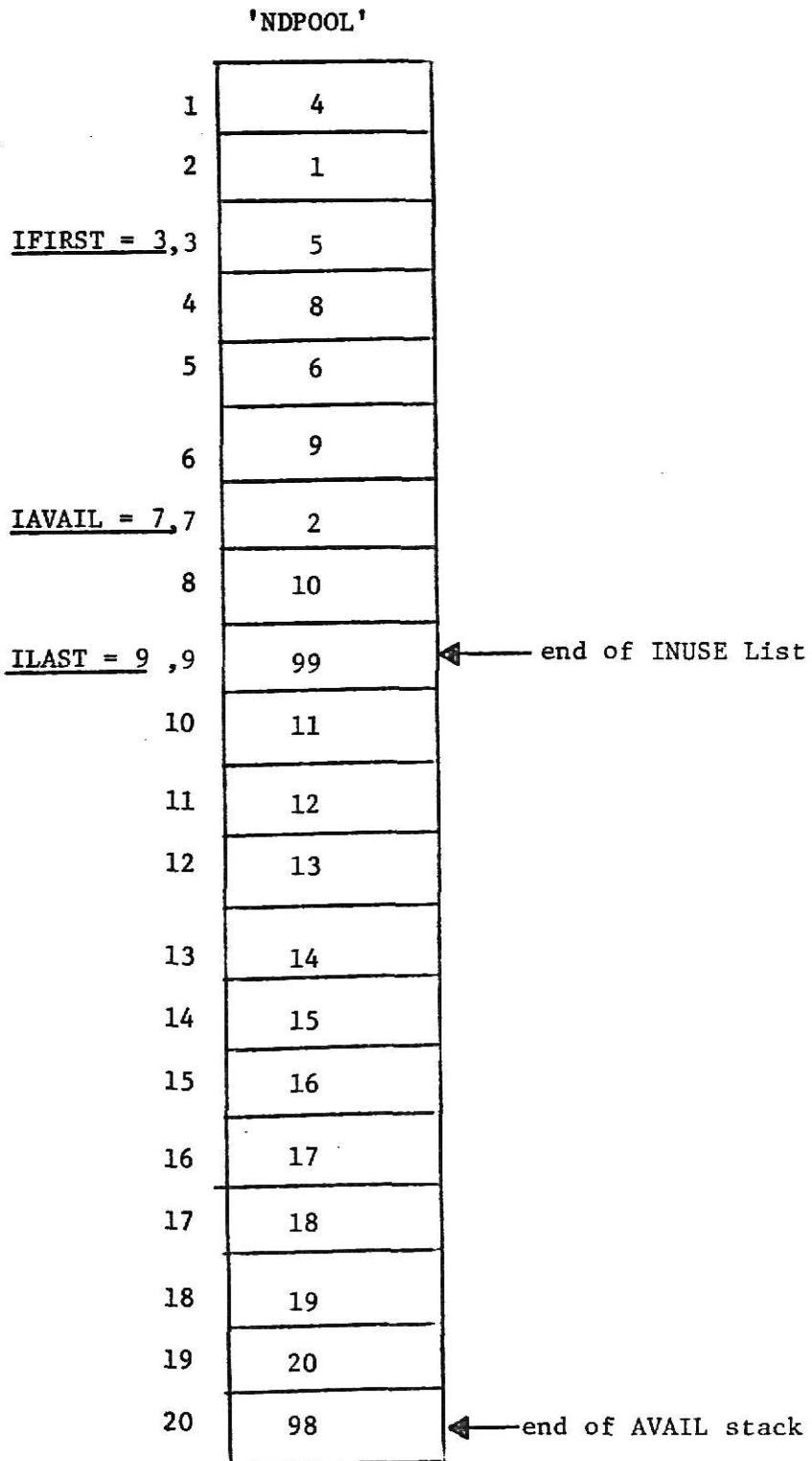


FIGURE 5.

called once for June 1 and once for June 2, both to simulate the 15% of the field represented by node 1. (The yellow nodes represent those nodes which are simulated each day.) On June 3 the SPMODL is called twice; once for node 1 and once for node 2. This process continues with each node entering the system as its emergence date is reached until June 5th where node 1 matures. At this point node 1 is merged into the Sink Node by the MERGE routine. Node 1's space is released by the FRNODE (free node) routine which is called by the MERGE routine and the daily simulation continues with one less node. Finally on June 9th the last node has reached maturity and is merged into the Sink Node (6). The daily simulation control routine senses this condition and passes control back to the main routine where the results are printed from the Sink Node. The field simulation is completed. The main routine next tries to read a new set of global and field data for a totally new field simulation. If no new data is available the program stops.

It is important, at this point, to note that the only convergence which actually occurs in the model as it is, is the converging of nodes 1, 2, 3, and 4 into the Sink Node (node 21). Objective four of this project stipulated that the emergence date variable would be used to test the proposed data structure. This stemmed from the fact that it is the emergence date variable which actually causes the

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(6) Obviously this example is not realistic.

first change in the various field plants. This change occurs prior to the model's entrance into the Daily Simulation Control Routine. The unfortunate aspect of using the emergence date for a test divergence is that, to date, no relationship has been developed for determining when various plants with different emergence dates can be considered similiar enough in growth to allow the model to converge. This question is still being researched. As a result, with the test data used, the only convergence that occurs is the merging of various nodes into the Sink Node. Section VII on Proposed Extentions will cover this problem in greater detail.

## V. MEMORY MANAGEMENT SCHEME

The one major drawback to the proposed data structure was the unknown factor of memory space requirements. This problem was complicated by the fact that the project was limited to a FORTRAN implementation (a stipulation set by the Agronomy Department) which has no instrument for allowing dynamic allocation and deallocation of memory. Because the Field Model would be creating and freeing nodes dynamically during the simulation process, it became necessary to establish some form of memory management to get freed nodes recycled back into the system. To accomplish this, a simple memory management scheme was established using an array of twenty pointers (called NDPOOL) and three special pointers (IAVAIL, IFIRST, and ILAST). The scheme is based upon two data structures; a queue called INUSE and a stack called AVAIL.

The INUSE queue is a linked list used to store pointers to the nodes which are presently in use by the model. IFIRST is a pointer to the node which has been in the queue the longest (called the bottom of the queue) and ILAST points to the last node added to the queue (the top of the queue). When new nodes are used ILAST is set to point to the new node and the node ILAST originally pointed to is set to point to the new node. However, contrary to the normal use of queues, IFIRST is not necessarily the next node to be taken off the queue. However, IFIRST is still of value as the node at which each new day's simulation begins.

The second data structure is the AVAIL stack which is a linked list of nodes which are not in use and which can be used by the model at any time. Access to AVAIL is always through the IAVAIL pointer which always points to the next available node. Since every node will be in one and only one of these two structures, one array can be used to store both structures. NDPOOL serves this function. Figure 5 shows how the INUSE queue and an AVAIL stack are both stored in NDPOOL. In Figure 5, the INUSE queue consists of nodes 3,5,6, and 9, respectively, and the rest of the nodes are on the AVAIL stack.

The first call to CREATE is made prior to reading in the field variables. This sets up the memory management pointers so that the first node is available for reading the field variables. At that point IFIRST is set to one which is the pointer into the INUSE list. NDPOOL(1) is set to 99 representing the end of the INUSE list (ie. there is only one node in use). ILAST is also set to one to point to the last node presently in use. This pointer will be used to add new nodes to the INUSE queue. The remaining NDPOOL elements are initialized to point to the next sequential element (for example, NDPOOL(4)=5, NDPOOL(5)=6, etc.) and the last NDPOOL element (NDPOOL(20)) is set to 98 to represent the end of the AVAIL stack. IAVAIL is set to 2 which is the first available node. This linked list is used as a stack with IAVAIL serving as the pointer for adding to or taking nodes from the AVAIL stack.

All other calls to the CREATE routine add an available node (the node pointed to by IAVAIL) to the end of the INUSE queue. IAVAIL is updated to the next available node. In addition, CREATE copies all node data from the node presently being processed to the newly created node, making no modifications to this data. The necessary modifications such as new weighting factors or emergence dates must be made by the routine calling CREATE after the new node has been created.

The CREATE routine does boundary checking to verify that nodes are available prior to allocating them. This condition should never occur, since nodes of less than 5% are not allowed. However, if it does occur CREATE will print an error message and force an immediate end to the program.

## VI. CONVERSION AND TESTING

Once the design of the Field Model was completed the conversion of the Single Plant Model to the Field Model was planned in three phases. The first phase was to modularize the Single Plant Model making it a Daily Simulation Routine (called SPMODL). This routine is called by a special section of the main routine which has been referred to as the Daily Simulation Control Routine (see Figure 3). In addition, a Block Data subroutine was added for load time initialization of most variables and an INITLZ routine was written to give run time initialization of the same variables. The INITLZ routine will be used for multiple simulation runs.

Implementing the daily simulation model involved a re-arrangement of the initial Single Plant Model which already had a daily simulation procedure imbedded within it. The procedure had to be extracted and made into a separate subroutine which would be called once for each node to be simulated for each day. The idea was to test the new structure with the same set of data as the original Single Plant Model. However, the debugging processes turned up several inherent program bugs which existed in the original Single Plant Model. Once these problems were corrected the two models corresponded and phase one was considered accomplished.

The second phase was to completely reorganize and

restructure the model's data structure. The Single Plant Model used six COMMON blocks, primarily for parameter passage. Since only parts of any particular block were used by each subroutine and since each subroutine had at least two or three COMMON blocks, this structure was overly complex. Its initial value in straightforward parameter passage had long since been lost in the numerous revisions and updates. As a result, phase two established two COMMON blocks. One block , NODBLK, is for the data relative to each node or leaf (field data) and the second block, COMBLK, is for the various other types of global data. NODBLK includes such items as emergence date, weighting percent, leaf area and leaf appearance dates. COMBLK has various independent variables such as those used in the memory management scheme, plus climatic data and daily light interception figures. In addition to using the two COMMON blocks, normal parameter passing via call statements were established. Again the procedure was to get the model to the point that it would correctly simulate one plant (node). Once the results matched those of the original Single Plant Model phase three, the hardest and most time consuming phase, was initiated.

The third and final phase of conversion involved modifying the new model to take advantage of the proposed digraph structure. The memory management scheme had to be implemented to create and free nodes and to keep track of all nodes in use and available. Divergence due to various emergence dates were forced at several locations within the

main routine in an effort to test the model's operation and to assure that all variables had been properly placed with respect to the new COMMON blocks. As set out in the objectives, the Emergence Data Routine was used as a policy for several divergences wherein several emergence dates and maturity dates could be used to test the model's accuracy and sensitivity.

Table 2 shows a summary of a test which forced three emergence divergences. Node 1 represented the test used on the Single Plant Model while node 2 had a forced divergence of two days prior to node 1 and node 3 was given an emergence date three days after node 1. The dates are given in Table 2 as Julian days from January 1. The second entry gives the anthesis or half-bloom point. As is seen in the table all three nodes are converging toward each other. Node 2 is only one day behind node 1 and node 3 is now only two days ahead of node 1 by half bloom. By maturity node 2 was still one day behind while node 1 had caught node 3 with both maturing on Julian day 211. Of course, the particulars of weather was a factor in the test. However, the results were reviewed and found to be in agreement with expected real plant responses.

## TABLE

|                | Node 1 | Node 2 | Node 3 |
|----------------|--------|--------|--------|
| Emergence Date | 0      | +3     | -2     |
| Half Bloom     | 210    | 211    | 208    |
| Maturity       | 242    | 242    | 240    |

Table 2. Summary of Field Model test results.

## VII. PROPOSED EXTENSIONS

As pointed out in the objectives, 95% of the project was to be oriented toward developing an approach for expanding the Single Plant Model to a field population model and then proving the approach is applicable by expanding the Single Plant Model to include the emergence date field variable. Obviously the emergence date field variable is only one of a number of potential field variables. The consequence of this is that the Field Level Model implemented by the project represents a very limited and narrow application of the proposed approach. This section will discuss how the implemented Field Level Model can be expanded to reach its full potential.

Among those variables which presently are being considered for the Field Level Model are tillering, available soil water, soil type, available nitrogen, hail damage, and seed distribution. It will not take many of these additional field variables to make the digraph structure very dynamic. Figure 6 exemplifies this fact by showing only two additional field variables; water availability and hail damage. It is easy to see the dynamic effects only three field variables could have on the digraph structure. The present Field Level Model was designed to allow easy inclusion of new field variables. There are, however, two new control modules which would have to be added. A Convergence Policy Control Routine (CPCR) and a Divergence Policy Control Routine (DPCR) would

have to be included to control the various sets of convergence and divergence policies. Figure 7 shows the proposed extended model's hierarch diagram. The red routines are the proposed extension routines. This proposed extension includes extracting the Daily Simulation Control Routine (DSCR), adding the Convergence Policy Control Routine, the Divergence Policy Control Routine, and the various Convergence and Divergence routines.

The Field Level Model is prepared for these extensions. The Divergence Policy Control Routine should be called prior to beginning a new day's simulation, and the Convergence Policy Control Routine should be called at the end of each day's simulation. Comment cards have been placed in the proper place in the program to indicate where these calls should occur. The objective in this calling arrangement is to allow the Divergence Policy Control Routine to scan the active field partitions (nodes) checking the condition of each node with the various divergence schemes available to it. If a candidate for divergence is found then the routine calls the proper divergence routine which does a detailed analysis of the field partition and, if necessary, calls CREATE to force a divergence. The control then passes back to the Divergence Policy Control Routine where statistical data is saved for later displaying and the rest of the nodes are scanned in the same manner. After all nodes have been scanned by the DPCR, the Daily Simulation Control Routine would be called to begin the simulation process for that day. After all active nodes

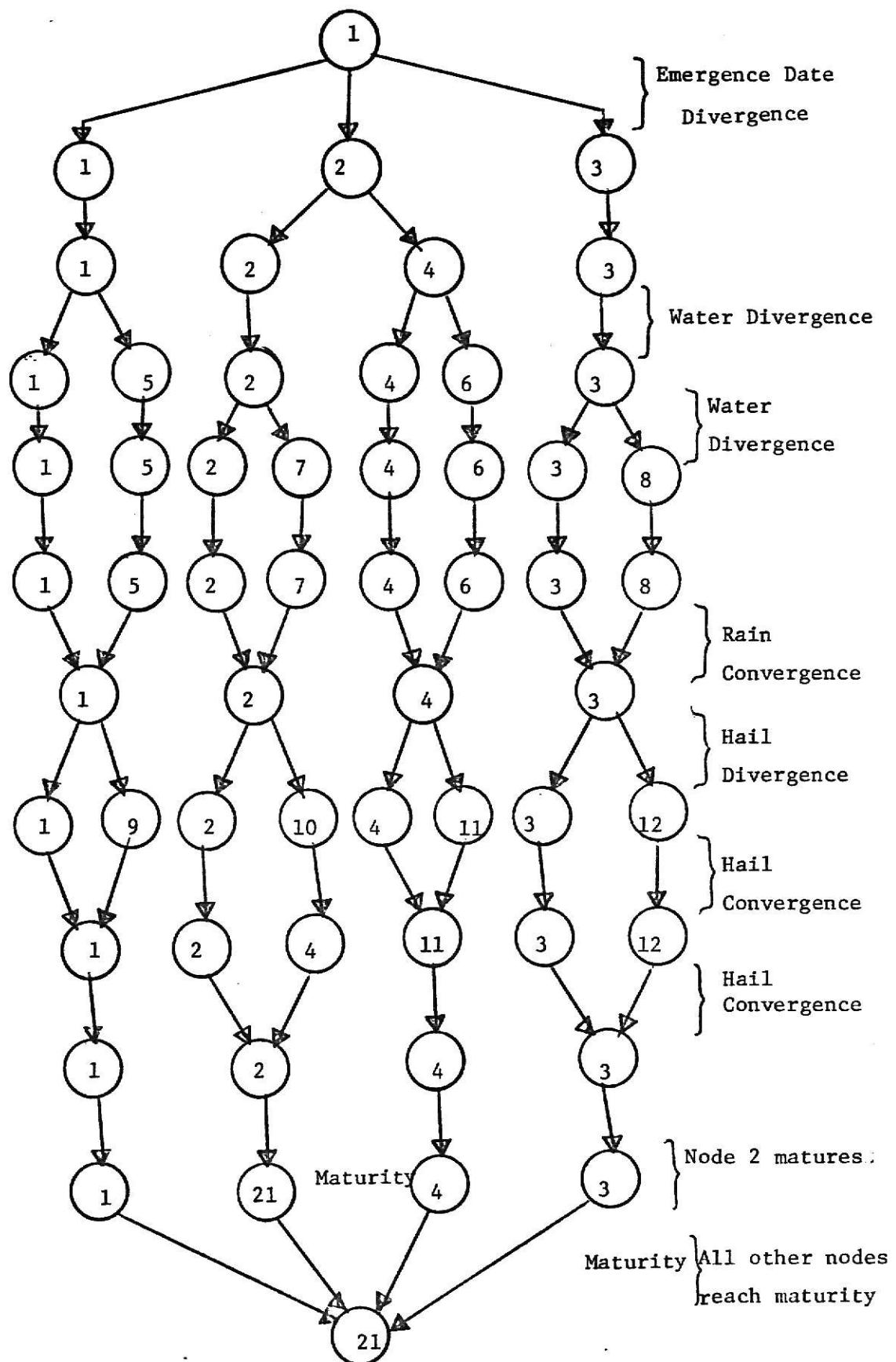


FIGURE 6.

**Field Level Model Hierarchy Diagram  
with Proposed Extensions**

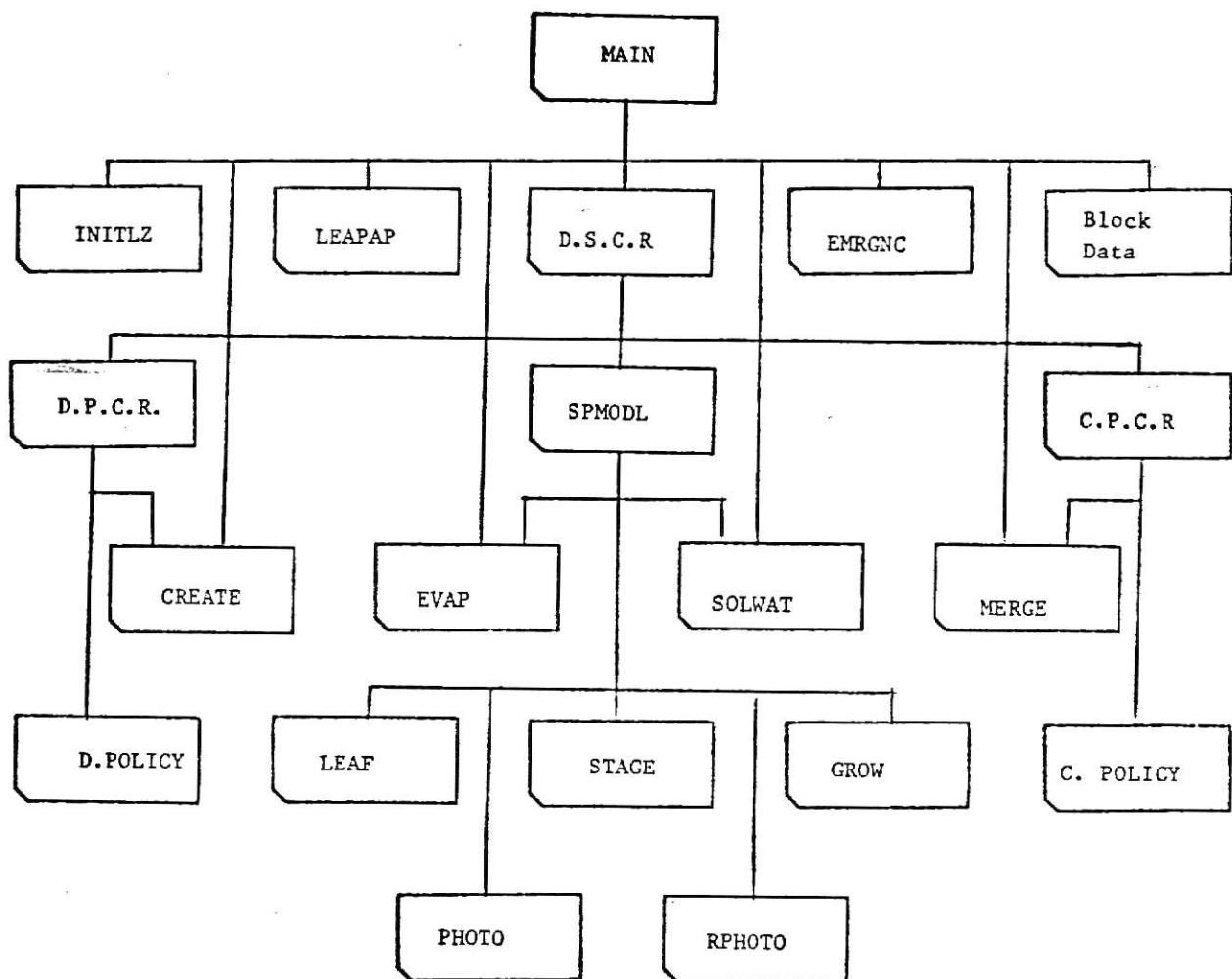


FIGURE 7.

have been simulated control would pass to the Convergence Policy Control Routine which would scan the INUSE list for any conditions which might warrant convergence. The MERGE routine would be called when necessary.

Convergence is allowed only with respect to an earlier divergence. This is to say that two field partitions can not merge simply because they look similar to the model. A convergence occurs, as explain earlier, when a critical field variable which caused a divergence earlier has been sufficiently effected to allow the plant to overcome its growth loss. At this point, and only at this point will convergence be allowed.

In order to facilitate this restriction a shared data base will be required between the DPCR and CPCR routines. The DPCR will add new data to the shared data base while the CPCR will access the data base to find candidates for convergence. After merging nodes, the CPCR will be allowed to update the shared data base.

Since the type and form of the information stored in the shared data base is totally dependent upon the convergence policies implemented, it was not a concern of this project to design the format of the shared data base. Again it should be pointed out that this particular structure was not required in the project model because no convergence policies, per se, were required.

## VIII. RESULTS AND CONCLUSIONS

The one major concern of the project was memory requirements. Efforts to reduce the memory requirements of the Single Plant Model were successfull in reducing execution requirements from 86K-bytes to 54K-bytes; a 37.2% reduction. The extension of the model raised the requirements to 76K-bytes. This resulted in a net improvement of 11.7% which is much better than was expected.

The field model was not expected to improve run time. In fact, initial estimates were that run time for the field model would increase directly with the number of nodes which had to be simulated. To test the model the Single Plant Model was run for one plant and using the same data, a field model was run forcing three divergences at the beginning. The anticipated run time was expected to be three times longer for the field model. The actual results were 2.7 times longer or slightly better than expected. This does, however, represent a serious consideration which must be taken into account when adding diverging policies; that is, that each daily simulation will take the same relative CPU time and too many diverging nodes can quickly cause drastic increases in run time.

Even under this constraint the proposed model structure offers a new and unique approach to crop population simulation. The feasibility of extending the model to a large number of field variables has been shown. Plans are

now being made and funding sought to expand the Field Level Model into four areas: hail damage, a better emergence model, nutrient effects, and tillering.

The conclusion drawn is that the proposed digraph structure is a good and viable approach to extending the Single Plant Model.

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## APPENDIX A

### Original Main Routine

```

COMMON /BLK1/GBO(366,20),XMAX(20),PDAYS(20),ROSPZ,PARE,A,TEMPCO,
1DAYPFO,LAT,WYE,BO,R2                                         CAR00180
COMMON /BLK2/TEPPMX(366),TEMPMN(366),TEMP(366),SPROUT,FERGDA   CAR00190
COMMON /BLK3/DLAI(366),SOLRAD(366),RAIN(366),SW,WATSCO,EO,UL,PLCAR00200
1L                                         CAR00210
COMMON /BLK4/RCOUNT(20),ACDAYS(20),N,1DAY3,1DAY6,1STAGE,DLA   CAR00220
COMMON /BLK5/F,WR,WL,WC,WH,WG,DRIWT,DWG,DWH,DWL,DWR          CAR00230
DIMENSION XDAY(21),SYDIN(20),TITLE(20),ICOR(12),FMT(20)       CAR00240
DATA HO,TOTWT/2*0./                                           CAR00250
DATA ICOR/1,-1,0,0,1,1,2,3,3,4,4,5/                           CAR00290
REAL LAT
98 READ(5,1301,END=100) TITLE
1301 FORMAT(20A4)                                              CAR00310
READ(5,1302) KI,N,MO,ND,IYR,ROSPZ,P,LAT,SW,UL,IFREQ
1302 FORMAT(5I4,F5.1,F10.0,3F5.2,T77.14)
READ(5,1000) (XMAX(J),J=1,N)
1000 FORMAT(10F7.2)
IF(MOD(IYR,4)) 1563,1564,1563
1564 LPY=1
GO TO 1569
1563 LPY=0
1569 ICDAY=30*(MO-1)+ICOR(MO-1)+ND+LPY
IMAX=ICDAY+KI-1
DO 5 J=1,N
PDAYS(J)=0.
RCOUNT(J)=0.
ACDAYS(J)=0.
DO 6 I=ICDAY,IMAX
GRO(I,J)=0.0
6 CONTINUE
5 CONTINUE
WR=0.
WL=0.
WC=0.

```

```

WH=0.
WG=0.
I STAGE=0
IDAY3=0
IDAY6=0
IDAY9=0
FMRGDA=0
1571 WRITE(6,1571) TITLE,ICDAY,MO,ND,IYR
      FORMAT(1H1,20A4//,5X,'PLANTING DATE=' ,I4,6X,'CALENDAR DAY=' ,3I6)
      IF(KI.EQ.0) GO TO 7
      READ(5,1301) FMT
      DO 4 K=1,KI
      READ(5,FET) (I,TEMPMX(I),TEMPMN(I),SOLRAD(I),RAIN(I))
      AVTEMP=(TEMPX(I)+TEMPN(I))/2.
      TEMP(I)=(AVTEMP-32.)*5./9.
      RAIN(I)=RAIN(I)*2.54
      4 CONTINUE
      7 CONTINUE
      CALL EMRGNC (ICDAY)
      I = SPROUT- (1.-FMRGDA) + .5
      ISPRT=SPROUT+.5
      XDAY(S(1))=0.0
      XDAY(S(2))=FMRGDA
      DO 102 J=1,N
      IF(J.NE.1) GO TO 1085
      RCOUNT(J)=SPROUT
      GO TO 1084
      104 SXDIN(J)=0.0
      PDAY(S(J-1))=XDAY(S(J))
      IF(XDAYS(2).GT.0.0) DAYS=SPROUT
      IF(XDAYS(S(J)).GT.0.) GO TO 13
      103 I=I+1
      DAYS=I
      IF(DAYS.GT.IMAX) GO TO 104
      13 AVTEMP=TEMP(I)
      IF(AVTEMP.GT.22) AVTEMP=22.
      IF(J.LT.6) GO TO 101
      IF(AVTEMP.LT.21.) GO TO 108
      CAR00420
      CAR00430
      CAR00440
      CAR00460
      CAR00470
      CAR00480
      CAR00490
      CAR00530
      CAR00540
      CAR00550
      CAR00560
      CAR00570
      CAR00580
      CAR00590
      CAR00600
      CAR00610
      CAR00620
      CAR00630
      CAR00640
      CAR00650
      CAR00660
      CAR00670
      CAR00680
      CAR00690
      CAR00700
      CAR00710
      CAR00720

```

```

      IF(TEMP(I) .GT. 30.) AVTEMP=30.
      DIN=2.957-.0562*(AVTEMP-21)
      GO TO 18
108   DIN=2.9+.0567*(AVTEMP-22.)***2
      GO TO 18
101   DIN=2.8+.0292*((AVTEMP-22.)***2)
18    IF(XDAYS(J).EQ.0.) GO TO 107
      XDIN=(1./DIN)*XDAYS(J)
      XDAYS(J)=0.0
      GO TO 14
107   XDIN=1./DIN
14    SXDIN(J)=XDIN+SDIN(J)
      IF(1.0-SXDIN(J)) 106,105,103
105   RCOUNT(J)=DAY_S
      XDAYS(J)=0.0
      GO TO 1108
106   XDAYS(J)=(SXDI(N(J)-1.0)*DIN
      RCOUNT(J)=DAY_S-XDAYS(J)
1108   XDAYS(J+1)=XDAYS(J)
      IF(J.EQ.N) PDAY(S(J)=XDAYS(J)
1084   WRITE(6,19) J,RCOUNT(J)
19    FORMAT(5X,'DAY LEAF',I3,' APPEARS = ',F7.2)
102   CONTINUE
104   CONTINUE
      PLL=UL*.25
      PAREA=100000000/P
      R2=PAREA/ROSPZ
      S=R2/ROSPZ
      WYE=0.404*ALOG(S)+1.49
      BO=EXP(-0.384*WYE)
      WRITE(6,22) P,ROSPZ,R2,PAREA
22    FORMAT(//,' PLANT SPACING= ',1X,F6.1,' AREA PER PLANT= ',1X,
      1F6.2,' ROW SPACING= ',1X,F6.2)
      WRITE(6,1001)
1001  FORMAT(//4X,'JULIAN DAY',3X,'STAGE',2X,'ROOT WT',3X,'LEAF WT',
      1,3X,'CULM WT',3X,'HEAD WT',3X,'GRAIN WT',2X,'TOTAL WT',3X,'LA,CM',CARO1070
      27X,'LAI',3X,'TCO',2X,'WCO',3X,'SW')
      DO 200 I=ISPRIT,IMAX
          CARO1090

```

```

CALL LEAF (I) CAR01100
CALL EVAP (I) CAR01110
CALL SOLWAT (I) CAR01120
CALL STAGE (I) CAR01130
CALL PHOTO (I) CAR01140
IF (TEMP(I).LT..5.0.OR.TEMP(I).GE..45.0) TEMP0=0. CAR01150
IF (TEMP(I).GE..25.0.AND.TEMP(I).LE..40.0) TEMP0=1. CAR01160
IF (TEMP(I).GE..5.0.AND.TEMP(I).LE..25.) TEMP0=.05*TEMP(I)-.25 CAR01170
IF (TEMP(I).GT..40.0.AND.TEMP(I).LT..45.) TEMP0=-.2*TEMP(I)+.9. CAR01180
TOFOTO=TEMP0*WATSCO*DAY PFO
TEMPN=(TEMPN(I)+TEMP(I))/2.
RESPG=.14*(.65+.011*TEMPN)
RESPN=RESPG*T0FOTO+RESPN*(TOTWT+WR)*1.43
TOFOTO=TOFOTO-RESPN
IF (TOFOTO.EQ.0.) WRITE(6,1003) TEMP0, WATSCO, DAYPFO
1003 FORMAT(1X,'TEMP0='',F4.2,5X,'WATSCO='',F4.2,5X,'DAYPFO='',F5.1)
DRIWT=TOFOTO*(PAREA/100.)*(12./44.)*(1./.4)*.001
CALL GROW (I)
TOTWT=WL+WC+WH+WG
IPRINT=I-1
IF (ISTAGE.EQ.5) GO TO 1006
IF (I.NE.IDAY6) GO TO 1007
WRITE(6,1005) I
1005 FORMAT(1X,'ANTHESES OCCURRED ON JULIAN DAY',I4)
1007 IF (MOD(IPRINT,1FREQ)) 200,1006,200
1006 WRITE(6,2000) I,IPRINT,ISTAGE,WR,WL,WC,WH,WG,TOTWT,DLA,DLAI (I),
1TEMP0,WATSCO,SW
2000 FORMAT(6X,I3,('I3,'),5X,I2,8F10.3,2F5.1,2F6.1)
1008 IF (ISTAGE.EQ.5) GO TO 201
200 CONTINUE
IF (ISTAGE.EQ.5) GO TO 201
WRITE(6,1004) IDAY9
1004 FORMAT('/1X,'PHYSIOLOGICAL MATURITY NOT REACHED.'/1X,'PREDICTED ON
1 JULIAN DAY',2X,I4//)
GO TO 99
201 WRITE(6,1002) I
1002 FORMAT('/1X,'PHYSIOLOGICAL MATURITY OCCURRED ON JULIAN DAY',I4//) CAR01470

```

99 CONTINUE  
      GO TO 98  
100 STOP  
      END

## APPENDIX B

## FIELD MODEL SOURCE LISTING

```

$JOB COMMON/NODBLK/NODE, IDAY(20), SUMES1(20), SUMES2(20), T(20), PDAY(20), PERCNT(21), XDAYS
      1INT(20), SUMES1(20), SUMES2(20), T(20), PDAY(20), PERCNT(21), XDAYS
      2(20,21), GRO(20,2,20), XMAX(20,20), SPROUT(20), SW(20), UL(20), PLL(20)
      3,RCOUNT(20,20), AC DAYS(20,20), IDAY3(20), IDAY6(20), IDAY9(20)
      4,ISTAGE(20), DLA(20), WR(21), WL(21), WC(21), WH(21), MG(21)
      COMMON/SPECIAL/ISPRT(20)
      COMMON/COMBLK/ROSPZ, PAREA, N,
      1TEMPCO, DAYPFO, LAT, WYE, BO, R2
      COMMON/COMBLK/TEMPMX(366), TEMPNN(366), TEMP(366), FMRGDA
      COMMON/COMBLK/DLAI(366), SOLRAD(366), RAIN(366), WATSCO, EOS, EO
      COMMON/COMBLK/F, DRIWT, DWG, DWH, DWC
      COMMON/COMBLK/SGDD, PMGDD, IAVAIL, IFIRST, ILAST, NDPOOL(20), MATURE(20)
      DATA HO, TOTWT/2*0./
      DIMENSION TITLE(20), ICOR(12), FMT(20), ACTW(366)
      DATA ICOR/1,-1,0,0,1,1,2,3,3,4,4,5/
      REAL LAT
      1571 FORMAT(1H1,20A4//,5X,'PLANTING DATE=',I4,6X,'CALENDAR DAY=',3I6)   CAR00430
      1000 FORMAT(10F7.2)               CAR00350
      1302 FORMAT(5I4,F5.1,F10.0,3F5.2,T77,14)                                CAR00310
      1301 FORMAT(20A4)               CAR01470
      1002 FORMAT(1IX,'PHYSIOLOGICAL MATURITY OCCURRED ON JULIAN DAY',I4//) CAR01430
      1004 FORMAT(1IX,'PHYSIOLOGICAL MATURITY NOT REACHED.'/1X,'PREDICTED ON'    CAR01440
      1 JULIAN DAY',2X,14//)
      2000 FORMAT(6X,I3,(13,1),'5X,I2,8F10.3,2F5.1,F6.1,3X,12)           CAR01380
      1005 FORMAT(1X,'ANTHEISIS OCCURRED ON JULIAN DAY',14)                   CAR01340
      CC THE FIRST PASS THROUGH- ALL VARIABLES ARE INITIALIZED BY
      CC THE BLOCK DATA ROUTINE THEREFORE THE CALL INITLZ IS
      CC BYPASSED. ALL OTHER PASSES CALL INITLZ TO INITIALIZE
      CC NECESSARY VARIABLES.
      CC
      DO 21 I=1,20

```

```

1 DAY(I)=0
DO 24 K=1,20
DO 23 J=1,2
23 GRO(I,J,K)=0.
24 CONTINUE
21 CONTINUE
NODE=0
      CALL CREATE
      PERCNT(NODE)=.20
      LOOP=0
97 IF(LOOP.NE.0)CALL INITLZ
      LOOP=1
      ----- READ DATA ROUTINE -----
CC
CC 98 READ(5,1301,END=100) TITLE
C
C   READ(5,1302) KI, N, MO, ND, IYR, R0SPZ, P, LAT, SW(NODE), UL(NODE), IFREQ
C   IFREQ=1
C   READ(5,1000) (XMAX(NODE,J),J=1,N)
C
C   CONVERT JULIAN DATES TO CALENDAR DATES
C
C   IF (MOD(IYR, 4)) 1563,1564,1563
C   LPY =1
C   GR TD 1569
C   1563 LPY =0
C   1569 ICDAY=30*(40-1)+ICOR(MO-1)+ND+LPY
C
C   ----- PRINT HEADINGS AND TITLE -----
CC
CC  WRITE(6,1571) TITLE,ICDAY,MO,ND,IYR
C
C   READ RAIN AND TEMP DATA AND CONVERT TO METRIC
C
C   IF(KI.EQ.0) GO TO 7
C   IMAX=ICDAY+KI-1
C   READ(5,1301) FMT
C
C   CAR00360
C   CAR00370
C   CAR00380
C   CAR00390
C   CAR00400
C
C   CAR00420
C
C   CAR00410
C   CAR00440

```

```

DO 4 K=1,K1
  READ(5,FMT) I,TEMPMX(I),TEMPMN(I),SOLRAD(I),RAIN(I)
  TEMP MX(I)=(TEMP MX(I)-32.)*5./9.
  TEMP MN(I)=(TEMP MN(I)-32.)*5./9.
  TEMP(I)=(TEMP MX(I)+TEMP MN(I))/2.
  RAIN(I)=RAIN(I)*2.54
  C
  C   CALCULATE EVAPORATION AND SOILWATER CONTENT WITHOUT PLANT'S
  C   PRESENCE IN THE SOIL, THEN FIND EMERGENCE DATE
  C
  CALL EVAP (I)
  CALL SOLWAT (I)
  ACTW(I)=SW(NODE)
  C
  4 CONTINUE
  7 CONTINUE
  CALL EMRGNC (ICDAY)
  C
  ISPR(T(NODE) = DAY NUMBER OF EMERGENCE FOR THE 'NODE' TH GROUP
  C
  C TEST CALL
  CALL CREATE
  PERCENT(ILAST)=.40
  SPROUT(ILAST)=SPROUT(NODE)+3.
  CALL CREATE
  SPROUT(ILAST)=SPROUT(NODE)-2.
  PERCENT(ILAST)=.40
  NODE=IFIRST
  IBEGIN=366
  C
  C   CALCULATE LEAF APPEARANCE DATES
  C   FOR ALL INITIAL NODES
  C   PRINT THESE DATA TIMES FIVE NODES AT
  C   ALSO FIND THE SMALLEST EMERGENCE DATE FOR
  C   BEGINNING THE SIMULATION LOOP FOLLOWING
  C
  25 I=SPROUT(NODE)-(1.-FMRGDA) + .5
  ISPR(T(NODE)=SPROUT(NODE)+ .5
  CALL LEAFAP (J,I,IMAX)
  C

```

```

IF( IBEGIN.GE.ISPRT(NODE) ) IBEGIN=ISPRT(NODE)
PLL(NODE)=UL(NODE)*.25
NODE=NDPOOL(NODE)
IF( NODE.NE.99 ) GO TO 25
NODE=IFIRST

CC          CALCULATE PLANT SPACING DATA
C
C
PARFA=10000000/P
R2=PARFA/ROSPZ
S=R2/RROSPZ
WYE=0.404*ALOG(S)+1.49
BO=EXP(-0.384*WYE)
WRITE(6,22) P,ROSPZ,R2,PAREA
FORMAT(1//1/,PLANTS PER HECTARE='1X,F10.0,/,ROW SPACING='1X,
1F6.2/,PLANT SPACING='1X,F6.1,/,AREA PER PLANT='1X,F8.2)
CARO1040
CARO1050
FORMAT(1//4X,'JULIAN DAY',3X,'STAGE',2X,'ROOT WT',3X,'LEAF WT',
1,3X,'CULM WT',3X,'HEAD WT',3X,'GRAIN WT',2X,'TOTAL WT',3X,'LA,CM',CARO1070
27X,'LAI',3X,'TCO',2X,'WCO',3X,'SW')
C          DAILY GROWTH SIMULATION
C
DO 200 I=IBEGIN,IMAX
NODE=IFIRST
CONTINUE
10
C          INSERT DIVERGENCE POLICY CONTROL ROUTINE HERE
C
        IF (MATURE(NODE).EQ.1) GO TO 11
CC          CALL THE SINGLE PLANT MODULE TO CALCULATE DAILY GROWTH
CC
        IF(I.LE.ISPRT(NODE))GO TO 11
        IF(I.EQ.ISPRT(NODE))SW(NODE)=ACTW(I)
        CALL SPMODL (I, TOTWT)
CC          CHECK TO SEE IF REQUESTED PRINT POINT HAS

```

```

C BEEN REACHED, IF SO PRINT, ELSE CCONTINUE
C
C IPRINT IS THE NUMBER OF DAYS OF THE NODE
C FROM EMERGENCE

C IPRINT(NODE)=I-1SPRT(NODE)
C IF(ISTAGE(NODE).EQ.5) GO TO 1006
C IF(I.NE.IDAY6(NODE)) GO TO 1007
C WRITE(6,1005) 1
C
C 1007 IF(MOD(IPRINT(NODE),IFREQ)) 11,1006,11
C 1006 WRITE(6,2000)I,IPRINT(NODE),ISTAGE(NODE),WR(NODE),
C 1 WC(NODE),WH(NODE),WG(NODE),TOTWT,DLA(NODE),DLAI(I),
C 2 TEMPCO,WATSCO,SW(NODE),NODE
C
C IF NODE IS MATURE ALREADY THEN MATURE(NODE)=1
C
C IF(ISTAGE(NODE).EQ.5) GO TO 201
C IF((ISTAGE(NODE).NE.5) GO TO 11
C   WRITE(6,1002) 1
C   MATURE(NODE)=1
C   CONTINUE
C
C INSERT CONVERGENCE CONTROL ROUTINE HERE
C
C NODE=NDPOOL(NODE)
C IF((NODE.NE.99) GO TO 10
C
C 200 CONTINUE
C   NODE=IFIRST
C   CONTINUE
C
C 95 IF ((MATURE(NODE).NE.1) GO TO 96
C   CALL MERGE(NODE,21)
C   GO TO 99
C
C 96 CONTINUE
C   IF(ISTAGE(NODE).EQ.5) GO TO 201
C   WRITE(6,1004) IDAY9(NODE)
C   GO TO 99
C
C 201 WRITE(6,1002) 1

```

```

99 CONTINUE NODE=NDPOOL(NODE)
IF (NODE.NE.99) GO TO 95

C FINAL NODE HAS MATURED--PRINT SINK NODE VALUES
C FLDWT=WL(21)+WC(21)+WH(21)+WG(21)
WRITE(6,1003)
1003 FORMAT (3X,'FIELD MATURITY REACHED')
      WRITE (6,1008) WL(21),WC(21),WH(21),WG(21),FLDWT
1008 FORMAT (3X,'LEAF= ',F10.3,3X,'CLUM= ',F10.3,3X,'HEAD= ',F10.3,3X
1,'GRAIN= ',F10.3,3X,3X,'FINAL TOTAL WT = ',F10.3)
GO TO 97
100 STOP
END

BLOCK DATA
COMMON/NODEBLK/NODE, IDAY(20),PL(20),YDLA(20),JDAY(20),ICOMP(20),IP
1PRINT(20),SUMES1(20),SUMES2(20),T(20),PDAYS(20,20),PERCNT(21),XDAYS
2(20,21),GRD(20,2,20),XMAX(20,20),SPROUT(20),SW(20),UL(20),PLL(20)
3,RCOUNT(20,20),ACDAYS(20,20),IDAY3(20),IDAY6(20),IDAY9(20)
4,ISTAGE(20),DLA(20),WR(21),WL(21),WC(21),WH(21),WG(21)
COMMON/SPECIAL/ISPRT(20)
COMMON/COMBLK/ROSPZ,PAREA,N,
1TEMPCO,DAYPFO,LAT,WYE,B0,R2
COMMON/COMBLK/TEMPMX(366),TEMPMN(366),TEMP(366),FMRGDA
COMMON/COMBLK/DLAI(366),SOLRAD(366),RAIN(366),WATSCO,EOS,EO
COMMON/COMBLK/F,DRINT,DWG,DWH,DWC
COMMON/COMBLK/SGDD,PMGDD,IAVAIL,IFIRST,ILAST,NDPOOL(20),MATURE(20)
DATA DLAI,UL,SW,PLL,SUMES1,SUMES2,ISPRT/366*0.,100*0.,20*0/
DATA PDAYS,XMAX/800*0./,RCOUNT/400*0./,ACDAYS/400*0./
DATA SPROUT/20*0./,DLA/20*0./
DATA WL,WC,WH,WG,SGDD,PMGDD,FMRGDA,WR,I STAGE,
1 IDAY3, IDAY6, IDAY9, IFREQ, IDAY/108*0.,80*0,5,20*0/
DATA IAVAIL,IFIRST,NDPOOL,MATURE/1,99,40*0/
DATA NODE,JDAY,ICOMP/41*0/,PL,YDLA/40*0./
DATA PEPCTN/20*0.,100./

END
SUBROUTINE CREATE

```

```

COMMON/NDBLCK/NODE, IDAY( 20 ), PL( 20 ), YDLA( 20 ), JDAY( 20 ), ICOMP( 20 ), IP
1RINT( 20 ), SUMES1( 20 ), SUMES2( 20 ), T( 20 ), PDAYS( 20, 20 ), PERCNT( 21 ), XDAYS
2( 20, 21 ), GRO( 20, 2, 20 ), XMAX( 20, 20 ), SPROUT( 20 ), SW( 20 ), UL( 20 ), PLL( 20 )
3, RCOUNT( 20, 20 ), ACDAYS( 20, 20 ), IDAY3( 20 ), IDAY6( 20 ), IDAY9( 20 )
4, I STAGE( 20 ), DLA( 20 ), WR( 21 ), WL( 21 ), WC( 21 ), WH( 21 ), WG( 21 )

COMMON/SPECIAL/ISPR( 20 )
COMMON/COMBLK/RDSPZ, PAREA, N,
1TEMPCO, DAYPFO, LAT, WYE, BO, R2
COMMON/COMBLK/TEMPMX( 366 ), TEMPMN( 366 ), TEMP( 366 ), FMRGDA
.COMMON/COMBLK/DLAI( 366 ), SOLRAD( 366 ), RAIN( 366 ), WATSCO, EOS, EO
COMMON/COMBLK/F, DRIWT, DWG, DWH, DWC
COMMON/COMBLK/SGDD, PMGDD, IAVAIL, IFIRST, ILAST, NDPOOL( 20 ), MATURE( 20 )

C   C   IF NODE=0 THEN INITILIZE MEMORY MANAGEMENT POINTERS
C
C   IF (NODE.NE.0) GO TO 5
      NODE=1
      IFIRST=1
      IAVAIL=2
      NDPOOL( 1 )=99
      ILAST=1
      DO 20 I=2, 19
         NDPOOL( I )=I+1
      20   NDPOOL( 20 )=99
      RETURN
5. IF (IAVAIL.NE.99) GO TO 10
      FORMAT( 1X, 'ERROR--NODE OVERFLOW, IN CREATE SUBROUTINE' )
      WRITE( 5, 100 )
      STOP

C   C   COPY DATA FROM PRESENT NODE TO NEXT AVAIL NODE
C
C   10 DO 15 I=1, 20
      GRO( IAVAIL, 1, 1 )=GRO( NODE, 1, 1 )
      PDAYS( IAVAIL, 1 )=PDAYS( NODE, 1 )
      GRN( IAVAIL, 2, 1 )=GRN( NODE, 2, 1 )
      XMAX( IAVAIL, 1 )=XMAX( NODE, 1 )
      RCOUNT( IAVAIL, 1 )=RCOUNT( NODE, 1 )

```

```

1RINT(20),SUMES1(20),SUMES2(20),T(20),PDAYS(20,20),PERCNT(21),XDAYS
2(20,21),GRO(20,2,20),XMAX(20,20),SPROUT(20),SW(20),UL(20),PLL(20)
3,RCOUNT(20,20),ACDAYS(20,20),IDAY3(20),IDAY6(20),IDAY9(20)
4,IStage(20),DLA(20),WR(21),WL(21),WC(21),WH(21),WG(21)
COMMON/COMBLK/ROSPZ,PAREA,N,
1TEMPCO,DAYPFO,LAT,WYE,B0,R2
COMMON/COMBLK/TEPPMX(366),TEMPMN(366),TEMP(366),FMRGDA
COMMON/COMBLK/DLAI(366),SOLRAD(366),RAIN(366),WATSCO,EOS,EO
COMMON/COMBLK/F,CRIWT,DWG,DWH,DWC
COMMON/COMBLK/SGDD,PMGDD,IAVAIL,IFIRST,ILAST,NDPOOL(20),MATURE(20)

C THIS ROUTINE MERGES THE FRCM-NODE (NODEF)
C INTO THE TO-NODE (NODET) WHERE PERCENT (NODET)
C IS GT PERCENT (NODEF)

C - AS IMPLEMENTED ONLY DRY MATTER OF PLANT PARTS
C AND PERCENT ARE MERGED
C -WHEN CONVERGENCE POLICIES ARE ADDED THIS ROUTINE
C MUST BE EXPANDED

C IF(NODET.EQ.21)GO TO 50
C IF (PERCNT (NODET).GE.PERCNT (NODEF)) GO TO 50
C NDSAVE = NODET
C NODET = NODEF
C NODEF = NDSAVE
C 50 CONTINUE

C COMBINE PLANT PARTS AND PERCENT

C WR(NODET) = WR (NODET)+WR (NODEF)
C WL(NODET) = WL (NODET)+WL (NODEF)
C WC(NODET) = WC (NODET)+WC (NODEF)
C WH(NODET) = WH (NODET)+WH (NODEF)
C WG(NODET) = WG(NODET)+WG (NODEF)
C PERCENT(NODET)=PERCENT (NODET)+PERCENT (NODEF)
C CALL FRNODE (NODEF)
C WRITE(6,1000) NODEF,NODET
C WRITE(6,1005)

```

```

ISPRTR(IAVAIL)=ISPRTR(NODE)
ACDAYS(IAVAIL,I)=ACDAYS(NODE,I)
CONTINUE
15
IDAY(IAVAIL)=IDAY(NODE)
PL(IAVAIL)=PL(NODE)
YDLA(IAVAIL)=YDLA(NODE)
JDAY(IAVAIL)=JDAY(NODE)
ICOMP(IAVAIL)=ICOMP(NODE)
MATURE(IAVAIL)=MATURE(NODE)
SPROUT(IAVAIL)=SPROUT(NODE)
SW(IAVAIL)=SW(NODE)
UL(IAVAIL)=UL(NODE)
PLL(IAVAIL)=PLL(NODE)
IDAY3(IAVAIL)=IDAY3(NODE)
IDAY6(IAVAIL)=IDAY6(NODE)
IDAY9(IAVAIL)=IDAY9(NODE)
ISTAGE(IAVAIL)=ISTAGE(NODE)
DLA(IAVAIL)=DLA(NODE)
WR(IAVAIL)=WR(NODE)
WL(IAVAIL)=WL(NODE)
WC(IAVAIL)=WC(NODE)
WH(IAVAIL)=WH(NODE)
WG(IAVAIL)=WG(NODE)
SUMES1(IAVAIL)=SUMES1(NODE)
SUMES2(IAVAIL)=SUMES2(NODE)
T(IAVAIL)=T(NODE)

UPDATE NODE POOL ARRAY NDPOOL
C C C
ITEMPX=NDPOOL(IAVAIL)
NDPOOL(IAVAIL)=99
NDPOOL(ILAST)=IAVAIL
ILAST=IAVAIL
IAVAIL=ITEMPX
RETURN
END

SUBROUTINE MERGE (NODEF, NODET)
COMMON/NODBLK/NODX, IDAY(20), PL(20), YDLA(20), JDAY(20), ICOMP(20), IP

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```

1005 FORMAT (1H1)
1000 FORMAT (2X,'NODE ',I2,1X,'MERGED INTO NODE ',I2)
      RETURN
END
      SUBROUTINE FRNODC (NODE)
COMMON/NODBLK/NODX, IDAY(20), PL(20), YDLA(20), JDAY(20), ICOMP(20), IP
1RINT(20), SUMES1(20), SUMES2(20), T(20), PDAYS(20,20), PERCNT(21), XDAYS
2(20,21), GRO(20,2,20), XMAX(20,20), SPROUT(20), SW(20), UL(20), PLL(20)
3,RCOUNT(20,20),ACDAY$1(20,20),IDAY3(20),IDAY6(20),IDAY9(20)
4,ISTAGE(20),DLA(20),WR(21),WL(21),WC(21),WH(21),WG(21)
COMMON/COMBLK/ROSPZ, PAREA,N,
COMMON/COMBLK/TEMPMX(366),TEMPMN(366),TEMP(366),FMRGDA
COMMON/COMBLK/DLA1(366),SOLRAD(366),RAIN(366),WATSCO,EOS,EO
COMMON/CCMBLK/F,DRIWT,DWG,DWH,DWC
COMMON/CORMLK/SGDD,PMGDD,IAVAIL,IFIRST,ILAST,NDPOOL(20),MATURE(20)
      FIND FDPOOL NODE POINTING TO NODE TO BE DELETED-LSAVE
      FIND FDPOOL NODE POINTING TO ILAST NODE- LSAVE
C
C
      ISAVE=0
      LSAVE=0
      DO 50 I=1,20
      IF (NDPOOL(I).EQ.NODE) ISAVE=1
      IF (NDPOOL(I).EQ.ILAST) LSAVE=1
      50 CONTINUE

C
C
      IF NODE TO BE DELETE IS IFIRST THEN UPDATE IFIRST
      C
      UPDATE NDPOOL NODE POINTING TO NODE TO BE DELETED
      C
      UPDATE IAVAIL TO NEW FREED NODE
      IF(NODE.EQ.ILAST) ILAST=LSAVE
      IF (NODE.EQ.IFIRST) IFIRST=NDPOOL(IFIRST)
      IF (ISAVE.NE.0) NDPOOL(ISAVE)=NDPOOL(NODE)
      NDPOOL(NODE) = IAVAIL
      IAVAIL = NODE
      RETURN
END
      SUBROUTINE SPMODL (I, TOTWT)
COMMON/NODBLK/NODE, IDAY(20), PL(20), YDLA(20), JDAY(20), ICOMP(20), IP

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```

1PINT(20),SUMES1(20),SUMES2(20),T(20),PDAY(20),PERCNT(21),XDAYS
2(20,21),GRO(20,2,20),XMAX(20,20),SPROUT(20),SW(20),UL(20),PLL(20)
3,RCOUNT(20,20),ACDAYS(20,20),IDAY3(20),IDAY6(20),IDAY9(20)
4,ISTAGE(20),DLA(20),WR(21),WL(21),WC(21),WH(21),WG(21)
COMMON/COMBLK/ROSPZ,PAREA,N,
1TEMPCO, DAYPFO, LAT, WYE, BO, R2
COMMON/COMBLK/TEMPMX(366), TEMPMLN(366), TEMP(366), FMRGDA
COMMON/COMBLK/DLAI(366), SOLRAD(366), RAIN(366), WATSCO, EOS, EO
COMMON/COMBLK/F, DRIWT, DWG, DWH, DWC
COMMON/COMBLK/SGDD, PMGDD, IAVAIL, IFIRST, ILAST, NDPOOL(20), MATURE(20)
REAL LAT
CALL LEAF (1)
CALL DAYPFO (1)
CALL EVAP (1)
CALL SOLWAT (1)
CALL STAGE (1,N)
CALL PHOTO (1)
CALL RPHOTO(1,TOTWT,TOFOTO)
IF(TOFOTO.EQ.0.) WRITE(6,1003) TEMP0, WATSCO, DAYPFO
1003 FORMAT(1X,'TEMP0=','F4.2',5X,'WATSC0=','F4.2',5X,'DAYPFO=','F5.1')
DRIWT=TOFOTO*(PAREA/100.)*(12./44.)*(1./.4)*.001
CALL GFW (1)
TOTWT=WL(NODE)+WC(NODE)+WG(NODE)
RETURN
END
SUBROUTINE INITLZ
COMMON/NODBLK/NODE, IDAY(20), PL(20), YDLA(20), JDAY(20), ICMP(20), IP
1RINT(20),SUMES1(20),SUMES2(20),T(20),PDAY(20),PERCNT(21),XDAYS
2(20,21),GRO(20,2,20),XMAX(20,20),SPROUT(20),SW(20),UL(20),PLL(20)
3,RCOUNT(20,20),ACDAYS(20,20),IDAY3(20),IDAY6(20),IDAY9(20)
4,ISTAGE(20),DLA(20),WR(21),WL(21),WC(21),WH(21),WG(21)
COMMON/SPECIAL/ISPR(20)
COMMON/COMBLK/ROSPZ,PAREA,N,
1TEMPCO, DAYPFO, LAT, WYE, BO, R2
COMMON/COMBLK/TEMPMX(366), TEMPMLN(366), TEMP(366), FMRGDA
COMMON/COMBLK/DLAI(366), SOLRAD(366), RAIN(366), WATSCO, EOS, EO
COMMON/COMBLK/F, DRIWT, DWG, DWH, DWC
COMMON/COMBLK/SGDD, PMGDD, IAVAIL, IFIRST, ILAST, NDPOOL(20), MATURE(20)
DO 10 NODE=1,20

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```

DO 5 J=1,20
RCOUNT(NODE,J)=0.
PDAYS(NODE,J)=0.
ISPR(J)=0.
XMAX(NODE,J)=0.
ACDAYS(NODE,J)=0.
XDAYS(NODE,J)=0.
5 CONTINUE
      MATURE(NODE)=0
      IStage(NODE)=0
      WL(NODE)=0.
      WC(NODE)=0.
      WH(NODE)=J.
      WG(NODE)=0.
      WR(NODE)=0.
      IDAY(NODE)=0
      IDAY3(NODE)=0
      IDAY6(NODE)=0
      IDAY9(NODE)=0
      DO 6 ITEMpx=1,20
      DO 7 I=1,2
      7 GRO(NODE,I,ITEMpx)=0.
      6 CONTINUE
      ICCMP(NODE)=0
      JDAY(NODE)=0
      PL(NODE)=0.
      YDLA(NODE)=0.
      NDPOOL(NODE)=NODE + 1
      DLL(NODE)=0.
      UL(NODE)=0.
      SPFOUT(NODE)=0.
      DLAINODE)=0.
      SW(NODE)=0.
      SUMES1(NODE)=0.
      SUMES2(NODE)=0.
      10 CONTINUE
      NDPOOL(20)=99
      IFIRST=0

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IAVAIL=1
SGDD=0
PMGDD=0
IFREQ=5.
NODE=0
DO 15 I=1,366
  DLA(I)=0.
15 CONTINUE
FMRGDA=0
RETURN
END
SUBROUTINE EMRGNC (ICDAY)
COMMON/NODBLK/NODE, IDAY(20), PL(20), YDLA(20), JDAY(20), ICMP(20), IP
1RINT(20), SUMES1(20), SUMES2(20), T(20), PDAYS(20,20), PERCNT(21), XDAYS
2(20,21), GRO(20,2,20), XMAX(20,20), SPROUT(20), SW(20), UL(20), PLL(20)
3,RCOUNT(20,20),ACDAYS(20,20),IDAY3(20),IDAY6(20),IDAY9(20)
4,I STAGE(20),DLA(20),WR(21),WL(21),WH(21),WG(21)
COMMON/COMBLK/FOSPZ, PAREA, N,
1TEMPCO, DAYPFN, LAT, MYE, BO, R2
COMMON/COMBLK/TEMPMX(366), TEMPNN(366), TEMP(366), FMRGDA
COMMON/CCMBLK/DLAI(366), SOLRAD(366), RAIN(366), WATSCO, EOS, EO
COMMON/COMBLK/F, DRINT, DWG, DWH, DWC
COMMON/CNMBLK/SGDD, PMGDD, IAVAIL, IFIRST, ILAST, NDPOOL(20), MATURE(20)
SMRGDA=0.
DO 2999 I=ICDAY, 366
AVSLTP=TEMP(1)
IF (AVSLTP*GT.21.4) AVSLTP=21.4
FMRGDA=1./(-1.05*AVSLTP+26.6)
SMRGDA=SMRGDA+EMRGDA
IF (SMRGDA-1.)2999,2997,2996
2999 CONTINUE
2996 FMRGDA=SMRGDA-1.
SPROUT(NODE)=I-FMRGDA
GO TO 2994
2997 SPCUT(NODE)=SMRGDA+ICDAY
2994 RETURN
END
SUBROUTINE RPHOTO (I, TOTWT, TOFOTO)
COMMON/COMBLK/ICDAY, CARO3730, CARO3740, CARO3750, CARO3750, CARO3770, CARO3780, CARO3790, CARO3800
COMMON/CCMBLK/ICDAY, CARO3810, CARO3820, CARO3830, CARO3840, CARO3850

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COMMON/NODBLK/NODE, IDAY(20), PL(20), YDLA(20), JDAY(20), ICOMP(20), IP
1RINT(20), SUMES1(20), SUMES2(20), T(20), PDAY(S(20,20), PERCENT(21), XDAYS
2(20,21), GRO(20,2,20), XMAX(20,20), SPROUT(20), SW(20), UL(20), PLL(20)
3,RCOUNT(20,20),ACDAY(S(20,20),IDAY3(20),IDAY6(20),IDAY9(20)
4,ISTAGE(20),DLA(20),WR(21),WL(21),WC(21),WH(21),WG(21)
COMMON/COMBLK/ROSPZ,PAREA,N,
1TEMPCO,DAYPFO,LAT,WYE,B0,R2
COMMON/COMBLK/TEMPMX(366),TEMPMN(366),TEMP(366),FMRGDA
COMMON/COMBLK/DLAI(366),SOLRAD(366),RAIN(366),WATSCO,EOSS,EO
COMMON/COMBLK/F,DRIFT,DWG,DWH,DWC
COMMON/COMBLK/SGDD,PMGDD,IAVAIL,IFIRST,ILAST,NDPOOL(20),MATURE(20)

CC
CC THIS ROUTINE REDUCES POTENTIAL PHOTOSYNTHESIS TO
CC ACTUAL PHOTOSYNTHESIS. THE DIFFERENCE IS DUE TO
CC THE LIMITING TEMP. AND WATER. THIS ROUTINE ALSO
CC SUBTRACTS THE RESPIRATION LOSS.
CC
IF (TEMP(I).LT.5.0.OR.TEMP(I).GE.45.0) TEMPCO=0.
IF (TEMP(I).GE.25.0.AND.TEMP(I).LE.40.0) TEMPCO=1.
IF (TEMP(I).GE.5.0.AND.TEMP(I).LE.25.) TEMPCO=.05*TEMP(I)-.25
IF (TEMP(I).GT.40.0.AND.TEMP(I).LT.45.) TEMPCO=-.2*TEMP(I)+.9.
TOFOTO=TEMPCO*WATSCO*DAY PFO
TEMPN=(TEMPMN(I)+TEMP(I))/2.
RESPG=.14*(.65+.011*TEMPN)
RESPM=.0054*(.044+.0019*TEMPN+.001*TEMPN*TEMPN)
RESPN=RESPG+TOFOTO+RESPM*(TOTWT+WR(NODE))*1.43
TOFACTO=TOFOTO-RESPN
RETURN
END
SUBROUTINE LEAFAP (J,I,IMAX)
COMMON/NODBLK/NODE, IDAY(20), PL(20), YDLA(20), JDAY(20), ICOMP(20), IP
1RINT(20), SUMES1(20), SUMES2(20), T(20), PDAY(S(20,20), PERCENT(21), XDAYS
2(20,21), GRO(20,2,20), XMAX(20,20), SPROUT(20), SW(20), UL(20), PLL(20)
3,RCOUNT(20,20),ACDAY(S(20,20),IDAY3(20),IDAY6(20),IDAY9(20)
4,ISTAGE(20),DLA(20),WR(21),WL(21),WC(21),WH(21),WG(21)
COMMON/COMBLK/ROSPZ,PAREA,N,
1TEMPCO,DAYPFO,LAT,WYE,B0,R2
COMMON/COMBLK/TEMPMX(366),TEMPMN(366),TEMP(366),FMRGDA

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COMMON/COMBLK/DLAI(366),SOLRAD(366),RAIN(366),WATSCO,EOS,EO
COMMON/CCMBLK/F,DRWT,DWG,DWH,DWC
COMMON/CMBLK/SGDD,PMGDD,IAVAIL,IFIRST,ILAST,NDPOOL(20),MATURE(20)
DIMENSION SXDIN(20)
XDAYSI(NODE,1)=0.0
XDAYSI(NODE,2)=FMRGDA
1104 DO 102 J=1,N
      IF(J.NE.1) GO TO 1085
      RCOUNT(NODE,J)=SPROUT(NODE)
      GO TO 1084
1085 SXDIN(J)=0.0
      PDAYS(NODE,J-1)=XDAYSI(NODE,J)
      IF(XDAYSI(NODE,2).GT.0.0) DAYS=SPROUT(NODE)
      IF(XDAYSI(NODE,J).GT.0.) GO TO 13
103 I=I+1
      DAYS=1
      IF(DAYS.GT.1MAX) GO TO 104
13 AVTEMP=TEMP(I)
      IF(J.LT.6) GO TO 101
      IF(AVTEMP.LT.21.) GO TO 1C8
      IF(TEMP(I).GT.30.) AVTEMP=30.
      DIN=2.957-.0562*(AVTEMP-21)
      GO TO 18
      DIN=2.9+.0567*(AVTEMP-22.)*2
      GO TO 18
101 IF(AVTEMP.GT.22) AVTEMP=22.
      DIN=2.8+.0292*((AVTEMP-22.)*2)
18 IF(XDAYSI(NODE,J).EQ.0.) GO TO 107
      XDIN=(1./DIN)*XDAYSI(NODE,J)
      XDAYSI(NODE,J)=0.0
      GO TO 14
107 XDIN=1./DIN
14 SXDIN(J)=XDIN+SXDIN(J)
      IF(1.0-SXDIN(J)) 106,105,103
      IF(1.0-SXDIN(J)) 106,105,103
105 RCOUNT(NODE,J)=DAYS
      XDAYSI(NODE,J)=0.0
      GO TO 1108
106 XDAYSI(NODE,J)= ( SXDIN(J)-1.0)*DIN
      CAR00570
      CAR00580
      CAR00590
      CAR00600
      CAR00610
      CAR00620
      CAR00630
      CAR00640
      CAR00650
      CAR00660
      CAR00670
      CAR00680
      CAR00690
      CAR00710
      CAR00720
      CAR00730
      CAR00740
      CAR00750
      CAR00760
      CAR00770
      CAR00820
      CAR00830
      CAR00840
      CAR00850
      CAR00860
      CAR00870
      CAR00880
      CAR00890

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RCOUNT(NODE,J)= DAYS-XDAYS(NODE,J)          CAR00900
1108 XDAYS(NODE,J+1)=XDAYS(NODE,J)          CAR00910
      IF (J.EQ.N) PDAY(S(NODE,J)=XDAYS(NODE,J)  CAR00920
1084 WRITE(6,19) J,RCOUNT(NODE,J)             CAR00930
19 FORMAT(5X, 'DAY LEAF', I3, ' APPEARS = ',F7.2)
102 CONTINUE
104 RETURN
END

SUBROUTINE LEAF (I)
COMMON/NODBLK/NODE, IDAY(20), PL(20), YDLA(20), ICOMP(20), IP
1RINT(20), SUMES1(20), SUMES2(20), T(20), PDAYS(20,20), PERCNT(21), XDAYS
2(20,21), GRO(20,2,20), XMAX(20,20), SPROUT(20), SW(20), UL(20), PLL(20)
3,RCOUNT(20,20),ACDAYS(20,20),IDAY3(20),IDAY6(20),IDAY9(20)
4,IStage(20),DLA(20),WR(21),WL(21),WC(21),WH(21),WG(21)
COMMON/CMBLKB/ROSPZ,PAREA,N,
ITEMPCO,DAYPFO,LAT,WYE,BO,R2
COMMON/COMBLK/TEMPMX(366),TEMPMN(366),TEMP(366),FMRGDA
COMMON/COMBLK/CLAI(366),SOLRAD(366),RAIN(366),WATSCO,EOS,EO
COMMON/CMBLKB/F,DRIVT,DWG,DWH,DWC
COMMON/COMBLK/SGDD,PMGDD,IAVAIL,IFIRST,ILAST,NDPOOL(20),MATURE(20)
DIMENSION SLA(20)                                CAR01570
DO 108 J=1,N                                     CAR01590
IF(TEMP(I).GT.12.) GO TO 101                   CAR01600
GFO(NODE,2,J)=GRO(NODE,1,J)                   CAR01610
GO TO 108                                         CAR01620
101 CONTINUE                                       CAR01630
  DAYS=I                                           CAR01640
  IF(RCOUNT(NODE,J)-DAYSS)110,111,109         CAR01650
110 CONTINUE                                       CAR01660
    IF(GRO(NODE,1,J).GT.0.) GO TO 111         CAR01670
    GRO(NODE,2,J)=(5.1*(TEMP(I)-12.)*PDAYS(NODE,J))
    GO TO 131
111 CONTINUE
    IF(ACDAYS(NODE,J).GT.0.) GRO(NODE,2,J)=GRO(NODE,1,J)
    IF(ACDAYS(NODE,N).GT.0.) GRO(NODE,2,J)=GRO(NODE,2,J)*.996
    IF(ACDAYS(NODE,J).GT.0.) GO TO 108
112 GFO(NODE,2,J)=5.1*(TEMP(I)-12.)

```

```

CAR01750
CAR01760
CAR01770
CAR01780
CAR01790
CAR01800
CAR01810
CAR01820
CAR01830
CAR01840
CAR01850
CAR01860
CAR01870
CAR01880
CAR01890
CAR01900
CAR01910
CAR01920
CAR01930
CAR01940
CAR01950
CAR01960
CAR01970
CAR01980
CAR01990
CAR02000
CAR02010
CAR02020
CAR02030
CAR02040
CAR02050
CAR02060
CAR02070
CAR02080
CAR02090

1 IF(GRO(NODE,1,J).GT.0.) GO TO 121
  GO TO 131
121 GRO(NODE,2,J)=(GRO(NODE,2,J)+GRO(NODE,1,J))
131 IF(GRO(NODE,2,J)-XMAX(NODE,J) 108,208,1280
1280 IF(ACDAYS(NODE,J).GT.0.) GO TO 108
  IF(DAYS-RCOUNT(NODE,J).GT.1.0)GO TO 1281
    FGR0=XMAX(NODE,J)/GRO(NODE,2,J)
    ACDAYS(NODE,J)=FGR0+RCOUNT(NODE,J)
    GO TO 209
  XXMAX=GRO(NODE,2,J)-XMAX(NCDE,J)
  DGRO=GRO(NODE,2,J)-GRO(NODE,1,J)
  FGR0=(1./DGRO)*XXMAX
  ACDAYS(NODE,J)=DAYS-FGR0
  GO TO 209
208 ACDAYS(NODE,J)=DAYS
209 WRITE(6,210)J,ACDAYS(NODE,J),XMAX(NODE,J),NODE
210 FORMAT(' LEAF NO.=',1X,12,5X,'DAY MAX LA ATTAINED=' ,F6.2,5X,
1'MAX LA=',F6.2,3X,12)
  GRO(NODE,2,J)=XMAX(NODE,J)
  IF(J.LE.11) GO TO 104
  GRO(NCDE,2,J-11)=0.0
  IF(J=5) 108,107,106
107 IDAY3(NODE)=(ACDAYS(NODE,5)+RCOUNT(NODE,N))/2.
106 IF(J=N) 108,105,108
105 IDAY6(NODE)=ACDAYS(NODE,N)+(RCOUNT(NODE,N)-IDAY3(NODE))*86)
  IDAY9(NODE)=(IDAY6(NODE)-RCOUNT(NODE,1))*1.6+RCOUNT(NODE,1)
108 CONTINUE
109 CONTINUE
  DO 1112 J=1,N
1112 IF(J.GT.1) GO TO 1100
  SLA(J)=GRO(NODE,2,J)
  GO TO 1112
1100 SLA(J)=SLA(J-1)+GRO(NODE,2,J)
1112 CONTINUE
1500 DLA(NODE)=SLA(N)
  DLA(I)=DLA(NODE)/PAREA
  DO 54 J=1,20
    GRO(NCDE,1,J)=GRO(NODE,2,J)

```

```

54 GRO(NODE,2,J)=0.
      RETURN
      END
      SUBROUTINE EVAP ( I )
COMMON/NODBLK/NODE, IDAY(20),PL(20),YDLA(20),JDAY(20),ICOMP(20),IP
1RINT(20),SUMES1(20),SUMES2(20),T(20),PDAYS(20,20),PERCNT(21),XDAYS
2(20,21),GRO(20,2,20),XMAX(20,20),SPROUT(20),SW(20),UL(20),PLL(20)
3,RCOUNT(20,20),ACDAYS(20,20),IDAY3(20),IDAY6(20),IDAY9(20)
4,ISTAGE(20),DLA(20),WR(21),WL(21),WH(21),WG(21),
COMMON/COMBLK/ROSPZ,PAREA,N,
1TEMPCO,DAYPFO,LAT,WYE,B0,R2
COMMON/COMBLK/TEMPMX(366),TEMPMN(366),TEMP(366),FMRGDA
COMMON/COMBLK/CLAI(366),SOLRAD(366),RAIN(366),WATSCO,EOS,EO
COMMON/COMBLK/F,DRINT,DWG,DWH,DWC
COMMON/COMBLK/SGDD,PMGDD,IAVAIL,IFIRST,ILAST,NDPOOL(20),MATURE(20)
DATA GAMMA/.68/
TK=TEMP(I)+273.
DELTA = (EXP(21.255-.5304./TK))/(TK**2)
D=DELTA/GAMMA
ALBEDO=.3367-.1867*EXP(-.6*DLAI(I))
PO=520+193*SIN(.0172*(I-80))
IF(SOLRAD(I).GT.R0) SOLRAD(I)=R0
R4=1.-.261*EXP(-7.77E-04*TEMP(I)**2)
R6=(R4-.96)*1.17E-07*TK**4*(.2+.8*(SOLRAD(I)/R0))
H=(1.-ALBEDO)*SOLRAD(I)+R6
HO = H/583.
EO=1.28*DELTA/(DELTAGAMMA)*HO
IF(DLAI(I).LT.0.5) EOS = EO
IF(DLAI(I).LT.0.5) GO TO 41
HOS = HO * EXP(-0.398*DLAI(I))
EOS = (D*HOS)/(D+1.)
41 RETURN
      END
      SUBROUTINE SOLWAT ( I )
COMMON/NODBLK/NODE, IDAY(20),PL(20),YDLA(20),JDAY(20),ICOMP(20),IP
1RINT(20),SUMES1(20),SUMES2(20),T(20),PDAYS(20,20),PERCNT(21),XDAYS
2(20,21),GRO(20,2,20),XMAX(20,20),SPROUT(20),SW(20),UL(20),PLL(20)
3,RCOUNT(20,20),ACDAYS(20,20),IDAY3(20),IDAY6(20),IDAY9(20)

```

```

4,I STAGE(20),DLA(20),WR(21),WL(21),WC(21),WH(21),WG(21)
COMMON/COMBLK/ROSPZ,PAREA,N,
1ITEMPCO,DAYPFO,LAT,WYE,BO,R2
COMMON/COMBLK/TEMPMX(366),TEMPMN(366),TEMP(366),FMRGDA
COMMON/COMBLK/DLA(366),SOLRAD(366),RAIN(366),WATSCO,EOS,EO
COMMON/COMBLK/F,DRIWT,DWG,DWH,DWC
COMMON/COMBLK/SGDD,PMGDD,IAVAIL,IFIRST,ILAST,NDPOOL(20),MATURE(20)
DATA U,CONA/.6,.35/
PRECIP=RAIN(I)
WATSCO=1.
1 IF(SUMES1(NODE) - U) 1,2,2
1 IF(PRECIP - SUMES1(NODE)) 3, 4,4
3 SUMES1(NODE) = SUMES1(NODE)-PRECIP
GO TO 5
4 SUMES1(NODE) = 0.
5 SUMES1(NODE) = SUMES1(NODE) + EOS
IF(SUMES1(NODE) - U) 6,6,7
6 ES = EOS
GO TO 24
7 ES = EOS - 0.4*(SUMES1(NODE) - U)
SUMES2(NODE) = 0.6*(SUMES1(NODE) - U)
T(NODE) = (SUMES2(NODE)/CCNA)**2
GO TO 24
2 IF(PRECIP - SUMES2(NODE)) 9,8,8
8 PRECIP=PRECIP-SUMES2(NODE)
SUMES1(NODE) = U - PRECIP
T(NODE) = 0.
IF(PRECIP-U) 5,5,4
T(NODE)=T(NODE)+1.
9 ES = CCNA*T(NODE)**0.5 - SUMES2(NODE)
IF(PRECIP .GT. 0.) GO TO 10
IF(ES .GT. EOS) ES = EOS
GO TO 11
10 ESX=0.8*PRECIP
IF(ESX .LE.ES) ESX = ES+PRECIP
IF(ESX .GT. EOS) ESX = EOS
ES = ESX
11 SUMES2(NODE) = SUMES2(NODE) + ES - PRECIP

```

```

T(NODE) = (SUMES2(NODE)/CONA) **2
24 IF(ES .LT. 0.) ES = 0.
    IF(DLA1(I) .GT. 3.0) GO TO 26
    EP=.53*DLAI(I)**.5*EO
    IF (EP .LT. 0.) EP = 0.
    GO TO 27
26 EP = EC - ES
27 IF(EP .LT. 0.) EP = 0.
25 ET=ES+EP
    IF(EO-ET) 39,41,41
39 ET=EO
    EP = ET - ES
41 CONTINUE
    IF(SW(NODE)*GT.*UL(NODE)) SW(NODE)=UL(NODE)
    ALLEO=PLL(NODE)
    IF(DLA1(I) - 1.0) 21,21,28
28 IF(DLA1(I)*LT.DLA1(I-1)) GO TO 23
    IF(DLA1(I)-2.7) 22,22,23
21 ALLEO=.8*UL(NODE)-.1*UL(NODE)*DLAI(I)
    GO TO 23
22 ALLEO=.59*PLL(NODE)*DLAI(I)-.44*UL(NODE)*DLAI(I)+1.*19*
    1 UL(NODE)-.59*PLL(NODE)
    23 IF(ALLEO-SW(NODE)) 30,30,29
29 WATSC0=SW(NODE)/ALLEO
    EP=EP*WATSC0
30 ET=ES+EP
    SW(NODE)=SW(NODE)-ET+RAIN(I)
    IF(SW(NODE)*LT.0.0) SW(NODE)=0.0
    IF(SW(NODE)*GT.*UL(NODE)) SW(NODE)=UL(NODE)
14 CONTINUE
    RETURN
END
SUBROUTINE STAGE (I,N)
COMMON/NODBLK/NODE,IDAY(20),PL(20),YDLAI(20),JDAY(20),ICOMP(20),IP
1RINT(20),SUMES1(20),SUMES2(20),T(20),PDAYS(20,20),PERCNT(21)*XDAYS
2(20,21),GRO(20,2,20),XMAX(20,20),SPROUT(20),SW(20),UL(20),PLL(20),
3,RCOUNT(20,20),ACDAYS(20,20),IDAY3(20),IDAY6(20),IDAY9(20),
4,ISTAGE(20),DLA(20),WR(21),WL(21),WC(21),WH(21),WG(21)

```

```

IF(ISTAGE(NODE).EQ.5) GO TO 199
IF(ACDAYS(NODE,5).EQ.0.) GO TO 100
IF(I.GT.IDAY3(NODE)) GO TO 101
100 ISTAGE(NODE)=1
      GO TO 199
101 IF(ACDAYS(NODE,N).GT.0.) GO TO 102
      ISTAGE(NODE)=2
      GO TO 199
102 IF(ACDAYS(NODE,N).NE.0.0.AND.I.GE.IDAY6(NODE)) GO TO 103
      ISTAGE(NODE)=3
      GO TO 199
103 ISTAGE(NODE)=4
      IF(I.EQ.IDAY9(NODE)) ISTAGE(NODE)=5
199 CONTINUE
      RETURN
END
SUBROUTINE GROW (I)
COMMON/NODBLK/NODE, IDAY(20),PL(20),YDLA(20),JDAY(20),ICOMP(20),IP
1RINT(20),SUMES1(20),SUMES2(20),T(20),PDAYS(20,20),PERCNT(21),XDAY$2(20,21),GRO(20,2,20),XMAX(20,20),SPROUT(20),SW(20),UL(20)
3,RCOUNT(20,20),ACDAYS(20,20),IDAY3(20),IDAY6(20),IDAY9(20)
4,ISTAGE(20),DLA(20),WR(21),WL(21),WH(21),WG(21)
COMMON/COMBLK/ROSPZ,PAREA,N,
1TEMPCO,DAYPFO,LAT,WYE,BO,R2
COMMON/COMBLK/TEMPMX(366),TEMPMN(366),TEMP(366),FMRGDA
COMMON/COMBLK/DLA(366),SOLRAD(366),RAIN(366),WATSCD,EOS,E0
COMMON/COMBLK/F,DRIWT,DWG,DWH,DWC
COMMON/COMBLK/SGDD,PMGDD,IAVAIL,IFIRST,ILAST,NDPOOL(20),MATURE(20)
IF(I-RCOUNT(NODE,1).LT.1.)PL(NODE)=1.
IF(I-RCOUNT(NODE,1).LT.1.)YDLA(NODE)=0.
IF(DLA(NODE).LE.0.) GO TO 5
IF(DRIWT.LE.0.) GO TO 5
IF(DLA=DLA(NODE)-YDLA(NODE))
SLW=YDLA(NODE)/(WL(NODE)+.00001)
IF(WL(NODE).LT..1) SLW=200.
ITEMPX=ISTAGE(NODE)
GO TO (1,2,3,4,4), ITEMXP
1 IF(SLW.GT.200.) SLW=200.

```

```

IF(SLW.LT.160.) SLW=160.
PDWL=DDLA/SLW
IF(DDLA.EQ.0.) GO TO 100
REQ=PDWL*1.25
F=DRIWT/REQ
IF(F.GT.1.25) F=1.25
PDWL=PDWL*F
100 DWL=PDWL
DWR=DRIWT-DWL
GO TO 600
2 IF(I.EQ.IDAY3(NODE)) IDAY(NODE)=0
IDAY(NODE)=IDAY(NODE)+1
IF(SLW.GT.160.) SLW=160.
IF(SLW.LT.140.) SLW=140.
204 PDWL=DDLA/SLW
IF(IDAY(NODE).LE.10) GO TO 200
REQ=PDWL*1.5
F=DRIWT/REQ
IF(F.GT.2.) F=2.
PDWL=PDWL*F
DWL=PDWL
IF(ISTAGE(NODE).NE.3) GO TO 202
3 PL(NODE)=PL(NODE)-1
IF(PL(NODE).LT.0.) PL(NODE)=0.
DWL=WL(NODE)/(I-IDAY3(NODE))*PL(NODE)
202 REM=DRIWT-DWL
DWR=REM*.20
DWC=REM*.45
DWH=REM*.35
GO TO 602
200 REQ=PDWL*2.
F=DRIWT/REQ
IF(F.GT.2.) F=2.
PDWL=PDWL*F
205 DWL=PDWL
REM=DRIWT-DWL
IF(REM.GE.DRIWT*.20) GO TO 203
REM=REM*.4

```

```

GO TO 206
203 DWR=DRIWT*.20
206 DWC=DRIWT-DWL-DWR
GO TO 601
4 IF(I.EQ.IDAY6(NODE)) JDAY(NODE)=0
     JDAY(NODE)=JDAY(NODE)+1
     ICOMP(NODE)=1*(IDAY6(NODE)-RCOUNT(NODE,1))+.5
     IF(JDAY(NODE).GT.ICOMP(NODE)) GO TO 402
     DWL=DRIWT*.1
     DWR=WIC(NODE)*.005
     DWC=DRIWT-DWH-DWR
     DWL=0.
GO TO 602
402 RES=WIC(NODE)*.025
     IF(JDAY(NODE).LE.(IDAY9(NODE)-ACDAYS(NODE,N)+10)*.5) GO TO 400
     RES=-.5*RES
     DWR=0.
GO TO 401
400 DWR=WIC(NODE)*.005
401 DWG=DRIWT+RES-DWR
     DWC=-RES
     DWH=0.
DWL=0.
WG(NODE)=WG(NODE)+DWG
602 WH(NODE)=WH(NODE)+DWH
601 WC(NODE)=WC(NODE)+DWC
600 WL(NODE)=WL(NODE)+DWL
     WR(NODE)=WR(NODE)+DWR
     YDLA(NODE)=DLA(NODE)
5 CONTINUE
RETURN
END
SUBROUTINE PHOTO (I)
COMMON/NODBLK/NODE, IDAY(20), PL(20), YDLA(20), JDAY(20), ICOMP(20), IP
1RINT(20), SUMES1(20), SUMES2(20), T(20), PDAYS(20,20), PERCNT(21), XDAYS
2(20,21), GRO(20,2,20), XMAX(20,20), SPRQUT(20), SW(20), UL(20), PLL(20)
3,RCOUNT(20,20), ACDAYS(20,20), IDAY3(20), IDAY6(20), IDAY9(20)
4,1STAGE(20), DLA(20), WR(21), WL(21), WC(21), WH(21), WG(21)
CAR05410
CAR05420
CAR05430
CAR05440
CAR05450
CAR05460
CAR05470
CAR05480
CAR05490
CAR05500
CAR05510
CAR05520
CAR05530
CAR05540
CAR05550
CAR05560
CAR05570
CAR05580
CAR05590
CAR05600
CAR05610
CAR05620
CAR05630
CAR05640
CAR05650
CAR05660
CAR05670
CAR05680
CAR05690
CAR05700
CAR05710
CAR02120

```

```

COMMON/COMBLK/ROSPZ,PAREA,N,
1 TEMP00,DAYPF0,LAT,WYE,BO,R2
COMMON/COMBLK/TEMPMX(366),TEMPMN(366),TEMP(366),FMRGDA
COMMON/COMBLK/DLAI(366),SOLRAD(366),RAIN(366),WATSCO,EOS,E0
COMMON/COMBLK/F,DRIWT,DWG,DWH,DWC
COMMON/COMBLK/SGDD,PMGDD,IAVAIL,IFIRST,ILAST,NDPOOL(20),MATURE(20)
INTEGER HOURAN
REAL LAT,L,KAPPA,LL,LLPP,K,LITRAN,INTPAR,LLAC,LLIN
IHR=0
DAYPF0=0.
RH0=90.
DEC DAY=I+100
DECLIN=SIN((DEC DAY*360./365.)/180.*3.141593)*(-23.47)
SUNRIS=12.-ARCCOS(-TAN(LAT/180.*3.141593)*TAN(DECLIN/180.*3.141593))/
100 LST=IHR+IFIX(SUNRIS)+1
HOURAN=15*IABS(12-LST)
TERM=SIN(LAT/180.*3.141593)*SIN(DECLIN/180.*3.141593)
SINBET=COS(LAT/180.*3.141593)*COS(HOURAN/180.*3.141593)*
*COS(DECLIN/180.*3.141593)+TERM
BETA=ARSIN(SINBET)/3.141593*180.
TERM1=COS(LAT/180.*3.141593)*SIN(DECLIN/180.*3.141593)
TERM2=COS(DECLIN/180.*3.141593)*SIN(LAT/180.*3.141593)*
*COS(HOURAN/180.*3.141593)
COSGAM=1./COS(BETA/180.*3.141593)*(TERM1-TERM2)
COSTST=ABS(COSGAM)
IF(COSGAM.LT.-1.) GO TO 101
IF(COSTST.LE.1.) GO TO 102
COSGAM=1.
GO TO 102
101 COSGAM=-1.
102 GAMMA=ARCOS(COSGAM)/3.141593*180.
IF(LST.LE.12) GO TO 103
GAMMA=360.-GAMMA
103 PHI=GAMMA-RHO
THETA=BETA
IF(PHI.LE.-90.) PHI=PHI+180.
IF(PHI.LE.0..AND.PHI.GT.-90.) PHI=ABS(PHI)

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```

IF(PHI.LE.90..AND.PHI.GT.0.) PHI=PHI          CAR02510
IF(PHI.LE.180..AND.PHI.GT.90.) PHI=180.-PHI   CAR02520
IF(PHI.LE.270..AND.PHI.GT.180.) PHI=PHI-180.   CAR02530
IF(PHI.GT.270.) PHI=360.-PHI                  CAR02540
IF(DLA(NODE).LT.700.) GO TO 125             CAR02550
DLATMP=DLA(NODE)
DLATG10(DLATMP)*62.5-136.25
GO TO 126
125 DLATMP=DLA(NODE)
L=ALOG10(DLATMP)*23.-18.
IF(L.LE.0.) L=.5
126 SAC=0.
AS=0.
AR=0.
IF(THETA.EQ.0.) GO TO 116
IF(THETA.EQ.90.) GO TO 116
IF(PHI.EQ.0.) GO TO 111
IF(L.GE.R2) GO TO 111
X=L/TAN(THETA/180.*3.141593)*SIN(PHI/180.*3.141593)
Y=R2-L
IF(X.LE.Y) GO TO 110
X=(R2-L)/L
Y=TAN(PHI/180.*3.141593)
IF(X.GE.Y) GO TO 110
AS=((R2-L)**2)*TAN(THETA/180.*3.141593)/TAN(PHI/180.*3.141593)
GO TO 111
110 AS=L*L
111 CONTINUE
IF(PHI.EQ.90.) GO TO 113
IF(L.GE.R0SPZ) GO TO 113
X=L/TAN(THETA/180.*3.141593)*COS(PHI/180.*3.141593)
Y=R0SPZ-L
IF(X.LE.Y) GO TO 112
X=L/(R0SPZ-L)
Y=TAN(PHI/180.*3.141593)
IF(X.LE.Y) GO TO 112
AR=((R0SPZ-L)**2)*TAN(THETA/180.*3.141593)*TAN(PHI/180.*3.141593)
GO TO 113

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```

112 AR=L*L
113 CONTINUE
X=TAN(THETA/180.*3.141593)
IF(L.GE.R2) GO TO 114
YY=SQRT(((ROSPZ-L)**2)+((R2-L)**2))
Y=L/YY
IF(X.GE.Y) GO TO 116
IF(PHI.EQ.0.) GO TO 114
X=TAN(PHI/180.*3.141593)
Y=(R2-L)/(ROSPZ-L)
IF(X.GE.Y) GO TO 114
SAC=((R2-L)/TAN(PHI/180.*3.141593)-(ROSPZ-L))*(L/TAN(THETA/
*180.*3.141593)-YY)*TAN(THETA/180.*3.141593)
GO TO 116
114 IF(PHI.EQ.90.) GO TO 116
IF(L.GE.ROSPZ) GO TO 116
IF(L.LE.R2) GO TO 115
AR=L*TAN(THETA/180.*3.141593)*(ROSPZ-L)*COS(PHI/180.*3.141593)
X=ROSPZ-L
Y=(L/TAN(THETA/180.*3.141593))*COS(PHI/180.*3.141593)
IF(X.LE.Y) GO TO 116
AR=L*L
GO TO 116
115 DOWN=((RCSPZ-L)*TAN(PHI/180.*3.141593)-(R2-L))
IF(DOWN.GT.L)DOWN=L
SAC=DOWN*(L/TAN(THETA/180.*3.141593)-YY)*TAN(THETA/180.*3.141593)
116 IF(L.GE.ROSPZ) GO TO 127
DLATMP=DLA(NODE)
ETA=SIN(THETA/180.*3.141593)*(-16.67*ALOG10(DLATMP)+112.08)*.01
GO TO 128
127 DLATMP=DLA(NODE)
ETA=(-16.67*ALOG10(DLATMP)+112.08)*.01
128 KAPPA=.5*COS(THETA/180.*3.141593)
PA=((AS+AR-SAC)/(L**2))*KAPPA+ETA)*DLA(NODE)
117 LL=SQRT(PA)
IF(LL.LE.R2) GO TO 121
NP=2*IFIX(LL/2./R2)
NPR=2*IFIX(LL/2./ROSPZ)

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```

IF(NP.RT.0) GO TO 122
IF(LL.GT.ROSPZ) GO TO 119
IF(NP.EQ.0) GO TO 118
WBD=LL-R2*FLOAT(NP)
A=(NP+1)*(WBD*LL)*(1./FLOAT(NP+1))+NP*(R2-WBD)*LL/FLOAT(NP)
GO TO 123
118 A=LL*LL-LL*(LL-R2)
GO TO 123
119 IF(NP.EQ.0) GO TO 120
WBD=LL-R2*FLOAT(NP)
LLPP=2.*(LL-ROSPZ)
XNP=NP
TERM=XNP*(R2-WBD)*(LL-LLPP)/XNP+XNP*(R2-WBD)*LLPP/(1.+2.*XNP)
A=(XNP+1.)*(WBD*(LL-LLPP))/(XNP+1.)+(XNP+1.)*(WBD*LLPP) +
* (3.+2.*XNP)+TERM
GO TO 123
120 A=PA-((2.*(LL-R2))*(LL-2.*(LL-ROSPZ))+(LL-R2)*(LL-2.*(LL-ROSPZ))+
*(LL-R2)*(LL-ROSPZ))
GO TO 123
121 A=PA
GO TO 123
122 WBD=LL-R2*XNP
WBL=R2-WBD
XNPR=NPR
WBDR=LL-XNPR*ROSPZ
WBLR=ROSPZ-WBDR
TERM1=(XNP+1.)*(XNPR+1.)*WBDR*WBD/(XNP+XNPR+2.)+
*XNP*XNPR*WBLR*WBL/(XNP+XNPR)
A=XNPR*(XNP+1.)*WBLR*WBD/(XNP+XNPR+1.)*XNP*(XNPR+1.)*WBDR*WBL/
*(XNP+XNPR+1.)*TERM1
123 ARATIO=A/PA
K=.11+.68J*ARATIO
124 LITRAN=EXP(-K*DLAI(I))*100.
EFFLAI=A/PAREA
DAYLN=120.*((12.-SUNRIS)
SUNTIM=FLOAT(IFIX(SUNRIS)+1)-SUNRIS
TIME=60.*((SUNTIM+FLOAT(IHR))
SOLARH=1.5708*SOLRAD(I)/DAYLN*SIN(TIME*180./DAYLN/180.*3.141593)

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```
INTPAR=.121*SOLARH*(1.-LITRAN/109.)*60.  
POFO=31.35*INTPAR**.5-13.32  
IF(POFO.LT.1.) POFO=INTPAR*.8  
DAYPFO=DAYPFO+POFO  
IHR=IHR+1  
LIMIT=2*(11-IFIX(SUNRISE))  
IF(IHR.LE.LIMIT) GO TO 100  
RETURN  
END
```

## Field Model Sample Output

MANHATTAN JUNE 1 1966 DATA R5610

| PLANTING DATE=        | CALCULATED DAY= | CALENDAR DAY= | 6 | 1 | 1966 |
|-----------------------|-----------------|---------------|---|---|------|
| DAY LEAF 1 APPEARS =  | 155.07          |               |   |   |      |
| DAY LEAF 2 APPEARS =  | 157.08          |               |   |   |      |
| DAY LEAF 3 APPEARS =  | 160.56          |               |   |   |      |
| DAY LEAF 4 APPEARS =  | 163.77          |               |   |   |      |
| DAY LEAF 5 APPEARS =  | 166.71          |               |   |   |      |
| DAY LEAF 6 APPEARS =  | 170.10          |               |   |   |      |
| DAY LEAF 7 APPEARS =  | 172.86          |               |   |   |      |
| DAY LEAF 8 APPEARS =  | 175.47          |               |   |   |      |
| DAY LEAF 9 APPEARS =  | 178.07          |               |   |   |      |
| DAY LEAF 10 APPEARS = | 180.58          |               |   |   |      |
| DAY LEAF 11 APPEARS = | 183.15          |               |   |   |      |
| DAY LEAF 12 APPEARS = | 185.67          |               |   |   |      |
| DAY LEAF 13 APPEARS = | 188.22          |               |   |   |      |
| DAY LEAF 14 APPEARS = | 191.67          |               |   |   |      |
| DAY LEAF 15 APPEARS = | 193.12          |               |   |   |      |
| DAY LEAF 16 APPEARS = | 195.57          |               |   |   |      |
| DAY LEAF 1 APPEARS =  | 158.87          |               |   |   |      |
| DAY LEAF 2 APPEARS =  | 161.15          |               |   |   |      |
| DAY LEAF 3 APPEARS =  | 163.55          |               |   |   |      |
| DAY LEAF 4 APPEARS =  | 166.51          |               |   |   |      |
| DAY LEAF 5 APPEARS =  | 170.01          |               |   |   |      |
| DAY LEAF 6 APPEARS =  | 172.76          |               |   |   |      |
| DAY LEAF 7 APPEARS =  | 175.39          |               |   |   |      |
| DAY LEAF 8 APPEARS =  | 177.95          |               |   |   |      |
| DAY LEAF 9 APPEARS =  | 180.49          |               |   |   |      |
| DAY LEAF 10 APPEARS = | 183.06          |               |   |   |      |
| DAY LEAF 11 APPEARS = | 185.59          |               |   |   |      |
| DAY LEAF 12 APPEARS = | 188.14          |               |   |   |      |
| DAY LEAF 13 APPEARS = | 190.59          |               |   |   |      |
| DAY LEAF 14 APPEARS = | 193.04          |               |   |   |      |
| DAY LEAF 15 APPEARS = | 195.49          |               |   |   |      |
| DAY LEAF 16 APPEARS = | 198.04          |               |   |   |      |
| DAY LEAF 1 APPEARS =  | 153.87          |               |   |   |      |
| DAY LEAF 2 APPEARS =  | 155.67          |               |   |   |      |
| DAY LEAF 3 APPEARS =  | 158.50          |               |   |   |      |
| DAY LEAF 4 APPEARS =  | 161.77          |               |   |   |      |
| DAY LEAF 5 APPEARS =  | 164.73          |               |   |   |      |
| DAY LEAF 6 APPEARS =  | 168.06          |               |   |   |      |
| DAY LEAF 7 APPEARS =  | 171.00          |               |   |   |      |
| DAY LEAF 8 APPEARS =  | 173.78          |               |   |   |      |
| DAY LEAF 9 APPEARS =  | 176.33          |               |   |   |      |
| DAY LEAF 10 APPEARS = | 179.92          |               |   |   |      |
| DAY LEAF 11 APPEARS = | 181.45          |               |   |   |      |
| DAY LEAF 12 APPEARS = | 184.01          |               |   |   |      |
| DAY LEAF 13 APPEARS = | 185.51          |               |   |   |      |
| DAY LEAF 14 APPEARS = | 189.05          |               |   |   |      |
| DAY LEAF 15 APPEARS = | 191.50          |               |   |   |      |
| DAY LEAF 16 APPEARS = | 193.95          |               |   |   |      |

PLANTS PER HECTARE = 125000.  
 ROW SPACING = 76.20  
 PLANT SPACING = 10.5  
 AREA PER PLANT = 830.00

| JULIAN DAY    | STAGE                      | ROOT WT | LEAF WT | CULM WT | HEAD WT | GRAIN WT | TOTAL WT | LA/CW | LAI   | TCO   | WCO  | SW   |
|---------------|----------------------------|---------|---------|---------|---------|----------|----------|-------|-------|-------|------|------|
| LEAF N.D.= 1  | DAY MAX LA ATTAINED=154.12 | 0.000   | 0.000   | 0.000   | 0.000   | 3        | 1.000    | 0.001 | 1.0   | 1.0   | 15.2 | 3    |
| 155( 1)       | DAY MAX LA ATTAINED=0.001  | 0.000   | 0.001   | 0.000   | 0.000   | 3        | 0.000    | 0.003 | 3.000 | 0.004 | 1.0  | 1.0  |
| LEAF N.D.= 2  | DAY MAX LA ATTAINED=155.76 | 0.000   | 0.000   | 0.000   | 0.000   | 3        | 2.00     | 0.000 | 1.0   | 1.0   | 15.2 | 3    |
| 155( 2)       | DAY MAX LA ATTAINED=0.003  | 0.000   | 0.000   | 0.000   | 0.000   | 3        | 1.00     | 0.000 | 1.0   | 1.0   | 15.2 | 3    |
| LEAF N.C.= 1  | DAY MAX LA ATTAINED=156.16 | 0.000   | 0.000   | 0.000   | 0.000   | 1        | 1.00     | 0.001 | 1.0   | 0.8   | 1.0  | 15.2 |
| 157( 1)       | DAY MAX LA ATTAINED=0.001  | 0.000   | 0.001   | 0.000   | 0.000   | 1        | 1.00     | 0.000 | 1.0   | 0.8   | 1.0  | 15.2 |
| 157( 2)       | DAY MAX LA ATTAINED=0.003  | 0.000   | 0.000   | 0.000   | 0.000   | 3        | 2.00     | 0.003 | 3.000 | 0.004 | 1.0  | 1.0  |
| LEAF N.C.= 2  | DAY MAX LA ATTAINED=157.82 | 0.000   | 0.000   | 0.000   | 0.000   | 1        | 2.00     | 0.000 | 1.0   | 0.8   | 1.0  | 15.2 |
| 158( 2)       | DAY MAX LA ATTAINED=0.003  | 0.000   | 0.000   | 0.000   | 0.000   | 1        | 2.00     | 0.003 | 3.000 | 0.004 | 1.0  | 1.0  |
| 158( 3)       | DAY MAX LA ATTAINED=0.008  | 0.000   | 0.003   | 0.000   | 0.000   | 1        | 1.00     | 0.003 | 3.000 | 0.004 | 1.0  | 1.0  |
| LEAF N.C.= 3  | DAY MAX LA ATTAINED=159.68 | 0.000   | 0.001   | 0.000   | 0.000   | 3        | 4.00     | 0.000 | 0.003 | 0.004 | 1.0  | 1.0  |
| 159( 3)       | DAY MAX LA ATTAINED=0.009  | 0.000   | 0.004   | 0.000   | 0.000   | 3        | 4.00     | 0.000 | 0.003 | 0.004 | 1.0  | 1.0  |
| LEAF N.C.= 4  | DAY MAX LA ATTAINED=0.004  | 0.000   | 0.003   | 0.000   | 0.000   | 1        | 2.00     | 0.000 | 1.0   | 0.8   | 1.0  | 15.2 |
| 160( 4)       | DAY MAX LA ATTAINED=0.003  | 0.000   | 0.000   | 0.000   | 0.000   | 1        | 2.00     | 0.000 | 1.0   | 0.8   | 1.0  | 15.2 |
| LEAF N.C.= 5  | DAY MAX LA ATTAINED=159.34 | 0.000   | 0.000   | 0.000   | 0.000   | 2        | 1.00     | 0.000 | 3.000 | 0.004 | 1.0  | 1.0  |
| 161( 5)       | DAY MAX LA ATTAINED=0.001  | 0.000   | 0.001   | 0.000   | 0.000   | 1        | 1.00     | 0.001 | 1.0   | 0.6   | 1.0  | 15.1 |
| 161( 6)       | DAY MAX LA ATTAINED=0.004  | 0.000   | 0.000   | 0.000   | 0.000   | 1        | 1.00     | 0.004 | 1.0   | 0.6   | 1.0  | 15.1 |
| 161( 7)       | DAY MAX LA ATTAINED=0.005  | 0.000   | 0.007   | 0.000   | 0.000   | 1        | 1.00     | 0.007 | 1.0   | 0.6   | 1.0  | 15.1 |
| 161( 8)       | DAY MAX LA ATTAINED=0.001  | 0.000   | 0.001   | 0.000   | 0.000   | 1        | 1.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.1 |
| 161( 9)       | DAY MAX LA ATTAINED=0.022  | 0.000   | 0.034   | 0.000   | 0.000   | 1        | 1.00     | 0.031 | 1.0   | 0.6   | 1.0  | 15.1 |
| LEAF N.C.= 6  | DAY MAX LA ATTAINED=161.04 | 0.000   | 0.000   | 0.000   | 0.000   | 1        | 4.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.3 |
| 162( 6)       | DAY MAX LA ATTAINED=0.015  | 0.000   | 0.015   | 0.000   | 0.000   | 1        | 4.00     | 0.015 | 7.000 | 0.009 | 1.0  | 1.0  |
| LEAF N.C.= 7  | DAY MAX LA ATTAINED=161.18 | 0.000   | 0.000   | 0.000   | 0.000   | 2        | 2.00     | 0.000 | 3.000 | 0.004 | 1.0  | 1.0  |
| 162( 7)       | DAY MAX LA ATTAINED=0.024  | 0.000   | 0.036   | 0.000   | 0.000   | 1        | 4.00     | 0.004 | 7.000 | 0.009 | 1.0  | 1.0  |
| LEAF N.C.= 8  | DAY MAX LA ATTAINED=162.20 | 0.000   | 0.000   | 0.000   | 0.000   | 3        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 162( 8)       | DAY MAX LA ATTAINED=0.026  | 0.000   | 0.020   | 0.000   | 0.000   | 1        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 163( 8)       | DAY MAX LA ATTAINED=0.016  | 0.000   | 0.016   | 0.000   | 0.000   | 1        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 163( 9)       | DAY MAX LA ATTAINED=0.015  | 0.000   | 0.015   | 0.000   | 0.000   | 1        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| LEAF N.C.= 9  | DAY MAX LA ATTAINED=0.036  | 0.000   | 0.064   | 0.000   | 0.000   | 1        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 163( 10)      | DAY MAX LA ATTAINED=0.031  | 0.000   | 0.031   | 0.000   | 0.000   | 1        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| LEAF N.C.= 10 | DAY MAX LA ATTAINED=164.03 | 0.000   | 0.000   | 0.000   | 0.000   | 2        | 4.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 164( 8)       | DAY MAX LA ATTAINED=0.019  | 0.000   | 0.030   | 0.000   | 0.000   | 1        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 164( 9)       | DAY MAX LA ATTAINED=0.007  | 0.000   | 0.010   | 0.000   | 0.000   | 1        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 165( 9)       | DAY MAX LA ATTAINED=0.062  | 0.000   | 0.022   | 0.000   | 0.000   | 1        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| LEAF N.C.= 11 | DAY MAX LA ATTAINED=0.031  | 0.000   | 0.030   | 0.000   | 0.000   | 1        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 165( 10)      | DAY MAX LA ATTAINED=164.30 | 0.000   | 0.015   | 0.000   | 0.000   | 2        | 4.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| LEAF N.C.= 12 | DAY MAX LA ATTAINED=165.35 | 0.000   | 0.000   | 0.000   | 0.000   | 3        | 12.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 165( 11)      | DAY MAX LA ATTAINED=0.056  | 0.000   | 0.037   | 0.000   | 0.000   | 1        | 12.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 165( 12)      | DAY MAX LA ATTAINED=0.040  | 0.000   | 0.030   | 0.000   | 0.000   | 1        | 12.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 166( 12)      | DAY MAX LA ATTAINED=0.013  | 0.000   | 0.015   | 0.000   | 0.000   | 1        | 12.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 166( 13)      | DAY MAX LA ATTAINED=0.084  | 0.000   | 0.037   | 0.000   | 0.000   | 1        | 12.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 167( 11)      | DAY MAX LA ATTAINED=0.045  | 0.000   | 0.049   | 0.000   | 0.000   | 1        | 12.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 167( 12)      | DAY MAX LA ATTAINED=0.015  | 0.000   | 0.023   | 0.000   | 0.000   | 1        | 12.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 167( 13)      | DAY MAX LA ATTAINED=0.011  | 0.000   | 0.037   | 0.000   | 0.000   | 1        | 12.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 168( 12)      | DAY MAX LA ATTAINED=167.08 | 0.000   | 0.008   | 0.015   | 0.000   | 1        | 12.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| LEAF N.C.= 14 | DAY MAX LA ATTAINED=167.15 | 0.000   | 0.048   | 0.059   | 0.000   | 2        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 168( 13)      | DAY MAX LA ATTAINED=0.117  | 0.000   | 0.029   | 0.000   | 0.000   | 2        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 168( 14)      | DAY MAX LA ATTAINED=0.123  | 0.000   | 0.037   | 0.000   | 0.000   | 2        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 168( 15)      | DAY MAX LA ATTAINED=0.079  | 0.000   | 0.059   | 0.000   | 0.000   | 2        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 169( 10)      | DAY MAX LA ATTAINED=0.034  | 0.000   | 0.023   | 0.000   | 0.000   | 2        | 7.00     | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| LEAF N.C.= 16 | DAY MAX LA ATTAINED=168.91 | 0.000   | 0.048   | 0.059   | 0.000   | 3        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 169( 11)      | DAY MAX LA ATTAINED=0.159  | 0.000   | 0.160   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 169( 12)      | DAY MAX LA ATTAINED=0.121  | 0.000   | 0.159   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 169( 13)      | DAY MAX LA ATTAINED=0.055  | 0.000   | 0.229   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 169( 14)      | DAY MAX LA ATTAINED=0.155  | 0.000   | 0.160   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 169( 15)      | DAY MAX LA ATTAINED=0.299  | 0.000   | 0.160   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 170( 11)      | DAY MAX LA ATTAINED=0.111  | 0.000   | 0.160   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 170( 12)      | DAY MAX LA ATTAINED=0.134  | 0.000   | 0.160   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 170( 13)      | DAY MAX LA ATTAINED=0.154  | 0.000   | 0.160   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 170( 14)      | DAY MAX LA ATTAINED=0.159  | 0.000   | 0.160   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 170( 15)      | DAY MAX LA ATTAINED=0.159  | 0.000   | 0.160   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 171( 11)      | DAY MAX LA ATTAINED=0.155  | 0.000   | 0.160   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 171( 12)      | DAY MAX LA ATTAINED=0.155  | 0.000   | 0.160   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 171( 13)      | DAY MAX LA ATTAINED=0.155  | 0.000   | 0.160   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 171( 14)      | DAY MAX LA ATTAINED=0.155  | 0.000   | 0.160   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |
| 171( 15)      | DAY MAX LA ATTAINED=0.155  | 0.000   | 0.160   | 0.000   | 0.000   | 2        | 28.00    | 0.000 | 1.0   | 0.6   | 1.0  | 15.2 |

| LEAF | NO.= | DAY | MAX   | LA    | ATTAINED= | 170.53    | MAX    | LA=   | 28.00 | 1     |
|------|------|-----|-------|-------|-----------|-----------|--------|-------|-------|-------|
| LEAF | 15   | 1   | 0.201 | 0.234 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 15   | 1   | DAY   | MAX   | LA        | ATTAINED= | 170.18 | MAX   | LA=   | 12.00 |
| LEAF | 15   | 1   | 0.065 | 0.064 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 15   | 1   | 0.649 | 0.193 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 16   | 1   | 0.421 | 0.234 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 16   | 1   | 0.106 | 0.064 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 16   | 1   | 0.602 | 0.566 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 16   | 1   | 0.704 | 0.286 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 16   | 1   | 0.166 | 0.150 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 7    | 1   | DAY   | MAX   | LA        | ATTAINED= | 172.39 | MAX   | LA=   | 64.00 |
| LEAF | 7    | 1   | 1.540 | 0.795 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 7    | 1   | 1.020 | 0.718 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 7    | 1   | DAY   | MAX   | LA        | ATTAINED= | 173.21 | MAX   | LA=   | 23.00 |
| LEAF | 7    | 1   | 0.319 | 0.239 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 20   | 1   | 2.270 | 0.403 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 7    | 1   | DAY   | MAX   | LA        | ATTAINED= | 177.08 | MAX   | LA=   | 84.00 |
| LEAF | 7    | 1   | 1.730 | 0.763 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 7    | 1   | 0.553 | 0.239 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 7    | 1   | 2.791 | 1.330 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 7    | 1   | 2.363 | 1.037 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 7    | 1   | 0.658 | 0.577 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 8    | 1   | DAY   | MAX   | LA        | ATTINED=  | 175.54 | MAX   | LA=   | 14.00 |
| LEAF | 8    | 1   | 3.456 | 1.673 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 22   | 1   | 2.632 | 1.637 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 22   | 1   | 1.777 | 1.637 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 22   | 1   | DAY   | MAX   | LA        | ATTAINED= | 176.40 | MAX   | LA=   | 64.00 |
| LEAF | 22   | 1   | 2.533 | 1.511 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 8    | 1   | DAY   | MAX   | LA        | ATTINED=  | 177.29 | MAX   | LA=   | 14.00 |
| LEAF | 8    | 1   | 4.02  | 2.042 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 23   | 1   | 1.777 | 1.677 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 23   | 1   | 1.514 | 0.777 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 23   | 1   | 1.409 | 0.736 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 23   | 1   | 4.525 | 2.575 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 23   | 1   | 3.593 | 2.448 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 23   | 1   | 1.800 | 1.402 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 23   | 1   | 5.114 | 3.317 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 24   | 1   | 4.419 | 3.156 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 8    | 1   | DAY   | MAX   | LA        | ATTAINED= | 178.61 | MAX   | LA=   | 14.00 |
| LEAF | 8    | 1   | 1.870 | 2.582 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 9    | 2   | DAY   | MAX   | LA        | ATTINED=  | 179.12 | MAX   | LA=   | 22.00 |
| LEAF | 9    | 2   | 5.463 | 4.193 | 0.524     | 0.300     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 9    | 2   | DAY   | MAX   | LA        | ATTINED=  | 179.66 | MAX   | LA=   | 22.00 |
| LEAF | 25   | 1   | 1.911 | 5.411 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 25   | 1   | 5.411 | 3.824 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 25   | 1   | 1.811 | 1.831 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 25   | 1   | 3.564 | 2.145 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 25   | 1   | 5.833 | 5.116 | 1.079     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 25   | 1   | 5.762 | 4.666 | 0.517     | 0.200     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 25   | 1   | 4.354 | 2.763 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 26   | 2   | 6.217 | 6.074 | 1.054     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 26   | 2   | 6.123 | 5.593 | 1.060     | 0.300     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 26   | 2   | 5.255 | 3.614 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 26   | 2   | DAY   | MAX   | LA        | ATTINED=  | 174.48 | MAX   | LA=   | 29.00 |
| LEAF | 26   | 2   | 6.427 | 7.101 | 2.271     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 26   | 2   | 6.430 | 6.605 | 1.670     | 0.300     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 9    | 1   | DAY   | MAX   | LA        | ATTINED=  | 183.26 | MAX   | LA=   | 22.00 |
| LEAF | 9    | 1   | 6.226 | 4.183 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 10   | 2   | DAY   | MAX   | LA        | ATTINED=  | 184.22 | MAX   | LA=   | 25.00 |
| LEAF | 10   | 2   | 6.556 | 7.673 | 2.310     | 0.300     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 25   | 1   | 1.941 | 2.101 | 0.196     | 2.94      | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 25   | 1   | 7.065 | 6.156 | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 25   | 1   | 1.841 | 1.96  | 0.000     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 25   | 1   | 6.556 | 5.099 | 0.511     | 0.000     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 25   | 1   | 7.531 | 9.360 | 3.426     | 0.100     | 0.000  | 0.000 | 0.000 | 0.000 |
| LEAF | 25   | 1   | 7.407 | 8.709 | 2.996     | 0.100     | 0.000  | 0.000 | 0.000 | 0.000 |

|      |                            |                            |        |        |       |       |        |          |         |
|------|----------------------------|----------------------------|--------|--------|-------|-------|--------|----------|---------|
| LEAF | '0. = 27)                  | 2                          | 6.990  | 6.089  | 1.145 | 0.300 | 0.000  | 7.234    | 811.352 |
|      | DAY MAX LA ATTAINED=185.66 |                            |        |        |       |       |        |          |         |
|      | 2                          | 8.020                      | 10.584 | 4.360  | 0.000 | 0.000 | 16.944 | 1347.230 |         |
|      | 2                          | 7.899                      | 10.005 | 3.709  | 0.000 | 0.000 | 13.715 | 1272.910 |         |
| LEAF | N.C. = 10                  | DAY MAX LA ATTAINED=196.36 |        |        |       |       |        |          |         |
|      | 2                          | 7.414                      | 7.149  | 1.701  | 0.000 | 0.000 | 8.930  | 934.572  |         |
|      | 2                          | 6.533                      | 11.866 | 5.129  | 0.300 | 0.000 | 16.995 | 1482.342 |         |
| LEAF | '0. = 11                   | DAY MAX LA ATTAINED=187.19 |        |        |       |       |        |          |         |
|      | 2                          | 8.286                      | 11.204 | 4.497  | 0.300 | 0.000 | 15.701 | 1356.808 |         |
|      | 2                          | 7.454                      | 8.157  | 2.535  | 0.000 | 0.000 | 10.692 | 1005.122 |         |
|      | 2                          | 9.066                      | 13.197 | 5.928  | 0.300 | 0.000 | 19.125 | 1523.442 |         |
|      | 2                          | 8.688                      | 12.459 | 5.250  | 0.000 | 0.000 | 17.708 | 1523.554 |         |
|      | 2                          | 8.307                      | 9.210  | 3.215  | 0.000 | 0.000 | 12.504 | 1176.268 |         |
| LEAF | '0. = 12                   | DAY MAX LA ATTAINED=188.33 |        |        |       |       |        |          |         |
|      | 2                          | 9.555                      | 14.521 | 6.722  | 0.000 | 0.000 | 21.243 | 1772.079 |         |
|      | 2                          | 9.402                      | 13.744 | 6.021  | 0.000 | 0.000 | 19.765 | 1729.654 |         |
| LEAF | '0. = 11                   | DAY MAX LA ATTAINED=189.62 |        |        |       |       |        |          |         |
|      | 2                          | 8.774                      | 10.458 | 3.915  | 0.000 | 0.000 | 14.373 | 1345.896 |         |
|      | 2                          | 9.775                      | 16.317 | 7.127  | 0.314 | 0.000 | 23.758 | 1989.918 |         |
| LEAF | '0. = 12                   | DAY MAX LA ATTAINED=190.12 |        |        |       |       |        |          |         |
|      | 2                          | 9.945                      | 15.111 | 6.825  | 0.000 | 0.000 | 21.936 | 1878.924 |         |
|      | 2                          | 9.275                      | 11.710 | 4.667  | 0.200 | 0.000 | 16.577 | 1491.637 |         |
|      | 2                          | 9.685                      | 18.218 | 7.554  | 0.647 | 0.000 | 26.419 | 2196.185 |         |
|      | 2                          | 10.150                     | 16.749 | 7.251  | 0.323 | 0.000 | 24.523 | 2034.622 |         |
|      | 2                          | 9.792                      | 13.002 | 5.442  | 0.000 | 0.000 | 18.445 | 1697.904 |         |
| LEAF | N.C. = 13                  | DAY MAX LA ATTAINED=191.05 |        |        |       |       |        |          |         |
|      | 2                          | 10.155                     | 20.131 | 7.985  | 0.682 | 0.000 | 29.098 | 2354.344 |         |
| LEAF | '0. = 13                   | DAY MAX LA ATTAINED=192.33 |        |        |       |       |        |          |         |
|      | 2                          | 10.320                     | 18.956 | 7.480  | 0.657 | 0.000 | 27.194 | 2248.326 |         |
|      | 2                          | 10.320                     | 18.956 | 7.480  | 0.657 | 0.000 | 20.587 | 1825.208 |         |
| LEAF | '0. = 12                   | DAY MAX LA ATTAINED=192.12 |        |        |       |       |        |          |         |
|      | 2                          | 10.328                     | 14.342 | 6.245  | 0.000 | 0.000 | 20.587 | 1825.208 |         |
| LEAF | N.C. = 14                  | DAY MAX LA ATTAINED=192.82 |        |        |       |       |        |          |         |
|      | 2                          | 10.143                     | 22.303 | 8.405  | 1.309 | 0.000 | 31.718 | 2596.673 |         |
|      | 2                          | 10.518                     | 20.330 | 8.124  | 1.103 | 0.000 | 29.956 | 2484.368 |         |
|      | 2                          | 10.487                     | 15.739 | 7.084  | 0.000 | 0.000 | 22.823 | 2049.673 |         |
|      | 2                          | 10.535                     | 24.917 | 8.037  | 1.644 | 0.000 | 34.398 | 2163.407 |         |
| LEAF | '0. = 14                   | DAY MAX LA ATTAINED=174.37 |        |        |       |       |        |          |         |
|      | 2                          | 10.703                     | 22.679 | 8.540  | 1.326 | 0.000 | 32.545 | 2631.307 |         |
| LEAF | '0. = 13                   | DAY MAX LA ATTAINED=194.48 |        |        |       |       |        |          |         |
|      | 2                          | 11.074                     | 17.603 | 7.505  | 0.527 | 0.000 | 25.439 | 2210.498 |         |
|      | 2                          | 10.735                     | 25.768 | 9.286  | 1.994 | 0.000 | 37.048 | 2892.986 |         |
|      | 2                          | 10.802                     | 23.652 | 8.759  | 1.497 | 0.000 | 33.908 | 2768.567 |         |
|      | 2                          | 11.173                     | 16.548 | 7.728  | 0.500 | 0.000 | 26.827 | 2430.510 |         |
| LEAF | '0. = 16                   | DAY MAX LA ATTAINED=195.69 |        |        |       |       |        |          |         |
|      | 3                          | 11.033                     | 25.763 | 9.958  | 2.517 | 0.000 | 38.243 | 2961.059 |         |
|      | 2                          | 11.099                     | 24.649 | 9.432  | 2.720 | 0.000 | 36.102 | 2838.294 |         |
|      | 2                          | 11.334                     | 20.214 | 8.091  | 2.783 | 0.000 | 29.389 | 2580.110 |         |
|      | 3                          | 11.539                     | 25.763 | 11.096 | 3.422 | 0.000 | 40.266 | 2905.317 |         |
| LEAF | N.C. = 16                  | DAY MAX LA ATTAINED=197.77 |        |        |       |       |        |          |         |
|      | 2                          | 11.583                     | 21.631 | 8.651  | 1.119 | 0.000 | 31.501 | 2679.298 |         |
|      | 3                          | 12.087                     | 25.763 | 12.310 | 4.361 | 0.000 | 42.459 | 2973.375 |         |
|      | 3                          | 12.209                     | 24.649 | 11.929 | 3.962 | 0.000 | 40.540 | 2933.417 |         |
| LEAF | N.C. = 15                  | DAY MAX LA ATTAINED=193.80 |        |        |       |       |        |          |         |
|      | 2                          | 11.771                     | 23.504 | 9.013  | 1.547 | 0.000 | 34.123 | 2981.886 |         |
|      | 3                          | 12.653                     | 25.768 | 13.603 | 5.352 | 0.000 | 44.723 | 2961.480 |         |
|      | 3                          | 12.661                     | 24.649 | 12.947 | 4.754 | 0.000 | 42.349 | 2921.683 |         |

| LEAF NO.=                          | DAY | MAX LA ATTAINED=199.73 | MAX LA=180.00 |        |
|------------------------------------|-----|------------------------|---------------|--------|
|                                    |     |                        | 10.093        | 2.340  |
| 203( 41)                           | 3   | 12.224                 | 23.504        | 0.000  |
| 203( 46)                           | 3   | 13.107                 | 25.768        | 6.146  |
| 203( 45)                           | 3   | 13.158                 | 24.649        | 5.620  |
| 201( 42)                           | 3   | 12.726                 | 23.504        | 11.622 |
| 201( 47)                           | 3   | 13.568                 | 25.768        | 15.662 |
| 202( 46)                           | 3   | 13.398                 | 24.649        | 14.605 |
| 202( 43)                           | 3   | 12.948                 | 23.504        | 11.768 |
| 202( 48)                           | 3   | 13.768                 | 25.768        | 16.111 |
| 223( 47)                           | 3   | 13.767                 | 24.649        | 15.434 |
| 203( 44)                           | 3   | 13.252                 | 23.504        | 12.631 |
| 203( 45)                           | 3   | 14.673                 | 25.768        | 16.797 |
| 205( 51)                           | 3   | 14.773                 | 24.649        | 14.357 |
| 204( 45)                           | 3   | 14.808                 | 23.294        | 13.557 |
| 204( 50)                           | 3   | 14.411                 | 25.768        | 15.434 |
| 205( 49)                           | 3   | 14.622                 | 24.649        | 17.360 |
| 205( 46)                           | 3   | 14.354                 | 23.504        | 14.304 |
| 205( 50)                           | 3   | 14.773                 | 25.768        | 18.383 |
| 206( 47)                           | 3   | 15.069                 | 25.768        | 15.662 |
| 207( 51)                           | 3   | 15.303                 | 24.649        | 18.591 |
| 207( 46)                           | 3   | 15.259                 | 23.504        | 16.222 |
| 207( 52)                           | 3   | 15.325                 | 25.768        | 16.637 |
| 208( 52)                           | 3   | 15.565                 | 24.649        | 19.480 |
| 209( 45)                           | 3   | 15.609                 | 23.504        | 17.710 |
| ANTHELIX OCCURRED ON JULIA DAY 208 |     |                        |               |        |
| 209( 54)                           | 4   | 15.433                 | 25.768        | 20.498 |
| 209( 53)                           | 3   | 16.037                 | 24.649        | 20.446 |
| 205( 50)                           | 3   | 16.687                 | 23.504        | 16.784 |
| 210( 55)                           | 4   | 15.536                 | 25.768        | 22.529 |
| 211( 55)                           | 4   | 16.254                 | 24.649        | 21.1   |
| ANTHELIX OCCURRED ON JULIA DAY 211 |     |                        |               |        |
| 212( 54)                           | 4   | 16.140                 | 24.649        | 22.815 |
| 212( 51)                           | 3   | 16.619                 | 23.504        | 19.983 |
| 212( 56)                           | 4   | 15.648                 | 25.768        | 24.797 |
| 211( 55)                           | 4   | 16.254                 | 24.649        | 25.168 |
| ANTHELIX OCCURRED ON JULIA DAY 211 |     |                        |               |        |
| 211( 52)                           | 4   | 16.719                 | 23.504        | 22.393 |
| 211( 57)                           | 4   | 15.772                 | 25.768        | 27.167 |
| 212( 56)                           | 4   | 16.380                 | 24.649        | 27.630 |
| 212( 52)                           | 4   | 16.831                 | 23.504        | 24.872 |
| 212( 56)                           | 4   | 15.908                 | 25.768        | 29.795 |
| 212( 57)                           | 4   | 16.518                 | 24.649        | 29.145 |
| 213( 54)                           | 4   | 16.956                 | 23.504        | 26.488 |
| 213( 56)                           | 4   | 16.056                 | 25.768        | 28.865 |
| 214( 56)                           | 4   | 16.664                 | 24.649        | 31.481 |
| 214( 55)                           | 4   | 17.034                 | 23.504        | 28.071 |
| 214( 60)                           | 4   | 16.201                 | 25.768        | 28.143 |
| 215( 59)                           | 4   | 16.821                 | 24.649        | 26.154 |
| 215( 56)                           | 4   | 17.232                 | 23.504        | 30.994 |
| 215( 61)                           | 4   | 16.341                 | 25.768        | 29.748 |
| 216( 61)                           | 4   | 16.975                 | 24.649        | 27.440 |
| 216( 57)                           | 4   | 17.386                 | 23.504        | 29.027 |
| 216( 62)                           | 4   | 16.478                 | 25.768        | 26.154 |
| 217( 61)                           | 4   | 17.124                 | 24.649        | 29.179 |
| 217( 58)                           | 4   | 17.526                 | 23.504        | 29.268 |
| 216( 62)                           | 4   | 16.612                 | 25.768        | 26.085 |
| 214( 62)                           | 4   | 17.270                 | 24.649        | 28.499 |
| 214( 59)                           | 4   | 17.682                 | 23.504        | 29.546 |
| 215( 64)                           | 4   | 17.763                 | 25.768        | 25.433 |
| ANTHELIX OCCURRED ON JULIA DAY 215 |     |                        |               |        |
| 35.937                             | 1.0 | 2.340                  | 0.000         | 5.8    |
| 2947.089                           | 1.0 | 2.340                  | 0.000         | 3.9    |
| 3.684                              | 1.0 | 2.340                  | 0.000         | 4.3    |
| 2949.634                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.687                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2949.995                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.764                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2937.834                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.672                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.623                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2898.354                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.594                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2998.956                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.749                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.658                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2926.082                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.608                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2886.760                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.580                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.734                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.704                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2914.377                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.643                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.514                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2875.212                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.565                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.719                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.628                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.589                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2951.256                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.559                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2879.561                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.551                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2840.845                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.551                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2939.450                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.574                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2866.022                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.585                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2929.481                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.537                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.660                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 2927.692                           | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.571                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.523                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.630                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.645                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.556                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.495                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.616                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.528                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.481                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.601                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.514                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.516                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.516                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.467                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.587                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.500                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.453                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.514                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.573                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.486                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.544                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.458                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.439                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.412                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.558                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.530                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.444                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.398                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.613                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.620                              | 1.0 | 2.340                  | 0.000         | 5.4    |
| 3.714                              | 1.0 | 2.340                  | 0.000         | 5.4    |

|          |   |        |        |        |        |        |          |
|----------|---|--------|--------|--------|--------|--------|----------|
| 1        | 2 | 2.5    | 0.7    | 1.0    | 0.8    | 0.8    | 2.0      |
| 219( 60) | 4 | 17.425 | 23.649 | 27.738 | 11.947 | 12.712 | 77.046   |
| 219( 65) | 4 | 16.870 | 25.768 | 26.797 | 11.301 | 11.155 | 2707.435 |
| 220( 64) | 4 | 17.551 | 24.669 | 27.045 | 11.216 | 17.246 | 79.027   |
| 220( 61) | 4 | 17.364 | 23.524 | 27.127 | 11.947 | 14.174 | 77.814   |
| 220( 66) | 4 | 16.994 | 24.578 | 24.177 | 11.301 | 12.833 | 2696.604 |
| 220( 65) | 4 | 17.687 | 24.669 | 26.369 | 11.216 | 18.551 | 2790.204 |
| 221( 62) | 4 | 18.059 | 23.534 | 26.449 | 11.301 | 11.947 | 79.712   |
| 221( 61) | 4 | 17.115 | 25.168 | 23.573 | 11.216 | 17.797 | 2722.402 |
| 222( 66) | 4 | 17.818 | 24.679 | 25.709 | 11.947 | 16.330 | 3.403    |
| 222( 62) | 4 | 18.232 | 23.524 | 23.524 | 11.301 | 15.258 | 3.403    |
| 222( 69) | 4 | 17.222 | 25.768 | 22.983 | 11.216 | 20.475 | 80.475   |
| 222( 67) | 4 | 17.547 | 24.679 | 25.067 | 11.947 | 14.997 | 77.961   |
| 223( 69) | 4 | 18.361 | 23.504 | 25.143 | 11.301 | 13.728 | 74.482   |
| 223( 66) | 4 | 17.547 | 25.768 | 22.409 | 11.216 | 17.797 | 79.843   |
| 224( 71) | 4 | 18.072 | 24.669 | 24.649 | 11.947 | 20.958 | 82.336   |
| 224( 65) | 4 | 18.486 | 23.594 | 24.515 | 11.301 | 15.258 | 75.451   |
| 224( 70) | 4 | 17.459 | 25.753 | 21.848 | 11.216 | 20.475 | 80.475   |
| 224( 71) | 4 | 18.194 | 24.679 | 23.829 | 11.947 | 18.849 | 80.510   |
| 225( 66) | 4 | 18.609 | 23.504 | 23.902 | 11.301 | 21.400 | 83.428   |
| 225( 71) | 4 | 17.555 | 25.168 | 21.302 | 11.216 | 21.400 | 80.696   |
| 226( 70) | 4 | 18.214 | 24.669 | 23.253 | 11.947 | 20.958 | 81.994   |
| 226( 71) | 4 | 17.728 | 23.534 | 23.304 | 11.301 | 19.726 | 79.245   |
| 226( 72) | 4 | 17.675 | 25.768 | 25.770 | 11.216 | 25.006 | 83.838   |
| 227( 71) | 4 | 18.430 | 24.649 | 22.652 | 11.947 | 21.400 | 83.304   |
| 227( 68) | 4 | 18.845 | 23.504 | 22.022 | 11.301 | 21.400 | 83.446   |
| 227( 73) | 4 | 17.779 | 25.168 | 20.250 | 11.216 | 27.004 | 85.292   |
| 228( 72) | 4 | 18.543 | 24.679 | 22.086 | 11.947 | 25.989 | 85.817   |
| 228( 65) | 4 | 18.553 | 23.504 | 22.154 | 11.301 | 21.400 | 83.349   |
| 228( 74) | 4 | 17.640 | 25.768 | 19.744 | 11.216 | 29.923 | 83.428   |
| 229( 73) | 4 | 18.153 | 24.679 | 21.534 | 11.947 | 28.621 | 87.856   |
| 229( 70) | 4 | 19.069 | 23.534 | 21.600 | 11.301 | 27.608 | 85.335   |
| 229( 75) | 4 | 17.979 | 25.168 | 20.250 | 11.216 | 32.386 | 89.617   |
| 229( 74) | 4 | 18.543 | 24.679 | 23.304 | 11.301 | 26.477 | 87.424   |
| 229( 71) | 4 | 19.177 | 23.504 | 21.060 | 11.216 | 30.846 | 83.000   |
| 229( 76) | 4 | 18.075 | 25.168 | 18.769 | 11.216 | 34.911 | 81.639   |
| 229( 73) | 4 | 18.865 | 24.679 | 24.679 | 11.947 | 33.417 | 81.547   |
| 230( 75) | 4 | 19.292 | 23.523 | 23.523 | 11.301 | 33.185 | 89.539   |
| 230( 74) | 4 | 18.161 | 24.679 | 20.995 | 11.216 | 36.653 | 93.098   |
| 230( 71) | 4 | 19.177 | 23.504 | 21.060 | 11.301 | 35.250 | 92.841   |
| 230( 76) | 4 | 18.075 | 25.168 | 20.220 | 11.216 | 35.194 | 91.058   |
| 231( 73) | 4 | 18.865 | 24.679 | 21.600 | 11.301 | 38.574 | 94.328   |
| 231( 72) | 4 | 19.069 | 23.534 | 21.571 | 11.216 | 37.242 | 94.308   |
| 231( 77) | 4 | 19.368 | 24.649 | 23.523 | 11.301 | 37.374 | 92.712   |
| 231( 77) | 4 | 19.169 | 25.558 | 18.300 | 11.216 | 40.451 | 95.736   |
| 232( 76) | 4 | 15.568 | 24.649 | 17.959 | 11.947 | 39.357 | 95.911   |
| 232( 72) | 4 | 16.345 | 23.504 | 20.220 | 11.301 | 39.655 | 94.520   |
| 232( 78) | 4 | 18.261 | 25.168 | 17.842 | 11.216 | 42.445 | 97.271   |
| 233( 77) | 4 | 19.068 | 24.649 | 19.460 | 11.947 | 40.179 | 96.834   |
| 233( 74) | 4 | 19.485 | 23.504 | 19.519 | 11.301 | 41.248 | 94.558   |
| 233( 77) | 4 | 18.437 | 24.679 | 18.459 | 11.947 | 44.508 | 103.052  |
| 233( 79) | 4 | 19.353 | 23.504 | 19.556 | 11.301 | 45.462 | 96.822   |
| 233( 76) | 4 | 18.437 | 25.168 | 17.174 | 11.216 | 47.333 | 101.490  |
| 234( 75) | 4 | 19.333 | 24.649 | 18.037 | 11.947 | 43.433 | 101.299  |
| 234( 77) | 4 | 19.771 | 23.504 | 18.092 | 11.301 | 47.176 | 100.073  |
| 235( 74) | 4 | 19.260 | 24.679 | 18.459 | 11.947 | 44.508 | 99.853   |
| 235( 81) | 4 | 19.678 | 23.504 | 19.556 | 11.301 | 41.248 | 102.623  |
| 235( 76) | 4 | 19.353 | 24.649 | 19.973 | 11.947 | 48.451 | 102.623  |
| 235( 81) | 4 | 18.437 | 25.168 | 17.174 | 11.216 | 42.946 | 103.445  |
| 235( 80) | 4 | 19.771 | 23.524 | 19.331 | 11.301 | 47.333 | 102.240  |
| 236( 77) | 4 | 19.433 | 24.649 | 18.037 | 11.947 | 46.656 | 104.576  |
| 236( 69) | 4 | 18.427 | 25.168 | 16.962 | 11.216 | 45.608 | 105.619  |
| 236( 74) | 4 | 19.260 | 24.679 | 18.459 | 11.947 | 44.508 | 101.490  |
| 236( 82) | 4 | 19.678 | 23.504 | 19.556 | 11.301 | 41.248 | 102.623  |
| 236( 81) | 4 | 19.353 | 24.649 | 19.973 | 11.947 | 48.451 | 102.623  |
| 236( 78) | 4 | 18.437 | 25.168 | 17.174 | 11.216 | 42.946 | 103.445  |
| 236( 80) | 4 | 19.771 | 23.524 | 19.331 | 11.301 | 47.333 | 102.240  |
| 237( 73) | 4 | 19.437 | 24.649 | 18.037 | 11.947 | 46.656 | 104.576  |
| 237( 62) | 4 | 19.433 | 25.168 | 17.636 | 11.216 | 50.386 | 105.619  |
| 237( 74) | 4 | 19.771 | 23.524 | 19.490 | 11.947 | 50.523 | 105.619  |
| 237( 76) | 4 | 19.771 | 23.524 | 19.547 | 11.301 | 51.004 | 104.435  |
| 237( 84) | 4 | 18.337 | 25.168 | 17.827 | 11.216 | 52.346 | 103.166  |

|          |   |        |        |        |        |        |         |          |       |     |     |     |
|----------|---|--------|--------|--------|--------|--------|---------|----------|-------|-----|-----|-----|
| 239( 83) | 4 | 19.353 | 24.649 | 18.721 | 11.947 | 52.856 | 108.173 | 2498.862 | 3.124 | 0.9 | 1.0 | 5.4 |
| 239( 80) | 4 | 19.771 | 23.504 | 18.779 | 11.301 | 53.265 | 106.868 | 2585.598 | 3.232 | 0.9 | 1.0 | 5.7 |
| 239( 85) | 4 | 18.437 | 25.768 | 18.048 | 11.216 | 54.519 | 109.551 | 2522.768 | 3.153 | 0.9 | 1.0 | 5.2 |
| 240( 84) | 4 | 19.353 | 24.649 | 18.955 | 11.947 | 55.115 | 110.666 | 2488.665 | 3.111 | 1.0 | 1.0 | 5.0 |
| 241( 81) | 4 | 19.771 | 23.504 | 19.013 | 11.301 | 55.383 | 109.201 | 2575.254 | 3.219 | 1.0 | 1.0 | 5.3 |
| 241( 86) | 5 | 18.437 | 25.768 | 18.274 | 11.216 | 56.630 | 111.888 | 2512.616 | 3.141 | 1.0 | 1.0 | 4.8 |

PHYSIOLOGICAL Maturity occurred on Julian Day 240

|          |   |        |        |        |        |        |         |          |       |     |     |     |
|----------|---|--------|--------|--------|--------|--------|---------|----------|-------|-----|-----|-----|
| 241( 85) | 4 | 19.353 | 24.649 | 19.192 | 11.947 | 57.096 | 112.804 | 2478.909 | 3.099 | 1.0 | 1.0 | 4.6 |
| 241( 82) | 4 | 19.771 | 23.504 | 19.251 | 11.301 | 57.234 | 111.290 | 2564.653 | 3.206 | 1.0 | 1.0 | 5.0 |
| 242( 86) | 5 | 19.353 | 24.649 | 19.432 | 11.947 | 59.337 | 115.365 | 2468.993 | 3.086 | 1.0 | 1.0 | 4.2 |

PHYSIOLOGICAL Maturity occurred on Julian Day 242

|          |   |        |        |        |        |        |         |          |       |     |     |     |
|----------|---|--------|--------|--------|--------|--------|---------|----------|-------|-----|-----|-----|
| 242( 83) | 5 | 19.771 | 23.504 | 19.492 | 11.301 | 59.332 | 113.628 | 2554.692 | 3.193 | 1.0 | 1.0 | 4.6 |
|----------|---|--------|--------|--------|--------|--------|---------|----------|-------|-----|-----|-----|

PHYSIOLOGICAL Maturity occurred on Julian Day 242

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NODE 1 MERGED INTO NODE 21
NODE 2 MERGED INTO NODE 21
NODE 3 MERGED INTO NODE 21
FIELD MATURITY REACHED
LEAF= 73.921 CLUM= 57.198 HEAD= 34.464 GRAIN= 175.298 FINAL TOTAL WT = 340.881
CORE USAGE OBJECT CODE= 58168 BYTES, ARRAY AREA= 24180 BYTES, TOTAL AREA AVAILABLE= 174176 BYTES
DIAGNOSTICS NUMBER OF ERRORS= 0, NUMBER OF WARNINGS= 0, NUMBER OF EXTENSIONS= 0
COMPILE TIME= 2.73 SEC, EXECUTION TIME= 30.38 SEC, WAITIV - JUL 1973 V1.4 9.58.06 TUESDAY 28 DEC 76

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THE USE OF A DYNAMIC DIGRAPH STRUCTURE  
IN A POPULATION SIMULATION MODEL  
FOR GRAIN SORGHUM

By

JESS WALTER CURRY, JR.

B.S. Oklahoma State University

Stillwater, 1970

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A MASTER'S REPORT

submitted in partial fulfillment of the  
requirements for the degree

MASTER OF SCIENCE

Department of Computer Science

KANSAS STATE UNIVERSITY

Manhattan, Kansas

1977

## ABSTRACT

This paper describes a model for simulating the growth of a field of grain sorghum. The model consists of a digraph structure, each node representing a logical partition of the field based on variables such as available water, emergence dates, or soil types. The structure is dynamic in that each node can diverge if conditions in different parts of the field become different. Equally important, nodes can converge if conditions change again in such a way that 1) the plants in several different partitions reach the same stage of development and 2) these partitions currently have the same conditions. The model may be applied to any crop simulation system where discrete simulation techniques are used to simulate a single "average" plant.