PRE-BREAKING: DOCUMENTING ITS EFFECTS

by

STEVEN P. CURRAN

B.S., Kansas State University, 1974

A MASTER'S THESIS

submitted in partial fulfillment of the

requirements for the degree

MASTER OF SCIENCE

Department of Grain Science and Industry

KANSAS STATE UNIVERSITY Manhattan, Kansas

1982

Approved by:

Major Professor

Spec. 2011. 2668 .T4 1982 C87

A11202 247633

TABLE OF CONTENTS

Cia	Ž	Page
	INTRODUCTION	. 1
	LITERATURE REVIEW	
	Pre-Breaking	
	Experimental Milling	
	Ash	. 11
	MATERIALS AND METHODS	
	Wheat	. 16
	Pre-Breaking	. 16
	Milling	. 19
	RESULTS AND DISCUSSION	
	Brabender Quadrumat Junior	. 38
	Brabender Quadrumat Senior	. 41
	Buhler Experimental Mill	
10	Ross Walking Flow	. 46
	Miag Multomat Mill	
	11208 1121200000 11212 1 1 1 1 1 1 1 1 1 1 1	
	SUMMARY AND CONCLUSIONS	. 53
	SUGGESTIONS FOR FUTURE WORK	. 55
	LITERATURE CITED	. 56
	LIST OF PLATES, TABLES AND FIGURES	. 58
	ACKNOWLEDGMENTS	. 60
	ACCOMPLED OF THE TOTAL OF THE TAX ASSESSED TO	. 50
	APPENDIX A	. 61
	APPENDIX B	. 171

INTRODUCTION

The purpose of this study is to document the effects of a preliminary breaking of wheat kernels prior to the actual milling process. To further understand this study, a basic explanation of the processing of wheat to obtain white flour should be given.

Most flour milling operations can be divided into six systems: Break System, Middlings Reduction System, Sizings System, Purification System, Tailings System, and Low Grade System. Properly conditioned wheat is first worked upon by the Break System which functions to open the wheat kernel and release particles of endosperm known as sizings and middlings from the bran coat. The Break System can consist of three to seven passages which employ pairs of cylindrical corrugated rolls, called roller mills. The rolls rotate towards each other with one roll rotating about two and one-half times as fast as the other roll. The number of corrugations increases while the depth of the corrugations decreases after each succeeding break. After each grind, the ground material is sent to sifters consisting of sieves covered with various cloths to separate out the different particle sizes. The coarsest material, mostly bran with adhering particles of endosperm, is sent on to the next break. Chunks of endosperm from the Primary Breaks (normally First, Second and Third Breaks), varying in size and purity, are sent to the Purification, Sizing and Middling Reduction Systems. Material from the Secondary Breaks (Fourth and Fifth Breaks) which is more bran-contaminated, is sent to the Tailings and Low Grade Systems. Some flour, made incidently, is removed from each sifting.

In most mills making white flour, materials consisting of endosperm chunks and small bran chips is sent to a Purification System. Purifiers utilize both reciprocating sieves and air currents to grade the stock

further by size and to purify it by lifting off the lighter bran chips. Cleaned endosperm material is then sent to the Sizings or Middlings Systems, depending on the degree of purity.

The larger chunks of endosperm with some adhering bran is sent to the Sizings System. Here, smooth or finely corrugated rolls operating at a differential of about 1.5 to 1 reduce the large particles of endosperm somewhat and at the same time remove adhering bran which is also slightly flattened. Sifters then separate the reduced endosperm chunks (to be sent to the Middlings Reduction System) from the chips of bran and germ which are sent to the Tailings System. Although some high quality flour is recovered in the Sizings System, the main function is to release the endosperm from the chunks of bran and germ and reduce these sizings to middlings.

The primary function of the Middlings Reduction System is to produce flour. Normally, middling stock is ground on smooth rollermills, operating at a differential of 1.5 to 1, set to produce the optimum amount of flour. Any small particles of bran or germ contained in the middlings stock are normally flattened by the rolls and scalped off to the Tailings System, while the middlings material that is not reduced to flour size is sent to the next middlings grind. A normal mill flow will contain four to five middling-reduction grinds with the amount of bran intrusion increasing with each successive pass.

The Tailings System receives stock that is mostly particles of bran with some adhering chunks of endosperm. The primary function is to recover any particles of endosperm to be returned to the Middlings System. The branny stock is sent to feed. A small amount of low quality flour is also

recovered. Again, smooth rolls operating at a low differential are normally used here.

The Low Grade System is the "finishing" system in the mill flow.

Poorer quality stock, not reduced in the Middling-Reduction System, feeds
the Low Grade System. The purpose here is to recover any flour produced
and send the remainder to feed.

The total objective of milling wheat into white flour is to provide an acceptable, uniform product to the customer, be it the commercial or home baker. Acceptability can be based on many different criteria depending on the customer's needs. Ultimately, the successful miller utilizes all the resources available to him to produce the maximum amount of salable flour at the least cost of production.

The purpose of this investigation is to determine whether the preliminary breaking of the wheat kernel prior to the Breaking System in the mill flow is beneficial to the miller in achieving his goals.

LITERATURE REVIEW

Pre-Breaking

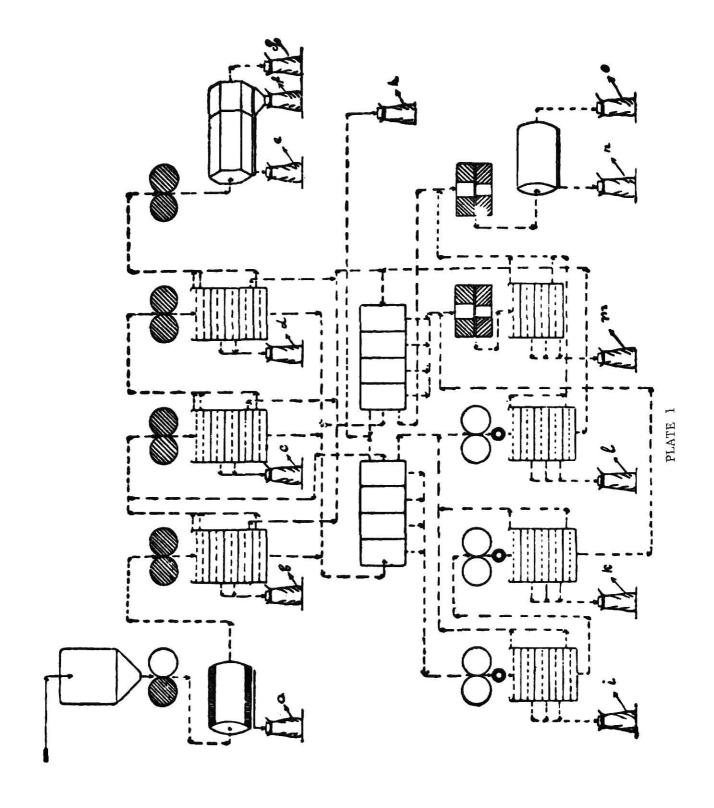
Although the concept of Pre-breaking is not a new one, there is virtually no published information on the subject. Commercial milling companies that utilize pre-breaking systems developed those systems for the most part on their own, and due to the competitive nature of the flour milling business, scientific literature on these systems is not readily available.

Kozmin (1), was the first known author to report on Pre-Breaking systems in discussions of some of the very first gradual reduction milling systems. He wrote, "As regards the character of reduction, high grinding (gradual reduction grinding) may be divided into four separate categories. In the first must be placed the breaking of the berry down the crease, which allows removal of dust settled in the crease from the halves, and otherwise inextractable in the cleaning process." He stated further that the French called this passage "l'avant broyage" or preliminary break and the Germans labeled it "Hochshrot." Two of these very early flowsheets using Pre-Break systems are shown in plates 1 and 2. Flour removed from these Pre-Breaks was called "blue flour" due to the blue-grey appearance as compared to the other recovered flours. Smith (2) also reported that at the time of the introduction of the roller mill in England in 1879, first break was initially used as a cracking roll with the broken grain being sifted immediately to extract what was known as the blue flour or crease dirt. He reported that the technique was dropped due to improved wheat cleaning machinery.

In June of 1929, the <u>National Miller</u> (3) provided a "round table discussion" in which the topic was "Splitting the Wheat in the Crease."

-

FLOWSHEET OF GERMAN SHORT FLOW USING PRE-BREAK



.

FLOWSHEET OF A GERMAN
ABRIDGED HIGH GRINDING FLOW
USING PRE-BREAK

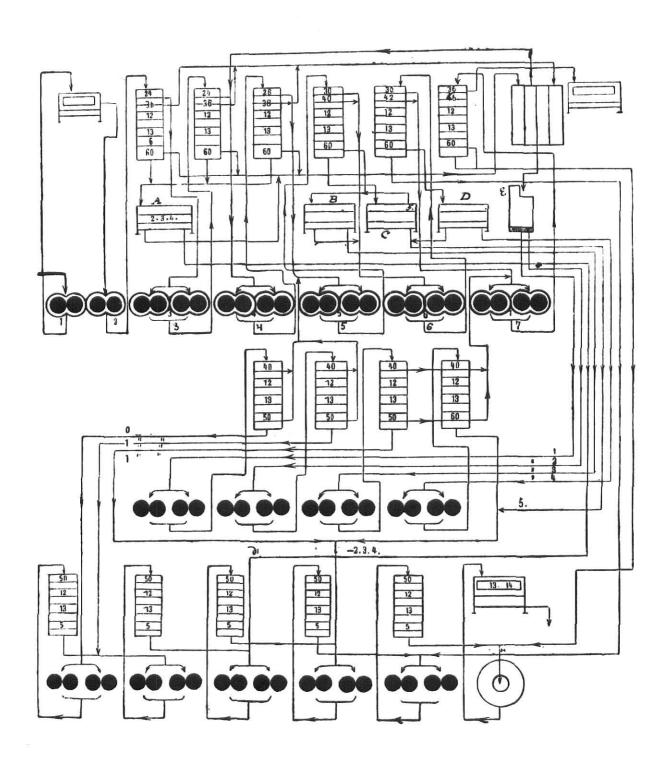


PLATE 2

Opinions of about 50 prominent millers were provided. The majority of the millers at this time felt it was not advantageous to Pre-Break the wheat. Of those that felt it would be advantageous to Pre-Break, most stated that it both removed crease dirt and made a broader bran. Two months later, August of 1929, in an article further discussing the splitting or Pre-Breaking of wheat, Reed (4) reported that the idea was sound, but that what was needed was a machine that could accurately split the wheat through the crease and remove all of the seam impurities and germ. He also finished by saying this couldn't be done.

From these early mentions of pre-breaking, there seems to be no other information published on the subject for a period of about 20 years. Even flow sheets available, dating to this period in time, do not show any use of Pre-Break Systems. In 1952, Farrell and Milner (5), in a survey of U.S. Flour Mills, found that some of the mills were using different forms of Pre-Break systems to help alleviate the problem of insect fragments in the finished flour. These systems utilized impact machines, generally known as entoleters, or rolls, or in some instances both were being used. The wheat was being cracked open by the entoleters or rolls and then followed with aspiration and/or sifting to remove small streams high in insect material. The surveyors gave no particular preference for either the rolls or entoleters but noted there were many variables influencing the effectiveness of the entoleter. Rolls were usually nine or ten inches in diameter and operated at approximately one to one differential. Roll surface was either smooth or finely corrugated with no spiral. Most importantly, the surveyors pointed out that some milling advantages other than insect fragment removal might also accrue from the practice of Pre-Breaking. They stated, "Advantages of pre-breaking claimed by some millers include increase in percentage of patent flours and increase in germ recovery with the resulting benefit of grinding less germ into the flour."

In a report on the use of impact machines for "Pre-Milling Control,"

Zerull (6) pointed out the advantages of such systems to be better mill

balance, cleaner middlings, lower ash due to the removal of more crease

and germ end dirt and due to the better recovery of germ before the break
ing process.

It is not known, exactly, the percentage of Pre-Break Systems in use today in commercial flour mills. In a survey by the Association of Operative Millers Technical Committee (7), Association members were sent questionnaires asking them to provide the information necessary to construct a flow sheet for a new 5000 hundredweight of flour per day flour mill.

Approximately 65 percent of those respondents reported that they would use some form of Pre-Break, either roller mills or impact machines. This may give some approximation as to the actual use of Pre-Break Systems in commercial mills today.

Experimental Milling

Since data from commercial mills is difficult to obtain, testing must be performed on smaller scale experimental mills. The question then arises, "Are experimental mills reliable enough to accurately predict the results of comparable tests on commercial mills?" Anderson (8) related it best when he stated, "The problem then in Experimental Milling resolves itself into the use of a minimum number of basic milling operations to secure results which furnish advance information concerning what will be obtained when wheat from the same mix is milled on the longer commercial system. . . ."

Miller (9) believed that experimental milling represents experimentation on a small scale; however, without it commercial milling itself would be largely experimental.

Rumold (10) stated that experimental milling can provide the miller with advanced milling data and mill chemists with material for analytical investigation. Herman (11) also believed that experimental milling can foretell in close approximation milling quality, yield of wheat and the characteristics of flour from it.

Zeleny (12) states that milling quality can be directly determined by means of experimental milling tests. He also reported that many commercial millers have been reasonably successful in adjusting and operating experimental milling equipment in such a manner that yield and quality of experimentally produced flours closely parallels the yield and quality of commercially produced flours.

The yield of flour and the ash conversion, according to Anderson (8), are two factors which should be observed in experimental milling.

The Ash Test and Cumulative Ash Curves

Once the wheat to be tested has been experimentally milled, the flours must be analyzed to determine if there are any quality differences between the control sample and the test sample. As mentioned earlier, the percentage yield of each flour stream and the ash content of each flour stream are important factors. The yield of each flour stream is self-explanatory but what is ash and why is it useful in studying milling performance and processes?

The Ash test (A.A.C.C. Cereal Laboratory Methods, 08-01) gives a measure of the mineral content of the material being tested. Since pure bran material contains, according to Swanson (13), from 20 to 25 times as

much ash as the pure endosperm, the Ash test has been used as a tool in measuring the amount of bran intrusion in the flour tested.

In the milling operation, a flour is produced each time material is ground and sifted. Commercial mills may have between 20 to 40 different flours being produced at the same time, each with different characteristics, including fairly wide differences in ash content. Since each mill stock classification to be ground has a different bran-to-endosperm ratio, each grind will produce varying amounts of bran intrusion. The breaking process seems to be most critical in this area. Robbins (14) states that "in the final analysis all ash in flour, other than that contained in the pure endosperm, is caused by bran contamination released by the breaks."

The germ of the wheat kernel is also relatively high in ash content. According to MacMasters et al. (15) the ash content of wheat germ in 156 different varieties was found to vary between 4.27 to 9.47% in ash content. This would mean that any germ ground by the corrugated break rolls could also contribute to the ash content of the break flours.

The ash content of pure endosperm also varies within the kernel itself. Morris et al. (16) reported spreads from .246% to .400% ash in Hard Red Winter wheat and spreads from .206% to .564% ash in Hard Red Spring wheat within the endosperm.

Due to the obvious complication of properly applying the ash test, it has been, throughout the years since its inception, misapplied in many instances. However, if properly applied it can be a useful tool. Clark (17) states: "Combined with the knowledge of yield, percentage of extraction, grade of wheat milled, variety of wheat milled, and the equipment of the mill, flour ash may be an index of efficient wheat milling." Shuey (18) believes that when ash is properly used it can be a useful tool or

yardstick for measuring milling characteristics as well as evaluating the milling performance of a mill. Swanson (13) also states, "The Ash test has a greater value than any other analytical determination for the control of the mechanical operation of the flour mill."

A simple listing of the ash content of each stream, however, is of little value. Therefore, methods of coupling the amount of ash contents with the corresponding stream weights have been devised that are of much greater value. Robbins (14) indicates that an ash analysis of the various flour mill streams in a mill when made in connection with a quantity measure of each stream is the most effective means available for studying the ash characteristics of the milling process.

Wissmar (19), believes that the Cumulative Ash Curve, developed by Professor Mohs, can be most useful to analyze mill efficiency. In this analysis, all the ash contents are arranged, lowest to highest ash, along with their corresponding percentage of the total of the milled products. Starting with the lowest ash stream, the next lowest ash stream is, in effect, blended with it to produce a new flour. This is continued until all the flour streams are added in at their corresponding percentages. Cumulated ashes can then be plotted versus their cumulated percentages to give the Cumulative Ash Curve which can be used to judge the effectiveness of milling processes given a common wheat.

.

.,27

PHOTOGRAPH OF WHOLE HARD RED WINTER WHEAT KERNELS
COMPARED WITH WHEAT AFTER PASSING
THROUGH PRE-BREAK ROLLS

PLATE 4

PHOTOGRAPH OF A STRAIGHT GRADE HARD RED WINTER FLOUR AS COMPARED TO FLOUR PRODUCED FROM PRE-BREAKING FROM THE SAME WHEAT, THE PEKAR TEST WAS USED TO SHOW DIFFERENCE IN QUALITY



Whole Wheat

Pre - Broken Wheat



Straight Grade Flour

Pre - Break Flour

PLATE 4

MATERIALS AND METHODS

Wheat

Several varieties of locally grown Hard Red Winter wheat were used for the milling tests. Table I shows some of the physical wheat data for the wheats used. The wheat used is typical of that used commercially for white flour production.

All wheat was cleaned in the Kansas State University Pilot Cleaning House. This flow includes a milling separator, stoner and gravity table, disc machines, Entoleter-Scourer, Aspirator and duo-aspirator. The Flow-sheet is shown in Figure I. The cleaning rate is 60 pounds per minute.

Wheat was conditioned prior to milling by adding water to bring the percentage of moisture in the wheat to about 16%. The wheat and water were thoroughly mixed and then allowed to rest for approximately 20 hours. For the large scale samples, on the Miag Multomat, the Kansas State University Tempering System (Figure I) was used. The remainder of the samples were tempered using a laboratory tempering system which consists of a small revolving drum and graduated cylinder, for metering the water. Since the capacity of the mixer is approximately 5000 grams, any sample lots needed over this amount were first mixed and then cross blended to assure even temper. Sample lots were then stored for the rest period in poly bags. Both initial moisture and moisture before milling were measured on the Tag-Heppenstal Moisture Meter.

Pre-Breaking

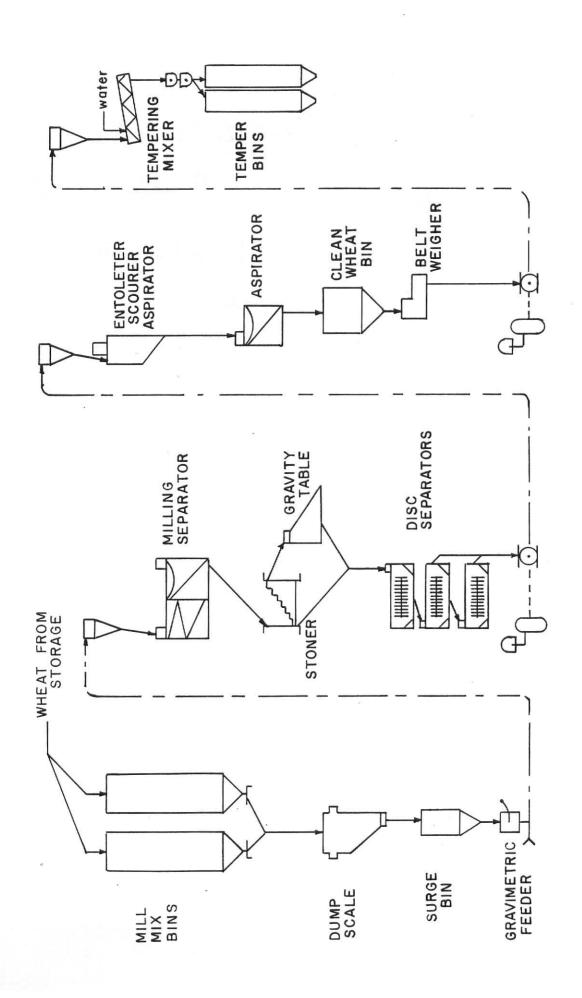
Since it was felt that there may be too many variables in the operation of an impact machine, the rollermill was selected to perform the pre-breaking. In most cases, smooth rolls were driven at approximately a one to one differential and set to ideally open all kernels at the crease.

TABLE 1

WHEAT SPECIFICATIONS

TEST	RESULTS 1
Moisture ²	12.4%
Protein ³	12.5%
Ash ⁴	1.5%
Test Weight ⁵	62.3 lbs/bushel
1000 Kernel Weight ⁶	31.3 gram/1000 kernels
Wheat Size Test ⁷ % Over 7W % over 9W % over 12W Theoretical Yield	70.0% 29.5% 0.5% 76.5%
Pearling Value ⁸	74.7%

- 1. Results given are the averaged results of three samples tested.
- 2. Tag-Heppenstal Moisture Tester.
- 3. AACC Cereal Laboratory Methods, 46-10. Expressed as percent protein on a 14% moisture basis.
- 4. AACC Cereal Laboratory Methods, 08-01. Expressed as percent ash on a 14% moisture basis.
- 5. As described in Circular No. 921, issued by the United States Department of Agriculture. Expressed as pounds, to the nearest tenth of a pound, per Winchester bushel.
- 6. 40 grams of whole, cleaned wheat is counted using an electronic seed counter. The number of kernels in 40 grams is then converted to the number of grams per 1000 kernels.
- 7. 200 grams of cleaned wheat is sifted for 1 minute using a Ro-Tap Shaker and 3 Tyler sieves of 7 wire, 9 wire, and 12 wire. The percentage remaining on each sieve is then determined, multiplied by factors of 78, 73 and 67, respectively, and summed to obtain a single number denoting the theoretical flour yield.
- 8. 20 grams of cleaned, whole wheat is retained for one minute in a Strong Scott Laboratory Barley Pearler equipped with a No. 30 grit stone and 1 10 mesh screen made of wire .041 inches in diameter (Tyler Code "Fijor"). Pearling value is the percent of original sample remaining over a 20 mesh wire after pearling.



System Tempering and State University Cleaning Figure Kansas

Plate 3 shows wheat after passage through a pre-break versus the whole wheat.

Milling

Five different experimental mills were used in this research:

Brabender Quadrumat Junior, Brabender Quadrumat Senior, Buhler Experimental Rollermill, K.S.U. Ross Walking Flow, and Miag Multomat. Since each mill employs a different method of operation and procedure of testing, each will be described separately.

(1) Brabender Quadrumat Junior (Figure 2, plate 5)

As can be seen from the flowsheet, the Quadrumat Junior makes three grinds with four corrugated rolls at a fixed gap before the stock is sifted. Normally, the ground material is sifted over a reel-type sifter that is part of the mill. To provide a better separation, the ground stock was sifted using a Great Western laboratory sifter having a speed of 180 rpm and throw of 4 inches. Sieves of 50 grits gauze, 70 grits gauze, and 9XX silk were used to make the separations, with cleaner frames below the 70GG and 9XX to aid in sifting. Sifting time was set at two minutes.

A Ross Experimental Rollstand, equipped with a pair of 9-inch diameter by 6-inch wide smooth rolls, was used to Pre-Break the wheat prior to milling on the Quadrumat Junior. The differential chain had been removed to give an approximate 1:1 differential, with the passage of the wheat turning the slow roll. A no load gap of .068 inch was chosen to perform the Pre-Breaking operation. This gap was used because it affected nearly every kernel to some extent but was not so severe that kernels were completely broken up.

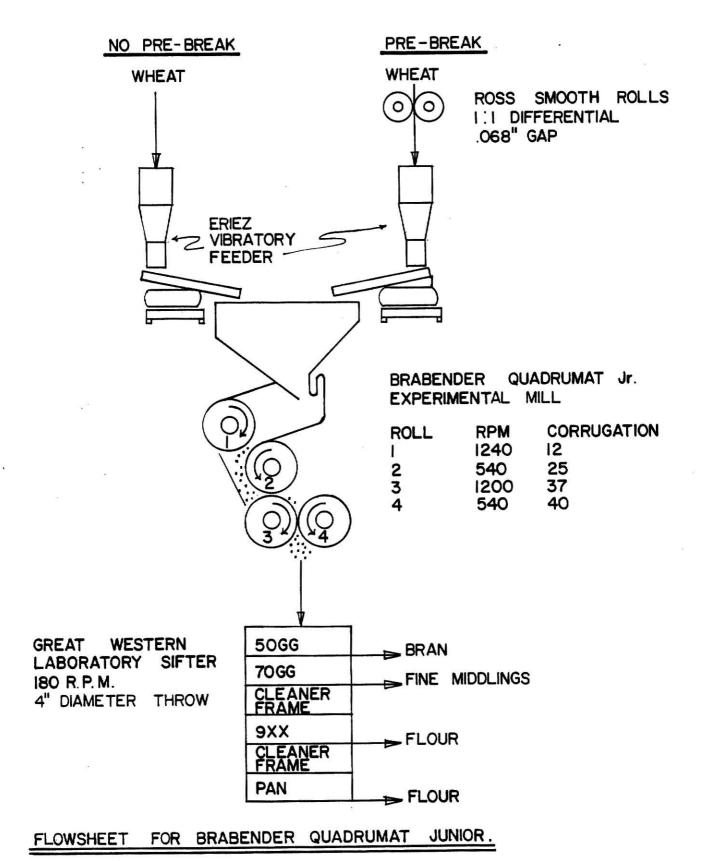


Figure 2

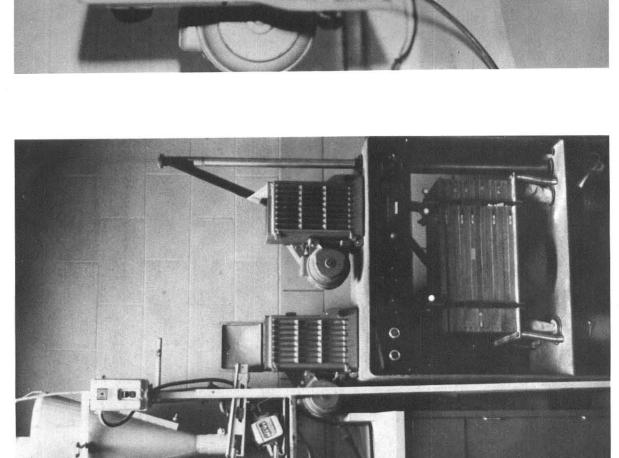
2.

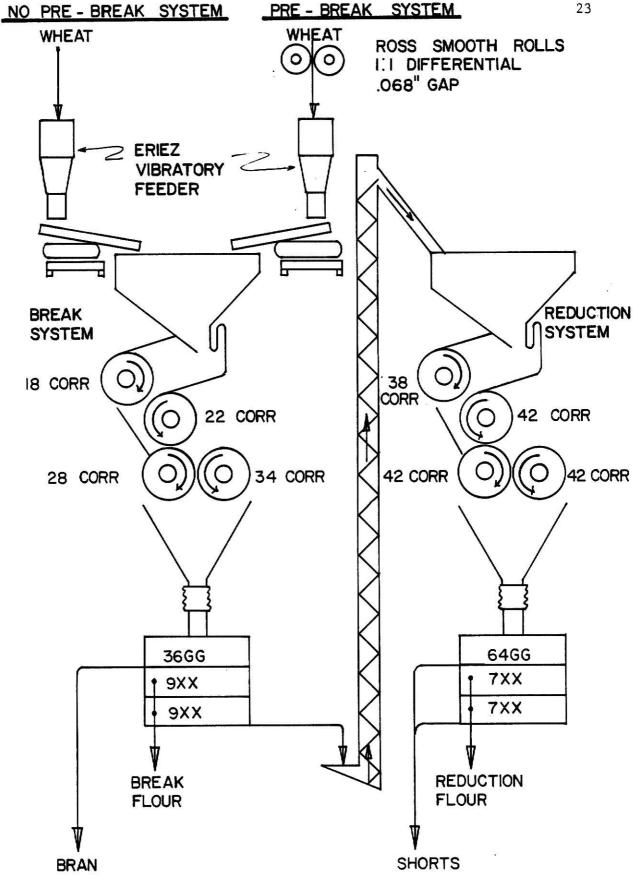
VIEW OF BRABENDER QUADRUMAT SENIOR EXPERIMENTAL MILL SHOWING SPECIAL FEEDING SYSTEM

PLATE 5

VIEW OF BRABENDER QUADRUMAT JUNIOR EXPERIMENTAL MILL







QUADRUMAT SENIOR. FOR BRABENDER FLOWSHEET

Since the flowability of the Pre-Broken wheat changed drastically, a further modification of the Quadrumat Junior had to be made. To allow the stock to flow properly, the feeder roll had to be removed. An Eriez vibratory feeder, with variable speed control, was then used to set the flow of whole wheat or Pre-Broken wheat to the mill. A feedrate of approximately 55 grams per minute was used for the grain to the mill.

After the feed rate was established, by running one minute tests, the mill was started and the feeder was set to run for exactly five minutes. The first five minute sample was set aside as the warm-up sample. A second five minute sample was then milled and sifted on the stack of sieves. Each separation was carefully weighed and the three finest separations were sampled and submitted for laboratory moisture and ash analysis. The feeder was then reset to deliver Pre-Broken wheat at the same feed rate. Again, a warm-up sample was first milled prior to milling the test sample. The test sample was sifted and the same fractions sampled for analysis. A total of five whole wheat samples and five Pre-Broken samples were milled with warm-up samples preceding each test run.

(2) Brabender Quadrumat Senior (Figure 3, plate 6)

As can been seen from the flowsheet and photograph, the Quadrumat Senior is similar to the Quadrumat Junior but utilizes more elaborate grinding and sifting equipment. Two grinding heads are used, one for Break grinding and one for Reduction grinding. Again, all rolls are corrugated and positioned at a fixed gap. A gyratory sifter, having a speed of 240 rpm and throw of 1-3/4 inches, is equipped with specially designed sieves for maximum efficiency.

Ground material from the Break head is sifted over 36 grits gauze to remove the bran and over two 9XX silks to remove the Break flour.

Middlings stock remaining above the 9XX is conveyed, by a vertical screw conveyor to the reduction head. Ground middlings from the Reduction head are then sifted over a 64 grits gauze and two 7XX silks. Any material not passing through the 7XX as flour is considered shorts.

As in the procedure for the Quadrumat Junior, a smooth pair of Ross rolls, running at a 1:1 differential, was used to Pre-Break the wheat. The roll gap of .068 inch was again used as the roll setting.

The Eriez vibratory feeder had to be used for feeding the stock to the mill due to the flow problem of the Pre-Broken wheat as developed in the Quadrumat Junior testing. The feeder roll from the Break head was also removed.

The testing procedure itself began by adjusting the vibratory feeder to a feed rate of approximately 130 grams per minute with whole wheat. The mill was then started and wheat was fed to the Break head for warm-up. The vibratory feeder was automatically timed to stop at the end of five minutes. When feed to the mill stopped, the mill was immediately shut down under load. Material from the four product containers was removed and the containers were replaced. The mill was then restarted and wheat was re-fed to the Break head to start the test sample. Again, at the end of five minutes, the feeder was stopped and the mill was shut down under load. The product containers were removed and the materials weighed. Samples of Break flour and Reduction flour were submitted to the analytical laboratory for moisture and ash analysis.

The feeder was then readjusted to feed the Pre-Broken wheat at 130 grams per minute and the above procedure was then repeated. The whole wheat and Pre-Broken wheat each was milled a total of five times.

(3) Buhler Experimental Mill (Figure 4, plate 7)

The Buhler Experimental Mill flow is somewhat different from the mill flows previously described. In the first two mills described, all the grinding is performed before any sifting. The Buhler flow provides grinding and sifting combinations much like those of a commercial mill. There are three corrugated break rolls and three smooth reduction rolls each with their own sifter section. Material to each roll is transported pneumatically. The six flours produced are collected individually in pans as are the feed products: bran and shorts.

Besides testing the effect of not Pre-Breaking the wheat prior to milling versus the effect of Pre-Breaking, a new variable was added. Pre-broken wheat was also sifted over a 10XX flour silk before being milled. This was done to determine whether removing the small amount of flour produced by Pre-Breaking would have any different effect on total flour quality. Some Pre-Break flour is shown in plate 4 compared to a straight grade flour.

Two thousand grams of the sample to be milled was placed in the feeder hopper and the feed rate set to approximately 125 grams per minute. The mill was then started and adjusted to provide proper milling classifications. When the feeder hopper emptied, the mill was immediately shut down under load. Product in the sample pans was weighed and recorded as "warm-up." A second 2000 gram sample of the same material was then placed in the feeder hopper and the mill was restarted. Again, as soon as the sample emptied from the hopper, the mill was shut down under load. All products from this milling were carefully weighed and samples of each of the six flours were submitted for moisture and ash analysis.

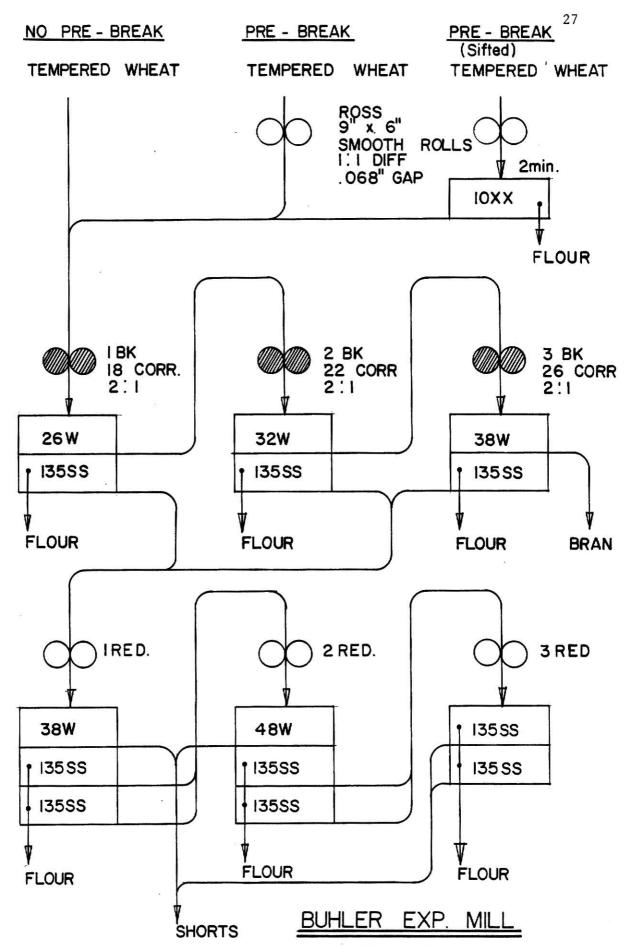


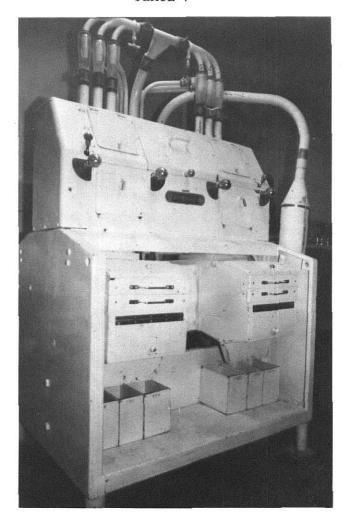
Figure 4

VIEW OF BUHLER EXPERIMENTAL MILL

PLATE 8

VIEW OF ROSS EXPERIMENTAL ROLL STANDS

PLATE 7



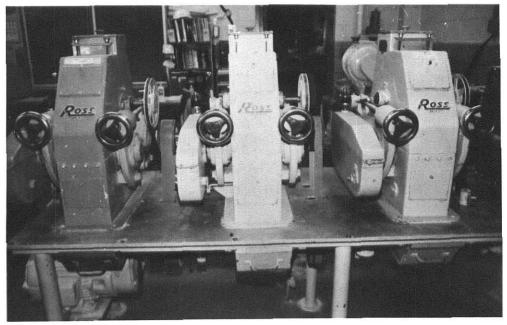
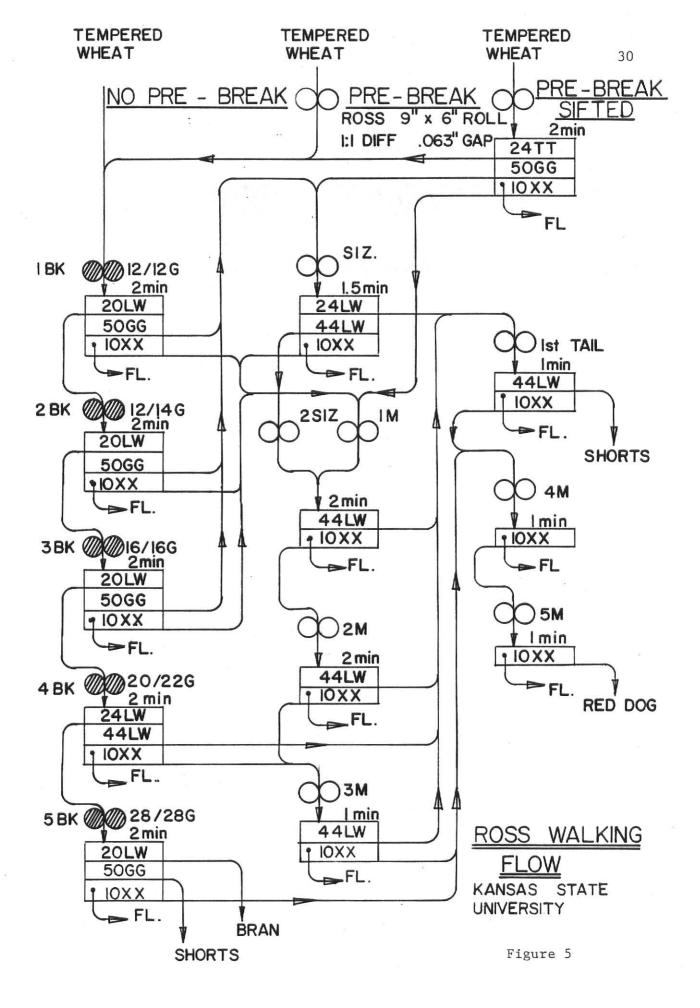


PLATE 8



The sequence in which the control and the two experimental samples were milled was changed for each day of milling. To provide further check on the milling, an extra sample of the first sample milled for that day was also milled. This series of four millings was performed a total of five times as follows:

Test A

- (1) No Pre-Break
- (2) Pre-Break (not sifted)
- (3) Pre-Break (sifted)
- (4) No Pre-Break

Break

- (1) Pre-Break (not sifted)
- (2) Pre-Break (sifted)

Test C

- (3) No Pre-Break
- (4) Pre-Break (not sifted)

Test B

- (1) Pre-Break (sifted)
- (2) No Pre-Break
- (3) Pre-Break (not sifted)
- (4) Pre-Break (sifted)

Test D

- (1) No Pre-Break
- (2) Pre-Break (sifted)
- (3) Pre-Break (not sifted)
- (4) No Pre-Break

Test E

- (1) Pre-Break (sifted)
- (2) Pre-Break (not sifted)
- (3) No Pre-Break
- (4) Pre-Break (sifted)

Again, the smooth Ross rolls set at a .068 inch gap were used to perform the Pre-Breaking prior to milling on the Buhler Mill. A Great
Western laboratory sifter was used to sift the pre-broken sample. Flour obtained from this sifting was weighed and analyzed.

(4) K.S.U. Ross Walking Flow (Figure 5, plate 8)

Although it is a batch operation rather than a continuous one, the Ross Walking Flow very closely simulates a full scale mill. As can be seen by the flowsheet, there are five Breaks and eight Reductions producing twelve flours, red dog, shorts and bran. Roll corrugations and differentials are given in the flowsheet.

Stock is fed by feeder rolls above each pair of rolls and the resulting ground material is caught in drawers below each roll stand.

The ground stock is then transferred to a sifter to make the size separations.

Break rolls were set according to a Break Release Schedule. A 100-gram sample of each Break Stock was ground on the proper roll and then sifted for 20 seconds over a 20 light wire sieve. The overs and thrus were then weighed to determine the percentage that had passed through the wire cloth, that being referred to as the amount "released." The rolls were then readjusted, if needed, to meet the desired release. The Break Release schedule used for the Roll Walking Flow is given as follows:

		<u>% −20 L.W.</u>
lst	Break	30
2nd	Break	40
3rd	Break	35
4th	Break	20
5th	Break	±30

Sizings rolls were set at a standard gap of .005 inch while second sizings and first tailings were standardized at .003 inch gap. All other rolls were set at less than .002 inch to produce as much flour as possible without producing flakes.

Sample size was 3000 grams. Since the Great Western laboratory sifter used here could not properly sift this amount, the sample was divided into two parts for First, Second and Third Breaks, Sizings and First Midds. The sifting times are listed on the flowsheet above each sifter box designation.

All stocks waiting to be ground or sifted were kept in aluminum cans with tight lids to keep moisture loss to a minimum. Each rollermill was cleaned thoroughly above and below the rolls to keep product loss to a minimum.

Three conditions were tested using the Ross Walking Flow. First, wheat was sent directly to First Break for the "No Pre-Break" test.

Second, wheat was Pre-Broken on the Ross smooth rolls at a .068 inch gap and then sent directly to First Break. Third, Pre-Broken wheat was sifted over a special stack of sieves to remove Sizings stock, Middlings stock and flour before being sent to First Break. These flows are shown in Figure 5.

All three test conditions were milled in one day. The tests were repeated a total of five times, each time milling the samples in a random order. After weighing, each flour was sampled and submitted to the analytical laboratory for moisture and ash analysis.

(5) Miag Multomat Experimental Mill (Figure 6, plates 9 and 10)

The Multomat Experimental Mill is a three-break, five-reduction

pneumatic mill. There are ten sifter sections, two of which are redust

sections. Speed of the sifter is 260 rpm at a 1-7/8 inch throw. The ten

flour streams are collected in pans beneath the sifter sections. This

being one of the largest of the experimental mills, feed rates from 700 to

1000 grams per minute may be used. The rate of wheat to the mill is set

by a Draver-type Feeder, which for these tests was set to deliver approximately 780 grams per minute.

The Break rolls were set according to a Break Release Schedule during operation. One-hundred grams of each break grind was sifted over a 20 mesh light wire for 20 seconds on a Rotomatic laboratory sifter operating at 180 rpm and 1-7/8 inch throw. The amount of material passing through the sieve was determined and the rolls were set to meet the following Break Release Schedule:

First Break 45% Second Break 50% Third Break ±35% (clean-up)

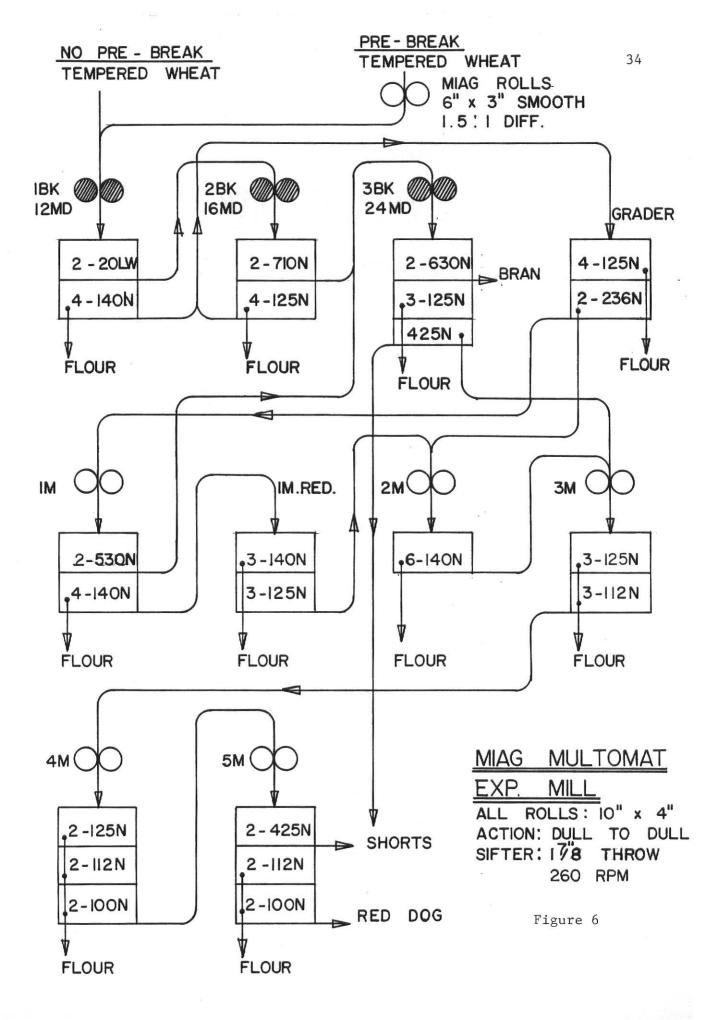


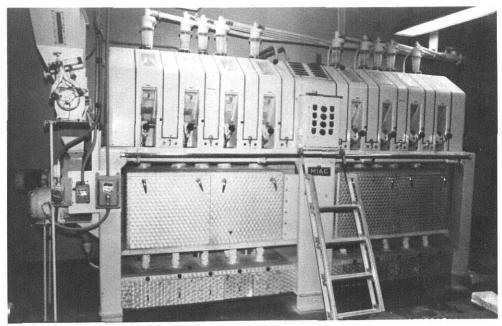
PLATE 9

PHOTOGRAPH OF THE MIAG MULTOMAT EXPERIMENTAL MILL

PLATE 10

PHOTOGRAPH OF MIAG PRE-BREAK ROLLS FOR THE MIAG MULTOMAT

PLATE 9



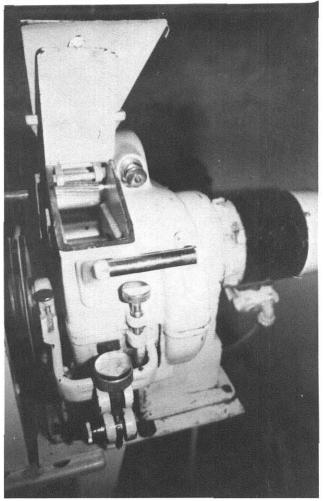


PLATE 10

Due to the relatively long reduction system on this mill, First Midds roll was set to grind to that more typical of a Sizings grind. The remaining rolls were set to produce flour.

This particular mill has been equipped with its own Pre-Break System (plate 10). Wheat from the feeder is fed directly to a pair of smooth six inch diameter by three inch wide rolls operating at a 1.5 to 1 differential. The grind on the Pre-Break roll was set with the use of a test sifter to give a two to three percent release through a 20 mesh light wire. The rolls could also be opened wide to allow the wheat to pass untouched when Pre-Breaking was not wanted.

The mill was allowed to "warm-up" on the sample being milled for a period of thirty minutes, during which time all rolls were set for proper grind. At the end of thirty minutes the wheat feeder was shut off and immediately following, the entire mill was shut down under load. All material pans were emptied and replaced. The mill was then restarted and wheat was again started to the mill. Break rolls and reduction rolls were again quickly checked for proper adjustment. At the end of forty-five minutes, the wheat feeder was shut off with the mill shut down immediately following. At this time all materials produced were carefully weighed and the flour streams were sampled for ash and moisture analysis.

The mill was again restarted and wheat fed to it. At this time, the Pre-Break rolls were either set for pre-breaking or opened fully, depending on the previous test. The above procedures of mill operation again followed. A total of five no Pre-Break/Pre-Break test series were run.

RESULTS AND DISCUSSION

Flour stream weights and their corresponding ash contents, on a 14% moisture basis, for the five millings of each of the experimental mill flows were averaged and from this, cumulative flour ash was calculated. Tables showing flour weights, their percentages of the total products and their ash contents as well as the cumulative ash calculations are given for each mill flow. Cumulative flour ash curves depicting the results are also given for each experimental mill. The summation of percentages of total product (S of Q) is given by the x-axis and the summation of the product of each stream ash times its percentage of total product dividend by the summation of percentages of total product (S of Q x A/S of Q) is given by the y-axis.

Complete stream weights, feed rates, and other miscellaneous information for each milling is listed in the appendix. Cumulative ash calculations and cumulative ash curves are also given in the appendix for each individual milling test.

(1) Brabender Quadrumat Junior.

Table 2 shows the averaged stream weights and ash contents of flours produced by the five millings as well as the cumulative ash calculations for the Quadrumat Junior. Figure 7 shows the results of the calculations graphically. The two flour streams sampled and shown are the throughs of a 70GG sieve and overs of a 9XX sieve (labeled +9XX) and the throughs of a 9XX (labeled -9XX).

As can be seen by both the calculations and cumulative ash curves, the use of Pre-Breaking prior to milling of the Quadrumat Junior provides a definite improvement in milling performance. In addition to substantially lowering the flour ash, flour yield was also improved by about .5%.

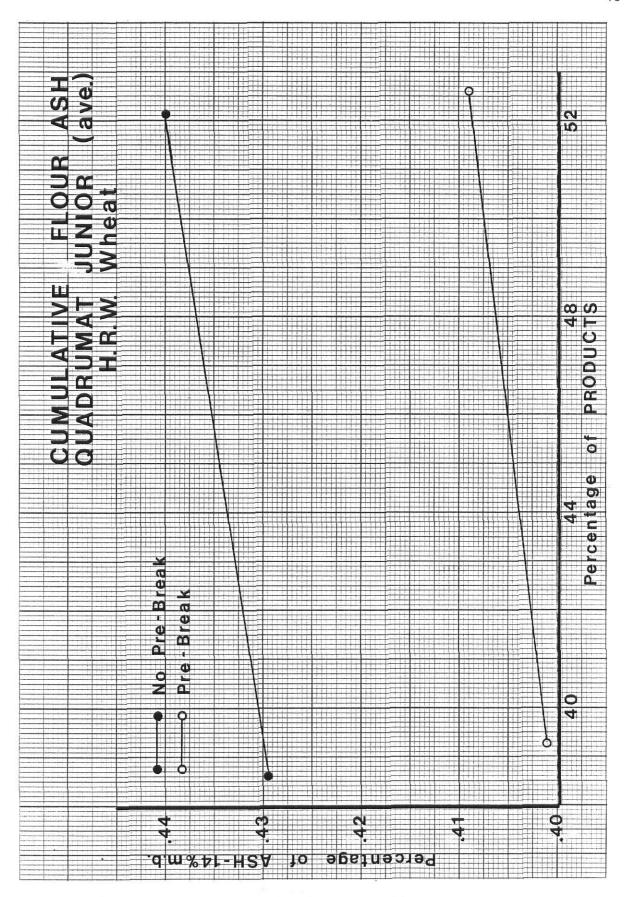
Table 2

Cumulative Flour Ash Calculations

A=ASH(14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL QUADRUMAT JUNIOR
TEST AVERAGE
HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QXA
			NO PRE	-BREAK			
-9XX	112	38.57	38.57	.429	16.54	16.54	.429
+9XX	39	13.50	52.07	.440	5.94	22.48	.432
			PRE-B	REAK			
-9XX	115	39.24	39.24	.402	15.77	15.77	.402
+9XX	39	13.35	52.59	.408	5.53	21.30	.405
		-					
					50 8 8 W		



Tigure 7

(2) Brabender Quadrumat Senior.

Table 3 lists the cumulative ash calculations for the average of the five millings on the Quadrumat Senior. The results are shown graphically in Figure 8. Two flours were produced and analyzed. Break flour (Brk. Fl.) was the throughs of two 9XX sieves produced by the break head and Reduction Flour (Red. Fl.) was the throughs of two 7XX sieves produced by the reduction head.

As in the Quadrumat Junior tests, a definite improvement is also seen by the use of Pre-Break on the resultant flour quality produced by the Quadrumat Senior. Flour ash content was lowered significantly and flour yield was also improved, again by .5%.

Most of this improvement came with more break flour being produced at a lower ash content. Since the rolls in the Quadrumat Senior are positioned at a fixed gap, the results would indicate that the Pre-Breaking of wheat provides less severity of grind by the break rolls. More low ash break flour is produced as well as cleaner middlings (overs of the flour cloths) being sent to the reduction head, as evidenced by the lower ash of the reduction flour.

(3) Buhler Experimental Mill.

Flour stream weights for the average of the millings on the Buhler Experimental Mill and the cumulative ash calculations are given by Table 4. The resulting cumulative flour ash curves are given by Figure 9. Flour streams analyzed were as follows:

Pre-Break	(P.BK)
First Break	(1 BK)
Second Break	(2 BK)
Third Break	(3 BK)
First Reduction	(1 RED)
Second Reduction	(2 RED)
Third Reduction	(3 RED)

Table 3

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)

Q=QUANTITY (% of Total Products)

S = SUMMATION

MILL QUADRUMAT SENIOR
TEST AVERAGE
WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	А	QXA	S of QXA	S of QXA
		1	NO PRE	-BREAK			
BRK.FL.	120	18.546	18.546	.335	6,213	6.213	.335
RED.FL.	319	49.492	68.038	.343	16.976	23.189	.341
				- Marketin de la sidil de la			
	neprisa and an indext (2) and (2)		PRE-B	REAK			
BRK.FL.	133	19.946	19.946	.312	6.223	6.223	.312
RED.FL.	326	48.676	68.622	.331	16.112	22.335	.325
							KOLILI AWAY
				W-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	TATION OF THE STATE STATE OF THE STATE OF TH		
			· · · · · · · · · · · · · · · · · · ·				
							· · · · · · · · · · · · · · · · · · ·
		is and a supplement			**************************************		

		- Commenter was the second					
					The state of the state of		
						and the same and t	
		WILLIAM TO THE PARTY OF THE PAR	www.				
:			Beering year 12 - 110,500 cost	Message and a second of the second		er anna e	
		i wii a waa a					wan just a second

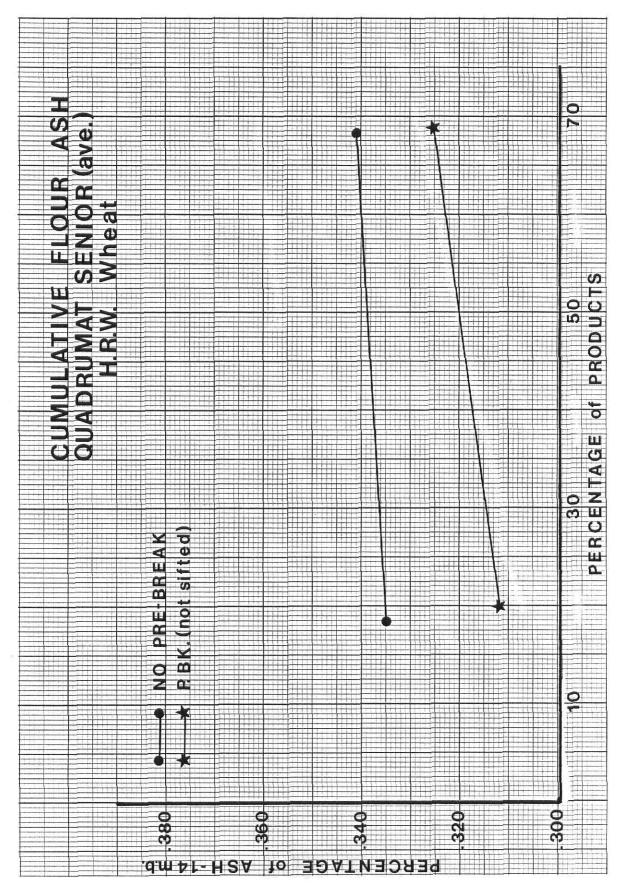


figure 8

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL BUHLER EXP. MILL
TEST AVERAGE
WHEAT HARD RED WINTER

1 RED. 753 1 BK. 151 2 BK. 113 2 RED. 237 3 BK. 32 3 RED. 102 1 RED. 754 1 BK. 158 2 BK. 113 2 RED. 214 3 BK. 33 3 RED. 102	38.15 7.65 5.72 12.01 1.62 5.17 P 39.31 8.24 5.89 11.16 1.72 5.32	NO PRE- 38.15 45.80 51.52 62.53 65.15 70.32 RE-BREAK 39.31 47.55 53.44 64.60 66.32	-BREAK	12.704 2.731 2.094 5.212 0.885 3.361 ED) 12.265 2.752 2.091	12.704 15.435 17.529 22.741 23.626 26.987	.333 .337 .340 .358 .363 .384
1 BK. 151 2 BK. 113 2 RED. 237 3 BK. 32 3 RED. 102 1 RED. 754 1 BK. 158 2 BK. 113 2 RED. 214 3 BK. 33 3 RED. 102	7.65 5.72 12.01 1.62 5.17 P 39.31 8.24 5.89 11.16 1.72	45.80 51.52 62.53 65.15 70.32 RE-BREAK 39.31 47.55 53.44 64.60	.357 .366 .434 .546 .650 (NOT SIFT) .312 .334 .355	2.731 2.094 5.212 0.885 3.361 ED) 12.265 2.752	15.435 17.529 22.741 23.626 26.987	.337 .340 .358 .363 .384
2 BK. 113 2 RED. 237 3 BK. 32 3 RED. 102 1 RED. 754 1 BK. 158 2 BK. 113 2 RED. 214 3 BK. 33 3 RED. 102	5.72 12.01 1.62 5.17 P 39.31 8.24 5.89 11.16 1.72	51.52 62.53 65.15 70.32 RE-BREAK 39.31 47.55 53.44 64.60	.366 .434 .546 .650 (NOT SIFT) .312 .334 .355	2.094 5.212 0.885 3.361 ED) 12.265 2.752	17.529 22.741 23.626 26.987 12.265 15.017	.340 .358 .363 .384
2 RED. 237 3 BK. 32 3 RED. 102 1 RED. 754 1 BK. 158 2 BK. 113 2 RED. 214 3 BK. 33 3 RED. 102	12.01 1.62 5.17 P 39.31 8.24 5.89 11.16 1.72	62.53 65.15 70.32 RE-BREAK 39.31 47.55 53.44 64.60	.434 .546 .650 (NOT SIFT) .312 .334 .355	5.212 0.885 3.361 ED) 12.265 2.752	22.741 23.626 26.987 12.265 15.017	.358 .363 .384
3 BK. 32 3 RED. 102 1 RED. 754 1 BK. 158 2 BK. 113 2 RED. 214 3 BK. 33 3 RED. 102	1.62 5.17 P 39.31 8.24 5.89 11.16 1.72	65.15 70.32 RE-BREAK 39.31 47.55 53.44 64.60	.546 .650 (NOT SIFT) .312 .334 .355	0.885 3.361 ED) 12.265 2.752	23.626 26.987 12.265 15.017	.363
1 RED. 754 1 BK. 158 2 BK. 113 2 RED. 214 3 BK. 33 3 RED. 102	5.17 P 39.31 8.24 5.89 11.16 1.72	70.32 RE-BREAK 39.31 47.55 53.44 64.60	.650 (NOT SIFT) .312 .334 .355	3.361 ED) 12.265 2.752	12.265 15.017	.384
1 RED. 754 1 BK. 158 2 BK. 113 2 RED. 214 3 BK. 33 3 RED. 102	39.31 8.24 5.89 11.16 1.72	RE-BREAK 39.31 47.55 53.44 64.60	(NOT SIFT) .312 .334 .355	ED) 12.265 2.752	12.265 15.017	.312
1 BK. 158 2 BK. 113 2 RED. 214 3 BK. 33 3 RED. 102	39.31 8.24 5.89 11.16 1.72	39.31 47.55 53.44 64.60	.312 .334 .355	12.265	15.017	
1 BK. 158 2 BK. 113 2 RED. 214 3 BK. 33 3 RED. 102	39.31 8.24 5.89 11.16 1.72	39.31 47.55 53.44 64.60	.312 .334 .355	12.265	15.017	
1 BK. 158 2 BK. 113 2 RED. 214 3 BK. 33 3 RED. 102	8.24 5.89 11.16 1.72	47.55 53.44 64.60	.334	2.752	15.017	
2 BK. 113 2 RED. 214 3 BK. 33 3 RED. 102	5.89 11.16 1.72	53.44 64.60	.355			316
2 RED. 214 3 BK. 33 3 RED. 102	11.16 1.72	64.60		2.091		
3 BK. 33 3 RED. 102	1.72		.404		17.108	.320
3 RED. 102		66.32		4.509	21.617	.335
	5.32		.525	0.903	22.520	.340
1 RED. 746		71.64	.577	3.070	25.590	.357
I RED. 746						
1 RED. 746		PRE-BREAK	(SIFTED))		
	39.08	39.08	.311	12.154	12.154	.311
L BK. 146	7.65	46.73	.327	2.502	14.656	.314
2 BK. 110	5.76	52.49	.348	2.004	16.660	.317
2 RED. 215	11.26	63.75	.391	4.403	21.063	.330
3 BK. 32	1.68	65.43	.519	0.872	21.935	.335
P.BK. 9	0.47	65.90	.550	0.259	22.194	.337
3 RED, 104	5.45	71.35	.553	3.014	25.208	.353

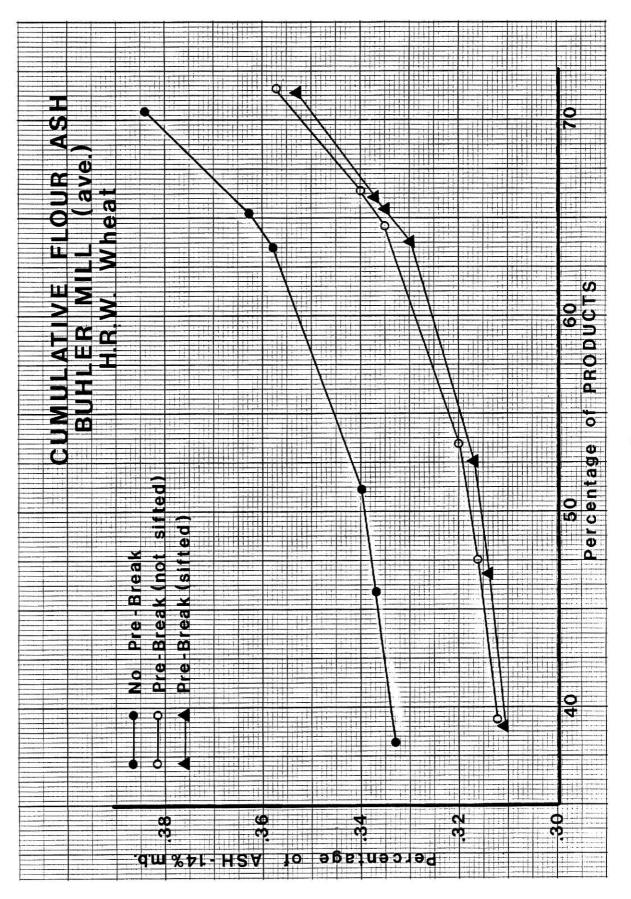


Figure 9

As mentioned in the methods, Pre-Broken wheat was both fed directly to first break on the Buhler Mill and sifted over a 9XX sieve to remove the Pre-Break flour produced before feeding to first break. As shown by the results, both methods of Pre-Breaking gave much improved milling results over not Pre-Breaking. A slight improvement is also shown by having sifted the Pre-Broken wheat prior to first break over Pre-Breaking without sifting.

All flour streams from the Pre-Break tests show improvement in ash contents and more than 1% average increase in flour extraction.

(4) Ross Walking Flow.

Table 5 gives the flour stream data and cumulative ash calculations for the average of the Ross flow millings. Figure 10 shows the cumulative flour ash curves of the plotted data. Flour streams analyzed were as follows:

Pre-Break	(P.BK)	Sizings	(SIZ)
First Break	(1 BK)	First Midds	(1 M)
Second Break	(2 BK)	Second Midds	(2 M)
Third Break	(3 BK)	Third Midds	(3 M)
Fourth Break	(4 BK)	First Tailing	(1 TA)
Fifth Break	(5 BK)	Fourth Midds	(4 M)
	57.5	Fifth Midds	(5 M)

Here again, other than feeding Pre-Broken stock directly to First Break, sifting was also performed on the stock before First Break grind. In this instance, as indicated by the flow sheet (Figure 5), the Pre-Break sifter was more elaborate. Other than removing the flour produced by Pre-Breaking, the sizings and middlings produced were also removed and sent to sizings and middlings grinds.

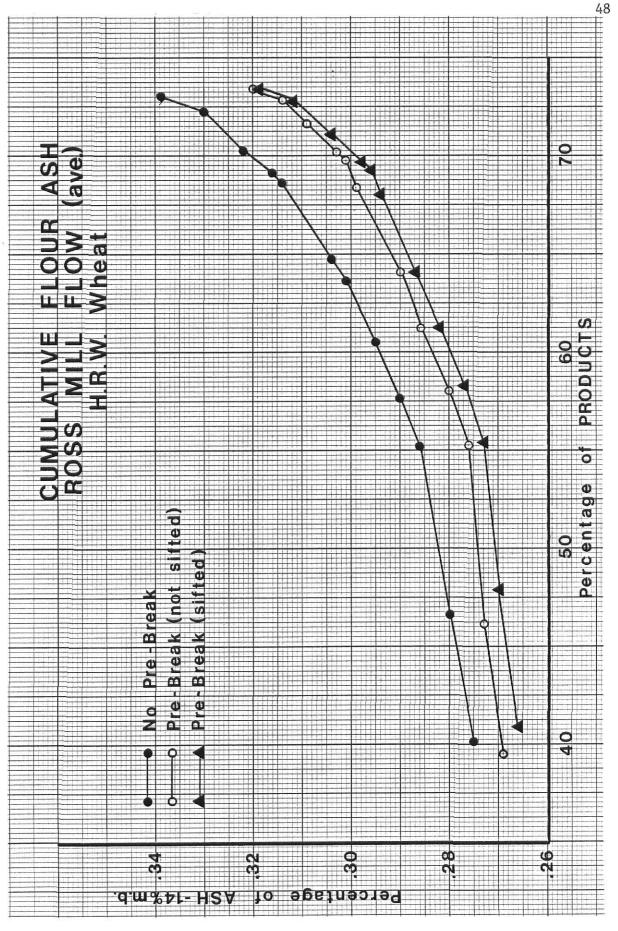
The cumulative ash curves again show a distinct improvement in milling performance by the use of the Pre-Breaking of the grain before actual

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)
Q=QUANTITY (% of Total. Products)
S=SUMMATION

MILL ROSS WALKING FLOW
AVERAGE
HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	QXA	S of QXA	S of QXA
			NO PRI	E-BREAK		•	
1 M	1171	40.05	40.05	.275	11.014	11.014	.275
SIZ	197	6.75	46.80	.311	2.099	13.113	.280
2 M	244	8.34	55.14	.317	2.644	15.575	.286
3 BK	72	2.47	57.61	.383	0.946	16.703	.290
2 BK	85	2.89	60.50	.406	1.173	17.876	.295
3 M	92	3.16	63.66	.409	1.292	19.169	.301
4 BK	34	1.18	64.84	.445	0.525	19.694	.304
1 BK	109	3.72	68.56	.494	1.838	21.531	.314
1 TA	14	0.49	69.05	.578	0.283	21.815	.316
5 BK	39	1.35	70.40	.617	0.833	22.648	.322
4 M	. 55	1.89	72.29	.633	1.196	23.844	.330
5 M	21	0.73	73.02	1.243	0.907	24.751	.339
		P	RE-BREAK ((NOT SIFTE	0)		
1 M	1150	39.51	39.51	.269	10.628	10.628	.269
SIZ	194	6.66	46.17	.295	1.965	12.593	.273
2 M	266	9.12	55.29	.295	2.690	15.283	.276
3 BK	79	2.70	57.99	.364	0.983	16.266	280
2 BK	93	3.18	61.17	.381	1.212	17.478	.286
3 M	83	2.85	64.02	.392	1.117	18.595	.290
1 BK	127	4.35	68.37	.418	1.818	20.413	. 299
4 BK	39	1.33	69.70	.427	0.568	20.981	.301
1 TA	12	0.43	70.13	.571	0.246	21.227	.303
4 M	44	1.50	71.63	.607	0.911	22.137	.309
5 BI	36	1.22	72.85	.615	0.750	22.887	.314
5 M	16	0.56	73.41	1.139	0.638	23.525	.320
			PRE-BREAK	(SIFTED)			
1 M	1194	40.88	40.88	.266	10.874	10.874	.266
SIZ	203	6.97	47.85	.291	2.028	12.902	.270
2 M	221	7.58	55.43	.297	2.251	15.154	.273
3 BK	80	2.74	58.17	.357	0.978	16.132	.277
2 BK	91	3.13	61.30	.374	1.171	17.302	.282
3 M	80	2.73	64.03	.389	1.062	18.364	.287
1 BK	115	3.94	67.97	.410	1.615	19.980	. 294
4 BK	37	1.26	69.23	.431	0.543	20.523	.296
1 TA	11	0.38	69.61	.533	0.203	20.725	.298
5 BK	40	1.36	70.97	.601	0.817	21.543	.304
P.BK	5	0.18	71.15	.607	0.109	21.652	.304
4 M	47	1.60	72.75	.646	1.034	22.686	.312
5 M	16	0.55	73.30	1.319	0.725	23.411	.319



milling. The use of the Pre-Break sifter is also favored due to the slightly lower ash curve produced.

Both tests using the Pre-Break also gave slightly higher average flour extractions. Improvements of .3% to .4% were realized.

(5) Miag Multomat Mill.

Flour stream data and cumulative ash calculations are listed in

Table 6 and the resulting cumulative ash curves are shown by Figure 11 for
the averaged results of the millings on the Miag Multomat. Flour streams
analyzed were as follows:

First Break	(1 BK)	Second Midds	(2 M)
Second Break	(2 BK)	First Midds Redust	(1 M RED)
Third Break	(3 BK)	Third Midds	(3 M)
Grader		Fourth Midds	(4 M)
First Midds	(1 M)	Fifth Midds	(5 M)

Although some improvement with the use of the Pre-Break is noticed, it does not appear as significant as in previous tests. Since this mill can be considered as relatively short on break roll surface, it would seem that the use of Pre-Break would be of great assistance in improving the flour milling performance. As indicated by the data, improvement was only slight and specific reasons for this are not known.

The actual Pre-Breaking operation, as discussed earlier, was performed on a slightly different roller mill than on the other test millings. This being a pair of 6" x 3" rolls running at a 1.5:1 differential versus 9" x 6" rolls running at a 1:1 differential. Although there is a slight difference between methods, it would not seem to be critical enough to significantly affect the results.

Feed rates for experimental mills is a critical factor in the correct operation and performance of the mills. In previous testing using the Miag Multomat, feed rates of 750 to 780 grams per minute were normally

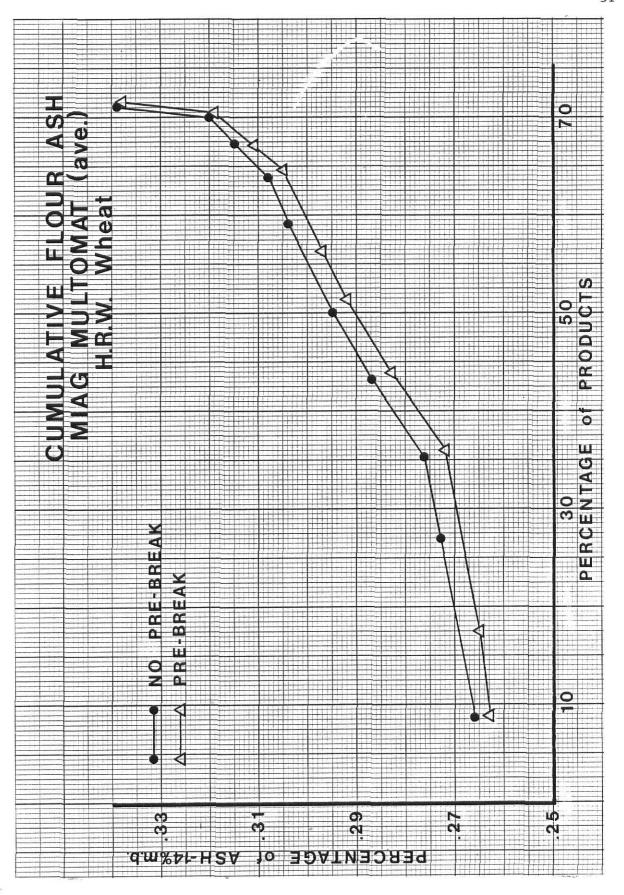
Table 6

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL MIAG MULTOMAT
TEST AVERAGE
WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QXA
			NO PRI	E-BREAK			
1 M RED	2803	8.65	8.65	.266	2.301	2.301	.266
2 M	5900	18.19	26.84	.277	5.039	7.340	.273
1 M	2769	8.52	35.36	.284	2.420	9.760	.276
1 BK	2509	7.78	43.14	.336	2.614	12.374	.287
2 BK	2219	6.88	50.02	.347	2.387	14.761	.295
3 M	2952	9.14	59.16	.353	3.226	17.987	.304
GRADER	1504	4.74	63.90	.356	1.687	19.674	.308
4 M	1124	3.50	67.40	.442	1.547	21.221	.315
3 BK	831	2.56	69.96	.464	1.188	22.409	.320
5 M	351	1.10	71.06	1.503	1.653	24.062	.339
W DED	2007	0.70	PRE-E		T 0 010	1 0 010	0.00
M RED	3007	8.79	8.79	.263	2.312	2.312	.263
1 M	2941	8.61	17.40	.267	2.299	4.611	.265
2 M	6378	18.65	36.05	.278	5.185	9.796	.272
1 BK	2673	7.80	43.85	.333	2.597	12.393	.283
2 BK	2547	7.45	51.30	.348	2.593	14.986	.292
RADER	1670	4.88	56.18	.349	1.703	16.689	.297
3 M	2888	8,45	64.63	.361	3.050	19.739	.305
3 BK	861	2,52	67.15	.452	1.139	20,878	.311
4 M	1127	3,29	70.44	.484	1.592	22,470	.319
5 M	333	0.97	71.41	1.720	1.668	24,138	.338
							MIND
- Van de la company							
						· · · · · · · · · · · · · · · · · · ·	
···							
			II:				
							den a ser de la catalità de la



igure 11

used and found to give adequate results and comfortable operating conditions. Since this particular mill flow has a relatively short Break System and a relatively long Reduction System, at the feed rates the mill is normally operated at, the tail of the mill was somewhat underloaded. By using the Pre-Break, this underloaded condition may have worsened, thereby causing bare-bolting in the sifting operation and in turn causing higher ash-flour streams.

If the data in Table 6 is further analyzed, it can be shown that this underloaded condition was further aggravated by the use of Pre-Break. By accumulating only the Break flours (1st Break, 2nd Break, Grader and 3rd Break), 21.96% flour at .359% ash was produced by the test milling not using Pre-Break versus 22.65% flour at .355% ash milling with the Pre-Break. A gain of about .7% is realized with the Pre-Break at approximately the same ash. Again, by only accumulating the Primary Middlings flours (1st Midds, 2nd Midds, 1st Midd. Redust) it is seen that 35.36% flour at .276% ash is produced by the "No Pre-Break" System versus 36.05% flour at .272% ash produced with Pre-Break. This results in a .7% gain in flour, using Pre-Break at essentially the same cumulated ash content. The remainder, secondary middlings flour, when accumulated gives a resultant flour of 13.74% at .468% ash for the system without Pre-Break versus 12.71% at .496% ash produced by the system using Pre-Break. Approximately 1% more flour was produced by the mill without the Pre-Break and at a lower ash.

From this analysis, it is therefore possible that the optimum feed rate was not utilized in these tests for proper analysis of the Pre-Break. Since more break flour and primary middling flour was produced with the use of the Pre-Break, the tail end of the mill, or Secondary Middlings, was below proper loading for optimum milling performance.

SUMMARY AND CONCLUSIONS

As previously stated, the purpose of this research was to document the effect of Pre-Breaking kernels of wheat prior to the actual procedure of milling. From the data obtained by test milling, using various experimental mills, it can be concluded that Pre-Breaking results in a positive effect upon milling and flour quality.

The flour miller is continually faced with many goals and problems in trying to achieve these goals. One of the primary goals or objectives that is basic to the milling of wheat is to obtain the highest percentage of flour at the highest quality obtainable from a given lot of wheat. Solutions to meet both of these goals may be difficult.

The results of these tests on Pre-Breaking show that, if properly applied, Pre-Break Systems may aid in providing both flours at lower ash contents and at somewhat higher extractions. In all cases, with the exception of the tests using the Miag Multomat, flour ash contents were significantly lowered while slight increases in total flour extractions were also realized, when the wheat was Pre-Broken prior to milling. Tests on the Miag Multomat using Pre-Break also produced flour of lower ash contents than when not using Pre-Break, but differences were not as great. This, as mentioned before, may have been due to problems of the feed rate of wheat to the mill.

The results also indicated that sifting of the Pre-Broken wheat before milling was also beneficial. Flours obtained from test millings where the Pre-Broken stock was sifted before milling were found to be slightly lower in ash than when Pre-Break was used without sifting.

Although not based on scientific fact, several reasons may be theorized as to why Pre-Breaking produces positive effects on milling performance.

- 1. As can be seen in that data, milling with a Pre-Break produced higher percentages of primary break flours at lower ash contents. This could be due to the better presentation of the wheat to the corrugated break rolls in particular the first and second break rolls. Normally, the First Breaking operation must both open up the wheat berry and scrape some portions of the endosperm from the bran. The design of the corrugations and differentials of the rolls lend themselves to doing a better job of the latter. Therefore if, as when using the Pre-Break, the kernel is partially opened and somewhat flattened out before the First Break, the First Break rolls may provide better grinding action with less severity of grind, resulting in less bran contamination. Besides producing lower ash flour on the Breaks, Sizings and Middlings stock lower in ash is also being produced.
- 2. Although not as yet researched, one may theorize that the wheat berries being exposed to the shock of compression by the Pre-Break rolls may develop stresses along the area where the endosperm adheres to the bran. This would allow for the easier removal of the endosperm by the subsequent Break rolls.
- 3. The grinding of the wheat germ, since it is relatively high in ash content, can increase the ash content of the flour being produced. It was observed that, when milling with the Pre-Break, more wheat germ was being released into the Sizings fraction. Once in the Sizings System, there is better chance for recovery and less chance for the grinding of the germ into flour.
- 4. Where the Pre-Broken wheat was sifted before milling, slightly lower flour ashes were also noted than when it was not sifted. This may be due to the removal, by the sifter, of any foreign material lodged in the crease of the wheat berry that was not removed in the cleaning process.

SUGGESTIONS FOR FUTURE WORK

Since this work dealt mainly with documenting the effects of Pre-Breaking, the theories as to why the use of a Pre-Break result in improved milling performance need to be substantiated. Work along these lines should be, if possible, scaled up to a larger, commercial-type mill.

Complete stream analysis on a large scale mill could be very revealing.

To determine if pre-breaking may loosen the bonds between the bran and the endosperm, studies using the Scanning Electron Microscope may be useful.

More work should also be done to better determine the method of Pre-Breaking which provides the optimum improvement in milling performance. In this study, only smooth rolls at very low differentials were utilized. Would corrugated rolls or a combination of a corrugated and a smooth roll provide better splitting action? Is a one to one differential the optimum differential to use?

Determining the severity of Pre-Breaking to give optimum performance is also needed. If slightly opening the wheat berry at the crease presents the stock better to the Break rolls, would smashing the kernel under high compression make an even better presentation to the Break rolls?

Although not fully tested in this work, there is some evidence that by using a Pre-Break, power consumption may be lowered for the subsequent grinding operations. If it was determined that by the use of Pre-Break system both total power consumption was lowered and milling performance was improved, the milling industry would surely benefit.

LITERATURE CITED

- 1. Kozmin, P. A. (1921) Flour Milling. London, England: George Routledge and Sons, Ltd. (Translated from Russian), 489.
- 2. Smith, L. (1944) Flour Milling Technology. Liverpool, England: The Northern Publishing Co., Ltd., 180.
- 3. "Splitting the Wheat in the Crease (A Round Table Discussion)," (1929) National Miller (June), 20.
- 4. Reed, H. J. (1929) "Wheat Splitting," <u>National Miller</u> (August), 28-29.
- 5. Farrell, E. P., and M. Milner. (1952) "Insect Fragment Problem in the Milling Industry," Kansas State College of Agriculture and Applied Science, Agriculture Experiment Station, Circular 291.
- 6. Zerull, L. (1965) "Pre-Milling Control," Association of Operative Millers Bulletin (May), 2860.
- 7. Wingfield, J., E. Gladow, and R. Reid. (1978) "Flow Sheet Review--A Project by the A.O.M. Technical Committee," Association of Operative Millers Technical Bulletin (August), 3732-3736.
- 8. Anderson, J. E. (1938) "Comparison of Experimental and Commercial Milling Results," Northwestern Miller (August), 46-53.
- 9. Miller, E. S. (1937-1943) "The Purpose of Experimental Milling," Association of Operative Millers Technical Bulletin, 2:75-78.
- 10. Rumold, P. (1942) "Interpreting Experimental Milling Data from a Commercial Aspect," Cereal Chemistry, 19:384-388.
- 11. Herman, R. S. (1927) "Value of Experimental Milling Test," <u>Cereal Chemistry</u>, 4:270-274.
- 12. Zeleny, L., and Y. Pomeranz, ed. (1964) "Criteria of Wheat Quality,"

 Wheat: Chemistry and Technology. St. Paul, The American Association of Cereal Chemists, Inc.
- 13. Swanson, C. O. (1932) "Is There Any Relief from Ash," Association of Operative Millers Technical Bulletin (April), 417-420.
- 14. Robbins, D. (1938-1943) "Ash Distribution in Flour Mill Stocks,"
 Association of Operative Millers Technical Bulletin, 2:247-251.
- 15. MacMasters, M. M., and Y. Pomeranz, ed. (1964) "Microscopic Structure and Composition of the Wheat Kernel," Wheat:

 Chemistry and Technology. St. Paul: The American Association of Cereal Chemists, Inc.

- 16. Morris, V. H., T. L. Alexander, and E. D. Pascoe. (1945) "Studies of the Composition of the Wheat Kernel. I. Distribution of Ash and Protein in Center Sections," Cereal Chemistry, 22:351-361.
- 17. Clark, R. J. (1926-1937) "The Tin God Ash," Association of Operative Millers Technical Bulletin, 1:407-409.
- 18. Shuey, W. C. (1961) "Measuring the Commercial Milling Value of Wheat," Association of Operative Millers Technical Bulletin (August), 2597-2600.
- 19. Wissmar, K. (1960) "Analytical Methods to Control Mill Efficiency,"

 <u>Association of Operative Millers Technical Bulletin</u> (August),

 2521-2523.

LIST OF PLATES

Plat	e Number			Page
1.	Flowsheet of German Short Flow Using Pre-Break	• •		6
2.	Flowsheet of a German Abridged High Grinding Flow Using Pre-Break			8
3.	Photograph of Whole Wheat Kernels vs. Pre-Broken Wheat	ě .		15
4.	Photograph of Pre-Break Flour vs. Straight Grade Flour	٠,		15
5.	Photograph of Brabender Quadrumat Junior	· ·	ı •	22
6.	Photograph of Brabender Quadrumat Senior	• •		22
7.	Photograph of Buhler Experimental Mill			29
8.	Photograph of Ross Millstands			29
9.	Photograph of Miag Multomat Mill			36
10.	Photograph of Miag Pre-Break Rolls			36
	LIST OF TABLES			
Table	e Number			Page
1.	Physical Wheat Data for Test Wheat			17
2.	Cumulative Flour Ash Calculations for Quadrumat Junior Test Averages			39
3.	Cumulative Flour Ash Calculations for Quadrumat Senior Test Averages			42
4.	Cumulative Flour Ash Calculations for Buhler Experimental Mill Test Averages			44
5.	Cumulative Flour Ash Calculations for Ross Walking Flour Test Averages			47
6.	Cumulative Flour Ash Calculations for Miag Multomat Test Averages			50

LIST OF FIGURES

Figu	re Number	Page
1.	Flowsheet of K.S.U. Wheat Cleaning House	. 18
2.	Flowsheet of Brabender Quadrumat Junior Tests	. 20
3.	Flowsheet of Brabender Quadrumat Senior Tests	. 23
4.	Flowsheet of Buhler Experimental Mill Tests	. 27
5.	Flowsheet of K.S.U. Ross Walking Flow	. 30
6.	Flowsheet of Miag Multomat Experimental Mill	. 34
7.	Cumulative Flour Ash Curves for Quadrumat Junior Averaged Tests	. 40
8.	Cumulative Flour Ash Curves for Quadrumat Senior Averaged Tests	. 43
9.	Cumulative Flour Ash Curves for Buhler Experimental Mill Averaged Tests	. 45
10.	Cumulative Flour Ash Curves for Ross Walking Flow Averaged Tests	. 48
11.	Cumulative Flour Ash Curves for Miag Multomat Experimental Mill Averaged Tests	. 51

ACKNOWLEDGMENTS

The writer would like to express his sincere appreciation to

Professor Arlin B. Ward, major professor, Department of Grain Science

and Industry, Kansas State University, for his guidance and support of
this research and especially for his dedication to the Milling Industry.

Appreciation would also like to be extended to Professor Emeritus

Eugene Farrell, Doctor Dale Eustace and Professor John Wingfield,

Department of Grain Science and Industry, Kansas State University, for
their continued assistance and sharing of ideas during this study.

The writer would especially like to express his deep gratitude to his wife, family and friends for their support, encouragement and patience.

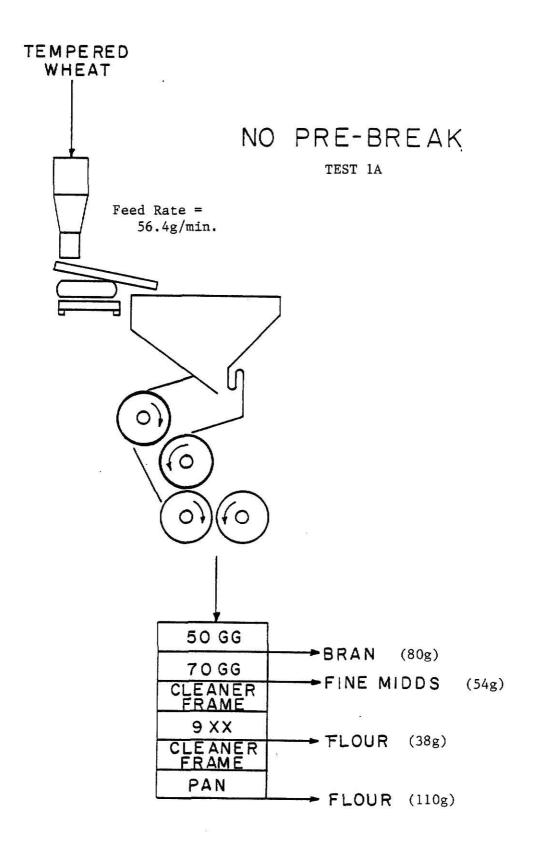
APPENDIX A

APPENDIX A

Appendix A contains all data from the individual tests on each experimental mill. Flowsheets of each mill are given with the stream weights entered for both flour and feed, and in the case of the Ross Walking Flow, all stream weights are given. Cumulative flour ash calculations and the resulting cumulative ash curves for each test are also shown.

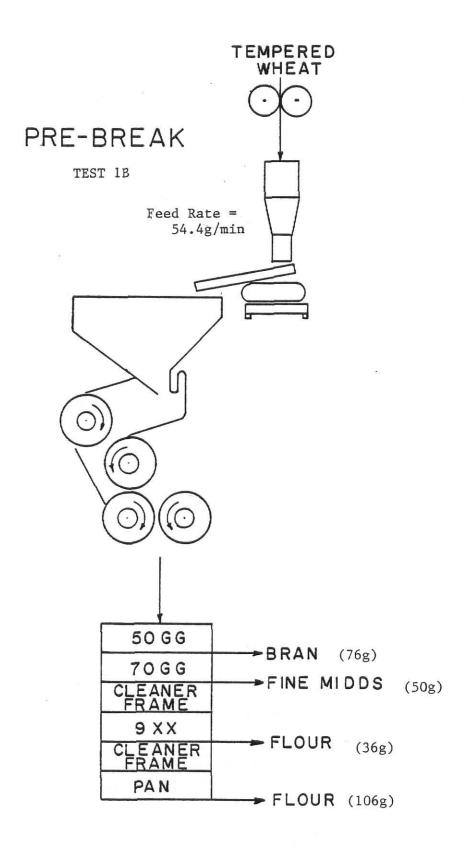
LIST OF FIGURES IN APPENDIX A

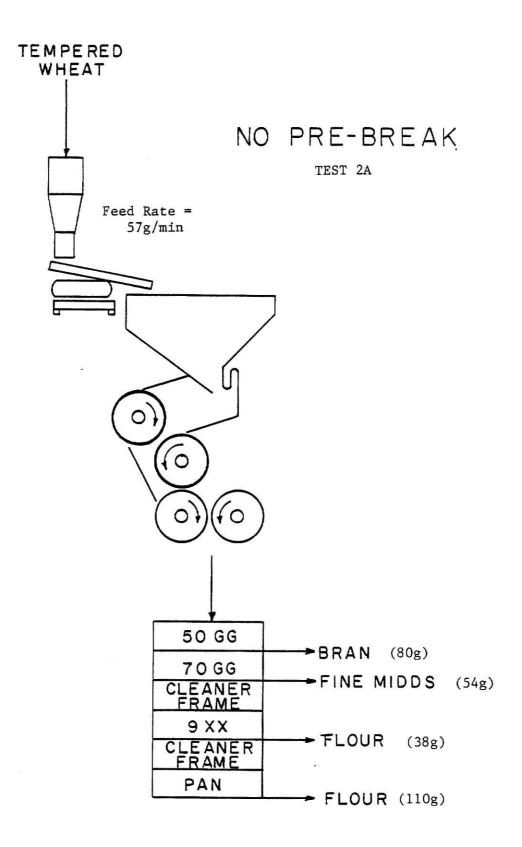
Figure	Number	Page
12-21	Flowsheets (with stream weights) for Quadrumat Junior, Tests 1 through 5	64-73
22-26	Cumulative Flour Ash Curves for Quadrumat Junior, Tests 1 through 5	75-79
27–36	Flowsheets (with stream weights) for Quadrumat Senior, Tests A through E	80-89
37-41	Cumulative Flour Curves for Quadrumat Senior, Tests A through E	91–95
42-61	Flowsheets (with stream weights) for Buhler Experimental Mill, Tests A through E	96-115
62-66	Cumulative Flour Ash Curves for Buhler Experimental Mill, Tests A through E	121-125
67-81	Flowsheets (with stream weights) for Ross Walking Flow, Tests C through G	126-140
82-86	Cumulative Flour Ash Curves for Ross Walking Flow, Tests C through G	146-150
87–96	Flowsheets (with stream weights) for Miag Multomat, Tests A through E	151-160
97–101	Cumulative Flour Ash Curves for Miag Multomat, Tests A through E	166-170
	LIST OF TABLES IN APPENDIX A	
Table :	Number	Page
7	Cumulative Flour Ash Calculations for Quadrumat Junior, Tests 1 through 5	74
8	Cumulative Flour Ash Calculations for Quadrumat Senior, Tests A through E	90
9-13	Cumulative Flour Ash Calculations for Buhler Experimental Mills, Tests A through E	116-120
14-18	Cumulative Flour Ash Calculations for Ross Walking Flow, Tests C through G	141-145
19-23	Cumulative Flour Ash Calculations for Miag Multomat, Tests A through E	161-165



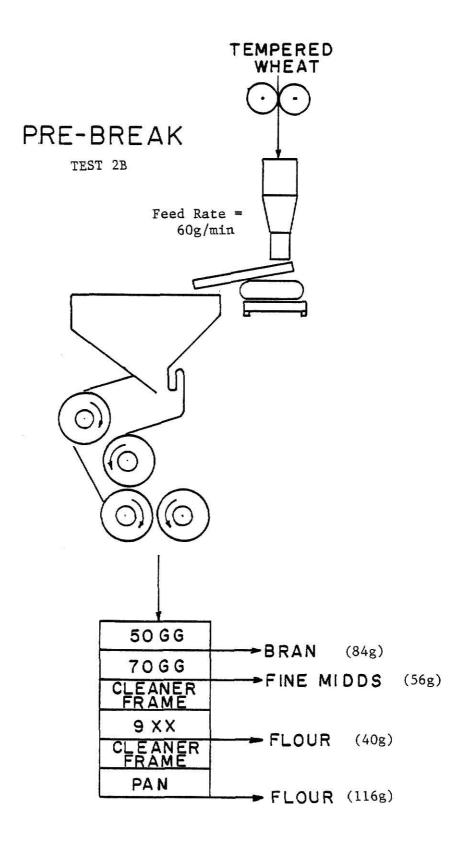
QUADRUMAT JUNIOR

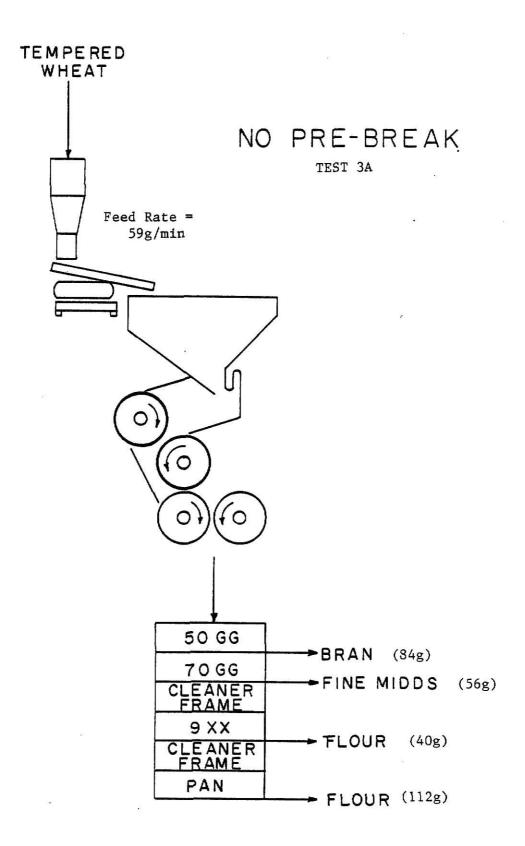
Figure 12



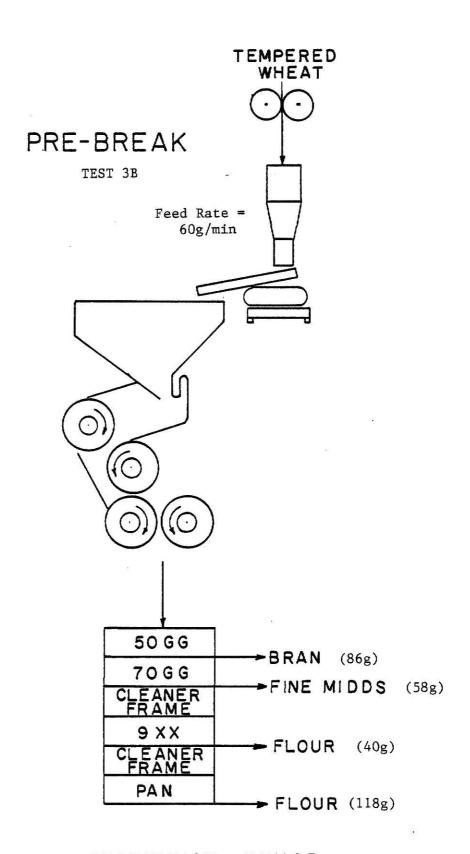


QUADRUMAT JUNIOR

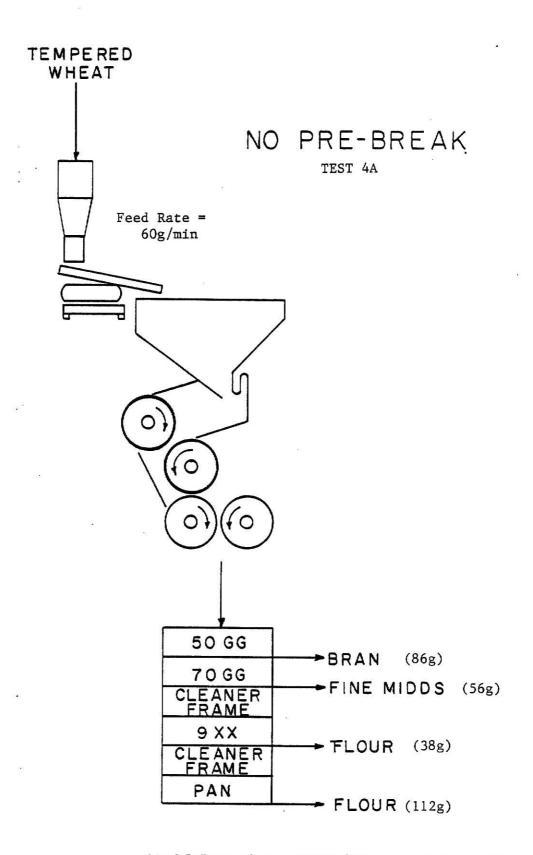


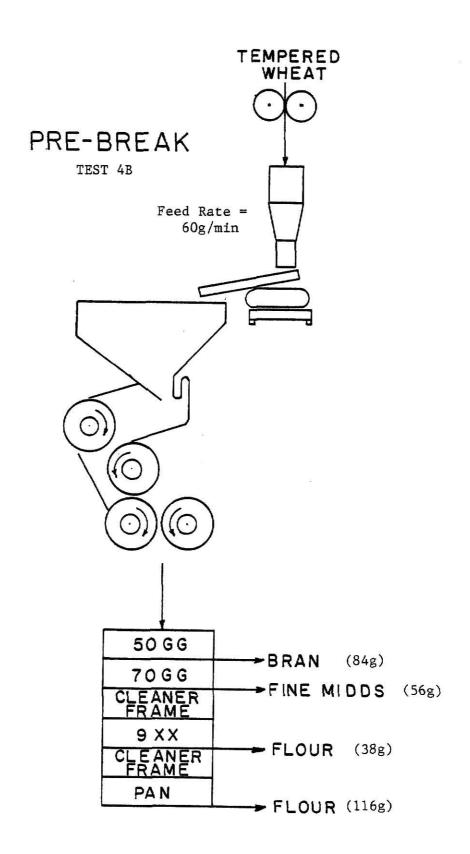


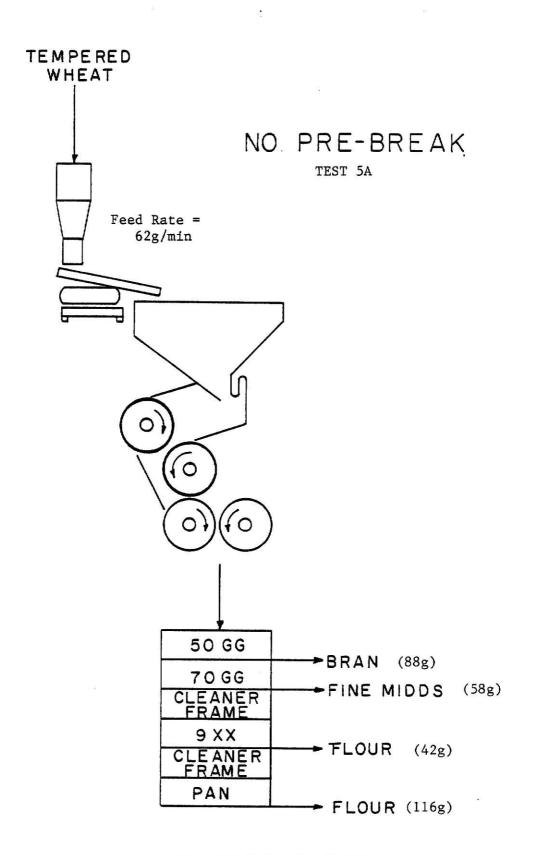
QUADRUMAT JUNIOR



QUADRUMAT JUNIOR







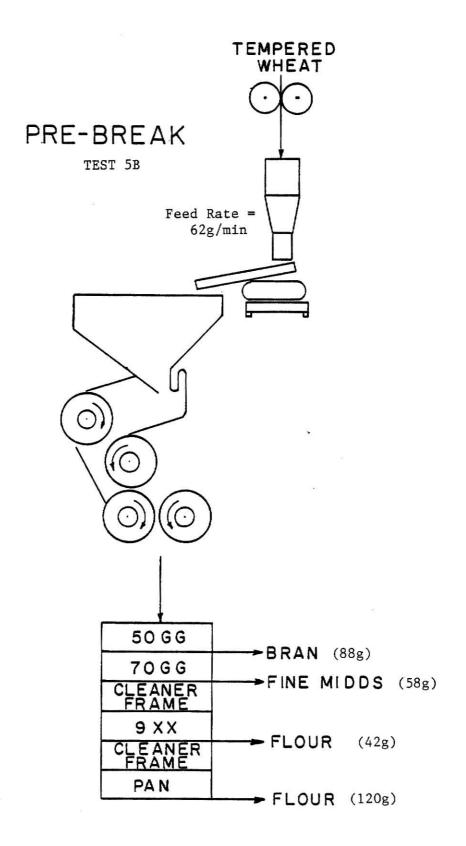


Figure 21

Table 7

Cumulative Flour Ash Calculations

A=ASH(14% Moisture Basis)
Q=QUANTITY(% of Total Products)
S=SUMMATION

MILL QUADRUMAT JUNIOR
TEST A, B, C, D, E
HARD RED WINTER

-9XX +9XX -9XX +9XX +9XX -9XX -9XX +9XX -9XX +9XX	110 38 106 36 38 110 116 40 112 40	39.01 13.48 T1 39.55 13.43 T1 13.48 39.01 T1 39.19 13.51 T1 38.36	39.01 52.49 EST 1B 39.55 52.98 EST 2A NO 13.48 52.49 EST 2B 39.19 52.70 EST 3A NO	PRE-BREA .440 .460 PRE-BREA .408 .427 PRE-BREA .428 .431 PRE-BREA .399 .416	17.16 6.20 K 16.14 5.73 K 5.77 16.81 K 15.64 5.62	17.16 23.36 16.14 21.87 5.77 22.58 15.64 21.26	.440 .445 .408 .413 .428 .430 .399 .403
+9XX -9XX +9XX -9XX -9XX +9XX -9XX -9XX -9XX	38 106 36 38 110 116 40	13.48 39.55 13.43 T1 13.48 39.01 T1 39.19 13.51 T1 38.36	52.49 EST 1B 39.55 52.98 EST 2A NO 13.48 52.49 EST 2B 39.19 52.70 EST 3A NO	.460 PRE-BREA .408 .427 PRE-BREA .428 .431 PRE-BREA .399 .416	6.20 K 16.14 5.73 K 5.77 16.81 K 15.64 5.62	23.36 16.14 21.87 5.77 22.58 15.64	.445 .408 .413 .428 .430
-9XX +9XX +9XX -9XX -9XX +9XX -9XX +9XX	106 36 38 110 116 40	T1 39.55 13.43 T1 13.48 39.01 T1 39.19 13.51	EST 1B 39.55 52.98 EST 2A NO 13.48 52.49 EST 2B 39.19 52.70	PRE-BREA .408 .427 PRE-BREA .428 .431 PRE-BREA .399 .416	K 16.14 5.73 K 5.77 16.81 K 15.64 5.62	16.14 21.87 5.77 22.58	.408 .413 .428 .430
+9XX +9XX -9XX -9XX +9XX -9XX -9XX	38 110 116 40	39.55 13.43 T1 13.48 39.01 T1 39.19 13.51 T1 38.36	39.55 52.98 EST 2A NO 13.48 52.49 EST 2B 39.19 52.70	.408 .427 PRE-BREA .428 .431 PRE-BREA .399 .416	16.14 5.73 K 5.77 16.81 K 15.64 5.62	5.77 22.58 15.64	.413
+9XX +9XX -9XX -9XX +9XX -9XX -9XX	38 110 116 40	13.43 T1 13.48 39.01 T1 39.19 13.51 T1 38.36	52.98 EST 2A NO 13.48 52.49 EST 2B 39.19 52.70 EST 3A NO	.427 PRE-BREA .428 .431 PRE-BREA .399 .416	5.73 K 5.77 16.81 K 15.64 5.62	5.77 22.58 15.64	.413
+9XX -9XX -9XX +9XX -9XX +9XX	38 110 116 40	T1 13.48 39.01 T1 39.19 13.51 T1 38.36	EST 2A NO 13.48 52.49 EST 2B 39.19 52.70 EST 3A NO	PRE-BREA .428 .431 PRE-BREA .399 .416	K 5.77 16.81 K 15.64 5.62	5.77 22.58	.428 .430
-9XX -9XX +9XX -9XX +9XX	110 116 40	13.48 39.01 T1 39.19 13.51	13.48 52.49 EST 2B 39.19 52.70	.428 .431 PRE-BREA .399 .416	5.77 16.81 K 15.64 5.62	22.58	.430
-9XX +9XX +9XX -9XX +9XX	110 116 40	13.48 39.01 T1 39.19 13.51	13.48 52.49 EST 2B 39.19 52.70	.428 .431 PRE-BREA .399 .416	5.77 16.81 K 15.64 5.62	22.58	.430
-9XX -9XX +9XX -9XX +9XX	110 116 40	39.01 39.19 13.51 T1 38.36	52.49 EST 2B 39.19 52.70 EST 3A NO	.431 PRE-BREA .399 .416	16.81 K 15.64 5.62	22.58	.430
-9XX +9XX -9XX +9XX	116 40	39.19 13.51 T1 38.36	EST 2B 39.19 52.70 EST 3A NO	PRE-BREA .399 .416	15.64 5.62	15.64	.399
+9XX -9XX +9XX	112	39.19 13.51 TI 38.36	39.19 52.70 EST 3A NO	.399	15.64		
+9XX -9XX +9XX	112	13.51 T)	52.70 EST 3A NO	.416	5.62		
-9XX +9XX	112	T) 38.36	EST 3A NO			21.20	1,403
+9XX -9XX		38.36		PRE-BREA	77		
+9XX -9XX			1 20 20		K		
+9XX -9XX			38.36	.428	16.42	16.42	.428
		13.70	52.06	.437	5.99	22.41	.430
	NAME AND ADDRESS OF OWNER,	T	EST 3B	PRE-BREA	K		
	118	39.07	39.07	.409	15.98	15.98	.409
+9XX	40	13.25	52.32	.410	5.43	21.41	.409
			TOT /A NO	DDE DDEA			
	110			PRE-BREA		16 /6	.429
-9XX	112	38.36	38.36	.429	16.46	16.46	.432
+9XX	38	13.01	51.37 EST 4B	.439 PRE-BREA	5.71	22.17	.432
+9XX	38	12.93	12.93	.399	5.16	5.16	.399
-9XX	116	39.46	52.39	.407	16.06	21.22	.405
- 7KK	110	33.40	32.33				
				PRE-BREA			
-9XX	116	38.16	38.16	.419	15.99	15.99	.419
+9XX	42	13.82	51.98	.436	6.03	22.02	.424
	verbroom to the second		EST 5B	PRE-BREA		15.55	1 000
-9XX	120	38.96	38.96	.388	15.12	15.12	.388
+9XX	42	13.64	52.60	.388	5.29	20.41	.388

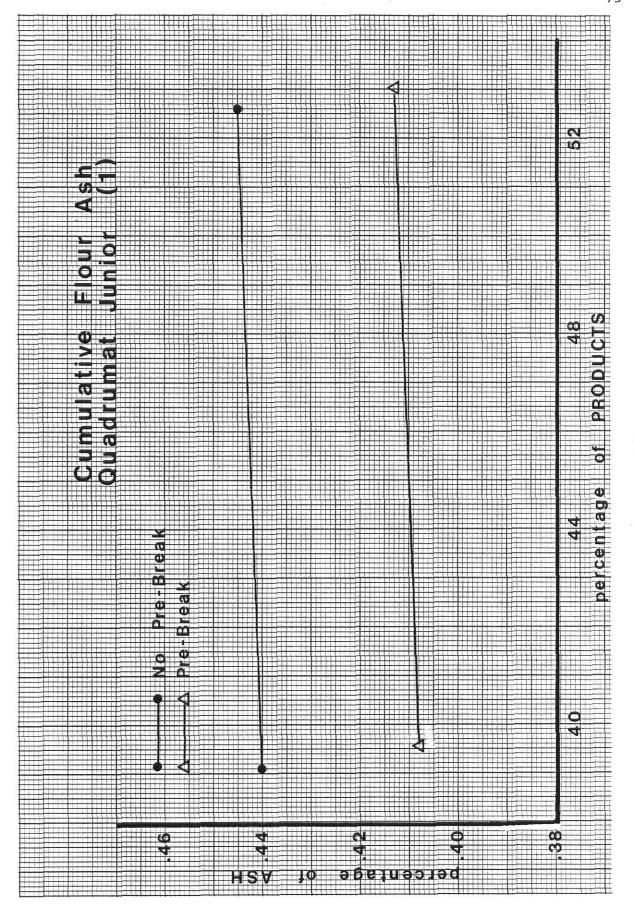


Figure 22

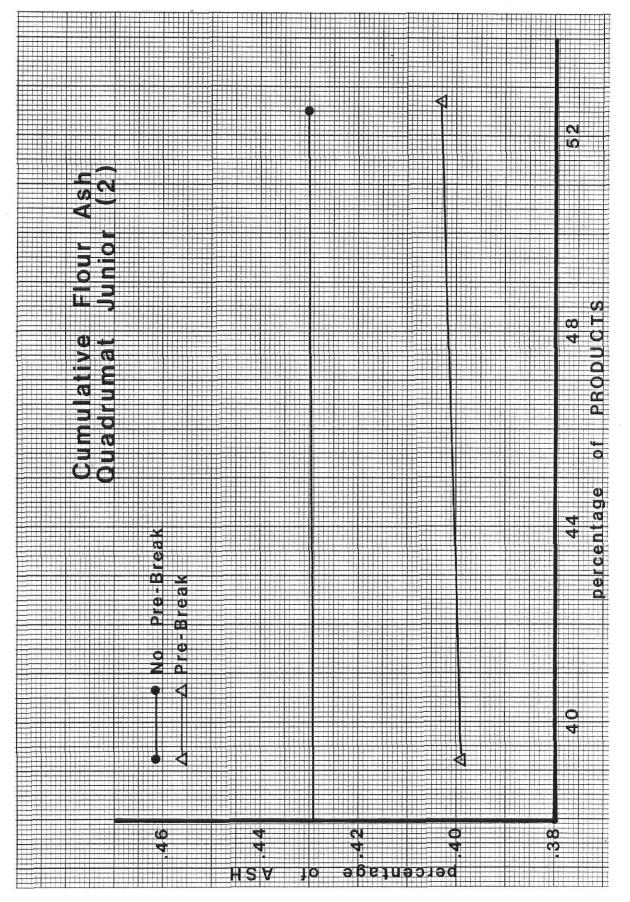


Figure 23

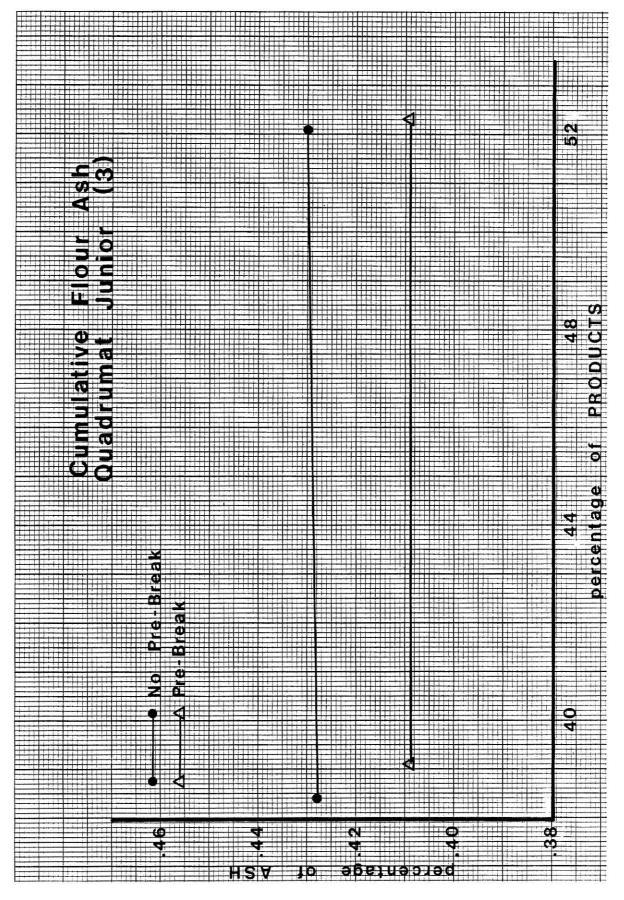


Figure 24

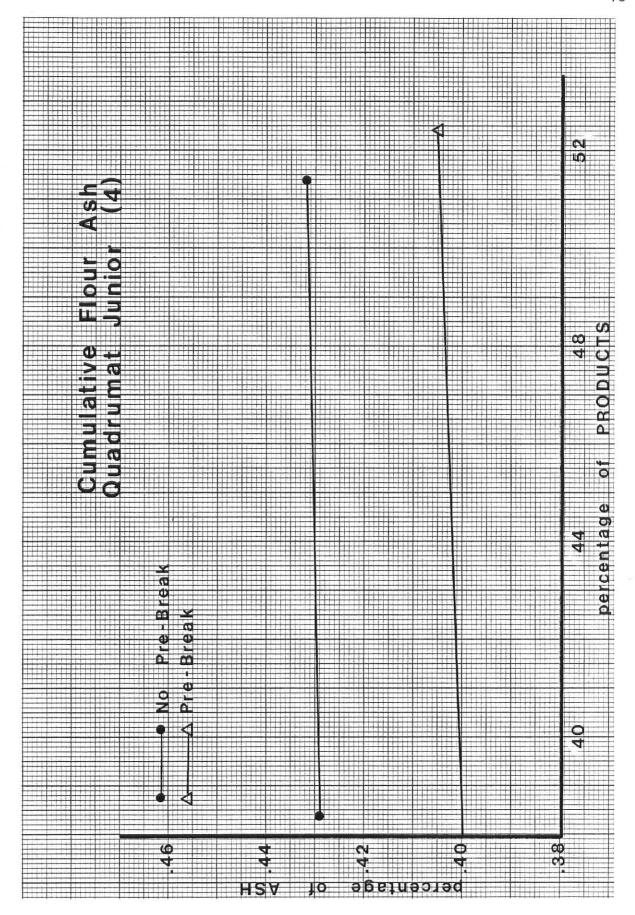
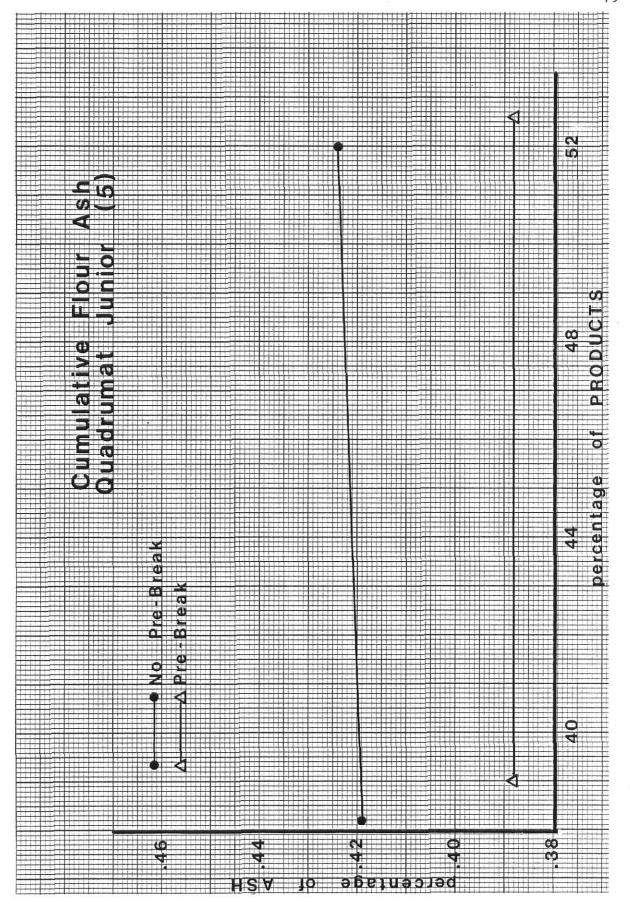
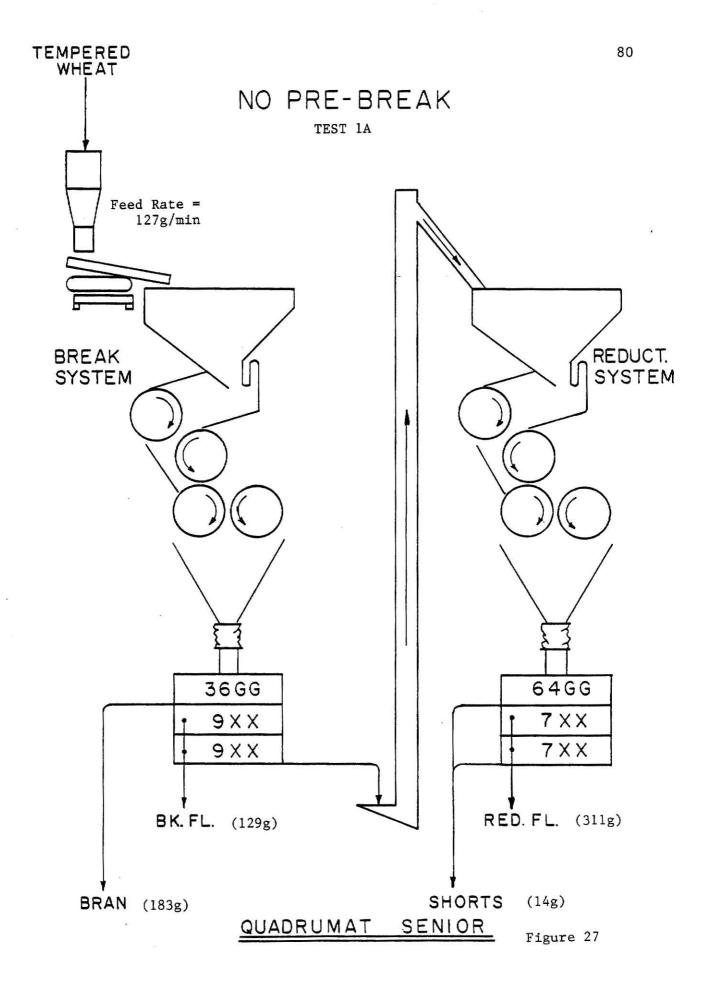


Figure 25





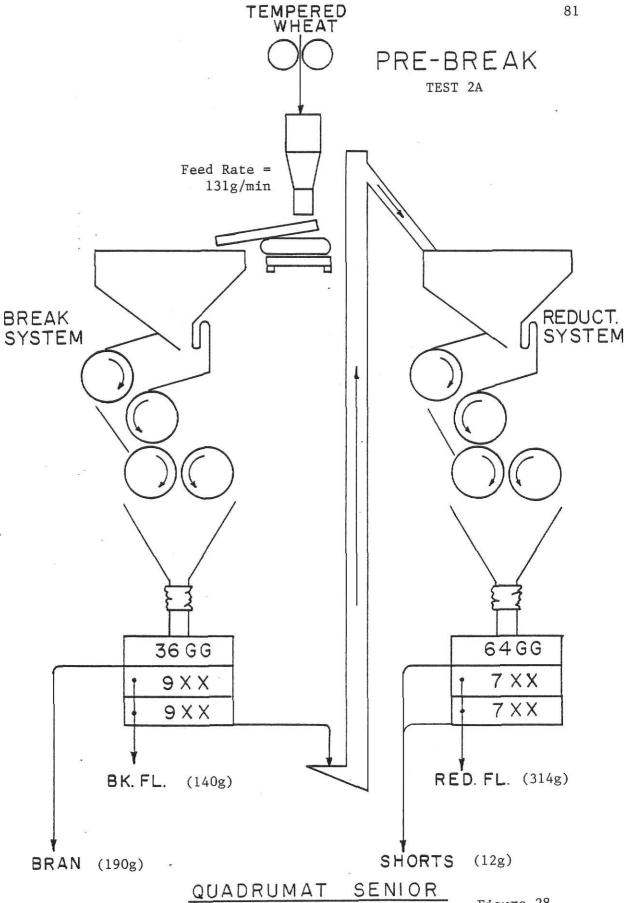
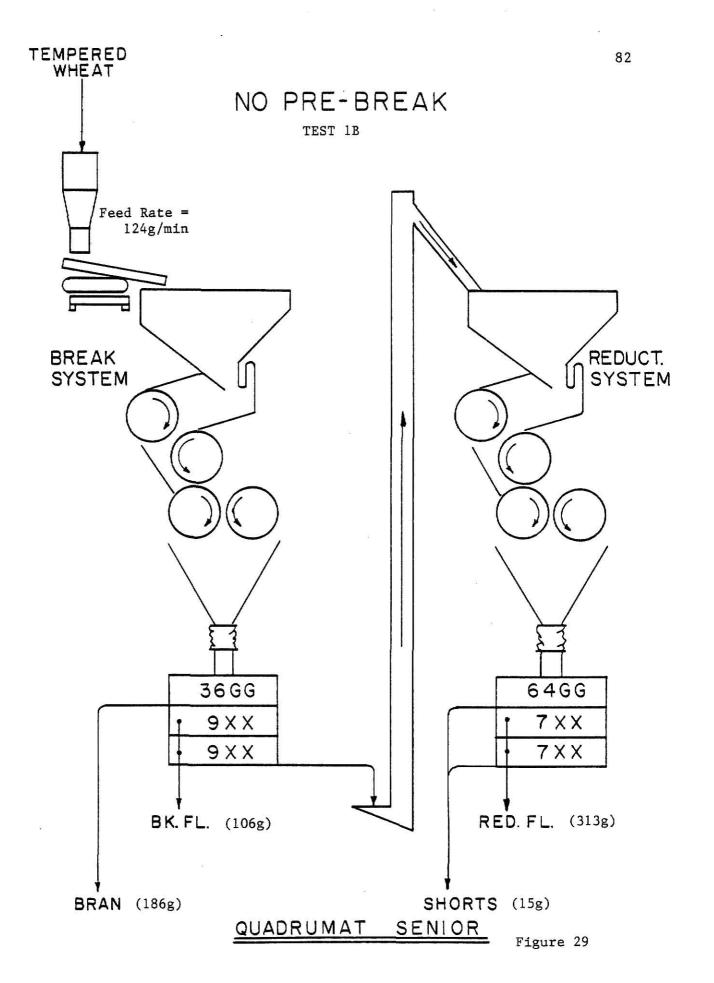
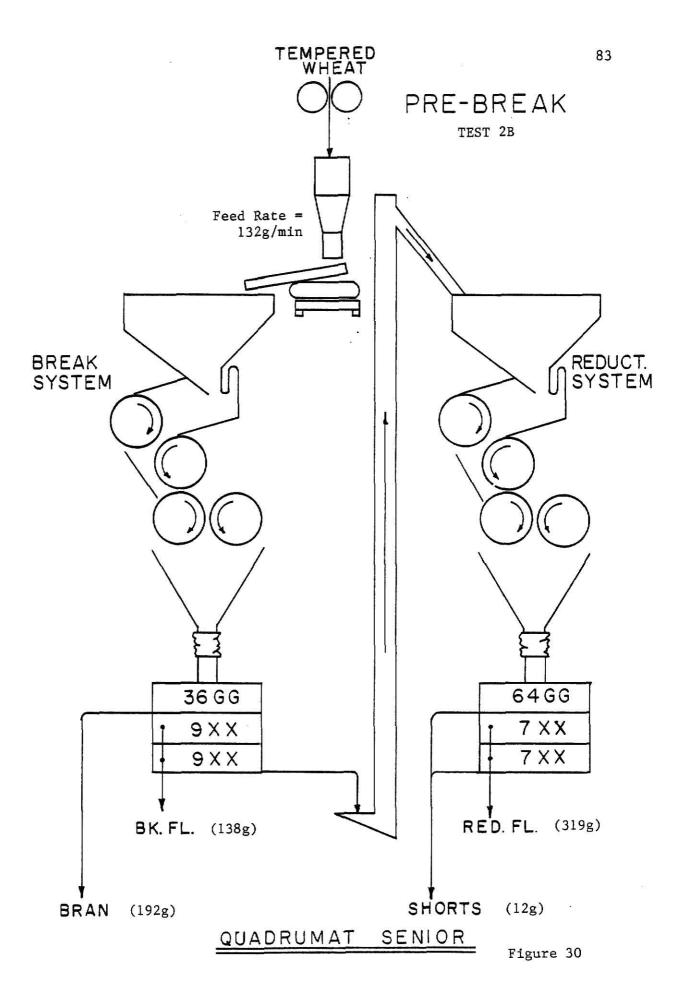
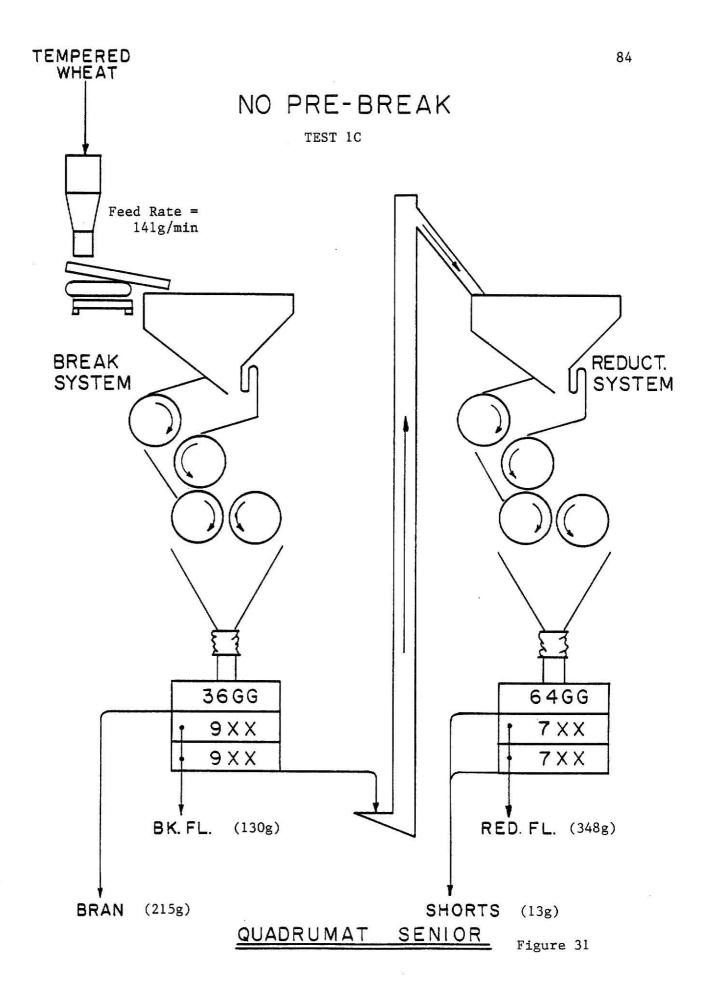
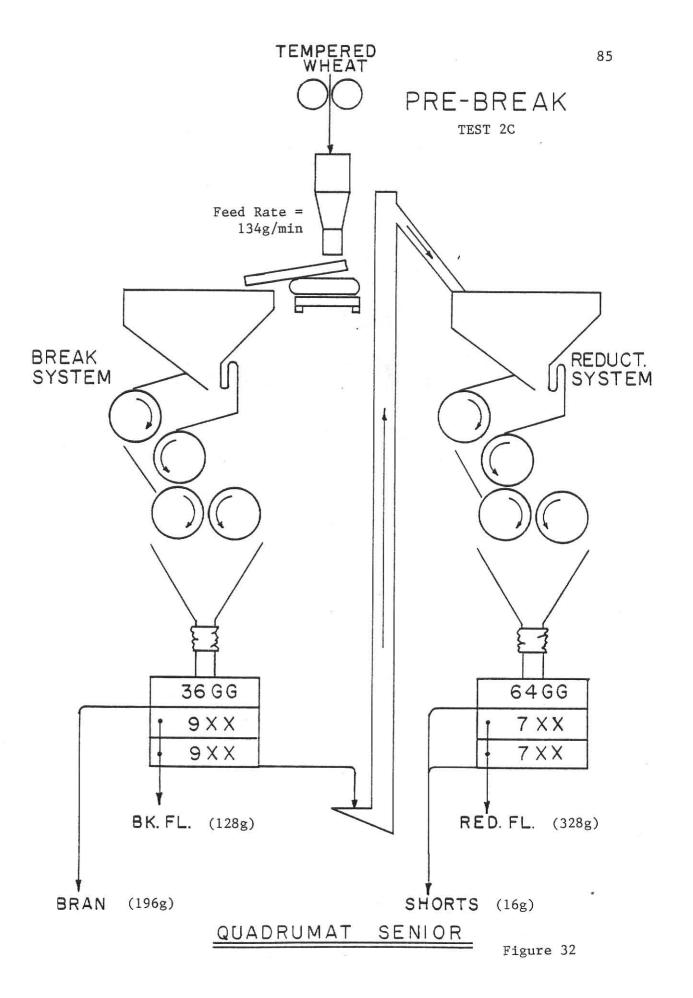


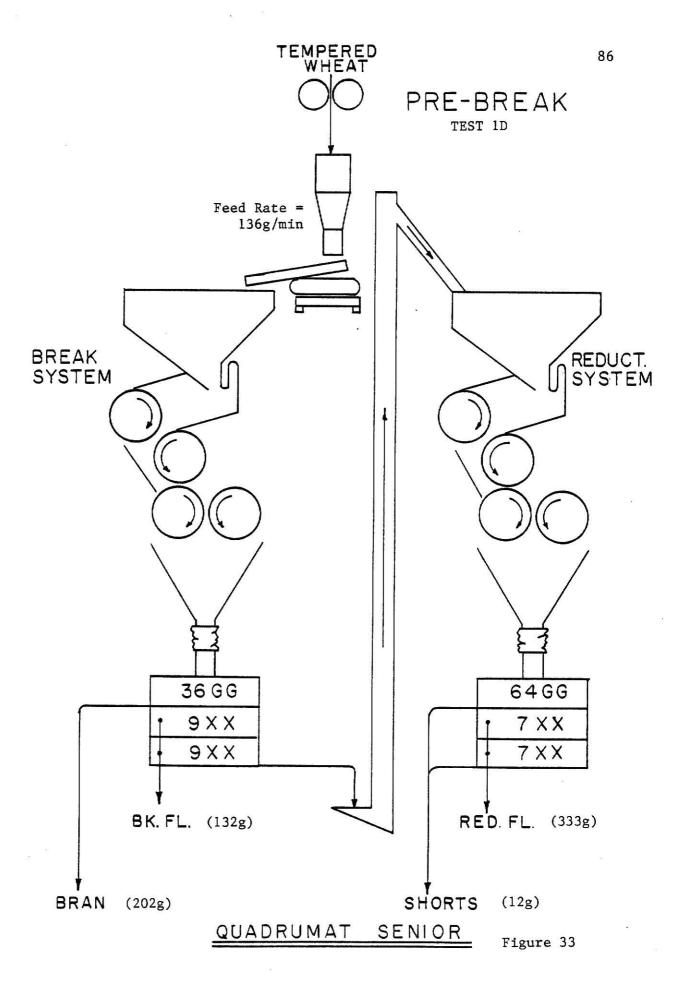
Figure 28

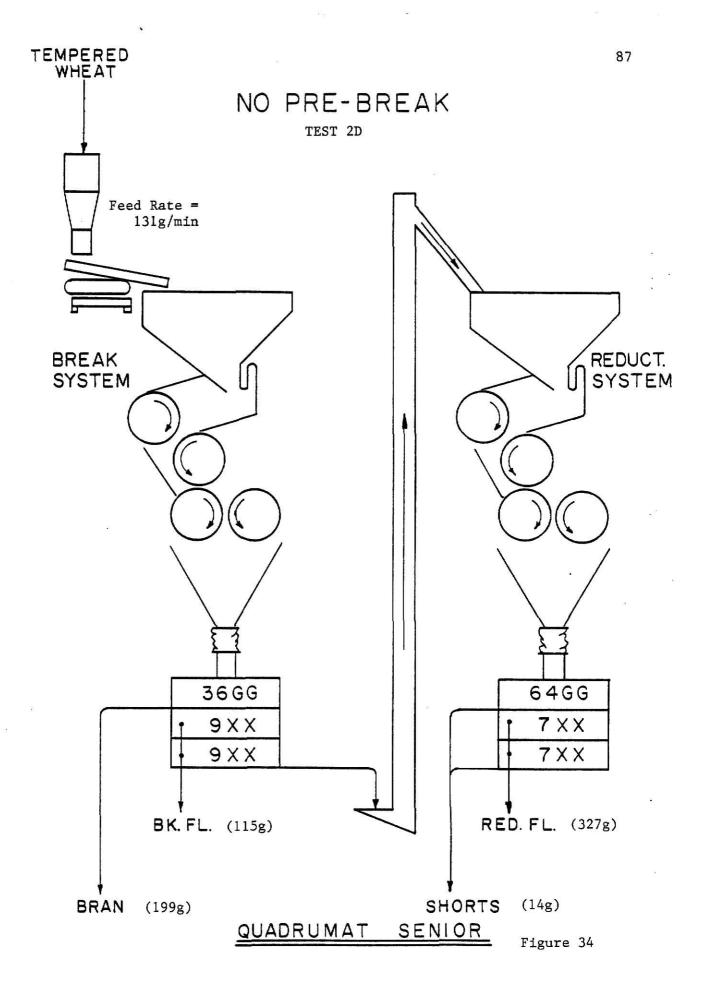


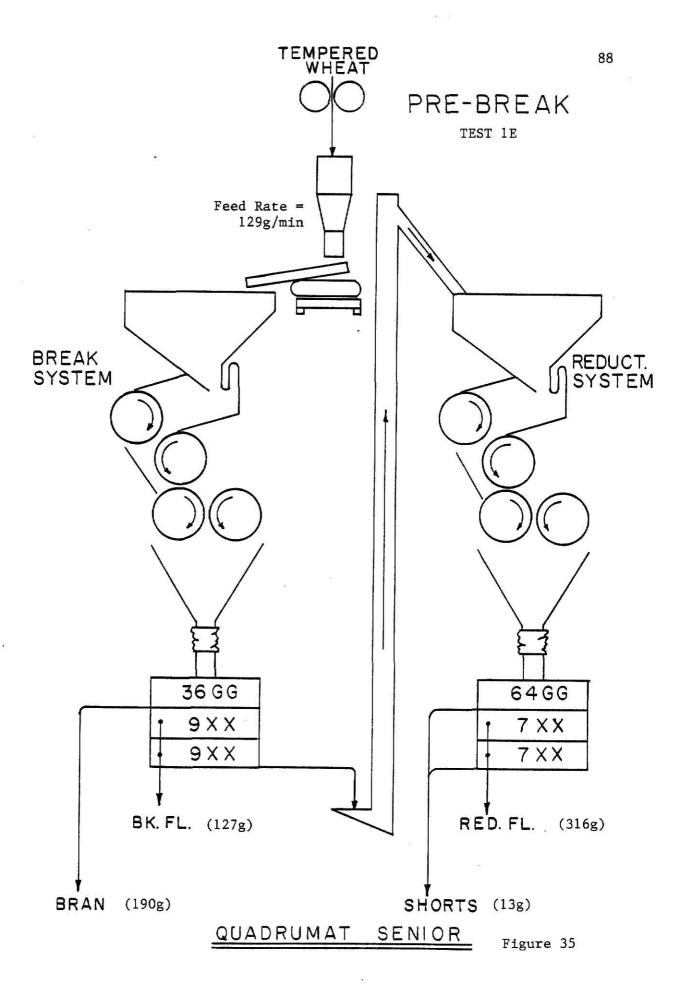


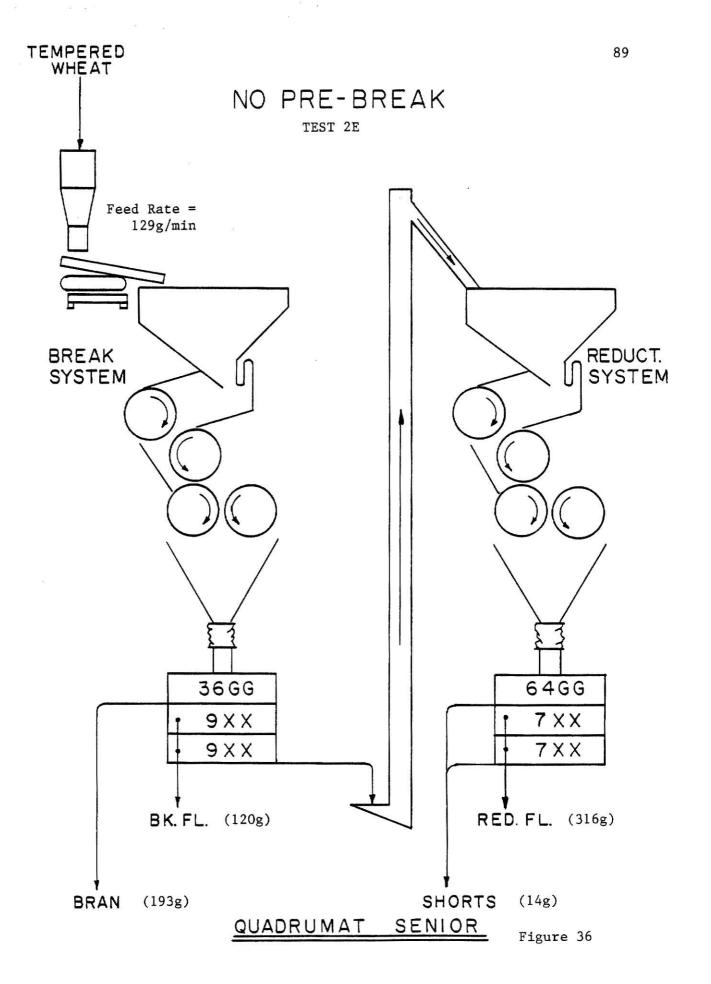












Cumulative Flour Ash Calculations

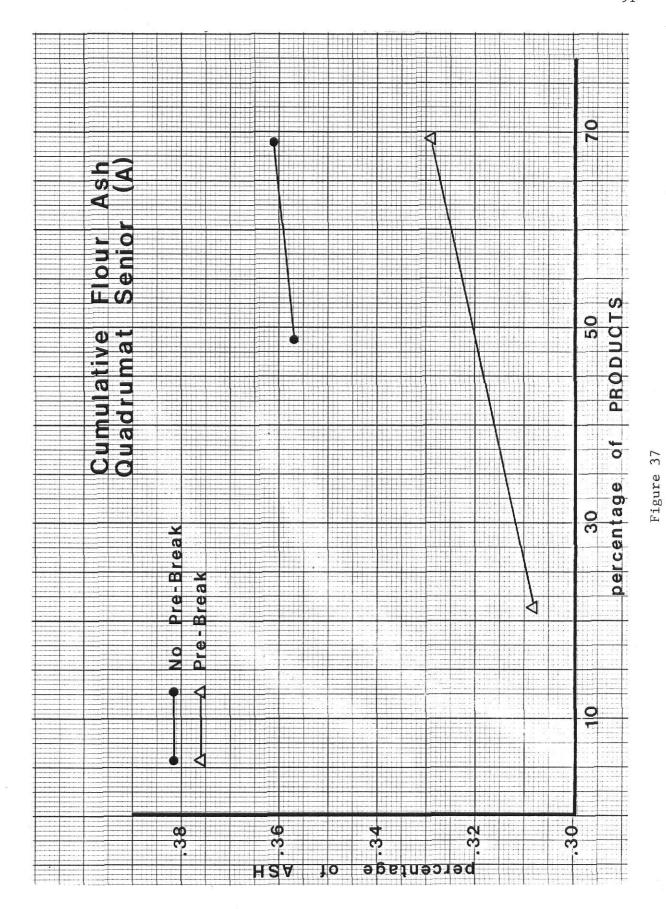
A=ASH (14% Moisture Basis)

Q=QUANTITY (% of Total Products)

S = SUMMATION

MILL QUADRUMAT SENIOR
TEST A, B, C, D, E
WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	А	QXA	S of QXA	S of QXA
		T	EST 1A NO	PRE-BRE	AK		
RED FL	311	48.82	48.82	.357	17.429	17.429	.357
BK FL	129	20.25	69.07	.369	7.472	24.901	.361
		T	EST 2A	PRE-BRE	AK		
BK FL	140	21.34	21.34	.308	6.573	6.573	.308
RED FL	314	47.87	69.21	.337	16.132	22.705	.325
		THE RESIDENCE OF THE PARTY OF T		PRE-BRE		-	
BK FL	106	17.10	17.10	.318	5.438	5.438	.318
RED FL	313	50.48	67.58	.328	16.557	21.995	.325
			EST 2B	PRE-BRE		_	
BK FL	138	20.88	20.88	.308	6.431	6.431	.308
RED FL	319	48.26	69.14	,328	15.829	22.260	.322
			ECM 1C	DDE DDE	A TZ		
D	100		EST 1C	PRE-BRE		1 5 670	200
BK FL	130	18.41	18.41	.308	5.670	5.670	.308
RED FL	348	49.29	67.70 EST 2C NO	.336 PRE-BRE	16.561	22.231	.328
BK FL	128	19.16	19.16	.329	6.304	6.304	.329
RED FL	328	49.10	68.26	.348	17.087	23.391	.343
	323	15115	1 00.20		12,1007		.313
		T	EST 1D	PRE-BRE	AK	· · · · · · · · · · · · · · · · · · ·	
RED FL	333	49.04	49.04	.318	15.595	15.595	.318
BK FL	132	19.44	68.58	.319	6.201	21.796	.318
		T	EST 2D NO	PRE-BRE	AK		
BK FL	115	17.56	17.56	.327	5.742	5.742	.327
RED FL	327	49.92	67.48	.335	16.723	22.465	.333
DIZ ET	107		EST 1E	PRE-BRE	AK 6.232	()))	1 217
BK FL	127	19.66	19.66	.317		6.232	.317
RED FL	316	48.92	68.58	.338	16.535	22.858	.333
				PRE-BRE	THE RESERVE OF THE PERSON NAMED IN	+ ,	
BK FL	120	18.66	18.66	.330	6.158	6.158	.330
RED FL	316	49.14	67.80	.349	17.150	23.308	.344



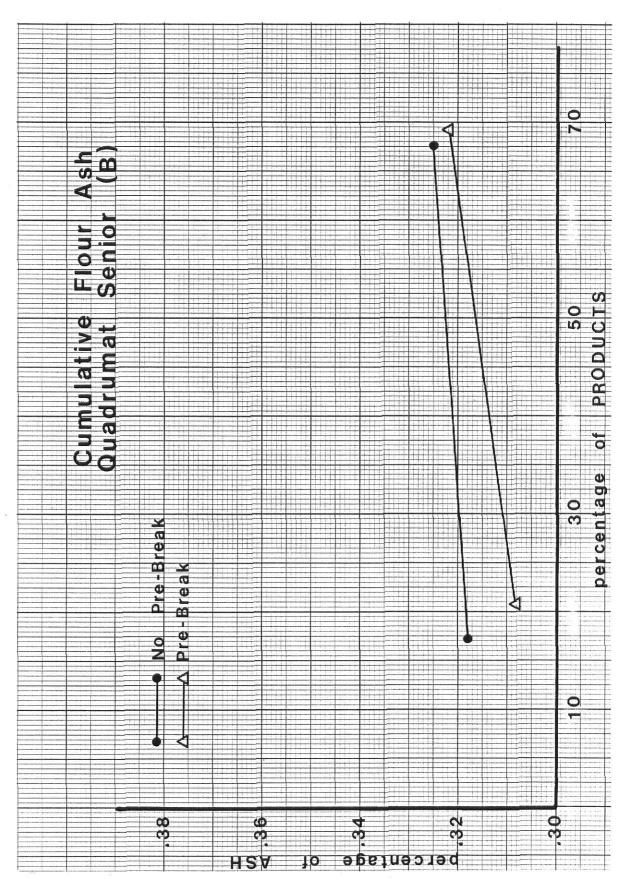


Figure 38

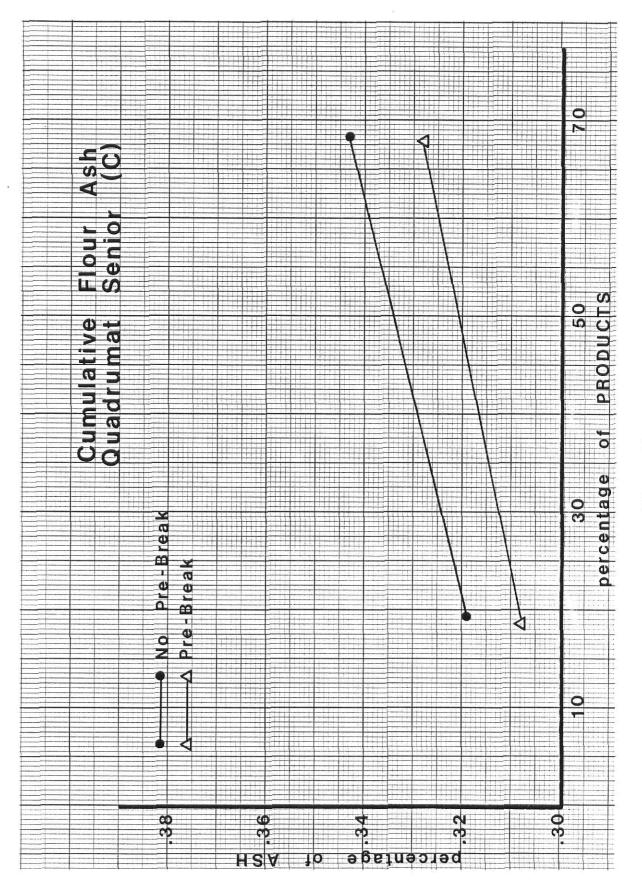


Figure 39

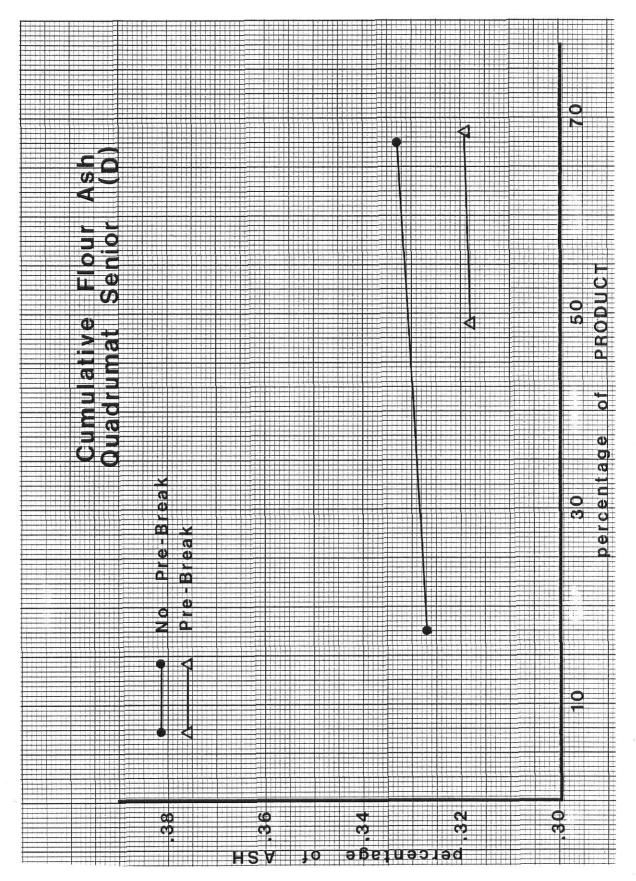


Figure 40

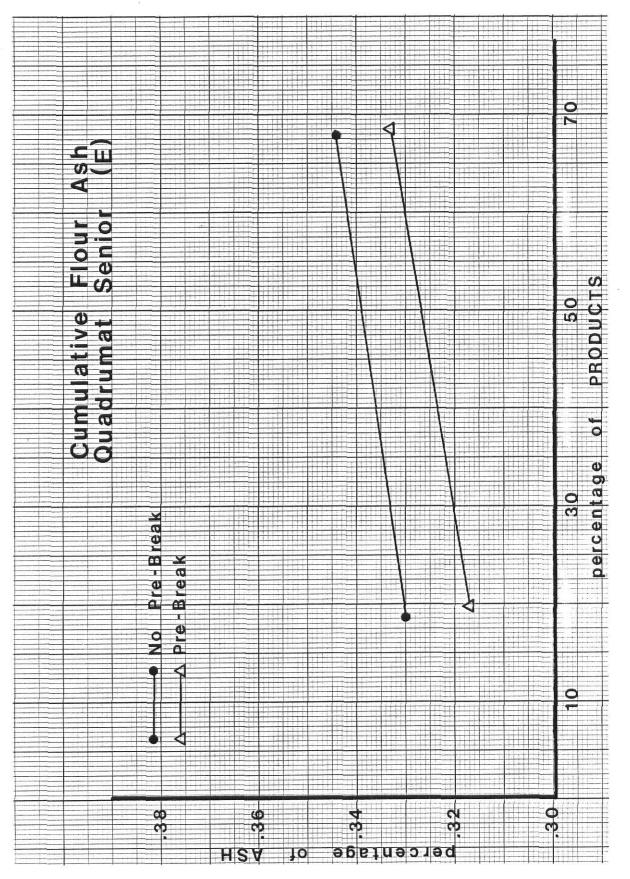
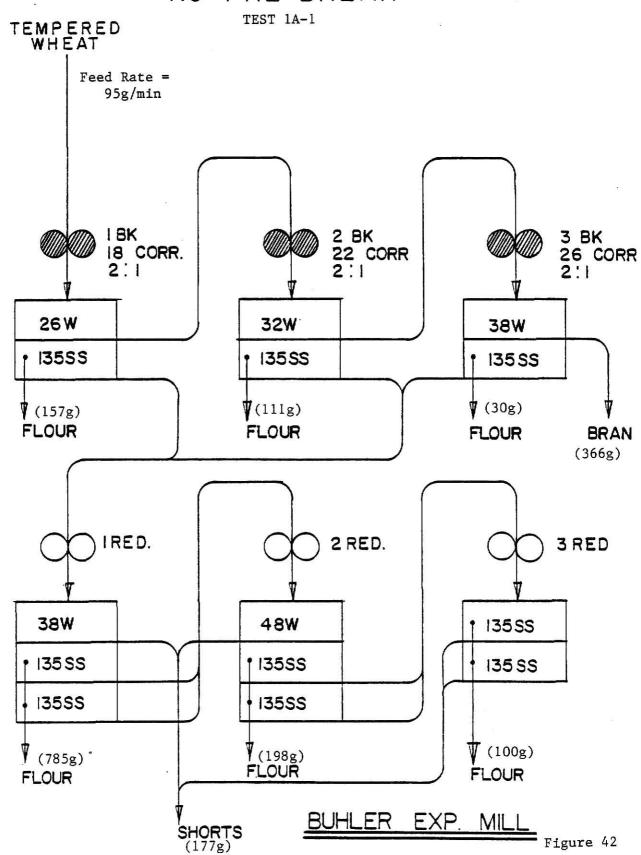
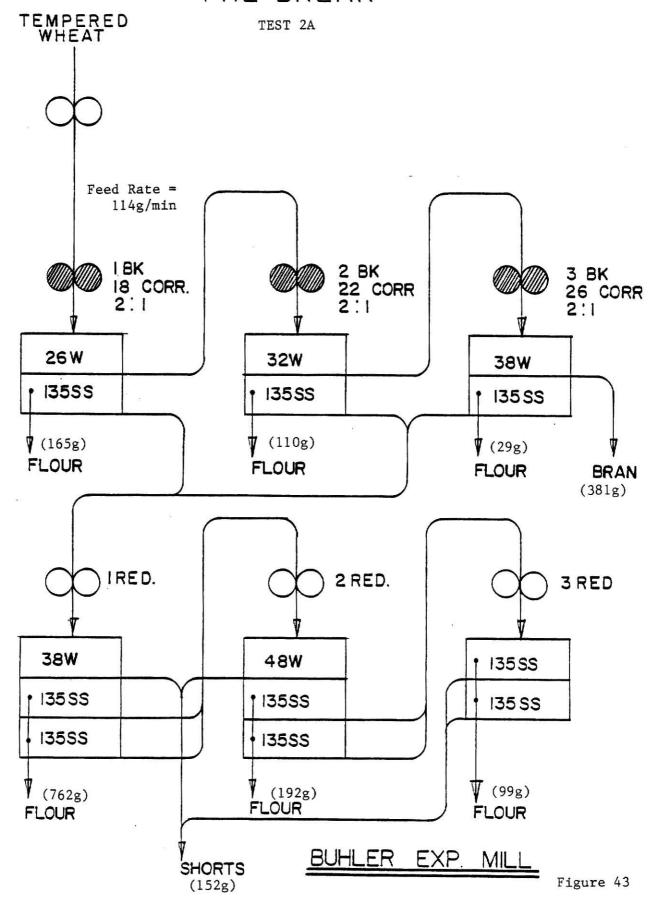


Figure 41

NO PRE-BREAK



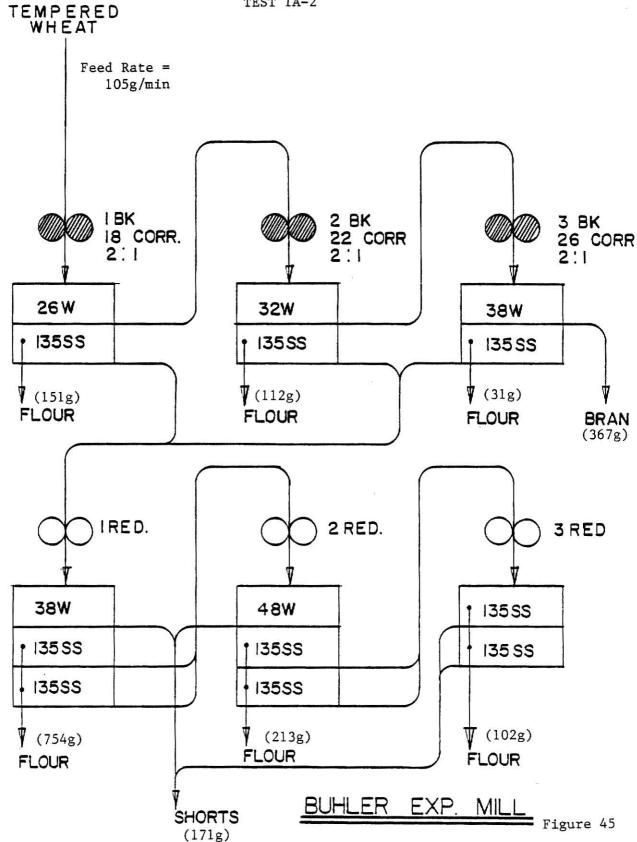
PRE-BREAK

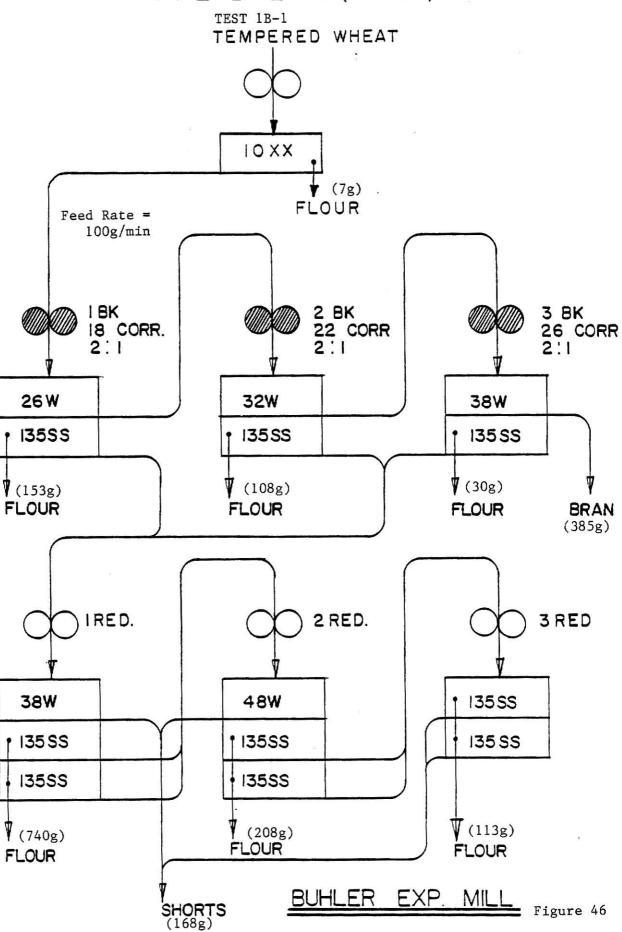


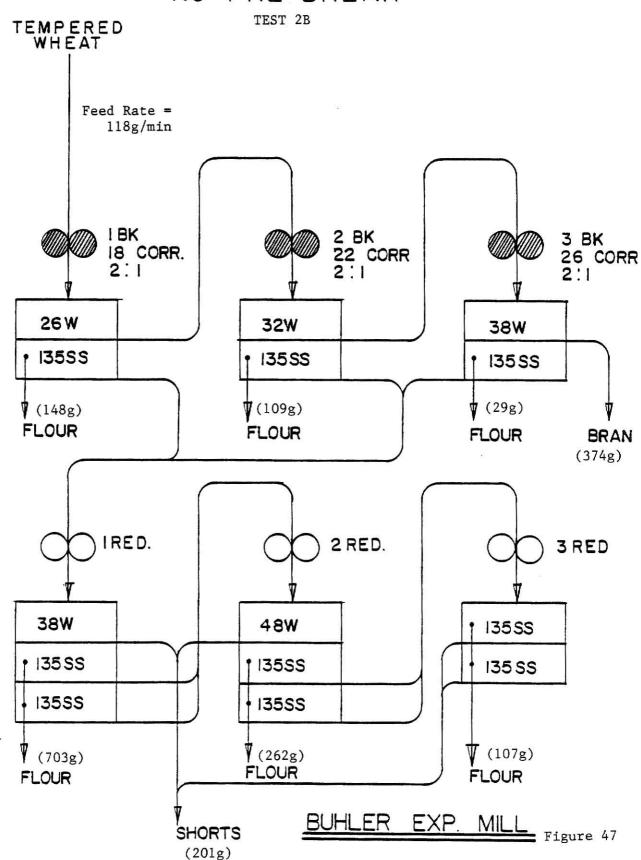
TEMPERED WHEAT IOXX (10g)Feed Rate = FLOUR 118g/min 1 8K 2 BK 22 CORR 3 BK 18 CORR. 26 CORR 2:1 2:1 2:1 26 W 32W 38W 13555 135SS 135SS (31g) (115g) (155g) FLOUR FLOUR **FLOUR** BRAN (406g) IRED. 2 RED. 3 RED **38W** 48W 135SS 135 SS **135SS** 135 SS 13555 13555 ₩ (104g) (227g)(764g) FLOUR FLOUR FLOUR EXP. MIL. SHORTS Figure 44 (171g)

NO PRE-BREAK

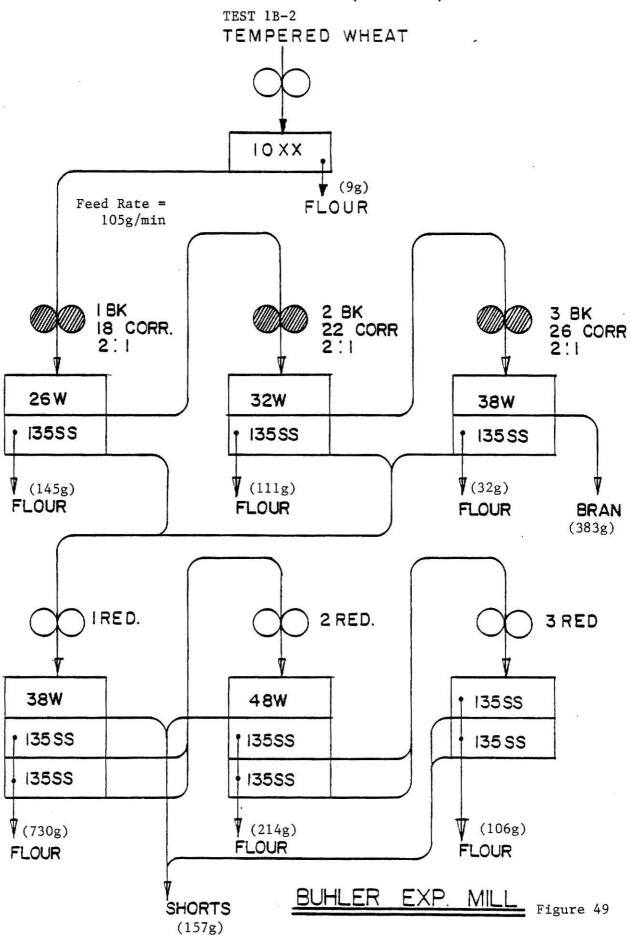
TEST 1A-2

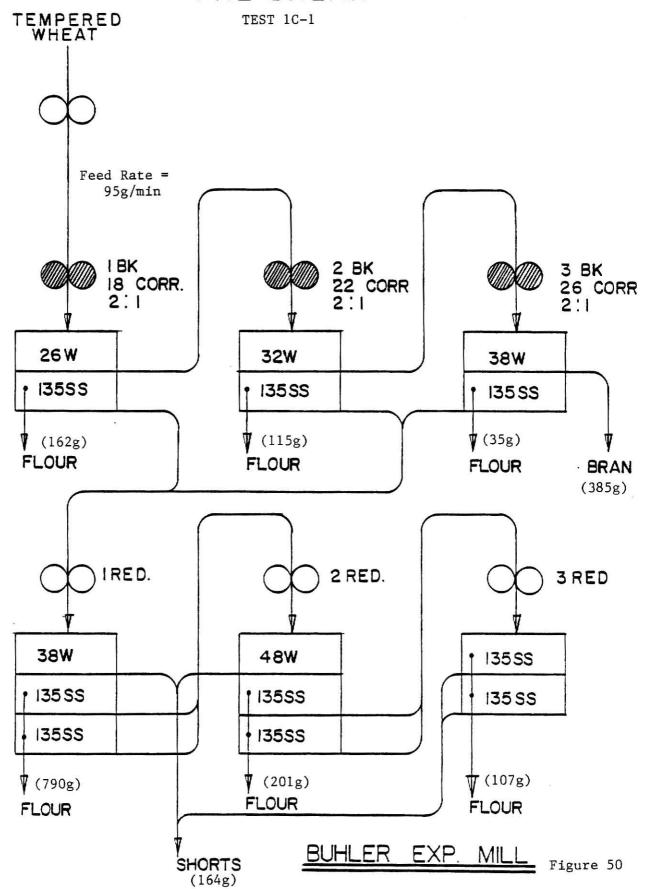




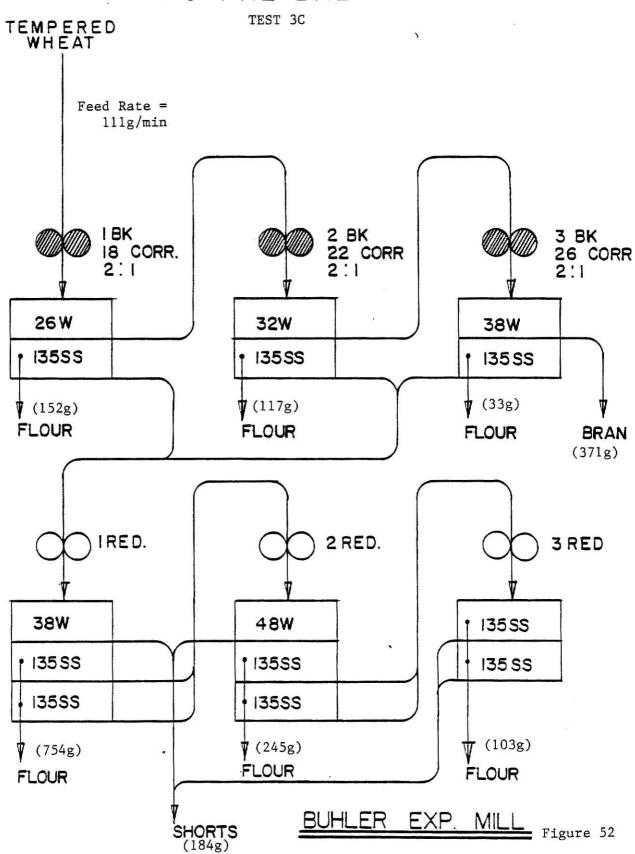


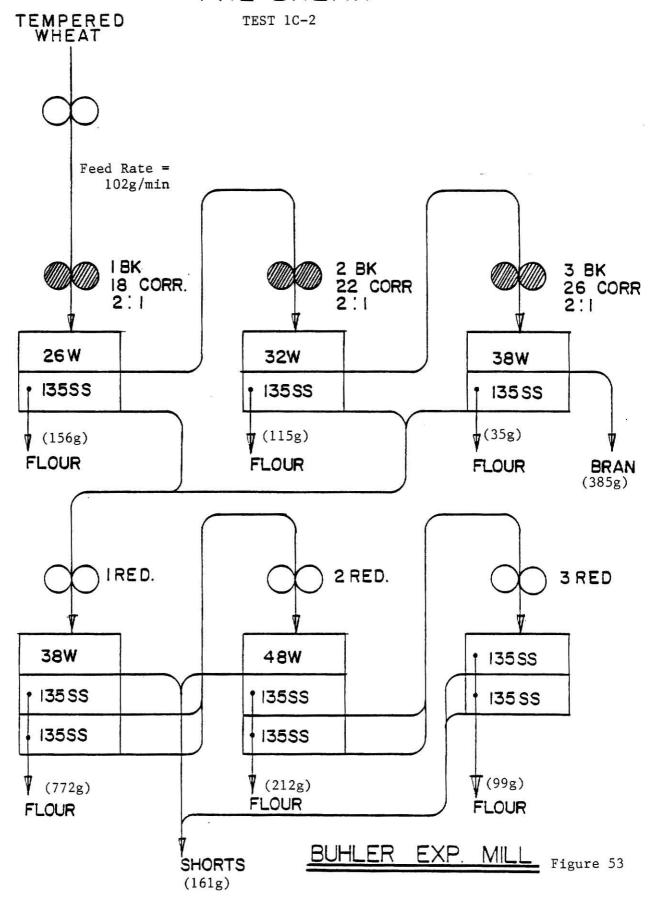
PRE-BREAK TEST 3B TEMPERED WHEAT Feed Rate = 113g/min IBK 2 BK 3 BK 18 CORR. 22 CORR 2:1 26 CORR 2:1 2:1 26 W 32W 38W 135SS 135SS 135SS (31g)**7** (112g) (160g) **FLOUR** FLOUR BRAN FLOUR (387g)IRED. 2 RED. 3 RED 38W 48W 135SS 13555 13555 135 SS **135SS 135SS** ▼ (113g) (226g) (723g) FLOUR FLOUR FLOUR BUHLER EXP. SHORTS Figure 48 (180g)

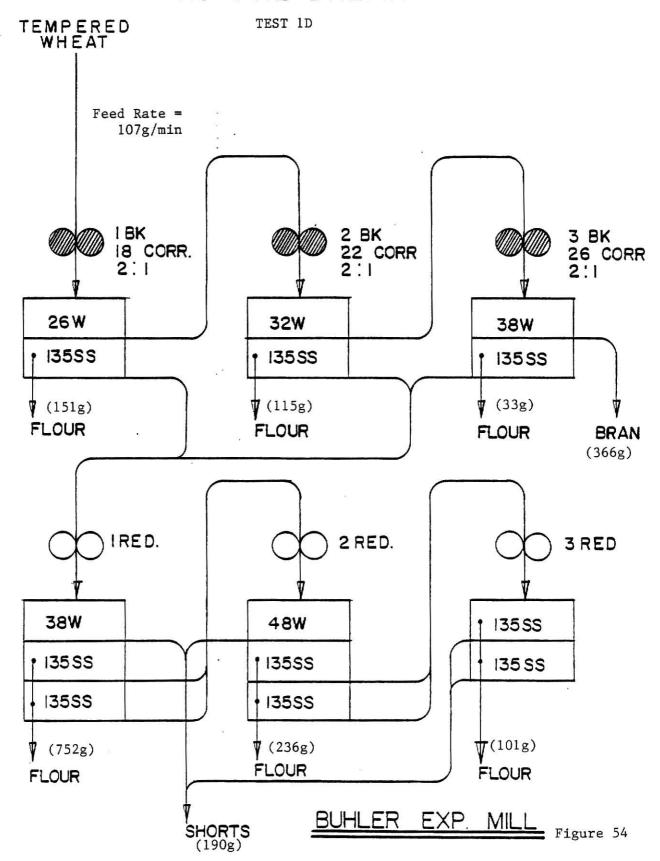




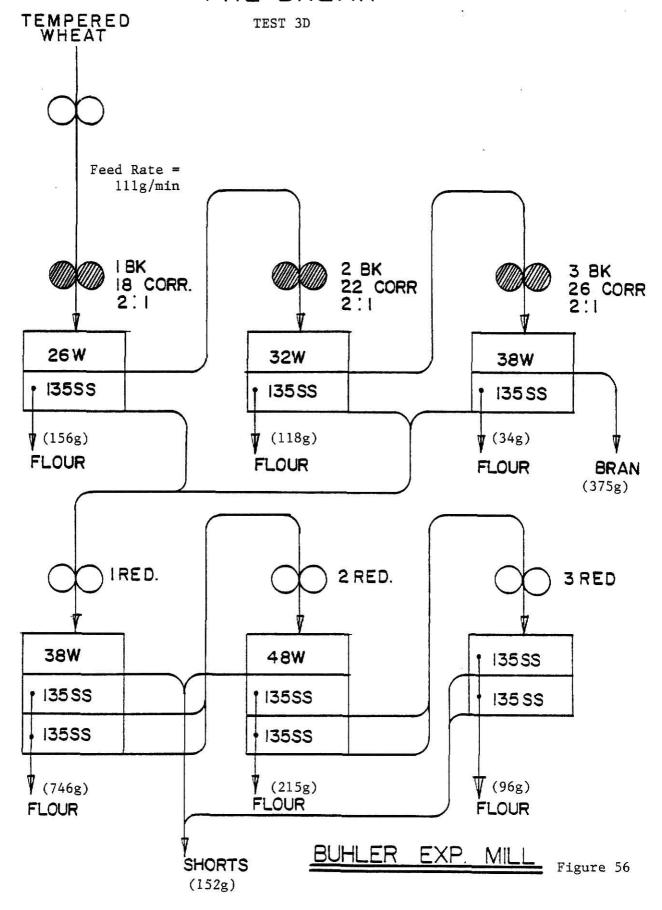
TEST 2C TEMPERED WHEAT IOXX (7g) FLOUR Feed Rate = 110g/min 2 BK IBK **3 BK** 22 CORR 18 CORR. 26 CORR 2:1 2:1 2:1 26 W 32W 38W 13555 135SS 135SS **♥** (32g) ▼ (115g) (147g) FLOUR FLOUR **FLOUR** BRAN (380g) IRED. 2 RED. 3 RED **38W** 48W 1 13555 13555 1 13555 135 SS **135SS 135SS** ▼(101g) (212g)(749g) FLOUR FLOUR FLOUR BUHLER EXP. MILL Figure 51 SHORTS (161g)







TEMPERED WHEAT IOXX (9g) FLOUR Feed Rate = 102g/min 2 BK 22 CORR 2:1 18K 3 BK 18 CORR. 26 CORR 2:1 2:1 26 W 32W 38W 13555 135SS 135SS (36g) (145g)**†** (114g) FLOUR FLOUR FLOUR BRAN (389g) IRED. 2 RED. 3 RED **38W** 48W 135SS 135 SS 13555 135 SS **135SS** 13555 ▼ (105g) (777g) (214g) **FLOUR** FLOUR **FLOUR** EXP. MIL SHORTS (162g) : Figure 55

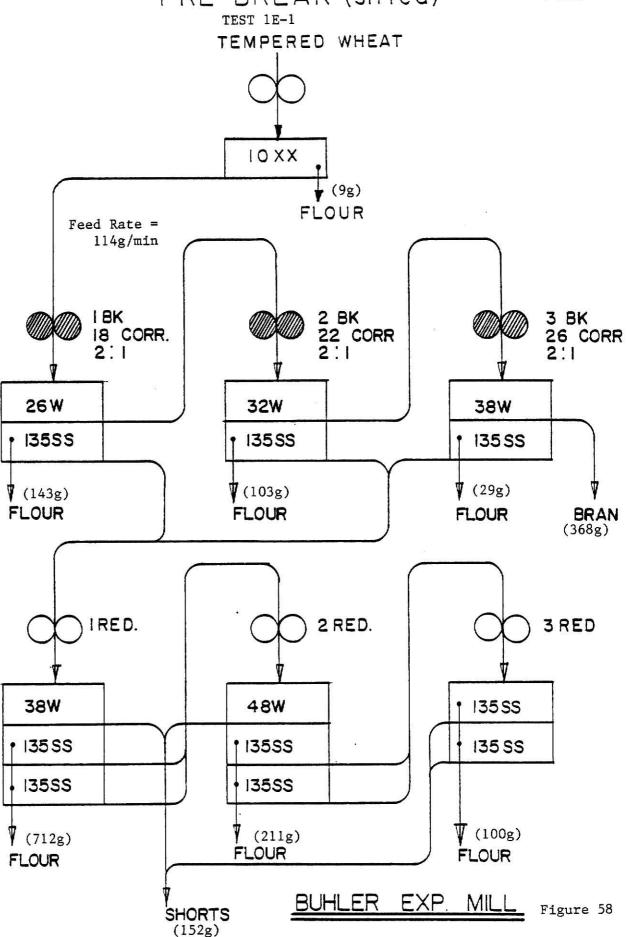


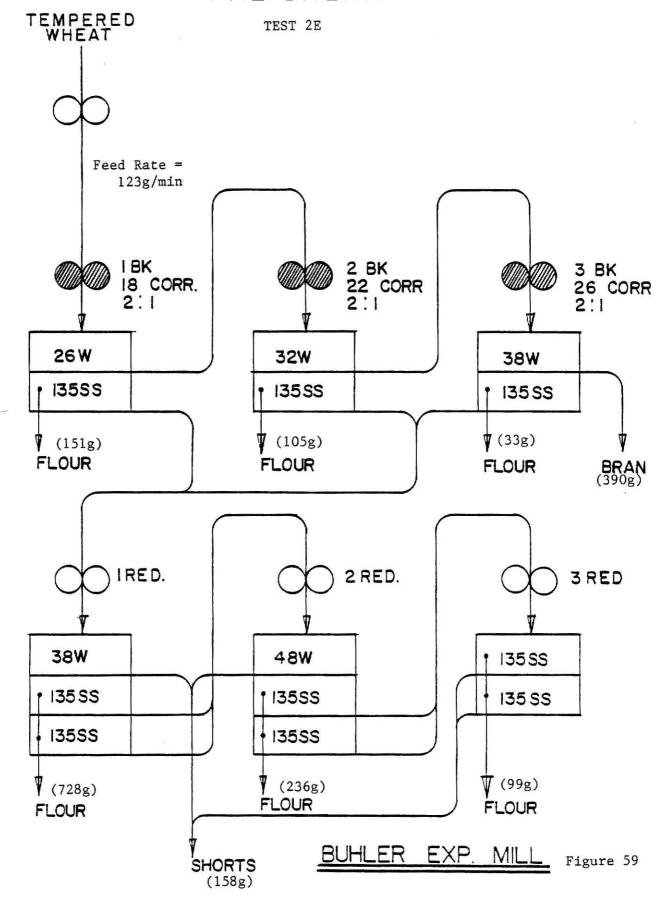
NO PRE-BREAK TEST 1D-2 TEMPERED WHEAT Feed Rate = 118g/min 2 BK 22 CORR IBK 3 BK 18 CORR. 26 CORR 2:1 2:1 26 W 32W 38W 13555 135SS 135SS **♥** (34g) (117g) (148g) **FLOUR** FLOUR **FLOUR** BRAN (374g)IRED. 2 RED. 3 RED 38W 48W 135SS 135 SS 135SS 135 SS **135SS 135SS** ₩ (97g) (257g) (732g) FLOUR FLOUR FLOUR

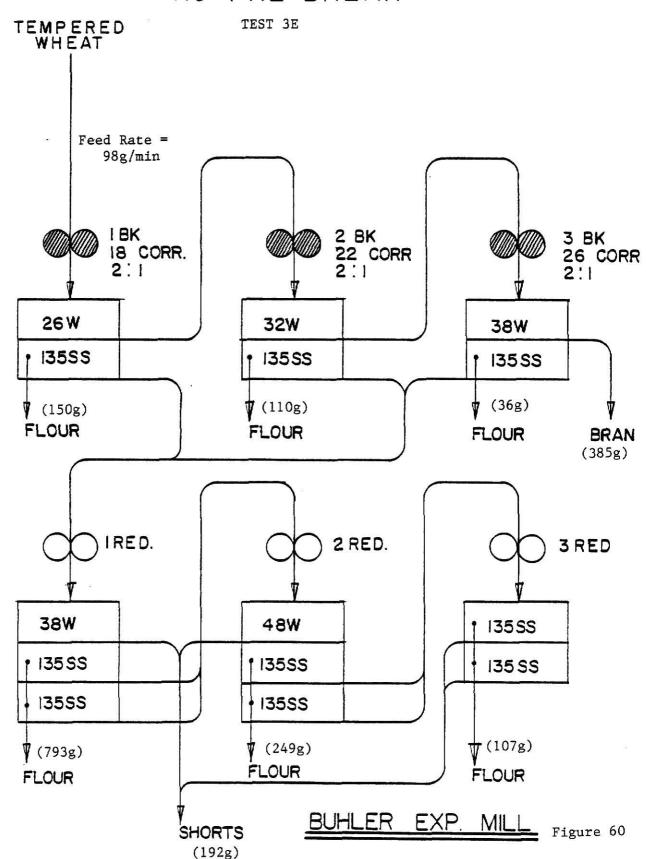
BUHLER EXP.

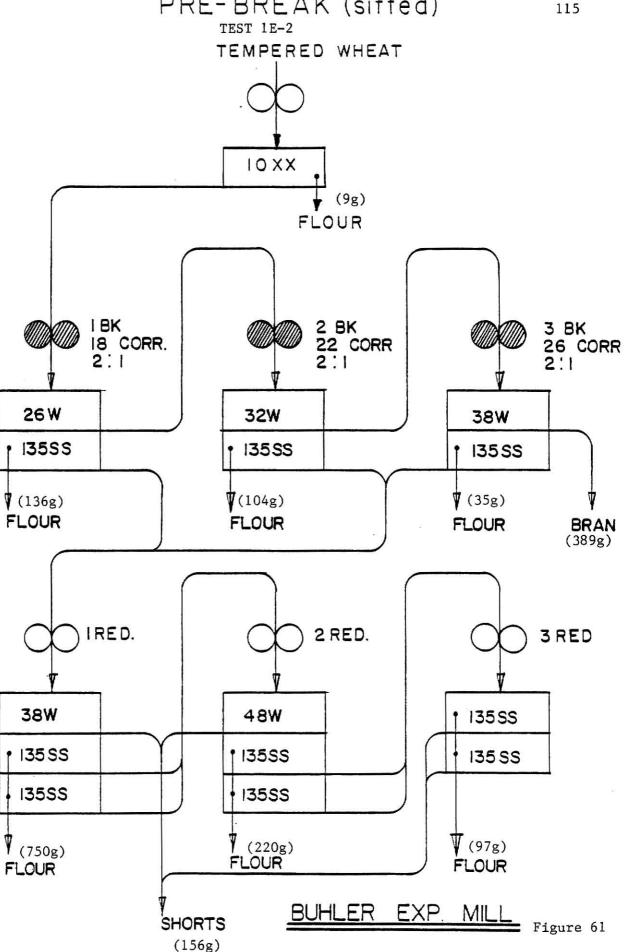
MILL

🗕 Figure 57









Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)

Q=QUANTITY (% of Total Products) S=SUMMATION

BUHLER EXP. MILL A TEST WHEAT HARD RED WINTER

	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QX S of Q
			NO PRE-B	REAK (1)	7		THE COLOR OF MANAGEMENT PRINTERS OF MANAGEMENT
1 RED	785	40.80	40.80	.338	13.790	13.790	.338
1 BK	157	8.16	48,96	.373	3.044	16.834	.344
2 BK	111	5.77	54.73	.377	2,175	19.009	.347
2 RED	198	10.29	65.02	.455	4,682	23.691	.364
3 BK	30	1.56	66.58	.569	0.888	24.579	.369
3 RED	100	5.20	71.78	.666	3.463	28.042	.391
-							
**************************************		P	RE-BREAK (NOT SIFT	ED)		
l RED	762	40.32	40.32	.315	12.701	12.701	.315
l BK	165	8.73	49.05	.340	2.968	15.669	.319
2 BK	110	5.82	54.87	.358	2.084	17,753	.324
2 RED	192	10.16	65.03	.413	4.196	21.949	.338
3 BK	29	1.53	66.56	.523	0.800	22.749	.342
3 RED	99	5.24	71.80	.607	3.181	25.930	.361
1 RED	764	38.53	PRE-BREAK	(SIFTED	12.137	12.137	.315
1 BK	155	7,82	46.35	.340	2.659	14.796	.319
2 BK	115	5.80	52.15	.356	2.065	16.861	.323
2 RED	227	11.45	63.60	.399	4.569	21,429	
Z KED	31	1.56	65.16	.511	0.797	22.226	.337
2 DV	71		65.66	.557	0.279	22.505	.343
and the second second	10	11 711					
3 BK P BK 3 RED	10 104	0.50 5.24	70.90	.573	3.003	25.507	.360
P BK				.573			
P BK 3 RED	104	5,24	70.90 NO PRE-B	.573 REAK (2)	3.003	25.507	.360
P BK 3 RED	754	39.66	70.90	.573 REAK (2)	3.003		.360
P BK 3 RED 1 RED 1 BK	754 151	39.66 7.94	70.90 NO PRE-B 39.66 47.60	.573 REAK (2) .342 .362	3.003 13.564 2.874	25.507 13.564 16.438	.342
P BK 3 RED 1 RED 1 BK 2 BK	754 151 112	39.66 7.94 5.89	70.90 NO PRE-B 39.66 47.60 53.49	.573 REAK (2) .342 .362 .365	13.564 2.874 2.150	13.564 16.438 18.588	.342 .345 .348
P BK	754 151	39.66 7.94	70.90 NO PRE-B 39.66 47.60	.573 REAK (2) .342 .362	3.003 13.564 2.874	25.507 13.564 16.438	.342

Table 10

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)

Q=QUANTITY (% of Total Products)

S = SUMMATION

MILL BUHLER EXP.
TEST B
WHEAT HARD RED WINTER

ST	REAM	WEIGHT (grams)	Q	S of Q	A	QXA	S of QXA	S of QX
				PRE-BREAK	SIFTED (1)		
1 I	RED	740	38.70	38.70	.309	11.958	11.958	.309
1 I	ЗК	153	8.00	46.70	.328	2.624	14.582	.312
2 I	3K	108	5.65	52.35	.348	1.966	16.549	.316
2 I	RED	208	10.88	63.23	.377	4.102	20,650	.327
3 I	RED	113	5.91	69.14	.498	2.943	23.593	.341
3 I	3K	30	1.57	70.71	.530	0.832	24.426	.345
PΙ	3K	7	0,37	71.08	.547	0.202	24.628	.346
		- Alexander - Alex						
				NO PRE	-BREAK			-
1 F	RED	703	36.37	36.37	.332	12.075	12.075	.332
1 E	3K	148	7.66	44.03	.349	2.673	14.748	.335
2 E	3K	109	5.64	49.67	.364	2.053	16.801	.338
2 F	RED	262	13.55	63.22	.408	5.526	22.330	.353
3 E	3K	29	1.50	64.72	.559	0.839	23.168	.358
3 E	RED	107	5.54	70.26	.580	3.213	26.381	.375
1 [(LA S	723		PRE-BREAK	The state of the s	AND DESCRIPTION OF THE PERSON	11.525	308
1 F		723	37.42	37.42	.308	11,525	11.525	.308
1 E	3K	160	37.42 8.28	37.42 45.70	.308	11,525	14,258	.312
-	3K 3K		37.42	37.42	.308	11,525		
1 E	BK BK RED	160 112	37.42 8.28 5.80	37.42 45.70 51.50	.308 .330 .348	11,525 2,732 2,018	14,258 16.276	.312
1 E 2 E 2 F	BK BK RED RED	160 112 226	37.42 8.28 5.80 11.70	37.42 45.70 51.50 63.20	.308 .330 .348 .382	11,525 2,732 2,018 4,469	14.258 16.276 20.746	.312 .316 .328
1 E 2 E 2 F 3 F	BK BK RED RED	160 112 226 113	37.42 8.28 5.80 11.70 5.85	37.42 45.70 51.50 63.20 69.05	.308 .330 .348 .382 .526	11,525 2,732 2,018 4,469 3,077	14.258 16.276 20.746 23.823	.312 .316 .328 .345
1 H 2 H 2 F 3 F	BK BK RED RED	160 112 226 113	37.42 8.28 5.80 11.70 5.85 1.60	37.42 45.70 51.50 63.20 69.05	.308 .330 .348 .382 .526 .529	11,525 2,732 2,018 4,469 3,077 0,846	14.258 16.276 20.746 23.823	.312 .316 .328 .345
1 E 2 E 2 F 3 F	BK BK RED RED BK	160 112 226 113	37.42 8.28 5.80 11.70 5.85 1.60	37.42 45.70 51.50 63.20 69.05 70.65	.308 .330 .348 .382 .526 .529	11,525 2,732 2,018 4,469 3,077 0,846	14.258 16.276 20.746 23.823	.312 .316 .328 .345
1 H 2 H 2 F 3 F 3 E	BK BK RED RED BK	160 112 226 113 31	37.42 8.28 5.80 11.70 5.85 1.60	37.42 45.70 51.50 63.20 69.05 70.65	.308 .330 .348 .382 .526 .529	11,525 2,732 2,018 4,469 3,077 0,846	14.258 16.276 20.746 23.823 24.669	.312 .316 .328 .345 .349
1 F	BK BK RED RED BK RED BK	160 112 226 113 31	37.42 8.28 5.80 11.70 5.85 1.60	37.42 45.70 51.50 63.20 69.05 70.65 PRE-BREAK 38.69	.308 .330 .348 .382 .526 .529 SIFTED (11,525 2,732 2,018 4,469 3,077 0,846	14.258 16.276 20.746 23.823 24.669	.312 .316 .328 .345 .349
1 E 2 E 3 E 3 E 1 E	BK BK RED BK RED BK RED BK RED BK	160 112 226 113 31 730 145	37.42 8.28 5.80 11.70 5.85 1.60 38.69 7.68	37.42 45.70 51.50 63.20 69.05 70.65 PRE-BREAK 38.69 46.37	.308 .330 .348 .382 .526 .529 SIFTED (.314 .317	2) 11,525 2,732 2,018 4,469 3,077 0,846 2) 12,149 2,435	14.258 16.276 20.746 23.823 24.669 12.149 14.583 16.577 21.147	.312 .316 .328 .345 .349
1 H 2 H 3 F 3 F 1 F 1 F 2 F	BK BK RED BK RED BK RED BK RED BK RED	160 112 226 113 31 730 145 111	37.42 8.28 5.80 11.70 5.85 1.60 38.69 7.68 5.88	37.42 45.70 51.50 63.20 69.05 70.65 PRE-BREAK 38.69 46.37 52.25	.308 .330 .348 .382 .526 .529 SIFTED (.314 .317 .339	2) 11,525 2,732 2,018 4,469 3,077 0,846 2) 12,149 2,435 1,993	14.258 16.276 20.746 23.823 24.669 12.149 14.583 16.577	.312 .316 .328 .345 .349
1 F 2 F 3 F 3 F 1 F 1 F 2 F 2 F	RED BK RED RED BK RED BK BK BK RED BK	160 112 226 113 31 730 145 111 214	37.42 8.28 5.80 11.70 5.85 1.60 38.69 7.68 5.88 11.34	37.42 45.70 51.50 63.20 69.05 70.65 PRE-BREAK 38.69 46.37 52.25 63.59	.308 .330 .348 .382 .526 .529 SIFTED (.314 .317 .339 .403	2) 11,525 2,732 2,018 4,469 3,077 0,846 2) 12,149 2,435 1,993 4,570	14.258 16.276 20.746 23.823 24.669 12.149 14.583 16.577 21.147	.312 .316 .328 .345 .349 .314 .314 .317 .333

Table 11

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)

O=OUANTITY (% of Total Pro

Q=QUANTITY (% of Total Products)

S = SUMMATION

MILL BUHLER EXP.
TEST C
WHEAT HARD RED WINTER

PRE-BREAK NOT SIFTED (1)	STREAM	WEIGHT (grams)	Q	S of Q	A	QXA	S of QXA	S of QX
The color of the			PR	E-BREAK NO	T SIFTED	(1)		
2 BK	1 RED	790	40.33	40.33	.306	12.341	12.341	.306
RED 201 10.26 64.73 .401 4.114 21.312 .32 3 BK 35 1.79 66.52 .525 0.940 22.252 .33 3 RED 107 5.46 71.98 .547 2.987 25.238 .35 1 RED 749 39.34 39.34 .306 12.038 12.038 .30 2 BK 147 7.72 47.06 .325 2.509 14.547 .30 2 BK 115 6.04 53.10 .344 2.078 16.625 .31 2 RED 212 11.13 64.23 .383 4.263 20.888 .32 3 BK 32 1.68 65.91 .516 0.867 21.754 .33 P BK 7 0.37 66.28 .528 0.195 21.950 .33 3 RED 101 5.30 71.58 .557 2.952 24.902 .34 NO PRE-BREAK 152 7.76 46.25 .347 2.693 15.471 .33 2 RED 245 12.51 64.73 .433 5.417 23.031 .35 3 BK 33 1.68 66.41 .535 0.899 23.930 .36 3 RED 103 5.26 71.67 .656 3.451 27.381 .38 PRE-BREAK NOT SIFTED (2) RED 772 39.90 39.90 .312 12.449 12.449 .31 1 BK 156 8.06 47.96 .329 2.652 15.101 .31 2 BK 115 5.94 53.90 .353 2.097 17.197 .31 2 RED 212 10.96 64.86 .424 4.647 21.844 .33 3 BK 35 1.81 66.67 .526 0.952 22.796 .34 3 BK 35 1.81 66.67 .526 0.952 22.796 .34 3 BK 35 1.81 66.67 .526 0.952 22.796 .34	1 BK	162	8.27	48.60	.336	2.779	15.120	.311
RED 754 38.49 38.49 332 12.779 12.779 33 3 3 3 3 3 3 3 3	2 BK	115	5.87	54.47	.354	2.078	17.198	.316
PRE-BREAK SIFTED 1 RED	2 RED	201	10.26	64.73	.401	4.114	21.312	.329
PRE-BREAK SIFTED 1 RED	3 BK	35	1.79	66.52	.525	0.940	22.252	.335
1 RED	3 RED	107	5.46	71.98	.547	2.987	25.238	.351
1 RED				DDF DDFA	V CIETEN			****
Table Tabl							10.000	200
NO PRE-BREAK 115 6.04 53.10 .344 2.078 16.625 .31 2 2 2 2 11.13 64.23 .383 4.263 20.888 .32 3 3 3 3 3 3 3 3 3		The second secon						
NO PRE-BREAK 117 5.97 52.22 .359 .2143 17.615 .33 .38 .38 .38 .39 .38 .39 .39 .39 .39 .39 .31 .39 .39 .31 .39 .39 .30 .31 .39 .30 .31 .39 .30 .31 .30								
NO PRE-BREAK NOT SIFTED No PRE-BREAK Not Sifted No Signature No Pre-Break No Pre-B								
NO PRE-BREAK NOT SIFTED NO PRE-BREAK NOT SIFTED NO PRE-BREAK NOT SIFTED NO PRE-BREAK NOT SIFTED NO PRE-BREAK NO PRE-BREAK								
NO PRE-BREAK NO P								
NO PRE-BREAK RED								1
RED 754 38.49 38.49 .332 12.779 12.779 .33 RED 7.76 46.25 .347 2.693 15.471 .33 RED 28K 117 5.97 52.22 .359 2.143 17.615 .33 RED 245 12.51 64.73 .433 5.417 23.031 .35 RED 33 1.68 66.41 .535 0.899 23.930 .36 RED 103 5.26 71.67 .656 3.451 27.381 .38 PRE-BREAK NOT SIFTED (2) RED 772 39.90 39.90 .312 12.449 12.449 .31 RED 78 8.06 47.96 .329 2.652 15.101 .31 RED 28K 115 5.94 53.90 .353 2.097 17.197 .31 RED 212 10.96 64.86 .424 4.647 21.844 .33 RED 212 10.96 64.86 .424 4.647 21.844 .33 RED 3 8K 35 1.81 66.67 .526 0.952 22.796 .344				NO PRE-	BREAK			
The color of the	1 PFD	754	38.49		·	12,779	12,779	.332
PRE-BREAK NOT SIFTED (2) 1 RED 772 39.90 39.90 312 12.449 12.449 .31 1 BK 156 8.06 47.96 .329 2.652 15.101 .31 2 BK 115 5.94 53.90 .353 2.097 17.197 .31 2 RED 212 10.96 64.86 .424 4.647 21.844 .33 3 BK 35 1.81 66.67 .526 0.952 22.796 .34	The state of the s							.335
PRE-BREAK NOT SIFTED (2) 1 RED 772 39.90 39.90 312 12.449 12.449 .31 1 BK 156 8.06 47.96 .329 2.652 15.101 .31 2 BK 115 5.94 53.90 .353 2.097 17.197 .31 2 RED 212 10.96 64.86 .424 4.647 21.844 .33 3 BK 35 1.81 66.67 .526 0.952 22.796 .345								.337
PRE-BREAK NOT SIFTED (2) 1 RED 772 39.90 39.90 312 12.449 12.449 .31 1 BK 156 8.06 47.96 .329 2.652 15.101 .31 2 BK 115 5.94 53.90 .353 2.097 17.197 .31 2 RED 212 10.96 64.86 .424 4.647 21.844 .33 3 BK 35 1.81 66.67 .526 0.952 22.796 .34					CONTRACTOR OF THE PARTY OF THE PARTY.			.356
PRE-BREAK NOT SIFTED (2) 1 RED 772 39.90 39.90 .312 12.449 12.449 .31 1 BK 156 8.06 47.96 .329 2.652 15.101 .31 2 BK 115 5.94 53.90 .353 2.097 17.197 .31 2 RED 212 10.96 64.86 .424 4.647 21.844 .33 3 BK 35 1.81 66.67 .526 0.952 22.796 .34						the state of the s	The second livering the se	.360
1 RED 772 39.90 39.90 .312 12.449 12.449 .31 1 BK 156 8.06 47.96 .329 2.652 15.101 .31 2 BK 115 5.94 53.90 .353 2.097 17.197 .31 2 RED 212 10.96 64.86 .424 4.647 21.844 .33 3 BK 35 1.81 66.67 .526 0.952 22.796 .34					.656	3.451	27.381	.382
1 RED 772 39.90 39.90 .312 12.449 12.449 .31 1 BK 156 8.06 47.96 .329 2.652 15.101 .31 2 BK 115 5.94 53.90 .353 2.097 17.197 .31 2 RED 212 10.96 64.86 .424 4.647 21.844 .33 3 BK 35 1.81 66.67 .526 0.952 22.796 .34								
1 BK 156 8.06 47.96 .329 2.652 15.101 .31 2 BK 115 5.94 53.90 .353 2.097 17.197 .31 2 RED 212 10.96 64.86 .424 4.647 21.844 .33 3 BK 35 1.81 66.67 .526 0.952 22.796 .34							1 10 110	
2 BK 115 5.94 53.90 .353 2.097 17.197 .31 2 RED 212 10.96 64.86 .424 4.647 21.844 .33 3 BK 35 1.81 66.67 .526 0.952 22.796 .34	1 RED		39.90					.312
2 RED 212 10.96 64.86 .424 4.647 21.844 .33 3 BK 35 1.81 66.67 .526 0.952 22.796 .34	1 BK	156						.315
3 BK 35 1.81 66.67 .526 0.952 22.796 .34	2 BK	115						.319
5 DK	2 RED	212						.337
3 RED 99 5.12 71.79 .616 3.154 25.950 .36	3 BK						the state of the s	.342
	3 RED	99	5.12	71.79	.616	3.154	25.950	.361

Cumulative Flour Ash Calculations

A=ASH(14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL BUHLER EXP.

TEST. D

HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QX S of Q
			NO PRE-B	REAK (1)			
1 RED	752	38.68	38.68	.331	12.803	12.803	.331
1 BK	151	7.77	46.45	.352	2.735	15.538	.335
2 BK	115	5.92	52.37	.366	2,167	17.705	.338
2 RED	236	12.14	64.51	.425	5.160	22.864	.354
3 BK	33	1.70	66.21	.538	0,915	23.779	.359
3 RED	101	5.20	71.41	.615	3,198	26,977	.378
22390							
			PRE-BREA	 			+
1 RED	777	39.83	39.83	.322	12,825	12.825	.322
1 BK	145	7.43	47.26	.326	2,422	15.247	.323
2 BK	114	5.84	53.10	.359	2.097	17.344	.327
2 RED	214	10.97	64.07	.423	4.640	21.984	.343
3 BK	36	1.85	65.92	.531	0.982	22.967	.348
P BK	9	0.46	66.38	.540	0.248	23.215	.350
3 RED	105	5.38	71.76	.601	3,233	26,448	.369
1 DED	746		PRE-BREAK			12 054	226
1 RED	/40	39.43	39.43	.326	12.854	12.854	.326
1 DV	156		1 47.00	1 .340	/ 01/17		220
	156	8.25	1				.328
2 BK	118	6.24	53.92	.365	2.278	17.937	.333
2 BK 2 RED	118 215	6.24 11.36	53.92 65.28	.365	2.278 4.885	17.937 22.822	.333
2 BK 2 RED 3 BK	118 215 34	6.24 11.36 1.80	53.92 65.28 67.08	.365 .430 .536	2.278 4.885 0.965	17.937 22.822 23.786	.333 .350 .355
2 BK 2 RED 3 BK	118 215	6.24 11.36	53.92 65.28	.365	2.278 4.885	17.937 22.822	.333
2 BK 2 RED 3 BK	118 215 34	6.24 11.36 1.80	53.92 65.28 67.08	.365 .430 .536 .642	2.278 4.885 0.965	17.937 22.822 23.786	.333 .350 .355
2 BK 2 RED 3 BK 3 RED	118 215 34	6.24 11.36 1.80	53.92 65.28 67.08 72.15	.365 .430 .536 .642	2.278 4.885 0.965	17.937 22.822 23.786	.333 .350 .355
2 BK 2 RED 3 BK 3 RED	118 215 34 96	6.24 11.36 1.80 5.07	53.92 65.28 67.08 72.15 NO PRE-B	.365 .430 .536 .642	2.278 4.885 0.965 3.255	17.937 22.822 23.786 27.041	.333 .350 .355 .375
2 BK 2 RED 3 BK 3 RED 1 RED	118 215 34 96	6.24 11.36 1.80 5.07	53.92 65.28 67.08 72.15 NO PRE-B 37.67 45.29	.365 .430 .536 .642 REAK (2)	2.278 4.885 0.965 3.255 12.431 2.682	17.937 22.822 23.786 27.041 12.431 15.113	.333 .350 .355 .375
2 BK 2 RED 3 BK 3 RED 1 RED 1 BK 2 BK	118 215 34 96 732 148	6.24 11.36 1.80 5.07 37.67 7.62 6.02	53.92 65.28 67.08 72.15 NO PRE-B 37.67	.365 .430 .536 .642 REAK (2) .330 .352 .361	2.278 4.885 0.965 3.255 12.431 2.682 2.173	17.937 22.822 23.786 27.041 12.431 15.113 17,287	.333 .350 .355 .375 .375
2 BK 2 RED 3 BK 3 RED 1 RED 1 BK 2 BK	118 215 34 96 732 148 117	6.24 11.36 1.80 5.07	53.92 65.28 67.08 72.15 NO PRE-B 37.67 45.29 51.31	.365 .430 .536 .642 REAK (2) .330 .352	2.278 4.885 0.965 3.255 12.431 2.682	17.937 22.822 23.786 27.041 12.431 15.113	.333 .350 .355 .375
2 BK 2 RED 3 BK 3 RED 1 RED 1 BK 2 BK 2 RED	732 148 117 257	6.24 11.36 1.80 5.07 37.67 7.62 6.02 13.23	53.92 65.28 67.08 72.15 NO PRE-B 37.67 45.29 51.31 64.54	.365 .430 .536 .642 REAK (2) .330 .352 .361 .432	2.278 4.885 0.965 3.255 12.431 2.682 2.173 5.715	17.937 22.822 23.786 27.041 12.431 15.113 17.287 23,002	.333 .350 .355 .375 .375

Table 13

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)

Q=QUANTITY (% of Total Products)

S = SUMMATION

MILL BUHLER EXP.
TEST E
WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QX
		P	RE-BREAK S	IFTED (1)		
1 RED	712	38.97	38.97	.302	11.769	11.769	.302
1 BK	143	7.83	46.80	.327	2.560	14.329	.306
2 BK	103	5.64	52.44	.345	1.946	16.275	.310
2 RED	211	11.55	63.99	.359	4.146	20,422	.319
3 RED	100	5.47	69.46	.479	2.620	23.042	.332
3 BK	29	1.59	71.05	.509	0.809	23.851	.336
P BK	9	0.49	71.54	.541	0.265	24,116	.337
-							
			PRE-BREAK	NOT SIFT	ED		
1 RED	728	38.32	38.32	.304	11.649	11.649	.304
1 BK	151	7.95	46.27	.330	2.624	14.273	.308
2 BK	105	5.53	51.80	.351	1.941	16.214	.313
2 RED	236	12.42	64.22	.374	4.645	20.359	.325
3 BK	33	1.74	65.96	.512	0.891	21.750	.330
3 RED	99	5.21	71.17	.521	2.714	24.464	.344
1 RED	793	39.22	NO PRE	-BREAK	12.786	12.786	.326
	1 1 2 3		The second secon				
		7.42	46.64	1 . 363	1 2.693	15.479	
1 BK	150	7.42 5.44	46.64 52.08	.363	2.693	15.479	.332
1 BK 2 BK	150 110	5.44	52.08	.373	2.029	17.508	.332
1 BK 2 BK 2 RED	150 110 249	5.44 12.31	52.08 64.39	.373 .425	2.029 5.232	17.508 22.740	.332 .336 .353
1 BK 2 BK	150 110	5.44	52.08	.373	2.029	17.508	.332
1 BK 2 BK 2 RED 3 BK	150 110 249 36	5.44 12.31 1.78	52.08 64.39 66.17	.373 .425 .532	2.029 5.232 0.947	17.508 22.740 23.687	.332 .336 .353 .358
1 BK 2 BK 2 RED 3 BK	150 110 249 36	5.44 12.31 1.78 5.29	52.08 64.39 66.17	.373 .425 .532 .618	2.029 5.232 0.947	17.508 22.740 23.687	.332 .336 .353 .358
1 BK 2 BK 2 RED 3 BK	150 110 249 36	5.44 12.31 1.78 5.29	52.08 64.39 66.17 71.46	.373 .425 .532 .618	2.029 5.232 0.947 3.269	17.508 22.740 23.687	.332 .336 .353 .358
1 BK 2 BK 2 RED 3 BK 3 RED	150 110 249 36 107	5.44 12.31 1.78 5.29	52.08 64.39 66.17 71.46	.373 .425 .532 .618	2.029 5.232 0.947 3.269	17.508 22.740 23.687 26.956	.332 .336 .353 .358 .377
1 BK 2 BK 2 RED 3 BK 3 RED 1 RED 1 BK	150 110 249 36 107	5.44 12.31 1.78 5.29	52.08 64.39 66.17 71.46 PRE-BREAK 39.56	.373 .425 .532 .618 SIFTED (2.029 5.232 0.947 3.269 2) 12.303	17.508 22.740 23.687 26.956	.332 .336 .353 .358 .377
1 BK 2 BK 2 RED 3 BK 3 RED 1 RED 1 BK 2 BK	150 110 249 36 107 750 136	5.44 12.31 1.78 5.29 39.56 7.17	52.08 64.39 66.17 71.46 PRE-BREAK 39.56 46.73	.373 .425 .532 .618 SIFTED (.311 .324	2.029 5.232 0.947 3.269 2) 12.303 2.323	17.508 22.740 23.687 26.956 12.303 14.626	.332 .336 .353 .358 .377
1 BK 2 BK 2 RED 3 BK 3 RED 1 RED 1 BK 2 BK 2 RED	150 110 249 36 107 750 136 104	5.44 12.31 1.78 5.29 39.56 7.17 5.49	52.08 64.39 66.17 71.46 PRE-BREAK 39.56 46.73 52.22	.373 .425 .532 .618 SIFTED (.311 .324 .345	2.029 5.232 0.947 3.269 2) 12.303 2.323 1.894	17.508 22.740 23.687 26.956 12.303 14.626 16.520	.332 .336 .353 .358 .377
1 BK 2 BK 2 RED 3 BK 3 RED	150 110 249 36 107 750 136 104 220	5.44 12.31 1.78 5.29 39.56 7.17 5.49 11.60	52.08 64.39 66.17 71.46 PRE-BREAK 39.56 46.73 52.22 63.82	.373 .425 .532 .618 SIFTED (.311 .324 .345 .390	2.029 5.232 0.947 3.269 2) 12.303 2.323 1.894 4.524	17.508 22.740 23.687 26.956 12.303 14.626 16.520 21.044	.332 .336 .353 .358 .377 .311 .313 .316 .330

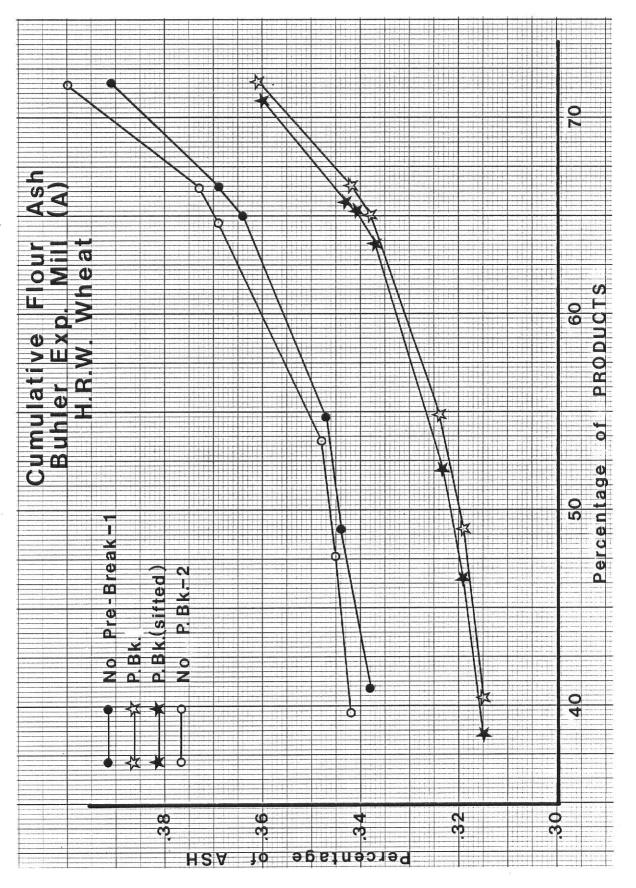


Figure 62

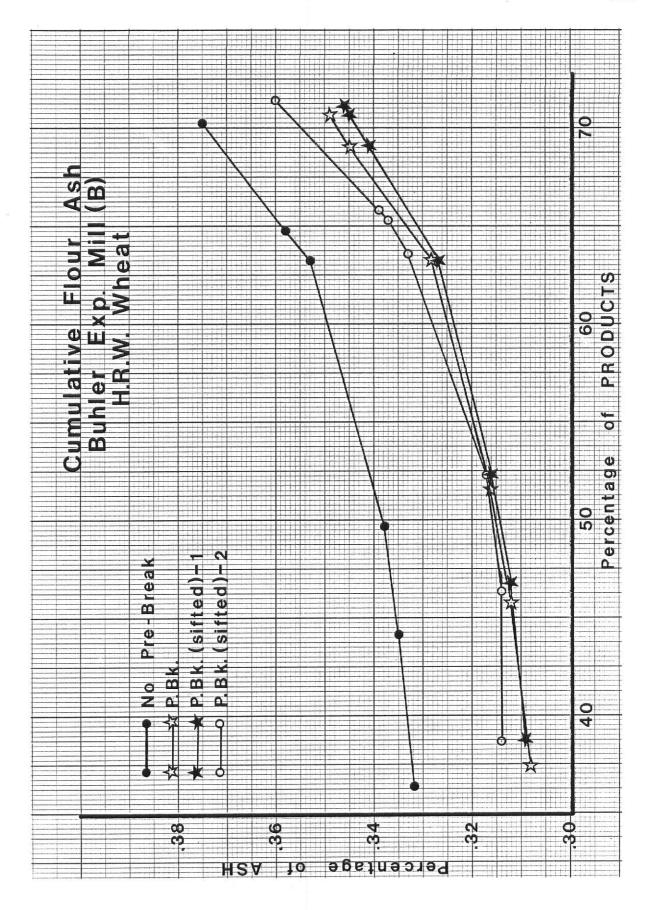


Figure 63

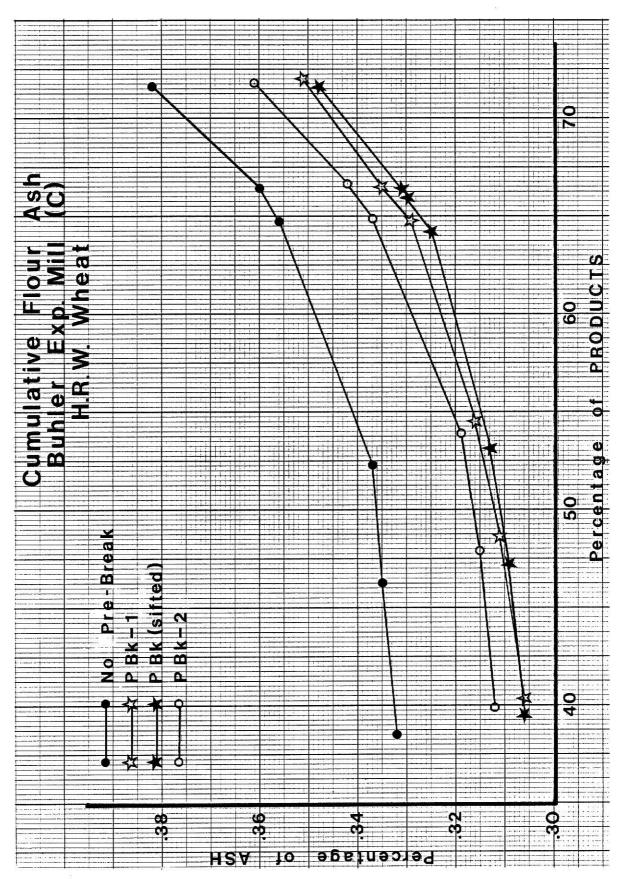


Figure 64

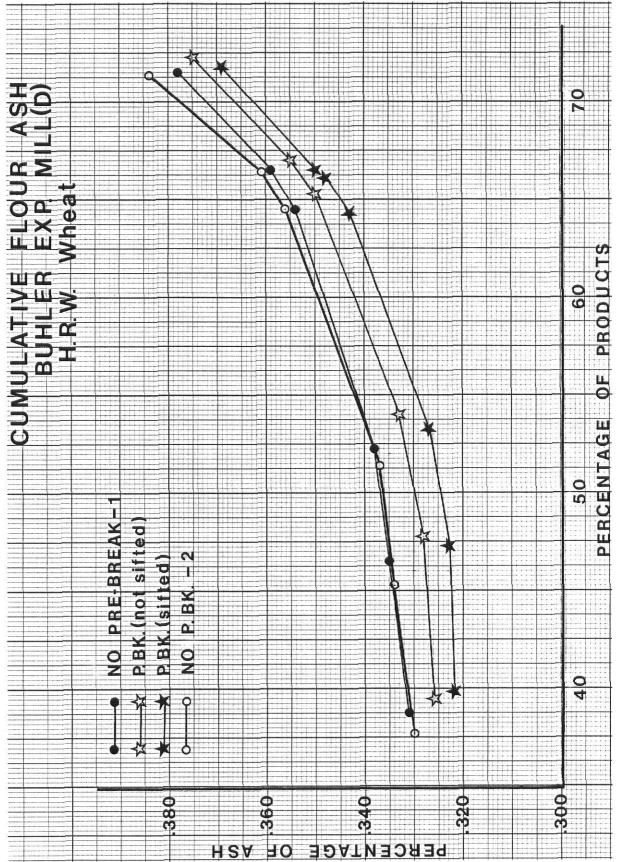
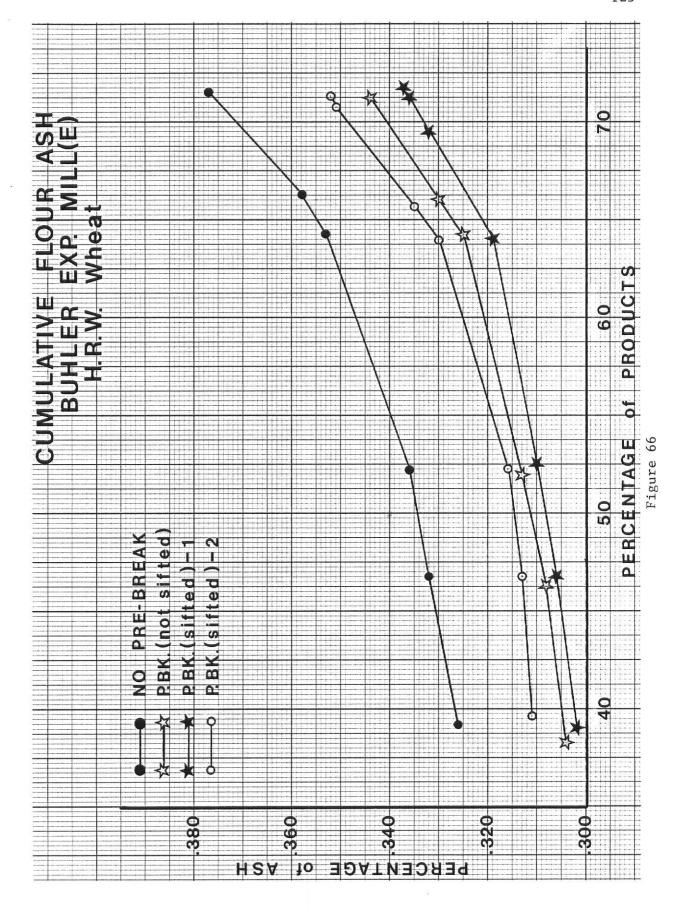
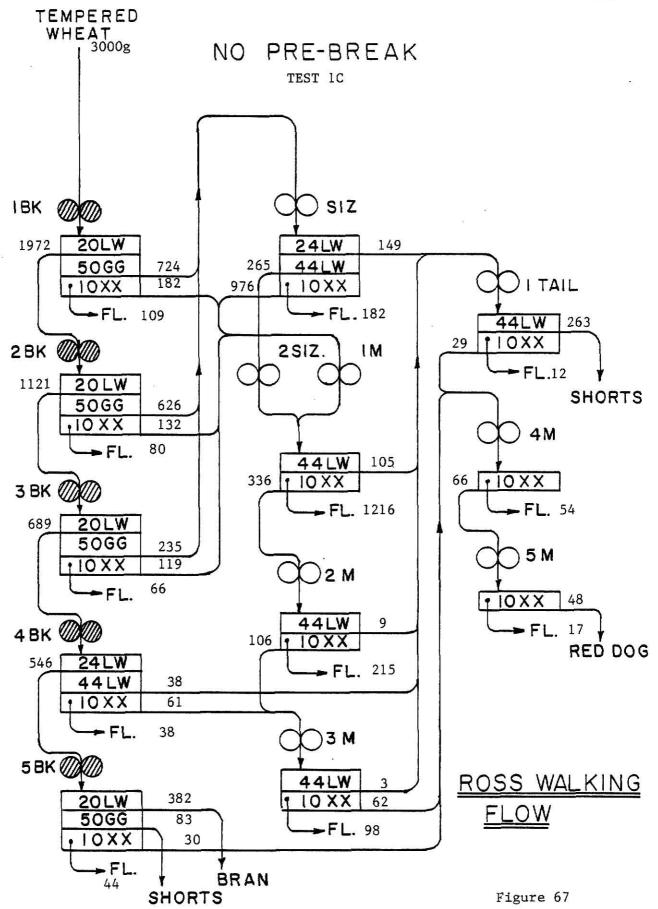


Figure 65





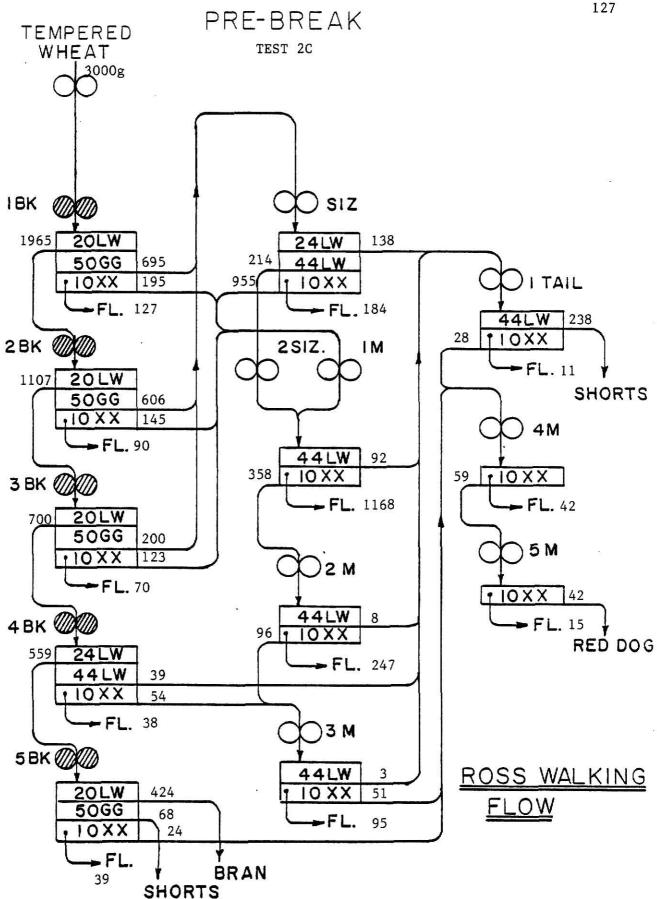


Figure 68

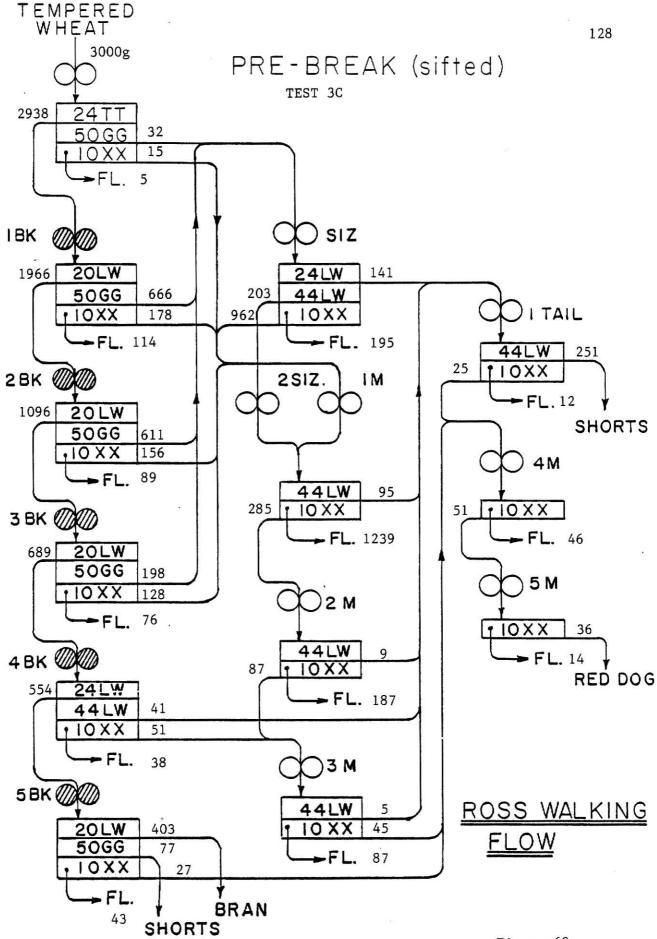


Figure 69

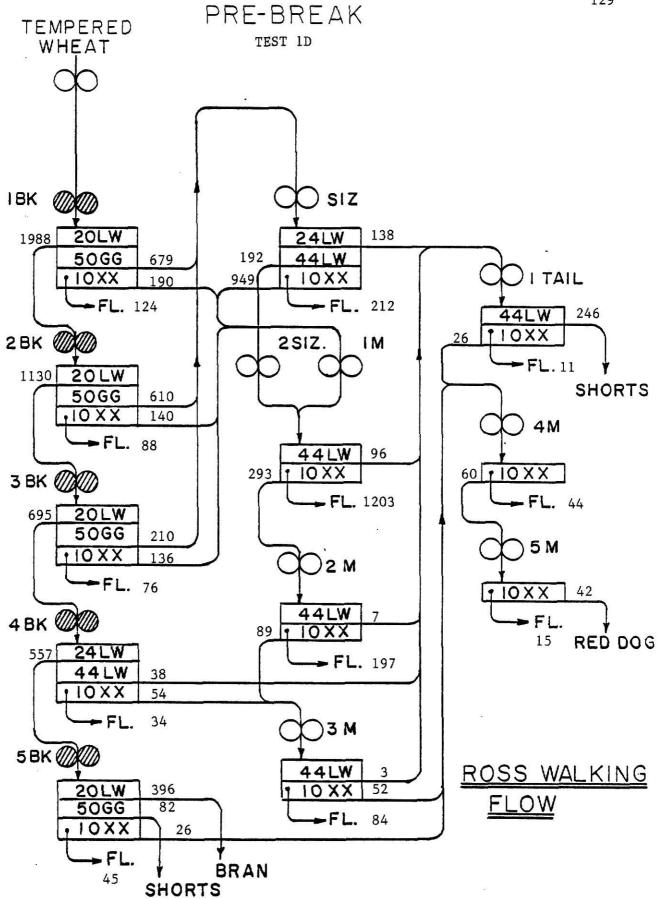
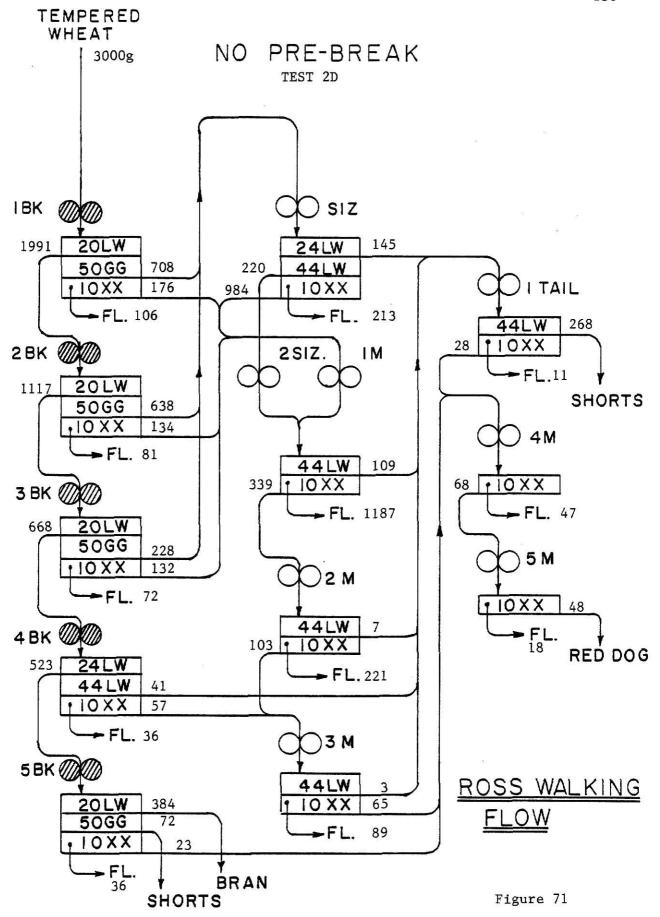


Figure 70



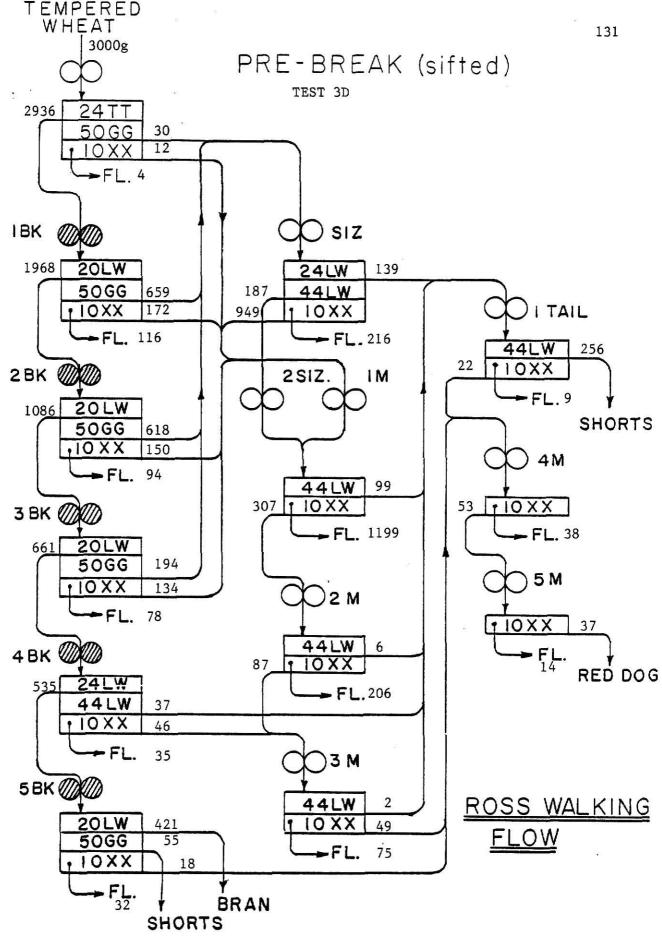


Figure 72

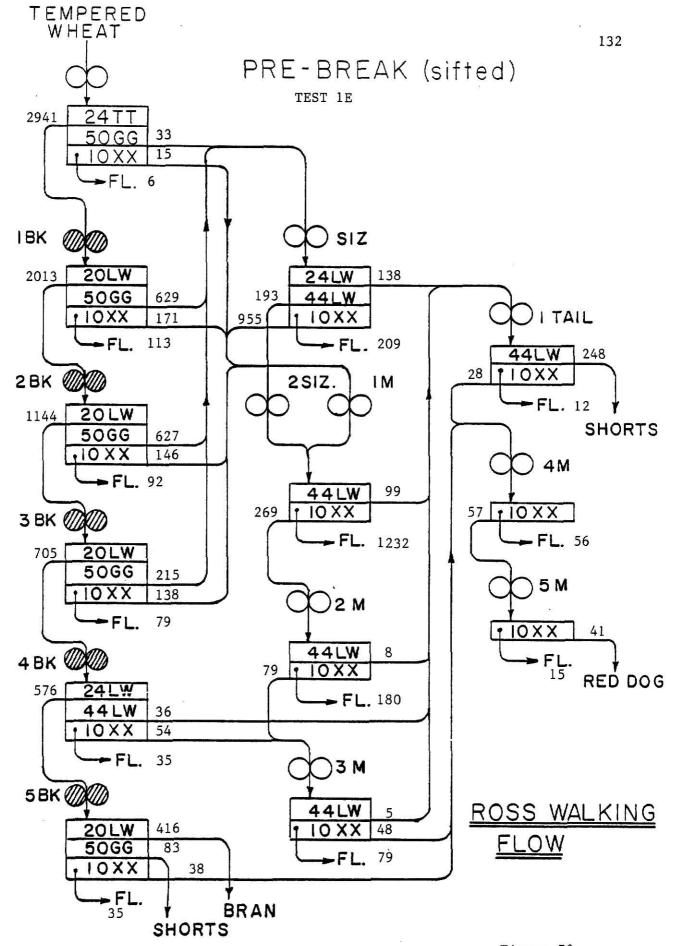
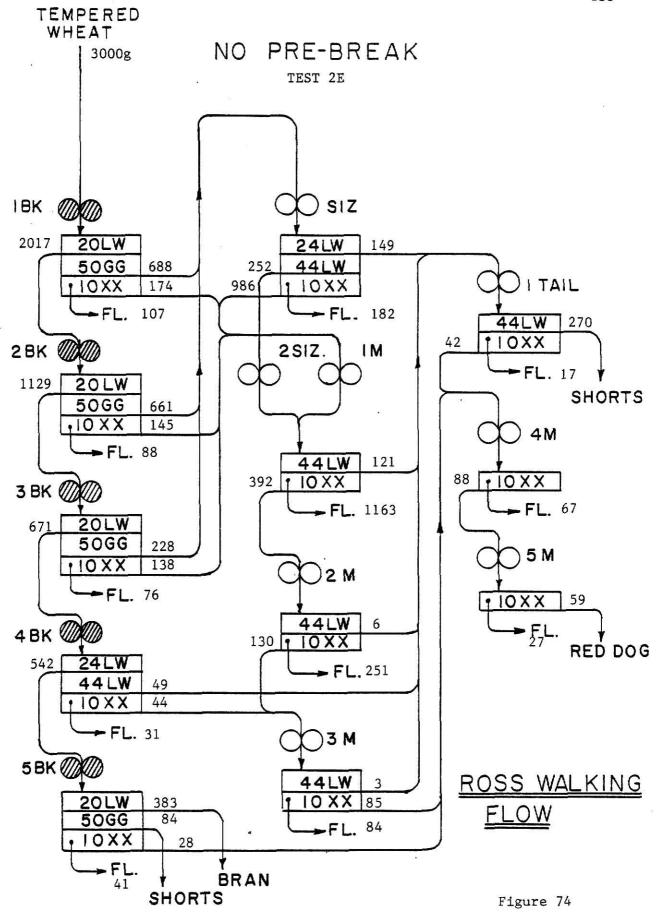


Figure 73



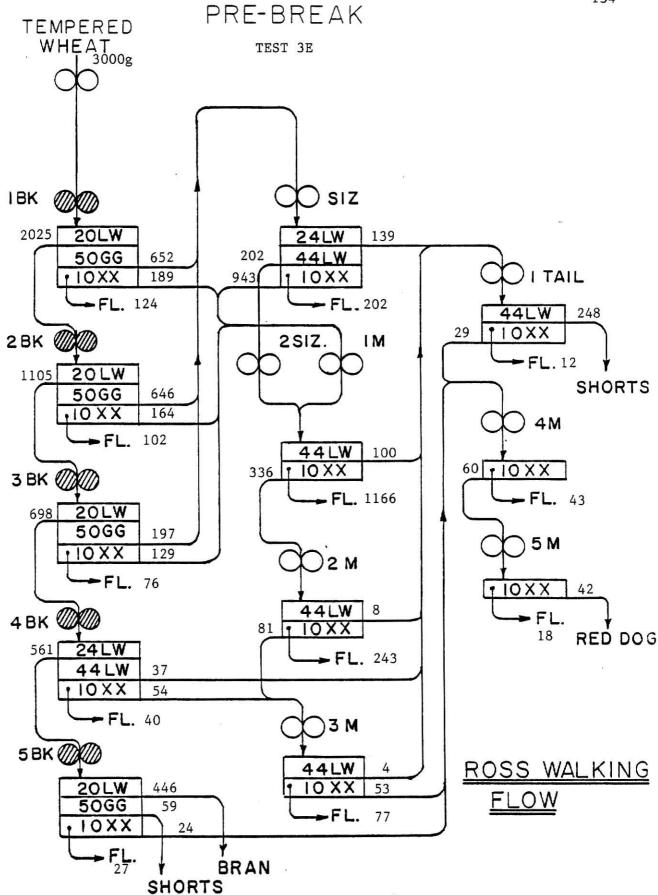
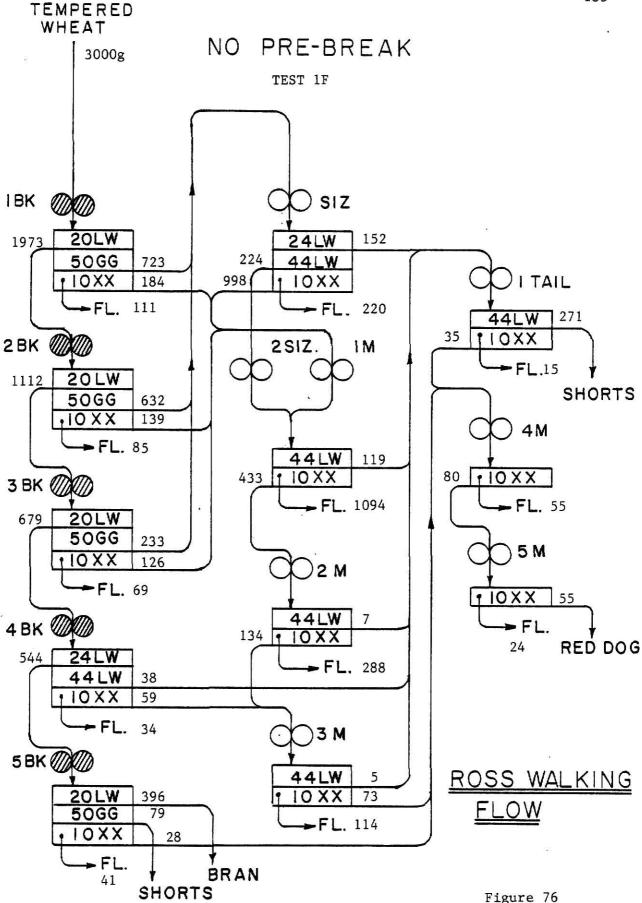


Figure 75



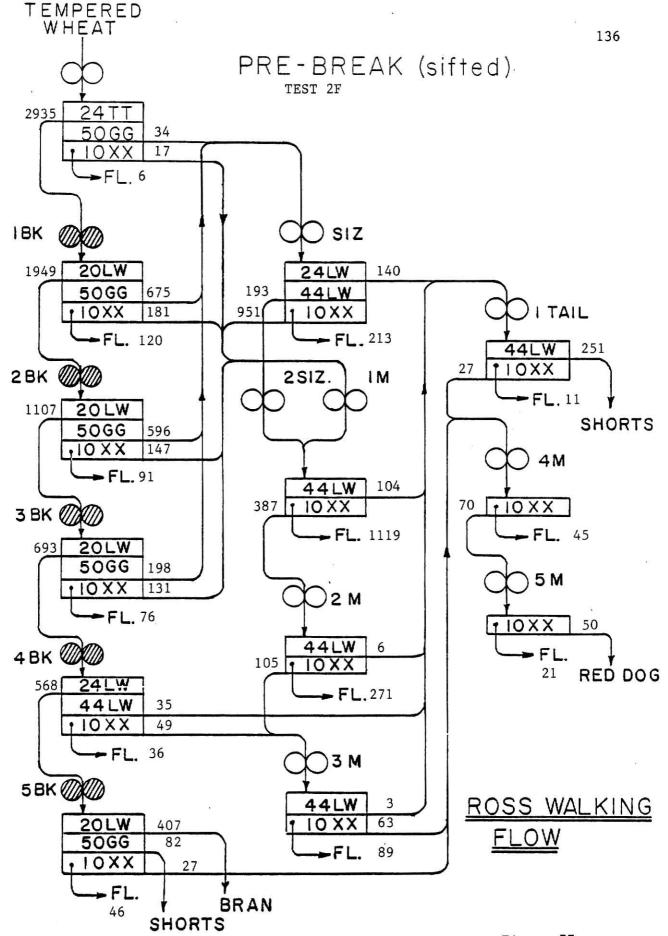


Figure 77

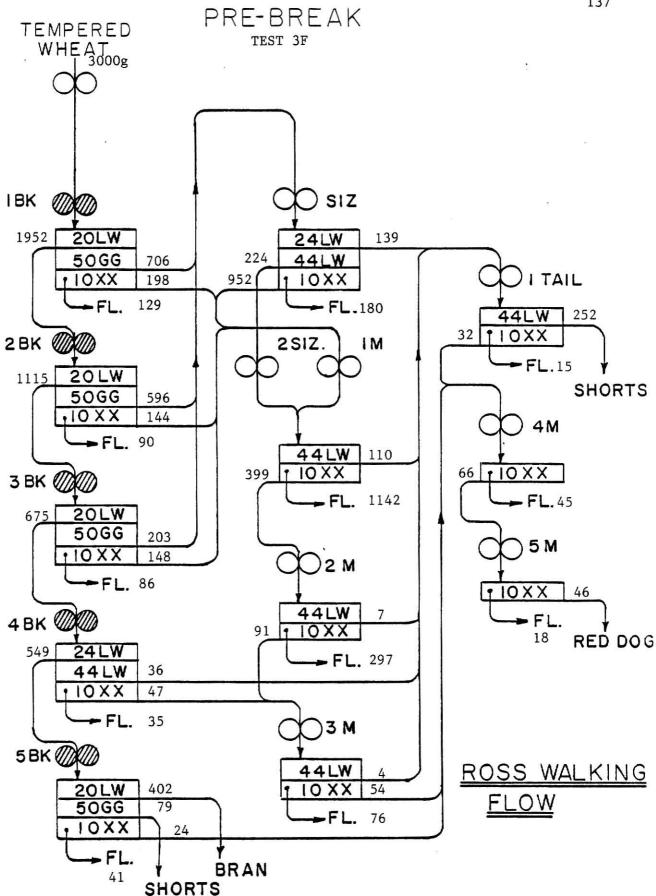


Figure 78

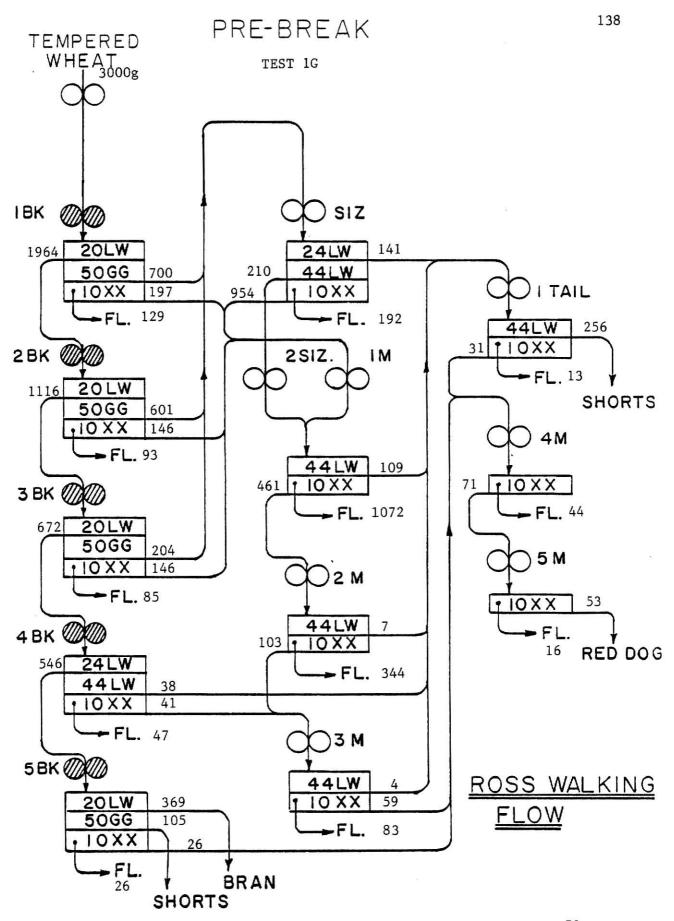
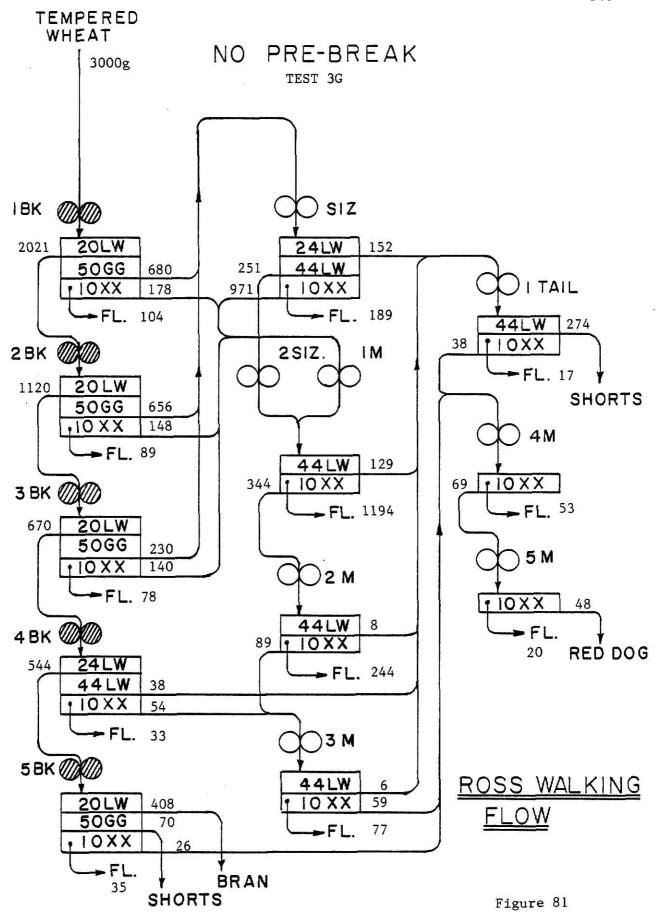


Figure 79

Figure 80



A=ASH (14% Moisture Basis)

Q=QUANTITY (% of Total Products)

S=SUMMATION

MILL

ROSS FLOW

TEST

WHEAT

HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QXA
			NO PRI	E-BREAK			
1 M	1216	41.83	41.83	.284	11.880	11.880	.284
SIZ	182	6.26	48.09	.315	1.972	13.852	.288
2 M	215	7.40	55.49	.319	2.361	16.213	.292
3 BK	66	2.27	57.76	.393	0.892	17.105	.296
2 BK	80	2.75	60.51	.413	1.136	18.241	.301
3 M	98	3.37	63.88	.417	1.405	19.646	.308
4 BK	38	1.31	65.19	.452	0.592	20.238	.310
1 BK	109	3.75	68.94	.496	1.860	22,098	.321
1 TA	12	0.41	69.35	,575	0.236	22.334	.322
5 BK	44	1.51	70.86	.644	0.972	23.306	.329
4 M	54	1.86	72.72	.714	1.328	24.634	.339
5 M	17	0.58	73.30	1.463	0.849	25.483	.348
			PRE-BREAK	NOT SIFT	ED		
1 M	1168	40.30	40.30	.269	10.841	10,841	,269
2 M	247	8.52	48.82	.293	2.496	13.337	.273
SIZ	184	6.35	55.17	.298	1.892	15.229	.276
3 BK	70	2.42	57.59	.369	0.893	16.122	.280
2 BK	90	3.11	60.70	.380	1.182	17.304	. 285
3 M	95	3.28	63.98	.393	1.289	18.593	.291
1 BK	127	4.38	68.36	.418	1.831	20.424	.299
4 BK	38	1.31	69.67	.429	0.562	20.986	.301
5 BK	39	1.35	71.02	.557	0.752	21.738	.306
1 TA	11	0.38	71.40	.575	0.219	21.956	.308
4 M	42	1.45	72.35	.601	0.871	22.828	.313
5 M	15	0.52	73.37	1.085	0.564	23,392	.319
			PRE-BREA	K SIFTED			
1 M	1239	42.55	42.55	.284	12.084	12.084	.284
2 M	187	6.42	46.97	.308	1.977	14.062	.287
SIZ	195	6.70	55.67	.311	2.084	16.145	.290
3 BK	76	2.61	58.28	.354	0.924	17.069	.293
2 BK	89	3.06	61.34	.360	1.102	18.171	.296
1 BK	114	3.91	65.25	.398	1.556	19.727	.302
3 M	87	2.99	68.24	.410	1.226	20.953	.307
4 BK	38	1.30	69.54	.448	0.582	21.535	.310
1 TA	12	0.41	69.95	,540	0.221	21.757	.311
P BK	5	0.17	70.12	.600	0.102	21,859	.312
5 BK	43	1.48	71.60	.601	0.889	22.748	.318
4 M	46	1.58	73.18	.728	1.150	23.898	.327
5 M	14	0.48	73.66	1.627	0.781	24.679	.335

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)
Q=QUANTITY (% of Total Products).
S=SUMMATION

MILL ROSS FLOW
TEST D
WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	QXA	S of QXA	S of QX
		5M/G	PRE-BREAK	NOT SIFT	ED		
1 M	1203	41.89	41.89	.274	11.748	11.748	.274
2 M	197	6.86	48.75	.296	2.031	13.508	.277
SIZ	212	7.38	56.13	.300	2.214	15.722	.280
3 BK	76	2.65	58.78	.369	0.978	16.700	. 284
2 BK	88	3.06	61.84	.388	1.187	17.888	.289
3 M	84	2.92	64.76	.392	1.145	19.032	.294
1 BK	124	4.32	69.08	.422	1.823	20.855	.302
4 BK	34	1.18	70.26	.432	0.510	21.365	.304
1 TA	11	0.38	70.64	.555	0.211	21.576	.305
5 BK	45	1.57	72.21	.632	0.992	22.568	.313
4 M	44	1.53	73.74	.641	0.981	23.549	.319
5 M	15	0.52	74.26	1.415	0.736	24.285	.327
	22		NO PRE	-BREAK			
1 M	1187	41.09	41.09	.279	11.464	11.464	.279
SIZ	213	7.37	48.46	.302	2.226	13.690	.283
2 M	221	7.65	56.11	.328	2.509	16.199	.289
3 BK	72	2.49	58.60	.379	.994	17.193	.293
2 BK	81	2.80	61.40	.406	1.137	18.330	.299
3 M	89	3.08	64.48	.441	1.358	19.688	.305
4 BK	36	1.25	65.73	.450	0.563	20.251	.308
1 BK	106	3.67	69.40	.487	1.787	22,038	.318
1 TA	11	0.38	69.78	.608	0.231	22.269	.319
5 BK	36	1.25	71.03	.625	0.781	23.050	.325
4 M	47	1.63	72.66	.717	1.169	24.219	.333
5 M	18	0.62	73.28	1.402	0.869	25.088	.342
				K SIFTED			
1 M	1199	41.56	41.56	.266	11.055	11.055	.266
SIZ	216	7.49	49.05	.290	2.172	13.227	.270
2M	206	7.14	56.19	.300	2.142	15.369	.274
3 BK	78	2.70	58.89	.367	0.991	16.360	.278
2 BK	94	3.26	62.15	.376	1.226	17.586	.283
1 BK	116	4.02	66.17	.410	1.648	19.234	.291
3 M	75	2.60	68.77	.417	1.084	20.318	.295
4 BK	35	1.21	69.98	.452	0.547	20.865	.298
1 TA	9	0.31	70.29	.562	0.174	21.039	.299
5 BK	32	1.11	71.40	.575	0.638	21.677	.304
P BK	. 4	0.14	71.54	.614	0.086	21.763	.304
4 M	38	1.32	72.86	.666	0.879	22.642	.311
5 M	14	0.49	73.35	1.446	0.709	23.351	.318

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL ROSS FLOW
TEST E
WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	QXA	S of QXA	S of QXA
*****	CONTRACTOR OF STREET		PRE-BREA	K SIFTED			
1 M	1232	42.03	42.03	.264	11.096	11.096	.264
SIZ	209	7.13	49.16	.288	2.053	13.149	.267
2 M	180	6.14	55.30	.293	1.799	14.948	.270
3 BK	79	2.70	58.00	.357	0.964	15.912	.274
3 M	79	2.70	60.70	.375	1.013	16.925	.279
2 BK	92	3.14	63.84	.378	1.187	18.112	.284
1 BK	113	3.86	67.70	.415	1.602	19.714	.291
4 BK	35	1.19	68.89	.421	0.501	20.215	.293
1 TA	12	0.41	69.30	.544	0.223	20.433	.295
5 BK	35	1.19	70.49	.566	0.674	21.111	.299
P BK	6	0.20	70.69	.600	0.120	21.231	.300
4 M	56	1.91	72.60	.636	1.215	22.446	.309
5 M	15	0.51	73.11	1.263	0.644	23.090	.316
			NO PRE	-BREAK			
1 M	1163	39.69	39.69	.266	10.558	10.558	.266
SIZ	182	6.21	45.90	.316	1.962	12.520	.273
2 M	251	8.57	54.47	.316	2.708	15.228	.280
3 M	84	2.87	57.34	.373	1.071	16.299	.284
3 BK	76	2.59	59.93	.382	0.989	17.288	.288
2 BK	88	3.00	62.93	.397	1.191	18.479	.294
4 BK	31	1.06	63.99	.449	0.476	18.955	.296
1 BK	107	3.65	67.64	.494	1.803	20.758	.307
4 M	67	2,29	69.93	.576	1.319	22.077	.316
1 TA	17	0.58	70.51	.586	0.340	22.417	.318
5 BK	41	1.40	71.91	.637	0.892	23.309	.324
5 M	27	0.92	72.83	1.057	0.972	24.281	.333
			PRE-BREAK		THE RESERVE AND ADDRESS OF THE PARTY OF THE	·	
1 M	1166	39.86	39.86	.267	10.643	10.643	.267
SIZ	202	6.91	46.77	.288	1.990	12.633	.270
2 M	243	8.31	55.08	.300	2.493	15.126	.275
3 BK	76	2.60	57.68	.364	0.946	16.072	.279
2 BK	102	3.49	61.17	.378	1.319	17.391	.284
3 M	77	2.63	63.80	.394	1.036	18.428	.289
1 BK	124	4.24	68.04	.415	1.760	20.187	.297
4 BK	40	1.37	69.41	.417	0.571	20.758	.299
5 BK	27	0.92	70.33	.523	0.481	21.240	.302
4 M	43	1.47	71.80	.580	0.853	22.092	.308
1 TA	12	0.41	72.21	.588	0.241	22.333	.309
5 M	18	0.62	72.83	1.081	0.670	23.003	.316

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)

Q=QUANTITY (% of Total Products)

S=SUMMATION

M

MILL ROSS FLOW
TEST F
WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QXA
			NO PRE	-BREAK			
1 M	1094	37.07	37.07	.277	10.268	10.268	.277
2 M	288	9.76	46.83	.299	2.918	13.187	.282
SIZ	220	7.46	54.29	.311	2.320	15.507	.286
3 BK	69	2.34	56.63	.381	0.892	16.398	.290
3 M	114	3.86	60.49	.382	1.475	17.873	.295
2 BK	85	2.88	63.37	.411	1.184	19.056	.301
4 BK	34	1.15	64.52	.417	0.480	19.536	.303
1 BK	111	3.76	68.28	.501	1.884	21.420	.314
4 M	55	1.86	70.14	.554	1.030	22.450	.320
1 TA	15	0.51	70.65	.569	0.290	22.740	.322
5 BK	41	1.39	72.04	.598	0.831	23.572	.327
5 M	24	0.81	72.85	1.014	0.821	24.393	.335
	Kanada Ingaran		PRE-BREA	K SIFTED			
1 M	1119	38.14	38.14	.254	9.688	9.688	.254
SIZ	213	7.26	45.40	.277	2.011	11.699	. 258
2 M	271	9.24	54.64	.279	2.578	14.277	.261
3 BK	76	2.59	57.23	.351	0.909	15.186	.265
3 M	89	3.03	60.26	.356	1.079	16.264	.270
2 BK	91	3.10	63.36	.386	1.197	17.461	.276
4 BK	36	1.23	64.59	.411	0.506	17.966	.278
1 BK	120	4.09	68.68	.412	1.639	19.656	.286
1 TA	11	0.37	69.05	.502	0.186	19.841	.287
4 M	45	1.53	70.58	.537	0.822	20.663	.293
5 BK	46	1.57	72.15	.581	0.912	21.575	.299
P BK	6	0.20	72.35	.646	0.129	21.704	.300
5 M	21	0.72	73.07	.939	0.676	22.380	.306
	The state of the s	5-25	PRE-BREAK	NOT SIFT	ED		
1 M	1142	38.94	38.94	.261	10.163	10.163	.261
SIZ	180	6.14	45.08	.292	1.793	11.956	.265
2 M	297	10.13	55.21	.292	2.958	14.914	.270
3 BK	86	2.93	58.14	.356	1.043	15.957	.274
2 BK	90	3.07	61.21	.374	1.148	17.105	.279
3 M	76	2.59	63.80	.398	1.031	18.136	.284
1 BK	129	4.40	68.20	.413	1.817	19.953	.293
4 BK	35	1,19	69.39	.423	0.503	20.456	.295
1 TA	15	0.51	69.90	.583	0.297	20.753	.297
4 M	45	1.53	71.43	.597	0.913	21.666	.303
5 BK	41	1.40	72.83	.679	0.951	22.617	.311
5 M	18	0.61	73.44	1.073	0.655	23.272	.317

A=ASH(14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL ROSS FLOW
TEST G
WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	QXA	S of QXA	S of QXA
			PRE-BREAK	NOT SIFT	ED		
1 M	1072	36.62	36.62	.274	10.034	10.034	.274
2 M	344	11.75	48.37	.294	3.455	13.488	.279
SIZ	192	6.56	54.93	.298	1.955	15.443	.281
3 BK	85	2,90	57.83	.363	1.053	16.496	.285
3 M	83	2.84	60.67	.381	1.082	17.578	.290
2 BK	93	3.18	63.85	.383	1,218	18.796	.294
1 BK	129	4.41	68.26	.423	1.865	20,661	.303
4 BK	47	1.61	69.87	.434	0.699	21,360	.306
1 TA	13	0.44	70.31	.561	0.247	21.607	.307
4 M	44	1.50	71.81	.617	0.926	22.532	.314
5 BK	26	0.89	72.70	.686	0.611	23.143	.318
5 M	16	0.55	73.25	1.039	0.571	23.714	.324
	र्युः ६ व		PRE-BREA	K SIFTED			
1 M	1180	40.15	40.15	.262	10.519	10.519	.262
SIZ	184	6.26	46.41	.288	1.803	12.322	.266
2 M	263	8.95	55.36	.306	2.739	15.061	.272
3 BK	91	3.10	58.46	.356	1.104	16.164	.277
2 BK	91	3.10	61.56	.368	1.141	17.305	.281
3 M	69	2.35	63.91	.387	0.909	18.215	.285
1 BK	112	3.81	67.72	.413	1.574	19.788	.292
4 BK	40	1.36	69.08	.432	0.588	20.376	.295
1 TA	11	0.37	69.45	.516	0.191	20.567	.296
P BK	6	0.20	69.65	.576	0.115	20.682	.297
4 M	49	1.67	71.32	.661	1.104	21.786	.305
5 BK	42	1,43	72,75	.680	0.972	22.758	.313
5 M	17	0.58	73.33	1.319	0.765	23.523	.321
			NO PRE	-BREAK			
1 M	1194	40.63	40.63	.268	10.889	10.889	.268
SIZ	189	6.43	47.06	.312	2.006	12.895	.274
2 M	244	8.30	55.36	.325	2.698	15.593	.282
3 BK	78	2.65	58.01	.381	1.010	16.602	.286
2 BK	89	3.03	61.04	.401	1.215	17.817	.292
3 M	77	2.62	63.66	.433	1.134	18.952	.298
4 BK	33	1.12	64.78	.456	0.511	19,462	.300
1 BK	110	3.74	68.52	.492	1.840	21.302	.311
1 TA	17	0.58	69.10	.560	0.325	21.627	.313
5 BK	35	1.19	70.29	.579	0.689	22.316	.317
4 M	53	1.80	72.09	.606	1.091	23.407	.325
5 M	20	0.68	72.77	1.279	0.870	24.277	.334

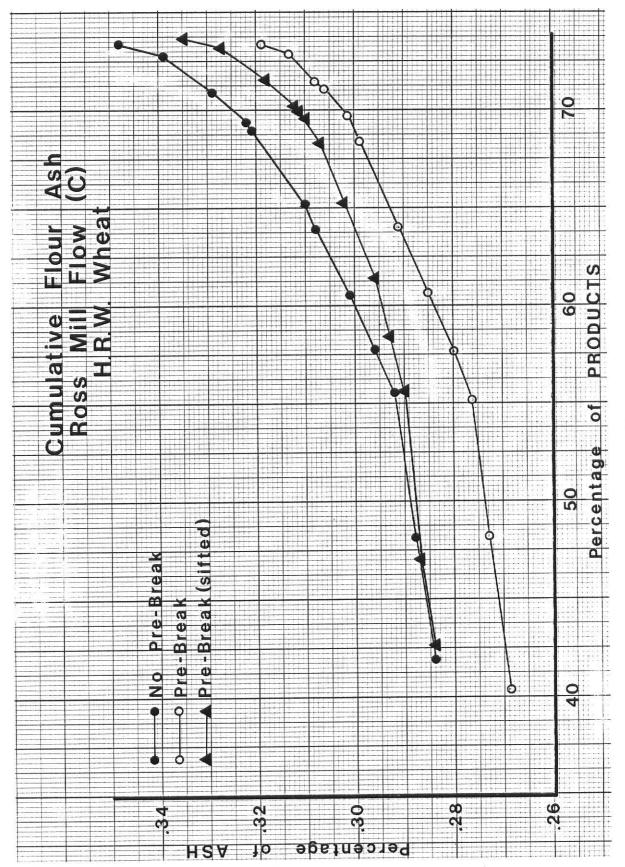
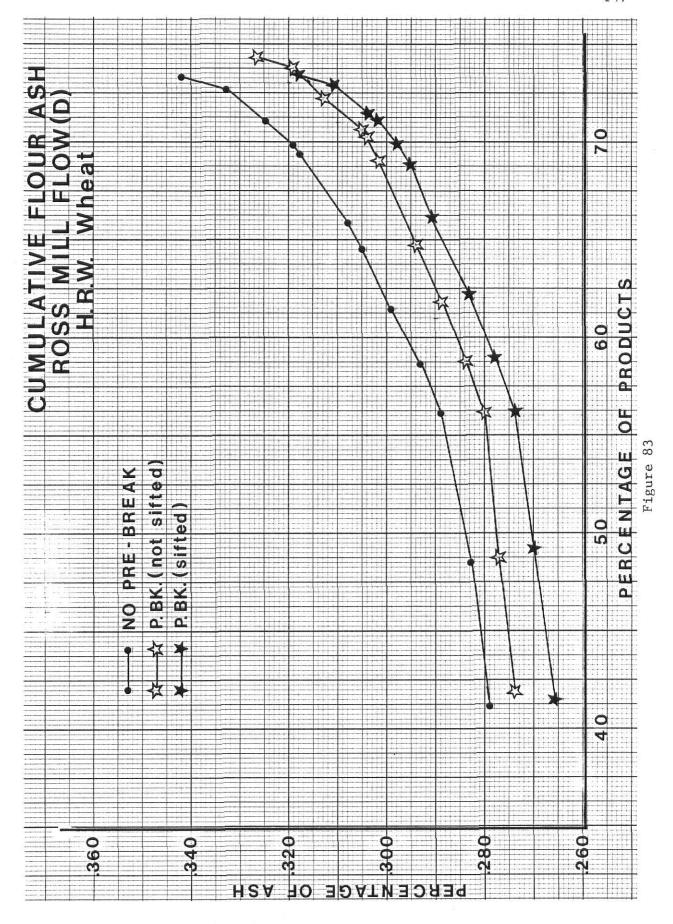
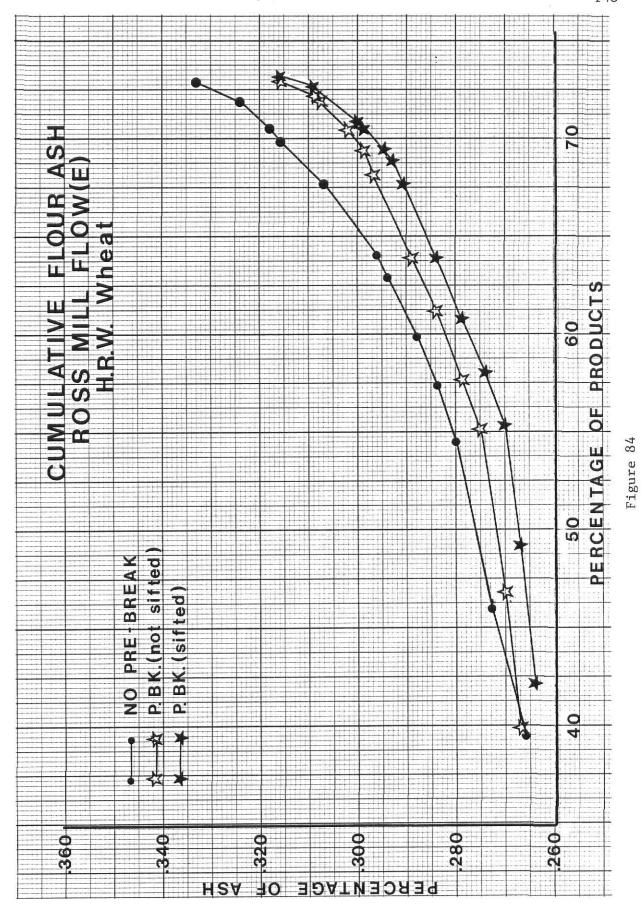


Figure 82





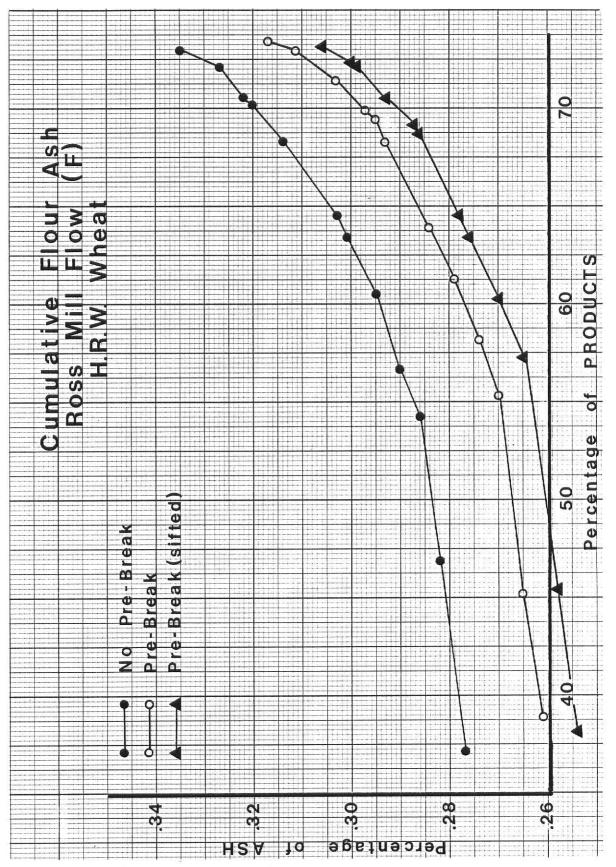


Figure 85

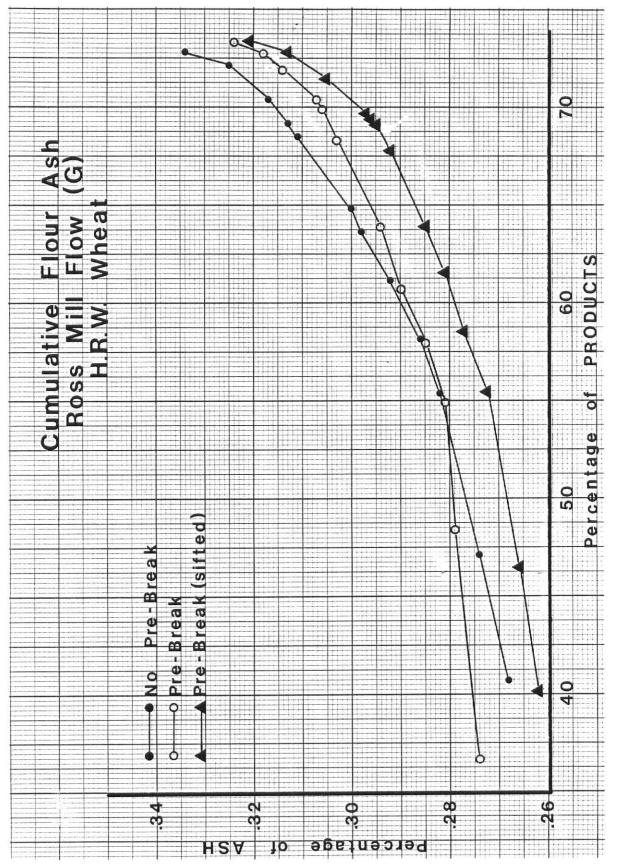
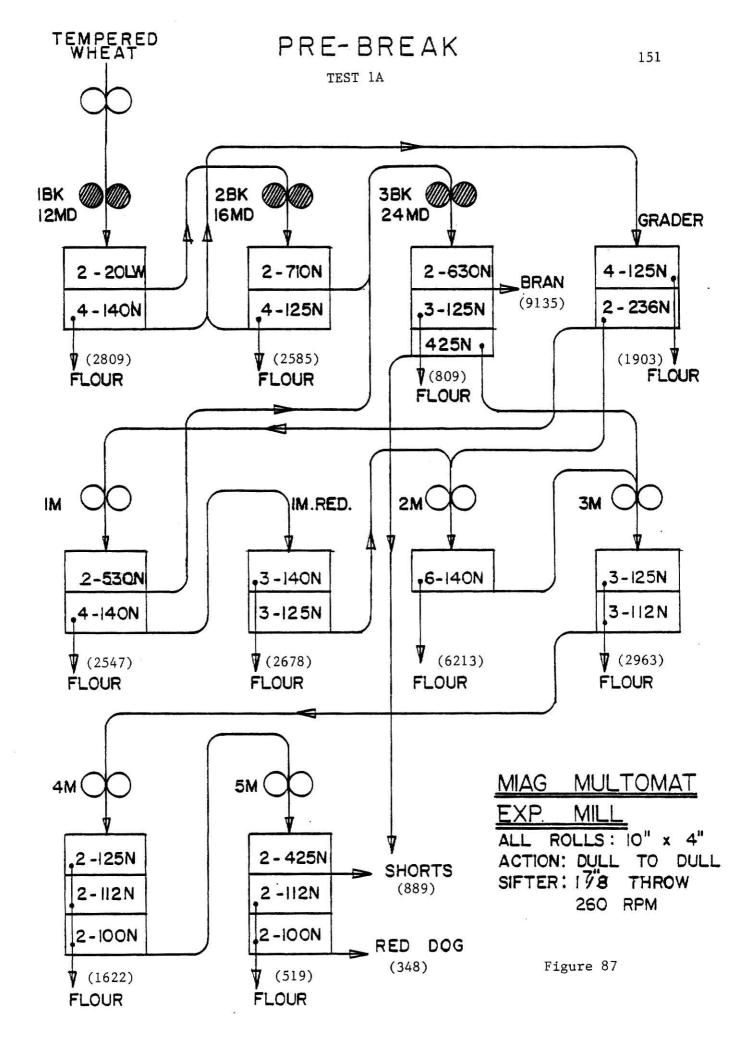


Figure 86



(316)

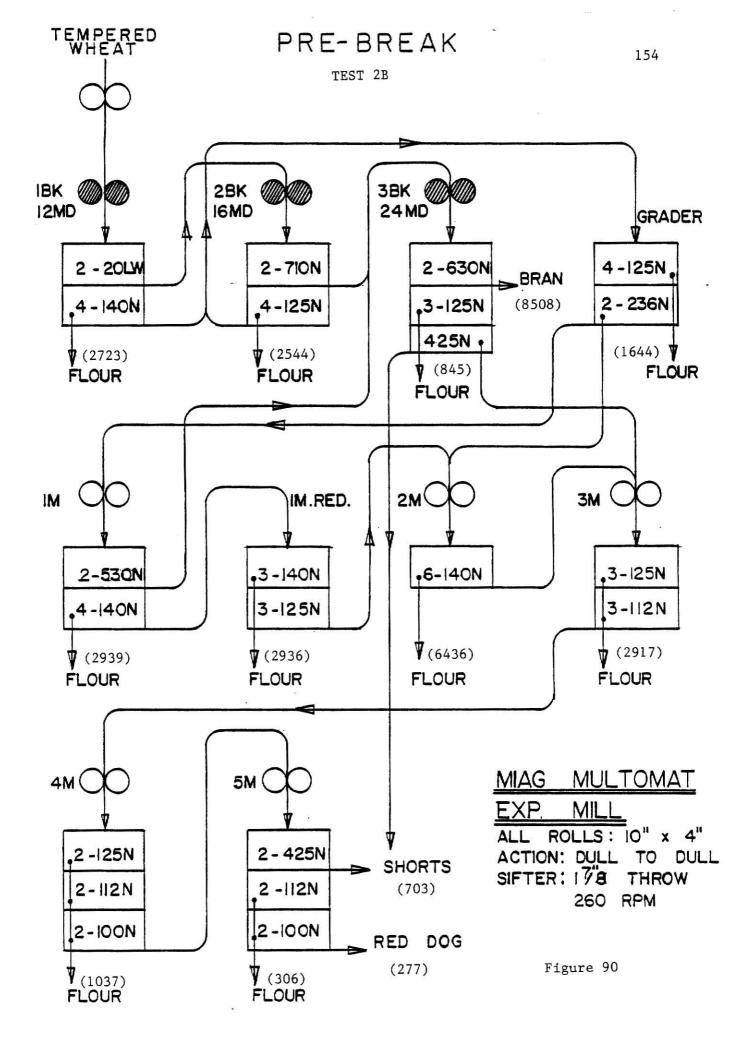
V (487)

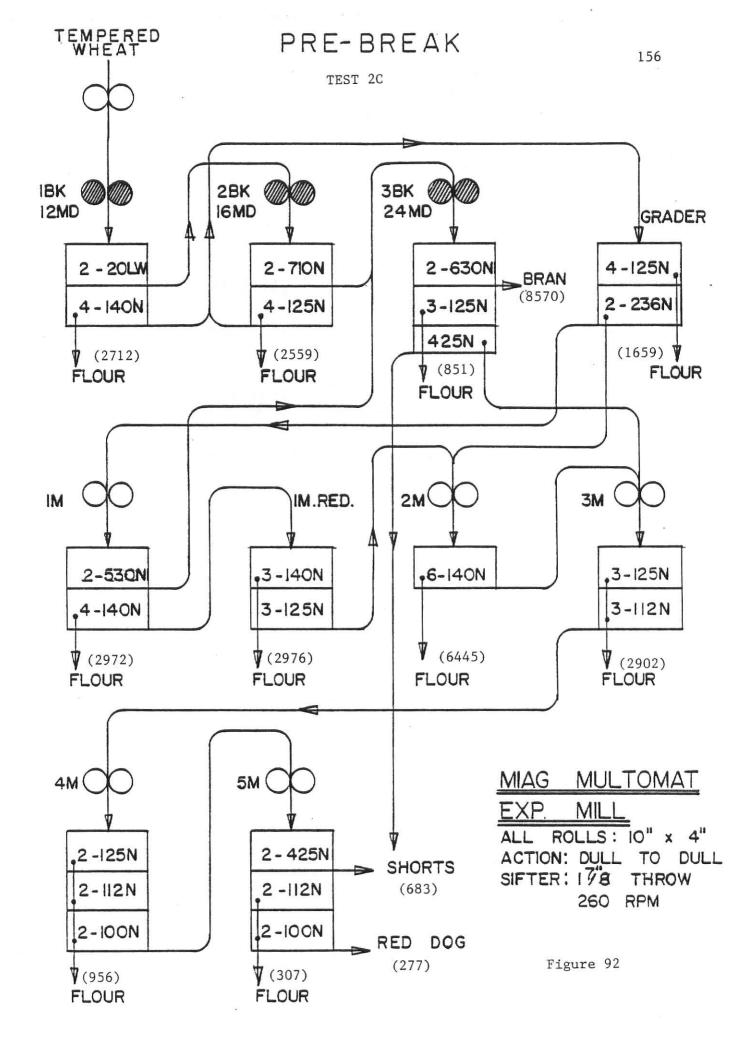
FLOUR

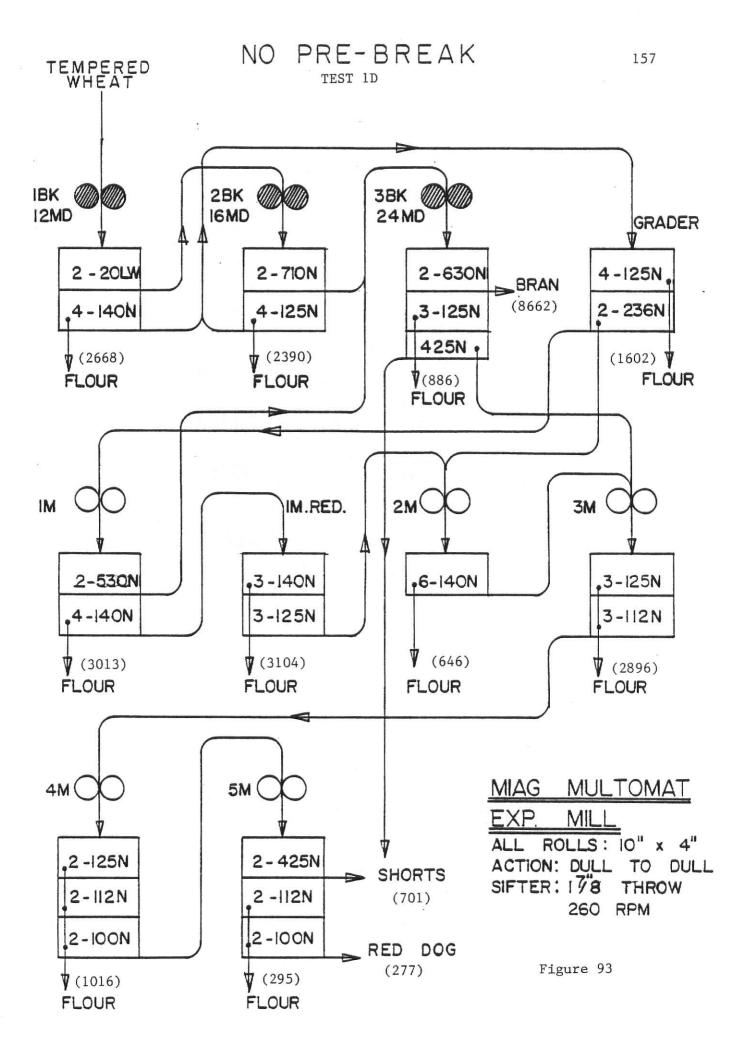
V (1557)

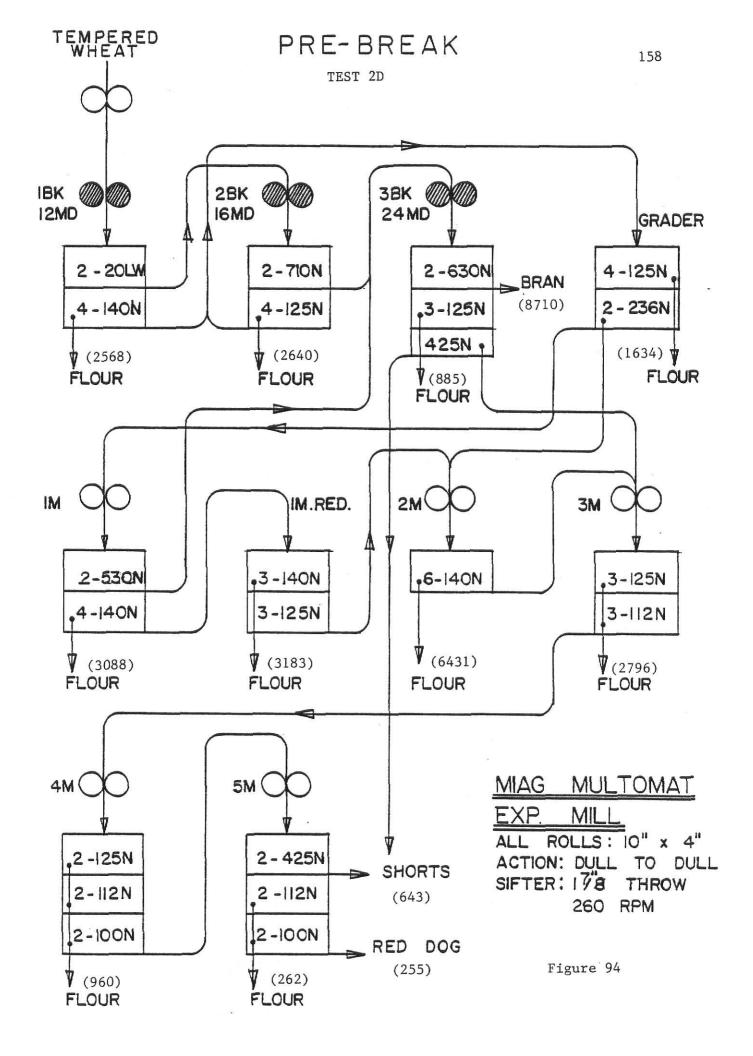
FLOUR

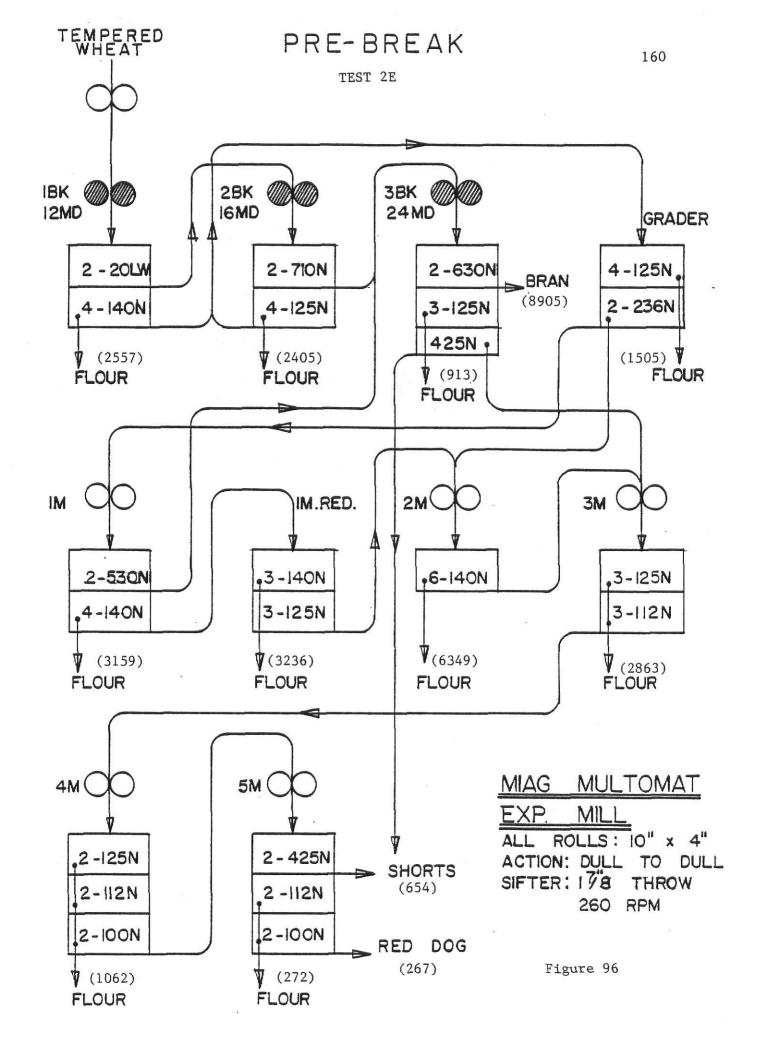
Figure 88











Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)

Q=QUANTITY (% of Total Products)

S = SUMMATION

MILL MIAG MULTOMAT
TEST A
HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	QXA	S of QXA	S of QXA
***************************************	Language De Maria de La Company		PRE-B	REAK			
1 M RED	2678	7.65	7.65	.261	1.997	1.997	.261
1 M	2547	7.27	14.92	.282	2.050	4.047	.271
2 M	6213	17.74	32.66	.291	5.162	9.209	.282
1 BK	2809	8.02	40.68	.305	2.446	11.655	.287
3 M	2963	8.46	49.14	.339	2.868	14.523	.296
2 BK	2585	7.38	56.52	.344	2.539	17.062	.302
GRADER	1903	5.43	61.95	.364	1.977	19.038	.307
4 M	1622	4.63	66.58	.378	1.750	20.789	.312
3 BK	809	2.31	68.89	.470	1.086	21.874	.318
5 M	519	1.48	70.37	1.181	1.748	23.622	.336
	5 Jan-19-19-19-19-19-19-19-19-19-19-19-19-19-			BREAK		-	
1 M RED	2702	7.43	7.43	.261	1.939	1.939	.261
2 M	6434	17.69	25.12	.280	4.953	6.892	.274
1 M	2671	7.34	32.46	.290	2.129	9.021	.278
3 M	3707	10.19	42.65	.328	3.342	12.363	.290
1 BK	2818	7.75	50.40	.334	2.589	14.952	.297
GRADER	1795	4.93	55.33	.353	1.740	16.692	.302
2 BK	2576	7.08	62.41	.354	2.506	19.198	.308
4 M	1557	4.28	66.69	.386	1.652	20.851	.313
3 BK	734	2.02	68.71	.456	0.921	21.772	.317
5 M	487	1.34	70.05	1.178	1.579	23.350	.333

A=ASH (14% Moisture Basis)

Q=QUANTITY (% of Total Products)

S = SUMMATION

MILL MIAG MULTOMAT
TEST B
HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QXA
The second secon			NO PRE	-BREAK			
1 M RED	3221	9.46	9.46	.261	2.469	2.469	.261
2 M	6383	18.75	28.21	.280	5.250	7.719	.274
1 M	3347	9.83	38.04	.281	2.762	10.481	.276
2 BK	2171	6.38_	44.42	.333	2.125	12,606	. 284
1 BK	2556	7.51	51.93	.344	2.583	15.189	.292
GRADER	1409	4.14	56.07	.352	1.457	16.647	.297
3 M	2863	8.41	64.48	.359	3.019	19.666	.305
3 BK	1037	3.05	67.53	.449	1.369	21.035	.311
4 M	1004	2.95	70.48	.457	1.348	22.383	.318
5 M	296	0.87	71.35	1.667	1.450	23.834	.334
1 1/ 222	0000	0.70	PRE-E		2.248	2.248	.259
1 M RED	2936	8.68	8.68	.259	5.309	7,557	.273
2 M	6436	19.03	27.71	.279	2.425	9.982	.274
1 M	2939	8.69	36.40	.279	2.423	12.655	.285
1 BK	2723	8.05	44.45	.332	2.572	15.226	.293
2 BK	2544	7.52	51.97	.342	1.711	16.937	.298
GRADER	1644	4.86	56.83	.352	3.150	20.087	.307
3 M	2917	8.63	65.46	.365		21.533	.314
4 M	1037	3.07	68.53	.471	1.446	22.748	.320
3 BK 5 M	845 306	2.50 0.90	71.03	1.747	1,215	24.320	.338
				A			
- Maller							

A=ASH (14% Moisture Basis)

Q=QUANTITY (% of Total Products) S=SUMMATION

MIAG MULTOMAT MILL C **TEST** WHEAT_ HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	QXA	S of QXA	S of QXA
			NO PRE	-BREAK			
2 M	6205	18.30	18.30	.279	5.106	5.106	.279
1 M RED	3124	9.22	27.52	.280	2.582	7.688	.279
1 M	3039	8.96	36.48	.290	2.598	10.286	.282
1 BK	2627	7.75	44.23	.344	2.666	12.952	.293
2 BK	2279	6.72	50.95	.363	2,439	15.391	.302
GRADER	1504	4.44	55.39	.372	1.652	17.043	.308
3 M	3068	9.05	64.44	.386	3.493	20.536	.319
4 M	1103	3.25	67.69	.473	1.537	22.073	.326
3 BK	959	2.83	70.52	.487	1.378	23.451	.333
5 M	367	1.08	71.60	1.565	1.690	25.141	.351
				=======================================			
1 1/	1 2072 1	0 77	PRE-B		1 0 050	1 2 252	0.00
1 M	2972	8.77	8.77	.269	2.359	2.359	.269
1 M RED	2976	8.79	17.56	.269	2.365	4.724	.269
2 M	6445	19.03	36.59	.278	5.290	10.014	.274
1 BK	2712	8.01	44.60	.333	2.667	12.681	.284
GRADER	1659	4.90	49.50	.340	1.666	14.347	.290
2 BK	2559	7.56	57.06	.343	2.593	16.940	.297
3 M	2902	8.57	65.63	.375	3.214	20.154	.307
3 BK	851	2.51	68.14	.479	1.202	21.356	.313
4 M	956	2.82	70.96	.491	1.385	21.741	.320
5 M	307	0.91	71.87	1.720	1.565	23.306	.324
		n en					
awadan.				. Latin and April Art I I and			
The second secon							

Cumulative Flour Ash Calculations

A=ASH(I4% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL MIAG MULTOMAT
TEST D
WHEAT HARD RED WINTER

2 M 6461 19.02 28.16 .268 5.097 7.465 .26 1 M 3013 8.87 37.03 .279 2.475 9.939 .26 1 BK 2668 7.85 44.88 .333 2.614 12.553 .28 2 BK 2390 7.04 51.92 .341 2.401 14.954 .28 GRADER 1602 4.72 56.64 .350 1.652 16.606 .29 3 M 2896 8.52 65.16 .365 3.110 19.716 .30 3 BK 886 2.61 67.77 .474 1.237 20.953 .30 4 M 1016 2.99 70.76 .509 1.522 22.475 .31 5 M 295 0.87 71.63 1.933 1.682 24.157 .33 PRE-BREAK 1 M RED 3183 9.35 18.42 .268 2.506 4.755 .25	2 M 1 M 1 BK 2 BK	3104 6461 3013	19.02	9.14	-		A STATE OF THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER. THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER.	SofQ
2 M 6461 19.02 28.16 .268 5.097 7.465 .26 1 M 3013 8.87 37.03 .279 2.475 9.939 .26 1 BK 2668 7.85 44.88 .333 2.614 12.553 .28 2 BK 2390 7.04 51.92 .341 2.401 14.954 .28 GRADER 1602 4.72 56.64 .350 1.652 16.606 .29 3 M 2896 8.52 65.16 .365 3.110 19.716 .30 3 BK 886 2.61 67.77 .474 1.237 20.953 .30 4 M 1016 2.99 70.76 .509 1.522 22.475 .31 5 M 295 0.87 71.63 1.933 1.682 24.157 .33 PRE-BREAK 1 M RED 3183 9.35 18.42 .268 2.506 4.755 .25	2 M 1 M 1 BK 2 BK	6461 3013	19.02	The second second	259			
1 M 3013 8.87 37.03 .279 2.475 9.939 .26 1 BK 2668 7.85 44.88 .333 2.614 12.553 .28 2 BK 2390 7.04 51.92 .341 2.401 14.954 .28 GRADER 1602 4.72 56.64 .350 1.652 16.606 .29 3 M 2896 8.52 65.16 .365 3.110 19.716 .30 3 BK 886 2.61 67.77 .474 1.237 20.953 .30 4 M 1016 2.99 70.76 .509 1.522 22.475 .31 5 M 295 0.87 71.63 1.933 1.682 24.157 .33 2 M 6431 18.88 37.30 .287 5.419 10.174 .27 1 BK 2568 7.54 44.84 .333 2.511 12.685 .28 GRADER 1634 4	1 M 1 BK 2 BK	3013		29 16	0 4 3 3	2.367	2.367	.259
1 M 3013 8.87 37.03 .279 2.475 9.939 .26 1 BK 2668 7.85 44.88 .333 2.614 12.553 .28 2 BK 2390 7.04 51.92 .341 2.401 14.954 .28 GRADER 1602 4.72 56.64 .350 1.652 16.606 .29 3 M 2896 8.52 65.16 .365 3.110 19.716 .30 3 BK 886 2.61 67.77 .474 1.237 20.953 .30 4 M 1016 2.99 70.76 .509 1.522 22.475 .31 5 M 295 0.87 71.63 1.933 1.682 24.157 .33 PRE-BREAK 1 M RED 3183 9.35 18.42 .268 2.506 4.755 .25 2 M 6431 18.88 37.30 .287 5.419 10.174 .27	1 M 1 BK 2 BK		8 87	20.10	.268	5.097	7.465	.265
1 BK 2668 7.85 44.88 .333 2.614 12.553 .28 2 BK 2390 7.04 51.92 .341 2.401 14.954 .28 GRADER 1602 4.72 56.64 .350 1.652 16.606 .29 3 M 2896 8.52 65.16 .365 3.110 19.716 .30 3 BK 886 2.61 67.77 .474 1.237 20.953 .30 4 M 1016 2.99 70.76 .509 1.522 22.475 .31 5 M 295 0.87 71.63 1.933 1.682 24.157 .33 PRE-BREAK 1 M RED 3183 9.35 18.42 .268 2.506 4.755 .25 2 M 6431 18.88 37.30 .287 5.419 10.174 .27 1 BK 2568 7.54 44.84 .333 2.511 12.685 .28 <t< td=""><td>1 BK 2 BK</td><td></td><td>0.07</td><td>37.03</td><td>.279</td><td>2.475</td><td>9.939</td><td>.268</td></t<>	1 BK 2 BK		0.07	37.03	.279	2.475	9.939	.268
2 BK 2390 7.04 51.92 .341 2.401 14.954 .28 GRADER 1602 4.72 56.64 .350 1.652 16.606 .29 3 M 2896 8.52 65.16 .365 3.110 19.716 .30 3 EK 886 2.61 67.77 .474 1.237 20.953 .30 4 M 1016 2.99 70.76 .509 1.522 22.475 .31 5 M 295 0.87 71.63 1.933 1.682 24.157 .33 PRE-BREAK 1 M RED 3183 9.35 18.42 .268 2.506 4.755 .25 2 M 6431 18.88 37.30 .287 5.419 10.174 .27 1 BK 2568 7.54 44.84 .333 2.511 12.685 .28 GRADER 1634 4.80 49.64 .349 1.675 14.360 .28	2 BK		7.85	44.88	.333	2.614	12.553	.280
GRADER 1602 4.72 56.64 .350 1.652 16.606 .29 3 M 2896 8.52 65.16 .365 3.110 19.716 .30 3 BK 886 2.61 67.77 .474 1.237 20.953 .30 4 M 1016 2.99 70.76 .509 1.522 22.475 .31 5 M 295 0.87 71.63 1.933 1.682 24.157 .33 PRE-BREAK 1 M RED 3183 9.35 18.42 .268 2.506 4.755 .25 2 M 6431 18.88 37.30 .287 5.419 10.174 .27 1 BK 2568 7.54 44.84 .333 2.511 12.685 .28 GRADER 1634 4.80 49.64 .349 1.675 14.360 .28 2 BK 2640 7.75 57.39 .352 2.728 17.088 .29		2390		51.92		2.401	14.954	.288
3 M 2896 8.52 65.16 .365 3.110 19.716 .30 3 BK 886 2.61 67.77 .474 1.237 20.953 .30 4 M 1016 2.99 70.76 .509 1.522 22.475 .31 5 M 295 0.87 71.63 1.933 1.682 24.157 .33 PRE-BREAK 1 M 3088 9.07 9.07 .248 2.249 2.249 .24 1 M RED 3183 9.35 18.42 .268 2.506 4.755 .25 2 M 6431 18.88 37.30 .287 5.419 10.174 .27 1 BK 2568 7.54 44.84 .333 2.511 12.685 .28 GRADER 1634 4.80 49.64 .349 1.675 14.360 .28 2 BK 2640 7.75 57.39 .352 2.728 17.088 .29 3 M 2796 8.21 65.60 .364 2.988 20.076	GRADER 1					1.652	16.606	.293
3 BK 886 2.61 67.77 .474 1.237 20.953 .30 4 M 1016 2.99 70.76 .509 1.522 22.475 .31 5 M 295 0.87 71.63 1.933 1.682 24.157 .33 PRE-BREAK 1 M 3088 9.07 9.07 .248 2.249 2.249 .24 1 M RED 3183 9.35 18.42 .268 2.506 4.755 .25 2 M 6431 18.88 37.30 .287 5.419 10.174 .27 1 BK 2568 7.54 44.84 .333 2.511 12.685 .28 GRADER 1634 4.80 49.64 .349 1.675 14.360 .28 2 BK 2640 7.75 57.39 .352 2.728 17.088 .29 3 M 2796 8.21 65.60 .364 2.988 20.076 .30 3 BK 885 2.60 68.20 .474 1.232 21.309 <td< td=""><td>THE REAL PROPERTY AND ADDRESS OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN</td><td></td><td>THE RESERVE THE PERSON NAMED IN COLUMN TWO</td><td>The second secon</td><td>The state of the s</td><td></td><td>THE RESERVE OF THE PARTY OF THE</td><td>.303</td></td<>	THE REAL PROPERTY AND ADDRESS OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN		THE RESERVE THE PERSON NAMED IN COLUMN TWO	The second secon	The state of the s		THE RESERVE OF THE PARTY OF THE	.303
4 M 1016 2.99 70.76 .509 1.522 22.475 .31 PRE-BREAK 1 M 3088 9.07 9.07 .248 2.249 2.249 .24 1 M RED 3183 9.35 18.42 .268 2.506 4.755 .25 2 M 6431 18.88 37.30 .287 5.419 10.174 .27 1 BK 2568 7.54 44.84 .333 2.511 12.685 .28 GRADER 1634 4.80 49.64 .349 1.675 14.360 .28 2 BK 2640 7.75 57.39 .352 2.728 17.088 .29 3 M 2796 8.21 65.60 .364 2.988 20.076 .30 3 BK 885 2.60 68.20 .474 1.232 21.309 .31 4 M 960 2.82 71.02 .538 1.517 22.826 .32				67.77	.474	1.237	20.953	.309
PRE-BREAK 1 M 3088 9.07 9.07 .248 2.249 2.249 .24 1 M RED 3183 9.35 18.42 .268 2.506 4.755 .25 2 M 6431 18.88 37.30 .287 5.419 10.174 .27 1 BK 2568 7.54 44.84 .333 2.511 12.685 .28 GRADER 1634 4.80 49.64 .349 1.675 14.360 .28 2 BK 2640 7.75 57.39 .352 2.728 17.088 .29 3 M 2796 8.21 65.60 .364 2.988 20.076 .30 3 BK 885 2.60 68.20 .474 1.232 21.309 .31 4 M 960 2.82 71.02 .538 1.517 22.826 .32	THE RESERVE THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO I			70.76	.509	1.522	22.475	.318
1 M 3088 9.07 9.07 .248 2.249 2.249 .24 1 M RED 3183 9.35 18.42 .268 2.506 4.755 .25 2 M 6431 18.88 37.30 .287 5.419 10.174 .27 1 BK 2568 7.54 44.84 .333 2.511 12.685 .28 GRADER 1634 4.80 49.64 .349 1.675 14.360 .28 2 BK 2640 7.75 57.39 .352 2.728 17.088 .29 3 M 2796 8.21 65.60 .364 2.988 20.076 .30 3 BK 885 2.60 68.20 .474 1.232 21.309 .31 4 M 960 2.82 71.02 .538 1.517 22.826 .32			The same of the sa			1.682	24.157	.337
1 M 3088 9.07 9.07 .248 2.249 2.249 .24 1 M RED 3183 9.35 18.42 .268 2.506 4.755 .25 2 M 6431 18.88 37.30 .287 5.419 10.174 .27 1 BK 2568 7.54 44.84 .333 2.511 12.685 .28 GRADER 1634 4.80 49.64 .349 1.675 14.360 .28 2 BK 2640 7.75 57.39 .352 2.728 17.088 .29 3 M 2796 8.21 65.60 .364 2.988 20.076 .30 3 BK 885 2.60 68.20 .474 1.232 21.309 .31 4 M 960 2.82 71.02 .538 1.517 22.826 .32		- H2						
1 M RED 3183 9.35 18.42 .268 2.506 4.755 .25 2 M 6431 18.88 37.30 .287 5.419 10.174 .27 1 BK 2568 7.54 44.84 .333 2.511 12.685 .28 GRADER 1634 4.80 49.64 .349 1.675 14.360 .28 2 BK 2640 7.75 57.39 .352 2.728 17.088 .29 3 M 2796 8.21 65.60 .364 2.988 20.076 .30 3 BK 885 2.60 68.20 .474 1.232 21.309 .31 4 M 960 2.82 71.02 .538 1.517 22.826 .32				PRE-I	BREAK			
2 M 6431 18.88 37.30 .287 5.419 10.174 .27 1 BK 2568 7.54 44.84 .333 2.511 12.685 .28 GRADER 1634 4.80 49.64 .349 1.675 14.360 .28 2 BK 2640 7.75 57.39 .352 2.728 17.088 .29 3 M 2796 8.21 65.60 .364 2.988 20.076 .30 3 BK 885 2.60 68.20 .474 1.232 21.309 .31 4 M 960 2.82 71.02 .538 1.517 22.826 .32	1 M	3088	9.07	9.07	.248	2.249	2.249	.248
1 BK 2568 7.54 44.84 .333 2.511 12.685 .28 GRADER 1634 4.80 49.64 .349 1.675 14.360 .28 2 BK 2640 7.75 57.39 .352 2.728 17.088 .29 3 M 2796 8.21 65.60 .364 2.988 20.076 .30 3 BK 885 2.60 68.20 .474 1.232 21.309 .31 4 M 960 2.82 71.02 .538 1.517 22.826 .32	1 M RED	3183	9.35	18.42	.268	2.506	4.755	.258
GRADER 1634 4.80 49.64 .349 1.675 14.360 .28 2 BK 2640 7.75 57.39 .352 2.728 17.088 .29 3 M 2796 8.21 65.60 .364 2.988 20.076 .30 3 BK 885 2.60 68.20 .474 1.232 21.309 .31 4 M 960 2.82 71.02 .538 1.517 22.826 .32	2 M	6431	18.88	37.30	.287	5.419	10.174	.273
2 BK 2640 7.75 57.39 .352 2.728 17.088 .29 3 M 2796 8.21 65.60 .364 2.988 20.076 .30 3 BK 885 2.60 68.20 .474 1.232 21.309 .31 4 M 960 2.82 71.02 .538 1.517 22.826 .32	1 BK	2568	7.54	44.84	.333	2.511	12.685	.283
2 BK 2640 7.75 57.39 .352 2.728 17.088 .29 3 M 2796 8.21 65.60 .364 2.988 20.076 .30 3 BK 885 2.60 68.20 .474 1.232 21.309 .31 4 M 960 2.82 71.02 .538 1.517 22.826 .32	GRADER	1634	4.80	49.64	.349	1.675	14.360	.289
3 M 2796 8.21 65.60 .364 2.988 20.076 .30 3 BK 885 2.60 68.20 .474 1.232 21.309 .31 4 M 960 2.82 71.02 .538 1.517 22.826 .32		2640	A STATE OF THE PERSON NAMED IN COLUMN 2 IS NOT THE OWNER.	57.39	.352	2,728	17.088	.298
3 BK 885 2.60 68.20 .474 1.232 21.309 .31 4 M 960 2.82 71.02 .538 1.517 22.826 .32	CONTRACTOR OF THE PARTY OF THE			65.60	.364	2.988	20.076	.306
4 M 960 2.82 71.02 .538 1.517 22.826 .32					.474	1.232	21.309	.312
						1.517	22.826	.321
	5 M	262	0.77	71,79		1.480	24.306	.339

Cumulative Flour Ash Calculations

A=ASH(14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL MIAG MULTOMAT
TEST
WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QXA
	Marky Arthur Daniel Commission		NO PRE	-BREAK			6
1 M RED	1866	7.99	7.99	.270	2.157	2.157	.270
1 M	1775	7.60	15.59	.278	2.113	4.270	.274
2 M	4016	17.20	32.79	.279	4.799	9.069	.277
1 BK	1874	8.03	40.82	.323	2.594	11.663	.286
3 M	2228	9.54	50.36	.327	3.120	14.782	.294
2 BK	1681	7.20	57.56	.342	2.462	17.245	.300
GRADER	1210	5.18	62.74	.353	1.829	19.073	.304
4 M	940	4.03	66.77	.386	1.556	20.629	.309
3 BK	538	2.30	69.07	. 455	1.047	21.675	.314
5 M	311	1.33	70.40	1.174	1.561	23.237	.330
			PRE-E	DEAU			
	0150	0.05			1 2 201	1 2 204	1 2/0
1 M	3159	9.25 9.48	9.25	.248	2.294	2.294 4.740	.248
1 M RED	3236		37.32	.265	4.926	9.666	.259
2 M	6349	18.59					A CONTRACTOR OF THE PARTY OF TH
1 BK	2557	7.49	44.81	.332	2.487	12.153	.271
GRADER	1505	4.41	49.22	.350	1.544	13.696	.278
2 BK	2405	7.04	56.26	.351	2.471	16.167	.287
3 M	2863	8.38	64.64	.373	3.126	19.293	.298
3 BK	913	2.67	67.31	.463	1.236	20.529	.305
4 M	1062	3.11	70.42	.536	1.667	22.196	.315
5 M	272	0.80	71.22	2.010	1.000	23,804	1

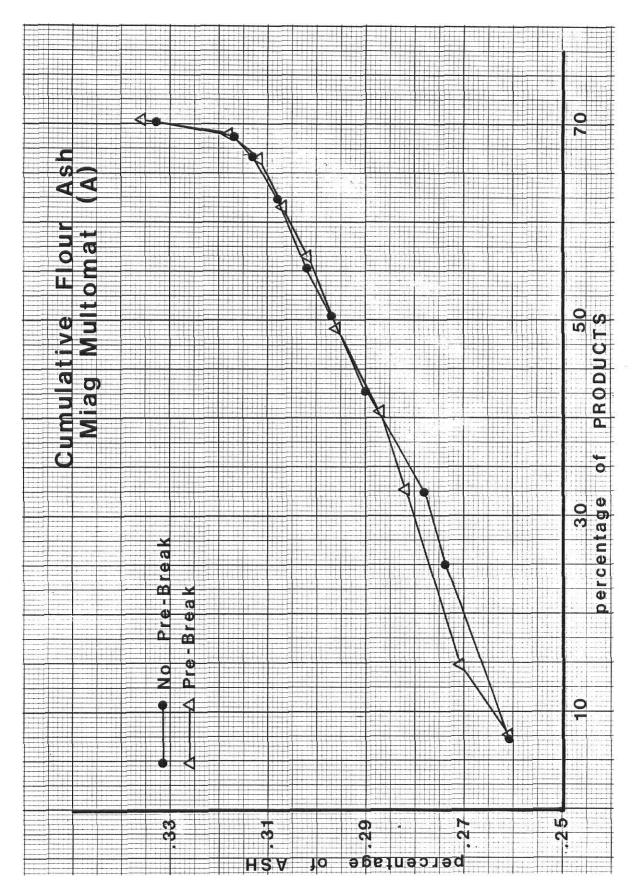


Figure 97

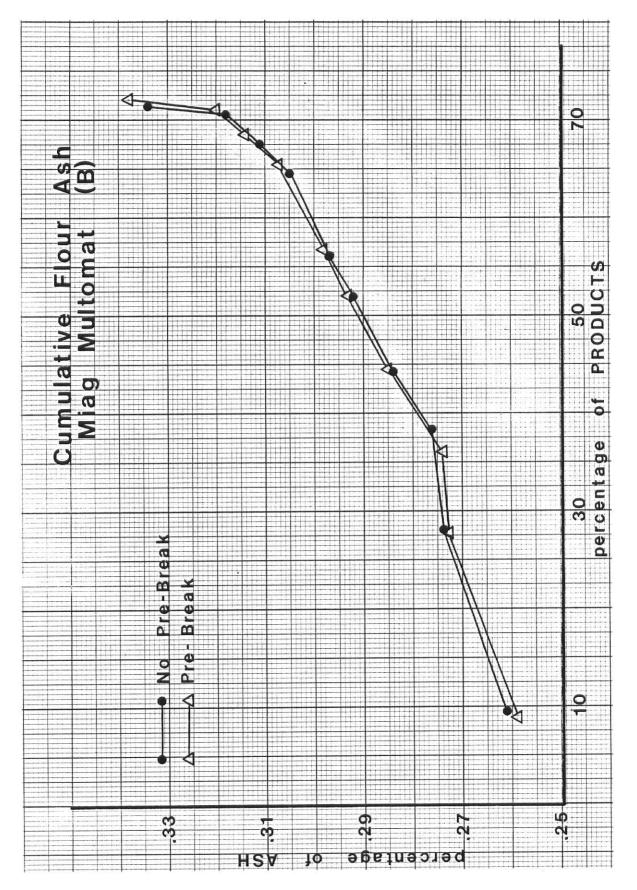


Figure 98

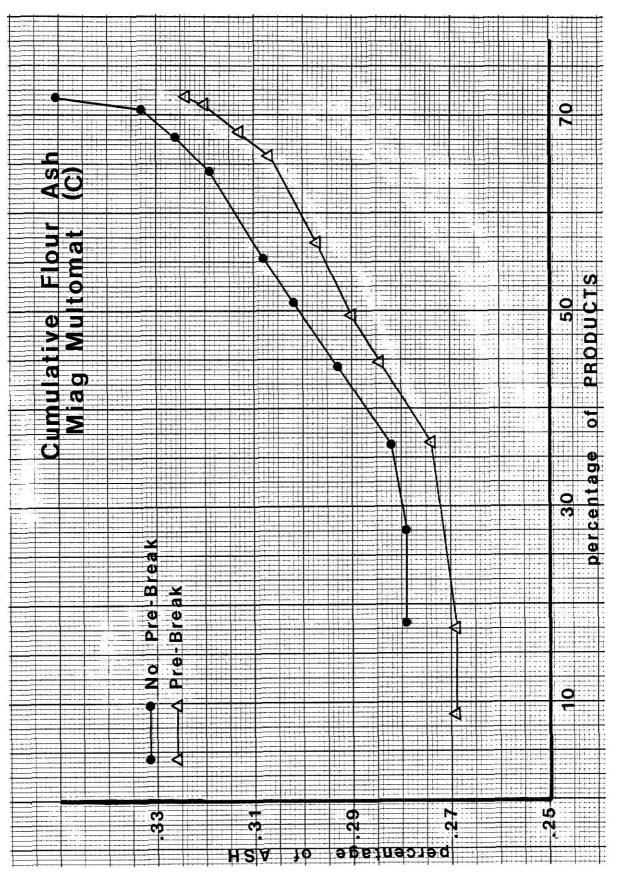
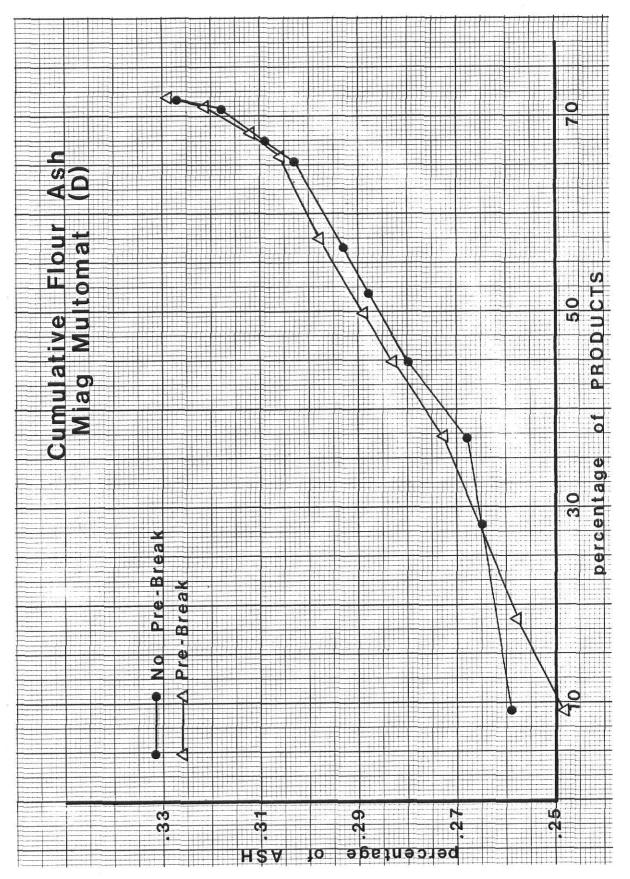
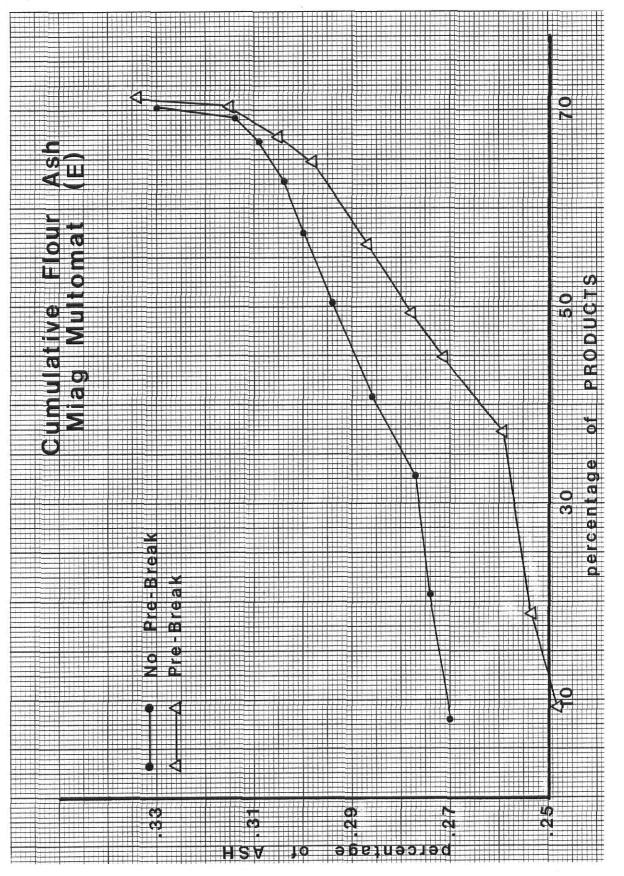


Figure 99



igure 100



igure 101

APPENDIX B

APPENDIX B

Preliminary Tests of Pre-Break on the Kansas State University Pilot Flour Mill

Preliminary testing of the use of Pre-Break on a large scale was initiated using the Kansas State University Pilot Flour Mill.

The KSU Pilot Mill has a capacity of approximately 200 hundredweights of flour in 24 hours. Although this is small in comparison to commercial mills, the equipment is scaled down to give comparable performance.

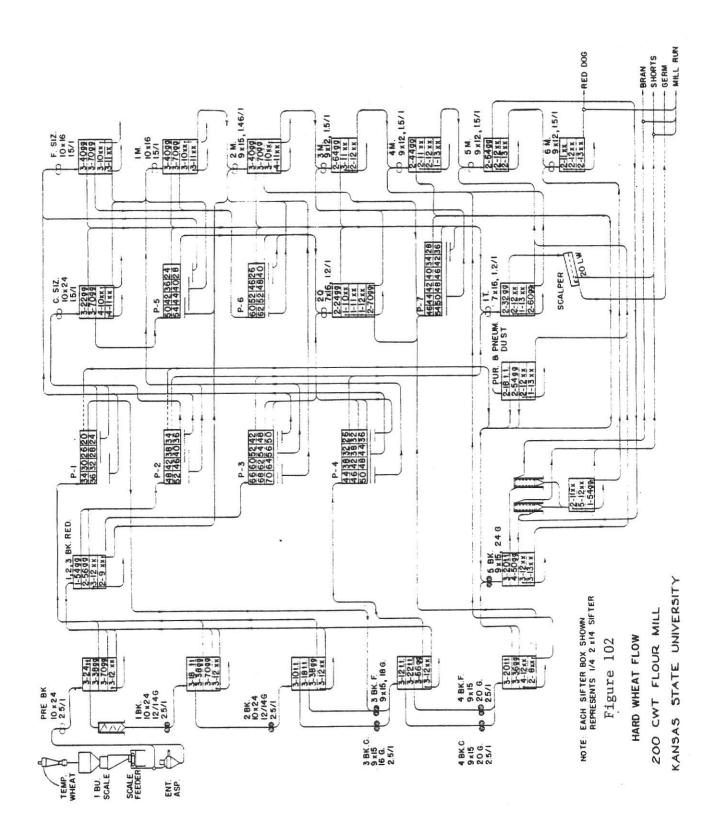
The Pilot Mill Flow (Figure 102) consists of 5 pairs of corrugated Breaks rolls, 10 pairs of smooth reduction rolls, 5 two-section free-swinging sifters and 5 purifiers (4 double, 1 single). Twenty-three separate flour streams are produced simulatneously with the capability of sampling each stream during mill operation. By obtaining 5-minute stream weights of each flour stream and sampling each for laboratory analysis of moisture and ash, milling performance for each mill run can be measured.

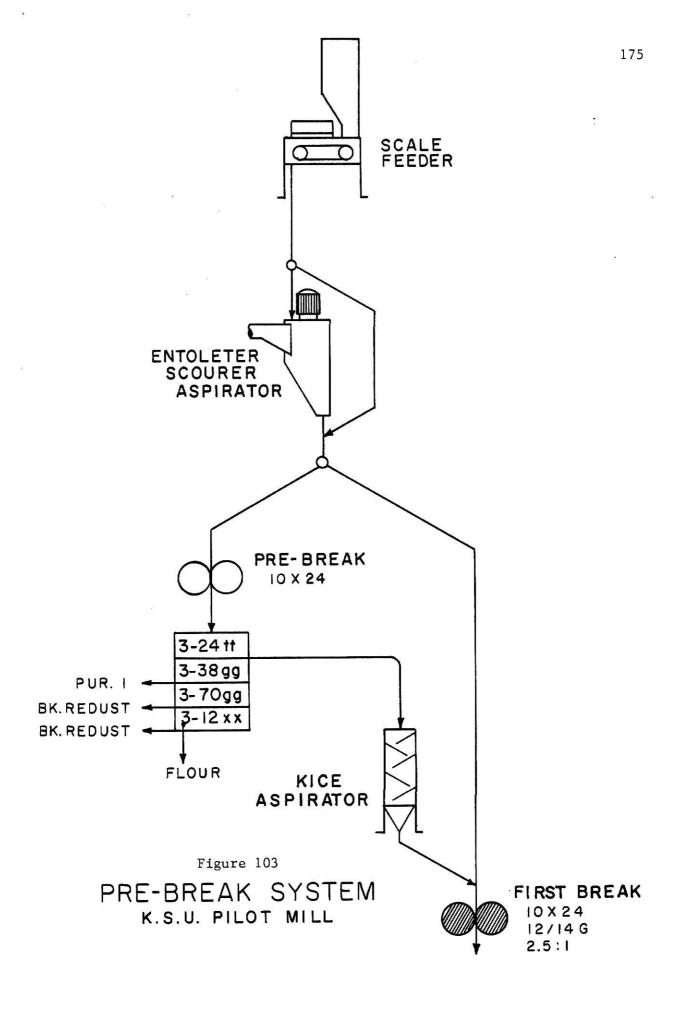
The Pre-Break System incorporated into the Pilot Mill Flow is shown in Figure 103. Tempered wheat from a belt scale feeder, to set the feed rate to the mill, can pass through an Entoleter-Scourer-Aspirator or directly to Pre-Break or First Break rolls. If Pre-Break is used, the Pre-Broken stock is sifted and the overs of a 24 light wire sieve are sent to an aspirator and then to First Break. Other separators from the sifter include sizings stock to purifier one, middlings stock to a Break Redust section and a small amount of flour.

Pre-Breaking itself is accomplished with a pair of smooth, 10 inch diameter by 24 inch length, Buhler rolls. Differential is created by a chain and sprocket drive. Initially, the roll was set up for a 2.5 to 1 differential, therefore the first two tests were run using this

differential. The chain was then removed for the remaining tests to give approximately a one to one differential with the flow of the wheat turning the free roll.

Data from these preliminary tests along with the resulting cumulative flour ash curves for each test are given in the following tables and figures.





A=ASH (14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL
TEST
WHEAT

K.S.U. PILOT MILL
NO. 1A 2.5:1 DIFF
HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	· A	QXA	S of QXA	S of QX
	(4) 4		NO PRE	-BREAK			
1 MB	1280	2.78	2.78	.254	0.706	0.706	.254
1 MT	4737	10.29	13.07	.263	2.706	3.412	.261
FSB	735	1.60	14.67	.264	0.422	3.835	.261
FST	3046	6.62	21.29	.274	1.814	5.649	.265
2 MB	1205	2.62	23.91	.283	0.741	6.390	.267
2 MT	4782	10.39	34.30	.293	3.044	9.434	.275
3 M	3361	7.30	41.60	.323	2.358	11.792	.283
2 Q	556	1.21	42.81	.325	0.393	12.186	.285
CST	12	0.03	42.84	.357	0.011	12.196	.285
CSB	266	0.58	43.42	.377	0.219	12.415	.286
2 BK	1689	3.67	47.09	.377	1.384	13.799	.293
4 M	2696	5.86	52.95	.382	2.239	16.037	.303
BK.RED	1388	3.02	55.97	.388	1.172	17.209	.307
3 BK	1638	3.56	59.53	.396	1.410	18.619	.313
1 BK	823	1.78	61.31	.408	0.726	19.435	.316
1 T	262	0.57	61.88	.475	0.271	19.616	.317
4 BK	778	1.69	63.57	.487	0.823	20.439	,322
5 M	1851	4.02	67.59	.530	2.131	22.569	.334
SUC	66	0.14	67.73	.645	0.090	22.659	.335
5 BK	658	1.43	69.16	.737	1.054	23.713	.343
6 M	810	1.76	70.92	1.194	2.101	25.815	364
B&SD	724	1.57	72.49	1.309	2.055	27.870	.384
	ALCONOMIC TO THE STATE OF THE S						

A=ASH (14% Moisture Basis)

Q=QUANTITY (% of Total Products)

S = SUMMATION

MILL
TEST
NO. 2A 2.5:1 DIFF
HARD RED WINTER

1 MB 1 MT FST FSB 2 MB 2 MT 3 M 2 Q CST BK.RED CSB 2 BK 1 BK 4 M	1442 4711 3126 683 1400 5851 4010 458 16 1371 238	2.88 9.40 6.24 1.36 2.79 11.68 8.00 0.91 0.03 2.74	HEAVY PR 2.88 12.28 18.52 19.88 22.67 34.35 42.35 43.26 43.29	.243 .243 .253 .254 .262 .262	0.700 2.284 1.579 0.345 0.731 3.060 2.328	0.700 2.984 4.563 4.908 5.639 8.699	.243 .243 .246 .247 .249 .253
1 MT FST FSB 2 MB 2 MT 3 M 2 Q CST BK.RED CSB 2 BK 1 BK 4 M	4711 3126 683 1400 5851 4010 458 16 1371 238	9.40 6.24 1.36 2.79 11.68 8.00 0.91 0.03	12.28 18.52 19.88 22.67 34.35 42.35 43.26	.243 .253 .254 .262 .262 .291	2.284 1.579 0.345 0.731 3.060	2.984 4.563 4.908 5.639	.243 .246 .247 .249
FST FSB 2 MB 2 MT 3 M 2 Q CST BK.RED CSB 2 BK 1 BK 4 M	3126 683 1400 5851 4010 458 16 1371 238	6.24 1.36 2.79 11.68 8.00 0.91 0.03	18.52 19.88 22.67 34.35 42.35 43.26	.253 .254 .262 .262 .291	1.579 0.345 0.731 3.060	4.563 4.908 5.639	.246 .247 .249
FSB 2 MB 2 MT 3 M 2 Q CST BK.RED CSB 2 BK 1 BK 4 M	683 1400 5851 4010 458 16 1371 238	1.36 2.79 11.68 8.00 0.91 0.03	19.88 22.67 34.35 42.35 43.26	.254 .262 .262 .291	0.345 0.731 3.060	4.908 5.639	.247
2 MB 2 MT 3 M 2 Q CST BK.RED CSB 2 BK 1 BK 4 M	1400 5851 4010 458 16 1371 238	2.79 11.68 8.00 0.91 0.03	22.67 34.35 42.35 43.26	.262 .262 .291	0.345 0.731 3.060	4.908 5.639	.247
2 MT 3 M 2 Q CST BK.RED CSB 2 BK 1 BK 4 M	5851 4010 458 16 1371 238	11.68 8.00 0.91 0.03	34.35 42.35 43.26	.262	3.060		
3 M 2 Q CST BK.RED CSB 2 BK 1 BK 4 M	4010 458 16 1371 238	8.00 0.91 0.03	42.35 43.26	.291		8.699	252
2 Q CST BK.RED CSB 2 BK 1 BK 4 M	458 16 1371 238	0.91 0.03	43.26	A COLUMN TO THE	2 328		. 255
CST BK.RED CSB 2 BK 1 BK 4 M	16 1371 238	0.03			4.040	11.027	.260
BK.RED CSB 2 BK 1 BK 4 M	1371 238		43 20	.293	0.267	11.294	.261
CSB 2 BK 1 BK 4 M	238	2.74	43.47	.306	0.009	11.303	.261
2 BK 1 BK 4 M			46.03	.315	0.863	12.166	. 264
1 BK 4 M		0.48	46.51	.325	0.156	12.322	. 265
4 M	1907	3.81	50.32	.326	1.242	13.564	.270
	875	1.75	52.07	.327	0.572	14.137	.271
	2858	5.71	57.78	.341	1.947	16.084	.279
3 BK	1667	3.33	61.11	.355	1.182	17.266	.283
P.BK	190	0.38	61.49	.396	0.150	17.416	. 283
1 T	317	0.63	62.12	.442	0.278	17.695	.285
4 BK	835	1.67	63.79	.446	0.745	18.440	.289
5 M	1937	3.87	67.66	.498	1.927	20.367	.301
SUC	45	0.09	67.75	.637	0.057	20.424	.301
5 BK	715	1.43	69.18	.675	0.965	21.389	.309
BSD	803	1.60	70.78	1.108	1.773	23.162	.327
6 M	745	1.49	72.27	1.189	1.772	24.934	.345

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)

Q=QUANTITY (% of Total Products)

S = SUMMATION

MILL K.S.U. PILOT MILL
TEST NO. 3A 2.5:1 DIFF
HARD RED WINTER

			A	QXA	S of QXA	SofQ
		LIGHT PI	RE-BREAK			
1402	2.90	2.90	.252	0.731	0.731	.252
2733	5.65	8.55	.252	1.424	2.155	.252
5081	10.50	19.05	.252	2.646	4.801	.252
814	1.68	20.73	.253	0.425	5.226	.252
1235	2.55	23.28	.282	0.719	5.945	.255
5775	11.94	35.22	.282	3.367	9.312	.264
14	0.03	35.25	.316	0.009	9.321	.264
472	0.98	36.23	.324	0.318	9.639	.266
1887	3.90	40.13	.334	1.303	10.941	.273
3475	7.18	47.31	.341	2.448	13.390	.283
267	0.55	47.86	.345	0.190	13.580	. 284
1718	3.55	51.41	.346	1.228	14.808	.288
974	2.01	53.42	.357	0.718	15.525	.291
2520	5.21	58.63	.400	2.084	17.609	.300
1895	3.92	62.55	.406	1.592	19.201	.307
47	0.10	62.65	.436	0.044	19.245	.307
335	0.69	63.34	.473	0.326	19.571	.309
1505	3.11	66.45	.517	1.608	21.179	.319
719	1.49	67.94	.547	0.815	21.994	.324
38	0.08	68.02	.599	0.048	22.042	.324
652	1.35	69.37	.766	1.034	23.076	.333
723	1.49	70.86	1.185	1.766	24.841	.351
662	1.37	72.23	1.206	1.652	26.494	.367
			And the second supplies of the second			
	5081 814 1235 5775 14 472 1887 3475 267 1718 974 2520 1895 47 335 1505 719 38 652 723	5081 10.50 814 1.68 1235 2.55 5775 11.94 14 0.03 472 0.98 1887 3.90 3475 7.18 267 0.55 1718 3.55 974 2.01 2520 5.21 1895 3.92 47 0.10 335 0.69 1505 3.11 719 1.49 38 0.08 652 1.35 723 1.49	5081 10.50 19.05 814 1.68 20.73 1235 2.55 23.28 5775 11.94 35.22 14 0.03 35.25 472 0.98 36.23 1887 3.90 40.13 3475 7.18 47.31 267 0.55 47.86 1718 3.55 51.41 974 2.01 53.42 2520 5.21 58.63 1895 3.92 62.55 47 0.10 62.65 335 0.69 63.34 1505 3.11 66.45 719 1.49 67.94 38 0.08 68.02 652 1.35 69.37 723 1.49 70.86	5081 10.50 19.05 .252 814 1.68 20.73 .253 1235 2.55 23.28 .282 5775 11.94 35.22 .282 14 0.03 35.25 .316 472 0.98 36.23 .324 1887 3.90 40.13 .334 3475 7.18 47.31 .341 267 0.55 47.86 .345 1718 3.55 51.41 .346 974 2.01 53.42 .357 2520 5.21 58.63 .400 1895 3.92 62.55 .406 47 0.10 62.65 .436 335 0.69 63.34 .473 1505 3.11 66.45 .517 719 1.49 67.94 .547 38 0.08 68.02 .599 652 1.35 69.37 .766	5081 10.50 19.05 .252 2.646 814 1.68 20.73 .253 0.425 1235 2.55 23.28 .282 0.719 5775 11.94 35.22 .282 3.367 14 0.03 35.25 .316 0.009 472 0.98 36.23 .324 0.318 1887 3.90 40.13 .334 1.303 3475 7.18 47.31 .341 2.448 267 0.55 47.86 .345 0.190 1718 3.55 51.41 .346 1.228 974 2.01 53.42 .357 0.718 2520 5.21 58.63 .400 2.084 1895 3.92 62.55 .406 1.592 47 0.10 62.65 .436 0.044 335 0.69 63.34 .473 0.326 1505 3.11 66.45 <t< td=""><td>5081 10.50 19.05 .252 2.646 4.801 814 1.68 20.73 .253 0.425 5.226 1235 2.55 23.28 .282 0.719 5.945 5775 11.94 35.22 .282 3.367 9.312 14 0.03 35.25 .316 0.009 9.321 472 0.98 36.23 .324 0.318 9.639 1887 3.90 40.13 .334 1.303 10.941 3475 7.18 47.31 .341 2.448 13.390 267 0.55 47.86 .345 0.190 13.580 1718 3.55 51.41 .346 1.228 14.808 974 2.01 53.42 .357 0.718 15.525 2520 5.21 58.63 .400 2.084 17.609 1895 3.92 62.55 .406 1.592 19.201 47 <t< td=""></t<></td></t<>	5081 10.50 19.05 .252 2.646 4.801 814 1.68 20.73 .253 0.425 5.226 1235 2.55 23.28 .282 0.719 5.945 5775 11.94 35.22 .282 3.367 9.312 14 0.03 35.25 .316 0.009 9.321 472 0.98 36.23 .324 0.318 9.639 1887 3.90 40.13 .334 1.303 10.941 3475 7.18 47.31 .341 2.448 13.390 267 0.55 47.86 .345 0.190 13.580 1718 3.55 51.41 .346 1.228 14.808 974 2.01 53.42 .357 0.718 15.525 2520 5.21 58.63 .400 2.084 17.609 1895 3.92 62.55 .406 1.592 19.201 47 <t< td=""></t<>

A=ASH(14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL
TEST
WHEAT

K.S.U. PILOT MILL
NO. 1B 2.5:1 DIFF
HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QXA
			LIGHT PR	E-BREAK			
FSB	1194	2.46	2.46	.253	0.622	0.622	.253
1 MB	1234	2.55	5.01	.253	0.645	1.268	.253
1 MT	4837	9.98	14.99	.253	2.525	3.792	.253
FST	4126	8.51	23.50	.262	2.230	6.022	.256
2 MT	5746	11.85	35.35	.271	3.211	9.233	.261
2 MB	1227	2.53	37.88	.272	0.688	9.922	.262
CST	13	0.03	37.91	.330	0.010	9.932	.262
3 M	3625	7.48	45.39	.331	2.476	12.407	.273
2 BK	1725	3.56	48.95	.346	1.232	13.639	.279
CSB	289	0.60	49.55	.362	0.217	13.856	.280
BK.RED	1582	3.26	52,81	.366	1.193	15.050	.285
1 BK	954	1,97	54.78	.367	0.723	15.772	.288
3 BK	1794	3.70	58.58	.396	1.465	17.238	.295
2 Q	243	0.50	58.98	.429	0.215	17.452	.296
4 M	1947	4.02	63.00	.438	1.761	19.213	.305
P.BK	54	0.11	63.11	.471	0.520	19.265	.305
4 BK	695	1.43	64.54	.525	0.751	20.016	.310
1 T	290	0.60	65.14	.567	0.340	20.356	.312
SUC	3	0.01	65.15	.598	0.006	20,362	.313
5 M	1478	3.05	68.20	.611	1.864	22.225	.326
6 M	1268	2.62	70.82	.648	1.698	23.923	.339
5 BK	619	1.28	72.10	.885	1.133	25.056	.348
BSD	681	1.40	73.50	1.387	1.942	26.998	.367

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL
TEST
WHEAT

K.S.U. PILOT MILL
NO. 3B 2.5:1 DIFF
HARD RED WINTER

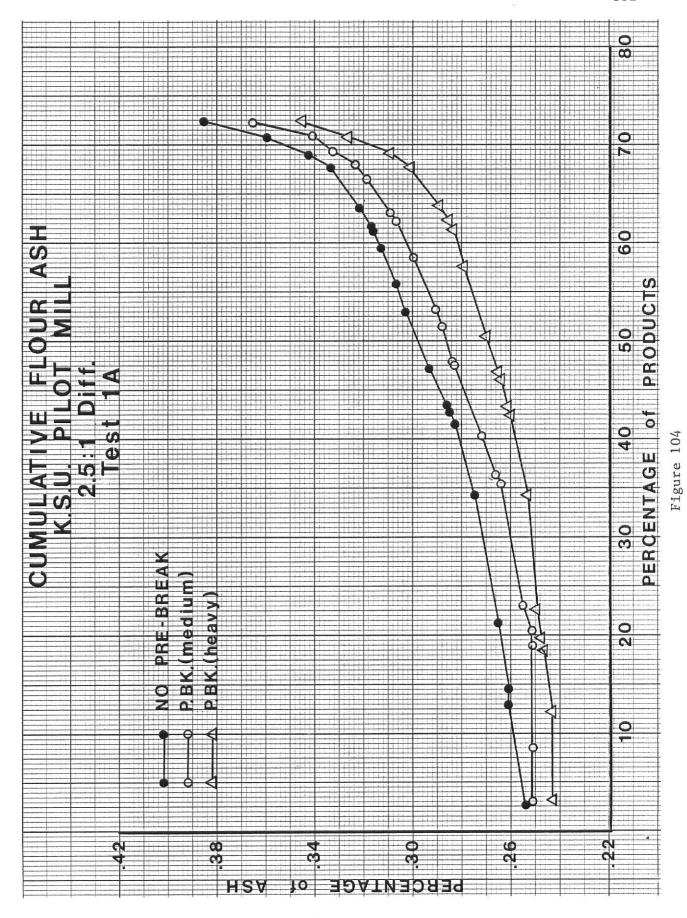
STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QXA
			NO PRE	E-BREAK			
1 MT	5136	10.68	10.68	.250	2.670	2.670	.250
FSB	1155	2.40	13.08	.251	0.602	3.272	.250
FST .	3893	8.10	21.18	.261	2.114	5.387	.254
2 MT	5847	12.16	33.34	.276	3.356	8.743	.262
2 MB	1205	2.51	35.85	.280	0.703	9.445	.263
1 MB	1447	3.01	38.86	.290	0.873	10.318	.266
CST	10	0.02	38.88	.345	0.007	10.325	.266
2 BK	1861	3.87	42.75	.346	1.339	11.664	.273
3 M	3969	8.25	51.00	.358	2.954	14.618	.287
BK.RED	1527	3.18	54.18	.375	1.193	15.810	.292
1 BK	972	2.02	56.20	.386	0.780	16.590	.295
3 BK	1736	3.61	59.81	.404	1.458	18.048	.302
CSB	280	0.58	60.39	.411	0.238	18.287	.303
2 Q	322	0.67	61.06	.448	0.300	18.587	.304
4 M	2122	4.41	65.47	.466	2.055	20.642	.315
4 BK	756	1.57	67.04	.511	0.802	21.444	.320
1 T	383	0.80	67.84	.557	0.446	21.890	.323
SUC	35	0.07	67.91	.576	0.040	21.930	.323
5 BK	730	1.52	69.43	.952	1.447	23.377	.337
5 M	1388	2.89	72.32	.985	2.847	26.224	.363
BSD	677	1.41	73.73	1.788	2,521	28,745	.390
6 M	441	0.92	74.65	3.009	2.768	31.513	.422

A=ASH (14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL
TEST
WHEAT

K.S.U. PILOT MILL
NO. 2B 2.5:1 DIFF
HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QXA
			HEAVY P	RE-BREAK			
1 MB	1355	2.92	2.92	.251	0.733	0.733	.251
FSB	1218	2.62	5,54	.251	0.658	1.391	.251
1 MT	5074	10.92	16.46	.251	2.741	4.131	.251
FST	4109	8.84	25.30	.262	2.316	6.448	.255
2 MB	1113	2.40	27.70	.271	0.650	7.098	.256
2 MT	5859	12.61	40.31	.271	3.417	10.515	.261
CST	10	0.02	40.33	.309	0.006	10.521	.261
3 BK	1870	4.40	44.73	.325	1.430	11.951	.267
BK.RED	1667	3.59	48.32	.335	1.203	13.154	.272
1 BK	917	1.97	50.29	.346	0.682	13.836	.275
3 M	3568	7.68	57.97	.348	2.673	16.508	.285
CSB	253	0.54	58.51	.351	0.190	16.698	.285
3 BK	1870	4.03	62.54	.384	1.548	18.245	.292
P.BK	203	0.44	62.98	.393	0.173	18.418	.292
2 Q	228	0.49	63.47	.457	0.224	18.642	.294
4 BK	899	1.94	65.41	.474	0.920	19.562	.299
4 M	1788	3.85	69.26	.505	1.944	21.506	.311
SUC	32	0.07	69.33	.577	0.040	21.546	.311
1 T	302	0.65	69.98	.615	0.400	21.946	.314
5 BK	746	1.61	71.59	.912	1.468	23.415	.327
5 M	916	1.97	73.56	1.178	2.321	25.735	.350
BSD	744	1.60	75.16	1.591	2,546	28,281	.376
6 M	372	0.80	75.96	2.615	2.092	30.373	400
		The second second					



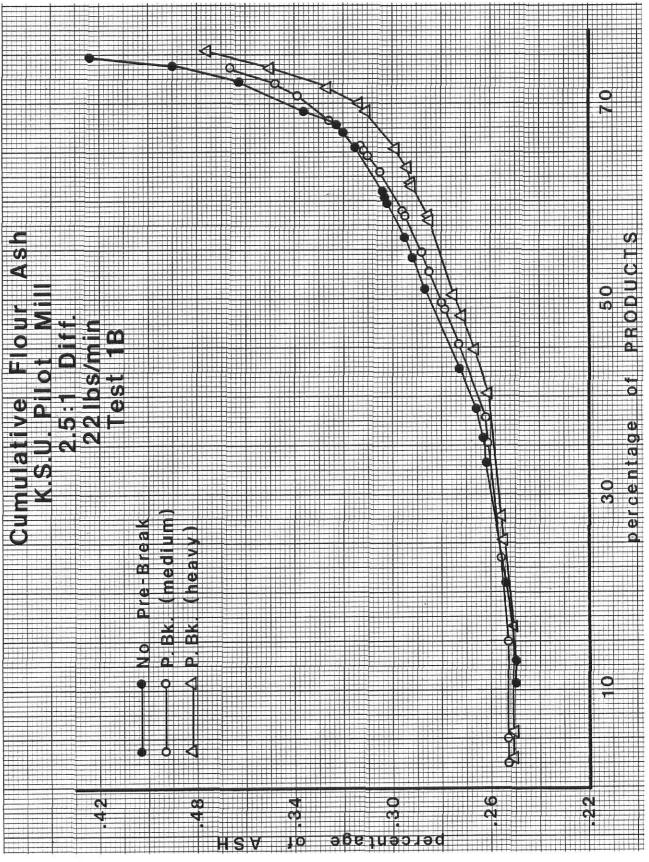


Figure 10

Cumulative Flour Ash Calculations

A=ASH(14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL
TEST
WHEAT

K.S.U. PILOT MILL
NO. 2A 1:1 DIFF
HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QXA
			LIGHT PI	RE-BREAK			
1 MT	6180	13.69	13.69	.258	3.532	3.532	.258
1 MB	1093	2.42	16.11	.259	0.627	4.159	.258
FSB	742	1.64	17.75	.269	0.441	4.600	.259
FST	3934	8.71	26.46	.270	2.352	6.952	.263
2 MT	5683	12.59	39.05	.287	3.613	10.565	.271
2 MB	381	0.84	39.89	.296	0.249	10.814	.271
BK.RED	1570	3.48	43.37	.344	1.197	12.011	.277
2 BK	1985	4.40	47.77	.345	1.518	13.529	.283
3 M	3412	7.56	55.33	.362	2.737	16.266	.294
1 BK	944	2.09	57.42	.366	0.765	17.030	.297
3 BK	1594	3.53	60.95	.384	1.356	18.386	.302
CSB	14	0.03	60.98	.392	0.012	18.398	.302
CST	252	0.56	61.54	.407	0.228	18.626	.303
2 Q	333	0.74	62.28	.453	0.335	18.961	.304
P.BK	31	0.07	62.35	.474	0.033	18.994	.305
4 BK	826	1.83	64.18	.479	0.877	19.871	.310
4 M	1432	3.17	67.35	.505	1.601	21.471	.319
SUC	130	0.29	67.64	.594	0.172	21.644	.320
1 T	403	0.89	68.53	.607	0.540	22.184	.324
5 BK	708	1.57	70.10	.735	1.154	23.338	.333
5 M	947	2.10	72.20	1.160	2.436	25.774	.357
BSD	592	1.31	73.51	1.370	1.795	27.569	.375
6 M	343	0.76	74.27	2.386	1.813	29.382	. 396

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL
TEST
WHEAT

K.S.U. PILOT MILL
NO. 3A 1:1 DIFF
HARD RED WINTER

39 41 87 93 76 53 34 26 14 18 78 55 51 14 65 92 60 89 01	1.66 2.34 13.68 8.53 12.76 0.79 4.35 3.88 2.05 0.04 6.92 4.17 0.57 0.34 0.71 3.07 1.78 0.36 0.87	MEDIUM 1.66 4.00 17.68 26.21 38.97 39.76 44.11 47.99 50.04 50.08 57.00 61.17 61.74 62.08 62.79 65.86 67.64 68.00 68.87	PRE-BREA	0.428 0.604 3.529 2.295 3.649 0.241 1.453 1.331 0.705 0.014 2.505 1.597 0.225 0.146 0.342 1.520 0.942 0.188	0.428 1.032 4.561 6.856 10.505 10.746 12.199 13.530 14.235 14.249 16.754 18.351 18.577 18.723 19.064 20.584 21.507 21.695	.258 .258 .258 .262 .270 .270 .277 .282 .284 .285 .294 .300 .301 .302 .304 .313 .318
41 87 93 76 53 34 26 14 18 78 57 55 51 14 65 92 60 89	2.34 13.68 8.53 12.76 0.79 4.35 3.88 2.05 0.04 6.92 4.17 0.57 0.34 0.71 3.07 1.78 0.36	4.00 17.68 26.21 38.97 39.76 44.11 47.99 50.04 50.08 57.00 61.17 61.74 62.08 62.79 65.86 67.64 68.00	.258 .258 .269 .286 .305 .334 .343 .344 .352 .362 .383 .395 .429 .481 .495	0.604 3.529 2.295 3.649 0.241 1.453 1.331 0.705 0.014 2.505 1.597 0.225 0.146 0.342 1.520 0.942	1.032 4.561 6.856 10.505 10.746 12.199 13.530 14.235 14.249 16.754 18.351 18.577 18.723 19.064 20.584 21.507	.258 .258 .262 .270 .270 .277 .282 .284 .285 .294 .300 .301 .302 .304 .313
87 93 76 53 34 26 14 18 78 57 55 51 14 65 92 60 89	13.68 8.53 12.76 0.79 4.35 3.88 2.05 0.04 6.92 4.17 0.57 0.34 0.71 3.07 1.78 0.36	17.68 26.21 38.97 39.76 44.11 47.99 50.04 50.08 57.00 61.17 61.74 62.08 62.79 65.86 67.64 68.00	.258 .269 .286 .305 .334 .343 .344 .352 .362 .383 .395 .429 .481 .495	3.529 2.295 3.649 0.241 1.453 1.331 0.705 0.014 2.505 1.597 0.225 0.146 0.342 1.520 0.942	4.561 6.856 10.505 10.746 12.199 13.530 14.235 14.249 16.754 18.351 18.577 18.723 19.064 20.584 21.507	.258 .262 .270 .270 .277 .282 .284 .285 .294 .300 .301 .302 .304 .313
93 76 53 34 26 14 18 78 57 55 51 14 65 92 60 89	8.53 12.76 0.79 4.35 3.88 2.05 0.04 6.92 4.17 0.57 0.34 0.71 3.07 1.78 0.36	26.21 38.97 39.76 44.11 47.99 50.04 50.08 57.00 61.17 61.74 62.08 62.79 65.86 67.64 68.00	.269 .286 .305 .334 .343 .344 .352 .362 .383 .395 .429 .481 .495	2.295 3.649 0.241 1.453 1.331 0.705 0.014 2.505 1.597 0.225 0.146 0.342 1.520 0.942	6.856 10.505 10.746 12.199 13.530 14.235 14.249 16.754 18.351 18.577 18.723 19.064 20.584 21.507	.262 .270 .270 .277 .282 .284 .285 .294 .300 .301 .302 .304 .313
76 53 34 26 14 18 78 57 55 51 14 65 92 60 89	12.76 0.79 4.35 3.88 2.05 0.04 6.92 4.17 0.57 0.34 0.71 3.07 1.78 0.36	38.97 39.76 44.11 47.99 50.04 50.08 57.00 61.17 61.74 62.08 62.79 65.86 67.64 68.00	.286 .305 .334 .343 .344 .352 .362 .383 .395 .429 .481 .495	3.649 0.241 1.453 1.331 0.705 0.014 2.505 1.597 0.225 0.146 0.342 1.520 0.942	10.505 10.746 12.199 13.530 14.235 14.249 16.754 18.351 18.577 18.723 19.064 20.584 21.507	.270 .270 .277 .282 .284 .285 .294 .300 .301 .302 .304 .313
53 34 26 14 18 78 57 55 51 14 65 92 60 89	0.79 4.35 3.88 2.05 0.04 6.92 4.17 0.57 0.34 0.71 3.07 1.78 0.36	39.76 44.11 47.99 50.04 50.08 57.00 61.17 61.74 62.08 62.79 65.86 67.64 68.00	.305 .334 .343 .344 .352 .362 .383 .395 .429 .481 .495	0.241 1.453 1.331 0.705 0.014 2.505 1.597 0.225 0.146 0.342 1.520 0.942	10.746 12.199 13.530 14.235 14.249 16.754 18.351 18.577 18.723 19.064 20.584 21.507	.270 .277 .282 .284 .285 .294 .300 .301 .302 .304 .313
34 26 14 18 78 57 55 51 14 65 92 60 89	4.35 3.88 2.05 0.04 6.92 4.17 0.57 0.34 0.71 3.07 1.78 0.36	44.11 47.99 50.04 50.08 57.00 61.17 61.74 62.08 62.79 65.86 67.64 68.00	.334 .343 .344 .352 .362 .383 .395 .429 .481 .495	1.453 1.331 0.705 0.014 2.505 1.597 0.225 0.146 0.342 1.520 0.942	12.199 13.530 14.235 14.249 16.754 18.351 18.577 18.723 19.064 20.584 21.507	.277 .282 .284 .285 .294 .300 .301 .302 .304 .313
26 14 18 78 57 55 51 14 65 92 60 89	3.88 2.05 0.04 6.92 4.17 0.57 0.34 0.71 3.07 1.78 0.36	47.99 50.04 50.08 57.00 61.17 61.74 62.08 62.79 65.86 67.64 68.00	.343 .344 .352 .362 .383 .395 .429 .481 .495	1.331 0.705 0.014 2.505 1.597 0.225 0.146 0.342 1.520 0.942	13.530 14.235 14.249 16.754 18.351 18.577 18.723 19.064 20.584 21.507	.282 .284 .285 .294 .300 .301 .302 .304 .313
26 14 18 78 57 55 51 14 65 92 60 89	2.05 0.04 6.92 4.17 0.57 0.34 0.71 3.07 1.78 0.36	50.04 50.08 57.00 61.17 61.74 62.08 62.79 65.86 67.64 68.00	.344 .352 .362 .383 .395 .429 .481 .495	0.705 0.014 2.505 1.597 0.225 0.146 0.342 1.520 0.942	14.235 14.249 16.754 18.351 18.577 18.723 19.064 20.584 21.507	.284 .285 .294 .300 .301 .302 .304 .313
18 78 57 55 51 14 65 92 60 89	0.04 6.92 4.17 0.57 0.34 0.71 3.07 1.78 0.36	50.08 57.00 61.17 61.74 62.08 62.79 65.86 67.64 68.00	.352 .362 .383 .395 .429 .481 .495	0.014 2.505 1.597 0.225 0.146 0.342 1.520 0.942	14.249 16,754 18.351 18.577 18.723 19.064 20.584 21.507	.285 .294 .300 .301 .302 .304 .313 .318
78 57 55 51 14 65 92 60 89	6.92 4.17 0.57 0.34 0.71 3.07 1.78 0.36	57.00 61.17 61.74 62.08 62.79 65.86 67.64 68.00	.352 .362 .383 .395 .429 .481 .495	2.505 1.597 0.225 0.146 0.342 1.520 0.942	16.754 18.351 18.577 18.723 19.064 20.584 21.507	.294 .300 .301 .302 .304 .313
78 57 55 51 14 65 92 60 89	6.92 4.17 0.57 0.34 0.71 3.07 1.78 0.36	57.00 61.17 61.74 62.08 62.79 65.86 67.64 68.00	.362 .383 .395 .429 .481 .495	2.505 1.597 0.225 0.146 0.342 1.520 0.942	16.754 18.351 18.577 18.723 19.064 20.584 21.507	.294 .300 .301 .302 .304 .313
57 55 51 14 65 92 60 89	4.17 0.57 0.34 0.71 3.07 1.78 0.36	61.17 61.74 62.08 62.79 65.86 67.64 68.00	.383 .395 .429 .481 .495	1.597 0.225 0.146 0.342 1.520 0.942	18.351 18.577 18.723 19.064 20.584 21.507	.300 .301 .302 .304 .313 .318
55 51 14 65 92 60 89	0.57 0.34 0.71 3.07 1.78 0.36	61.74 62.08 62.79 65.86 67.64 68.00	.395 .429 .481 .495	0.225 0.146 0.342 1.520 0.942	18.577 18.723 19.064 20.584 21.507	.301 .302 .304 .313
51 14 65 92 60 89	0.34 0.71 3.07 1.78 0.36	62.08 62.79 65.86 67.64 68.00	.429 .481 .495 .519	0.146 0.342 1.520 0.942	18.723 19.064 20.584 21.507	.302 .304 .313 .318
14 65 92 60 89	0.71 3.07 1.78 0.36	62.79 65.86 67.64 68.00	.481 .495 .519	0.342 1.520 0.942	19.064 20.584 21.507	.304 .313 .318
92 60 89	1.78 0.36	67.64 68.00	.519	0.942	21.507	.318
92 60 89	1.78 0.36	67.64 68.00	.519	0.942	21.507	.318
60 89	0.36	68.00				
89		+		NAME OF TAXABLE PARTY.		
		1 00.07	,616	0.536	22,231	.323
	1.35	70.22	.762	1.029	23.260	.331
85	2.21	72.43	1.156	2.555	25.814	.356
26	1.41	73.84	1.269	1.789	27.604	.374
57	0.80	74.64	2.100	1.680	29.284	.392

A=ASH (14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL K.S.U. PILOT MILL NO. 4A 1:1 DIFF HARD RED WINTER

FSB 615 1.37 1 MB 1004 2.24 1 MT 5830 13.02 2 MT 5386 12.03 FST 3808 8.51 2 MB 278 0.62 CST 164 0.37 BK.RED 1737 3.88 1 BK 847 1.89 2 BK 2220 4.96 3 BK 1758 3.93 CSB 10 0.02 P.BK 289 0.65 3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02 6 M 371 0.83	1.37 3.61 16.63 28.66 37.17 37.79 38.16 42.04 43.93 48.89 52.82 52.84 53.49 59.41 61.51 62.10 65.00 65.23 66.07	PRE-BREAK	0.351 0.573 3.463 3.429 2.527 0.187 0.116 1.242 0.607 1.597 1.446 0.007 0.247 2.303 1.023 0.293 1.569 0.129 0.546	0.351 0.924 4.387 7.816 10.344 10.531 10.647 11.888 12.495 14.092 15.538 15.546 15.793 18.095 19.118 19.411 20.980 21.109	.256 .256 .264 .273 .278 .279 .279 .283 .284 .288 .294 .295 .305 .311 .313
1 MB 1004 2.24 1 MT 5830 13.02 2 MT 5386 12.03 FST 3808 8.51 2 MB 278 0.62 CST 164 0.37 BK.RED 1737 3.88 1 BK 847 1.89 2 BK 2220 4.96 3 BK 1758 3.93 CSB 10 0.02 P.BK 289 0.65 3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	3.61 16.63 28.66 37.17 37.79 38.16 42.04 43.93 48.89 52.82 52.84 53.49 59.41 61.51 62.10 65.00 65.23 66.07	.256 .266 .285 .297 .302 .313 .320 .321 .322 .368 .369 .389 .487 .496 .541 .562	0.573 3.463 3.429 2.527 0.187 0.116 1.242 0.607 1.597 1.446 0.007 0.247 2.303 1.023 0.293 1.569 0.129	0.924 4.387 7.816 10.344 10.531 10.647 11.888 12.495 14.092 15.538 15.546 15.793 18.095 19.118 19.411 20.980	.256 .264 .273 .278 .279 .279 .283 .284 .288 .294 .295 .305 .311 .313
1 MT 5830 13.02 2 MT 5386 12.03 FST 3808 8.51 2 MB 278 0.62 CST 164 0.37 BK.RED 1737 3.88 1 BK 847 1.89 2 BK 2220 4.96 3 BK 1758 3.93 CSB 10 0.02 P.BK 289 0.65 3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	16.63 28.66 37.17 37.79 38.16 42.04 43.93 48.89 52.82 52.84 53.49 59.41 61.51 62.10 65.00 65.23 66.07	.266 .285 .297 .302 .313 .320 .321 .322 .368 .369 .380 .389 .487 .496 .541 .562	3.463 3.429 2.527 0.187 0.116 1.242 0.607 1.597 1.446 0.007 0.247 2.303 1.023 0.293 1.569 0.129	4.387 7.816 10.344 10.531 10.647 11.888 12.495 14.092 15.538 15.546 15.793 18.095 19.118 19.411 20.980	.264 .273 .278 .279 .279 .283 .284 .284 .294 .294 .295 .305 .311 .313
2 MT 5386 12.03 FST 3808 8.51 2 MB 278 0.62 CST 164 0.37 BK.RED 1737 3.88 1 BK 847 1.89 2 BK 2220 4.96 3 BK 1758 3.93 CSB 10 0.02 P.BK 289 0.65 3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	28.66 37.17 37.79 38.16 42.04 43.93 48.89 52.82 52.84 53.49 59.41 61.51 62.10 65.00 65.23 66.07	.285 .297 .302 .313 .320 .321 .322 .368 .369 .380 .389 .487 .496 .541 .562	3.429 2.527 0.187 0.116 1.242 0.607 1.597 1.446 0.007 0.247 2.303 1.023 0.293 1.569 0.129	7.816 10.344 10.531 10.647 11.888 12.495 14.092 15.538 15.546 15.793 18.095 19.118 19.411 20.980	.273 .278 .279 .279 .283 .284 .288 .294 .295 .305 .311 .313
FST 3808 8.51 2 MB 278 0.62 CST 164 0.37 BK.RED 1737 3.88 1 BK 847 1.89 2 BK 2220 4.96 3 BK 1758 3.93 CSB 10 0.02 P.BK 289 0.65 3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	37.17 37.79 38.16 42.04 43.93 48.89 52.82 52.84 53.49 59.41 61.51 62.10 65.00 65.23 66.07	.297 .302 .313 .320 .321 .322 .368 .369 .380 .389 .487 .496 .541 .562	2.527 0.187 0.116 1.242 0.607 1.597 1.446 0.007 0.247 2.303 1.023 0.293 1.569 0.129	10.344 10.531 10.647 11.888 12.495 14.092 15.538 15.546 15.793 18.095 19.118 19.411 20.980	.278 .279 .279 .283 .284 .288 .294 .294 .295 .305 .311 .313
2 MB 278 0.62 CST 164 0.37 BK.RED 1737 3.88 1 BK 847 1.89 2 BK 2220 4.96 3 BK 1758 3.93 CSB 10 0.02 P.BK 289 0.65 3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	37.79 38.16 42.04 43.93 48.89 52.82 52.84 53.49 59.41 61.51 62.10 65.00 65.23 66.07	.302 .313 .320 .321 .322 .368 .369 .380 .389 .487 .496 .541 .562	0.187 0.116 1.242 0.607 1.597 1.446 0.007 0.247 2.303 1.023 0.293 1.569 0.129	10.531 10.647 11.888 12.495 14.092 15.538 15.546 15.793 18.095 19.118 19.411 20.980	.279 .279 .283 .284 .288 .294 .294 .295 .305 .311
CST 164 0.37 BK.RED 1737 3.88 1 BK 847 1.89 2 BK 2220 4.96 3 BK 1758 3.93 CSB 10 0.02 P.BK 289 0.65 3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	38.16 42.04 43.93 48.89 52.82 52.84 53.49 59.41 61.51 62.10 65.00 65.23 66.07	.313 .320 .321 .322 .368 .369 .380 .389 .487 .496 .541 .562	0.116 1.242 0.607 1.597 1.446 0.007 0.247 2.303 1.023 0.293 1.569 0.129	10.531 10.647 11.888 12.495 14.092 15.538 15.546 15.793 18.095 19.118 19.411 20.980	.279 .279 .283 .284 .288 .294 .294 .295 .305 .311
BK.RED 1737 3.88 1 BK 847 1.89 2 BK 2220 4.96 3 BK 1758 3.93 CSB 10 0.02 P.BK 289 0.65 3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	42.04 43.93 48.89 52.82 52.84 53.49 59.41 61.51 62.10 65.00 65.23 66.07	.313 .320 .321 .322 .368 .369 .380 .389 .487 .496 .541 .562	1.242 0.607 1.597 1.446 0.007 0.247 2.303 1.023 0.293 1.569 0.129	10.647 11.888 12.495 14.092 15.538 15.546 15.793 18.095 19.118 19.411 20.980	.279 .283 .284 .288 .294 .294 .295 .305 .311
BK.RED 1737 3.88 1 BK 847 1.89 2 BK 2220 4.96 3 BK 1758 3.93 CSB 10 0.02 P.BK 289 0.65 3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	42.04 43.93 48.89 52.82 52.84 53.49 59.41 61.51 62.10 65.00 65.23 66.07	.320 .321 .322 .368 .369 .380 .389 .487 .496 .541 .562	1.242 0.607 1.597 1.446 0.007 0.247 2.303 1.023 0.293 1.569 0.129	11.888 12.495 14.092 15.538 15.546 15.793 18.095 19.118 19.411 20.980	.283 .284 .288 .294 .294 .295 .305 .311 .313
1 BK 847 1.89 2 BK 2220 4.96 3 BK 1758 3.93 CSB 10 0.02 P.BK 289 0.65 3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	43.93 48.89 52.82 52.84 53.49 59.41 61.51 62.10 65.00 65.23 66.07	.321 .322 .368 .369 .380 .389 .487 .496 .541 .562	0.607 1.597 1.446 0.007 0.247 2.303 1.023 0.293 1.569 0.129	12.495 14.092 15.538 15.546 15.793 18.095 19.118 19.411 20.980	.284 .288 .294 .294 .295 .305 .311 .313
3 BK 1758 3.93 CSB 10 0.02 P.BK 289 0.65 3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	52.82 52.84 53.49 59.41 61.51 62.10 65.00 65.23 66.07	.368 .369 .380 .389 .487 .496 .541 .562	1.446 0.007 0.247 2.303 1.023 0.293 1.569 0.129	15.538 15.546 15.793 18.095 19.118 19.411 20.980	.294 .294 .295 .305 .311 .313
CSB 10 0.02 P.BK 289 0.65 3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	52.84 53.49 59.41 61.51 62.10 65.00 65.23 66.07	.369 .380 .389 .487 .496 .541 .562	0.007 0.247 2.303 1.023 0.293 1.569 0.129	15.546 15.793 18.095 19.118 19.411 20.980	.294 .295 .305 .311 .313
P.BK 289 0.65 3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	53.49 59.41 61.51 62.10 65.00 65.23 66.07	.380 .389 .487 .496 .541 .562	0.247 2.303 1.023 0.293 1.569 0.129	15.793 18.095 19.118 19.411 20.980	.295 .305 .311 .313
3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	59.41 61.51 62.10 65.00 65.23 66.07	.389 .487 .496 .541 .562 .650	2.303 1.023 0.293 1.569 0.129	18.095 19.118 19.411 20.980	.305 .311 .313
3 M 2649 5.92 4 BK 942 2.10 2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	59.41 61.51 62.10 65.00 65.23 66.07	.487 .496 .541 .562 .650	1.023 0.293 1.569 0.129	19.118 19.411 20.980	.311
2 Q 263 0.59 4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	62.10 65.00 65.23 66.07	.496 .541 .562 .650	0.293 1.569 0.129	19.411 20.980	.313
4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	65.00 65.23 66.07	.541 .562 .650	1.569 0.129	20.980	
4 M 1299 2.90 SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	65.23 66.07	.562 .650	0.129		.320
SUC 102 0.23 1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	65.23 66.07	.562 .650	0.129		
1 T 378 0.84 5 BK 693 1.55 BSD 811 1.81 5 M 903 2.02	66.07	.650	The state of the s		.324
BSD 811 1.81 5 M 903 2.02	67.62	.699	0.540	21.655	.328
5 M 903 2.02	Married and Association of the Control of the Contr		1.083	22.730	.336
5 M 903 2.02	69.43	1.073	1.942	24.681	.355
		1.341	2.709	27.389	.383
		2.091	1.736	29.125	.403

A=ASH(14% Moisture Basis)

Q=QUANTITY (% of Total Products)

S = SUMMATION

MILL
TEST
WHEAT

K.S.U. PILOT MILL
NO. 5A 1:1 DIFF
HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	А	QXA	S of QXA	S of QXA
***			NO PRE	E-BREAK			
1 MB	1181	2.64	2.64	.257	0.678	0.678	.257
FSB	747	1.67	4.31	.258	0.431	1.109	.257
1 MT	6086	13.63	17.94	.267	3.639	4.749	.265
FST	3682	8.25	26.19	.277	2.285	7.034	.269
2 MT	5731	12.83	39.02	.295	3.785	10.819	.277
2 MB	453	1.01	40.03	.303	0.306	11.125	.278
2 BK	1868	4.18	44.21	.373	1.559	12,684	.287
3 M	3963	8.87	53.08	.379	3.362	16.046	.302
BK.RED	1597	3.58	56.66	.392	1.403	17.449	.309
CSB	13	0.03	56.69	.399	0.012	17.461	.309
1 BK	748	1.67	58.36	.403	0.673	18.134	.311
3 BK	1767	3.96	62.32	.411	1.628	19.761	.317
CST	259	0.58	62.90	.473	0.274	20.036	,319
2 Q	331	0.74	63.64	.508	0.376	20.412	.321
4 BK	803	1.80	65.44	.515	0.927	21.339	.326
4 M	1340	3.00	68.44	.530	1.590	22.929	.335
SUC	192	0.43	68.87	.552	0.237	23.166	.336
1 T	415	0.93	69.80	.643	0.598	23.764	.340
5 BK	639	1.43	71.23	.799	1.143	24.907	.350
5 M	967	2.17	73.40	1.244	2.699	27.606	.376
B&SD	680	1.52	74.92	1.262	1.918	29.524	.394
6 M	440	0.99	75.91	2.081	2,060	31.585	.416
			100				
							A CONTRACTOR OF STREET

Table 34

A=ASH (14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL K.S.U. PILOT MILL

TEST NO. 1B 1:1 DIFF

WHEAT HARD RED WINTER

/	WEIGHT (grams)	Q	S of Q	Α	QXA	SofQXA	S of QXA
			NO PRE-	BREAK			
1 MB	1463	2.83	2.83	.269	0.761	0.761	.269
1 MT	6163	11.91	14.74	.270	3.216	3.977	.270
FSB	1527	2.95	17.69	.280	0.826	4.803	.272
FST	6224	12.03	29.72	.291	3.501	8.304	.279
2 MB	444	0.86	30.58	.307	0.264	8.568	.280
2 MT	5839	11.29	41.87	,308	3,477	12.045	.288
CSB	12	0.02	41.89	.356	0.007	12,052	. 288
3 M	3518	6.80	48.69	.375	2.550	14.602	.300
BK.RED	1349	2.61	51.30	.395	1.031	15.633	.305
2 BK	1829	3.54	54.84	.396	1.402	17.035	.311
CST	503	0.97	55,81	.430	0.417	17.452	.313
3 BK	1770	3.42	59.23	.434	1.484	18.936	.320
1 BK	1058	2.05	61.28	.437	0.896	19.832	.324
2 Q	411	0.79	62.07	.466	0.368	20.200	.325
4 M	2221	4.29	66.36	.473	2.029	22.229	.335
4 BK	945	1.83	68.19	.593	1.085	23.315	.342
1 T	385	0.74	68.93	.681	0.504	23.819	.346
SUC	56	0.11	69.04	.757	0.083	23.902	.346
5 M	914	1.77	70.81	.804	1.423	25.325	.358
5 BK	609	1.18	71.99	.928	1.095	26.420	.367
6 M	786	1.52	73.51	1.558	2,368	28.788	.392
BSD	646	1.25	74.76	1.781	2.226	31.014	.415

A=ASH(14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL
TEST
WHEAT

K.S.U. PILOT MILL
NO. 2B 1:1 DIFF
HARD RED WINTER

1369 1420 6040 5527 6113 767 11 1614 1993 3581	2.69 2.78 11.83 10.83 11.97 1.50 0.02 3.16	MEDIUM E 2.69 5.47 17.30 28.13 40.10 41.60 41.62	.239 .248 .259 .270 .287	0.643 0.689 3.064 2.924 3.435	0.643 1.332 4.396 7.320	.239 .244 .254
1420 6040 5527 6113 767 11 1614 1993	2.78 11.83 10.83 11.97 1.50 0.02	5.47 17.30 28.13 40.10 41.60	.248 .259 .270 .287	0.689 3.064 2.924	1.332	.244
6040 5527 6113 767 11 1614 1993	11.83 10.83 11.97 1.50 0.02	17.30 28.13 40.10 41.60	.259 .270 .287	3.064 2.924	1.332	.254
5527 6113 767 11 1614 1993	10.83 11.97 1.50 0.02	28.13 40.10 41.60	.270	2.924		
6113 767 11 1614 1993	11.97 1.50 0.02	40.10	.287		7.320	260
767 11 1614 1993	1.50	41.60		3.435		.260
11 1614 1993	0.02		287		10.756	.268
1614 1993		41 62	. 207	0.431	11.186	.269
1993	3.16	1 41.02	.316	0.006	11,193	.269
1993		44.78	. 344	1.087	12.280	274
3581	3.90	48.68	.355	1.385	13.664	.281
	7.01	55.69	.363	2.545	16,209	.291
1233	2.42	58,11	.366	0.886	17.095	. 294
463	0.91	59.02	.369	0.336	17.430	295
2026	3.97	62.99	.404	1.604	19.034	.302
258	0.51	63.50	.421	0.215	19.249	.303
339	0.66	64.16	.454	0.300	19.549	.305
1973	3.86	68.02	.566	2.185		.320
879	1.72	69.74	.609	1.047	22,781	.327
372	0.73	70.47	.686	0.501	23.282	.330
3	0.01	70.48	.759			.330
497	0.97	71.45	.928			.339
635	1.24	72,69	.972	1.205	25.395	.349
626	1.23	73.92	1.560	1.919	27,313	.369
556	1.09	75.01	1-826	1 990	29 304	391
	258 339 1973 879 372 3 497 635	258 0.51 339 0.66 1973 3.86 879 1.72 372 0.73 3 0.01 497 0.97 635 1.24 626 1.23	258 0.51 63.50 339 0.66 64.16 1973 3.86 68.02 879 1.72 69.74 372 0.73 70.47 3 0.01 70.48 497 0.97 71.45 635 1.24 72.69 626 1.23 73.92	258 0.51 63.50 .421 339 0.66 64.16 .454 1973 3.86 68.02 .566 879 1.72 69.74 .609 372 0.73 70.47 .686 3 0.01 70.48 .759 497 0.97 71.45 .928 635 1.24 72.69 .972 626 1.23 73.92 1.560	258 0.51 63.50 .421 0.215 339 0.66 64.16 .454 0.300 1973 3.86 68.02 .566 2.185 879 1.72 69.74 .609 1.047 372 0.73 70.47 .686 0.501 3 0.01 70.48 .759 0.008 497 0.97 71.45 .928 0.900 635 1.24 72.69 .972 1.205 626 1.23 73.92 1.560 1.919	258 0.51 63.50 .421 0.215 19.249 339 0.66 64.16 .454 0.300 19.549 1973 3.86 68.02 .566 2.185 21.733 879 1.72 69.74 .609 1.047 22.781 372 0.73 70.47 .686 0.501 23.282 3 0.01 70.48 .759 0.008 23.289 497 0.97 71.45 .928 0.900 24.189 635 1.24 72.69 .972 1.205 25.395 626 1.23 73.92 1.560 1.919 27.313

Cumulative Flour Ash Calculations

A=ASH(14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL
TEST
NO. 3B 1:1 DIFF
HARD RED WINTER

TREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QX
			HEAVY PR	E-BREAK			
FSB	1168	2.31	2.31	.268	0.619	0.619	.268
1_ MT	5569	11.03	13.34	.269	2.967	3.586	.269
FST	5249	10.40	23.74	.278	2.891	6.447	.273
2 MB	687	1.36	25.10	.287	0.390	6.868	.274
2 MT	6103	12.09	37.19	.288	3.482	10.350	.276
1 MB	1525	3.02	40.21	.298	0.900	11.250	.280
1 BK	1196	2.37	42.58	.342	0.811	12.060	.283
2 BK	2119	4.20	46.78	.342	1.436	13.496	.289
BK.RED	1989	3.94	50.72	.346	1.363	14.860	.293
P.BK	39	0.08	50.80	.361	0.029	14.889	.293
CSB	10	0.02	50.82	.363	0.007	14.896	.293
3 BK	1995	3.95	54.77	.371	1.465	16.361	.299
3 M	3077	6.10	60.87	.392	2.391	18.753	.308
CST	362	0.72	61.59	.409	0.294	19.047	.309
2 Q	396	0.78	62.37	.453	0.353	19.400	.311
4 BK	971	1.92	64.29	.561	1.077	20.477	.319
4 M	1622	3.21	67.50	.576	1.849	22.326	.331
SUC	317	0.63	68.13	.653	0.411	22.738	.334
1 T	342	0.68	68.81	.715	0.486	23.224	.338
5 BK	710	1.41	70.22	.822	1.159	24.383	.347
5 M	842	1.67	71.89	1.068	1.784	26.167	.364
BSD	785	1.56	73.45	1.275	1.989	28.156	.383
6 M	642	1.27	74.72	1.830	2.324	30.480	.408

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)

Q=QUANTITY (% of Total Products)

S = SUMMATION

MILL
TEST
WHEAT

K.S.U. PILOT MILL
NO. 1C 1:1 DIFF
HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QXA
			MEDIUM P	RE-BREAK			
FSB	1272	2.61	2.61	.23	0.60	0.60	.230
1 MT	5163	10.58	13.19	.25	2.65	3.25	.246
1 MB	692	1.42	14.61	. 25	0.36	3.60	.246
FST	5091	10.43	25.04	.27	2.82	6.42	.256
2 MT	5293	10.84	35.88	.27	2.93	9.34	.260
2 MB	445	0.91	36.79	.29	0.26	9.61	.261
3 M	3733	7.65	44.44	.31	2.37	11.98	.270
CSB	13	0.03	44.47	.33	0.01	11.99	.270
2 Q	768	1.57	46.04	.33	0.52	12.51	.272
BK.RED	1172	2.40	48.44	.34	0.82	13.32	.275
4 M	2148	4.40	52.84	.36	1.58	14.91	.282
2 BK	1577	3.23	56.07	.37	1.23	16.14	.287
3 BK	1563	3.20	59.27	.37	1.18	17.32	.292
CST	381	0.78	60.05	.37	0.29	17.61	.293
1 BK	1110	2.27	62.32	.38	0.86	18.47	.296
P.BK	154	0.32	62.64	.43	0.14	18.61	.297
4 BK	987	2.02	64.66	.44	0.89	19.50	.301
1 T	451	0.92	65.58	.53	0.49	19.98	.304
SUC	137	0.28	65.85	.53	0.15	20.14	.305
5 M	700	1.43	67.29	.69	0.99	21.12	.313
5 BK	1047	2.14	69.43	.70	1.50	22.62	.325
6 M	880	1.80	71.23	1.07	1.93	24.54	.344
BSD	825	1.69	72.92	1.38	2.33	26.88	.368
		Welling Monty of the Princeton					

A=ASH(14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL
TEST
WHEAT

K.S.U. PILOT MILL
NO. 2C 1:1 DIFF
HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QXA
			HEAVY P	RE-BREAK			
FSB	1083	2.21	2.21	. 24	0.53	0.53	.240
1 MT	5392	11.02	13.23	.25	2.76	3.29	.249
1 MB	824	1.68	14.91	.25	0.42	3.71	.249
FST	5213	10.65	25.56	.26	2.77	6.47	.253
2 MT	4984	10.19	35.75	. 28	2.85	9.33	.261
2 MB	320	0.65	36.40	.29	0.19	9.52	.262
2 BK	1950	3.99	40.39	.31	1.24	10.75	.266
BK.RED	1583	3.24	43.63	.31	1.00	11.76	.270
1 BK	949	1.94	45.57	.33	0.64	12.40	.272
CSB	13	0.03	45.60	.35	0.01	12.41	.272
3 BK	1937	3.96	49.56	.35	1.39	13.79	.278
P.BK	700	1.43	50.99	.36	0.51	14.31	.281
3 M	2825	5.77	56.76	.37	2.13	16.44	.290
2 Q	299	0.61	57.37	.39	0.24	16.68	.291
CST	237	0.48	57.85	.41	0.20	16.88	.292
4 BK	1010	2.06	59.91	.46	0.95	17.83	.298
4 M	1488	3.04	62.95	.49	1.49	19.32	.307
SUC	120	0.25	63.20	.52	0.13	19.45	.308
1 T	384	0.78	63.98	.62	0.48	19.93	.311
5 BK	935	1.91	65.89	.72	1.38	21.31	.323
5 M	569	1.16	67.05	.75	0.87	22.18	.331
6 M	1106	2.26	69.31	.97	2.19	24.37	.352
BSD	1099	2.25	71.56	1.09	2,45	26.82	.375

Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)
Q=QUANTITY (% of Total Products)
S=SUMMATION

MILL
TEST
NO. 3C 1:1 DIFF
WHEAT
HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	Α	QXA	S of QXA	S of QXA
			NO PRE	-BREAK			
1 MT	5645	11.66	11.66	.23	2.682	2.682	.230
1 MB	780	1.61	13.27	.25	0.403	3.084	.232
FSB	1275	2.63	15.90	.26	0.684	3.768	.237
FST	5433	11.22	27.12	.27	3.029	6,798	.251
2 MT	4895	10.11	37.23	.30	3.033	9.831	.264
2 MB	241	0.50	37.73	.31	0.155	9.986	.265
3 M	4009	8.28	46.01	.32	2.650	12.635	.275
CSB	16	0.03	46.04	.35	0.011	12.646	.275
2 Q	613	1.27	47.31	.36	0.457	13.103	.277
2 BK	1374	2.84	50.15	.38	1.079	14.182	.283
BK.RED	1031	2.13	52.28	.38	0.809	14.991	.287
4 M	2200	4.55	56.83	.39	1.775	16.766	.295
3 BK	1360	2.81	59.64	.40	1.124	17.890	.300
1 BK	960	1.98	61.62	.41	0.812	18.702	.304
CST	392	0.81	62.43	.43	0.348	19.050	.305
4 BK	854	1.76	64.19	.46	0.810	19.860	.309
SUC	173	0.36	64.55	.53	0.191	20.050	.311
1 T	435	0.90	65.45	.54	0.486	20.536	.314
5 M	1352	2.79	68.24	.59	1.646	22.183	.325
5 BK	1097	2.27	70.51	.61	1.385	23.567	.334
6 M	972	2.01	75.52	1.16	2.332	25.899	.357
BSO	763	1.58	74.10	1.48	2.338	28.237	.381
A							
				1			

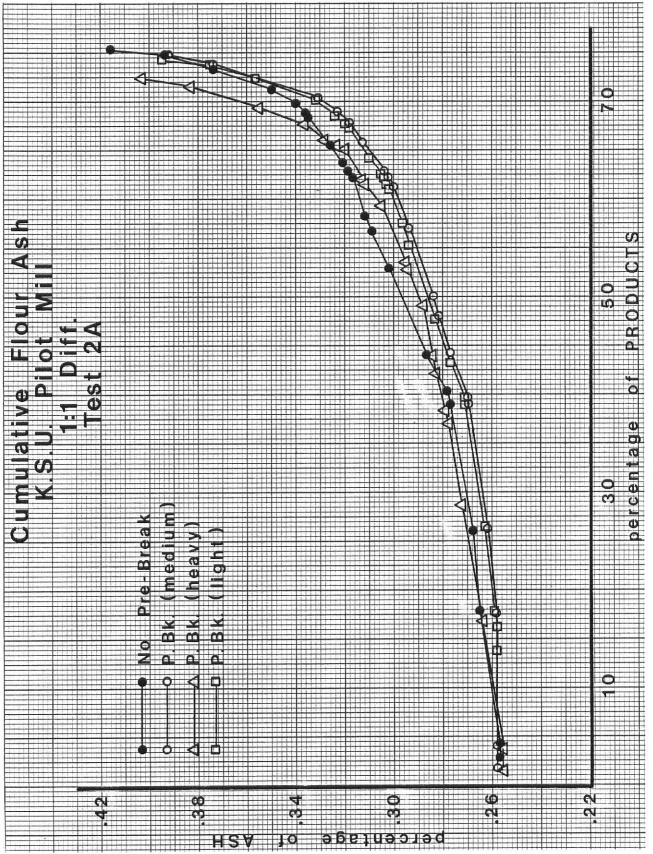
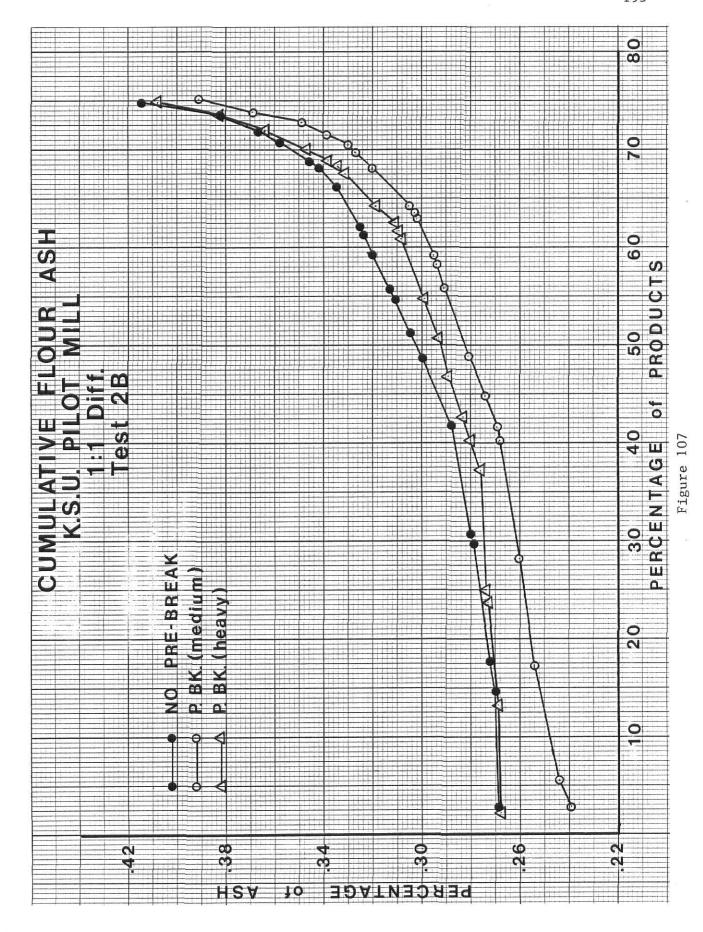
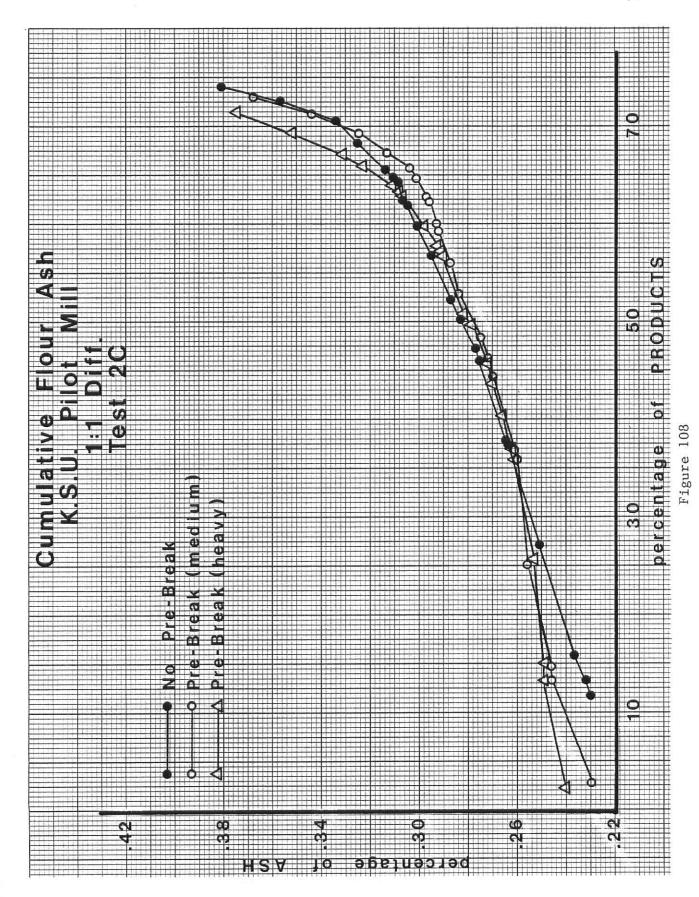


Figure 106





PRE-BREAKING: DOCUMENTING ITS EFFECTS

by

STEVEN P. CURRAN

B.S., Kansas State University, 1974

AN ABSTRACT OF A MASTER'S THESIS

submitted in partial fulfillment of the

requirements for the degree

MASTER OF SCIENCE

Department of Grain Science and Industry

KANSAS STATE UNIVERSITY
Manhattan, Kansas

The purpose of this research was to document the effect of Pre-Breaking wheat kernels prior to the actual milling process. Five different types of experimental mills were used for the testing. A Hard Red Winter Wheat was used for all of the milling.

The five experimental mills which were utilized for the testing are as follows:

- 1. Brabender Quadrumat Junior
- 2. Brabender Quadrumat Senior
- 3. Buhler Experimental Mill
- 4. Ross Mill Walking Flow
- 5. Miag Multomat

Testing on each mill involved milling with the whole wheat kernels going directly to the First Breaking operation, as in a normal milling operation, and milling with the whole kernels being slightly broken, or opened at the crease of the kernel, before proceeding to the First Break. This Pre-Breaking was accomplished using, in most cases, smooth 9" x 6" rolls operating at a one to one differential. Where possible the Pre-Broken stock was also sifted prior to milling; this being done to determine if sifting of the Pre-Broken wheat had any effects other than just simple Pre-Breaking.

Flours from each milling were weighed and analyzed for both moisture and ash content. Cumulative flour ash was then calculated for each milling. To analyze the effect Pre-Breaking had on milling quality for each test, cumulative flour ash was plotted against the cumulative percentage of total products.

The analysis of the test results showed that, in all cases, milling performance of the same wheat mix was improved by Pre-Breaking the wheat prior to milling. Flour ash content was significantly lowered and a slight improvement in total extraction was realized for the samples that

were Pre-Broken. Where sifting of the Pre-Broken wheat was done prior to milling, improvement was noticed over the samples that were Pre-Broken and not sifted.