

PRE-BREAKING: DOCUMENTING ITS EFFECTS

by

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## INTRODUCTION

The purpose of this study is to document the effects of a preliminary breaking of wheat kernels prior to the actual milling process. To further understand this study, a basic explanation of the processing of wheat to obtain white flour should be given.

Most flour milling operations can be divided into six systems: Break System, Middlings Reduction System, Sizings System, Purification System, Tailings System, and Low Grade System. Properly conditioned wheat is first worked upon by the Break System which functions to open the wheat kernel and release particles of endosperm known as sizings and middlings from the bran coat. The Break System can consist of three to seven passages which employ pairs of cylindrical corrugated rolls, called roller mills. The rolls rotate towards each other with one roll rotating about two and one-half times as fast as the other roll. The number of corrugations increases while the depth of the corrugations decreases after each succeeding break. After each grind, the ground material is sent to sifters consisting of sieves covered with various cloths to separate out the different particle sizes. The coarsest material, mostly bran with adhering particles of endosperm, is sent on to the next break. Chunks of endosperm from the Primary Breaks (normally First, Second and Third Breaks), varying in size and purity, are sent to the Purification, Sizing and Middling Reduction Systems. Material from the Secondary Breaks (Fourth and Fifth Breaks) which is more bran-contaminated, is sent to the Tailings and Low Grade Systems. Some flour, made incidently, is removed from each sifting.

In most mills making white flour, materials consisting of endosperm chunks and small bran chips is sent to a Purification System. Purifiers utilize both reciprocating sieves and air currents to grade the stock

further by size and to purify it by lifting off the lighter bran chips. Cleaned endosperm material is then sent to the Sizings or Middlings Systems, depending on the degree of purity.

The larger chunks of endosperm with some adhering bran is sent to the Sizings System. Here, smooth or finely corrugated rolls operating at a differential of about 1.5 to 1 reduce the large particles of endosperm somewhat and at the same time remove adhering bran which is also slightly flattened. Sifters then separate the reduced endosperm chunks (to be sent to the Middlings Reduction System) from the chips of bran and germ which are sent to the Tailings System. Although some high quality flour is recovered in the Sizings System, the main function is to release the endosperm from the chunks of bran and germ and reduce these sizings to middlings.

The primary function of the Middlings Reduction System is to produce flour. Normally, middling stock is ground on smooth rollermills, operating at a differential of 1.5 to 1, set to produce the optimum amount of flour. Any small particles of bran or germ contained in the middlings stock are normally flattened by the rolls and scalped off to the Tailings System, while the middlings material that is not reduced to flour size is sent to the next middlings grind. A normal mill flow will contain four to five middling-reduction grinds with the amount of bran intrusion increasing with each successive pass.

The Tailings System receives stock that is mostly particles of bran with some adhering chunks of endosperm. The primary function is to recover any particles of endosperm to be returned to the Middlings System. The branny stock is sent to feed. A small amount of low quality flour is also

recovered. Again, smooth rolls operating at a low differential are normally used here.

The Low Grade System is the "finishing" system in the mill flow. Poorer quality stock, not reduced in the Middling-Reduction System, feeds the Low Grade System. The purpose here is to recover any flour produced and send the remainder to feed.

The total objective of milling wheat into white flour is to provide an acceptable, uniform product to the customer, be it the commercial or home baker. Acceptability can be based on many different criteria depending on the customer's needs. Ultimately, the successful miller utilizes all the resources available to him to produce the maximum amount of salable flour at the least cost of production.

The purpose of this investigation is to determine whether the preliminary breaking of the wheat kernel prior to the Breaking System in the mill flow is beneficial to the miller in achieving his goals.

## LITERATURE REVIEW

## Pre-Breaking

Although the concept of Pre-breaking is not a new one, there is virtually no published information on the subject. Commercial milling companies that utilize pre-breaking systems developed those systems for the most part on their own, and due to the competitive nature of the flour milling business, scientific literature on these systems is not readily available.

Kozmin (1), was the first known author to report on Pre-Breaking systems in discussions of some of the very first gradual reduction milling systems. He wrote, "As regards the character of reduction, high grinding (gradual reduction grinding) may be divided into four separate categories. In the first must be placed the breaking of the berry down the crease, which allows removal of dust settled in the crease from the halves, and otherwise inextractable in the cleaning process." He stated further that the French called this passage "l'avant broyage" or preliminary break and the Germans labeled it "Hochshrot." Two of these very early flowsheets using Pre-Break systems are shown in plates 1 and 2. Flour removed from these Pre-Breaks was called "blue flour" due to the blue-grey appearance as compared to the other recovered flours. Smith (2) also reported that at the time of the introduction of the roller mill in England in 1879, first break was initially used as a cracking roll with the broken grain being sifted immediately to extract what was known as the blue flour or crease dirt. He reported that the technique was dropped due to improved wheat cleaning machinery.

In June of 1929, the National Miller (3) provided a "round table discussion" in which the topic was "Splitting the Wheat in the Crease."



PLATE 1

FLWSHEET OF GERMAN SHORT  
FLOW USING PRE-BREAK

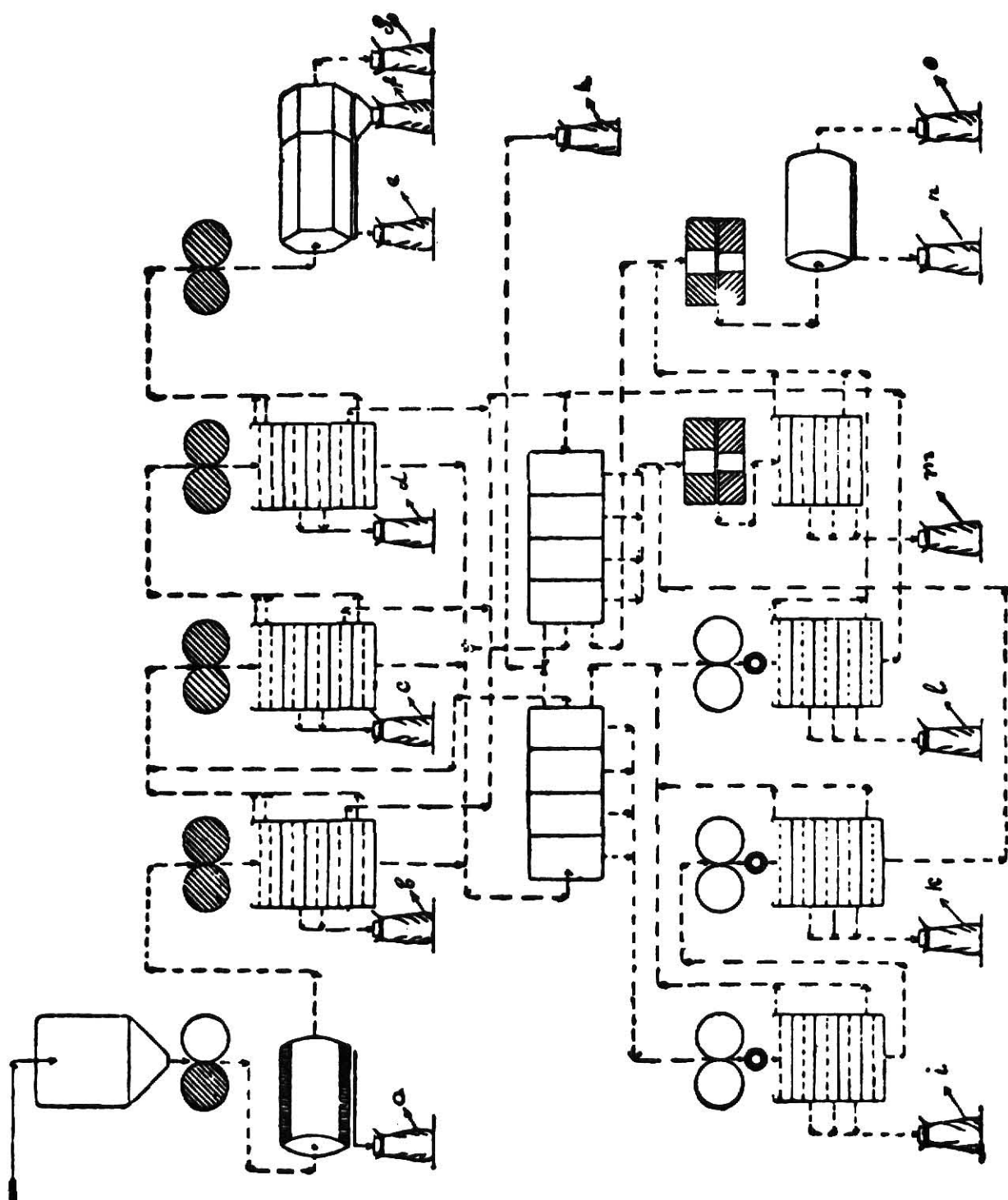


PLATE 1





PLATE 2

FLowsheet of a German  
ABRIDGED HIGH GRINDING FLOW  
USING PRE-BREAK

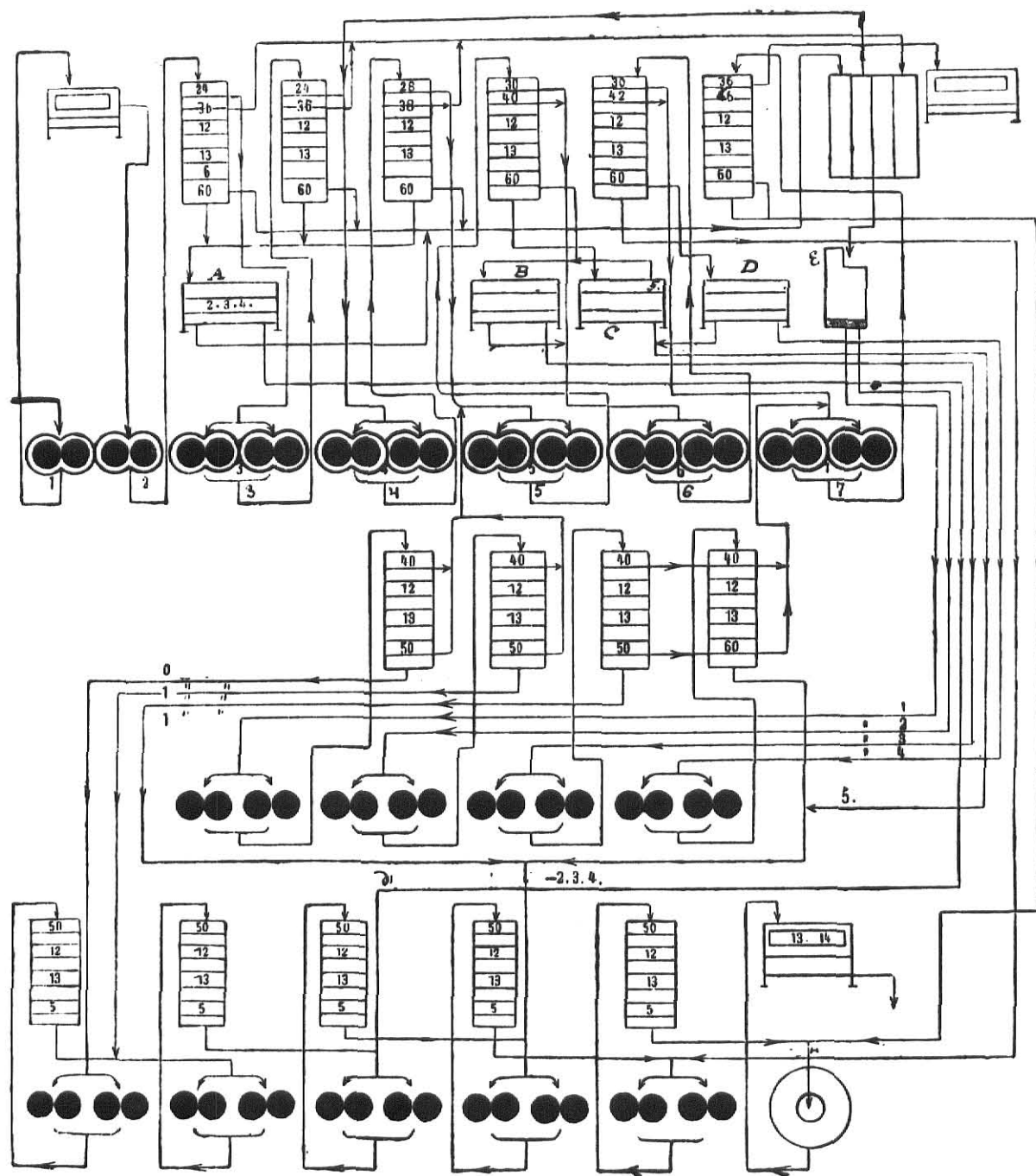


PLATE 2

Opinions of about 50 prominent millers were provided. The majority of the millers at this time felt it was not advantageous to Pre-Break the wheat. Of those that felt it would be advantageous to Pre-Break, most stated that it both removed crease dirt and made a broader bran. Two months later, August of 1929, in an article further discussing the splitting or Pre-Breaking of wheat, Reed (4) reported that the idea was sound, but that what was needed was a machine that could accurately split the wheat through the crease and remove all of the seam impurities and germ. He also finished by saying this couldn't be done.

From these early mentions of pre-breaking, there seems to be no other information published on the subject for a period of about 20 years. Even flow sheets available, dating to this period in time, do not show any use of Pre-Break Systems. In 1952, Farrell and Milner (5), in a survey of U.S. Flour Mills, found that some of the mills were using different forms of Pre-Break systems to help alleviate the problem of insect fragments in the finished flour. These systems utilized impact machines, generally known as entoletters, or rolls, or in some instances both were being used. The wheat was being cracked open by the entoletters or rolls and then followed with aspiration and/or sifting to remove small streams high in insect material. The surveyors gave no particular preference for either the rolls or entoletters but noted there were many variables influencing the effectiveness of the entoletter. Rolls were usually nine or ten inches in diameter and operated at approximately one to one differential. Roll surface was either smooth or finely corrugated with no spiral. Most importantly, the surveyors pointed out that some milling advantages other than insect fragment removal might also accrue from the practice of Pre-Breaking. They stated, "Advantages of pre-breaking claimed by some millers

include increase in percentage of patent flours and increase in germ recovery with the resulting benefit of grinding less germ into the flour."

In a report on the use of impact machines for "Pre-Milling Control," Zerull (6) pointed out the advantages of such systems to be better mill balance, cleaner middlings, lower ash due to the removal of more crease and germ end dirt and due to the better recovery of germ before the breaking process.

It is not known, exactly, the percentage of Pre-Break Systems in use today in commercial flour mills. In a survey by the Association of Operative Millers Technical Committee (7), Association members were sent questionnaires asking them to provide the information necessary to construct a flow sheet for a new 5000 hundredweight of flour per day flour mill. Approximately 65 percent of those respondents reported that they would use some form of Pre-Break, either roller mills or impact machines. This may give some approximation as to the actual use of Pre-Break Systems in commercial mills today.

#### Experimental Milling

Since data from commercial mills is difficult to obtain, testing must be performed on smaller scale experimental mills. The question then arises, "Are experimental mills reliable enough to accurately predict the results of comparable tests on commercial mills?" Anderson (8) related it best when he stated, "The problem then in Experimental Milling resolves itself into the use of a minimum number of basic milling operations to secure results which furnish advance information concerning what will be obtained when wheat from the same mix is milled on the longer commercial system. . . ."

Miller (9) believed that experimental milling represents experimentation on a small scale; however, without it commercial milling itself would be largely experimental.

Rumold (10) stated that experimental milling can provide the miller with advanced milling data and mill chemists with material for analytical investigation. Herman (11) also believed that experimental milling can foretell in close approximation milling quality, yield of wheat and the characteristics of flour from it.

Zeleny (12) states that milling quality can be directly determined by means of experimental milling tests. He also reported that many commercial millers have been reasonably successful in adjusting and operating experimental milling equipment in such a manner that yield and quality of experimentally produced flours closely parallels the yield and quality of commercially produced flours.

The yield of flour and the ash conversion, according to Anderson (8), are two factors which should be observed in experimental milling.

#### The Ash Test and Cumulative Ash Curves

Once the wheat to be tested has been experimentally milled, the flours must be analyzed to determine if there are any quality differences between the control sample and the test sample. As mentioned earlier, the percentage yield of each flour stream and the ash content of each flour stream are important factors. The yield of each flour stream is self-explanatory but what is ash and why is it useful in studying milling performance and processes?

The Ash test (A.A.C.C. Cereal Laboratory Methods, 08-01) gives a measure of the mineral content of the material being tested. Since pure bran material contains, according to Swanson (13), from 20 to 25 times as

much ash as the pure endosperm, the Ash test has been used as a tool in measuring the amount of bran intrusion in the flour tested.

In the milling operation, a flour is produced each time material is ground and sifted. Commercial mills may have between 20 to 40 different flours being produced at the same time, each with different characteristics, including fairly wide differences in ash content. Since each mill stock classification to be ground has a different bran-to-endosperm ratio, each grind will produce varying amounts of bran intrusion. The breaking process seems to be most critical in this area. Robbins (14) states that "in the final analysis all ash in flour, other than that contained in the pure endosperm, is caused by bran contamination released by the breaks."

The germ of the wheat kernel is also relatively high in ash content. According to MacMasters et al. (15) the ash content of wheat germ in 156 different varieties was found to vary between 4.27 to 9.47% in ash content. This would mean that any germ ground by the corrugated break rolls could also contribute to the ash content of the break flours.

The ash content of pure endosperm also varies within the kernel itself. Morris et al. (16) reported spreads from .246% to .400% ash in Hard Red Winter wheat and spreads from .206% to .564% ash in Hard Red Spring wheat within the endosperm.

Due to the obvious complication of properly applying the ash test, it has been, throughout the years since its inception, misapplied in many instances. However, if properly applied it can be a useful tool. Clark (17) states: "Combined with the knowledge of yield, percentage of extraction, grade of wheat milled, variety of wheat milled, and the equipment of the mill, flour ash may be an index of efficient wheat milling." Shuey (18) believes that when ash is properly used it can be a useful tool or

yardstick for measuring milling characteristics as well as evaluating the milling performance of a mill. Swanson (13) also states, "The Ash test has a greater value than any other analytical determination for the control of the mechanical operation of the flour mill."

A simple listing of the ash content of each stream, however, is of little value. Therefore, methods of coupling the amount of ash contents with the corresponding stream weights have been devised that are of much greater value. Robbins (14) indicates that an ash analysis of the various flour mill streams in a mill when made in connection with a quantity measure of each stream is the most effective means available for studying the ash characteristics of the milling process.

Wissmar (19), believes that the Cumulative Ash Curve, developed by Professor Mohs, can be most useful to analyze mill efficiency. In this analysis, all the ash contents are arranged, lowest to highest ash, along with their corresponding percentage of the total of the milled products. Starting with the lowest ash stream, the next lowest ash stream is, in effect, blended with it to produce a new flour. This is continued until all the flour streams are added in at their corresponding percentages. Cumulated ashes can then be plotted versus their cumulated percentages to give the Cumulative Ash Curve which can be used to judge the effectiveness of milling processes given a common wheat.





PLATE 3

PHOTOGRAPH OF WHOLE HARD RED WINTER WHEAT KERNELS  
COMPARED WITH WHEAT AFTER PASSING  
THROUGH PRE-BREAK ROLLS

PLATE 4

PHOTOGRAPH OF A STRAIGHT GRADE HARD RED  
WINTER FLOUR AS COMPARED TO FLOUR PRODUCED  
FROM PRE-BREAKING FROM THE SAME WHEAT,  
THE PEKAR TEST WAS USED TO SHOW  
DIFFERENCE IN QUALITY

**PLATE 3**

Whole Wheat

Pre - Broken Wheat



Straight Grade Flour

Pre - Break Flour

**PLATE 4**

## MATERIALS AND METHODS

### Wheat

Several varieties of locally grown Hard Red Winter wheat were used for the milling tests. Table I shows some of the physical wheat data for the wheats used. The wheat used is typical of that used commercially for white flour production.

All wheat was cleaned in the Kansas State University Pilot Cleaning House. This flow includes a milling separator, stoner and gravity table, disc machines, Entoleter-Scourer, Aspirator and duo-aspirator. The Flow-sheet is shown in Figure I. The cleaning rate is 60 pounds per minute.

Wheat was conditioned prior to milling by adding water to bring the percentage of moisture in the wheat to about 16%. The wheat and water were thoroughly mixed and then allowed to rest for approximately 20 hours. For the large scale samples, on the Miag Multomat, the Kansas State University Tempering System (Figure I) was used. The remainder of the samples were tempered using a laboratory tempering system which consists of a small revolving drum and graduated cylinder, for metering the water. Since the capacity of the mixer is approximately 5000 grams, any sample lots needed over this amount were first mixed and then cross blended to assure even temper. Sample lots were then stored for the rest period in poly bags. Both initial moisture and moisture before milling were measured on the Tag-Heppenstal Moisture Meter.

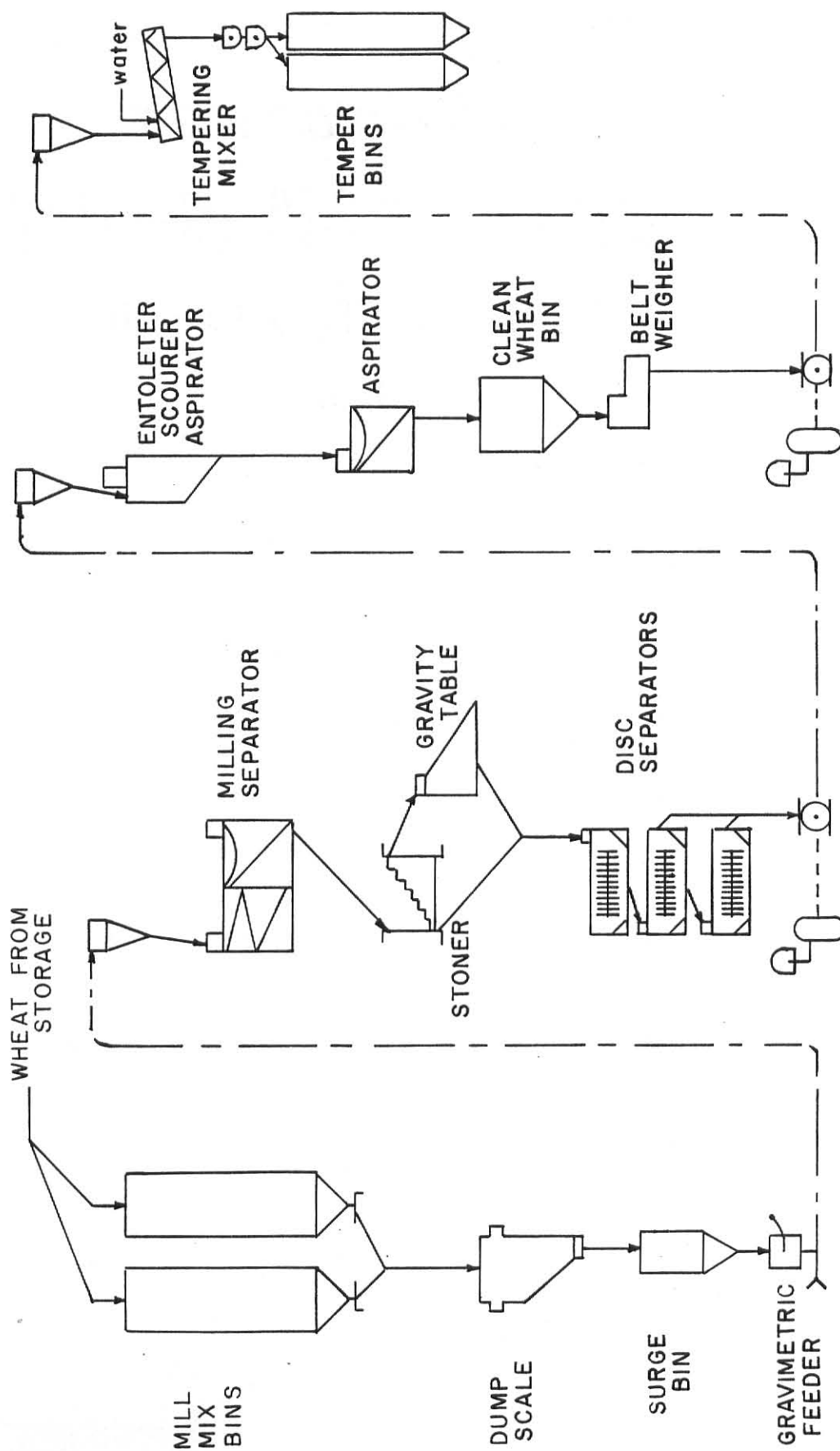
### Pre-Breaking

Since it was felt that there may be too many variables in the operation of an impact machine, the rollermill was selected to perform the pre-breaking. In most cases, smooth rolls were driven at approximately a one to one differential and set to ideally open all kernels at the crease.

TABLE 1  
WHEAT SPECIFICATIONS

<u>TEST</u>	<u>RESULTS</u> <sup>1</sup>
Moisture <sup>2</sup>	12.4%
Protein <sup>3</sup>	12.5%
Ash <sup>4</sup>	1.5%
Test Weight <sup>5</sup>	62.3 lbs/bushel
1000 Kernel Weight <sup>6</sup>	31.3 gram/1000 kernels
Wheat Size Test <sup>7</sup>	
% Over 7W	70.0%
% over 9W	29.5%
% over 12W	0.5%
Theoretical Yield	76.5%
Pearling Value <sup>8</sup>	74.7%

1. Results given are the averaged results of three samples tested.
2. Tag-Heppenstal Moisture Tester.
3. AACC Cereal Laboratory Methods, 46-10. Expressed as percent protein on a 14% moisture basis.
4. AACC Cereal Laboratory Methods, 08-01. Expressed as percent ash on a 14% moisture basis.
5. As described in Circular No. 921, issued by the United States Department of Agriculture. Expressed as pounds, to the nearest tenth of a pound, per Winchester bushel.
6. 40 grams of whole, cleaned wheat is counted using an electronic seed counter. The number of kernels in 40 grams is then converted to the number of grams per 1000 kernels.
7. 200 grams of cleaned wheat is sifted for 1 minute using a Ro-Tap Shaker and 3 Tyler sieves of 7 wire, 9 wire, and 12 wire. The percentage remaining on each sieve is then determined, multiplied by factors of 78, 73 and 67, respectively, and summed to obtain a single number denoting the theoretical flour yield.
8. 20 grams of cleaned, whole wheat is retained for one minute in a Strong Scott Laboratory Barley Pearler equipped with a No. 30 grit stone and 1 10 mesh screen made of wire .041 inches in diameter (Tyler Code "Fijor"). Pearling value is the percent of original sample remaining over a 20 mesh wire after pearling.



Kansas State University Cleaning and Tempering System

Figure 1



Plate 3 shows wheat after passage through a pre-break versus the whole wheat.

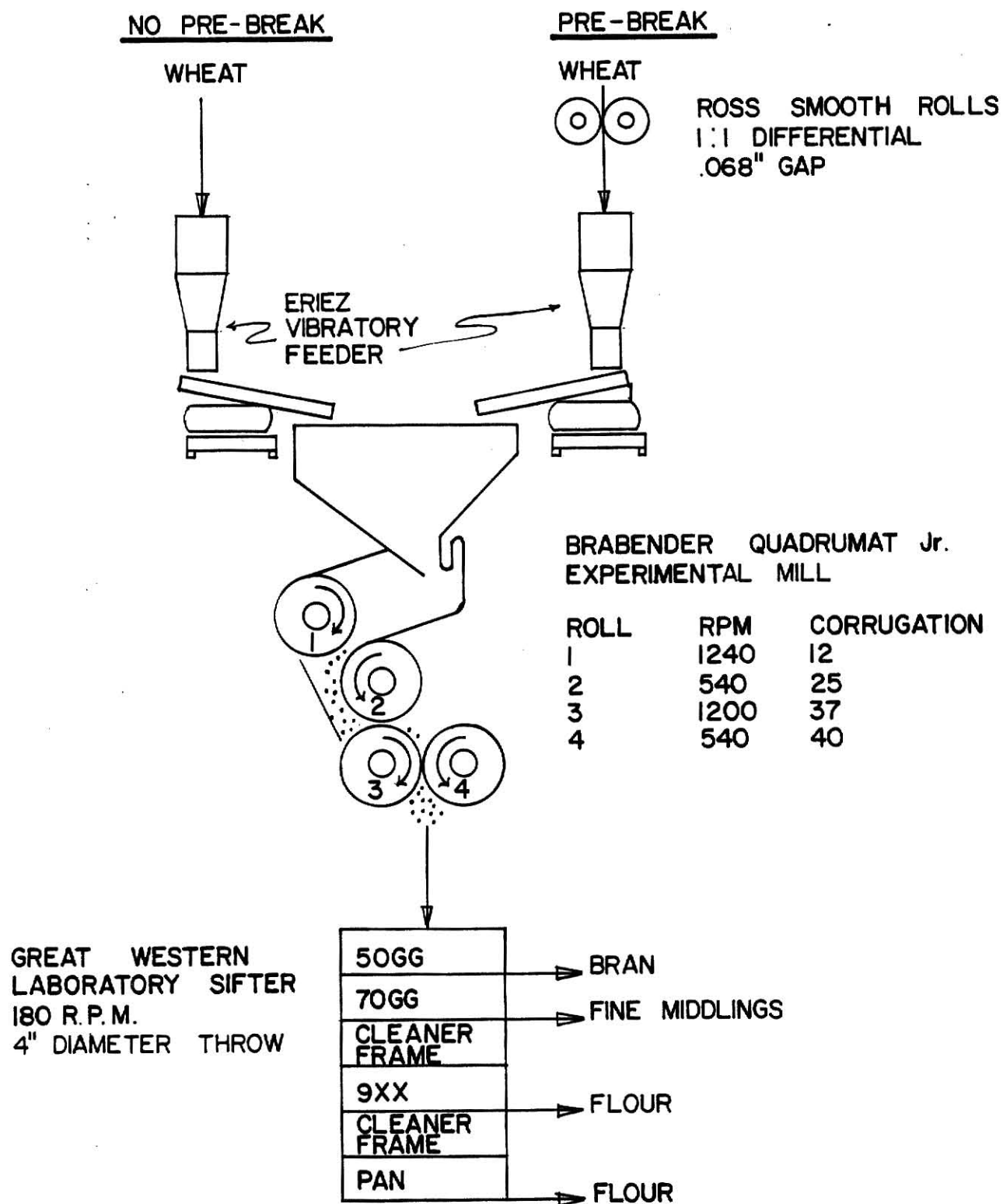
### Milling

Five different experimental mills were used in this research: Brabender Quadrumat Junior, Brabender Quadrumat Senior, Buhler Experimental Rollermill, K.S.U. Ross Walking Flow, and Miag Multomat. Since each mill employs a different method of operation and procedure of testing, each will be described separately.

#### (1) Brabender Quadrumat Junior (Figure 2, plate 5)

As can be seen from the flowsheet, the Quadrumat Junior makes three grinds with four corrugated rolls at a fixed gap before the stock is sifted. Normally, the ground material is sifted over a reel-type sifter that is part of the mill. To provide a better separation, the ground stock was sifted using a Great Western laboratory sifter having a speed of 180 rpm and throw of 4 inches. Sieves of 50 grits gauze, 70 grits gauze, and 9XX silk were used to make the separations, with cleaner frames below the 70GG and 9XX to aid in sifting. Sifting time was set at two minutes.

A Ross Experimental Rollstand, equipped with a pair of 9-inch diameter by 6-inch wide smooth rolls, was used to Pre-Break the wheat prior to milling on the Quadrumat Junior. The differential chain had been removed to give an approximate 1:1 differential, with the passage of the wheat turning the slow roll. A no load gap of .068 inch was chosen to perform the Pre-Breaking operation. This gap was used because it affected nearly every kernel to some extent but was not so severe that kernels were completely broken up.



FLWSHEET FOR BRABENDER QUADRUMAT JUNIOR.

Figure 2





PLATE 6

VIEW OF BRABENDER QUADRUMAT  
SENIOR EXPERIMENTAL MILL  
SHOWING SPECIAL FEEDING SYSTEM

PLATE 5

VIEW OF BRABENDER QUADRUMAT  
JUNIOR EXPERIMENTAL MILL

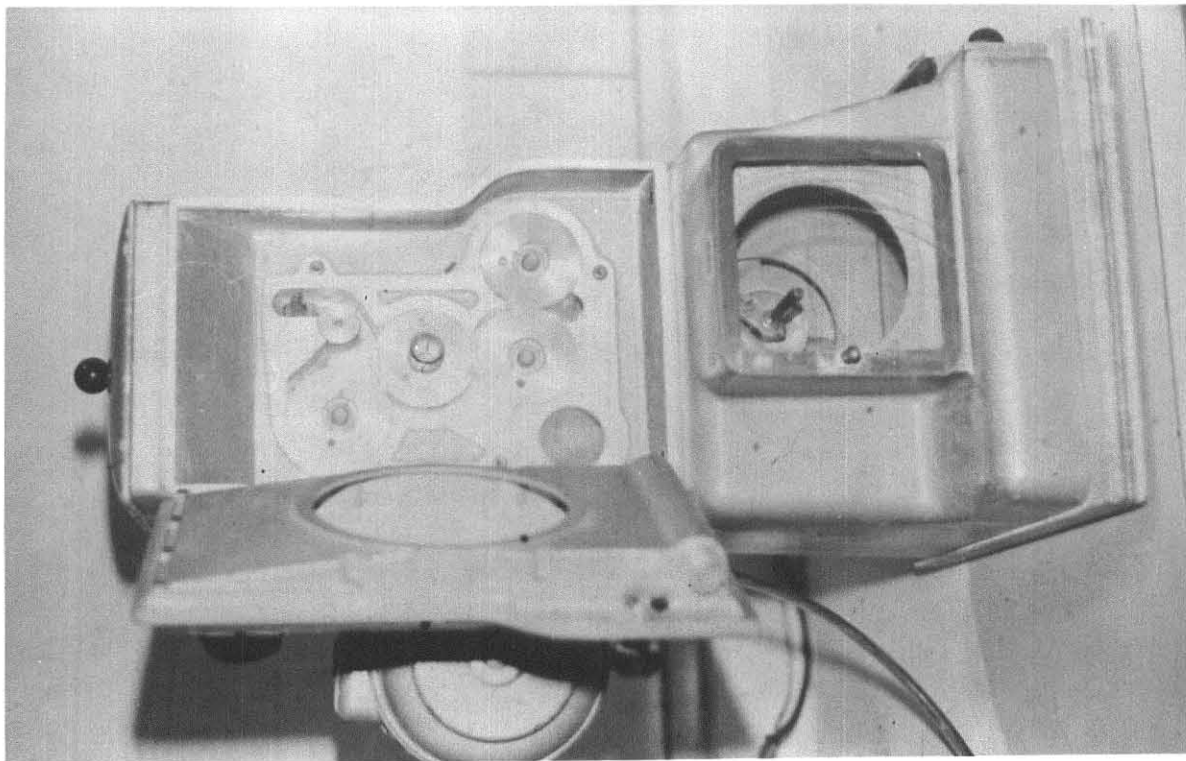


PLATE 5

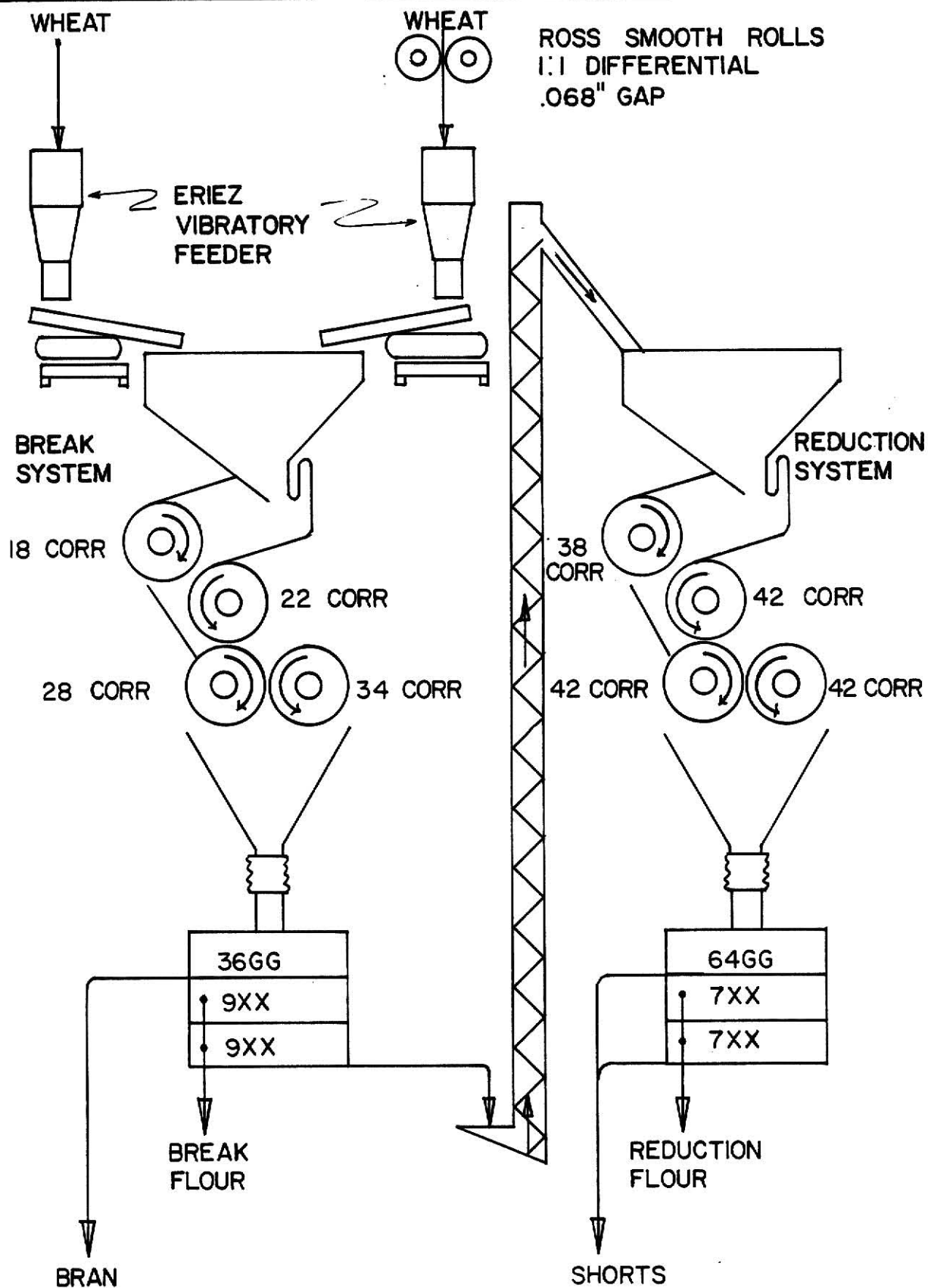


PLATE 6

NO PRE - BREAK SYSTEM

PRE - BREAK SYSTEM

23



FLWSHEET FOR BRABENDER QUADRUMAT SENIOR.

Figure 3

Since the flowability of the Pre-Broken wheat changed drastically, a further modification of the Quadrumat Junior had to be made. To allow the stock to flow properly, the feeder roll had to be removed. An Eriez vibratory feeder, with variable speed control, was then used to set the flow of whole wheat or Pre-Broken wheat to the mill. A feedrate of approximately 55 grams per minute was used for the grain to the mill.

After the feed rate was established, by running one minute tests, the mill was started and the feeder was set to run for exactly five minutes. The first five minute sample was set aside as the warm-up sample. A second five minute sample was then milled and sifted on the stack of sieves. Each separation was carefully weighed and the three finest separations were sampled and submitted for laboratory moisture and ash analysis. The feeder was then reset to deliver Pre-Broken wheat at the same feed rate. Again, a warm-up sample was first milled prior to milling the test sample. The test sample was sifted and the same fractions sampled for analysis. A total of five whole wheat samples and five Pre-Broken samples were milled with warm-up samples preceding each test run.

## (2) Brabender Quadrumat Senior (Figure 3, plate 6)

As can be seen from the flowsheet and photograph, the Quadrumat Senior is similar to the Quadrumat Junior but utilizes more elaborate grinding and sifting equipment. Two grinding heads are used, one for Break grinding and one for Reduction grinding. Again, all rolls are corrugated and positioned at a fixed gap. A gyratory sifter, having a speed of 240 rpm and throw of 1-3/4 inches, is equipped with specially designed sieves for maximum efficiency.

Ground material from the Break head is sifted over 36 grits gauze to remove the bran and over two 9XX silks to remove the Break flour.

Middlings stock remaining above the 9XX is conveyed, by a vertical screw conveyor to the reduction head. Ground middlings from the Reduction head are then sifted over a 64 grits gauze and two 7XX silks. Any material not passing through the 7XX as flour is considered shorts.

As in the procedure for the Quadrumat Junior, a smooth pair of Ross rolls, running at a 1:1 differential, was used to Pre-Break the wheat. The roll gap of .068 inch was again used as the roll setting.

The Eriez vibratory feeder had to be used for feeding the stock to the mill due to the flow problem of the Pre-Broken wheat as developed in the Quadrumat Junior testing. The feeder roll from the Break head was also removed.

The testing procedure itself began by adjusting the vibratory feeder to a feed rate of approximately 130 grams per minute with whole wheat. The mill was then started and wheat was fed to the Break head for warm-up. The vibratory feeder was automatically timed to stop at the end of five minutes. When feed to the mill stopped, the mill was immediately shut down under load. Material from the four product containers was removed and the containers were replaced. The mill was then restarted and wheat was re-fed to the Break head to start the test sample. Again, at the end of five minutes, the feeder was stopped and the mill was shut down under load. The product containers were removed and the materials weighed. Samples of Break flour and Reduction flour were submitted to the analytical laboratory for moisture and ash analysis.

The feeder was then readjusted to feed the Pre-Broken wheat at 130 grams per minute and the above procedure was then repeated. The whole wheat and Pre-Broken wheat each was milled a total of five times.

(3) Buhler Experimental Mill (Figure 4, plate 7)

The Buhler Experimental Mill flow is somewhat different from the mill flows previously described. In the first two mills described, all the grinding is performed before any sifting. The Buhler flow provides grinding and sifting combinations much like those of a commercial mill. There are three corrugated break rolls and three smooth reduction rolls each with their own sifter section. Material to each roll is transported pneumatically. The six flours produced are collected individually in pans as are the feed products: bran and shorts.

Besides testing the effect of not Pre-Breaking the wheat prior to milling versus the effect of Pre-Breaking, a new variable was added. Pre-broken wheat was also sifted over a 10XX flour silk before being milled. This was done to determine whether removing the small amount of flour produced by Pre-Breaking would have any different effect on total flour quality. Some Pre-Break flour is shown in plate 4 compared to a straight grade flour.

Two thousand grams of the sample to be milled was placed in the feeder hopper and the feed rate set to approximately 125 grams per minute. The mill was then started and adjusted to provide proper milling classifications. When the feeder hopper emptied, the mill was immediately shut down under load. Product in the sample pans was weighed and recorded as "warm-up." A second 2000 gram sample of the same material was then placed in the feeder hopper and the mill was restarted. Again, as soon as the sample emptied from the hopper, the mill was shut down under load. All products from this milling were carefully weighed and samples of each of the six flours were submitted for moisture and ash analysis.

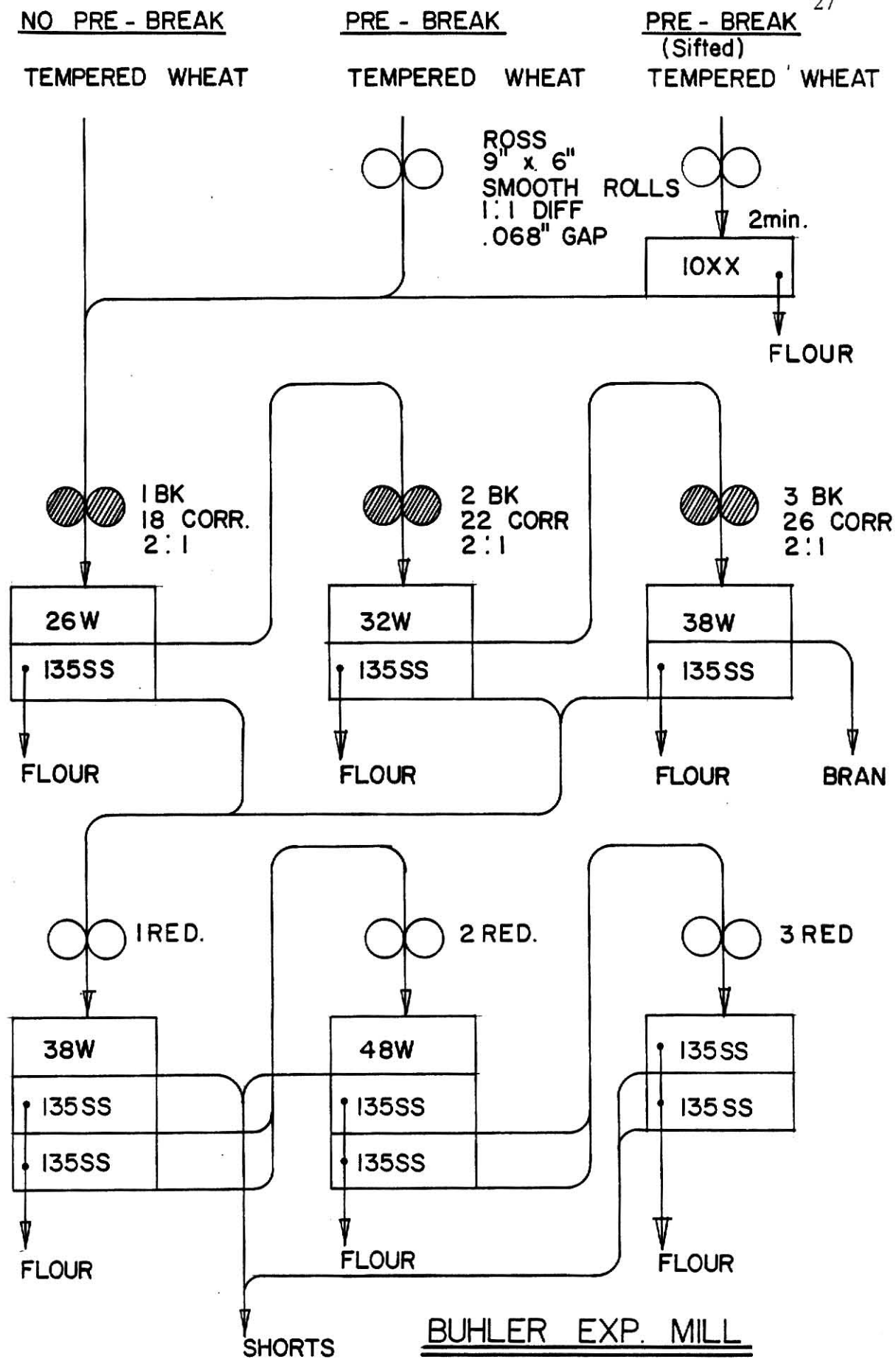


Figure 4





PLATE 7

VIEW OF BUHLER EXPERIMENTAL MILL

PLATE 8

VIEW OF ROSS EXPERIMENTAL  
ROLL STANDS

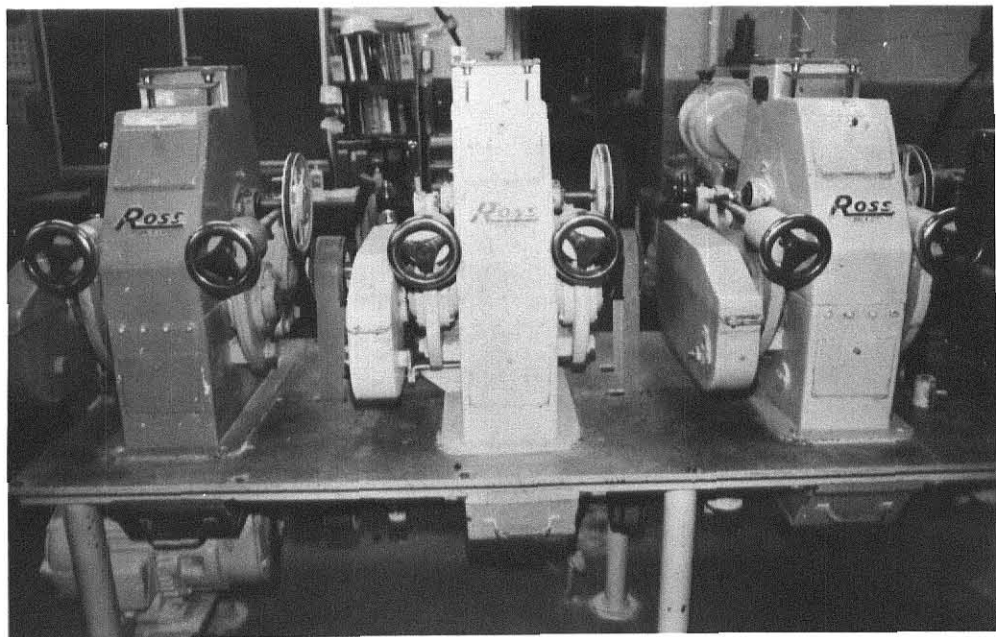
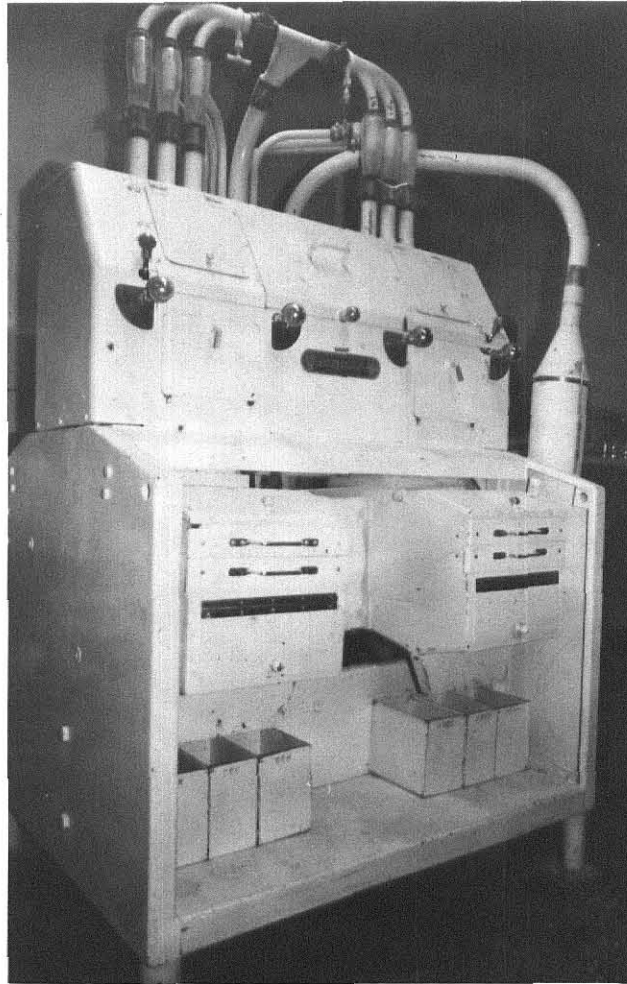


PLATE 8

TEMPERED  
WHEAT

TEMPERED  
WHEAT

TEMPERED  
WHEAT

30

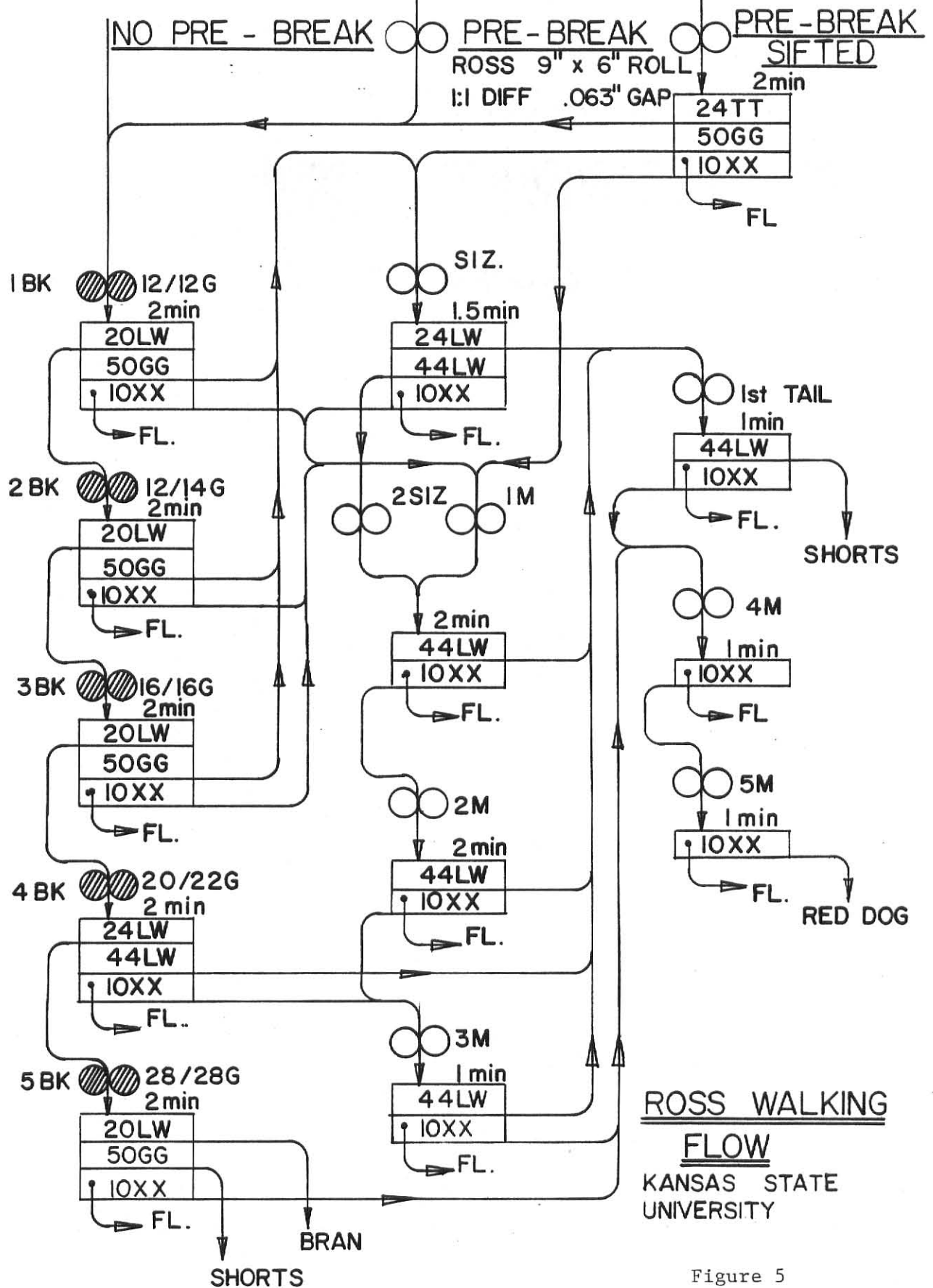


Figure 5

The sequence in which the control and the two experimental samples were milled was changed for each day of milling. To provide further check on the milling, an extra sample of the first sample milled for that day was also milled. This series of four millings was performed a total of five times as follows:

<u>Test A</u>	<u>Test B</u>
(1) No Pre-Break	(1) Pre-Break (sifted)
(2) Pre-Break (not sifted)	(2) No Pre-Break
(3) Pre-Break (sifted)	(3) Pre-Break (not sifted)
(4) No Pre-Break	(4) Pre-Break (sifted)
<u>Test C</u>	<u>Test D</u>
(1) Pre-Break (not sifted)	(1) No Pre-Break
(2) Pre-Break (sifted)	(2) Pre-Break (sifted)
(3) No Pre-Break	(3) Pre-Break (not sifted)
(4) Pre-Break (not sifted)	(4) No Pre-Break
<u>Test E</u>	
(1) Pre-Break (sifted)	
(2) Pre-Break (not sifted)	
(3) No Pre-Break	
(4) Pre-Break (sifted)	

Again, the smooth Ross rolls set at a .068 inch gap were used to perform the Pre-Breaking prior to milling on the Buhler Mill. A Great Western laboratory sifter was used to sift the pre-broken sample. Flour obtained from this sifting was weighed and analyzed.

(4) K.S.U. Ross Walking Flow (Figure 5, plate 8)

Although it is a batch operation rather than a continuous one, the Ross Walking Flow very closely simulates a full scale mill. As can be seen by the flowsheet, there are five Breaks and eight Reductions producing twelve flours, red dog, shorts and bran. Roll corrugations and differentials are given in the flowsheet.

Stock is fed by feeder rolls above each pair of rolls and the resulting ground material is caught in drawers below each roll stand.

The ground stock is then transferred to a sifter to make the size separations.

Break rolls were set according to a Break Release Schedule. A 100-gram sample of each Break Stock was ground on the proper roll and then sifted for 20 seconds over a 20 light wire sieve. The overs and thrus were then weighed to determine the percentage that had passed through the wire cloth, that being referred to as the amount "released." The rolls were then readjusted, if needed, to meet the desired release. The Break Release schedule used for the Roll Walking Flow is given as follows:

% -20 L.W.

1st Break	30
2nd Break	40
3rd Break	35
4th Break	20
5th Break	±30

Sizings rolls were set at a standard gap of .005 inch while second sizings and first tailings were standardized at .003 inch gap. All other rolls were set at less than .002 inch to produce as much flour as possible without producing flakes.

Sample size was 3000 grams. Since the Great Western laboratory sifter used here could not properly sift this amount, the sample was divided into two parts for First, Second and Third Breaks, Sizings and First Midds. The sifting times are listed on the flowsheet above each sifter box designation.

All stocks waiting to be ground or sifted were kept in aluminum cans with tight lids to keep moisture loss to a minimum. Each rollermill was cleaned thoroughly above and below the rolls to keep product loss to a minimum.

Three conditions were tested using the Ross Walking Flow. First, wheat was sent directly to First Break for the "No Pre-Break" test. Second, wheat was Pre-Broken on the Ross smooth rolls at a .068 inch gap and then sent directly to First Break. Third, Pre-Broken wheat was sifted over a special stack of sieves to remove Sizings stock, Middlings stock and flour before being sent to First Break. These flows are shown in Figure 5.

All three test conditions were milled in one day. The tests were repeated a total of five times, each time milling the samples in a random order. After weighing, each flour was sampled and submitted to the analytical laboratory for moisture and ash analysis.

(5) Miag Multomat Experimental Mill (Figure 6, plates 9 and 10)

The Multomat Experimental Mill is a three-break, five-reduction pneumatic mill. There are ten sifter sections, two of which are redust sections. Speed of the sifter is 260 rpm at a 1-7/8 inch throw. The ten flour streams are collected in pans beneath the sifter sections. This being one of the largest of the experimental mills, feed rates from 700 to 1000 grams per minute may be used. The rate of wheat to the mill is set by a Draver-type Feeder, which for these tests was set to deliver approximately 780 grams per minute.

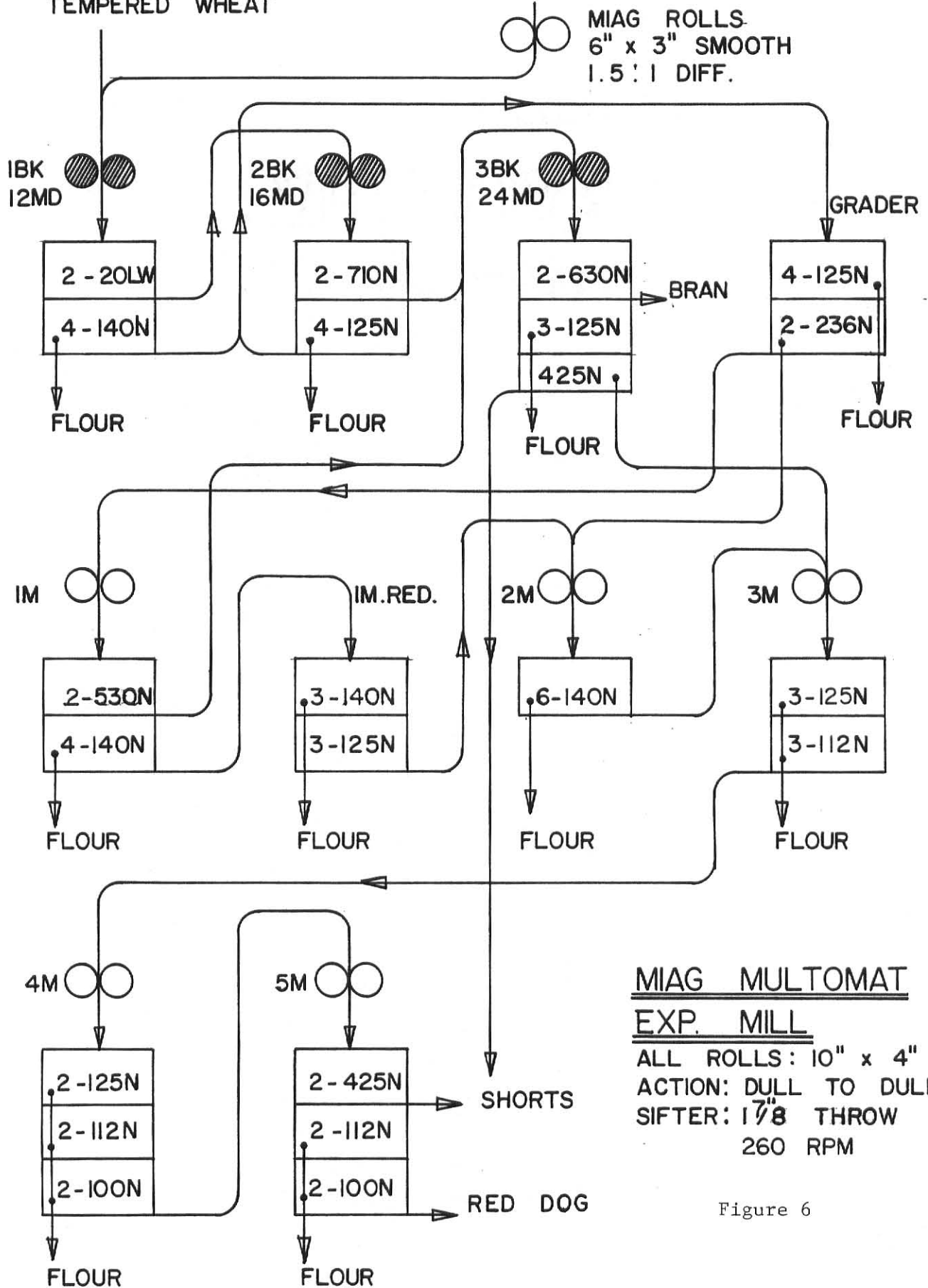
The Break rolls were set according to a Break Release Schedule during operation. One-hundred grams of each break grind was sifted over a 20 mesh light wire for 20 seconds on a Rotomatic laboratory sifter operating at 180 rpm and 1-7/8 inch throw. The amount of material passing through the sieve was determined and the rolls were set to meet the following Break Release Schedule:

First Break	45%
Second Break	50%
Third Break	±35% (clean-up)

NO PRE - BREAK  
TEMPERED WHEAT

PRE - BREAK  
TEMPERED WHEAT

34



MIAG MULTOMAT  
EXP. MILL

ALL ROLLS: 10" x 4"  
ACTION: DULL TO DULL  
SIFTER: 17/8" THROW  
260 RPM

Figure 6



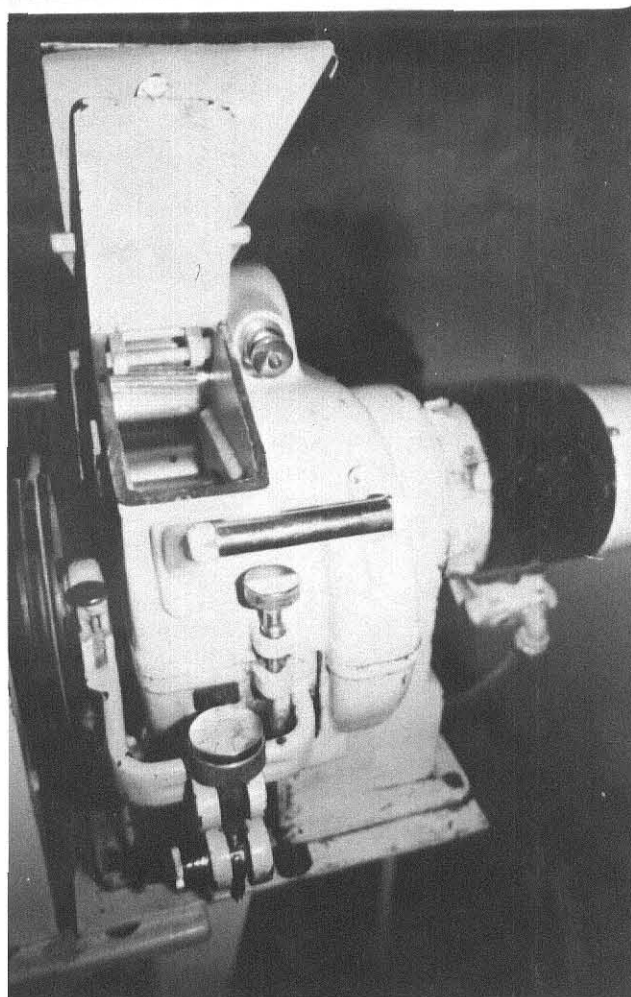
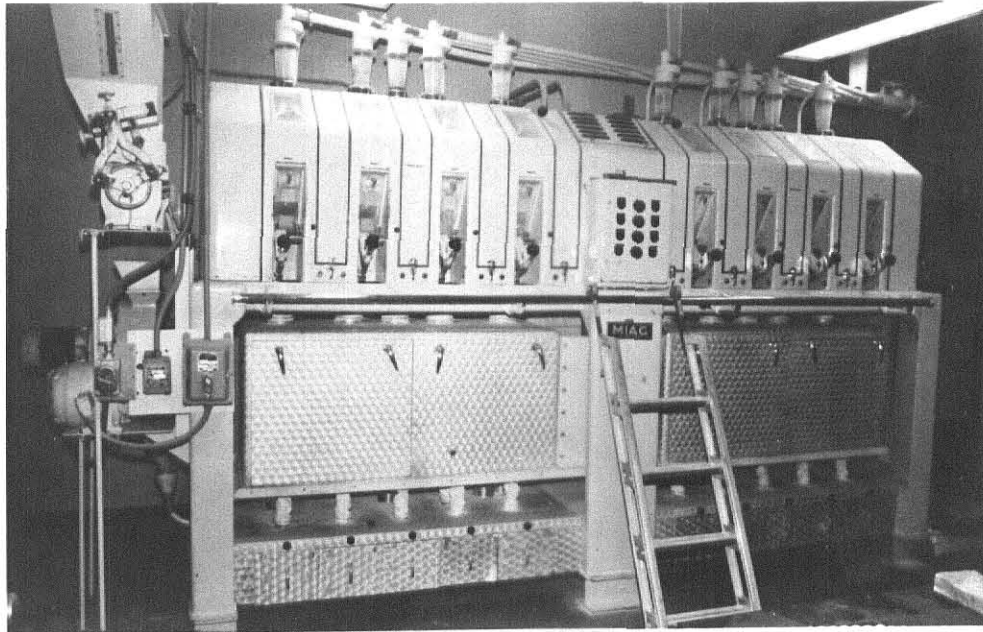


PLATE 9

PHOTOGRAPH OF THE MIAG MULTOMAT  
EXPERIMENTAL MILL

PLATE 10

PHOTOGRAPH OF MIAG PRE-BREAK ROLLS  
FOR THE MIAG MULTOMAT



Due to the relatively long reduction system on this mill, First Midds roll was set to grind to that more typical of a Sizings grind. The remaining rolls were set to produce flour.

This particular mill has been equipped with its own Pre-Break System (plate 10). Wheat from the feeder is fed directly to a pair of smooth six inch diameter by three inch wide rolls operating at a 1.5 to 1 differential. The grind on the Pre-Break roll was set with the use of a test sifter to give a two to three percent release through a 20 mesh light wire. The rolls could also be opened wide to allow the wheat to pass untouched when Pre-Breaking was not wanted.

The mill was allowed to "warm-up" on the sample being milled for a period of thirty minutes, during which time all rolls were set for proper grind. At the end of thirty minutes the wheat feeder was shut off and immediately following, the entire mill was shut down under load. All material pans were emptied and replaced. The mill was then restarted and wheat was again started to the mill. Break rolls and reduction rolls were again quickly checked for proper adjustment. At the end of forty-five minutes, the wheat feeder was shut off with the mill shut down immediately following. At this time all materials produced were carefully weighed and the flour streams were sampled for ash and moisture analysis.

The mill was again restarted and wheat fed to it. At this time, the Pre-Break rolls were either set for pre-breaking or opened fully, depending on the previous test. The above procedures of mill operation again followed. A total of five no Pre-Break/Pre-Break test series were run.

## RESULTS AND DISCUSSION

Flour stream weights and their corresponding ash contents, on a 14% moisture basis, for the five millings of each of the experimental mill flows were averaged and from this, cumulative flour ash was calculated. Tables showing flour weights, their percentages of the total products and their ash contents as well as the cumulative ash calculations are given for each mill flow. Cumulative flour ash curves depicting the results are also given for each experimental mill. The summation of percentages of total product (S of Q) is given by the x-axis and the summation of the product of each stream ash times its percentage of total product dividend by the summation of percentages of total product ( $S \text{ of } Q \times A/S \text{ of } Q$ ) is given by the y-axis.

Complete stream weights, feed rates, and other miscellaneous information for each milling is listed in the appendix. Cumulative ash calculations and cumulative ash curves are also given in the appendix for each individual milling test.

(1) Brabender Quadrumat Junior.

Table 2 shows the averaged stream weights and ash contents of flours produced by the five millings as well as the cumulative ash calculations for the Quadrumat Junior. Figure 7 shows the results of the calculations graphically. The two flour streams sampled and shown are the throughs of a 70GG sieve and overs of a 9XX sieve (labeled +9XX) and the throughs of a 9XX (labeled -9XX).

As can be seen by both the calculations and cumulative ash curves, the use of Pre-Breaking prior to milling of the Quadrumat Junior provides a definite improvement in milling performance. In addition to substantially lowering the flour ash, flour yield was also improved by about .5%.



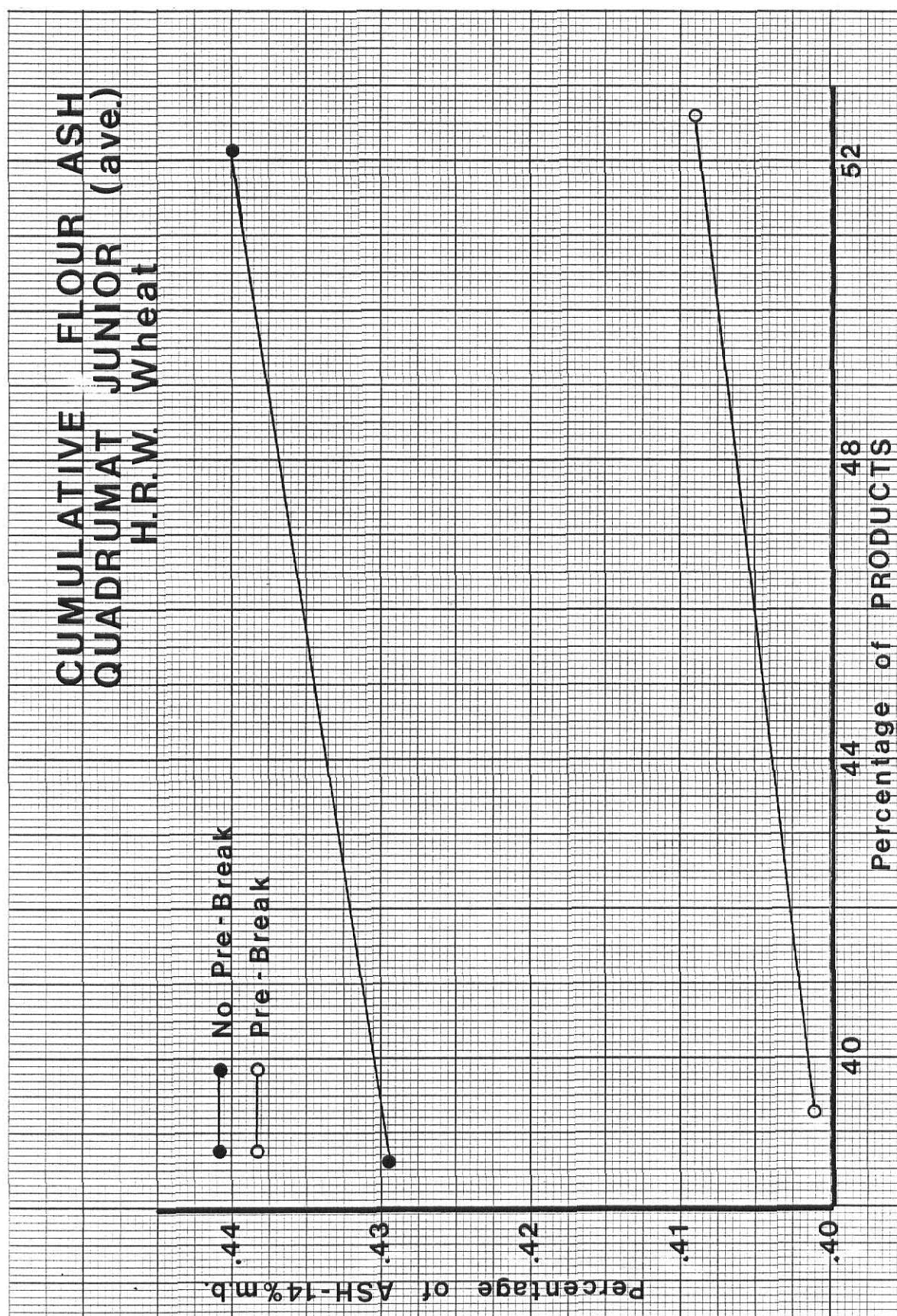


Figure 7

## (2) Brabender Quadrumat Senior.

Table 3 lists the cumulative ash calculations for the average of the five millings on the Quadrumat Senior. The results are shown graphically in Figure 8. Two flours were produced and analyzed. Break flour (Brk. Fl.) was the throughs of two 9XX sieves produced by the break head and Reduction Flour (Red. Fl.) was the throughs of two 7XX sieves produced by the reduction head.

As in the Quadrumat Junior tests, a definite improvement is also seen by the use of Pre-Break on the resultant flour quality produced by the Quadrumat Senior. Flour ash content was lowered significantly and flour yield was also improved, again by .5%.

Most of this improvement came with more break flour being produced at a lower ash content. Since the rolls in the Quadrumat Senior are positioned at a fixed gap, the results would indicate that the Pre-Breaking of wheat provides less severity of grind by the break rolls. More low ash break flour is produced as well as cleaner middlings (overs of the flour cloths) being sent to the reduction head, as evidenced by the lower ash of the reduction flour.

## (3) Buhler Experimental Mill.

Flour stream weights for the average of the millings on the Buhler Experimental Mill and the cumulative ash calculations are given by Table 4. The resulting cumulative flour ash curves are given by Figure 9.

Flour streams analyzed were as follows:

Pre-Break	(P.BK)
First Break	(1 BK)
Second Break	(2 BK)
Third Break	(3 BK)
First Reduction	(1 RED)
Second Reduction	(2 RED)
Third Reduction	(3 RED)







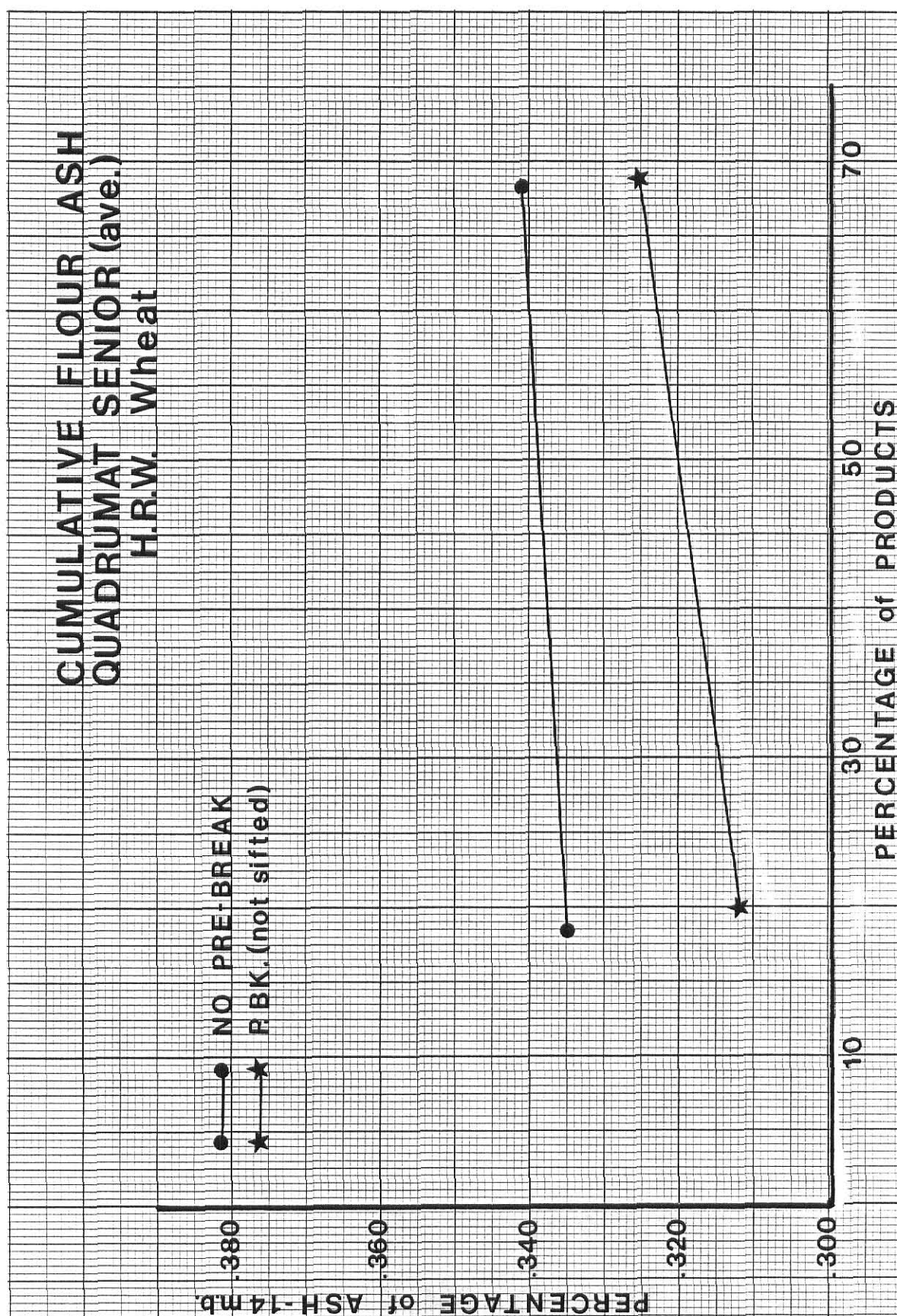


Figure 8

MILL	BUHLER EXP. MILL
TEST	AVERAGE
WHEAT	HARD RED WINTER

[illegible]

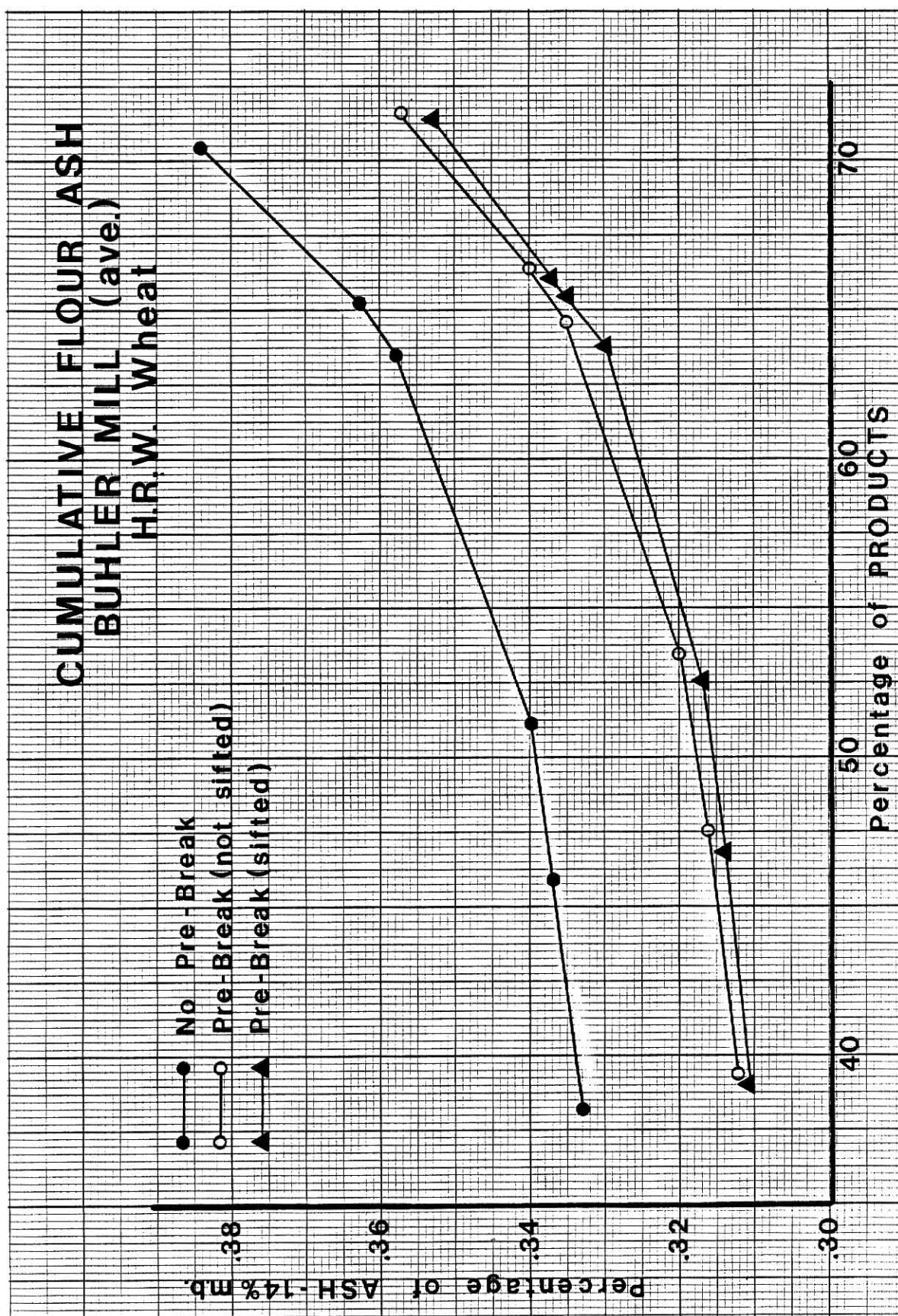


Figure 9

As mentioned in the methods, Pre-Broken wheat was both fed directly to first break on the Buhler Mill and sifted over a 9XX sieve to remove the Pre-Break flour produced before feeding to first break. As shown by the results, both methods of Pre-Breaking gave much improved milling results over not Pre-Breaking. A slight improvement is also shown by having sifted the Pre-Broken wheat prior to first break over Pre-Breaking without sifting.

All flour streams from the Pre-Break tests show improvement in ash contents and more than 1% average increase in flour extraction.

#### (4) Ross Walking Flow.

Table 5 gives the flour stream data and cumulative ash calculations for the average of the Ross flow millings. Figure 10 shows the cumulative flour ash curves of the plotted data. Flour streams analyzed were as follows:

Pre-Break	(P.BK)	Sizings	(SIZ)
First Break	(1 BK)	First Midds	(1 M)
Second Break	(2 BK)	Second Midds	(2 M)
Third Break	(3 BK)	Third Midds	(3 M)
Fourth Break	(4 BK)	First Tailing	(1 TA)
Fifth Break	(5 BK)	Fourth Midds	(4 M)
		Fifth Midds	(5 M)

Here again, other than feeding Pre-Broken stock directly to First Break, sifting was also performed on the stock before First Break grind. In this instance, as indicated by the flow sheet (Figure 5), the Pre-Break sifter was more elaborate. Other than removing the flour produced by Pre-Breaking, the sizings and middlings produced were also removed and sent to sizings and middlings grinds.

The cumulative ash curves again show a distinct improvement in milling performance by the use of the Pre-Breaking of the grain before actual



## Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)  
 Q=QUANTITY (% of Total Products)  
 S= SUMMATION

MILL ROSS WALKING FLOW  
 TEST AVERAGE  
 WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	Q X A	S of QXA	S of QXA S of Q
NO PRE-BREAK							
1 M	1171	40.05	40.05	.275	11.014	11.014	.275
SIZ	197	6.75	46.80	.311	2.099	13.113	.280
2 M	244	8.34	55.14	.317	2.644	15.575	.286
3 BK	72	2.47	57.61	.383	0.946	16.703	.290
2 BK	85	2.89	60.50	.406	1.173	17.876	.295
3 M	92	3.16	63.66	.409	1.292	19.169	.301
4 BK	34	1.18	64.84	.445	0.525	19.694	.304
1 BK	109	3.72	68.56	.494	1.838	21.531	.314
1 TA	14	0.49	69.05	.578	0.283	21.815	.316
5 BK	39	1.35	70.40	.617	0.833	22.648	.322
4 M	55	1.89	72.29	.633	1.196	23.844	.330
5 M	21	0.73	73.02	1.243	0.907	24.751	.339
PRE-BREAK (NOT SIFTED)							
1 M	1150	39.51	39.51	.269	10.628	10.628	.269
SIZ	194	6.66	46.17	.295	1.965	12.593	.273
2 M	266	9.12	55.29	.295	2.690	15.283	.276
3 BK	79	2.70	57.99	.364	0.983	16.266	.280
2 BK	93	3.18	61.17	.381	1.212	17.478	.286
3 M	83	2.85	64.02	.392	1.117	18.595	.290
1 BK	127	4.35	68.37	.418	1.818	20.413	.299
4 BK	39	1.33	69.70	.427	0.568	20.981	.301
1 TA	12	0.43	70.13	.571	0.246	21.227	.303
4 M	44	1.50	71.63	.607	0.911	22.137	.309
5 BI	36	1.22	72.85	.615	0.750	22.887	.314
5 M	16	0.56	73.41	1.139	0.638	23.525	.320
PRE-BREAK (SIFTED)							
1 M	1194	40.88	40.88	.266	10.874	10.874	.266
SIZ	203	6.97	47.85	.291	2.028	12.902	.270
2 M	221	7.58	55.43	.297	2.251	15.154	.273
3 BK	80	2.74	58.17	.357	0.978	16.132	.277
2 BK	91	3.13	61.30	.374	1.171	17.302	.282
3 M	80	2.73	64.03	.389	1.062	18.364	.287
1 BK	115	3.94	67.97	.410	1.615	19.980	.294
4 BK	37	1.26	69.23	.431	0.543	20.523	.296
1 TA	11	0.38	69.61	.533	0.203	20.725	.298
5 BK	40	1.36	70.97	.601	0.817	21.543	.304
P.BK	5	0.18	71.15	.607	0.109	21.652	.304
4 M	47	1.60	72.75	.646	1.034	22.686	.312
5 M	16	0.55	73.30	1.319	0.725	23.411	.319

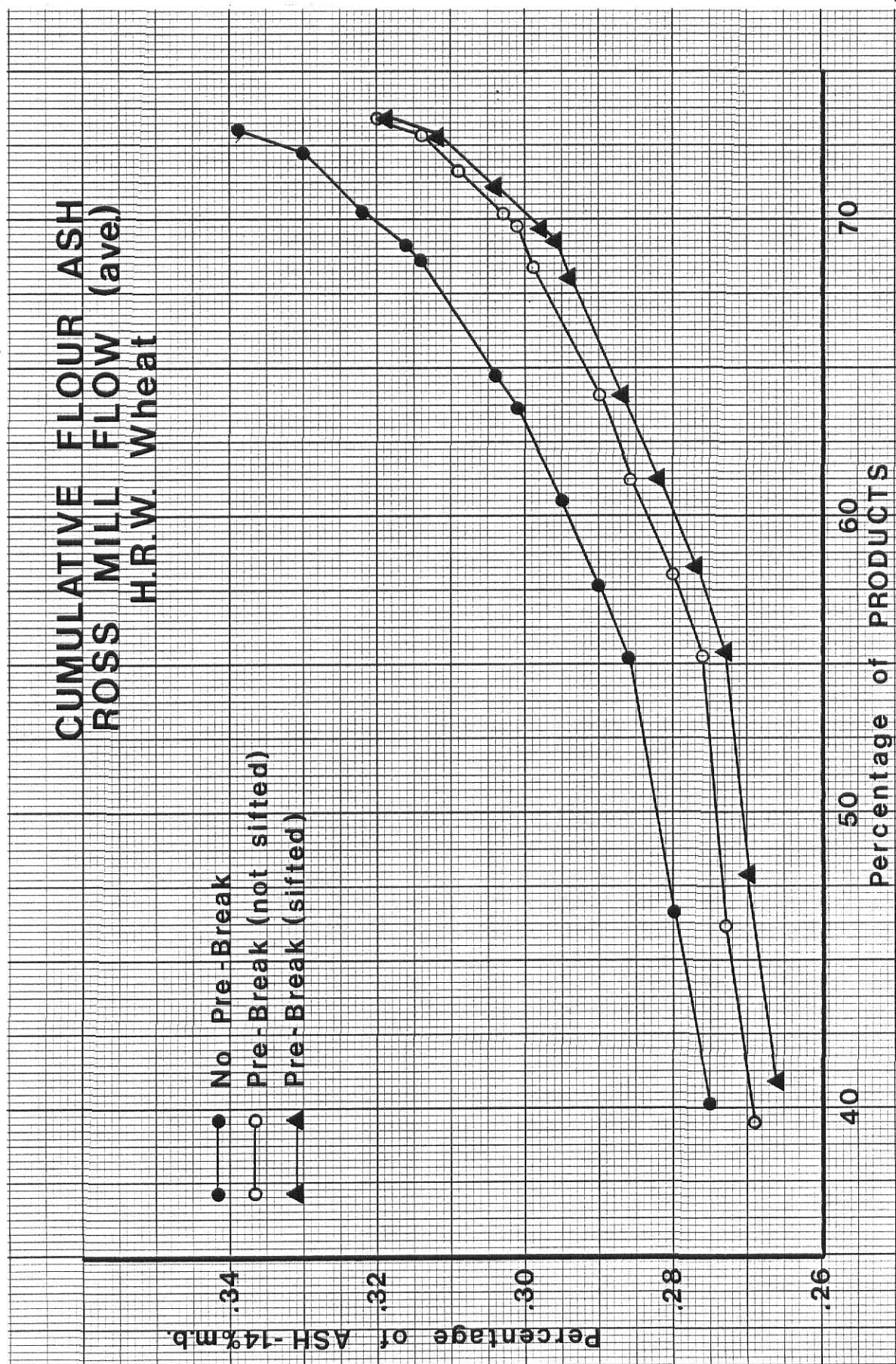


Figure 10

milling. The use of the Pre-Break sifter is also favored due to the slightly lower ash curve produced.

Both tests using the Pre-Break also gave slightly higher average flour extractions. Improvements of .3% to .4% were realized.

(5) Miag Multomat Mill.

Flour stream data and cumulative ash calculations are listed in Table 6 and the resulting cumulative ash curves are shown by Figure 11 for the averaged results of the millings on the Miag Multomat. Flour streams analyzed were as follows:

First Break	(1 BK)	Second Midds	(2 M)
Second Break	(2 BK)	First Midds Redust	(1 M RED)
Third Break	(3 BK)	Third Midds	(3 M)
Grader		Fourth Midds	(4 M)
First Midds	(1 M)	Fifth Midds	(5 M)

Although some improvement with the use of the Pre-Break is noticed, it does not appear as significant as in previous tests. Since this mill can be considered as relatively short on break roll surface, it would seem that the use of Pre-Break would be of great assistance in improving the flour milling performance. As indicated by the data, improvement was only slight and specific reasons for this are not known.

The actual Pre-Breaking operation, as discussed earlier, was performed on a slightly different roller mill than on the other test millings. This being a pair of 6" x 3" rolls running at a 1.5:1 differential versus 9" x 6" rolls running at a 1:1 differential. Although there is a slight difference between methods, it would not seem to be critical enough to significantly affect the results.

Feed rates for experimental mills is a critical factor in the correct operation and performance of the mills. In previous testing using the Miag Multomat, feed rates of 750 to 780 grams per minute were normally





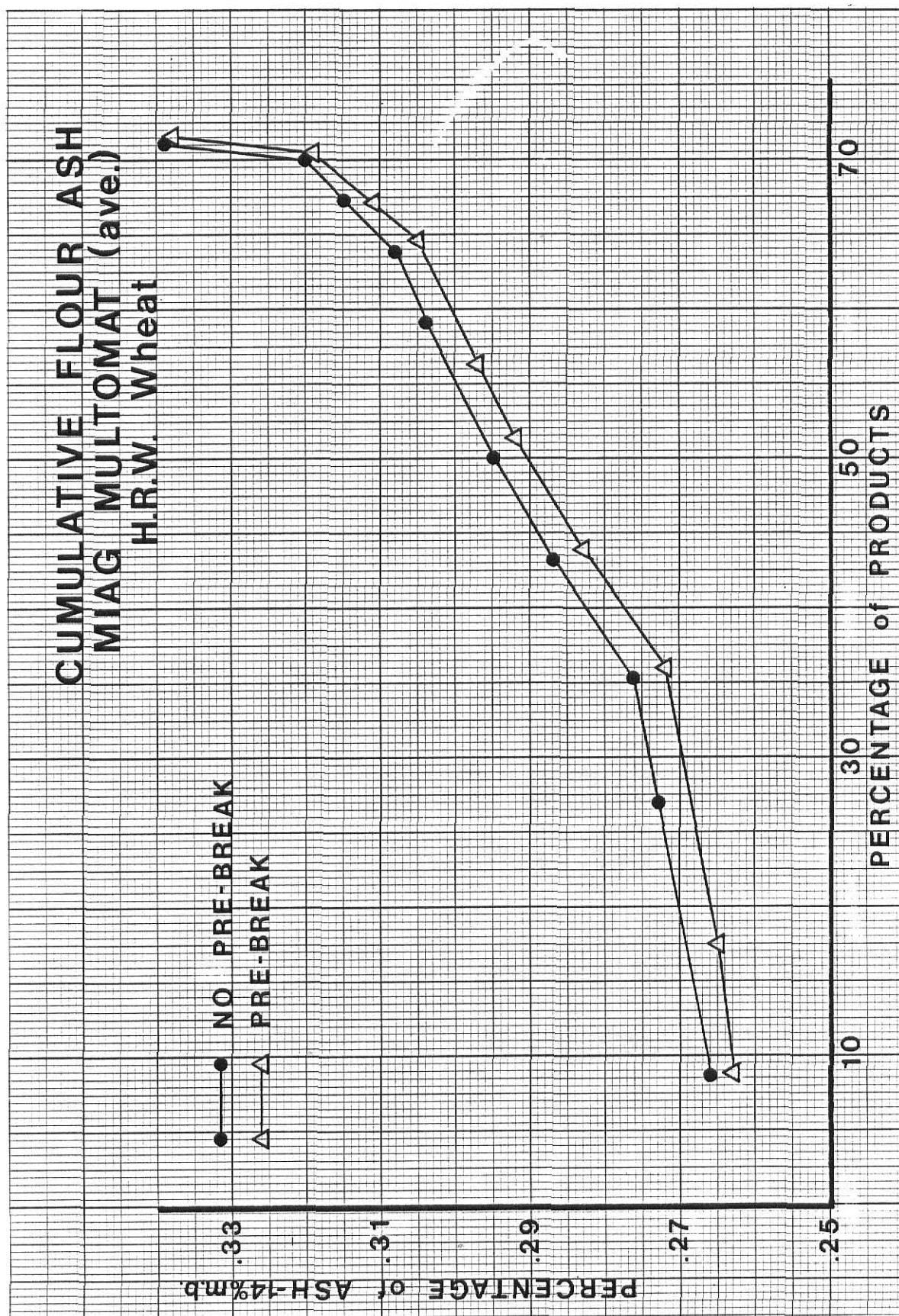


Figure 11

used and found to give adequate results and comfortable operating conditions. Since this particular mill flow has a relatively short Break System and a relatively long Reduction System, at the feed rates the mill is normally operated at, the tail of the mill was somewhat underloaded. By using the Pre-Break, this underloaded condition may have worsened, thereby causing bare-bolting in the sifting operation and in turn causing higher ash-flour streams.

If the data in Table 6 is further analyzed, it can be shown that this underloaded condition was further aggravated by the use of Pre-Break. By accumulating only the Break flours (1st Break, 2nd Break, Grader and 3rd Break), 21.96% flour at .359% ash was produced by the test milling not using Pre-Break versus 22.65% flour at .355% ash milling with the Pre-Break. A gain of about .7% is realized with the Pre-Break at approximately the same ash. Again, by only accumulating the Primary Middlings flours (1st Midds, 2nd Midds, 1st Midd. Redust) it is seen that 35.36% flour at .276% ash is produced by the "No Pre-Break" System versus 36.05% flour at .272% ash produced with Pre-Break. This results in a .7% gain in flour, using Pre-Break at essentially the same cumulated ash content. The remainder, secondary middlings flour, when accumulated gives a resultant flour of 13.74% at .468% ash for the system without Pre-Break versus 12.71% at .496% ash produced by the system using Pre-Break. Approximately 1% more flour was produced by the mill without the Pre-Break and at a lower ash.

From this analysis, it is therefore possible that the optimum feed rate was not utilized in these tests for proper analysis of the Pre-Break. Since more break flour and primary middling flour was produced with the use of the Pre-Break, the tail end of the mill, or Secondary Middlings, was below proper loading for optimum milling performance.

## SUMMARY AND CONCLUSIONS

As previously stated, the purpose of this research was to document the effect of Pre-Breaking kernels of wheat prior to the actual procedure of milling. From the data obtained by test milling, using various experimental mills, it can be concluded that Pre-Breaking results in a positive effect upon milling and flour quality.

The flour miller is continually faced with many goals and problems in trying to achieve these goals. One of the primary goals or objectives that is basic to the milling of wheat is to obtain the highest percentage of flour at the highest quality obtainable from a given lot of wheat. Solutions to meet both of these goals may be difficult.

The results of these tests on Pre-Breaking show that, if properly applied, Pre-Break Systems may aid in providing both flours at lower ash contents and at somewhat higher extractions. In all cases, with the exception of the tests using the Miag Multomat, flour ash contents were significantly lowered while slight increases in total flour extractions were also realized, when the wheat was Pre-Broken prior to milling. Tests on the Miag Multomat using Pre-Break also produced flour of lower ash contents than when not using Pre-Break, but differences were not as great. This, as mentioned before, may have been due to problems of the feed rate of wheat to the mill.

The results also indicated that sifting of the Pre-Broken wheat before milling was also beneficial. Flours obtained from test millings where the Pre-Broken stock was sifted before milling were found to be slightly lower in ash than when Pre-Break was used without sifting.

Although not based on scientific fact, several reasons may be theorized as to why Pre-Breaking produces positive effects on milling performance.

1. As can be seen in that data, milling with a Pre-Break produced higher percentages of primary break flours at lower ash contents. This could be due to the better presentation of the wheat to the corrugated break rolls in particular the first and second break rolls. Normally, the First Breaking operation must both open up the wheat berry and scrape some portions of the endosperm from the bran. The design of the corrugations and differentials of the rolls lend themselves to doing a better job of the latter. Therefore if, as when using the Pre-Break, the kernel is partially opened and somewhat flattened out before the First Break, the First Break rolls may provide better grinding action with less severity of grind, resulting in less bran contamination. Besides producing lower ash flour on the Breaks, Sizings and Middlings stock lower in ash is also being produced.

2. Although not as yet researched, one may theorize that the wheat berries being exposed to the shock of compression by the Pre-Break rolls may develop stresses along the area where the endosperm adheres to the bran. This would allow for the easier removal of the endosperm by the subsequent Break rolls.

3. The grinding of the wheat germ, since it is relatively high in ash content, can increase the ash content of the flour being produced. It was observed that, when milling with the Pre-Break, more wheat germ was being released into the Sizings fraction. Once in the Sizings System, there is better chance for recovery and less chance for the grinding of the germ into flour.

4. Where the Pre-Broken wheat was sifted before milling, slightly lower flour ashes were also noted than when it was not sifted. This may be due to the removal, by the sifter, of any foreign material lodged in the crease of the wheat berry that was not removed in the cleaning process.

## SUGGESTIONS FOR FUTURE WORK

Since this work dealt mainly with documenting the effects of Pre-Breaking, the theories as to why the use of a Pre-Break result in improved milling performance need to be substantiated. Work along these lines should be, if possible, scaled up to a larger, commercial-type mill. Complete stream analysis on a large scale mill could be very revealing. To determine if pre-breaking may loosen the bonds between the bran and the endosperm, studies using the Scanning Electron Microscope may be useful.

More work should also be done to better determine the method of Pre-Breaking which provides the optimum improvement in milling performance. In this study, only smooth rolls at very low differentials were utilized. Would corrugated rolls or a combination of a corrugated and a smooth roll provide better splitting action? Is a one to one differential the optimum differential to use?

Determining the severity of Pre-Breaking to give optimum performance is also needed. If slightly opening the wheat berry at the crease presents the stock better to the Break rolls, would smashing the kernel under high compression make an even better presentation to the Break rolls?

Although not fully tested in this work, there is some evidence that by using a Pre-Break, power consumption may be lowered for the subsequent grinding operations. If it was determined that by the use of Pre-Break system both total power consumption was lowered and milling performance was improved, the milling industry would surely benefit.

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The writer would especially like to express his deep gratitude to his wife, family and friends for their support, encouragement and patience.

## APPENDIX A

## APPENDIX A

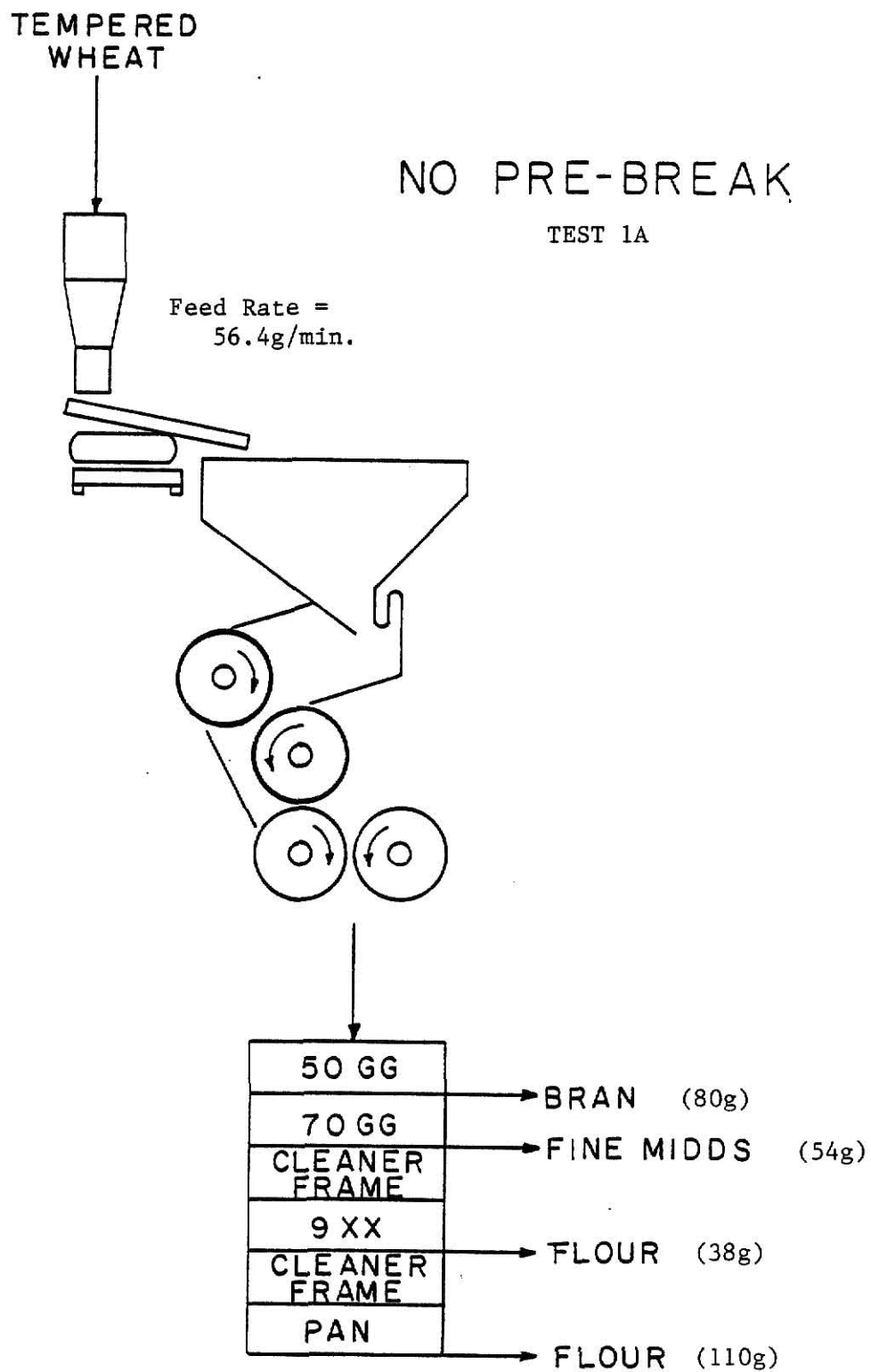
Appendix A contains all data from the individual tests on each experimental mill. Flowsheets of each mill are given with the stream weights entered for both flour and feed, and in the case of the Ross Walking Flow, all stream weights are given. Cumulative flour ash calculations and the resulting cumulative ash curves for each test are also shown.

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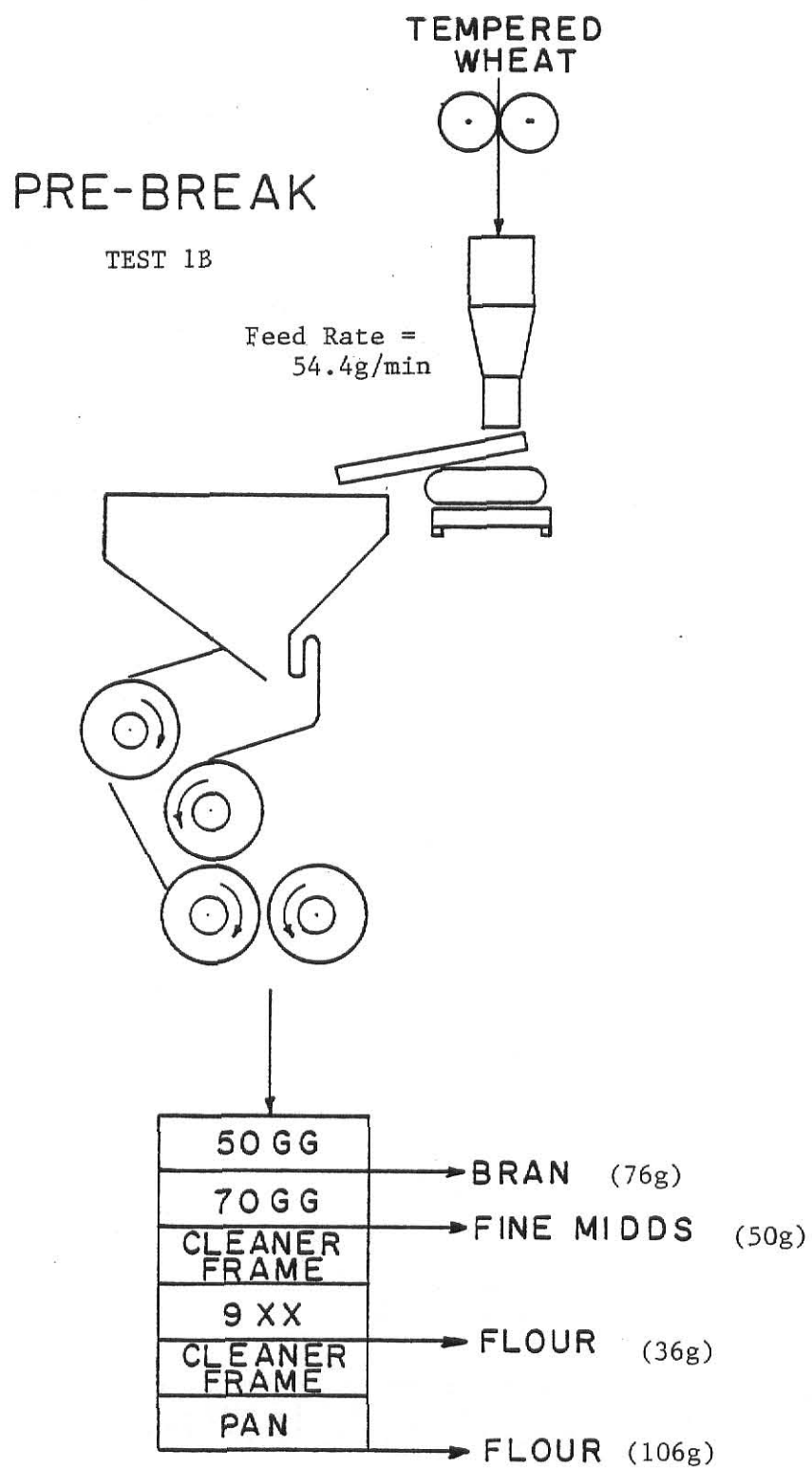
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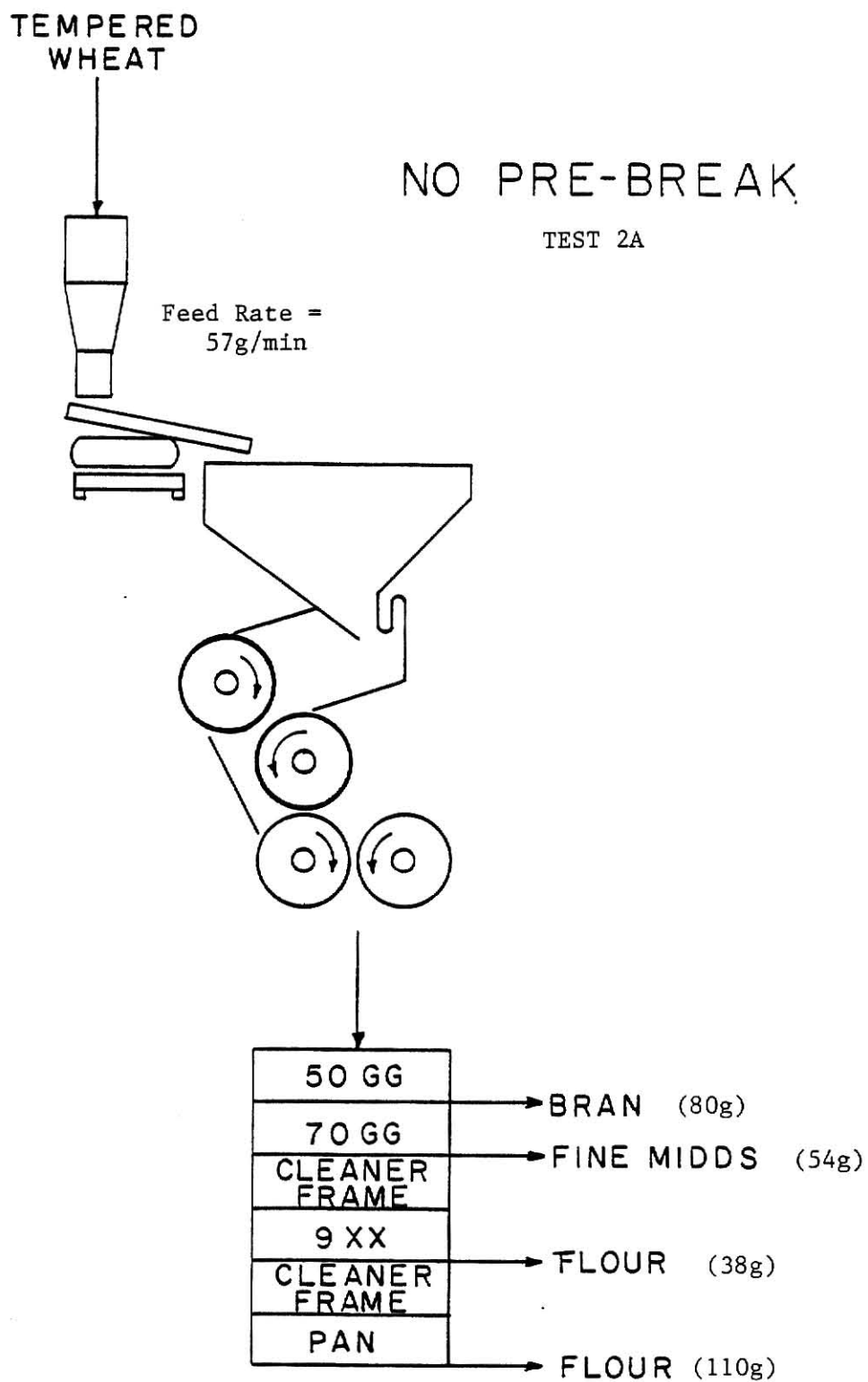
QUADRUMAT JUNIOR

Figure 12



QUADRUMAT JUNIOR

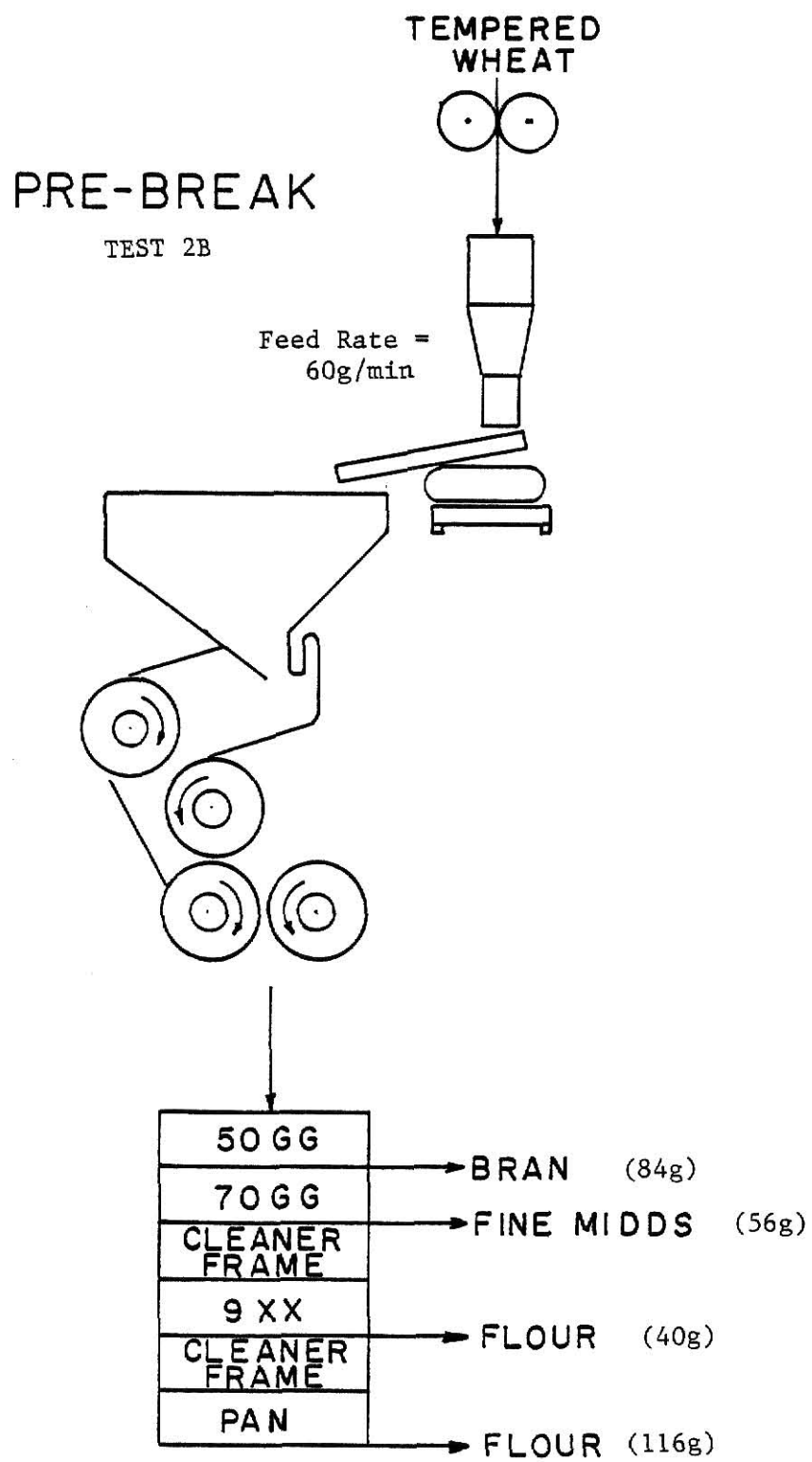
Figure 13



QUADRUMAT JUNIOR

Figure 14





QUADRUMAT JUNIOR

Figure 15

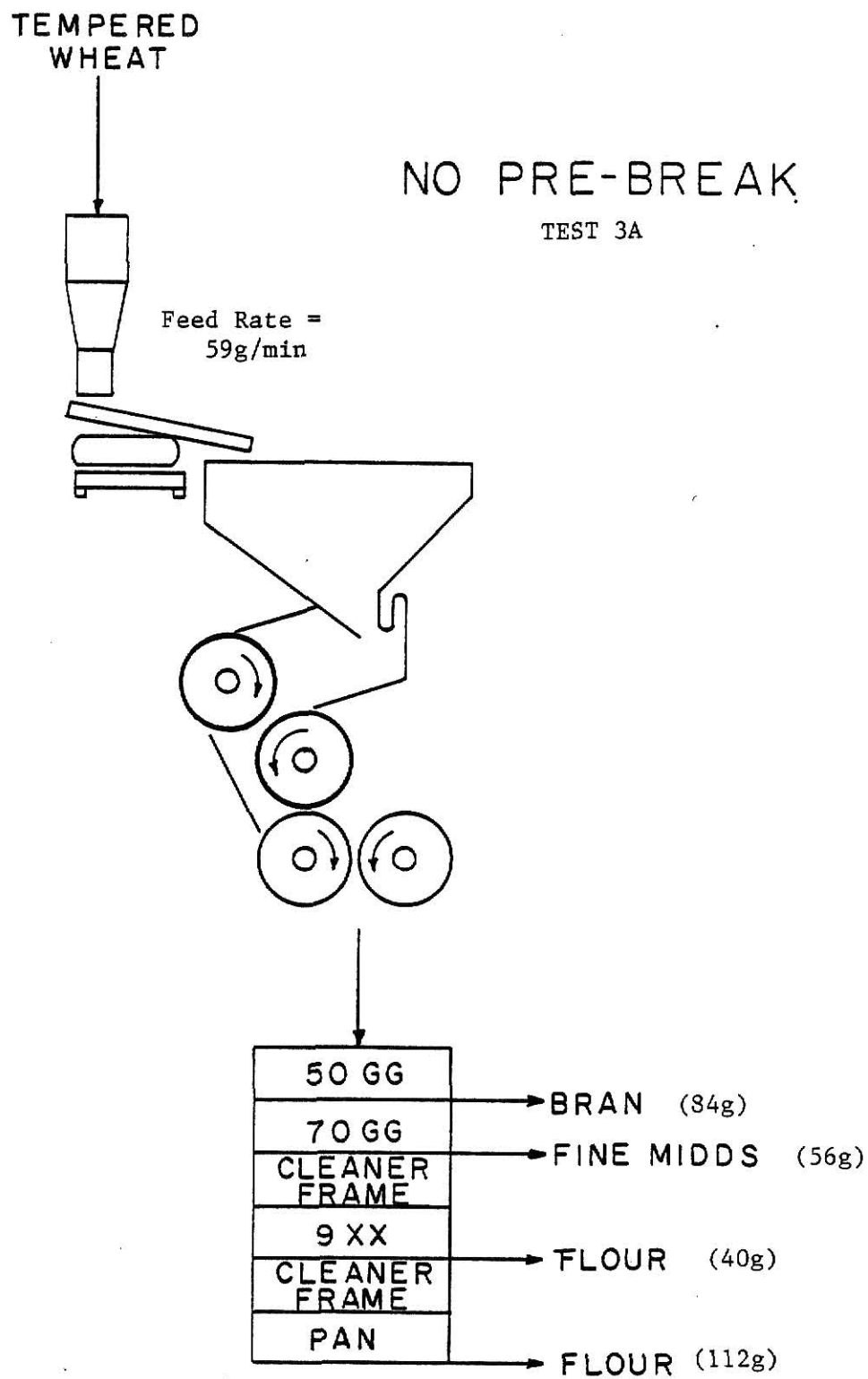
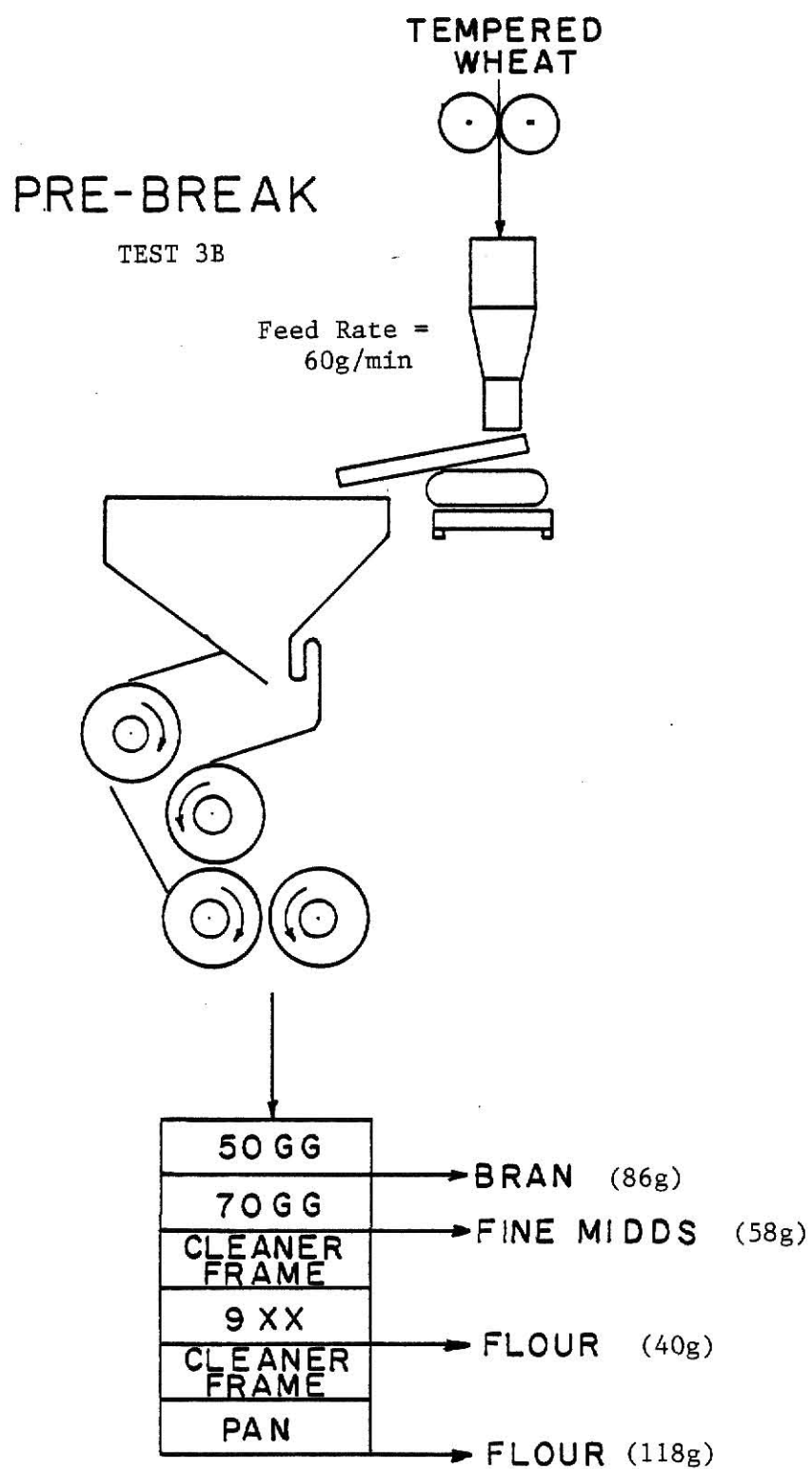
QUADRUMAT JUNIOR

Figure 16



QUADRUMAT JUNIOR

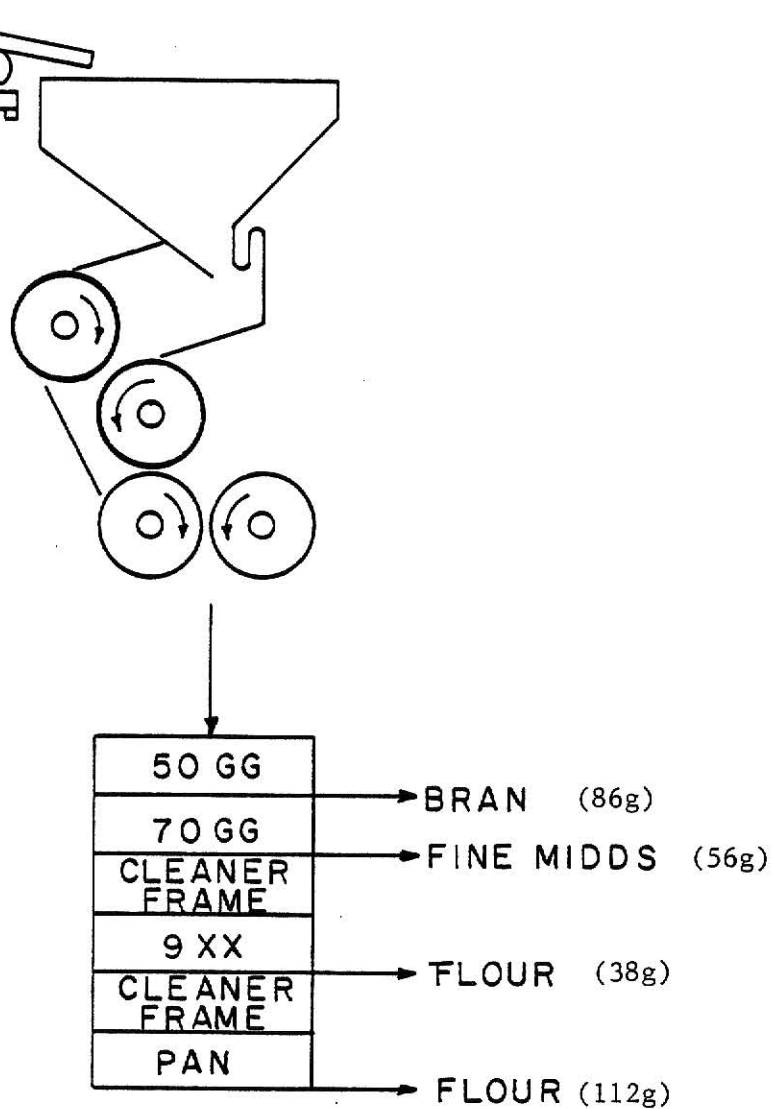
Figure 17

TEMPERED  
WHEAT

NO PRE-BREAK

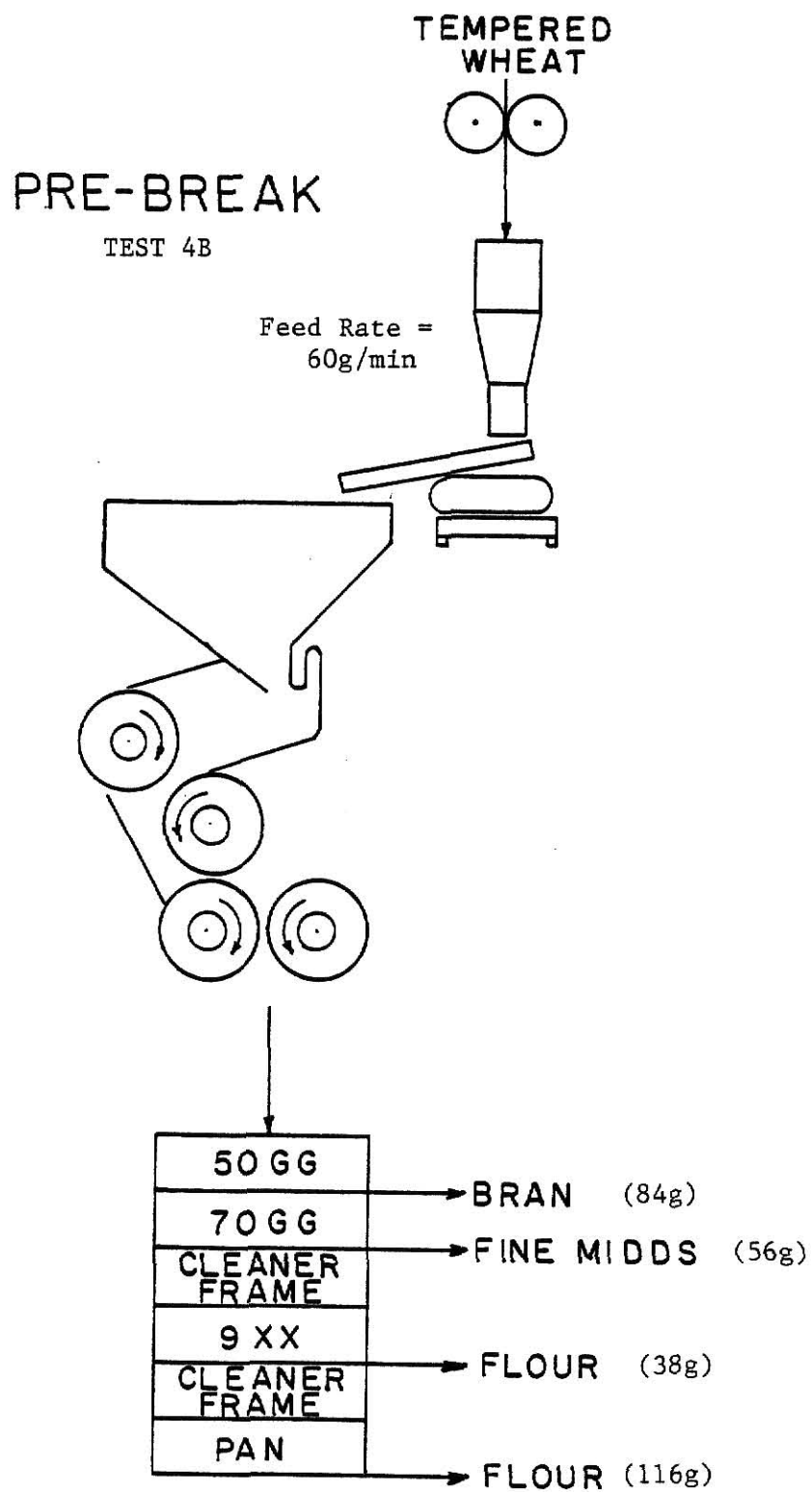
TEST 4A

Feed Rate =  
60g/min



QUADRUMAT JUNIOR

Figure 18



QUADRUMAT JUNIOR

Figure 19

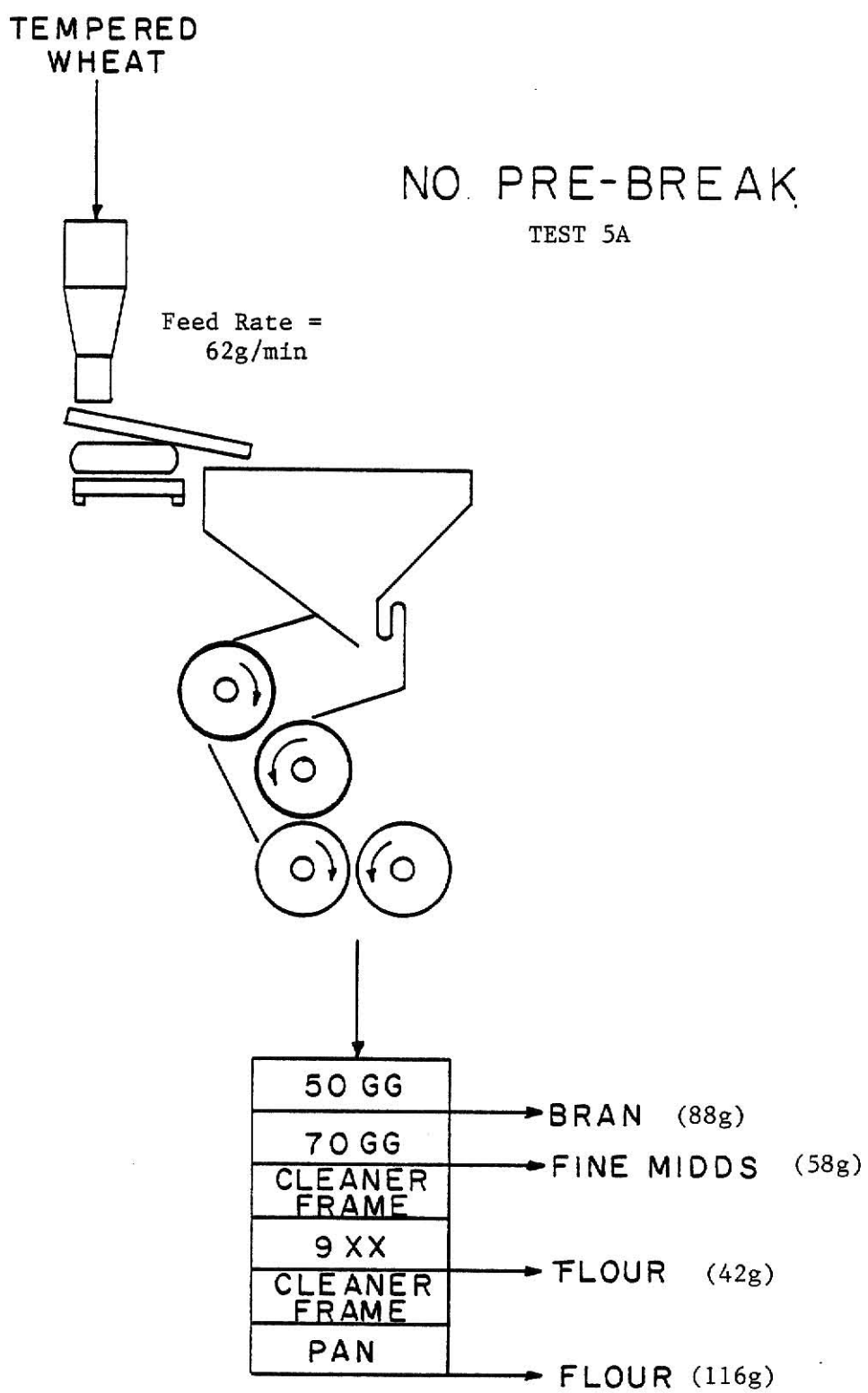
QUADRUMAT JUNIOR

Figure 20

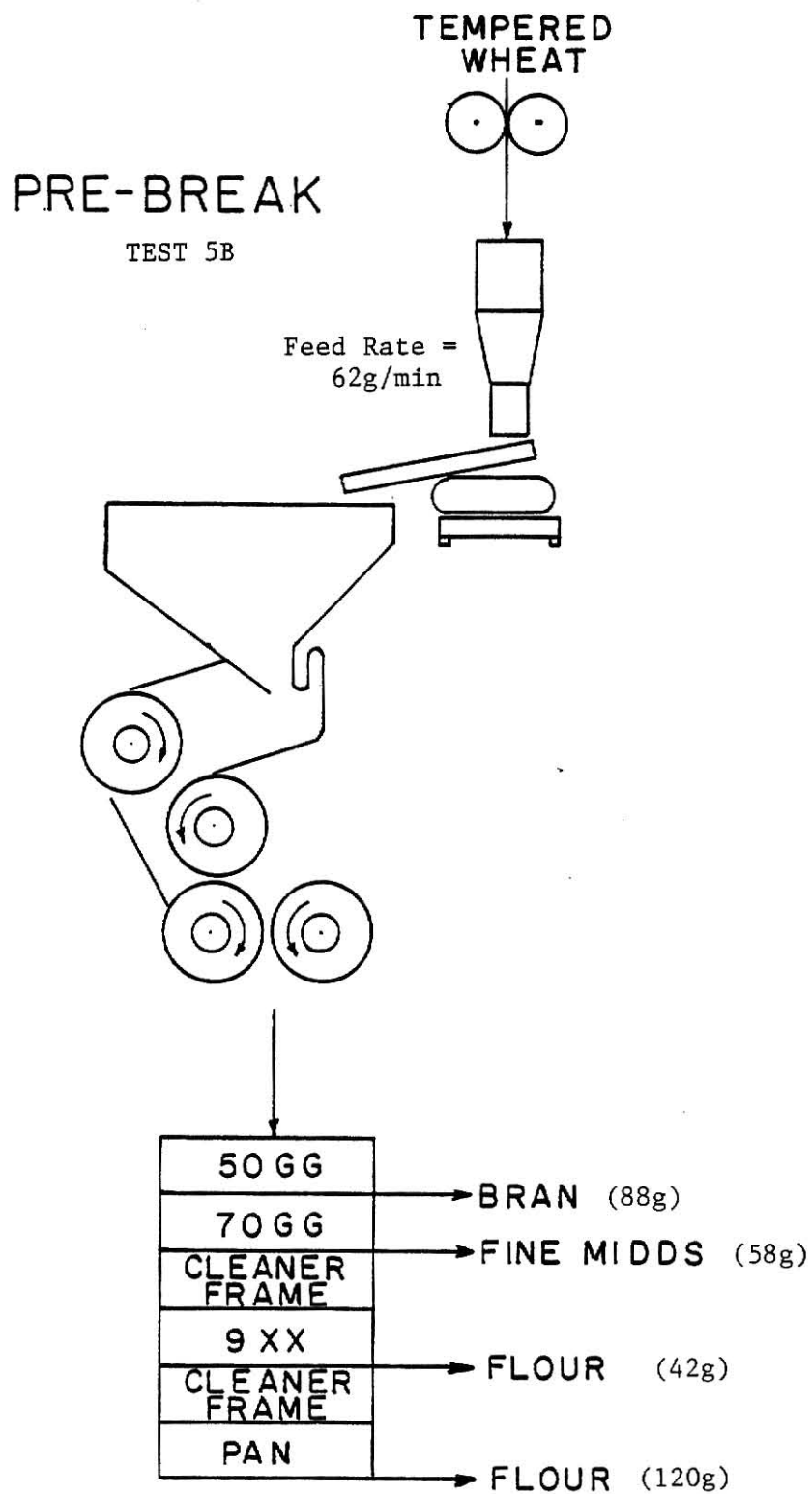
QUADRUMAT JUNIOR

Figure 21

## Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)  
 Q=QUANTITY (% of Total Products)  
 S= SUMMATION

MILL QUADRUMAT JUNIOR  
 TEST A, B, C, D, E  
 WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	Q X A	S of QXA	S of QXA S of Q
TEST 1A NO PRE-BREAK							
-9XX	110	39.01	39.01	.440	17.16	17.16	.440
+9XX	38	13.48	52.49	.460	6.20	23.36	.445
TEST 1B PRE-BREAK							
-9XX	106	39.55	39.55	.408	16.14	16.14	.408
+9XX	36	13.43	52.98	.427	5.73	21.87	.413
TEST 2A NO PRE-BREAK							
+9XX	38	13.48	13.48	.428	5.77	5.77	.428
-9XX	110	39.01	52.49	.431	16.81	22.58	.430
TEST 2B PRE-BREAK							
-9XX	116	39.19	39.19	.399	15.64	15.64	.399
+9XX	40	13.51	52.70	.416	5.62	21.26	.403
TEST 3A NO PRE-BREAK							
-9XX	112	38.36	38.36	.428	16.42	16.42	.428
+9XX	40	13.70	52.06	.437	5.99	22.41	.430
TEST 3B PRE-BREAK							
-9XX	118	39.07	39.07	.409	15.98	15.98	.409
+9XX	40	13.25	52.32	.410	5.43	21.41	.409
TEST 4A NO PRE-BREAK							
-9XX	112	38.36	38.36	.429	16.46	16.46	.429
+9XX	38	13.01	51.37	.439	5.71	22.17	.432
TEST 4B PRE-BREAK							
+9XX	38	12.93	12.93	.399	5.16	5.16	.399
-9XX	116	39.46	52.39	.407	16.06	21.22	.405
TEST 5A NO PRE-BREAK							
-9XX	116	38.16	38.16	.419	15.99	15.99	.419
+9XX	42	13.82	51.98	.436	6.03	22.02	.424
TEST 5B PRE-BREAK							
-9XX	120	38.96	38.96	.388	15.12	15.12	.388
+9XX	42	13.64	52.60	.388	5.29	20.41	.388



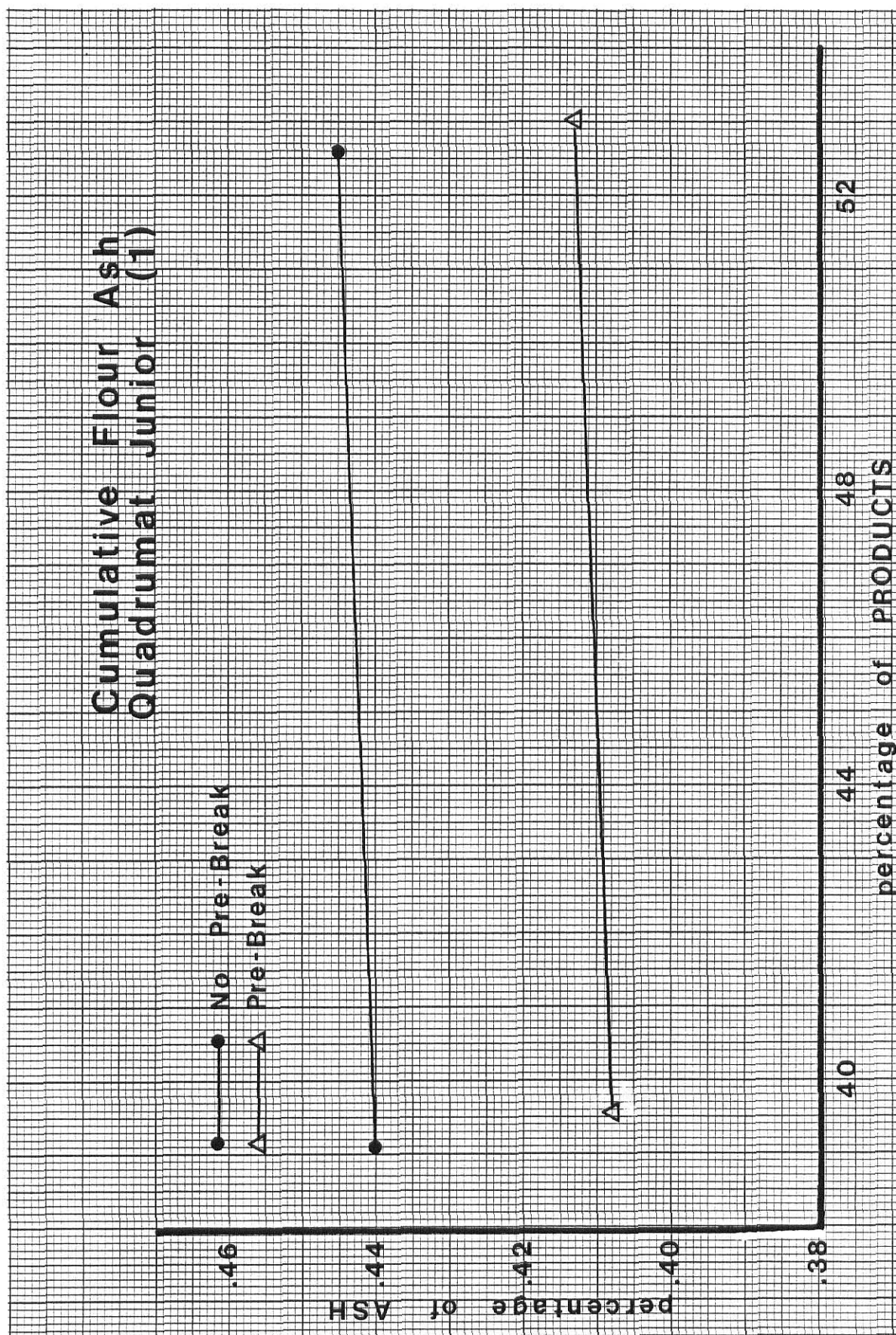


Figure 22

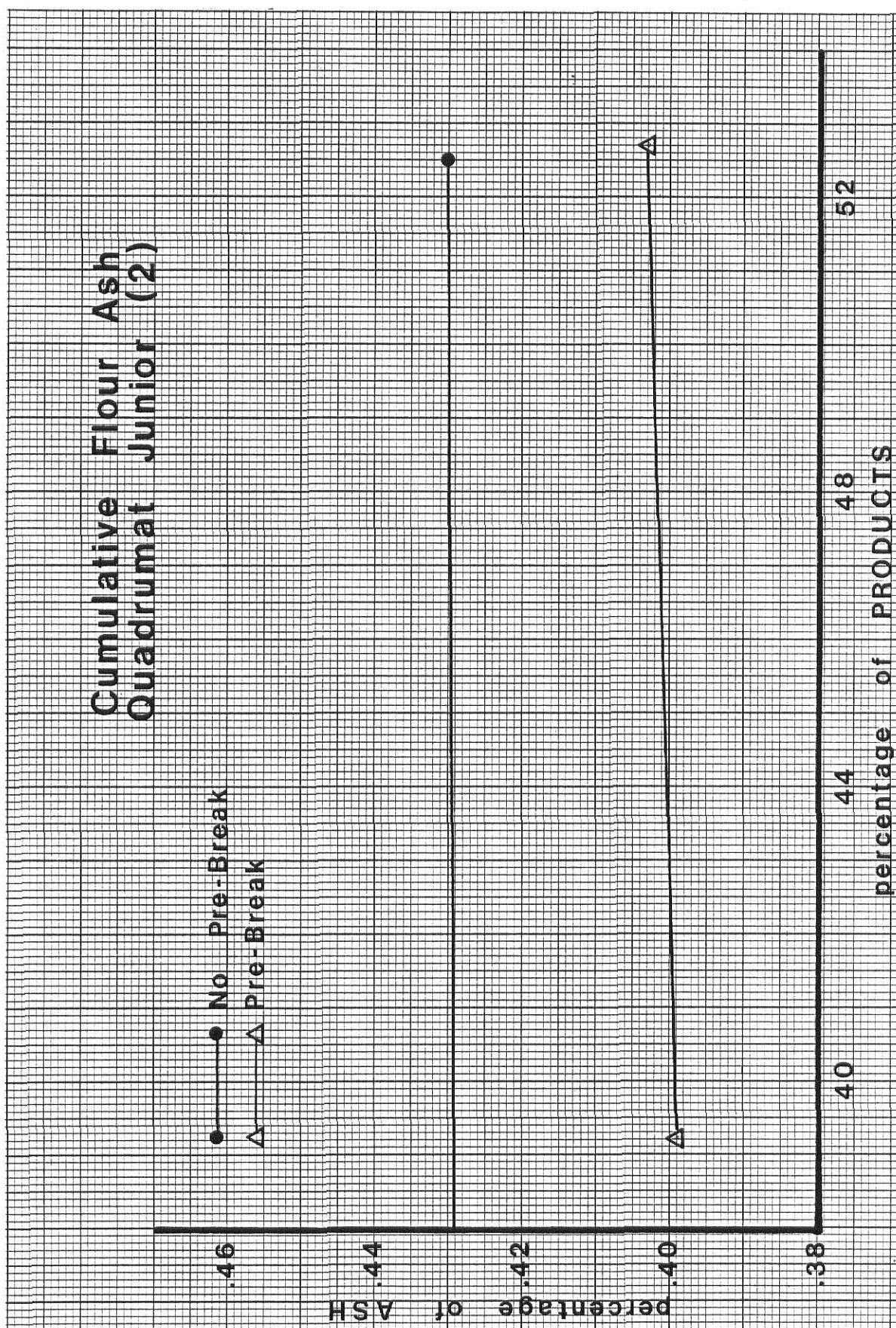


Figure 23



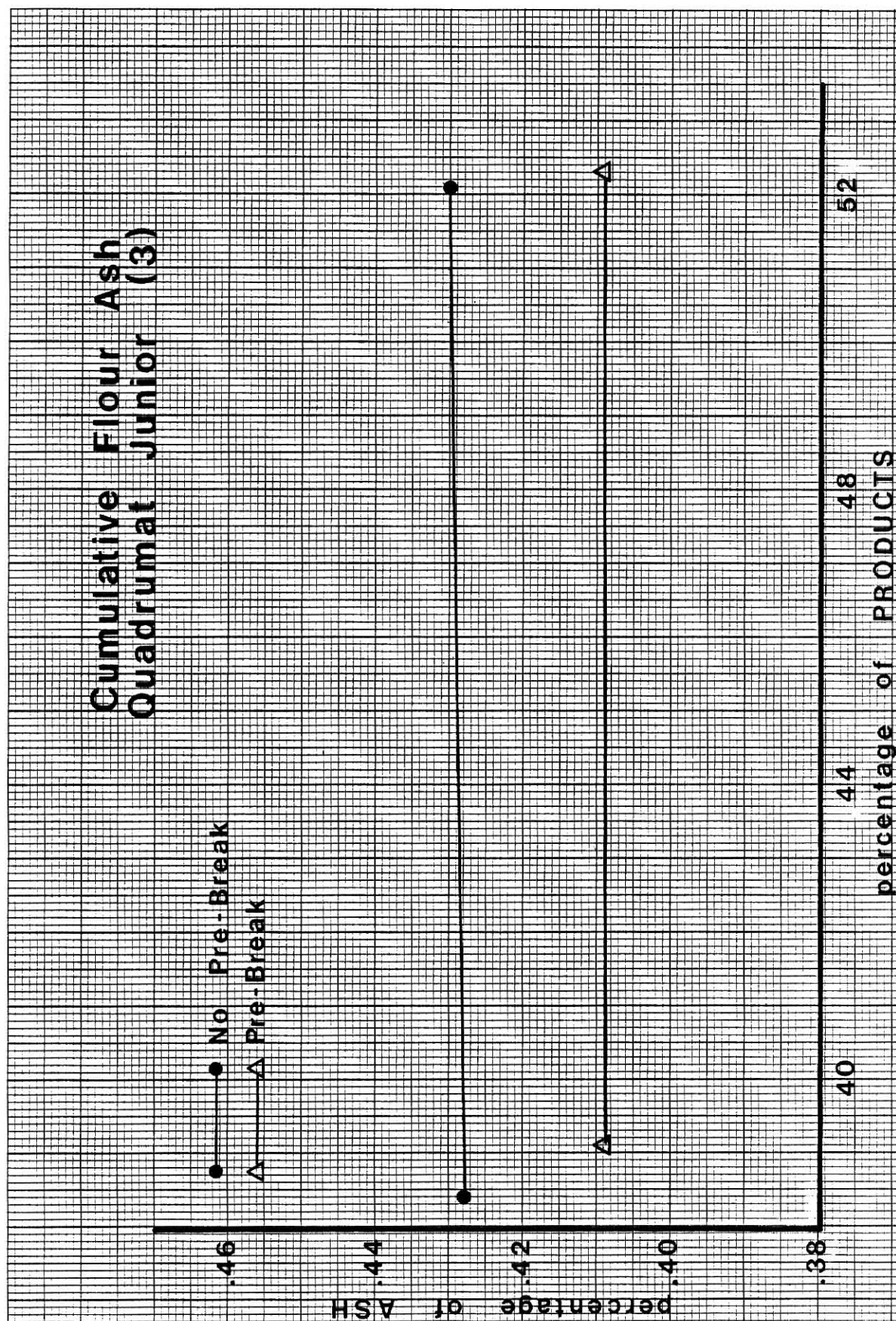


Figure 24

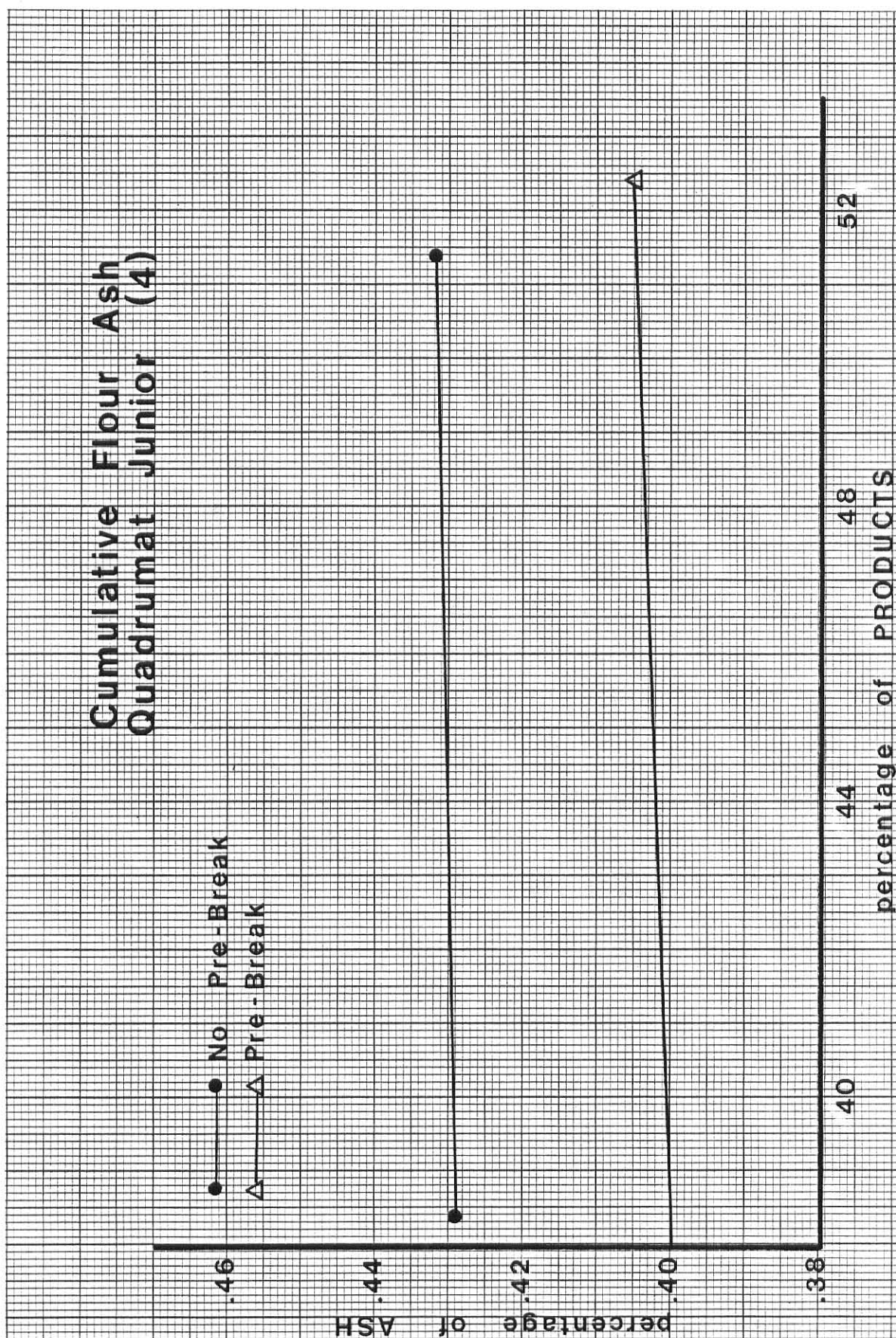


Figure 25



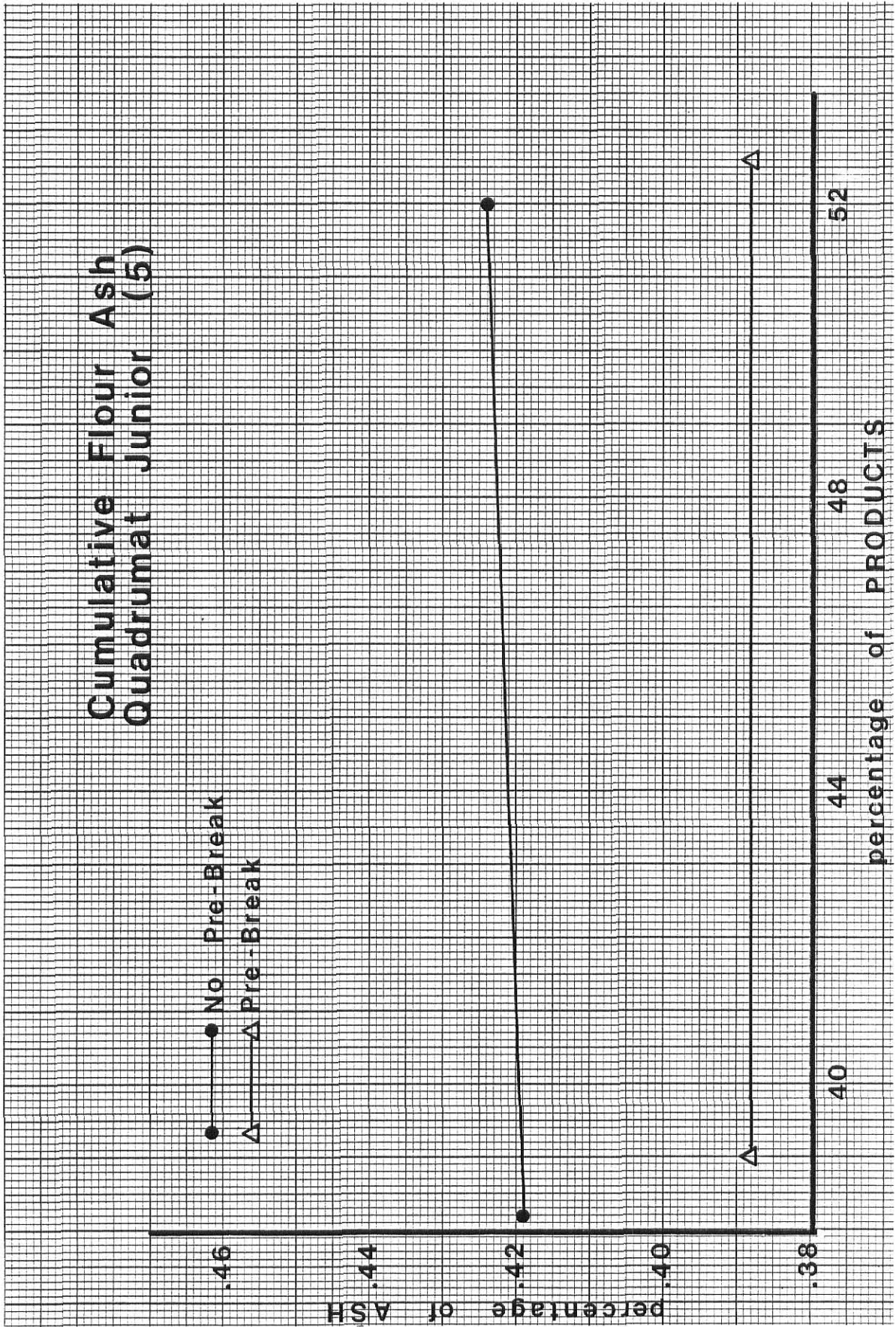


Figure 26

TEMPERED  
WHEAT

## NO PRE-BREAK

TEST 1A

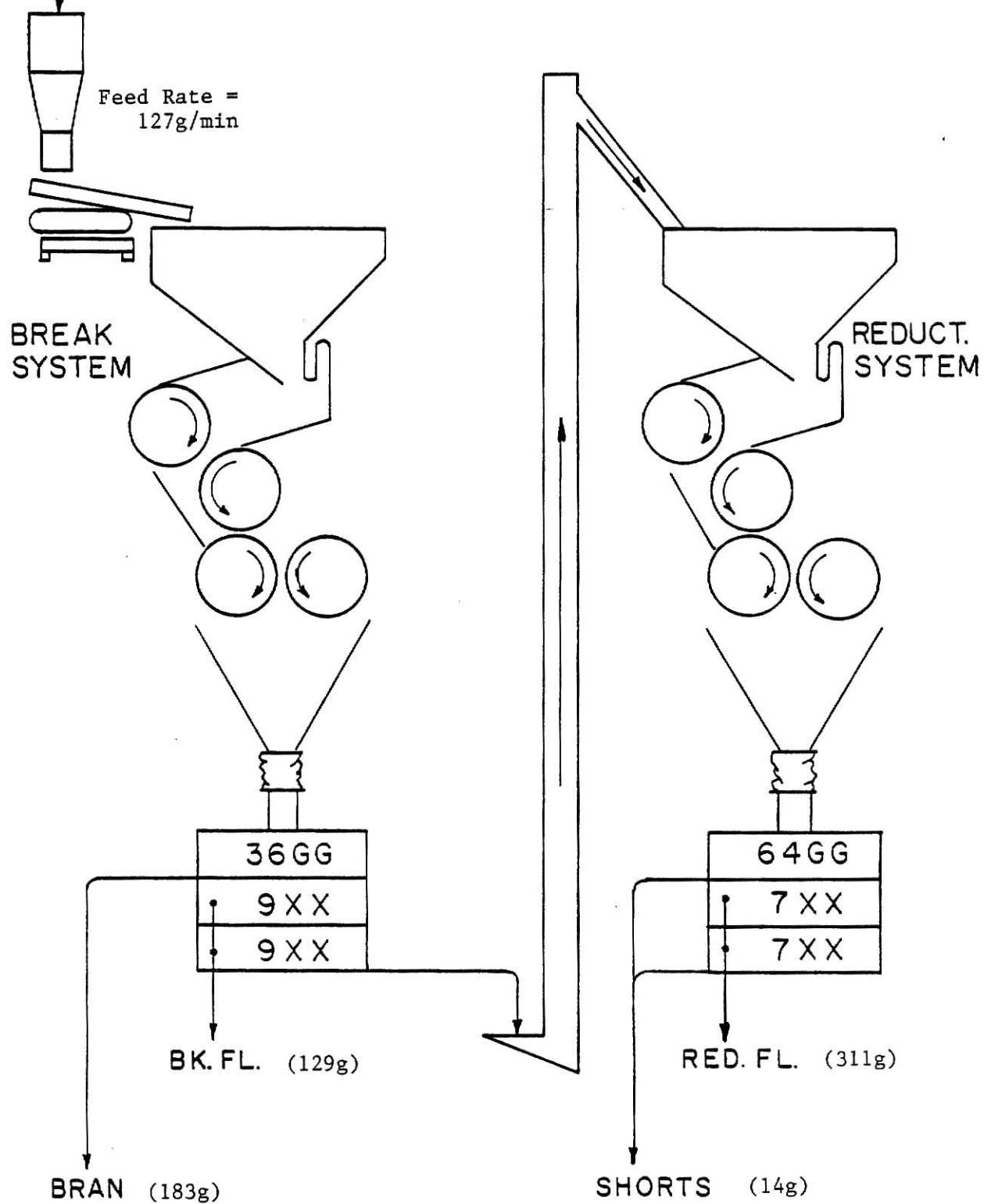
QUADRUMAT SENIOR

Figure 27

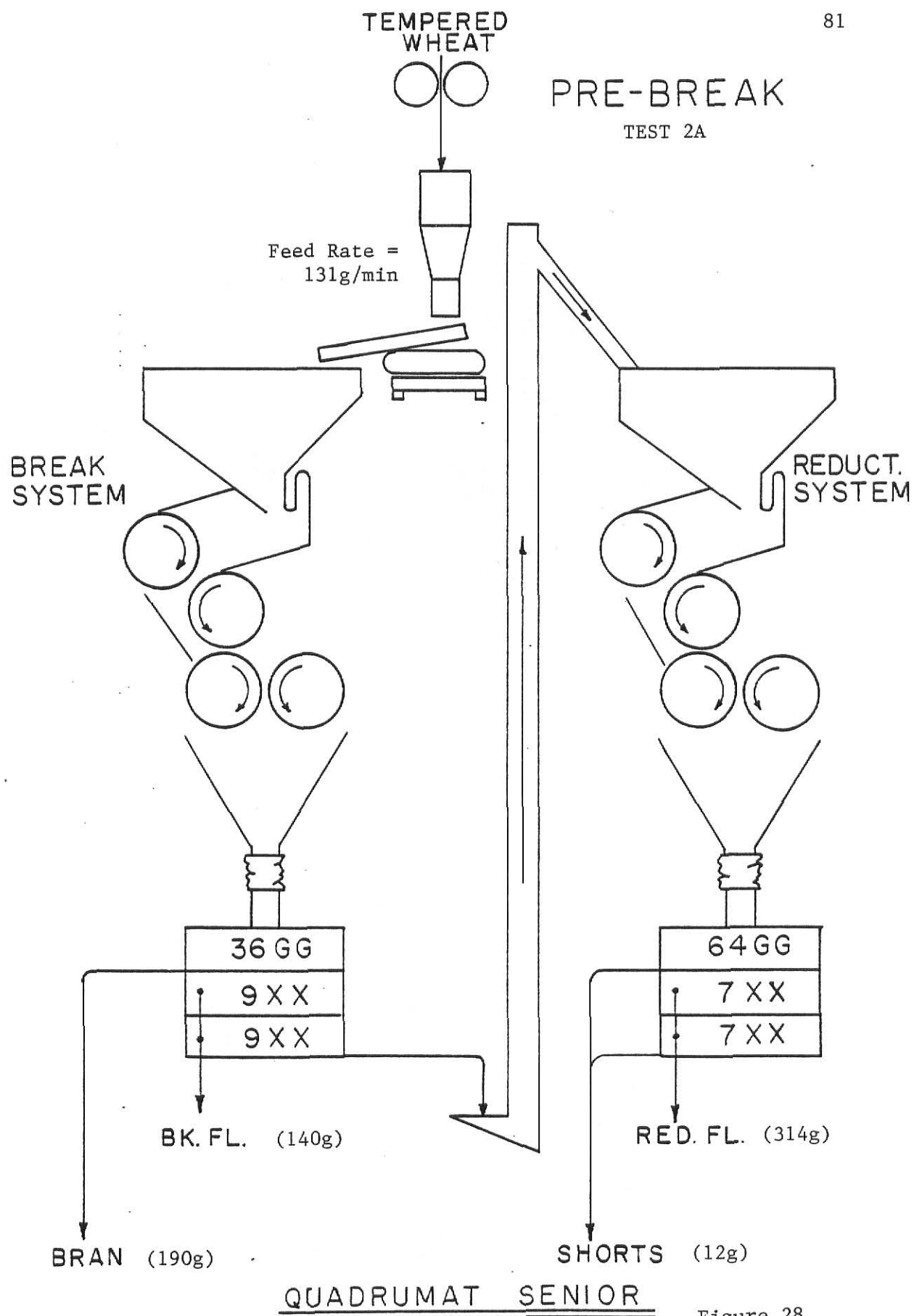


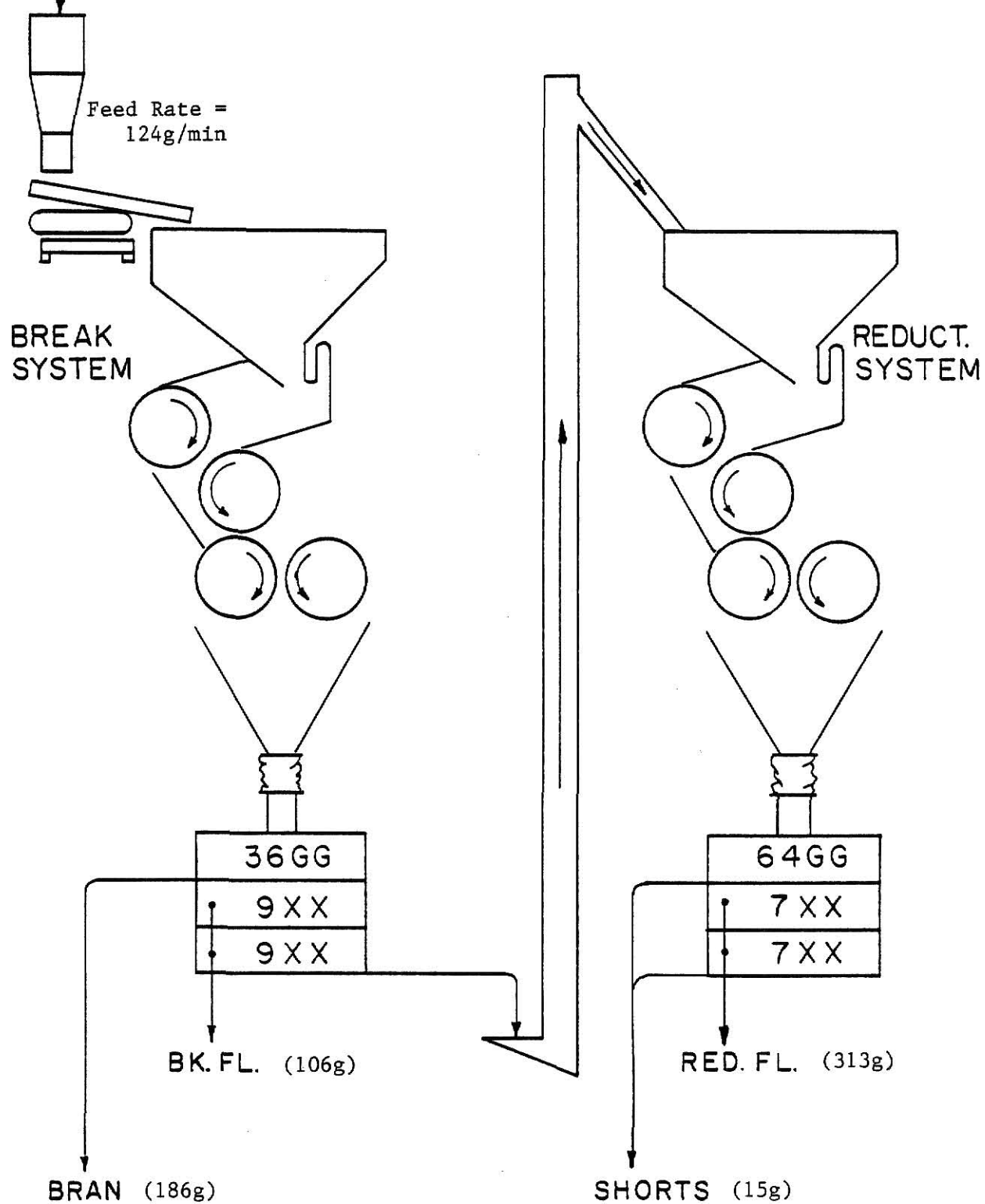
Figure 28

TEMPERED  
WHEAT

82

# NO PRE-BREAK

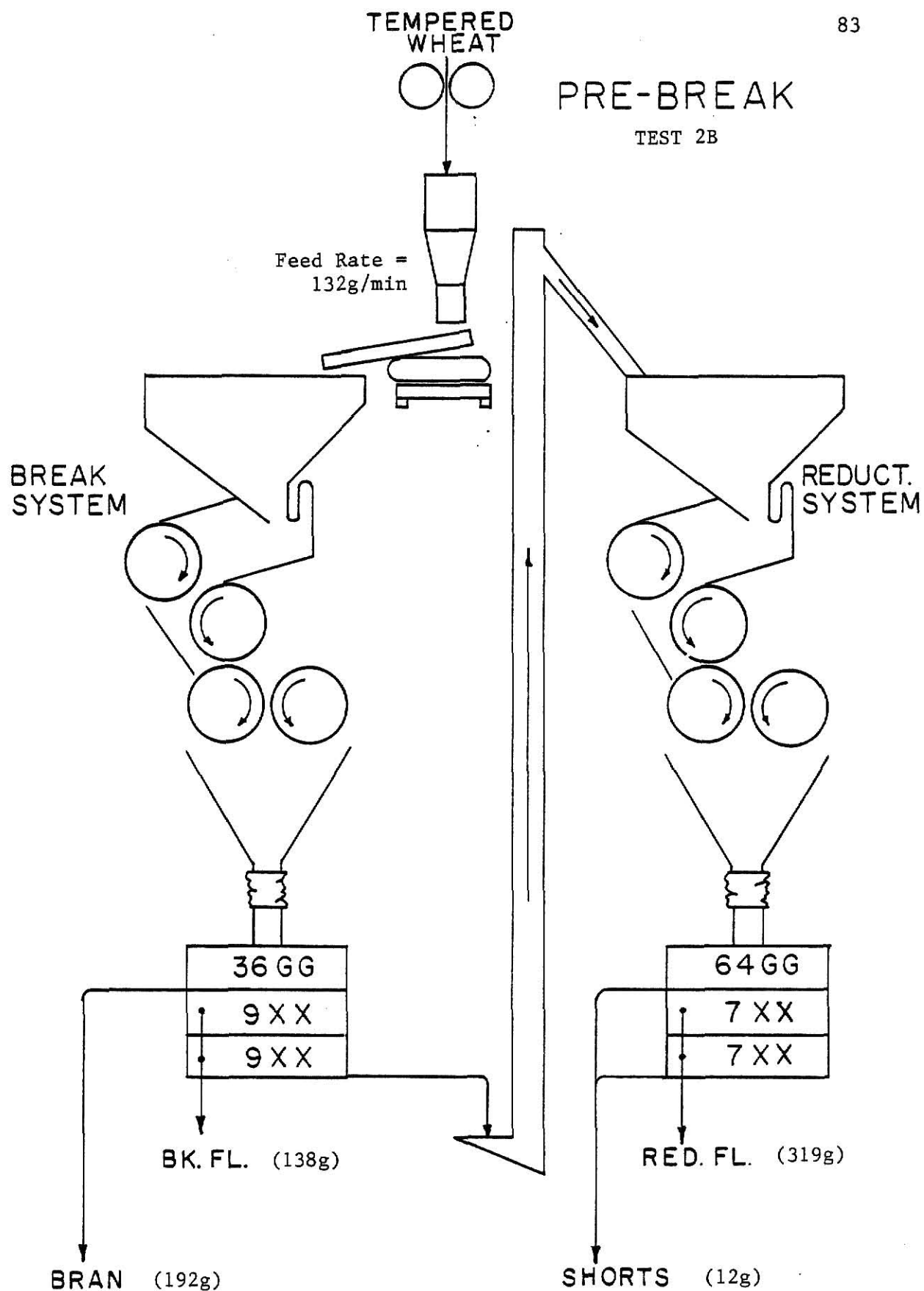
TEST 1B



QUADRUMAT SENIOR

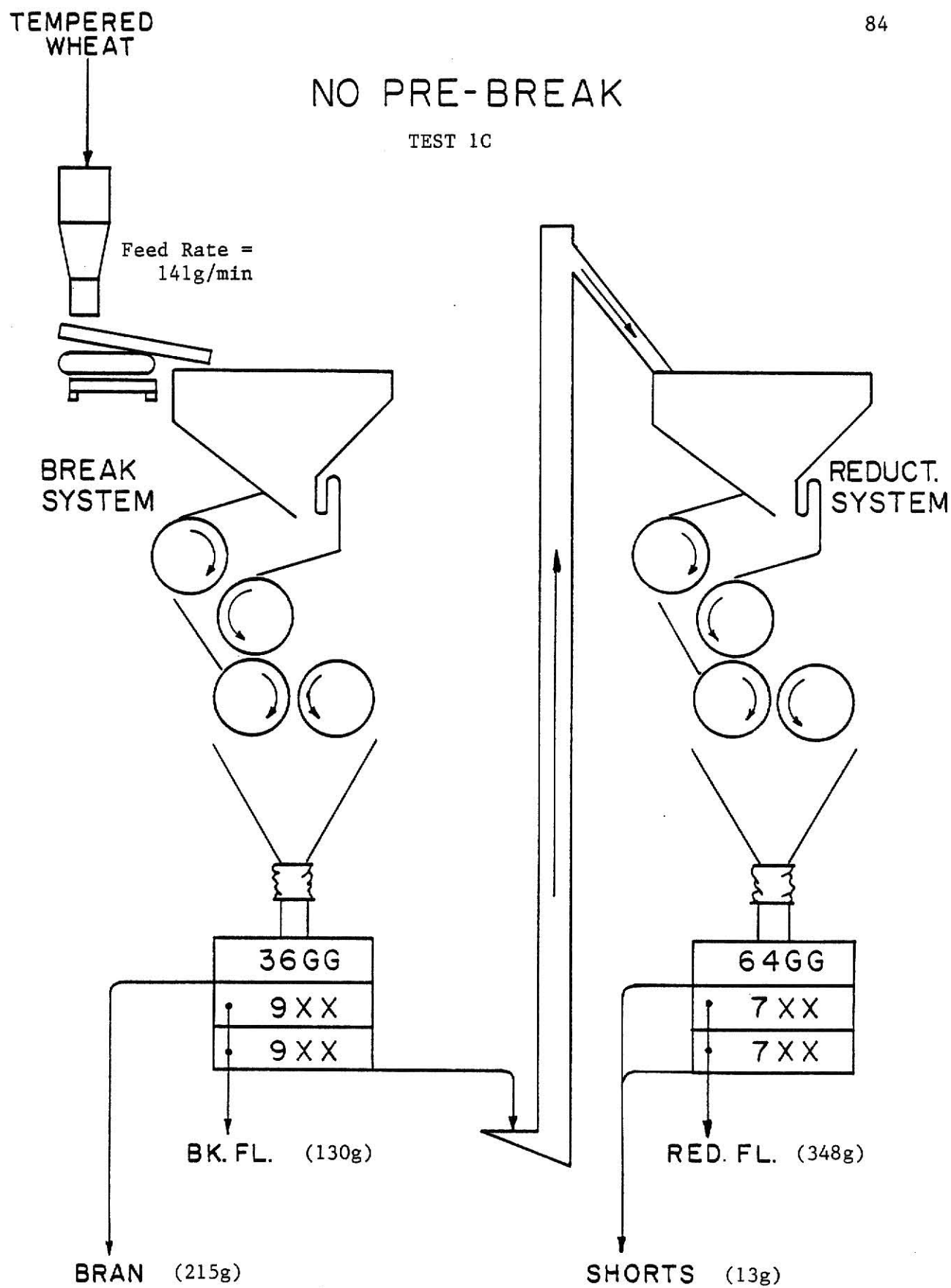
Figure 29





QUADRUMAT SENIOR

Figure 30



QUADRUMAT SENIOR

Figure 31

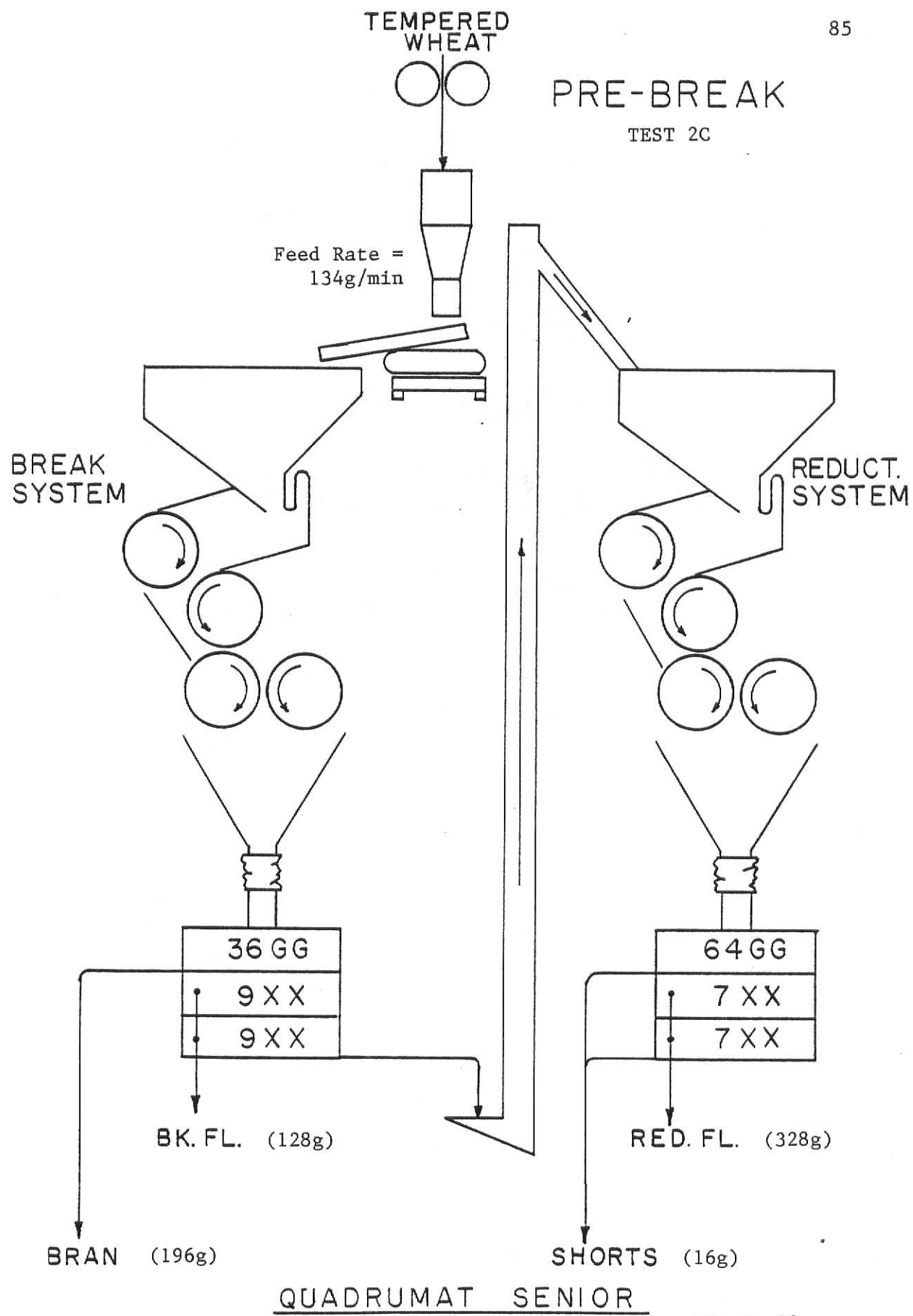
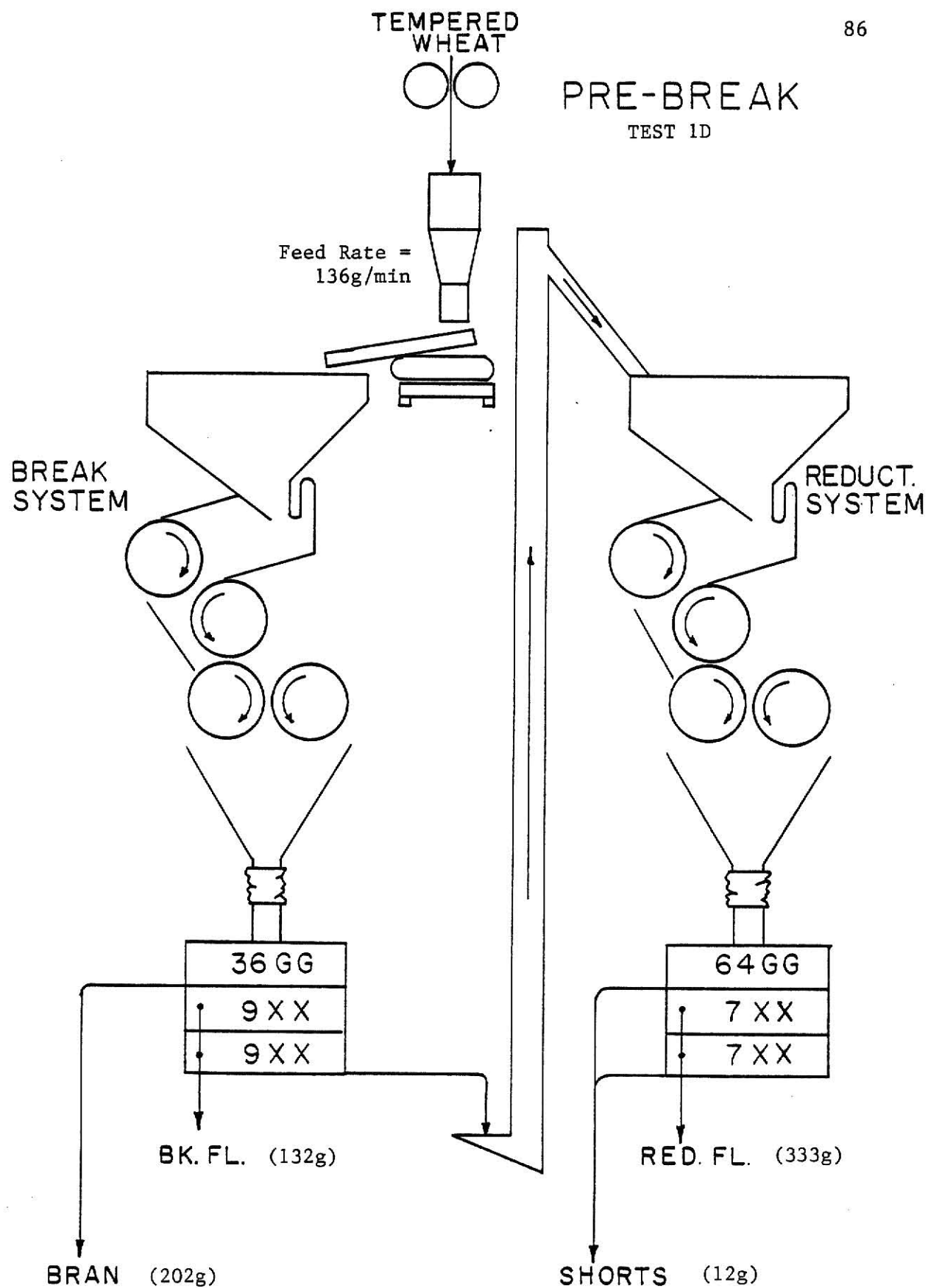


Figure 32



QUADRUMAT SENIOR

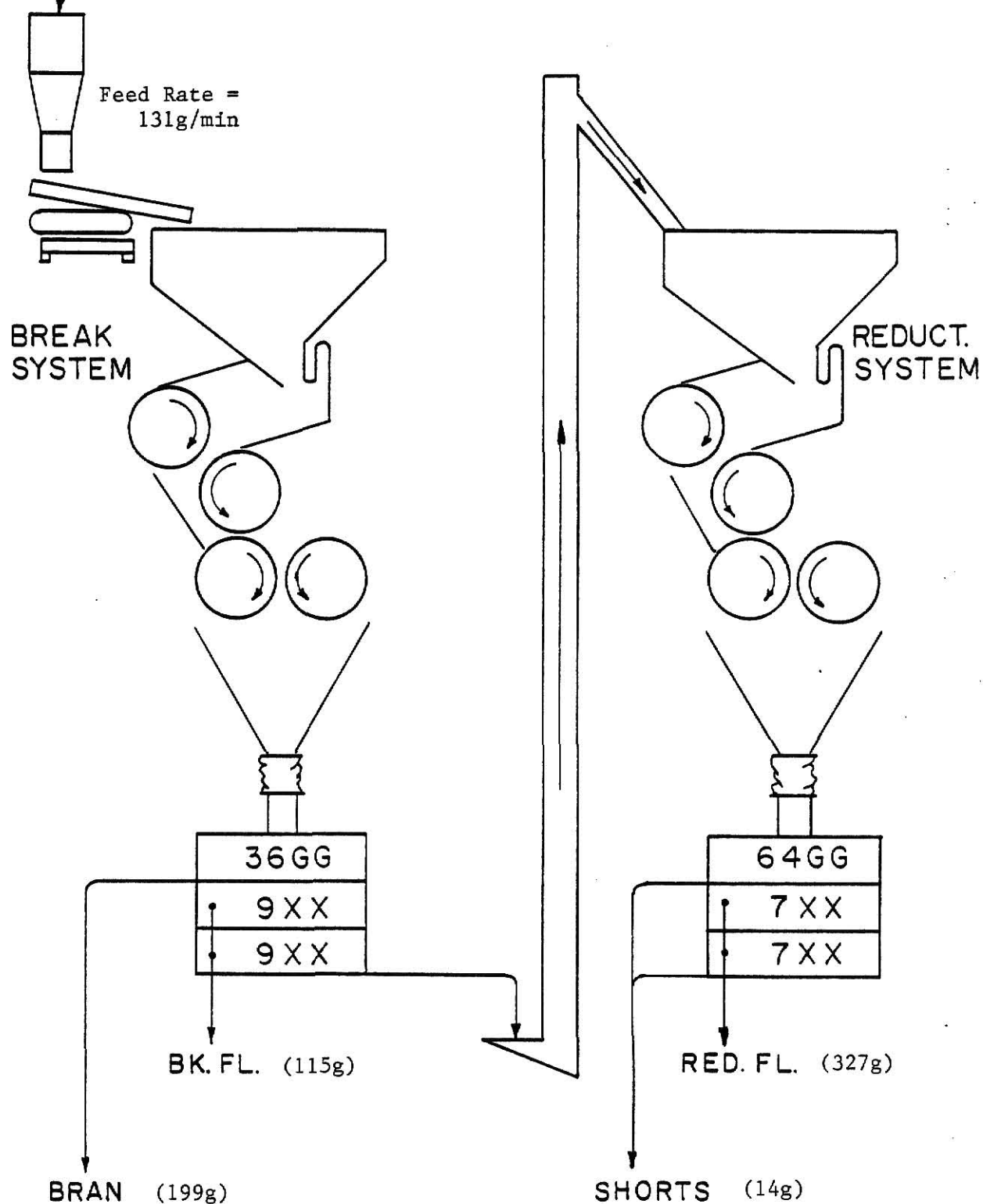
Figure 33

TEMPERED  
WHEAT

87

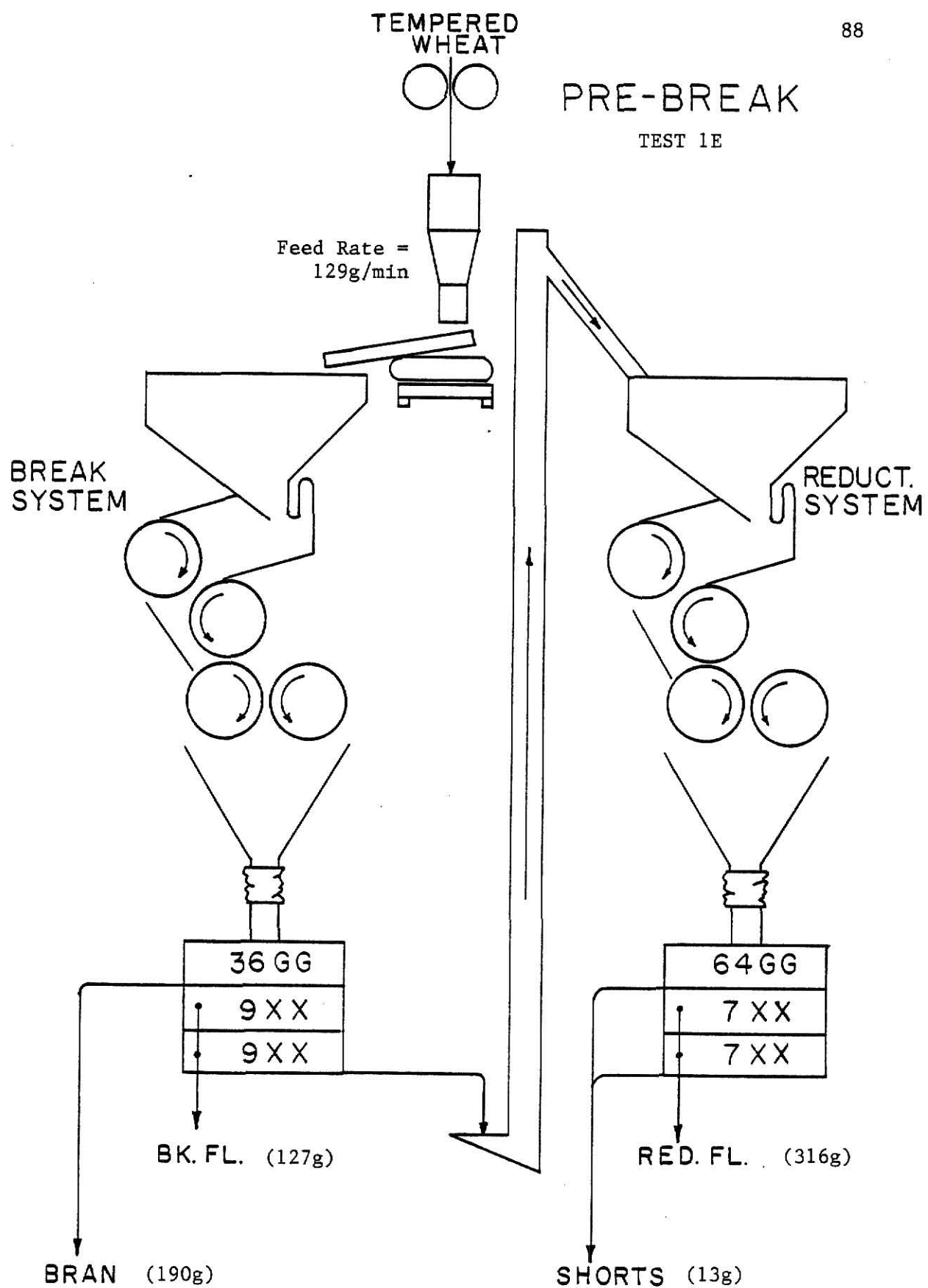
# NO PRE-BREAK

TEST 2D



QUADRUMAT SENIOR

Figure 34



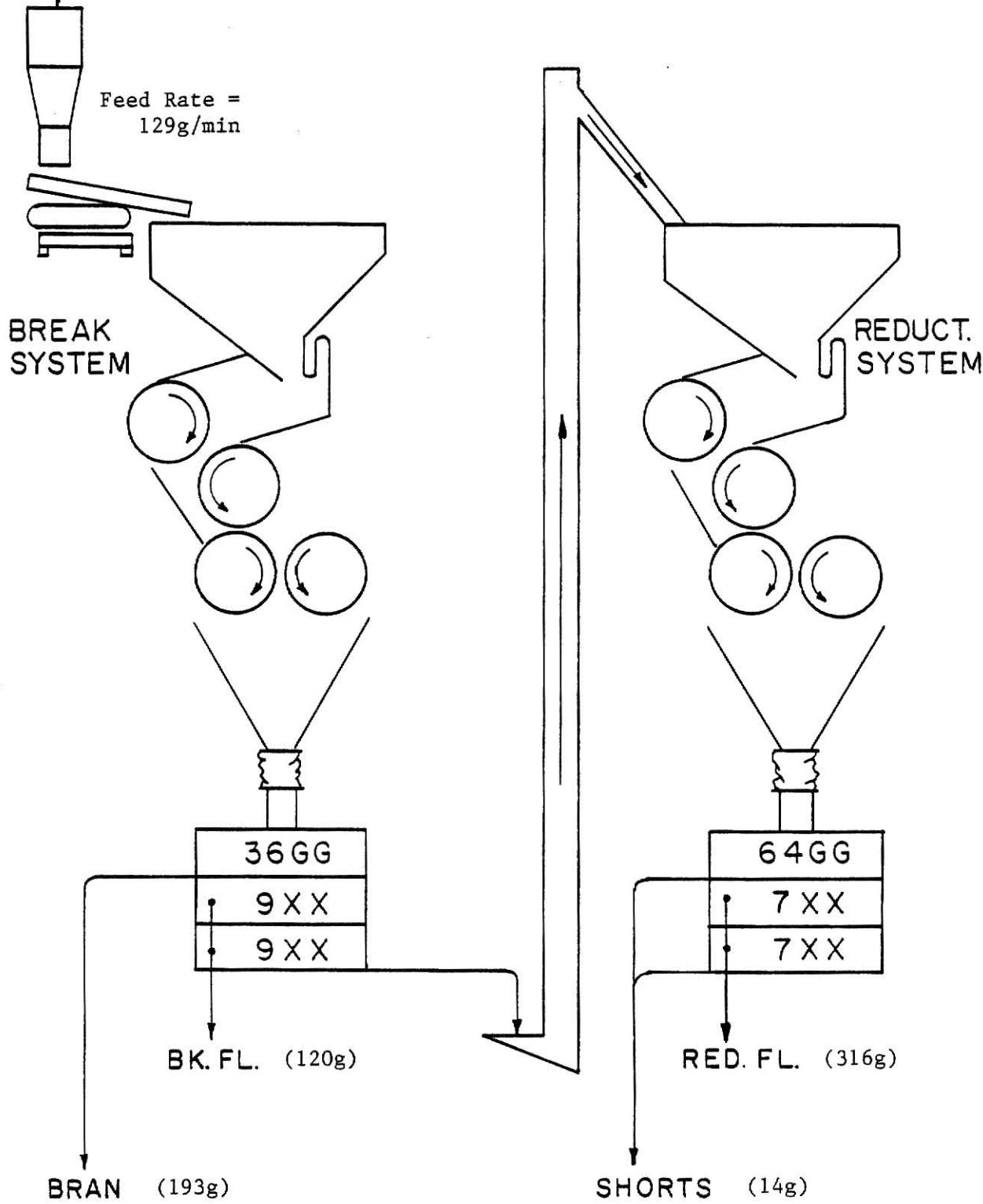
QUADRUMAT SENIOR

Figure 35

TEMPERED  
WHEAT

# NO PRE-BREAK

TEST 2E



QUADRUMAT SENIOR

Figure 36

## Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)  
 Q=QUANTITY (% of Total Products)  
 S= SUMMATION

MILL QUADRUMAT SENIOR  
 TEST A, B, C, D, E  
 WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	Q X A	S of QXA	S of QXA S of Q
TEST 1A NO PRE-BREAK							
RED FL	311	48.82	48.82	.357	17.429	17.429	.357
BK FL	129	20.25	69.07	.369	7.472	24.901	.361
TEST 2A PRE-BREAK							
BK FL	140	21.34	21.34	.308	6.573	6.573	.308
RED FL	314	47.87	69.21	.337	16.132	22.705	.325
TEST 1B NO PRE-BREAK							
BK FL	106	17.10	17.10	.318	5.438	5.438	.318
RED FL	313	50.48	67.58	.328	16.557	21.995	.325
TEST 2B PRE-BREAK							
BK FL	138	20.88	20.88	.308	6.431	6.431	.308
RED FL	319	48.26	69.14	.328	15.829	22.260	.322
TEST 1C PRE-BREAK							
BK FL	130	18.41	18.41	.308	5.670	5.670	.308
RED FL	348	49.29	67.70	.336	16.561	22.231	.328
TEST 2C NO PRE-BREAK							
BK FL	128	19.16	19.16	.329	6.304	6.304	.329
RED FL	328	49.10	68.26	.348	17.087	23.391	.343
TEST 1D PRE-BREAK							
RED FL	333	49.04	49.04	.318	15.595	15.595	.318
BK FL	132	19.44	68.58	.319	6.201	21.796	.318
TEST 2D NO PRE-BREAK							
BK FL	115	17.56	17.56	.327	5.742	5.742	.327
RED FL	327	49.92	67.48	.335	16.723	22.465	.333
TEST 1E PRE-BREAK							
BK FL	127	19.66	19.66	.317	6.232	6.232	.317
RED FL	316	48.92	68.58	.338	16.535	22.858	.333
TEST 2E NO PRE-BREAK							
BK FL	120	18.66	18.66	.330	6.158	6.158	.330
RED FL	316	49.14	67.80	.349	17.150	23.308	.344



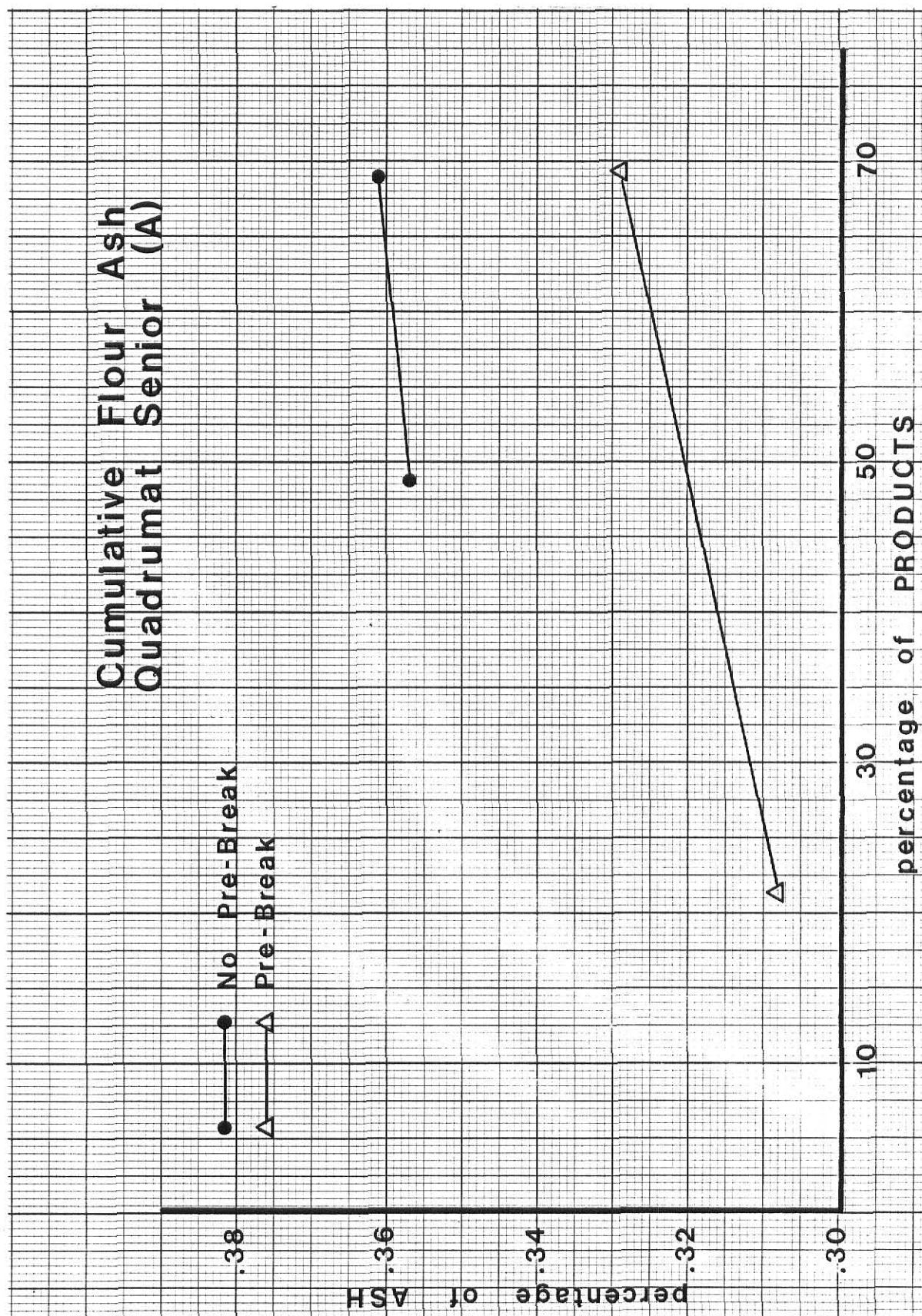


Figure 37

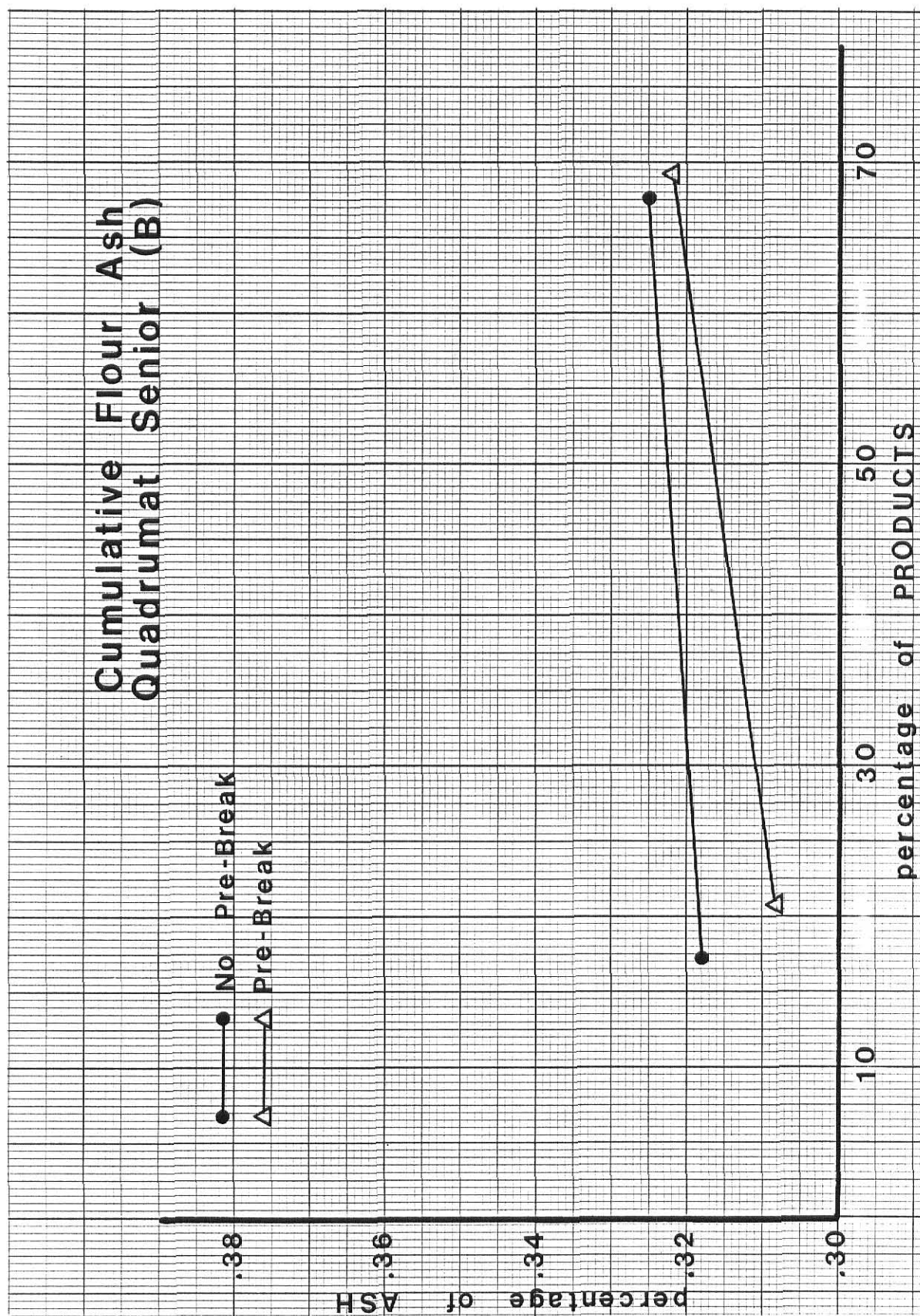


Figure 38

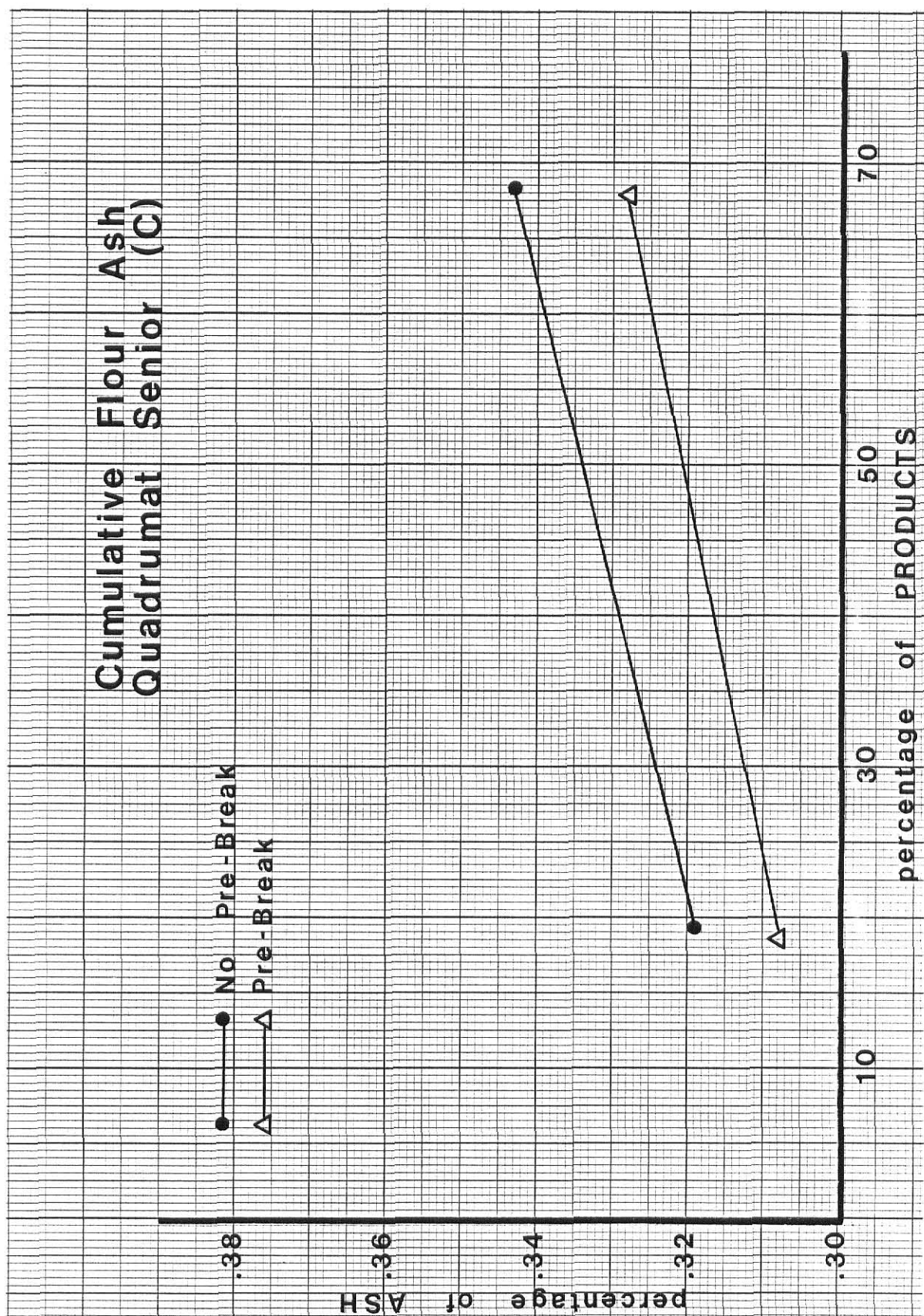


Figure 39



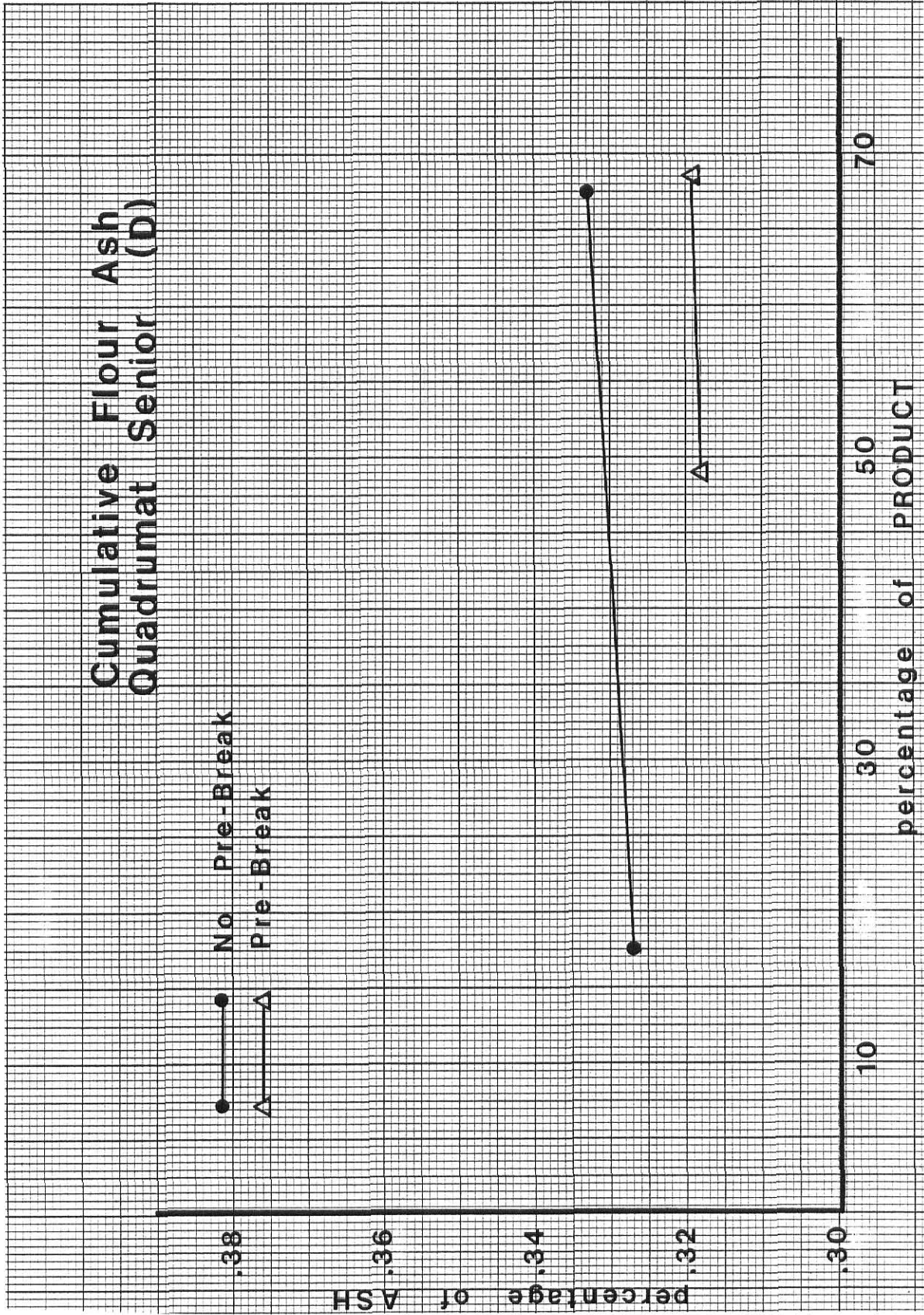


Figure 40

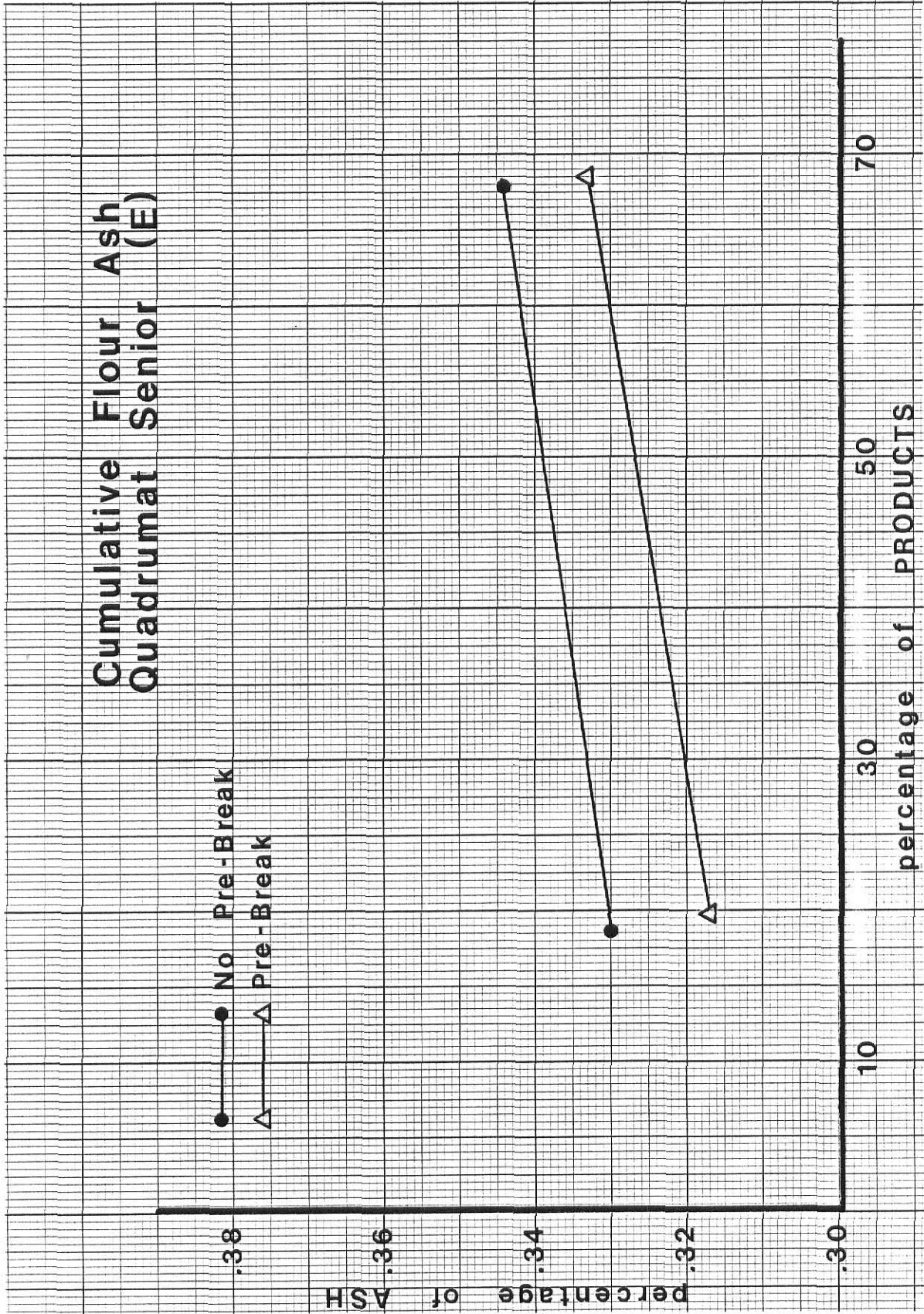


Figure 41



## PRE-BREAK

TEST 2A

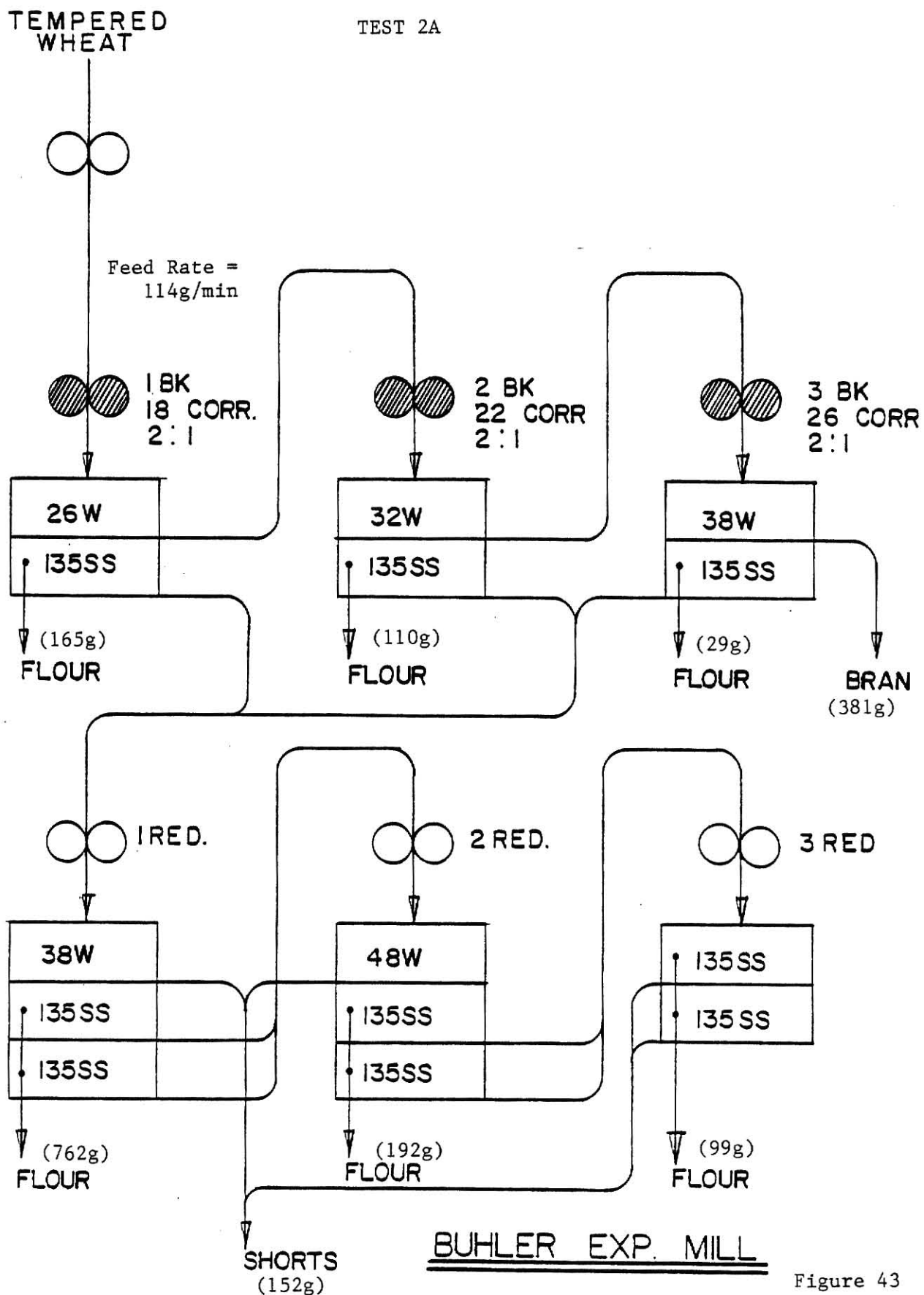


Figure 43

# PRE-BREAK (sifted)

98

TEST 3A

TEMPERED WHEAT

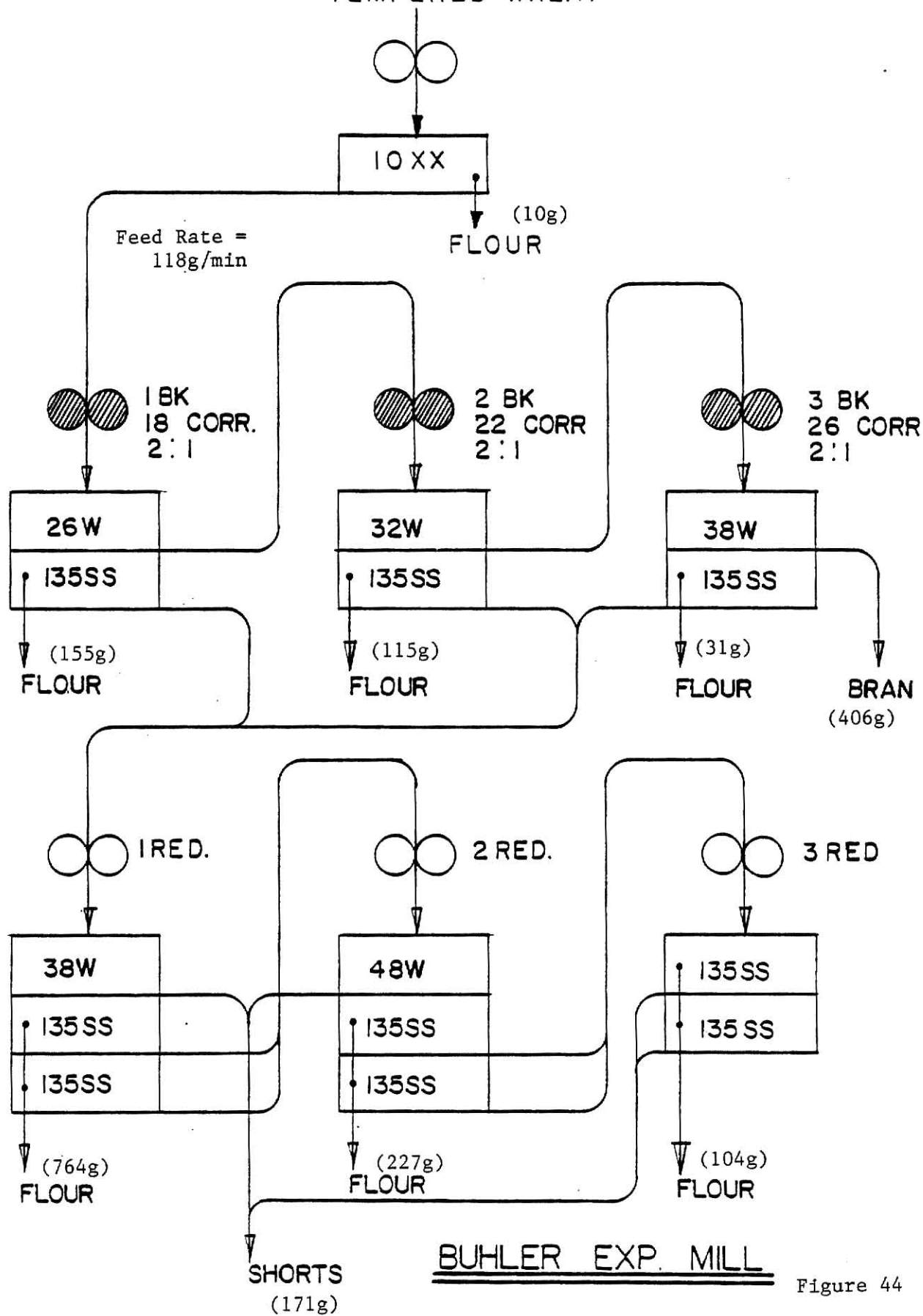


Figure 44



# NO PRE-BREAK

TEST 1A-2

TEMPERED  
WHEAT

Feed Rate =  
105g/min

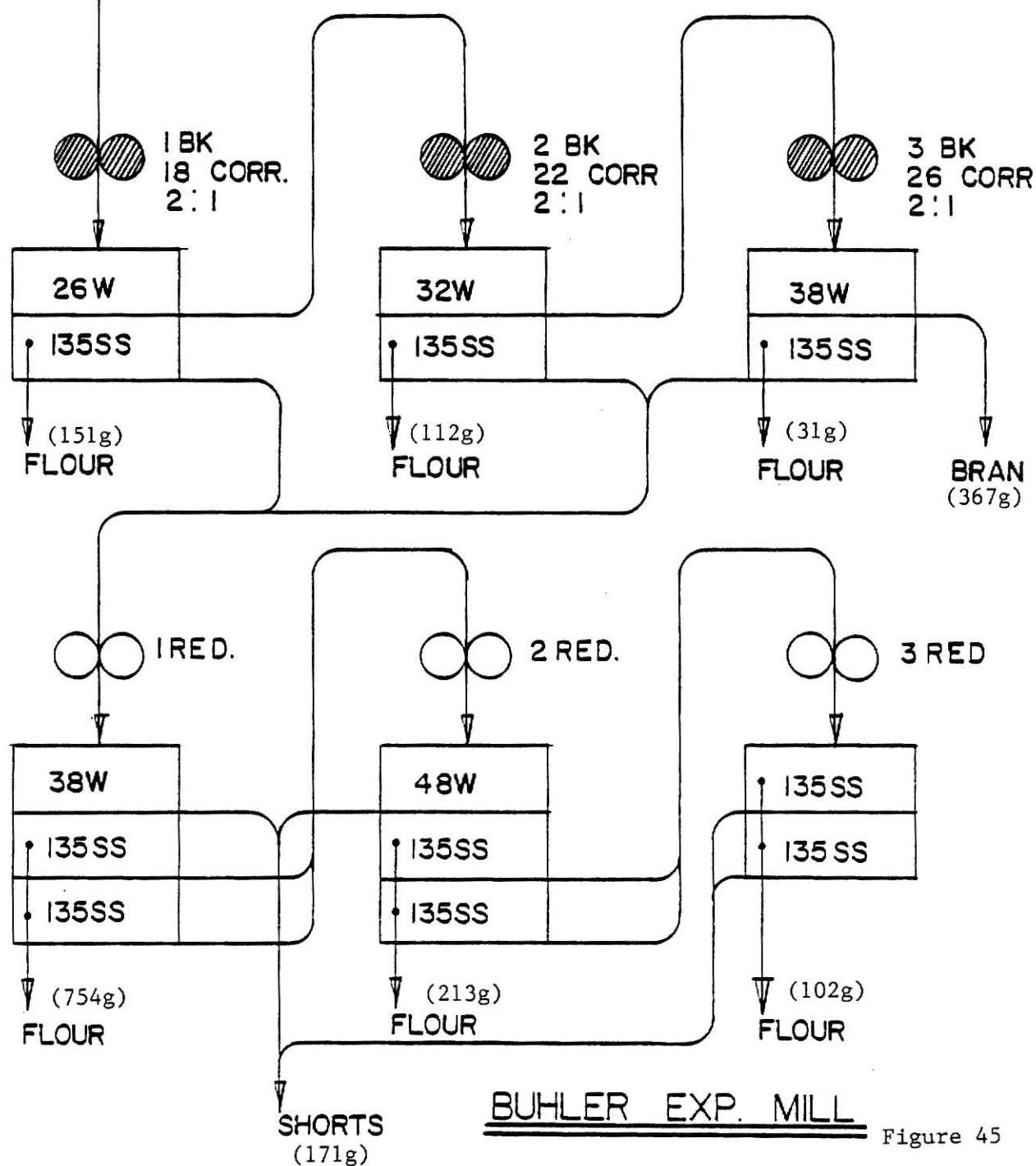


Figure 45

# PRE-BREAK (sifted)

100

TEST 1B-1  
TEMPERED WHEAT

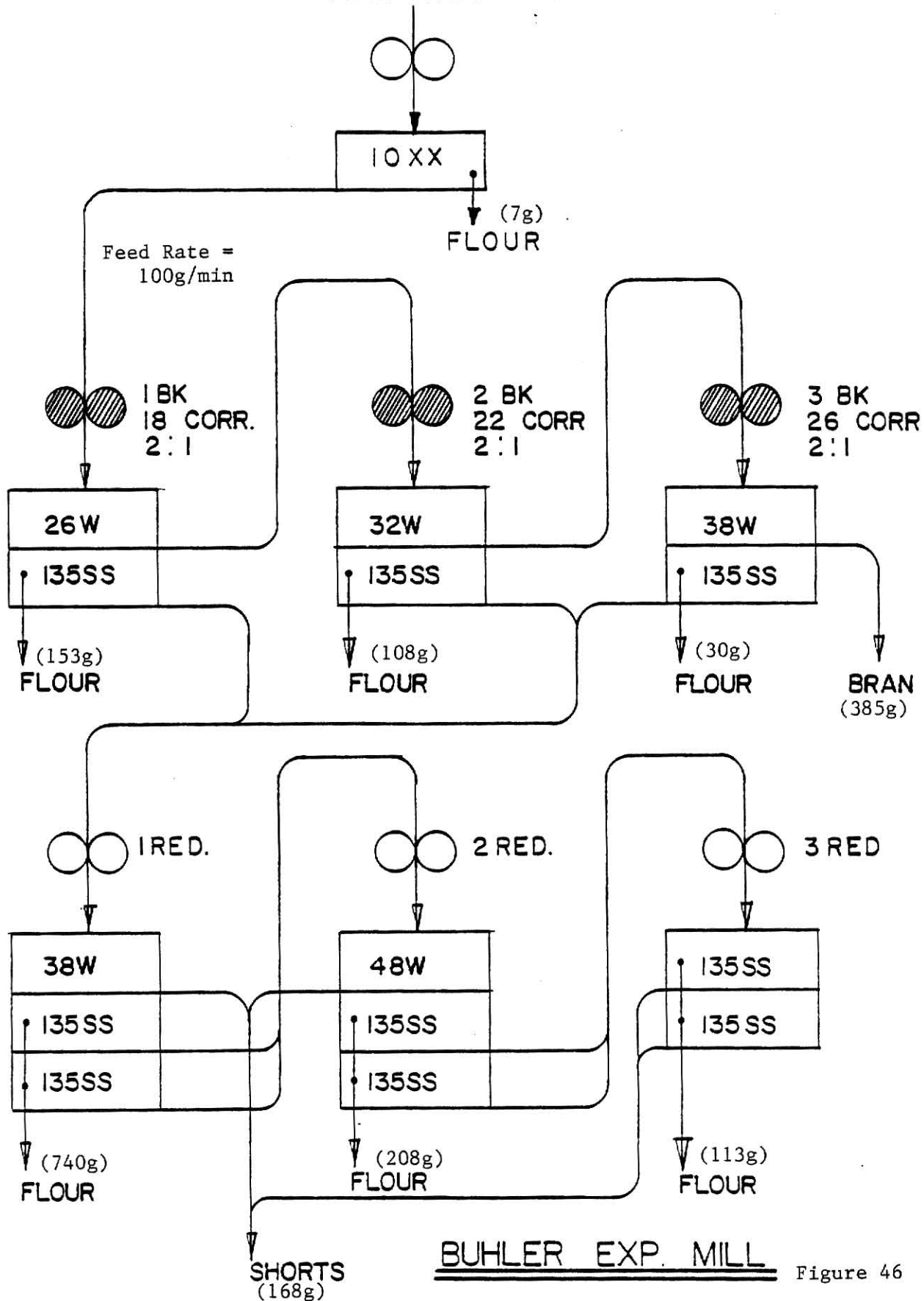


Figure 46

## NO PRE-BREAK

TEST 2B

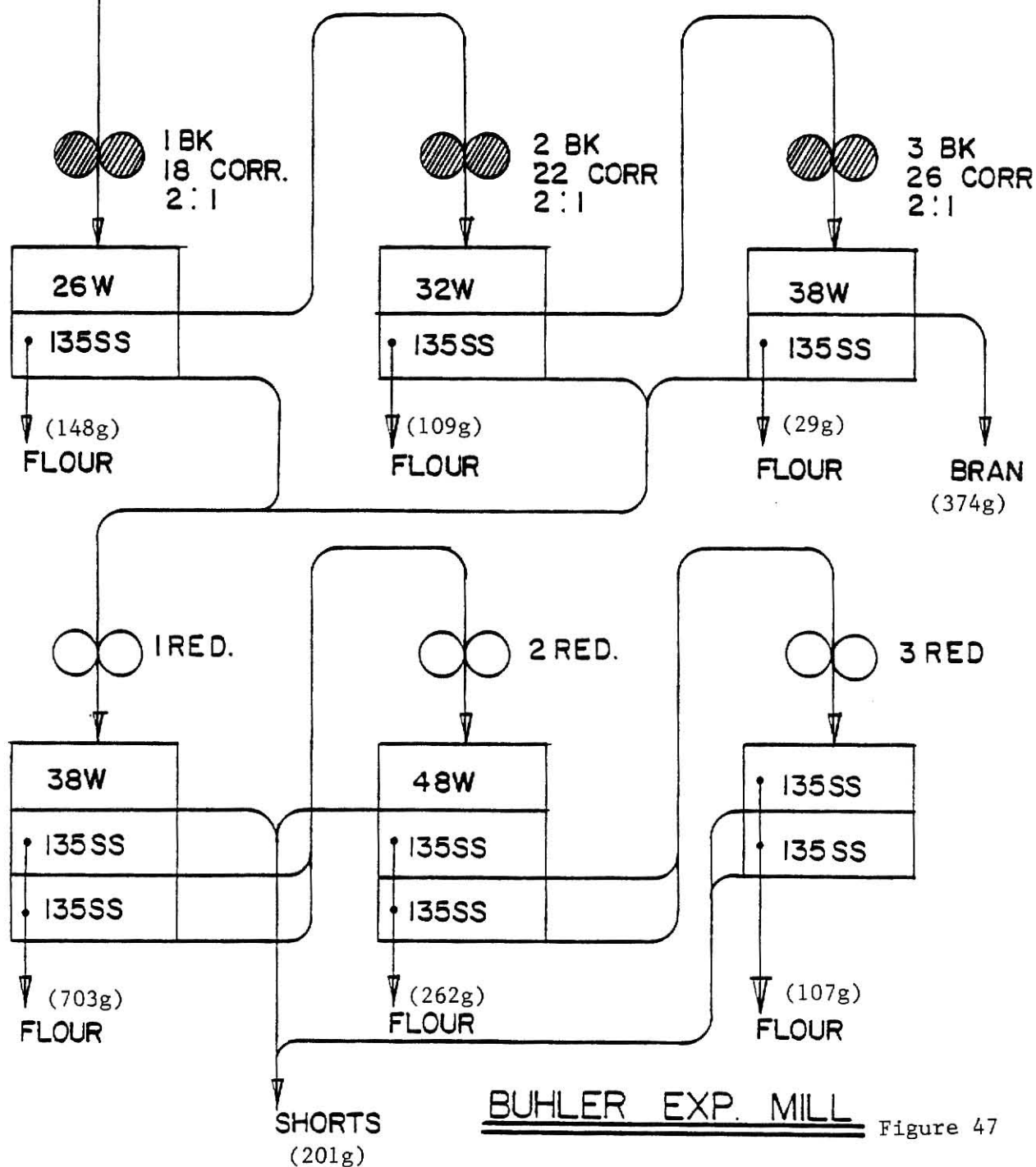
TEMPERED  
WHEATFeed Rate =  
118g/min

Figure 47

## PRE-BREAK

TEST 3B

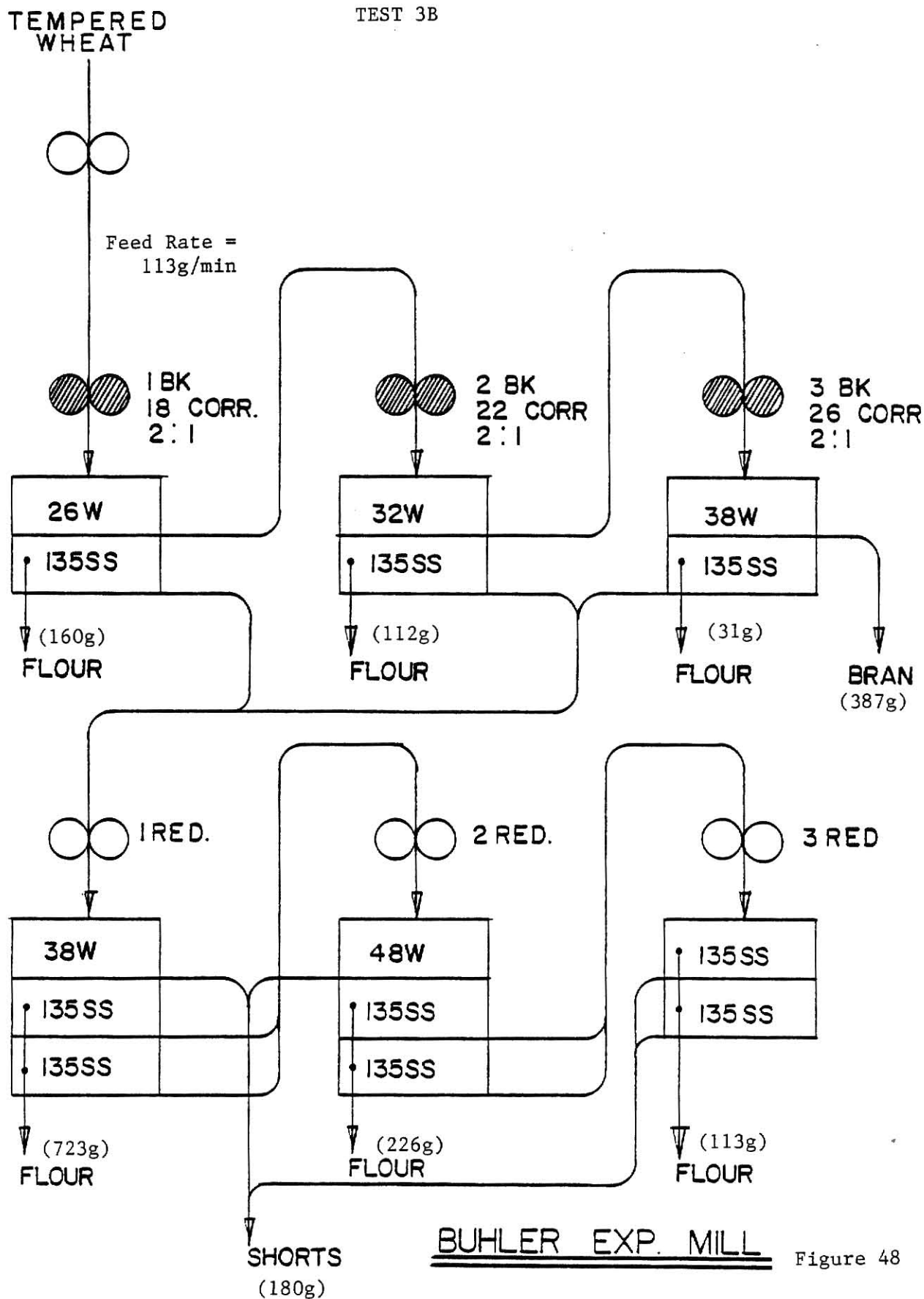


Figure 48

# PRE-BREAK (sifted)

103

TEST 1B-2

TEMPERED WHEAT

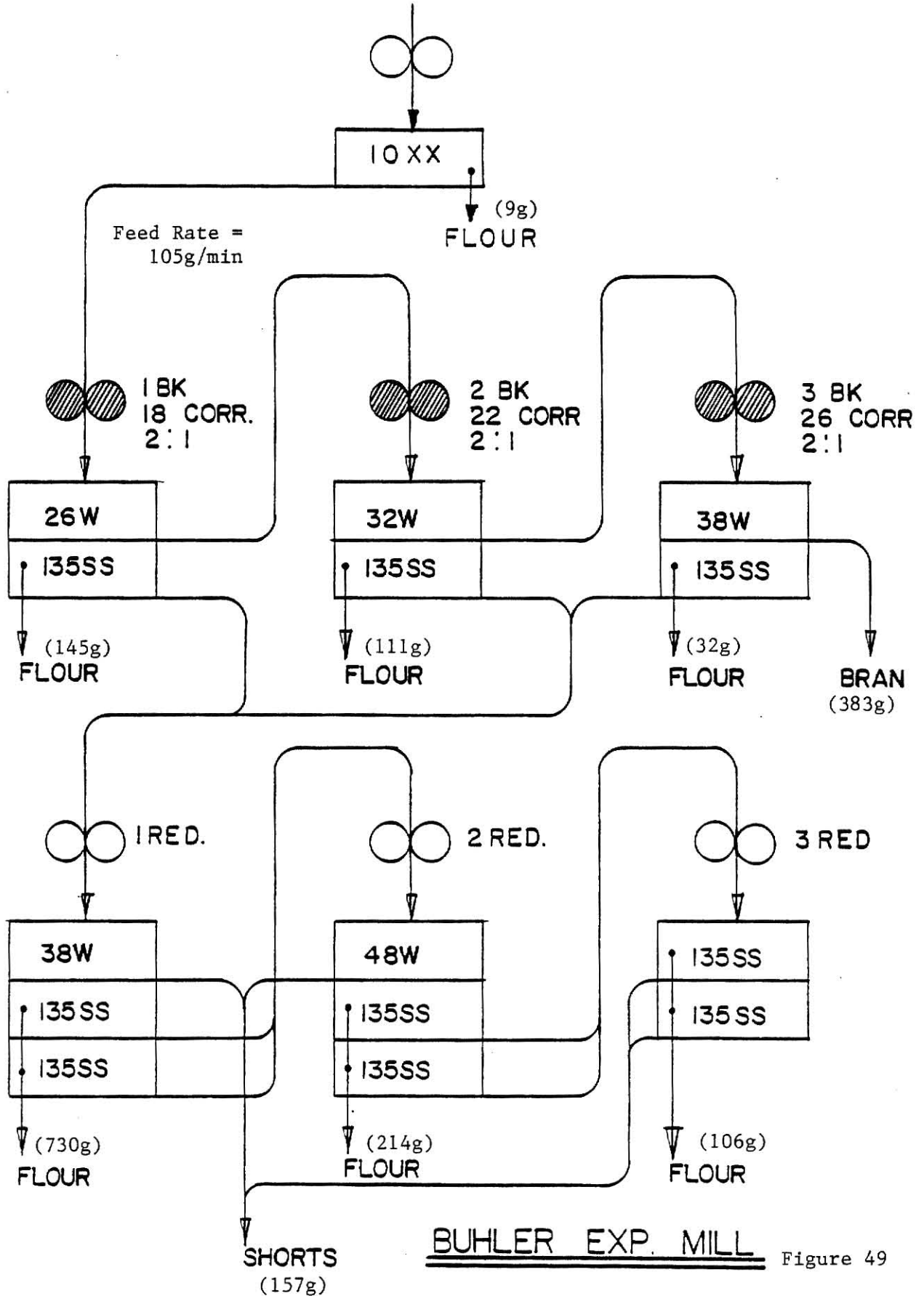


Figure 49



# PRE-BREAK (sifted)

105

TEST 2C

TEMPERED WHEAT

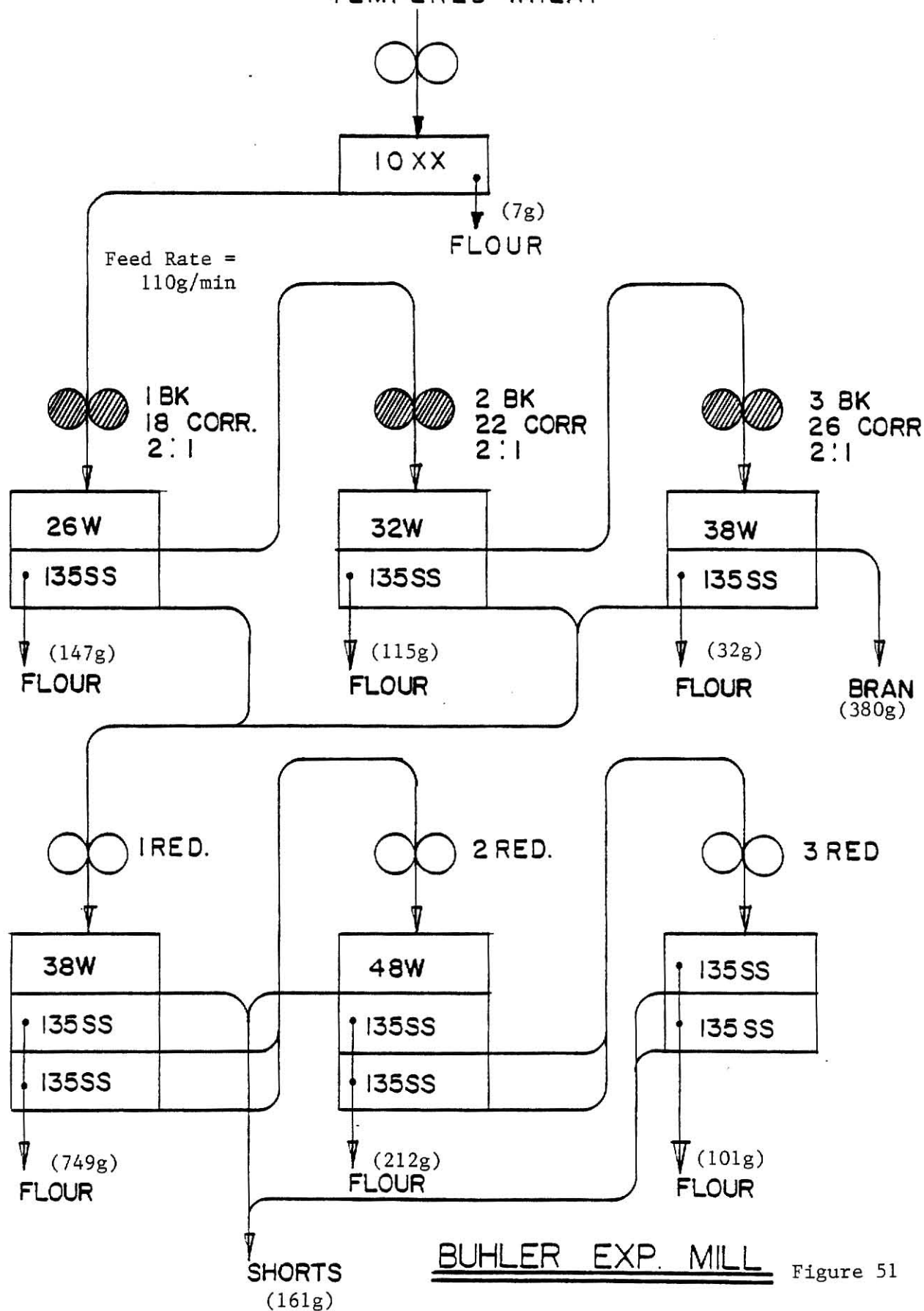


Figure 51

## NO PRE-BREAK

TEST 3C

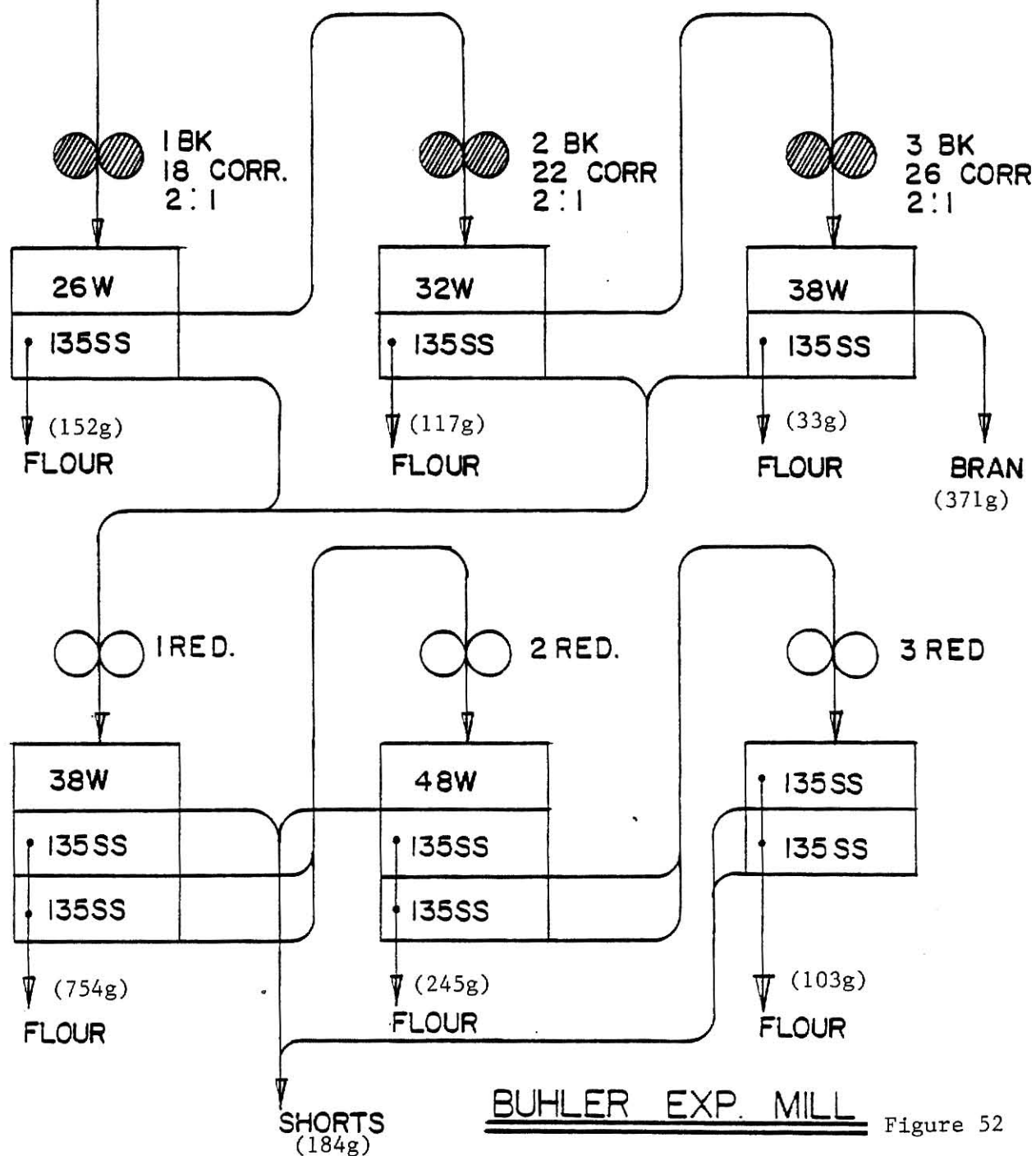
TEMPERED  
WHEATFeed Rate =  
111g/min

Figure 52



## PRE-BREAK

TEST 1C-2

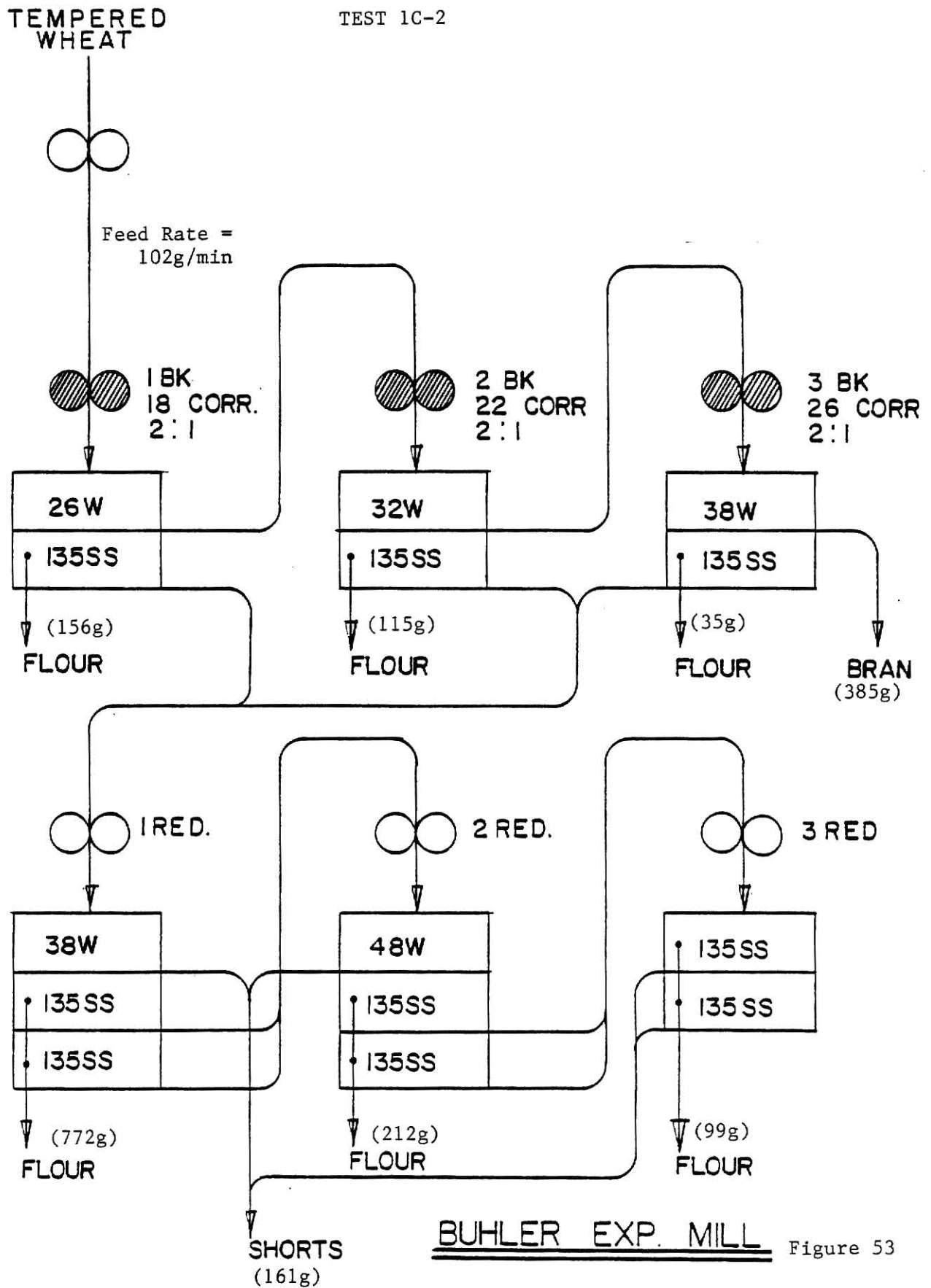


Figure 53

## NO PRE-BREAK

TEST 1D

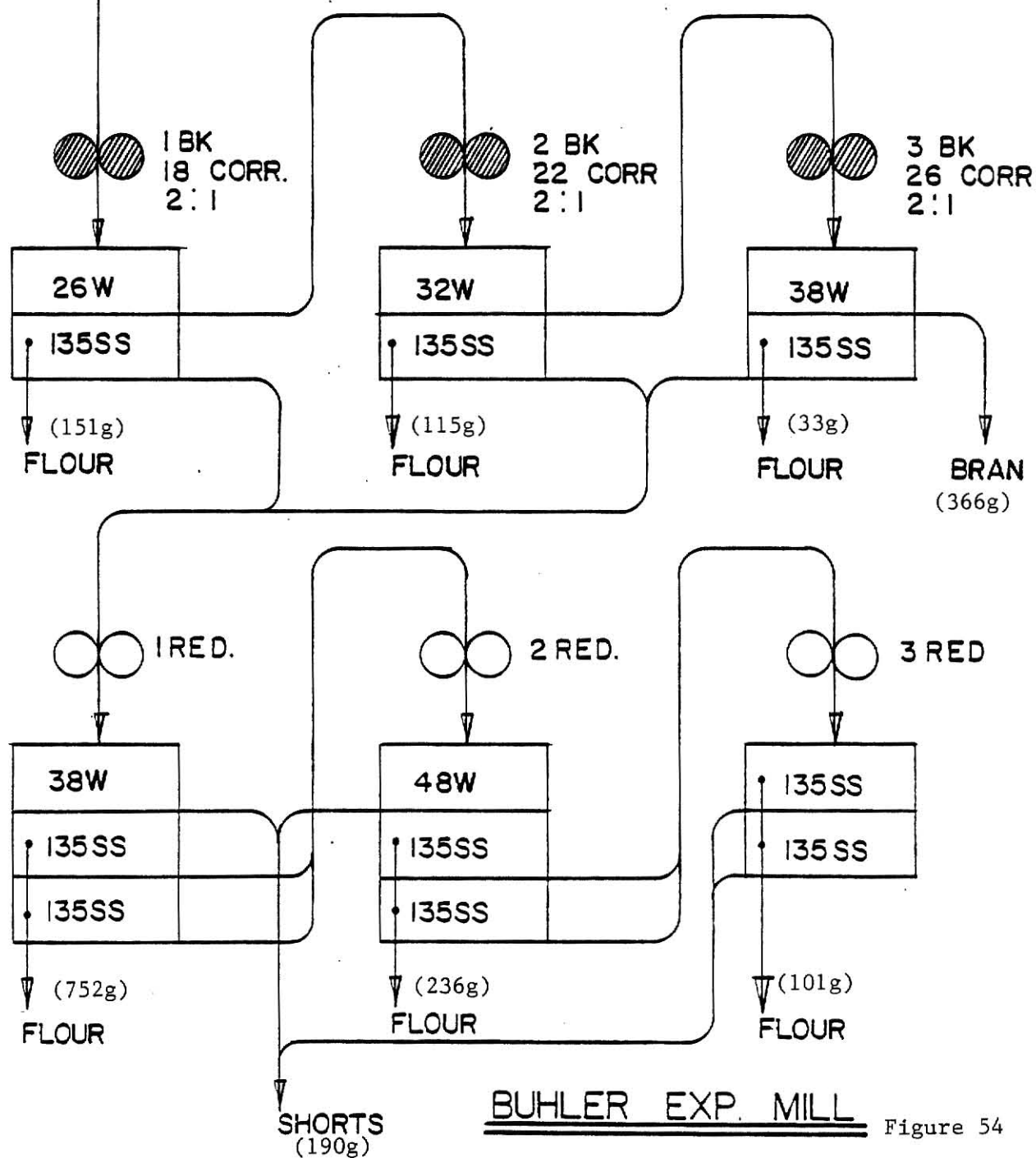
TEMPERED  
WHEATFeed Rate =  
107g/min

Figure 54

# PRE-BREAK (sifted)

109

TEST 2D

TEMPERED WHEAT

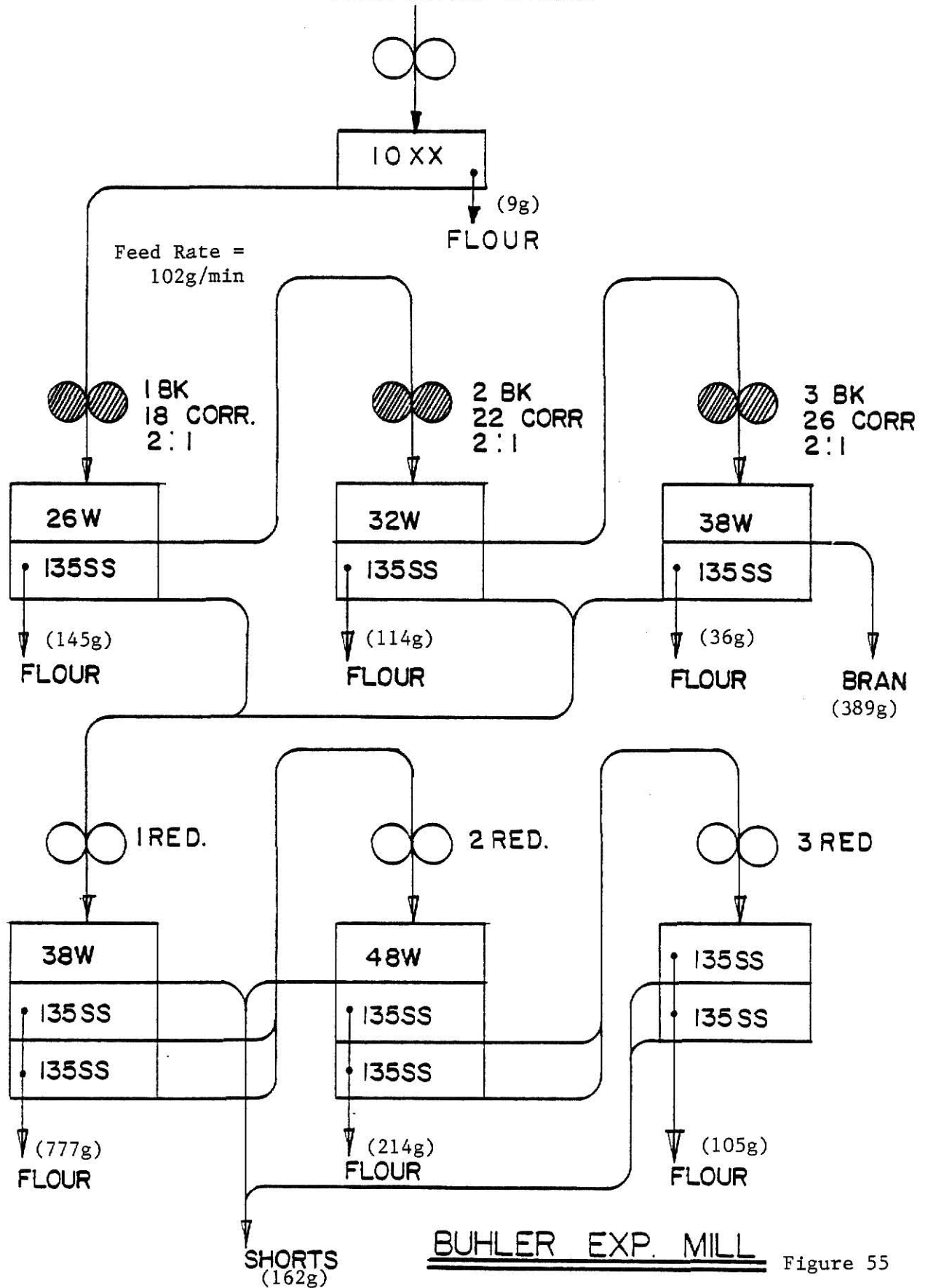


Figure 55

## PRE-BREAK

TEST 3D

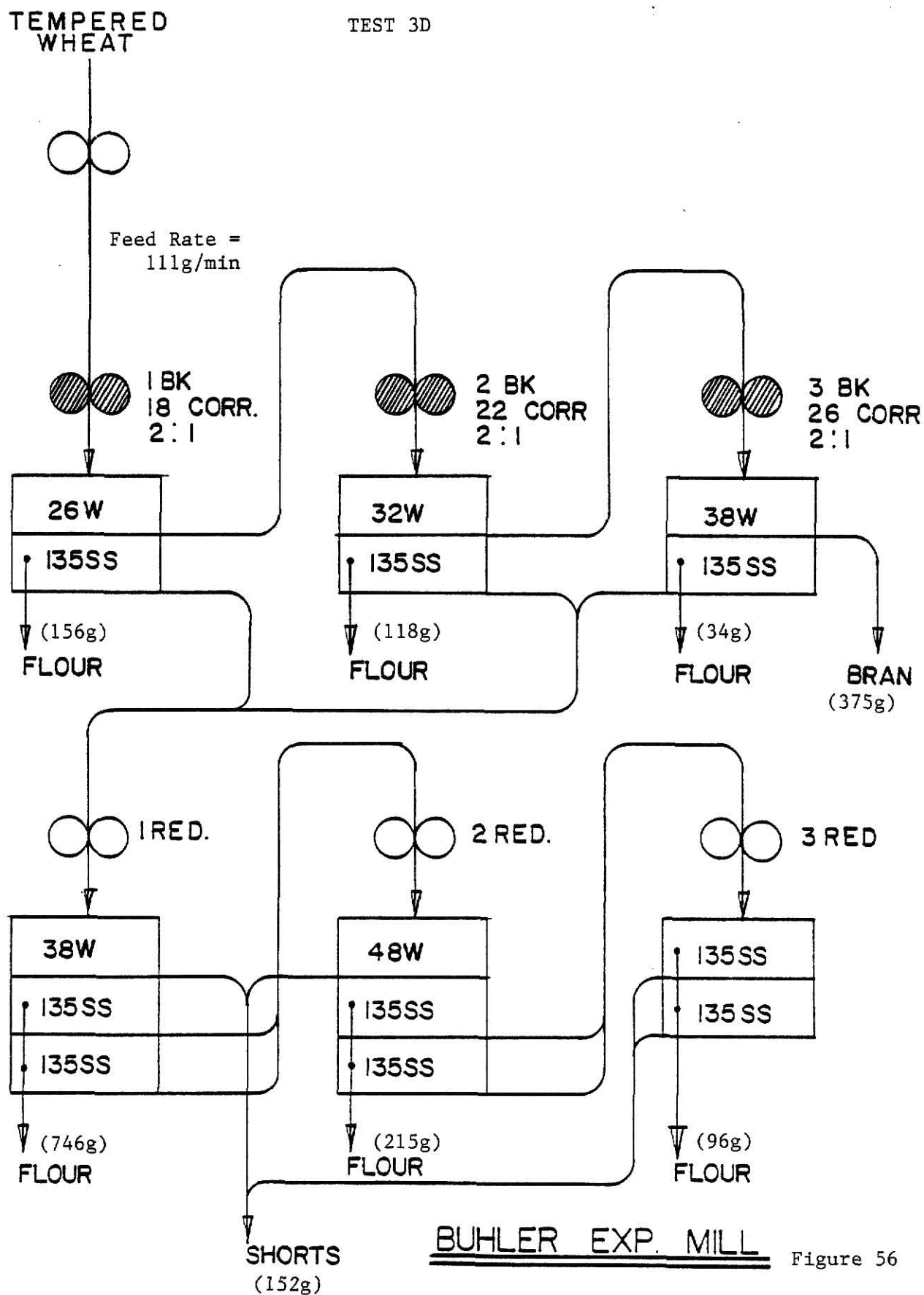


Figure 56

## NO PRE-BREAK

TEST 1D-2

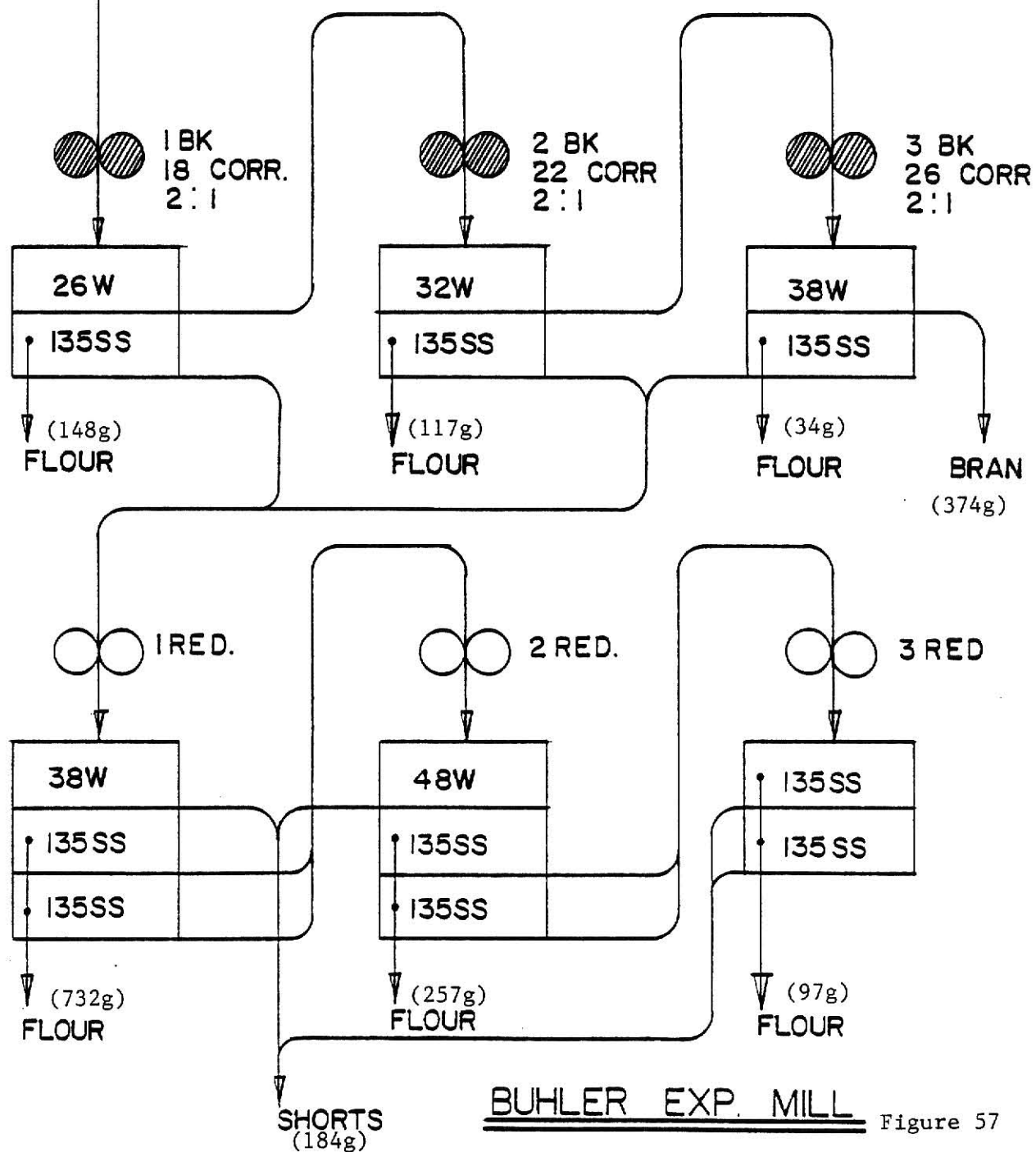
TEMPERED  
WHEATFeed Rate =  
118g/min

Figure 57

# PRE-BREAK (sifted)

112

TEST 1E-1

TEMPERED WHEAT

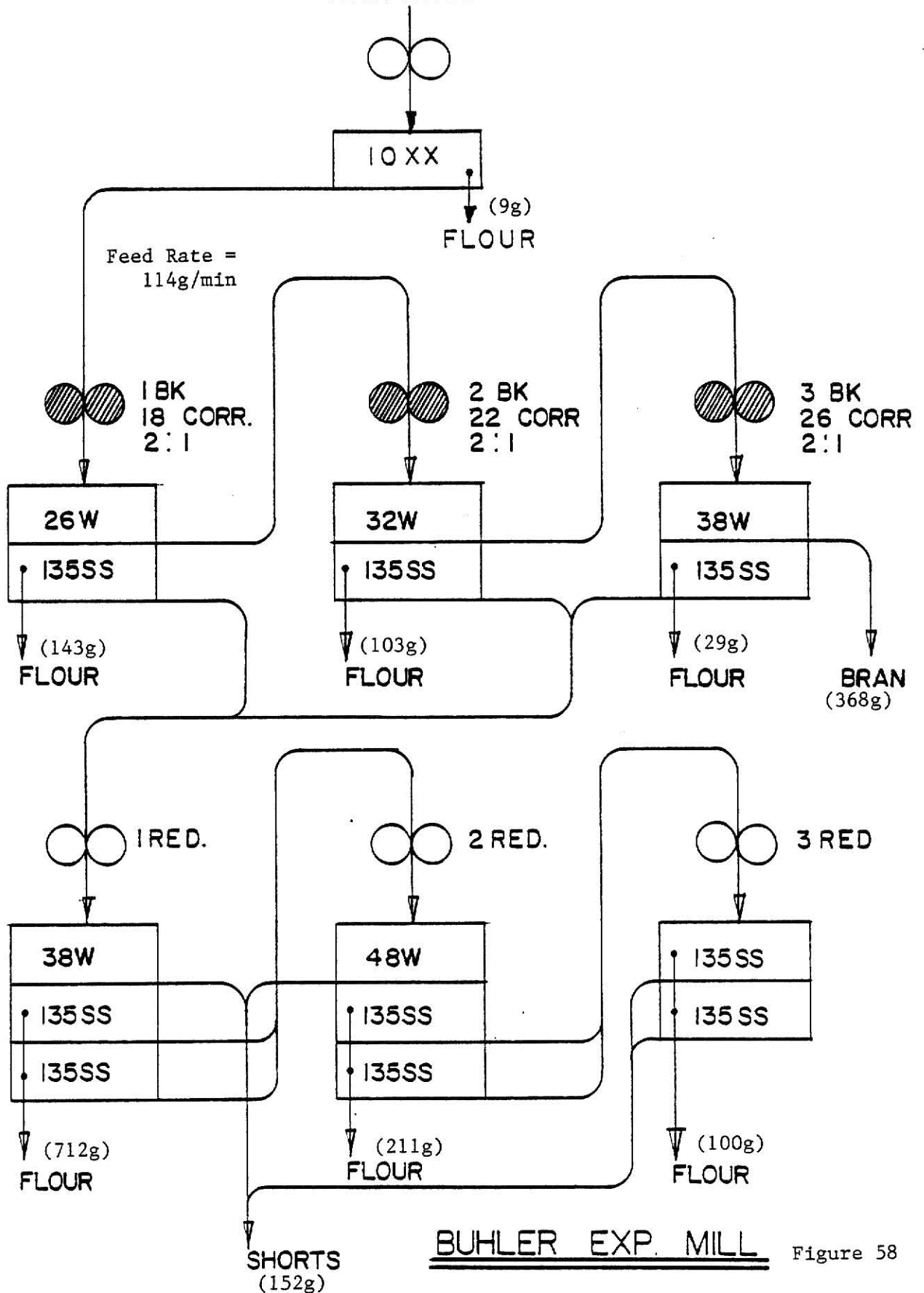


Figure 58

## PRE-BREAK

TEST 2E

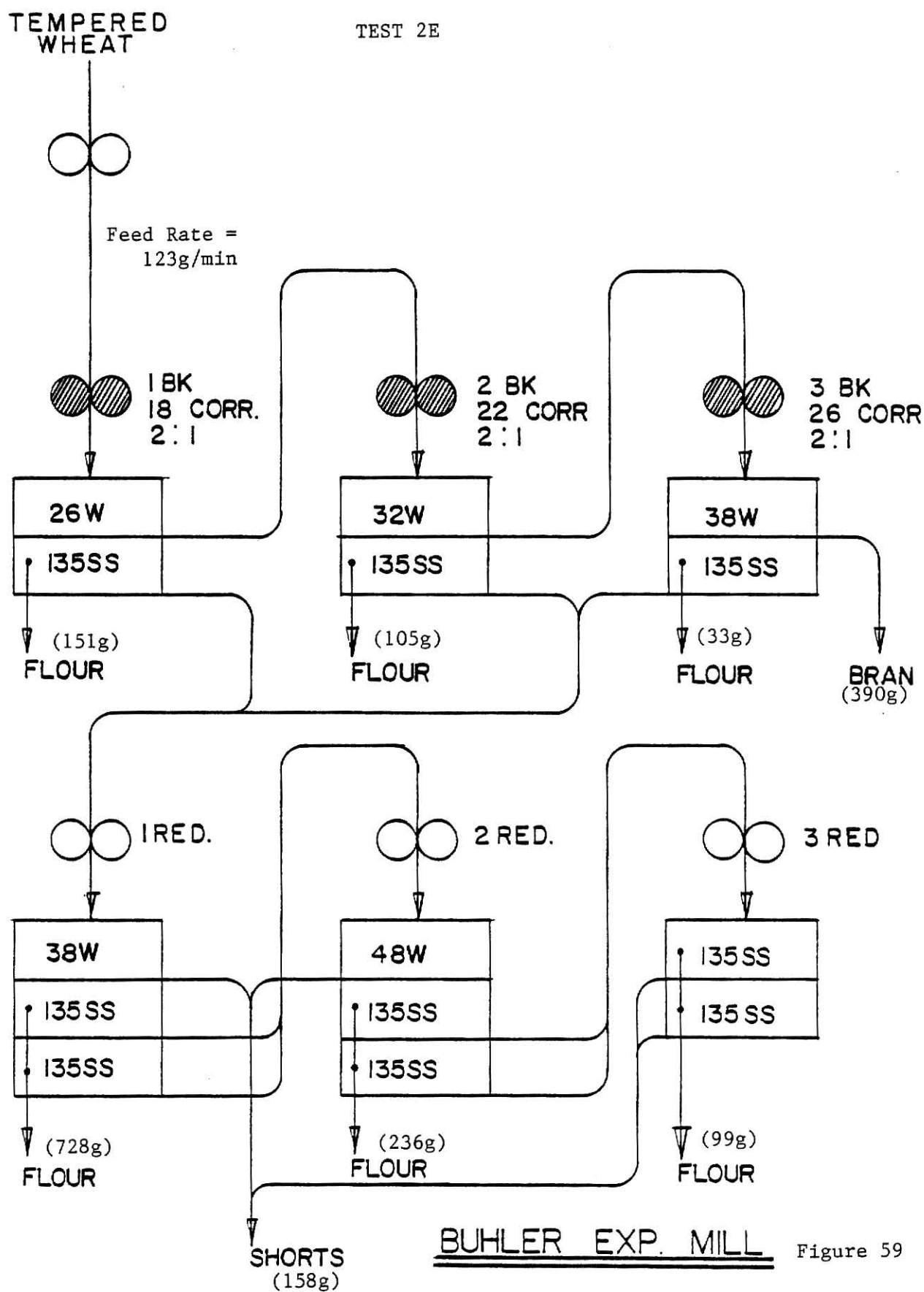


Figure 59

## NO PRE-BREAK

TEST 3E

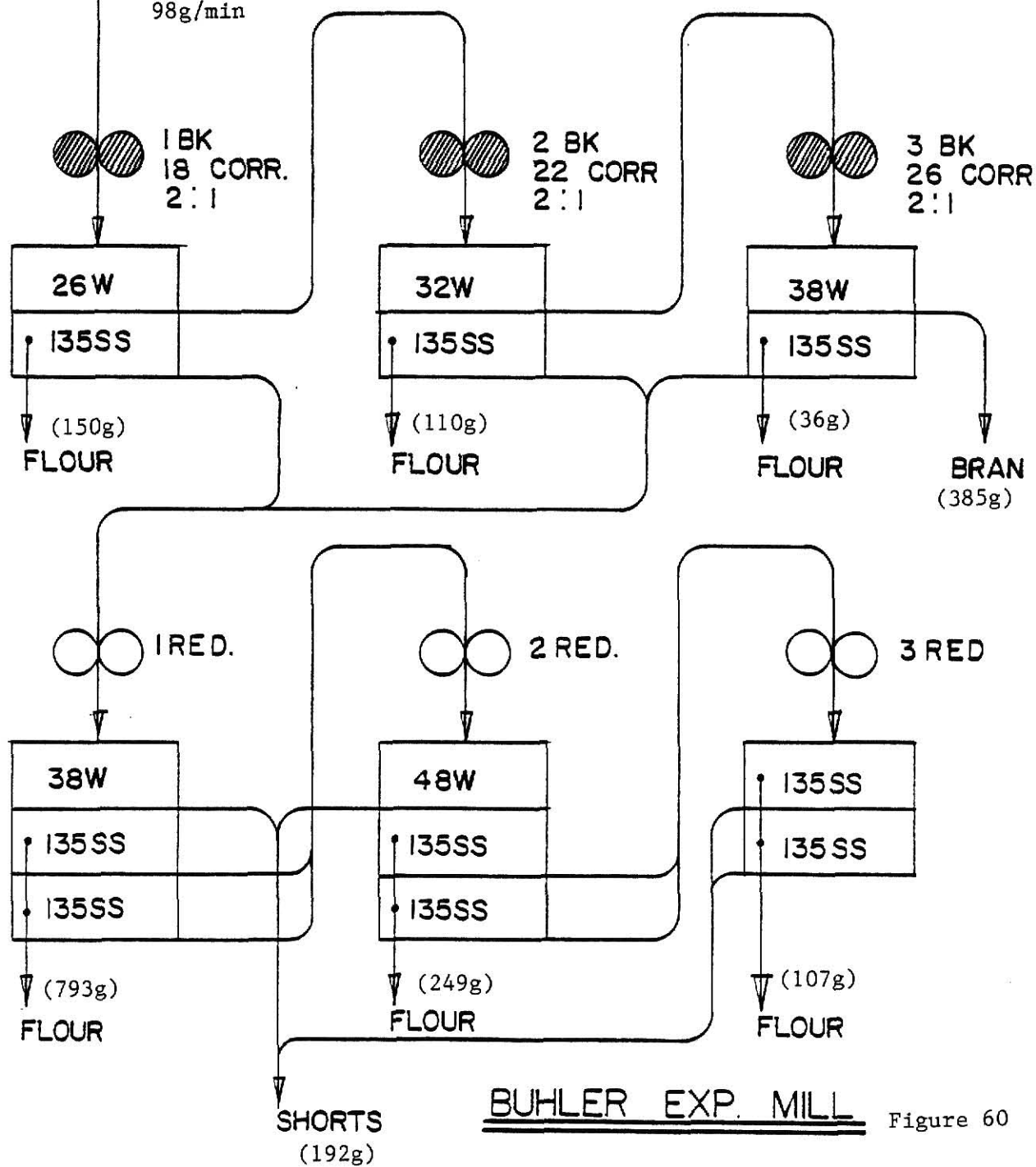
TEMPERED  
WHEATFeed Rate =  
98g/min

Figure 60



# PRE-BREAK (sifted)

115

TEST 1E-2

TEMPERED WHEAT

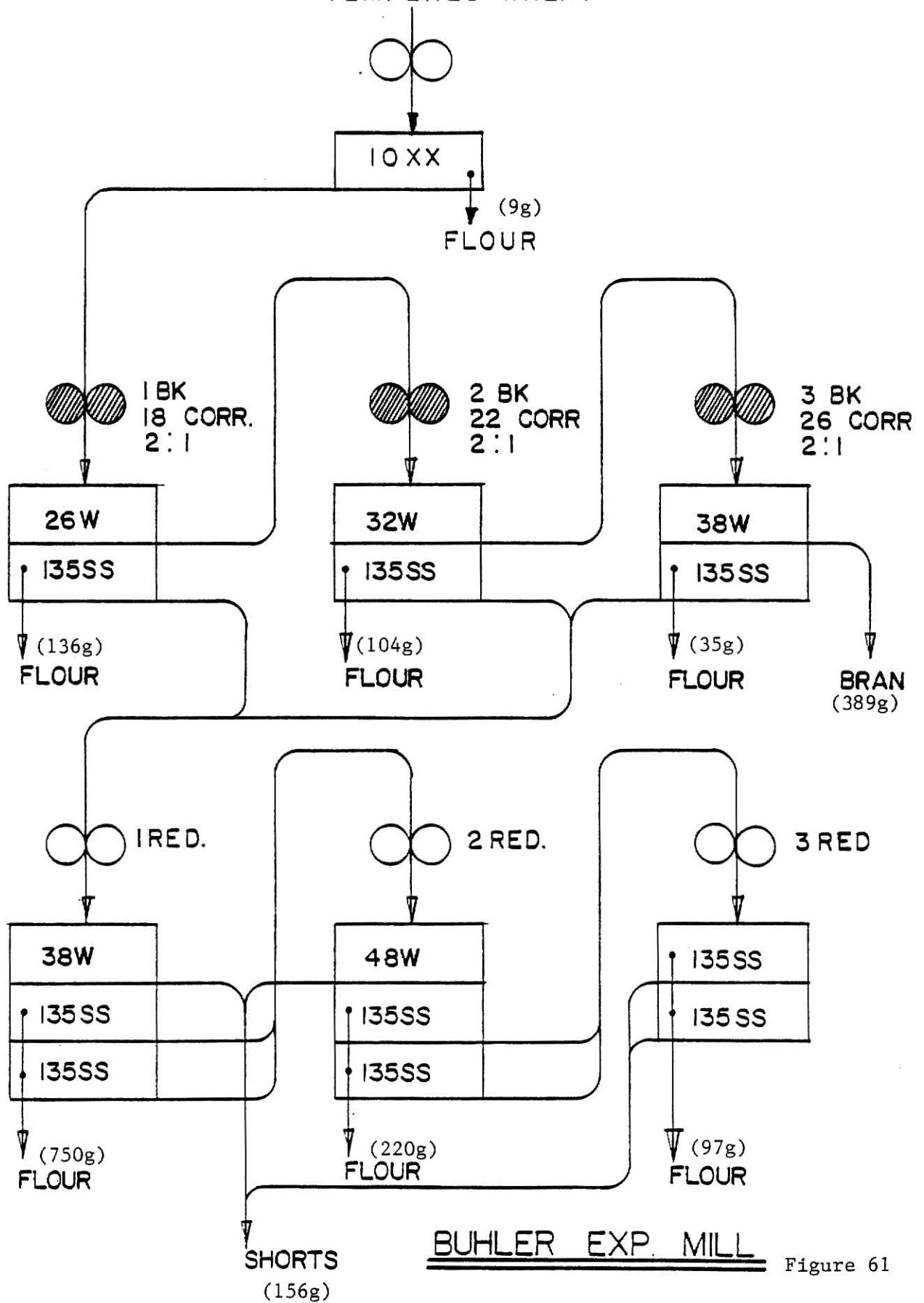


Figure 61

## Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)  
 Q=QUANTITY (% of Total Products)  
 S= SUMMATION

MILL BUHLER EXP.  
 TEST A  
 WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	Q X A	S of QXA	S of QXA S of Q
NO PRE-BREAK (1)							
1 RED	785	40.80	40.80	.338	13.790	13.790	.338
1 BK	157	8.16	48.96	.373	3.044	16.834	.344
2 BK	111	5.77	54.73	.377	2.175	19.009	.347
2 RED	198	10.29	65.02	.455	4.682	23.691	.364
3 BK	30	1.56	66.58	.569	0.888	24.579	.369
3 RED	100	5.20	71.78	.666	3.463	28.042	.391
PRE-BREAK (NOT SIFTED)							
1 RED	762	40.32	40.32	.315	12.701	12.701	.315
1 BK	165	8.73	49.05	.340	2.968	15.669	.319
2 BK	110	5.82	54.87	.358	2.084	17.753	.324
2 RED	192	10.16	65.03	.413	4.196	21.949	.338
3 BK	29	1.53	66.56	.523	0.800	22.749	.342
3 RED	99	5.24	71.80	.607	3.181	25.930	.361
PRE-BREAK (SIFTED)							
1 RED	764	38.53	38.53	.315	12.137	12.137	.315
1 BK	155	7.82	46.35	.340	2.659	14.796	.319
2 BK	115	5.80	52.15	.356	2.065	16.861	.323
2 RED	227	11.45	63.60	.399	4.569	21.429	.337
3 BK	31	1.56	65.16	.511	0.797	22.226	.341
P BK	10	0.50	65.66	.557	0.279	22.505	.343
3 RED	104	5.24	70.90	.573	3.003	25.507	.360
NO PRE-BREAK (2)							
1 RED	754	39.66	39.66	.342	13.564	13.564	.342
1 BK	151	7.94	47.60	.362	2.874	16.438	.345
2 BK	112	5.89	53.49	.365	2.150	18.588	.348
2 RED	213	11.20	64.69	.470	5.264	23.852	.369
3 BK	31	1.63	66.32	.545	0.888	24.740	.373
3 RED	102	5.37	71.70	.733	3.936	28.676	.400

## Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)  
 Q=QUANTITY (% of Total Products)  
 S= SUMMATION

MILL BUHLER EXP.  
 TEST B  
 WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	Q X A	S of QXA	$\frac{S \text{ of QXA}}{S \text{ of Q}}$
PRE-BREAK SIFTED (1)							
1 RED	740	38.70	38.70	.309	11.958	11.958	.309
1 BK	153	8.00	46.70	.328	2.624	14.582	.312
2 BK	108	5.65	52.35	.348	1.966	16.549	.316
2 RED	208	10.88	63.23	.377	4.102	20.650	.327
3 RED	113	5.91	69.14	.498	2.943	23.593	.341
3 BK	30	1.57	70.71	.530	0.832	24.426	.345
P BK	7	0.37	71.08	.547	0.202	24.628	.346
NO PRE-BREAK							
1 RED	703	36.37	36.37	.332	12.075	12.075	.332
1 BK	148	7.66	44.03	.349	2.673	14.748	.335
2 BK	109	5.64	49.67	.364	2.053	16.801	.338
2 RED	262	13.55	63.22	.408	5.526	22.330	.353
3 BK	29	1.50	64.72	.559	0.839	23.168	.358
3 RED	107	5.54	70.26	.580	3.213	26.381	.375
PRE-BREAK NOT SIFTED							
1 RED	723	37.42	37.42	.308	11.525	11.525	.308
1 BK	160	8.28	45.70	.330	2.732	14.258	.312
2 BK	112	5.80	51.50	.348	2.018	16.276	.316
2 RED	226	11.70	63.20	.382	4.469	20.746	.328
3 RED	113	5.85	69.05	.526	3.077	23.823	.345
3 BK	31	1.60	70.65	.529	0.846	24.669	.349
PRE-BREAK SIFTED (2)							
1 RED	730	38.69	38.69	.314	12.149	12.149	.314
1 BK	145	7.68	46.37	.317	2.435	14.583	.314
2 BK	111	5.88	52.25	.339	1.993	16.577	.317
2 RED	214	11.34	63.59	.403	4.570	21.147	.333
3 BK	32	1.70	65.29	.520	.884	22.031	.337
P BK	9	0.48	65.77	.547	.263	22.293	.339
3 RED	106	5.62	71.39	.602	3.383	25.676	.360

## Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)  
 Q=QUANTITY (% of Total Products)  
 S= SUMMATION

MILL BUHLER EXP.  
 TEST C  
 WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	Q X A	S of QXA	S of QXA S of Q
PRE-BREAK NOT SIFTED (1)							
1 RED	790	40.33	40.33	.306	12.341	12.341	.306
1 BK	162	8.27	48.60	.336	2.779	15.120	.311
2 BK	115	5.87	54.47	.354	2.078	17.198	.316
2 RED	201	10.26	64.73	.401	4.114	21.312	.329
3 BK	35	1.79	66.52	.525	0.940	22.252	.335
3 RED	107	5.46	71.98	.547	2.987	25.238	.351
PRE-BREAK SIFTED							
1 RED	749	39.34	39.34	.306	12.038	12.038	.306
1 BK	147	7.72	47.06	.325	2.509	14.547	.309
2 BK	115	6.04	53.10	.344	2.078	16.625	.313
2 RED	212	11.13	64.23	.383	4.263	20.888	.325
3 BK	32	1.68	65.91	.516	0.867	21.754	.330
P BK	7	0.37	66.28	.528	0.195	21.950	.331
3 RED	101	5.30	71.58	.557	2.952	24.902	.348
NO PRE-BREAK							
1 RED	754	38.49	38.49	.332	12.779	12.779	.332
1 BK	152	7.76	46.25	.347	2.693	15.471	.335
2 BK	117	5.97	52.22	.359	2.143	17.615	.337
2 RED	245	12.51	64.73	.433	5.417	23.031	.356
3 BK	33	1.68	66.41	.535	0.899	23.930	.360
3 RED	103	5.26	71.67	.656	3.451	27.381	.382
PRE-BREAK NOT SIFTED (2)							
1 RED	772	39.90	39.90	.312	12.449	12.449	.312
1 BK	156	8.06	47.96	.329	2.652	15.101	.315
2 BK	115	5.94	53.90	.353	2.097	17.197	.319
2 RED	212	10.96	64.86	.424	4.647	21.844	.337
3 BK	35	1.81	66.67	.526	0.952	22.796	.342
3 RED	99	5.12	71.79	.616	3.154	25.950	.361

## Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)  
 Q=QUANTITY (% of Total Products)  
 S= SUMMATION

MILL BUHLER EXP.  
 TEST D  
 WHEAT HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	Q X A	S of QXA	S of QXA S of Q
NO PRE-BREAK (1)							
1 RED	752	38.68	38.68	.331	12.803	12.803	.331
1 BK	151	7.77	46.45	.352	2.735	15.538	.335
2 BK	115	5.92	52.37	.366	2.167	17.705	.338
2 RED	236	12.14	64.51	.425	5.160	22.864	.354
3 BK	33	1.70	66.21	.538	0.915	23.779	.359
3 RED	101	5.20	71.41	.615	3.198	26.977	.378
PRE-BREAK SIFTED							
1 RED	777	39.83	39.83	.322	12.825	12.825	.322
1 BK	145	7.43	47.26	.326	2.422	15.247	.323
2 BK	114	5.84	53.10	.359	2.097	17.344	.327
2 RED	214	10.97	64.07	.423	4.640	21.984	.343
3 BK	36	1.85	65.92	.531	0.982	22.967	.348
P BK	9	0.46	66.38	.540	0.248	23.215	.350
3 RED	105	5.38	71.76	.601	3.233	26.448	.369
PRE-BREAK NOT SIFTED							
1 RED	746	39.43	39.43	.326	12.854	12.854	.326
1 BK	156	8.25	47.68	.340	2.805	15.659	.328
2 BK	118	6.24	53.92	.365	2.278	17.937	.333
2 RED	215	11.36	65.28	.430	4.885	22.822	.350
3 BK	34	1.80	67.08	.536	0.965	23.786	.355
3 RED	96	5.07	72.15	.642	3.255	27.041	.375
NO PRE-BREAK (2)							
1 RED	732	37.67	37.67	.330	12.431	12.431	.330
1 BK	148	7.62	45.29	.352	2.682	15.113	.334
2 BK	117	6.02	51.31	.361	2.173	17.287	.337
2 RED	257	13.23	64.54	.432	5.715	23.002	.356
3 BK	34	1.75	66.29	.541	0.947	23.949	.361
2 RED	97	4.99	71.28	.684	3.413	27.362	.384



## Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)  
 Q=QUANTITY (% of Total Products)  
 S= SUMMATION

MILL \_\_\_\_\_  
 TEST \_\_\_\_\_  
 WHEAT \_\_\_\_\_

BUHLER EXP.  
 E  
 HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	Q X A	S of QXA	S of QXA S of Q
PRE-BREAK SIFTED (1)							
1 RED	712	38.97	38.97	.302	11.769	11.769	.302
1 BK	143	7.83	46.80	.327	2.560	14.329	.306
2 BK	103	5.64	52.44	.345	1.946	16.275	.310
2 RED	211	11.55	63.99	.359	4.146	20.422	.319
3 RED	100	5.47	69.46	.479	2.620	23.042	.332
3 BK	29	1.59	71.05	.509	0.809	23.851	.336
P BK	9	0.49	71.54	.541	0.265	24.116	.337
PRE-BREAK NOT SIFTED							
1 RED	728	38.32	38.32	.304	11.649	11.649	.304
1 BK	151	7.95	46.27	.330	2.624	14.273	.308
2 BK	105	5.53	51.80	.351	1.941	16.214	.313
2 RED	236	12.42	64.22	.374	4.645	20.359	.325
3 BK	33	1.74	65.96	.512	0.891	21.750	.330
3 RED	99	5.21	71.17	.521	2.714	24.464	.344
NO PRE-BREAK							
1 RED	793	39.22	39.22	.326	12.786	12.786	.326
1 BK	150	7.42	46.64	.363	2.693	15.479	.332
2 BK	110	5.44	52.08	.373	2.029	17.508	.336
2 RED	249	12.31	64.39	.425	5.232	22.740	.353
3 BK	36	1.78	66.17	.532	0.947	23.687	.358
3 RED	107	5.29	71.46	.618	3.269	26.956	.377
PRE-BREAK SIFTED (2)							
1 RED	750	39.56	39.56	.311	12.303	12.303	.311
1 BK	136	7.17	46.73	.324	2.323	14.626	.313
2 BK	104	5.49	52.22	.345	1.894	16.520	.316
2 RED	220	11.60	63.82	.390	4.524	21.044	.330
3 BK	35	1.85	65.67	.513	0.949	21.993	.335
3 RED	97	5.12	70.79	.558	2.857	24.850	.351
P BK	9	0.47	71.26	.588	0.276	25.127	.353

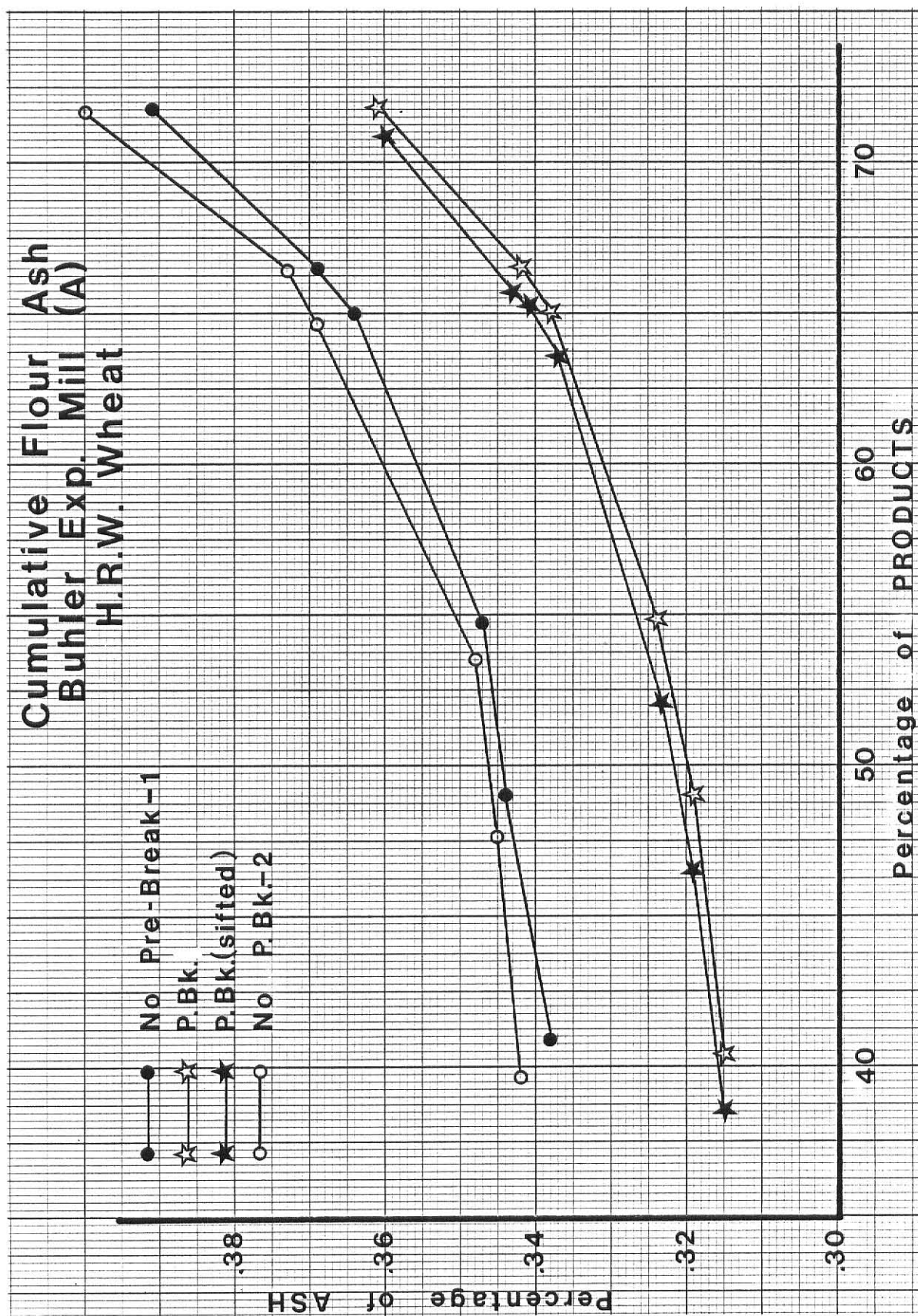


Figure 62

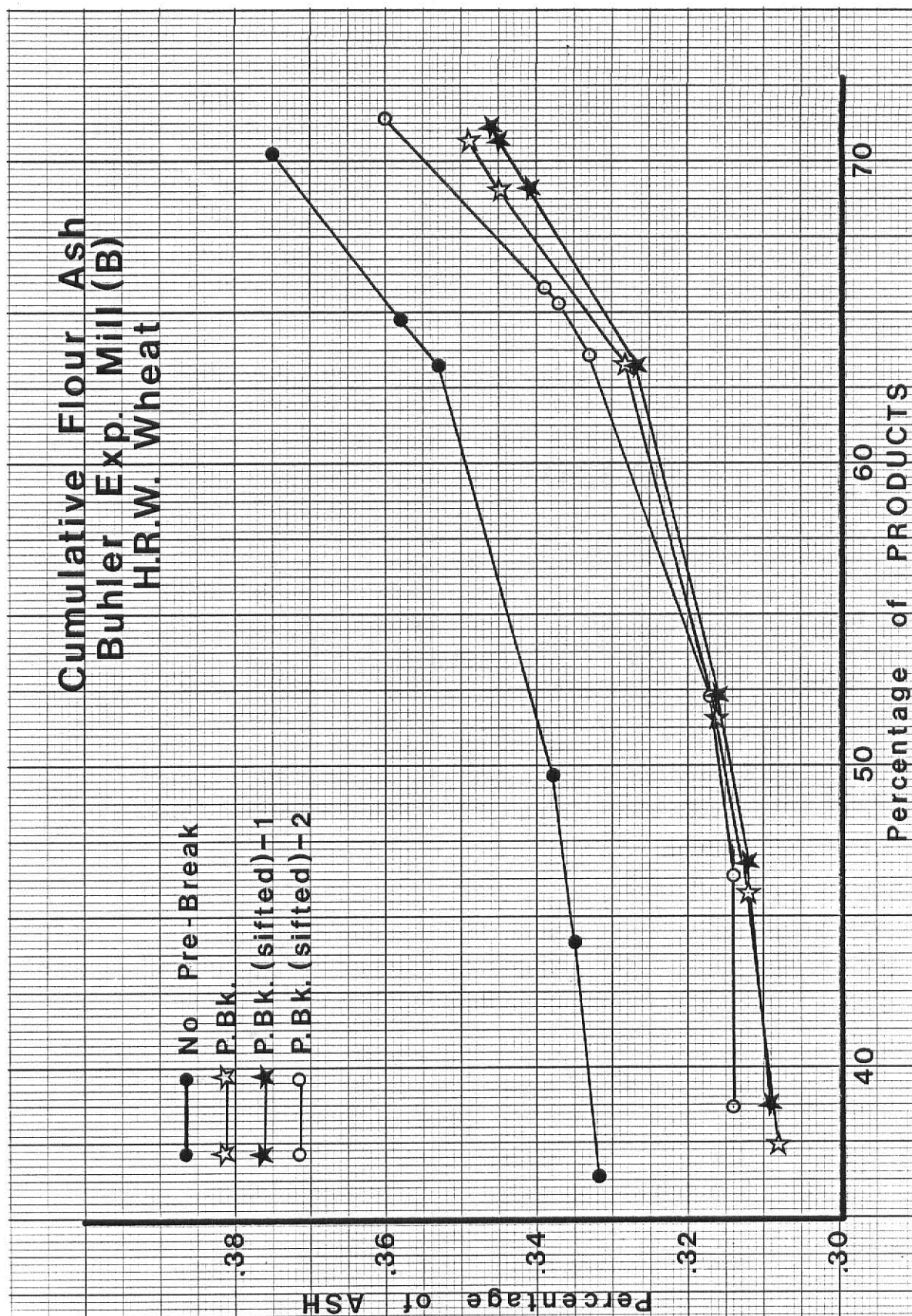


Figure 63



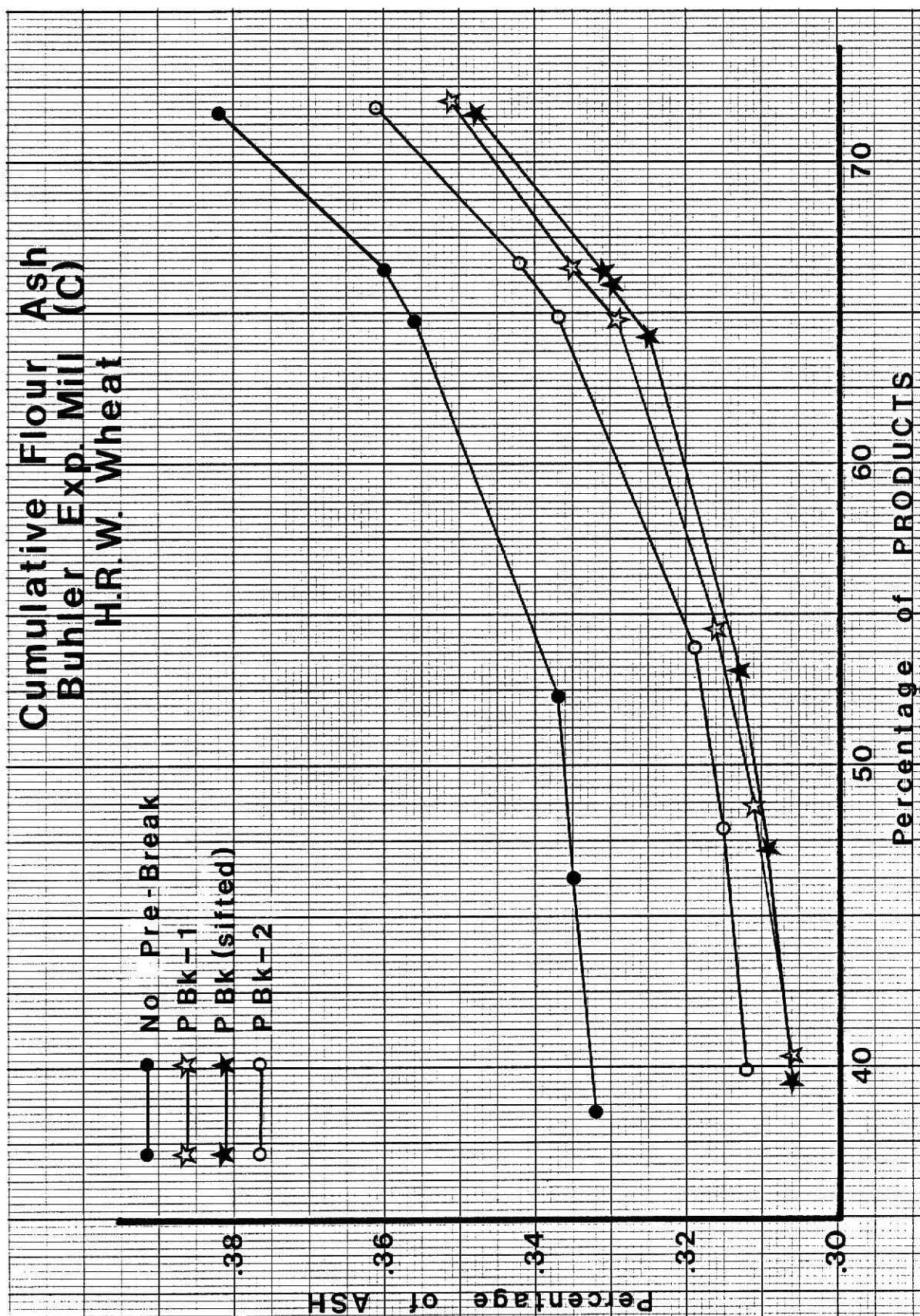


Figure 64

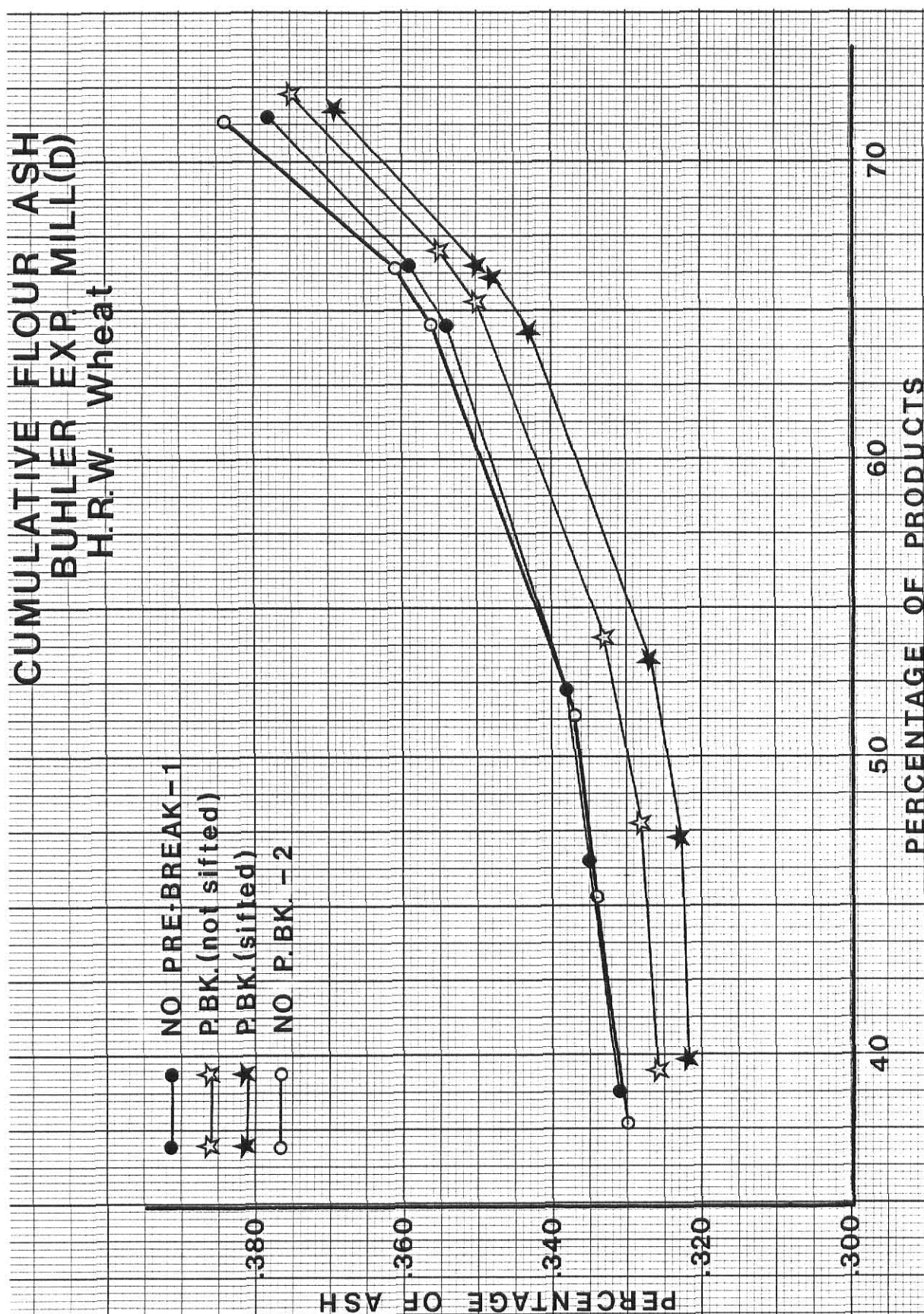


Figure 65

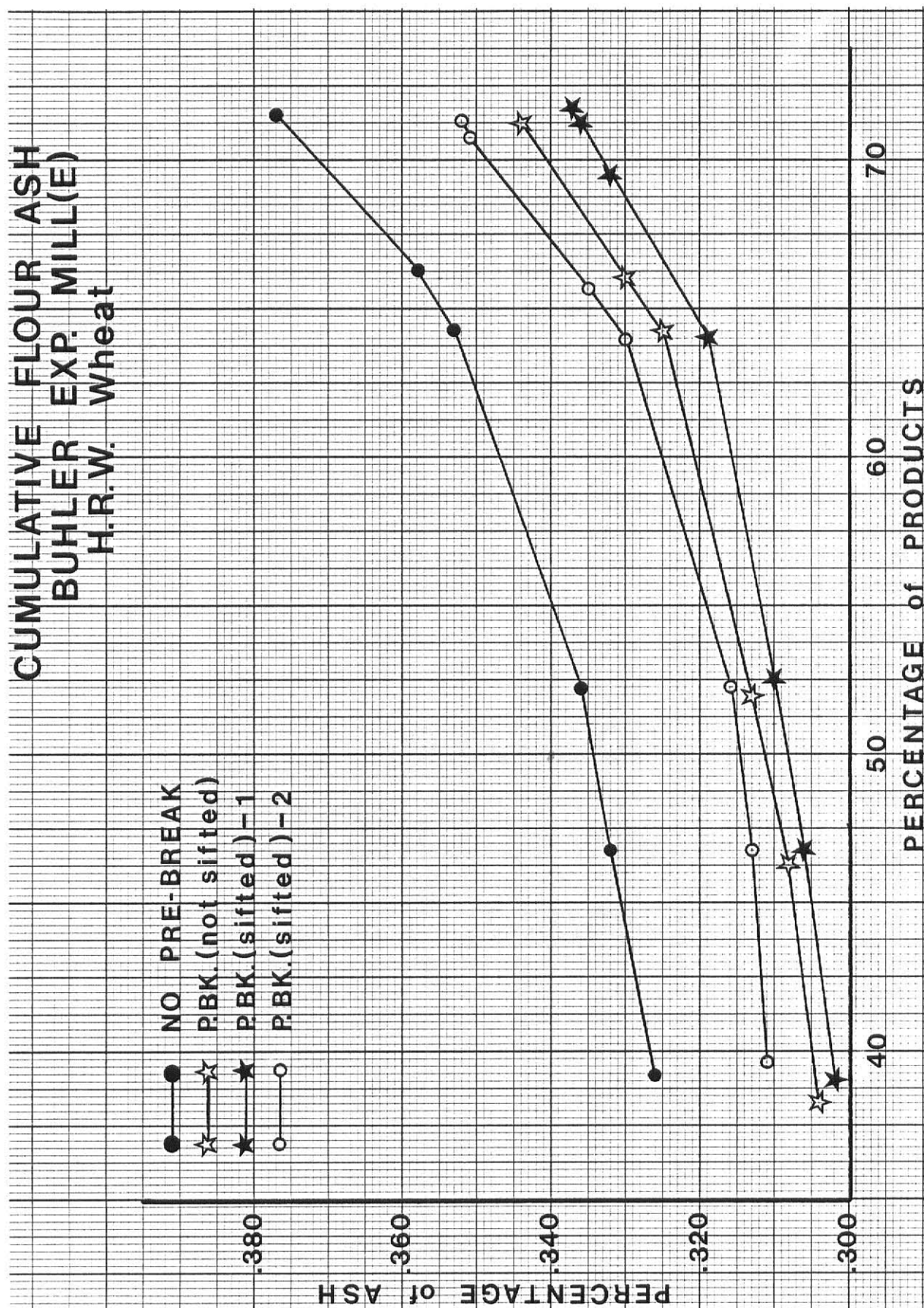
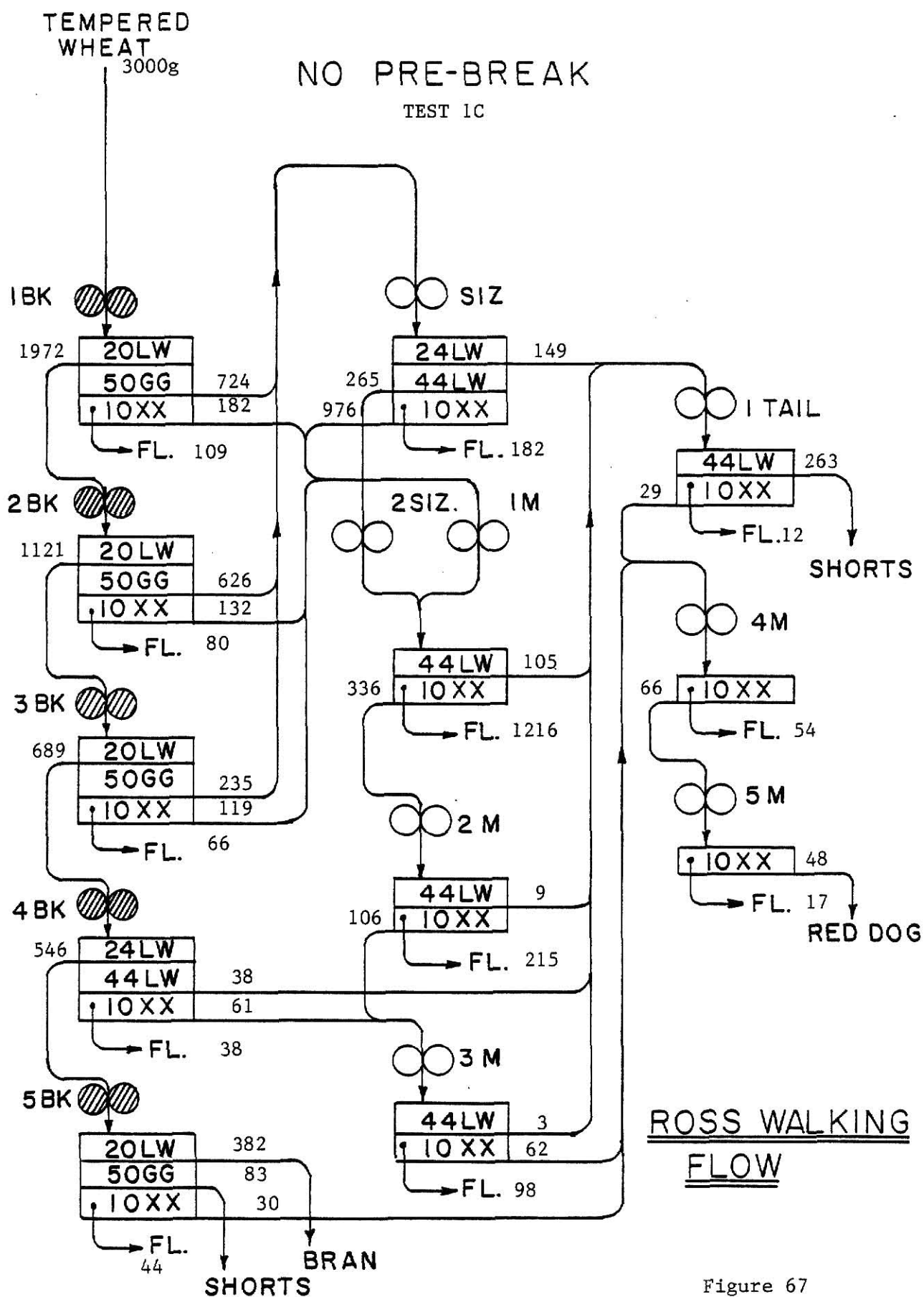


Figure 66





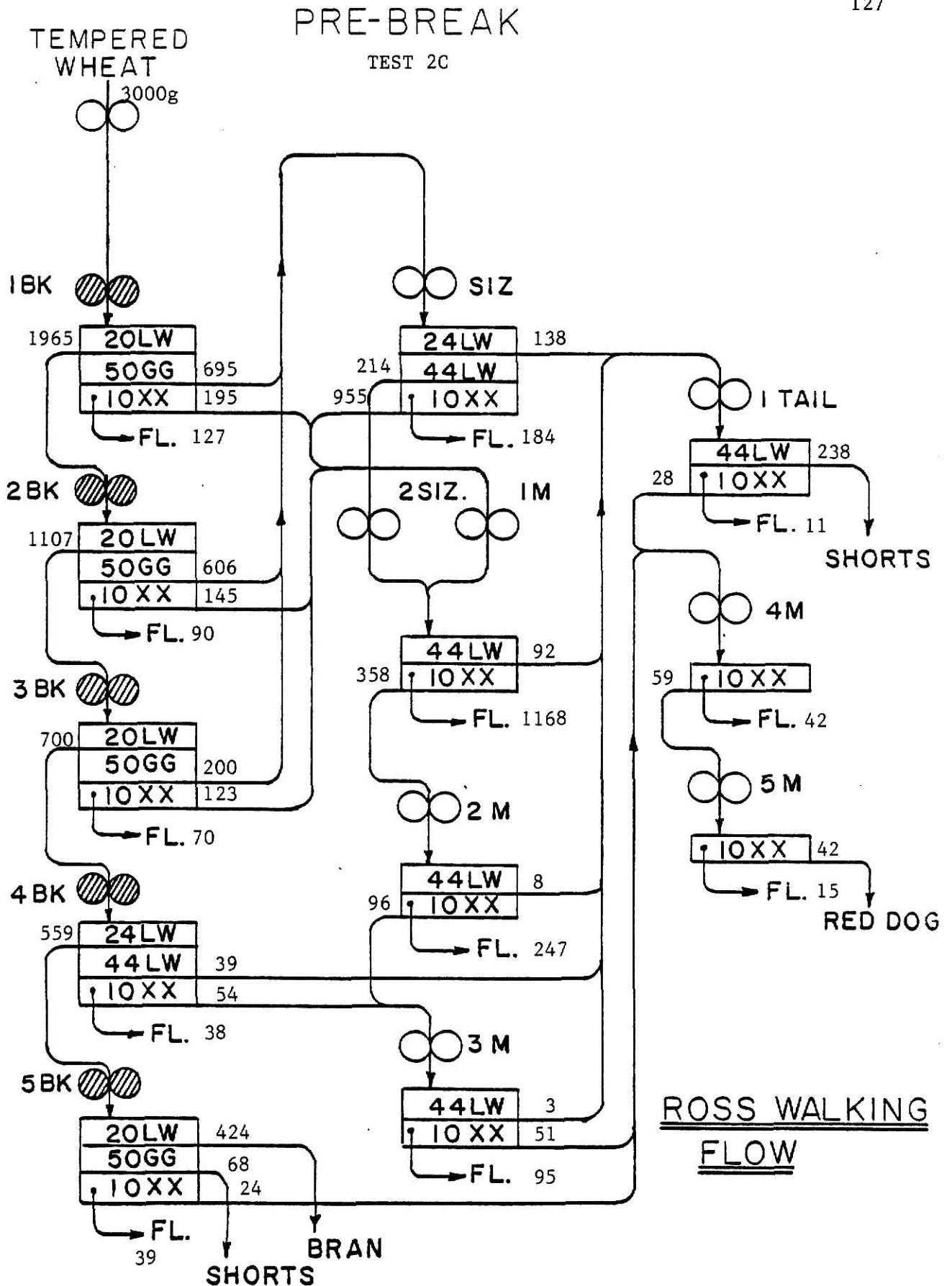


Figure 68

TEMPERED  
WHEAT

3000g

## PRE-BREAK (sifted)

TEST 3C

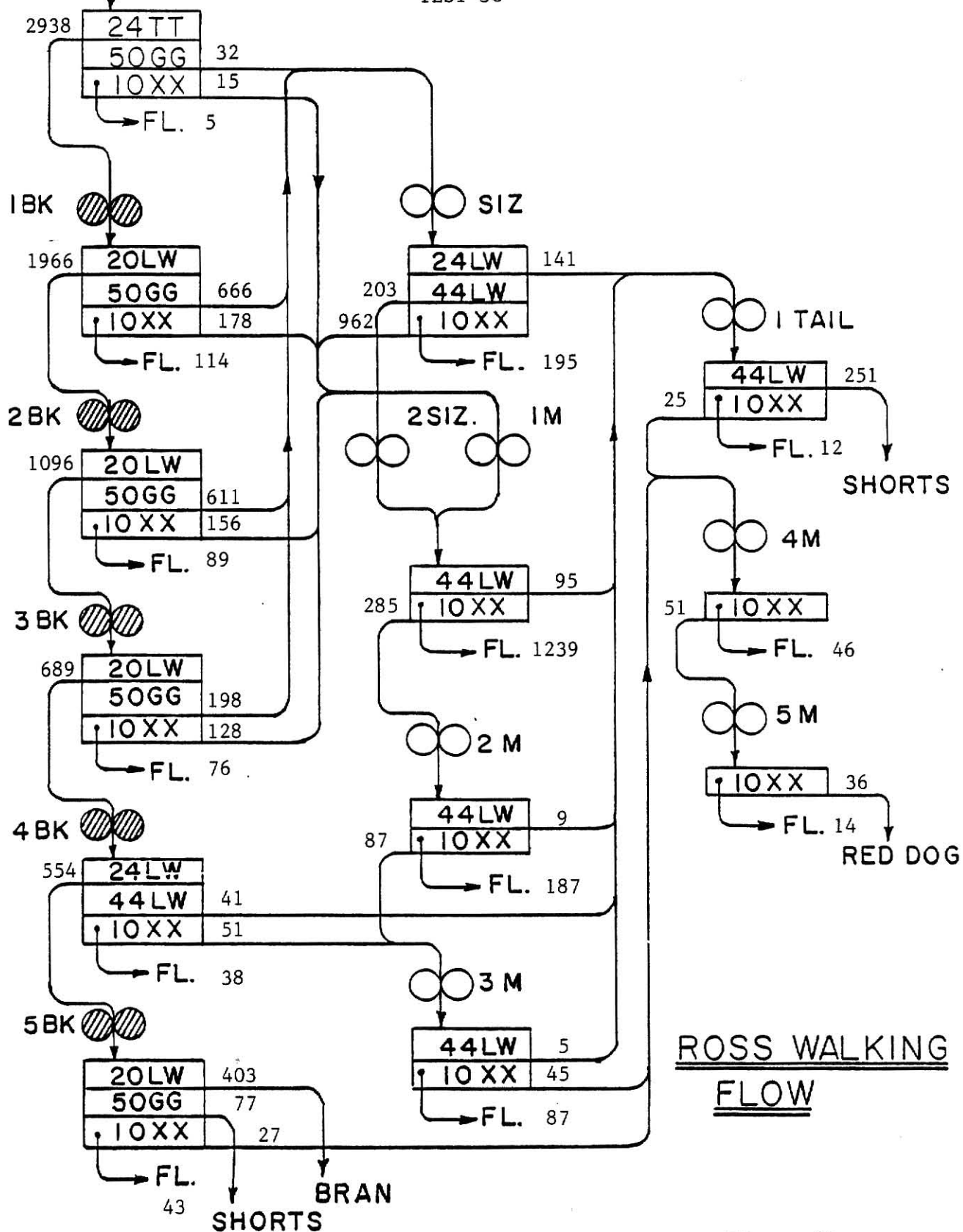


Figure 69

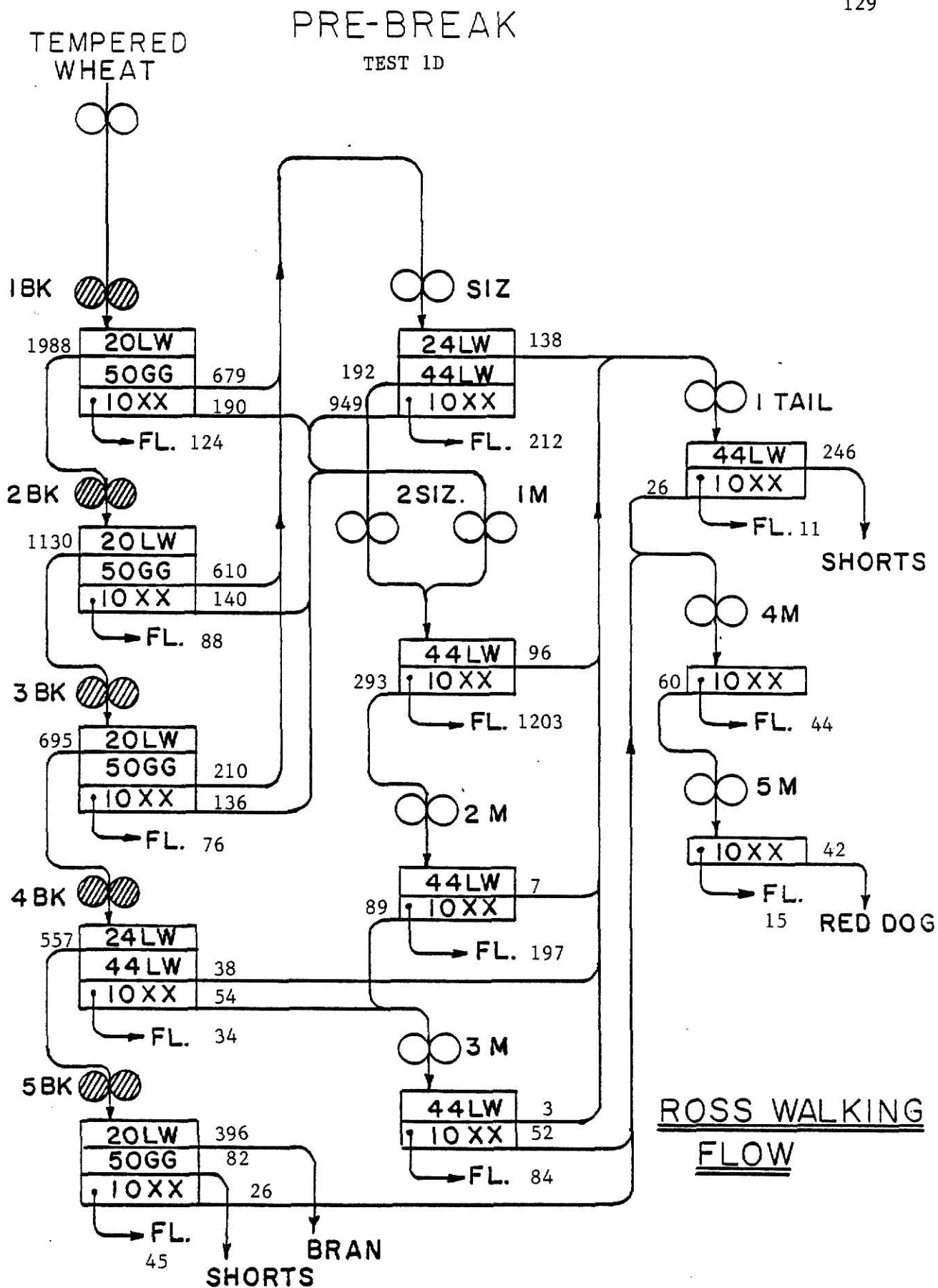


Figure 70

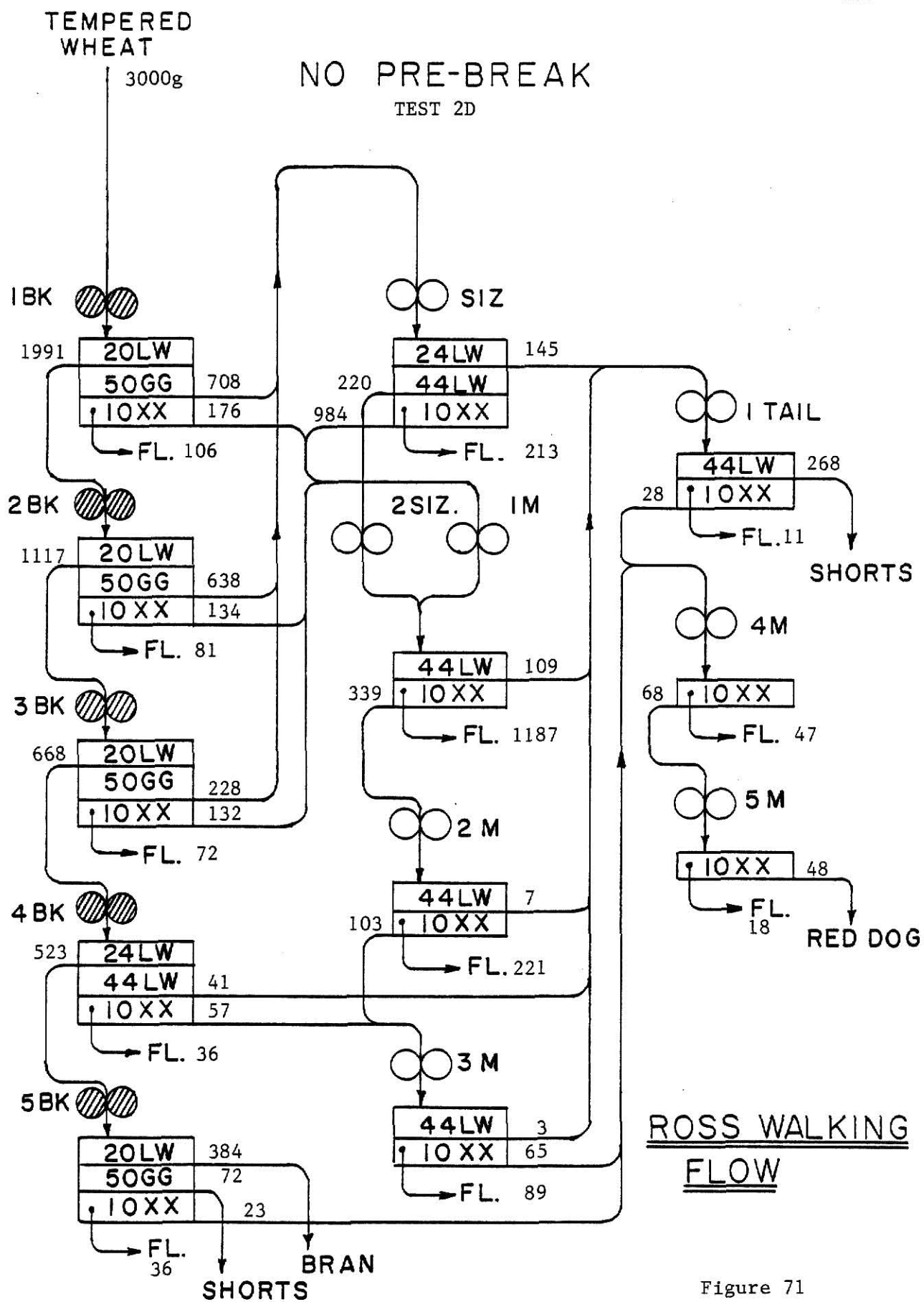


Figure 71



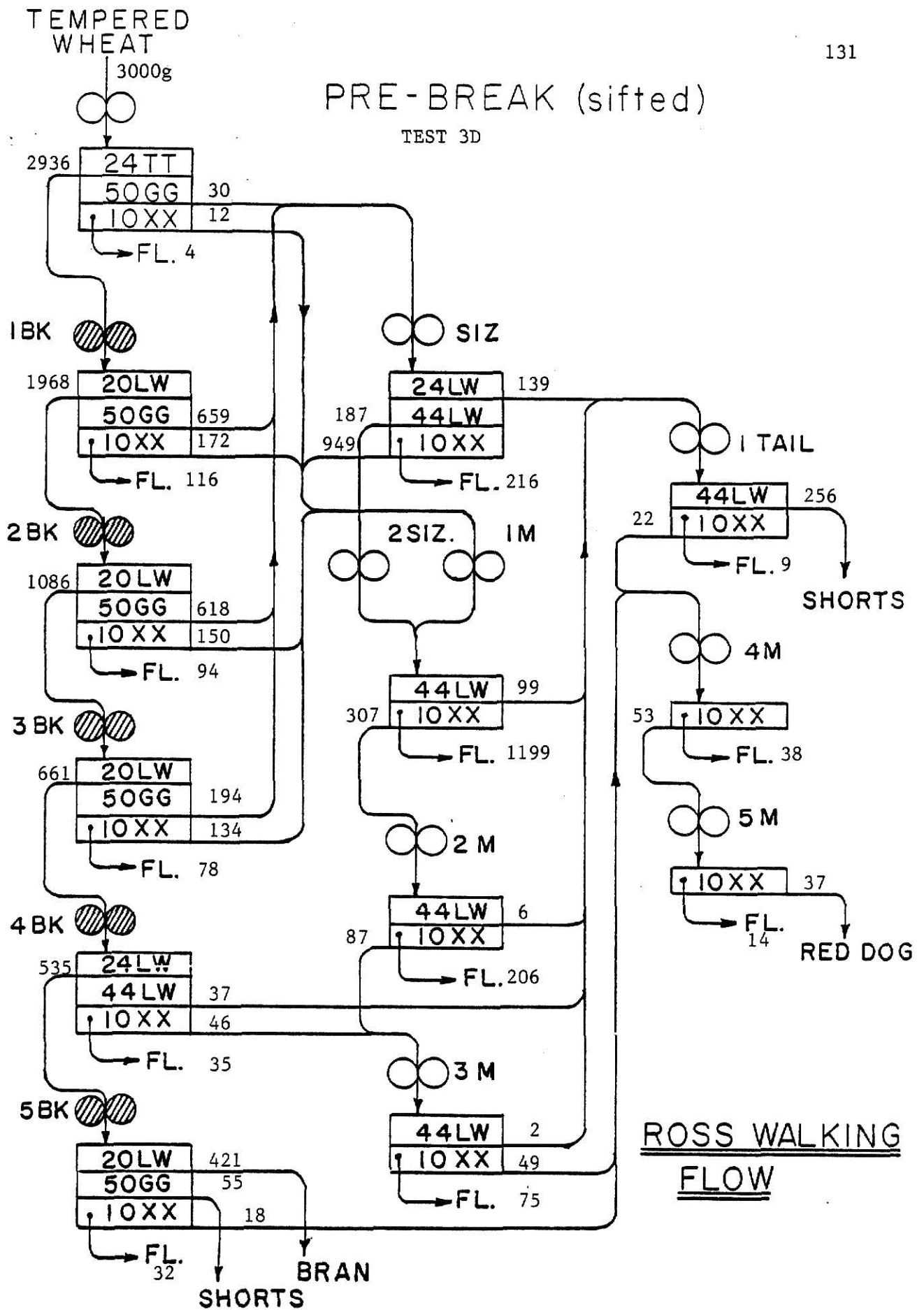


Figure 72

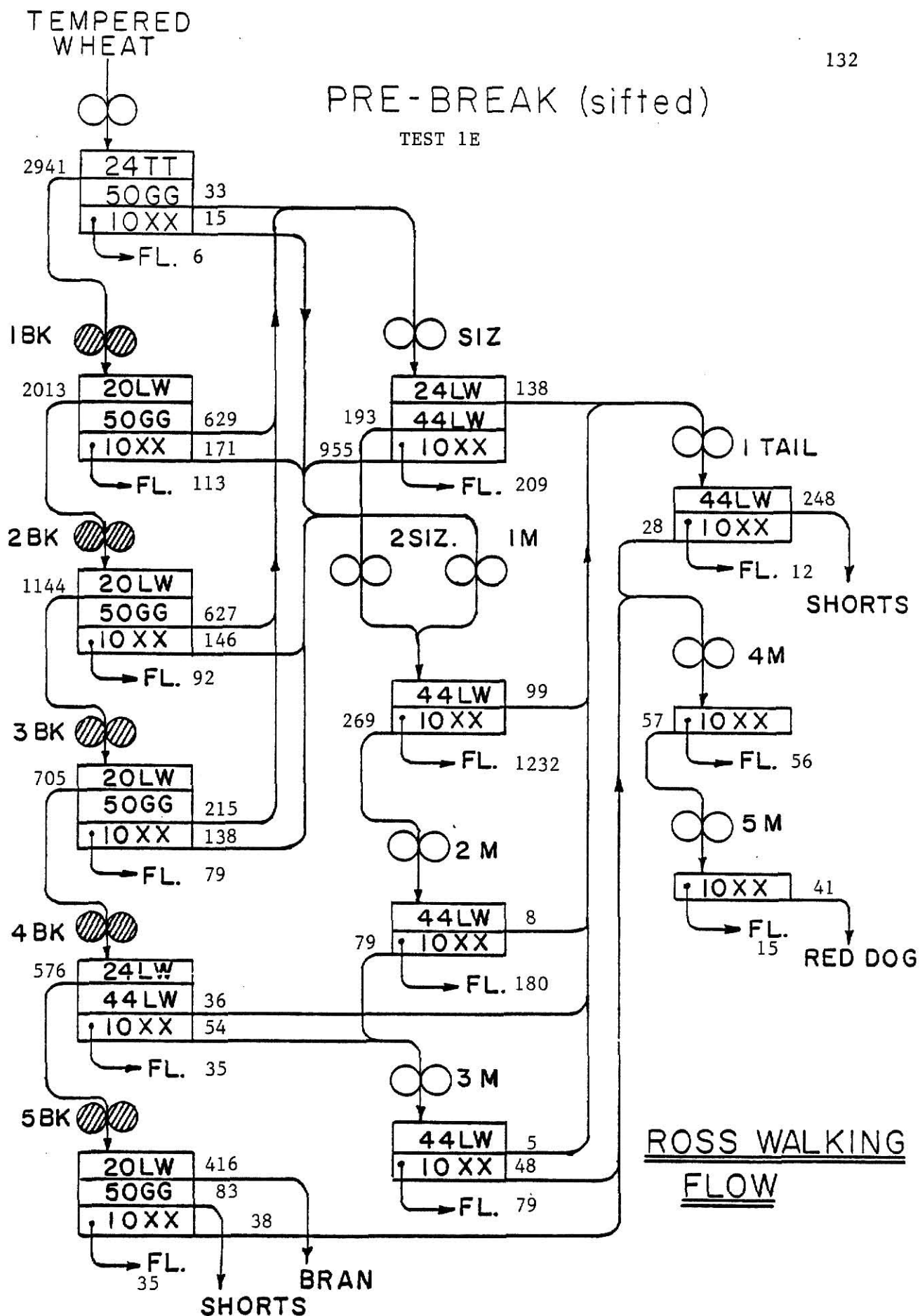


Figure 73

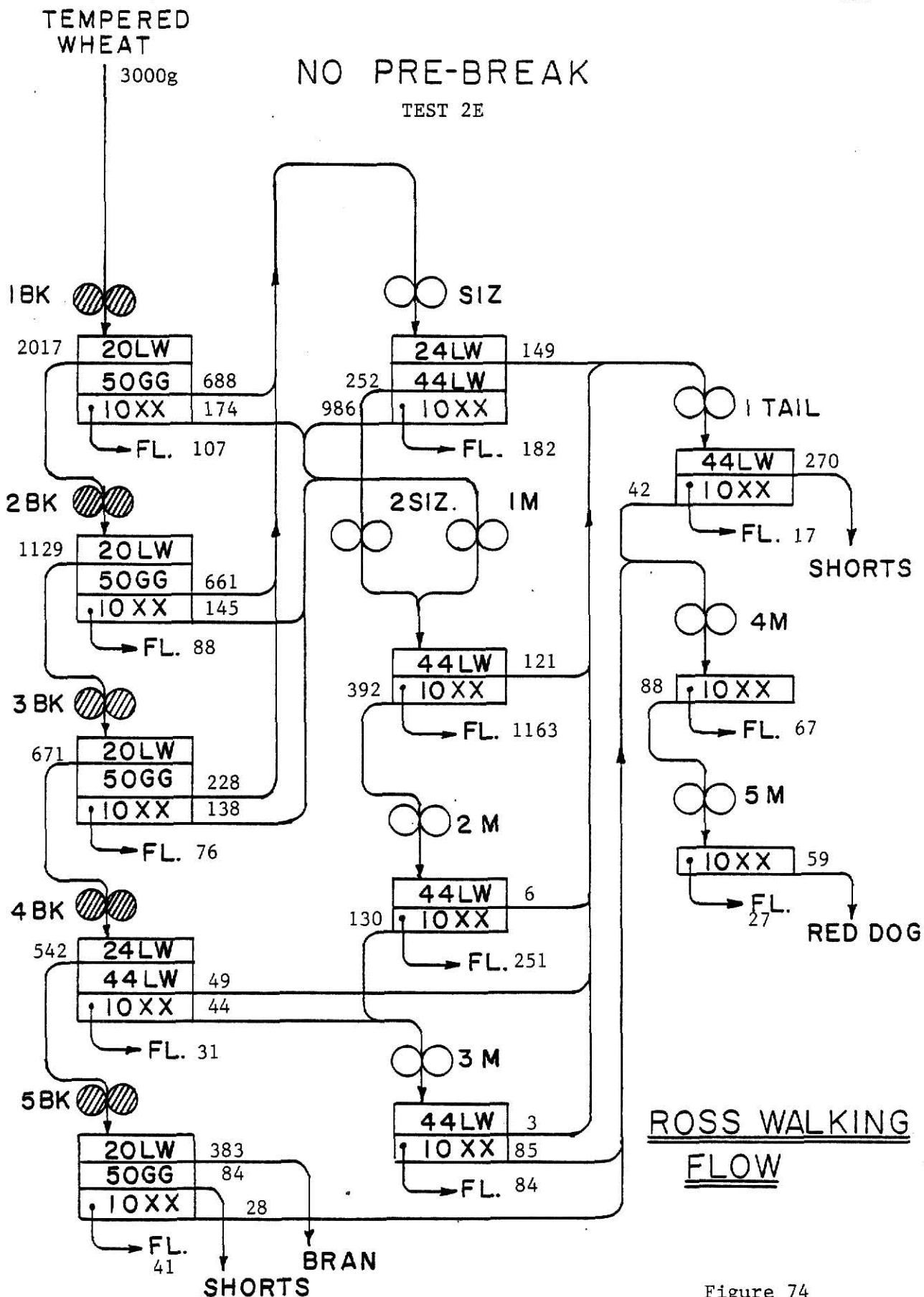


Figure 74

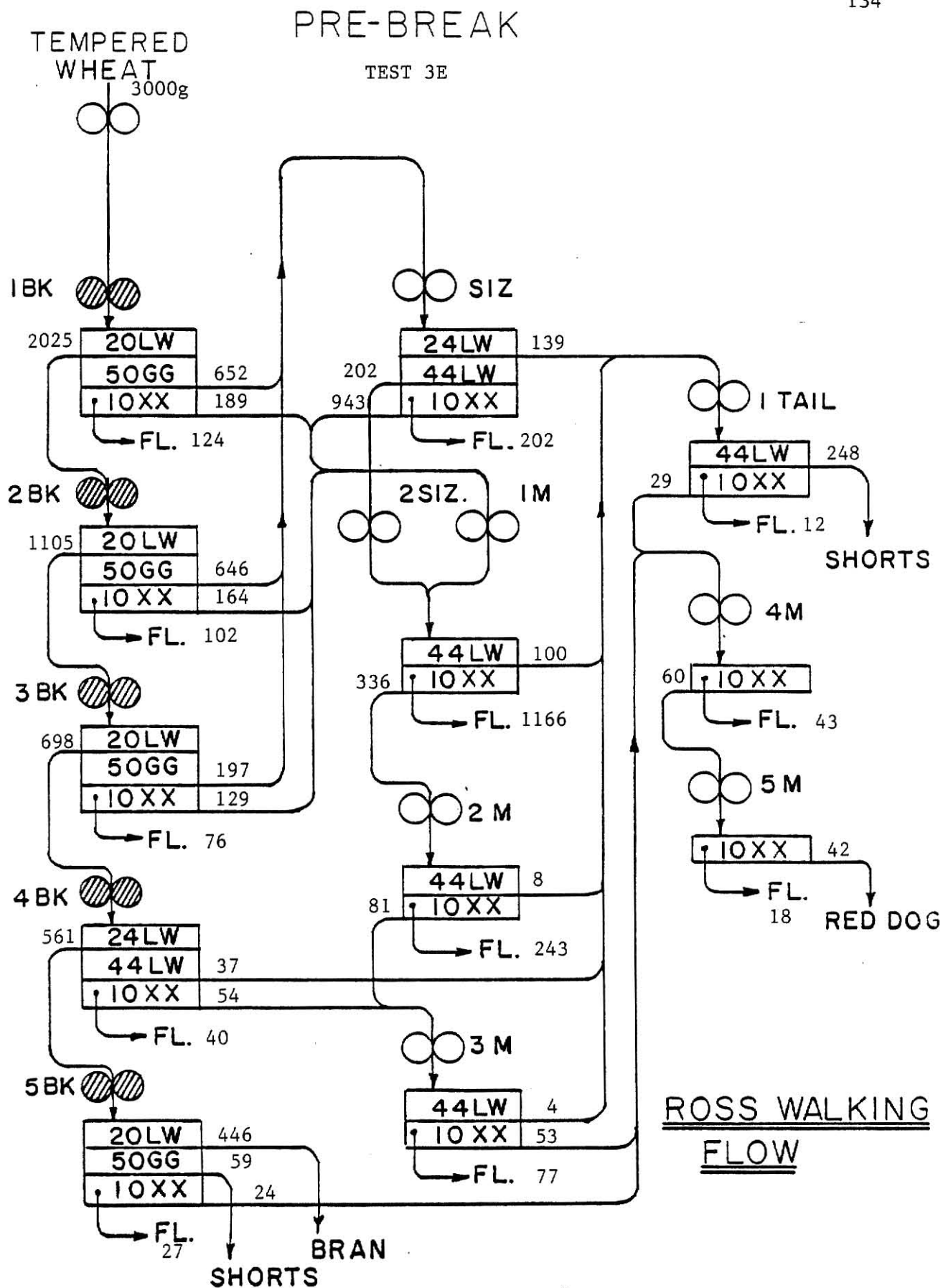


Figure 75

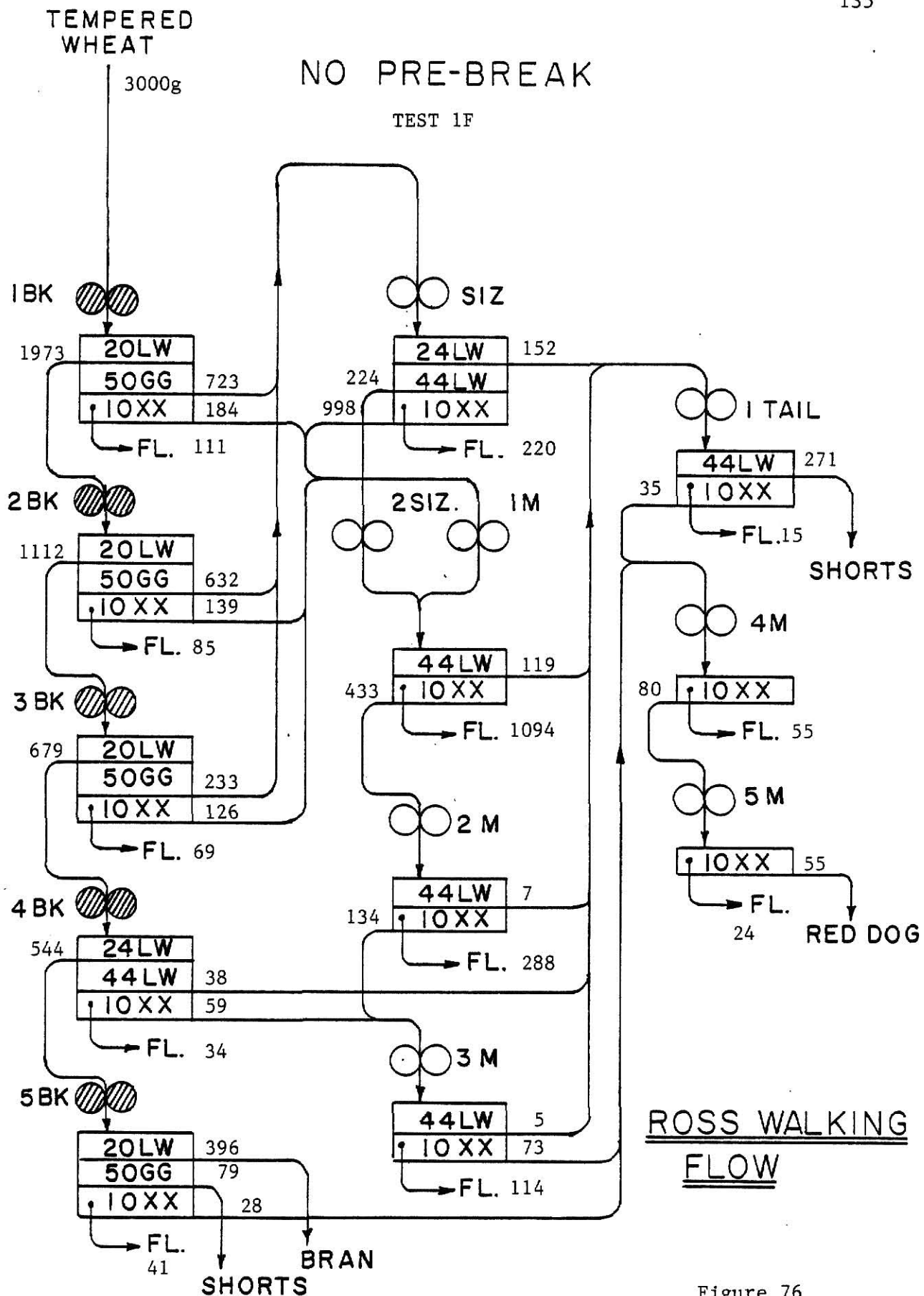


Figure 76

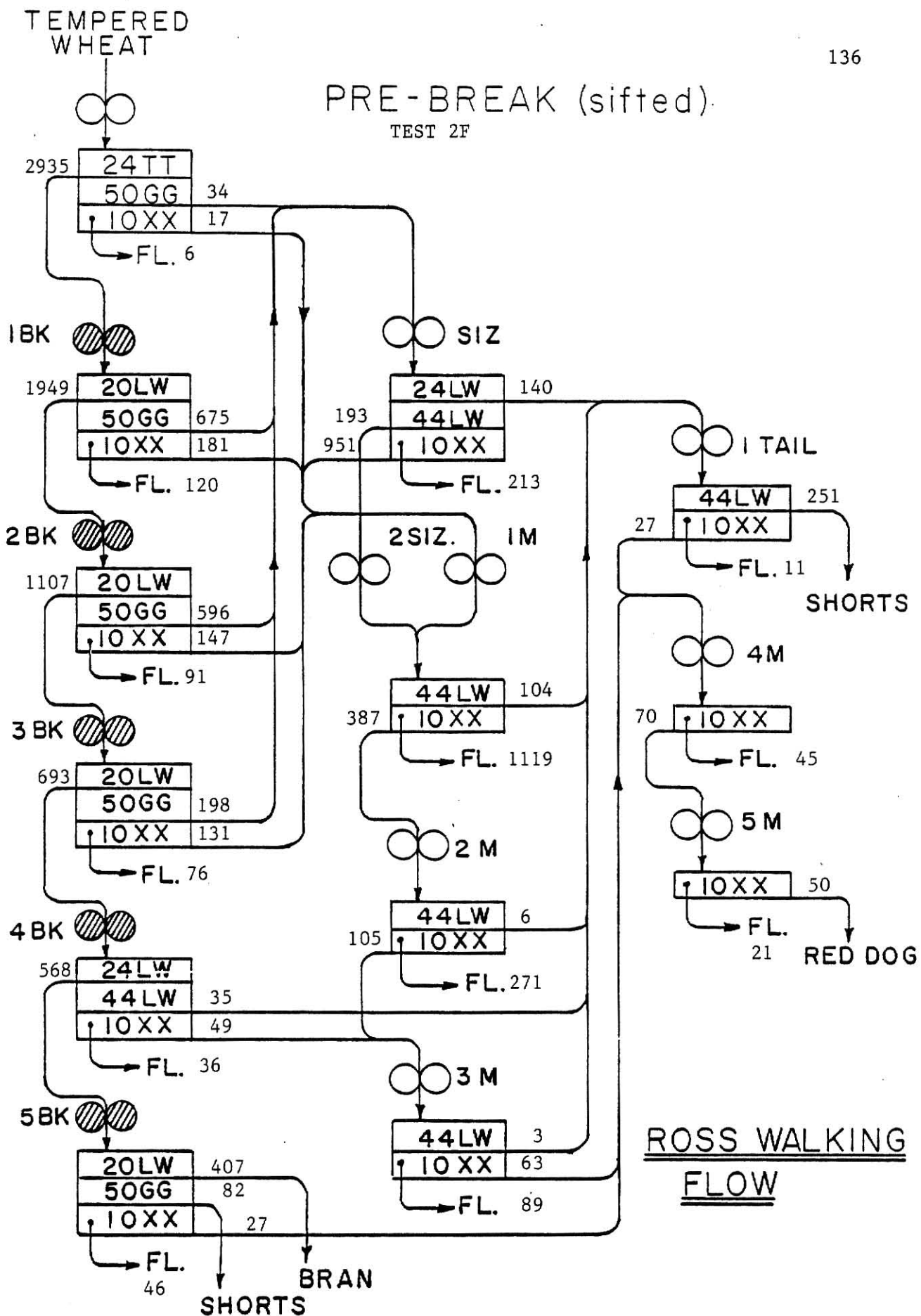


Figure 77

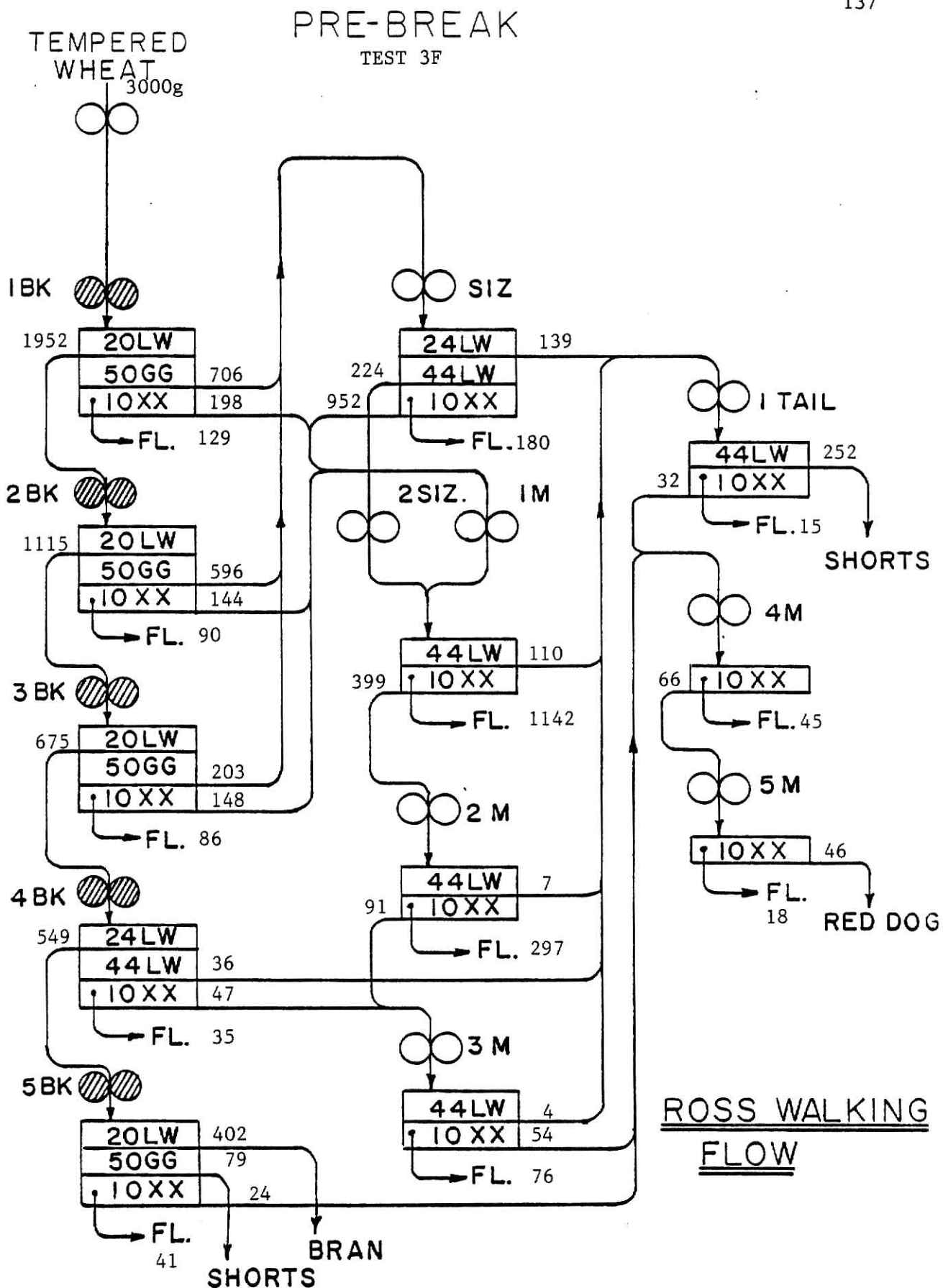


Figure 78



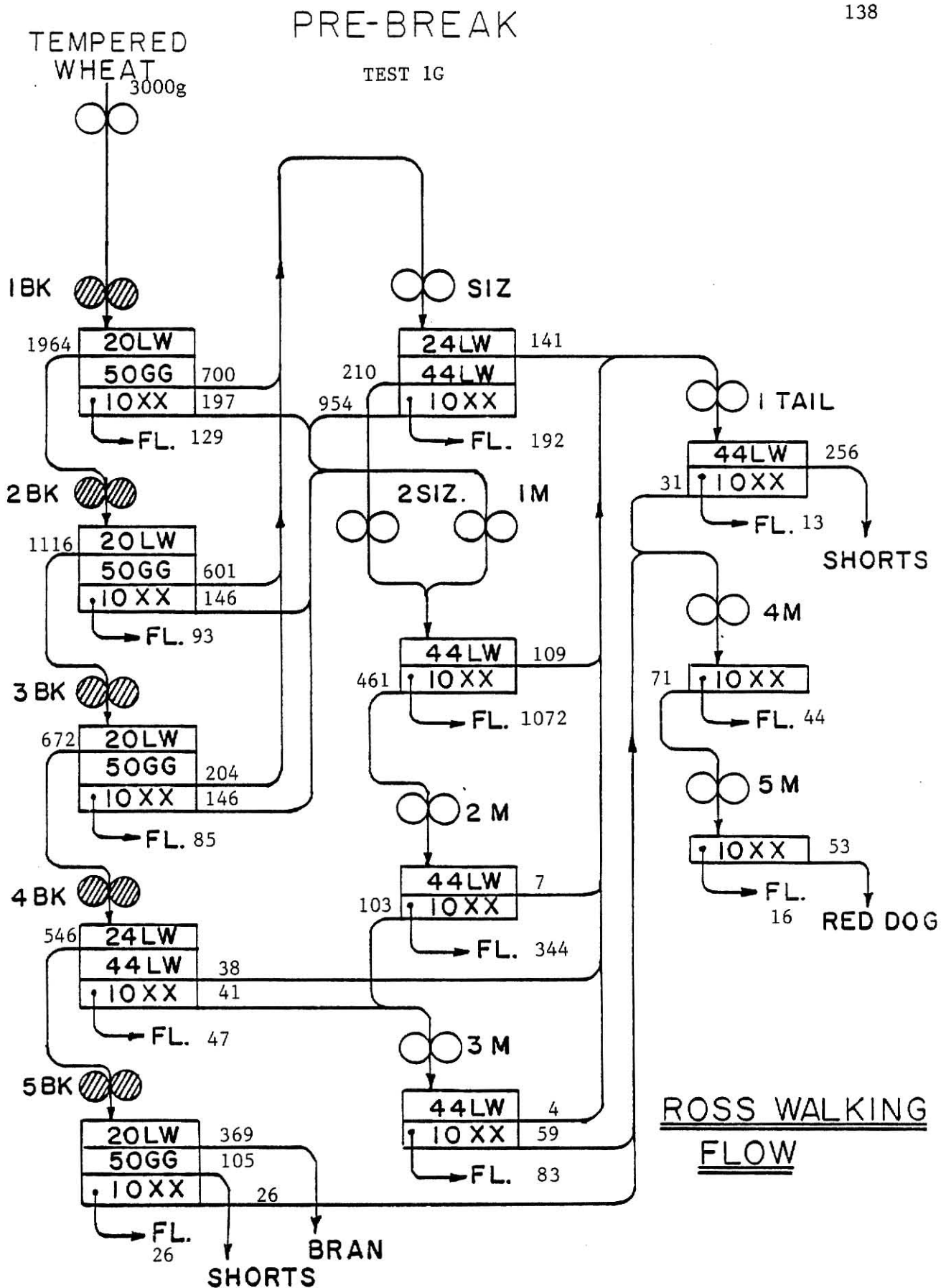


Figure 79

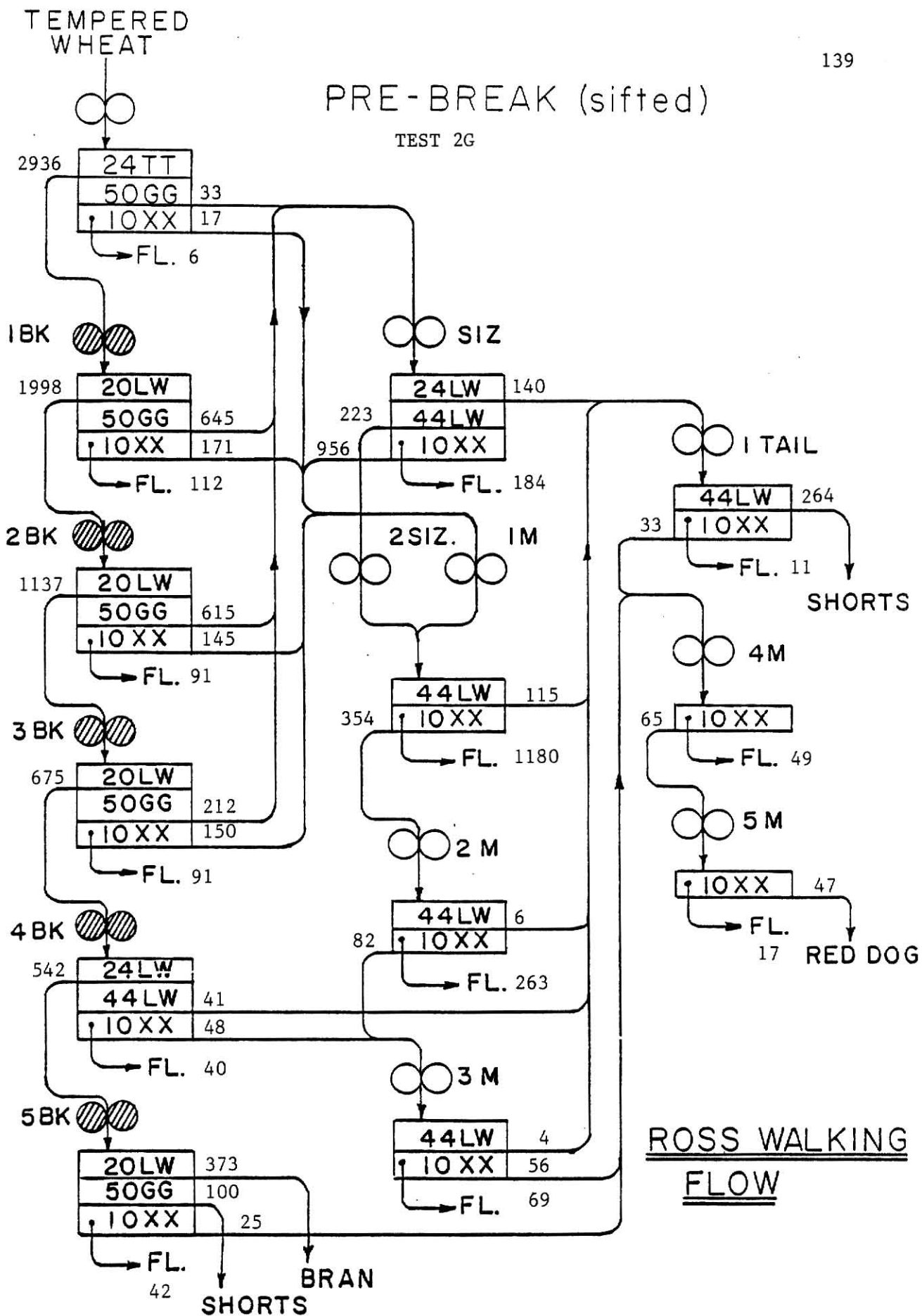


Figure 80

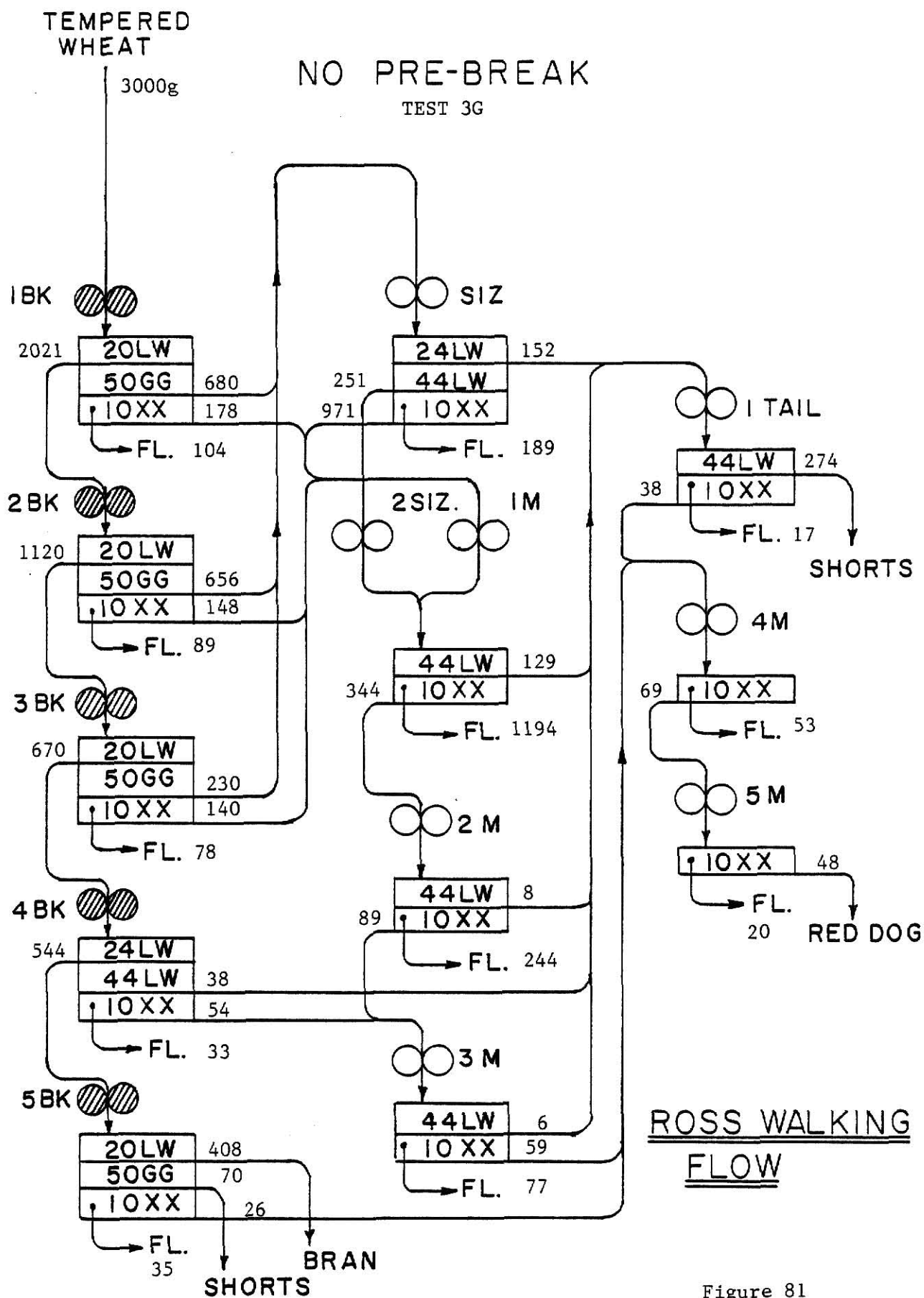


Figure 81



MILL	ROSS FLOW
TEST	D
WHEAT	HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	Q X A	S of QXA	S of QXA S of Q
PRE-BREAK NOT SIFTED							
1 M	1203	41.89	41.89	.274	11.748	11.748	.274
2 M	197	6.86	48.75	.296	2.031	13.508	.277
SIZ	212	7.38	56.13	.300	2.214	15.722	.280
3 BK	76	2.65	58.78	.369	0.978	16.700	.284
2 BK	88	3.06	61.84	.388	1.187	17.888	.289
3 M	84	2.92	64.76	.392	1.145	19.032	.294
1 BK	124	4.32	69.08	.422	1.823	20.855	.302
4 BK	34	1.18	70.26	.432	0.510	21.365	.304
1 TA	11	0.38	70.64	.555	0.211	21.576	.305
5 BK	45	1.57	72.21	.632	0.992	22.568	.313
4 M	44	1.53	73.74	.641	0.981	23.549	.319
5 M	15	0.52	74.26	1.415	0.736	24.285	.327
NO PRE-BREAK							
1 M	1187	41.09	41.09	.279	11.464	11.464	.279
SIZ	213	7.37	48.46	.302	2.226	13.690	.283
2 M	221	7.65	56.11	.328	2.509	16.199	.289
3 BK	72	2.49	58.60	.379	.994	17.193	.293
2 BK	81	2.80	61.40	.406	1.137	18.330	.299
3 M	89	3.08	64.48	.441	1.358	19.688	.305
4 BK	36	1.25	65.73	.450	0.563	20.251	.308
1 BK	106	3.67	69.40	.487	1.787	22.038	.318
1 TA	11	0.38	69.78	.608	0.231	22.269	.319
5 BK	36	1.25	71.03	.625	0.781	23.050	.325
4 M	47	1.63	72.66	.717	1.169	24.219	.333
5 M	18	0.62	73.28	1.402	0.869	25.088	.342
PRE-BREAK SIFTED							
1 M	1199	41.56	41.56	.266	11.055	11.055	.266
SIZ	216	7.49	49.05	.290	2.172	13.227	.270
2M	206	7.14	56.19	.300	2.142	15.369	.274
3 BK	78	2.70	58.89	.367	0.991	16.360	.278
2 BK	94	3.26	62.15	.376	1.226	17.586	.283
1 BK	116	4.02	66.17	.410	1.648	19.234	.291
3 M	75	2.60	68.77	.417	1.084	20.318	.295
4 BK	35	1.21	69.98	.452	0.547	20.865	.298
1 TA	9	0.31	70.29	.562	0.174	21.039	.299
5 BK	32	1.11	71.40	.575	0.638	21.677	.304
P BK	4	0.14	71.54	.614	0.086	21.763	.304
4 M	38	1.32	72.86	.666	0.879	22.642	.311
5 M	14	0.49	73.35	1.446	0.709	23.351	.318

A=ASH (14% Moisture Basis)  
Q= QUANTITY (% of Total Products)  
S= SUMMATION

MILL	ROSS FLOW
TEST	E
WHEAT	HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	Q X A	S of QXA	S of QXA S of Q
PRE-BREAK SIFTED							
1 M	1232	42.03	42.03	.264	11.096	11.096	.264
SIZ	209	7.13	49.16	.288	2.053	13.149	.267
2 M	180	6.14	55.30	.293	1.799	14.948	.270
3 BK	79	2.70	58.00	.357	0.964	15.912	.274
3 M	79	2.70	60.70	.375	1.013	16.925	.279
2 BK	92	3.14	63.84	.378	1.187	18.112	.284
1 BK	113	3.86	67.70	.415	1.602	19.714	.291
4 BK	35	1.19	68.89	.421	0.501	20.215	.293
1 TA	12	0.41	69.30	.544	0.223	20.433	.295
5 BK	35	1.19	70.49	.566	0.674	21.111	.299
P BK	6	0.20	70.69	.600	0.120	21.231	.300
4 M	56	1.91	72.60	.636	1.215	22.446	.309
5 M	15	0.51	73.11	1.263	0.644	23.090	.316
NO PRE-BREAK							
1 M	1163	39.69	39.69	.266	10.558	10.558	.266
SIZ	182	6.21	45.90	.316	1.962	12.520	.273
2 M	251	8.57	54.47	.316	2.708	15.228	.280
3 M	84	2.87	57.34	.373	1.071	16.299	.284
3 BK	76	2.59	59.93	.382	0.989	17.288	.288
2 BK	88	3.00	62.93	.397	1.191	18.479	.294
4 BK	31	1.06	63.99	.449	0.476	18.955	.296
1 BK	107	3.65	67.64	.494	1.803	20.758	.307
4 M	67	2.29	69.93	.576	1.319	22.077	.316
1 TA	17	0.58	70.51	.586	0.340	22.417	.318
5 BK	41	1.40	71.91	.637	0.892	23.309	.324
5 M	27	0.92	72.83	1.057	0.972	24.281	.333
PRE-BREAK NOT SIFTED							
1 M	1166	39.86	39.86	.267	10.643	10.643	.267
SIZ	202	6.91	46.77	.288	1.990	12.633	.270
2 M	243	8.31	55.08	.300	2.493	15.126	.275
3 BK	76	2.60	57.68	.364	0.946	16.072	.279
2 BK	102	3.49	61.17	.378	1.319	17.391	.284
3 M	77	2.63	63.80	.394	1.036	18.428	.289
1 BK	124	4.24	68.04	.415	1.760	20.187	.297
4 BK	40	1.37	69.41	.417	0.571	20.758	.299
5 BK	27	0.92	70.33	.523	0.481	21.240	.302
4 M	43	1.47	71.80	.580	0.853	22.092	.308
1 TA	12	0.41	72.21	.588	0.241	22.333	.309
5 M	18	0.62	72.83	1.081	0.670	23.003	.316



## Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)  
 Q=QUANTITY (% of Total Products)  
 S= SUMMATION

MILL \_\_\_\_\_ ROSS FLOW  
 TEST \_\_\_\_\_ F  
 WHEAT \_\_\_\_\_ HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	Q X A	S of QXA	S of QXA S of Q
NO PRE-BREAK							
1 M	1094	37.07	37.07	.277	10.268	10.268	.277
2 M	288	9.76	46.83	.299	2.918	13.187	.282
SIZ	220	7.46	54.29	.311	2.320	15.507	.286
3 BK	69	2.34	56.63	.381	0.892	16.398	.290
3 M	114	3.86	60.49	.382	1.475	17.873	.295
2 BK	85	2.88	63.37	.411	1.184	19.056	.301
4 BK	34	1.15	64.52	.417	0.480	19.536	.303
1 BK	111	3.76	68.28	.501	1.884	21.420	.314
4 M	55	1.86	70.14	.554	1.030	22.450	.320
1 TA	15	0.51	70.65	.569	0.290	22.740	.322
5 BK	41	1.39	72.04	.598	0.831	23.572	.327
5 M	24	0.81	72.85	1.014	0.821	24.393	.335
PRE-BREAK SIFTED							
1 M	1119	38.14	38.14	.254	9.688	9.688	.254
SIZ	213	7.26	45.40	.277	2.011	11.699	.258
2 M	271	9.24	54.64	.279	2.578	14.277	.261
3 BK	76	2.59	57.23	.351	0.909	15.186	.265
3 M	89	3.03	60.26	.356	1.079	16.264	.270
2 BK	91	3.10	63.36	.386	1.197	17.461	.276
4 BK	36	1.23	64.59	.411	0.506	17.966	.278
1 BK	120	4.09	68.68	.412	1.639	19.656	.286
1 TA	11	0.37	69.05	.502	0.186	19.841	.287
4 M	45	1.53	70.58	.537	0.822	20.663	.293
5 BK	46	1.57	72.15	.581	0.912	21.575	.299
P BK	6	0.20	72.35	.646	0.129	21.704	.300
5 M	21	0.72	73.07	.939	0.676	22.380	.306
PRE-BREAK NOT SIFTED							
1 M	1142	38.94	38.94	.261	10.163	10.163	.261
SIZ	180	6.14	45.08	.292	1.793	11.956	.265
2 M	297	10.13	55.21	.292	2.958	14.914	.270
3 BK	86	2.93	58.14	.356	1.043	15.957	.274
2 BK	90	3.07	61.21	.374	1.148	17.105	.279
3 M	76	2.59	63.80	.398	1.031	18.136	.284
1 BK	129	4.40	68.20	.413	1.817	19.953	.293
4 BK	35	1.19	69.39	.423	0.503	20.456	.295
1 TA	15	0.51	69.90	.583	0.297	20.753	.297
4 M	45	1.53	71.43	.597	0.913	21.666	.303
5 BK	41	1.40	72.83	.679	0.951	22.617	.311
5 M	18	0.61	73.44	1.073	0.655	23.272	.317



## Cumulative Flour Ash Calculations

A=ASH (14% Moisture Basis)  
 Q=QUANTITY (% of Total Products)  
 S= SUMMATION

MILL \_\_\_\_\_ ROSS FLOW  
 TEST \_\_\_\_\_ G  
 WHEAT \_\_\_\_\_ HARD RED WINTER

STREAM	WEIGHT (grams)	Q	S of Q	A	Q X A	S of QXA	S of QXA S of Q
PRE-BREAK NOT SIFTED							
1 M	1072	36.62	36.62	.274	10.034	10.034	.274
2 M	344	11.75	48.37	.294	3.455	13.488	.279
SIZ	192	6.56	54.93	.298	1.955	15.443	.281
3 BK	85	2.90	57.83	.363	1.053	16.496	.285
3 M	83	2.84	60.67	.381	1.082	17.578	.290
2 BK	93	3.18	63.85	.383	1.218	18.796	.294
1 BK	129	4.41	68.26	.423	1.865	20.661	.303
4 BK	47	1.61	69.87	.434	0.699	21.360	.306
1 TA	13	0.44	70.31	.561	0.247	21.607	.307
4 M	44	1.50	71.81	.617	0.926	22.532	.314
5 BK	26	0.89	72.70	.686	0.611	23.143	.318
5 M	16	0.55	73.25	1.039	0.571	23.714	.324
PRE-BREAK SIFTED							
1 M	1180	40.15	40.15	.262	10.519	10.519	.262
SIZ	184	6.26	46.41	.288	1.803	12.322	.266
2 M	263	8.95	55.36	.306	2.739	15.061	.272
3 BK	91	3.10	58.46	.356	1.104	16.164	.277
2 BK	91	3.10	61.56	.368	1.141	17.305	.281
3 M	69	2.35	63.91	.387	0.909	18.215	.285
1 BK	112	3.81	67.72	.413	1.574	19.788	.292
4 BK	40	1.36	69.08	.432	0.588	20.376	.295
1 TA	11	0.37	69.45	.516	0.191	20.567	.296
P BK	6	0.20	69.65	.576	0.115	20.682	.297
4 M	49	1.67	71.32	.661	1.104	21.786	.305
5 BK	42	1.43	72.75	.680	0.972	22.758	.313
5 M	17	0.58	73.33	1.319	0.765	23.523	.321
NO PRE-BREAK							
1 M	1194	40.63	40.63	.268	10.889	10.889	.268
SIZ	189	6.43	47.06	.312	2.006	12.895	.274
2 M	244	8.30	55.36	.325	2.698	15.593	.282
3 BK	78	2.65	58.01	.381	1.010	16.602	.286
2 BK	89	3.03	61.04	.401	1.215	17.817	.292
3 M	77	2.62	63.66	.433	1.134	18.952	.298
4 BK	33	1.12	64.78	.456	0.511	19.462	.300
1 BK	110	3.74	68.52	.492	1.840	21.302	.311
1 TA	17	0.58	69.10	.560	0.325	21.627	.313
5 BK	35	1.19	70.29	.579	0.689	22.316	.317
4 M	53	1.80	72.09	.606	1.091	23.407	.325
5 M	20	0.68	72.77	1.279	0.870	24.277	.334

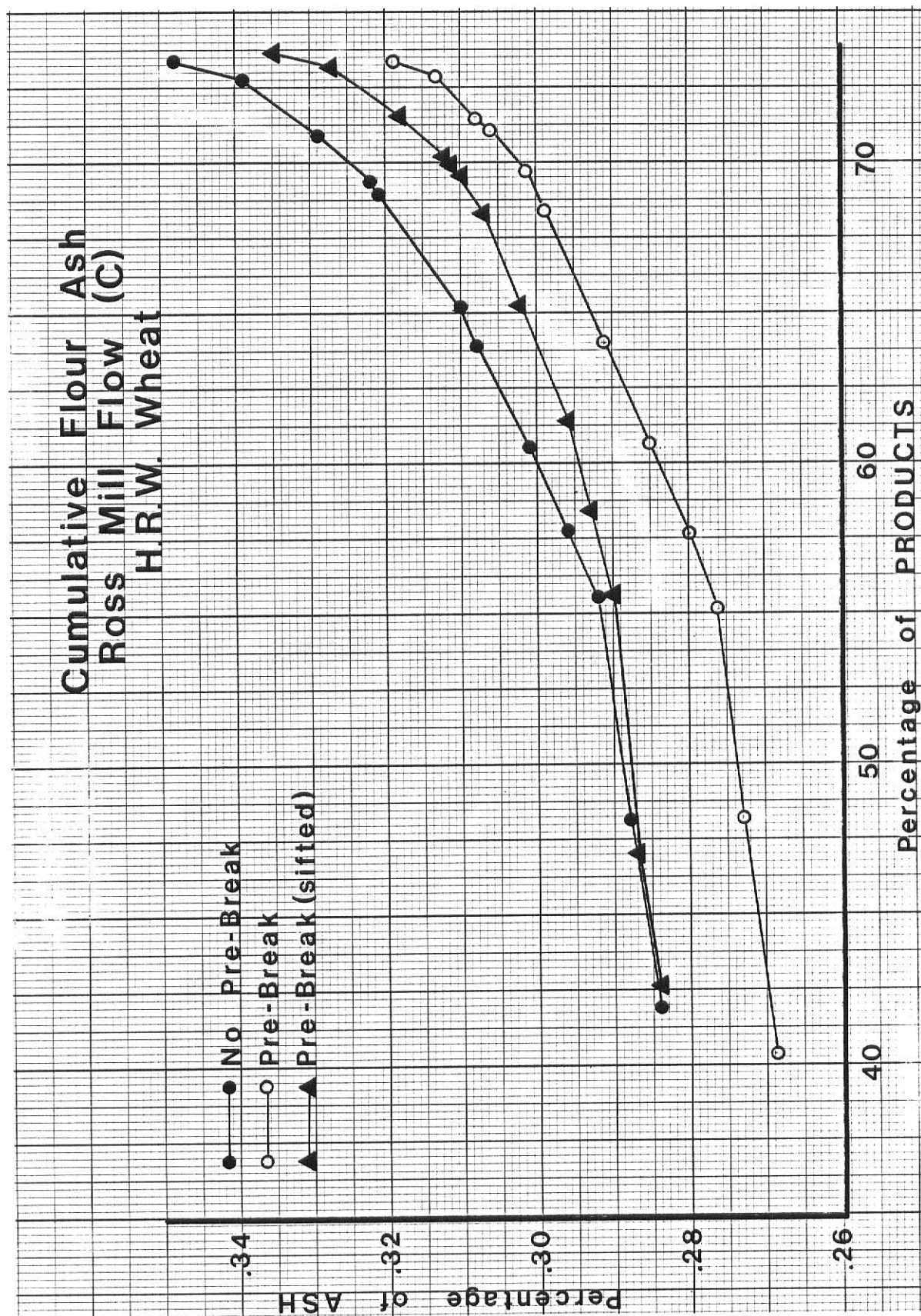


Figure 82

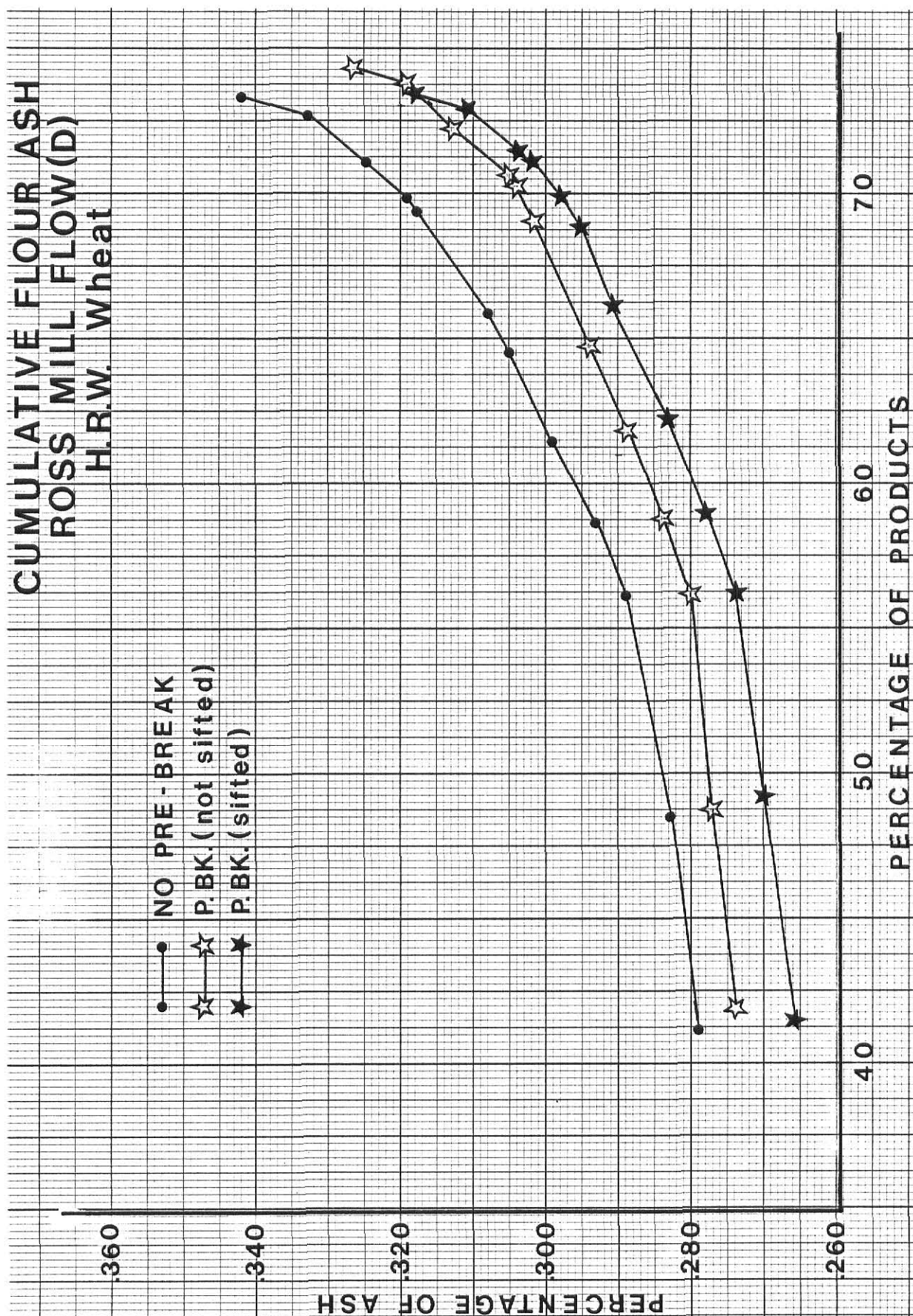


Figure 83



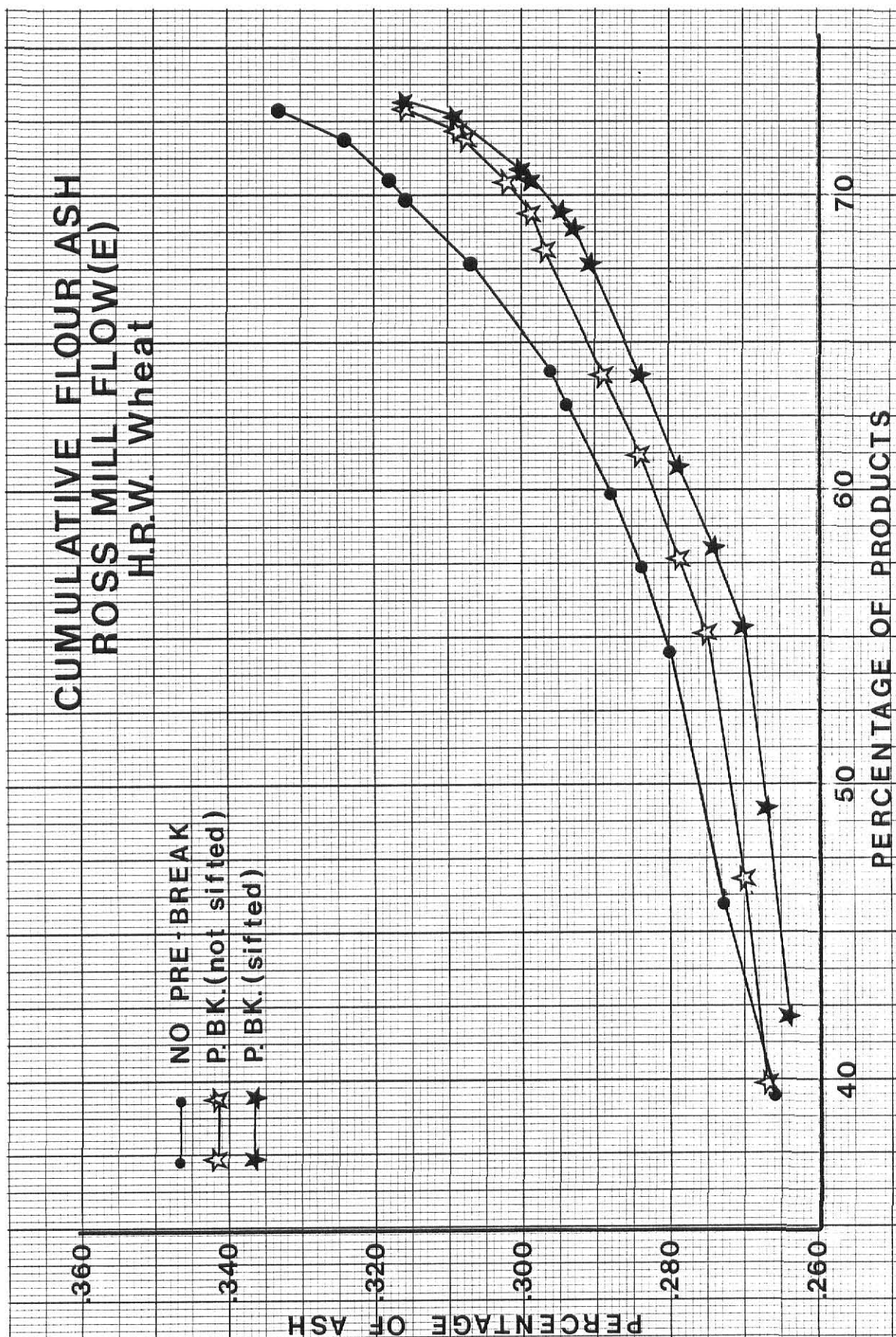


Figure 84

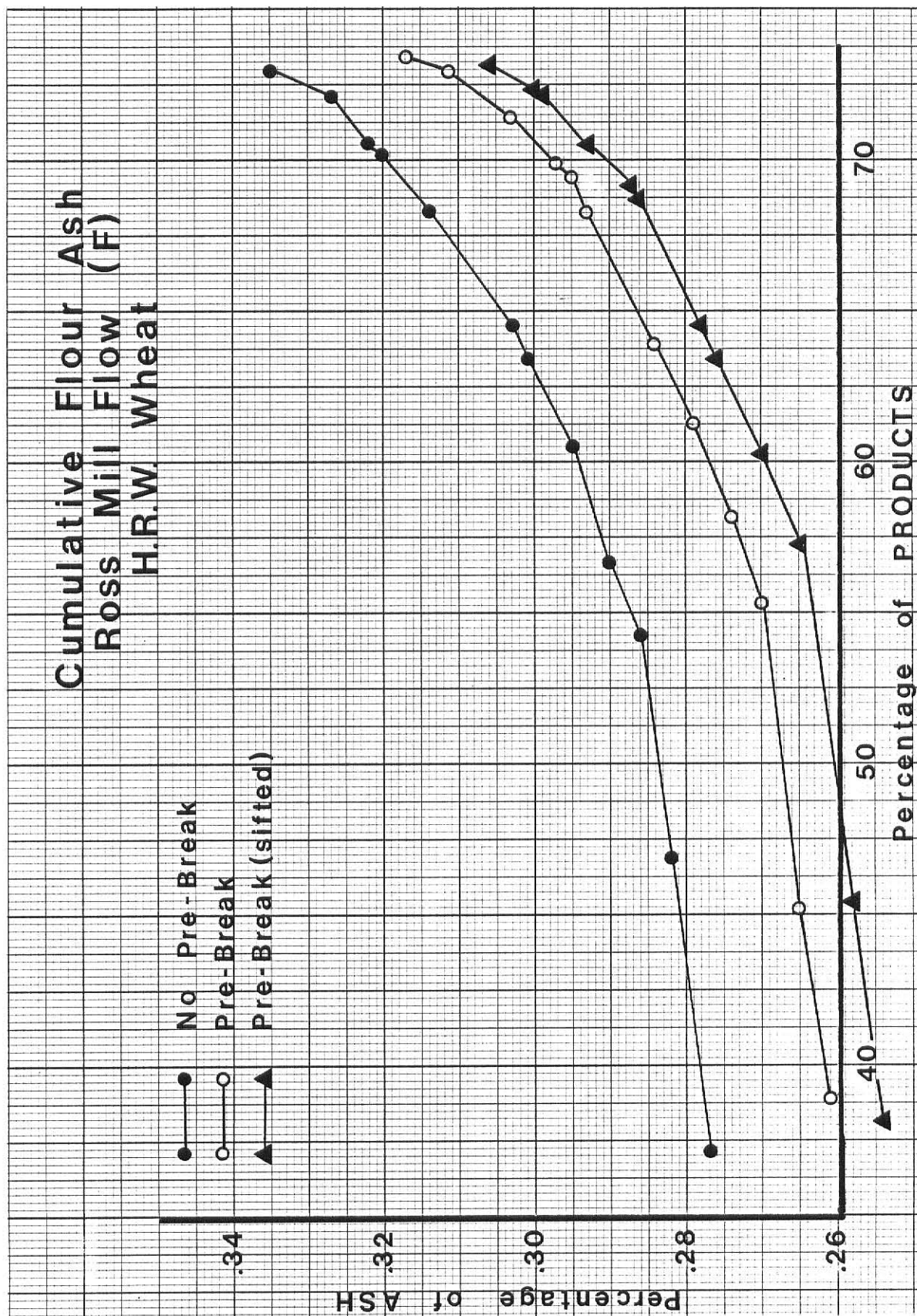


Figure 85

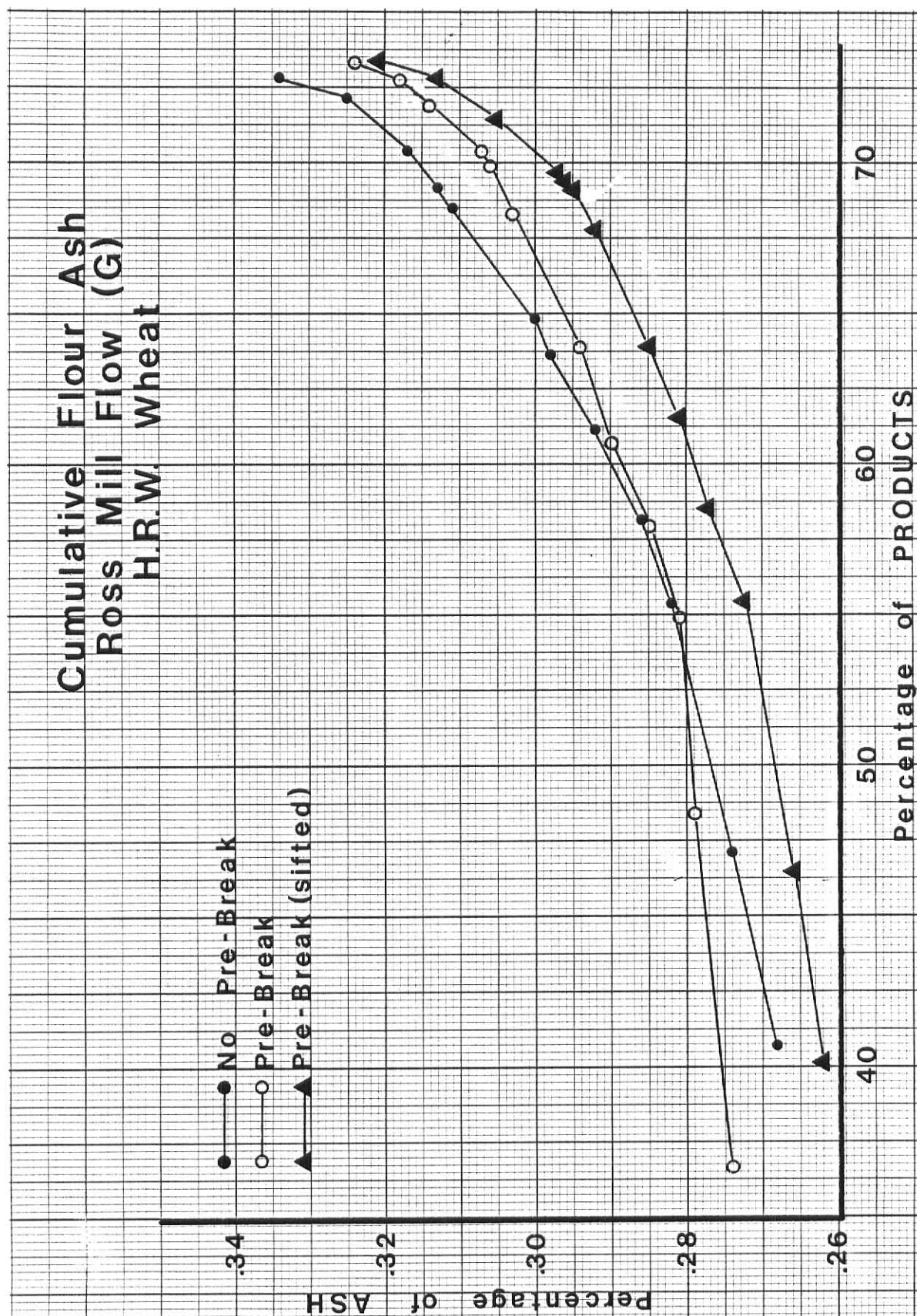


Figure 86



TEMPERED  
WHEAT

# PRE-BREAK

TEST 1A

151

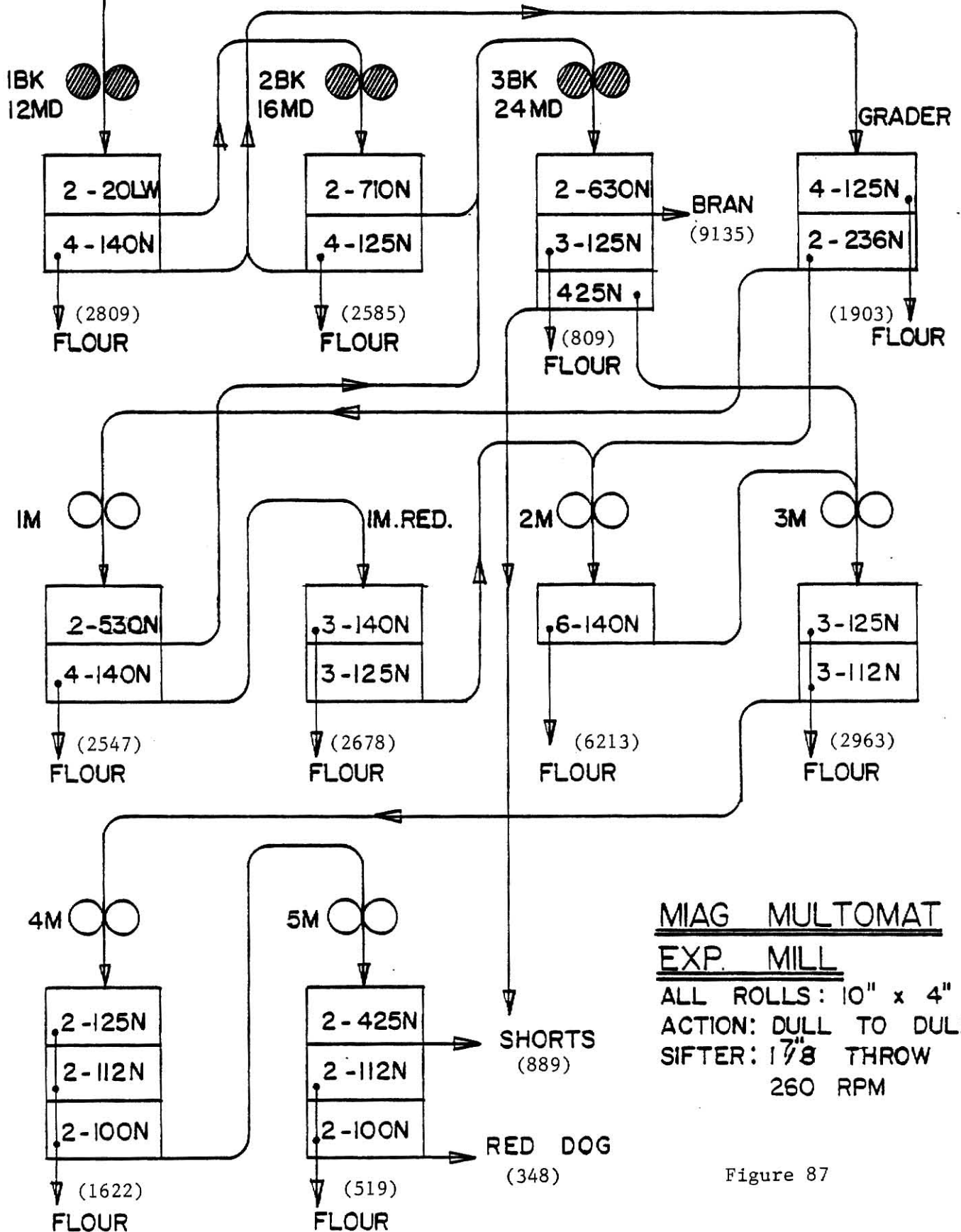


Figure 87



# NO PRE-BREAK

152

TEST 2A

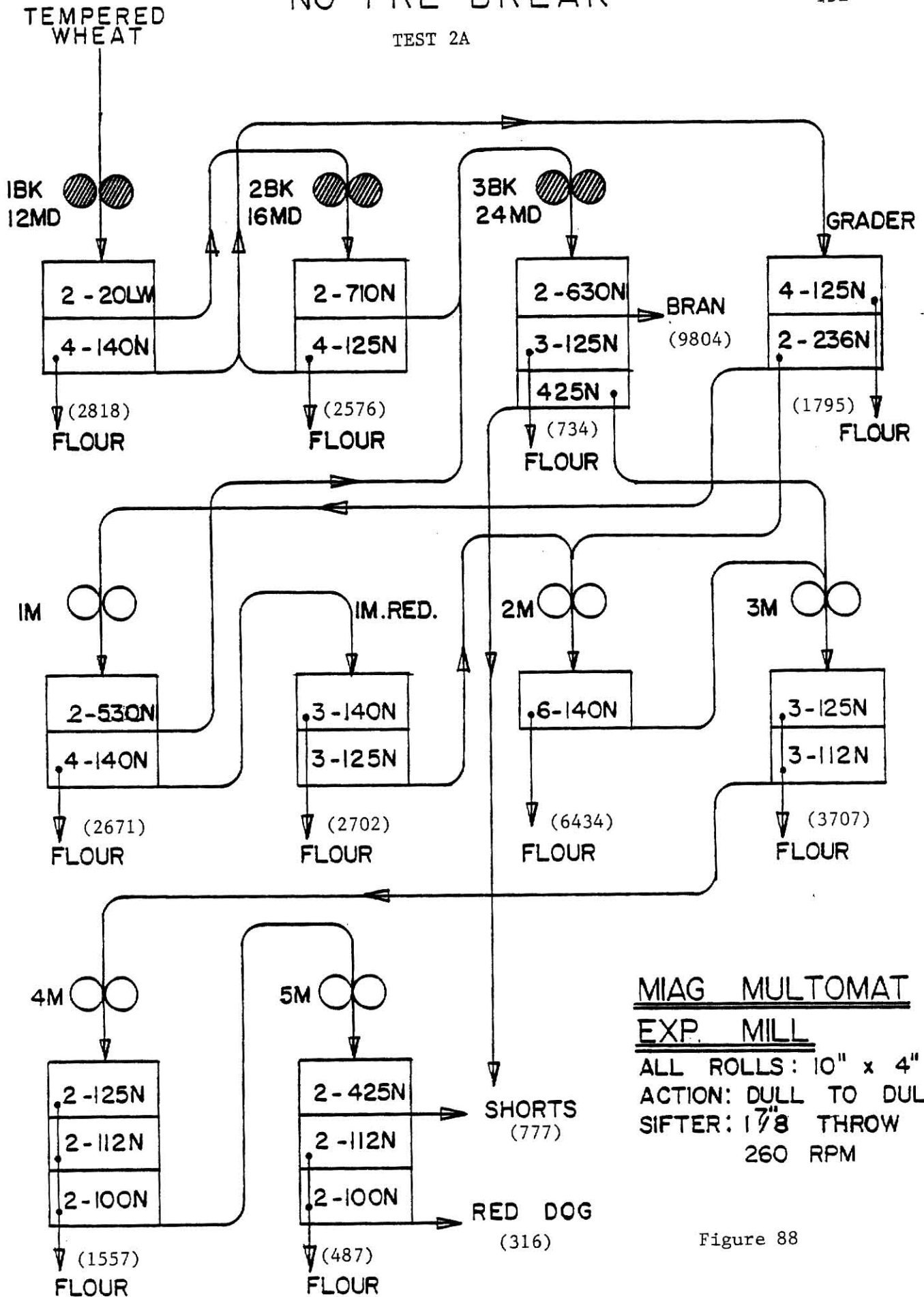
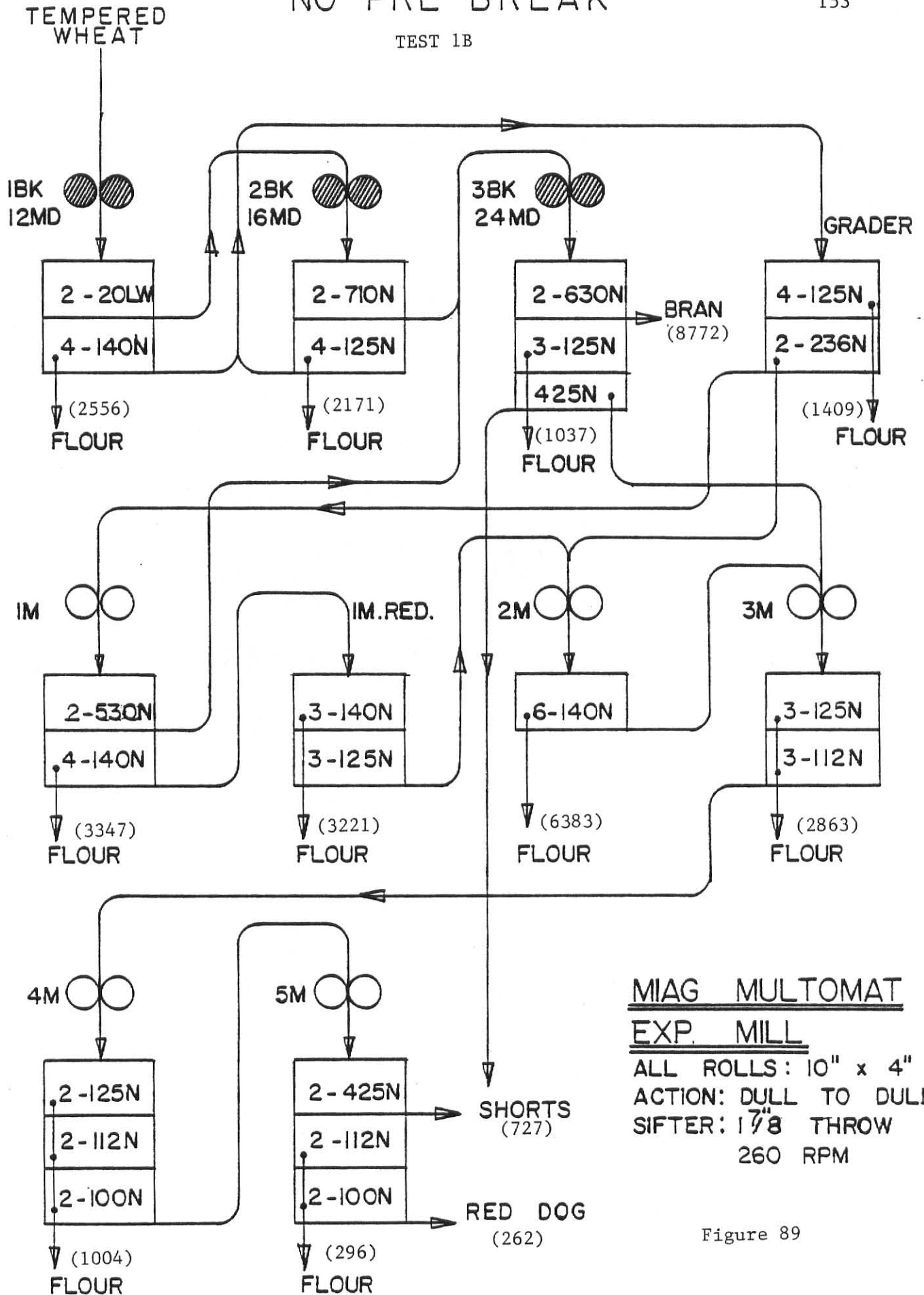


Figure 88

# NO PRE-BREAK

153

TEST 1B



MIAG MULTOMAT  
EXP. MILL  
 ALL ROLLS: 10" x 4"  
 ACTION: DULL TO DULL  
 SIFTER: 17/8 THROW  
 260 RPM

Figure 89

TEMPERED  
WHEAT

# PRE-BREAK

154

TEST 2B

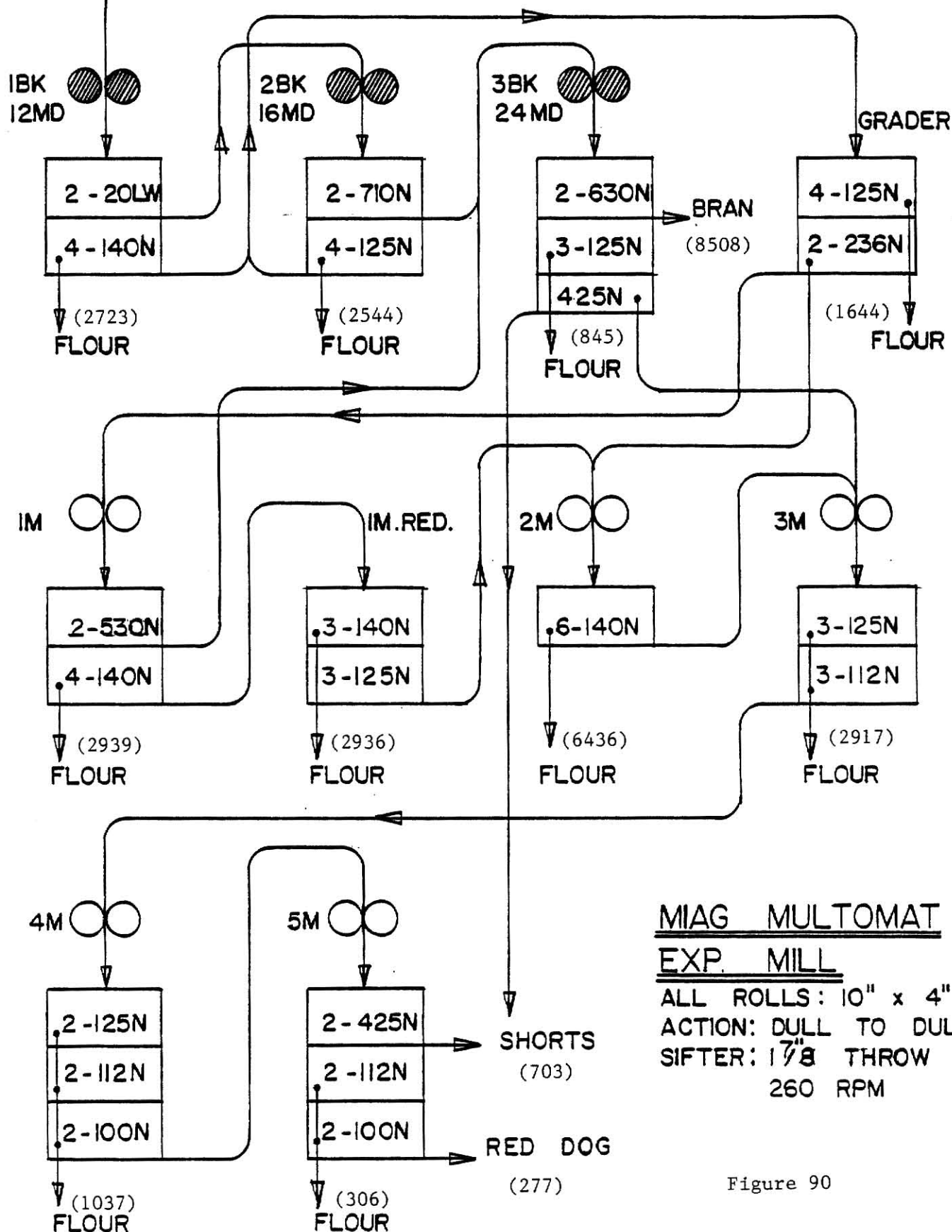


Figure 90

# NO PRE-BREAK

TEST 1C

155

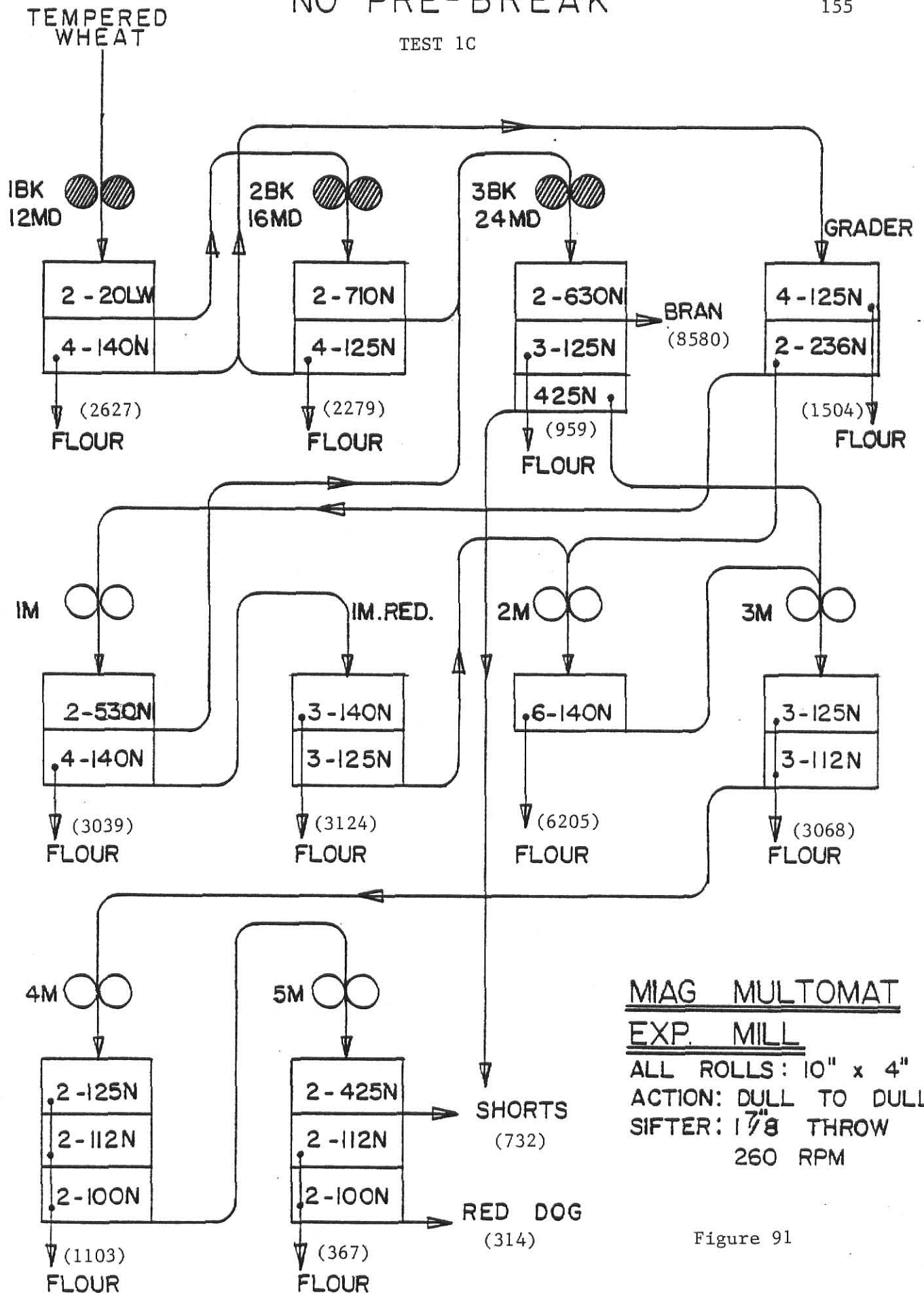


Figure 91

TEMPERED  
WHEAT

# PRE-BREAK

156

TEST 2C

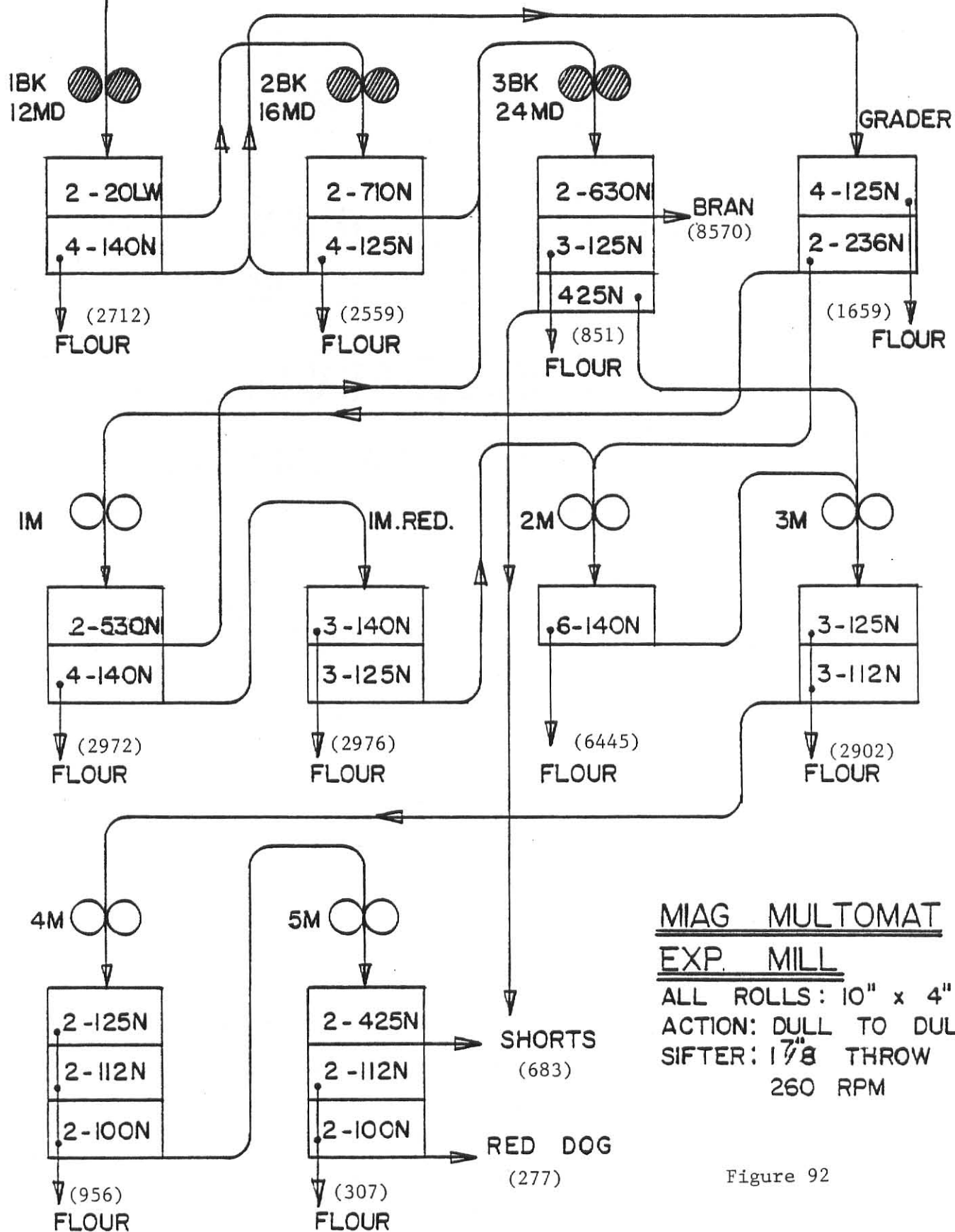


Figure 92

# NO PRE-BREAK

TEST 1D

157

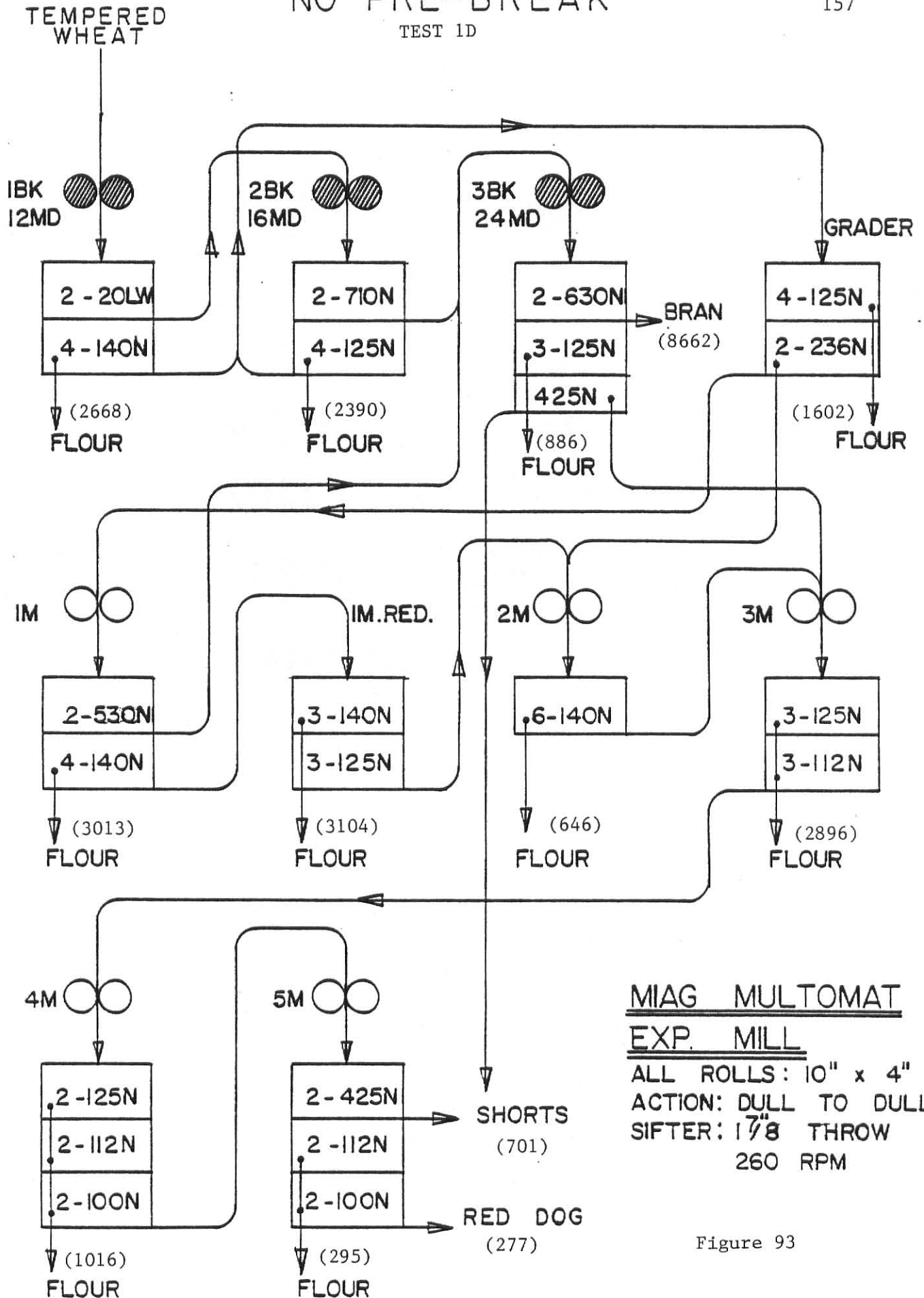


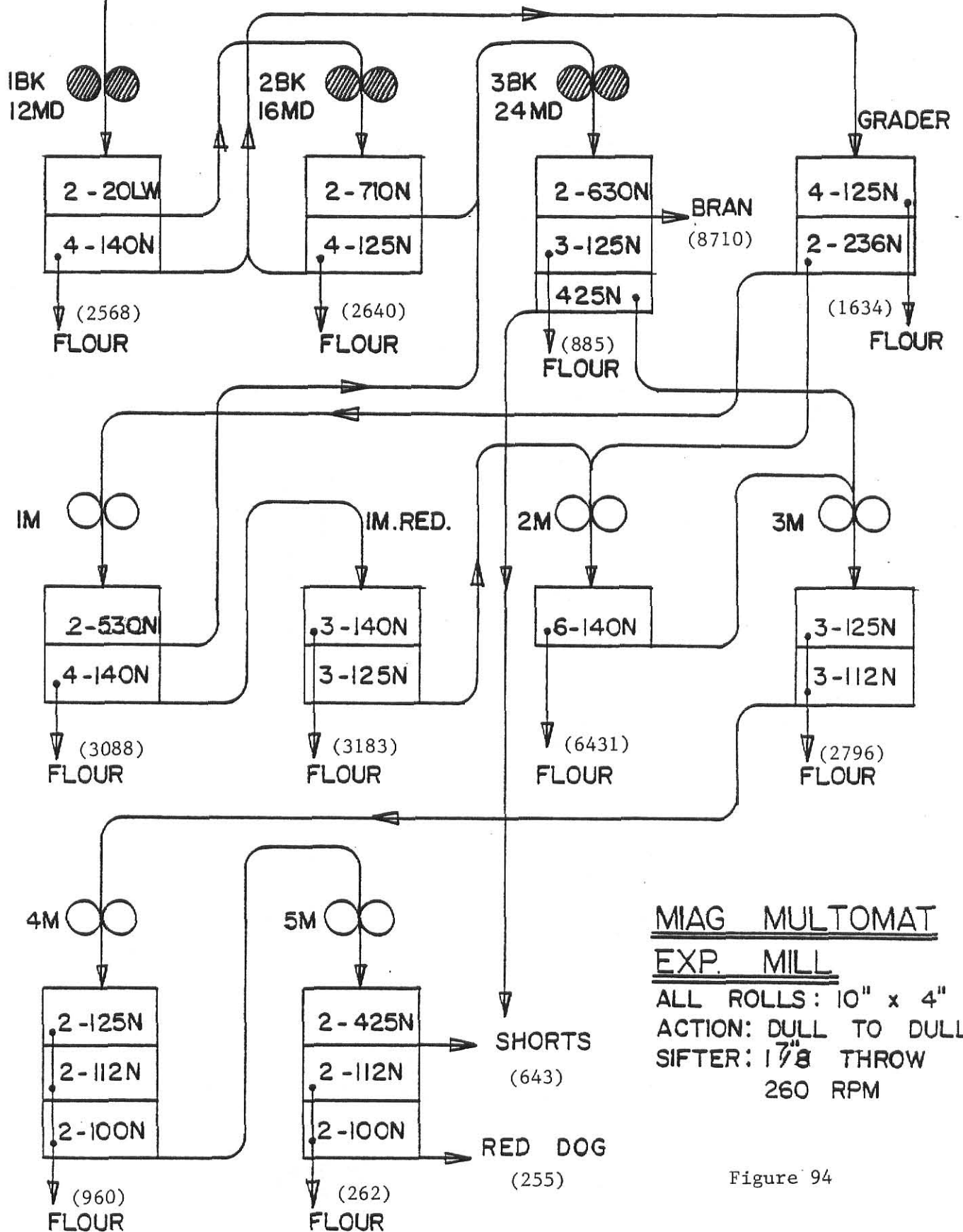
Figure 93

TEMPERED  
WHEAT

# PRE-BREAK

TEST 2D

158



MIAG MULTOMAT  
EXP. MILL  
ALL ROLLS: 10" x 4"  
ACTION: DULL TO DULL  
SIFTER: 17/8 THROW  
260 RPM

Figure 94



# NO PRE-BREAK

TEST 1E

159

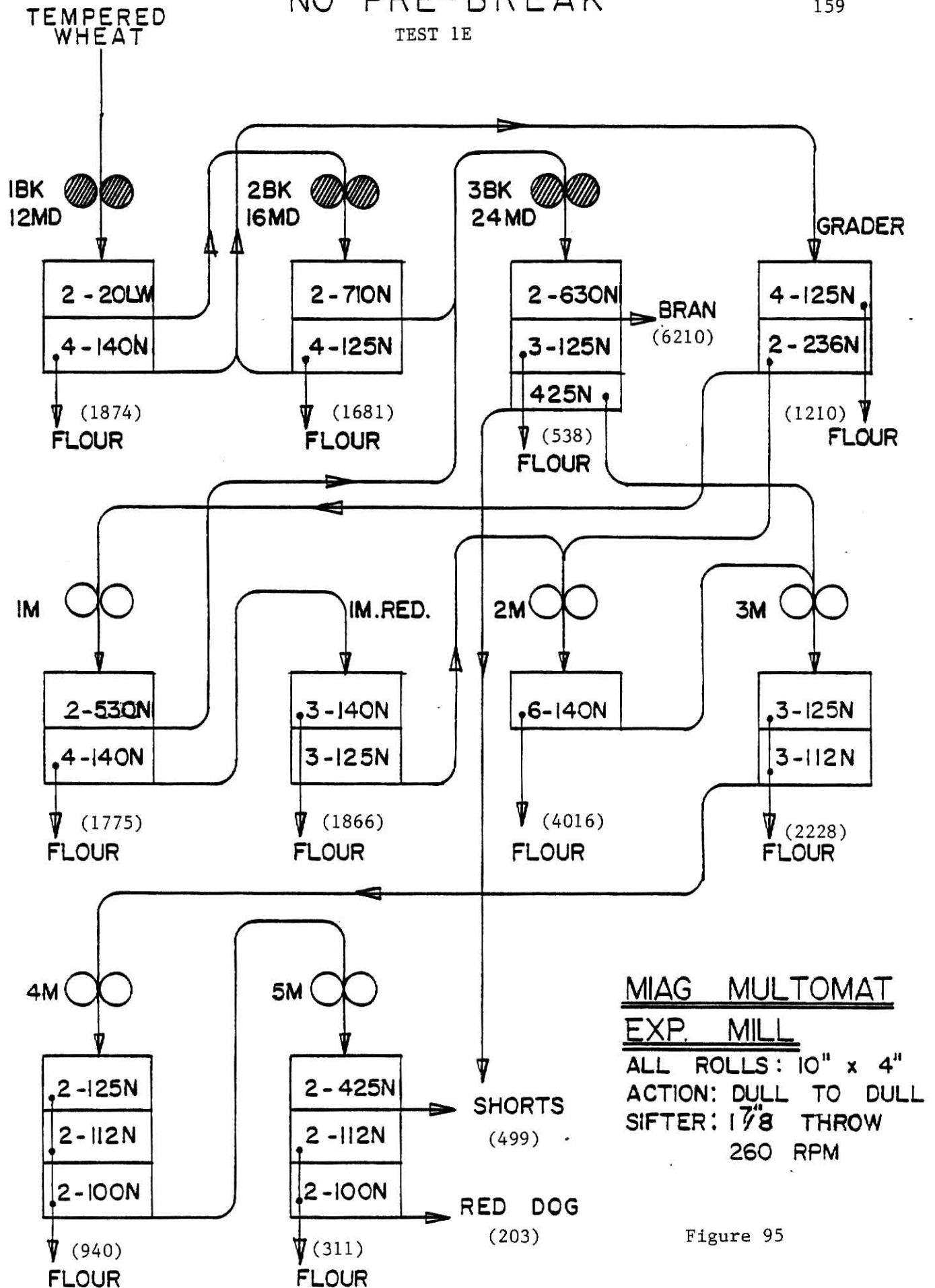


Figure 95

TEMPERED  
WHEAT

# PRE-BREAK

TEST 2E

160

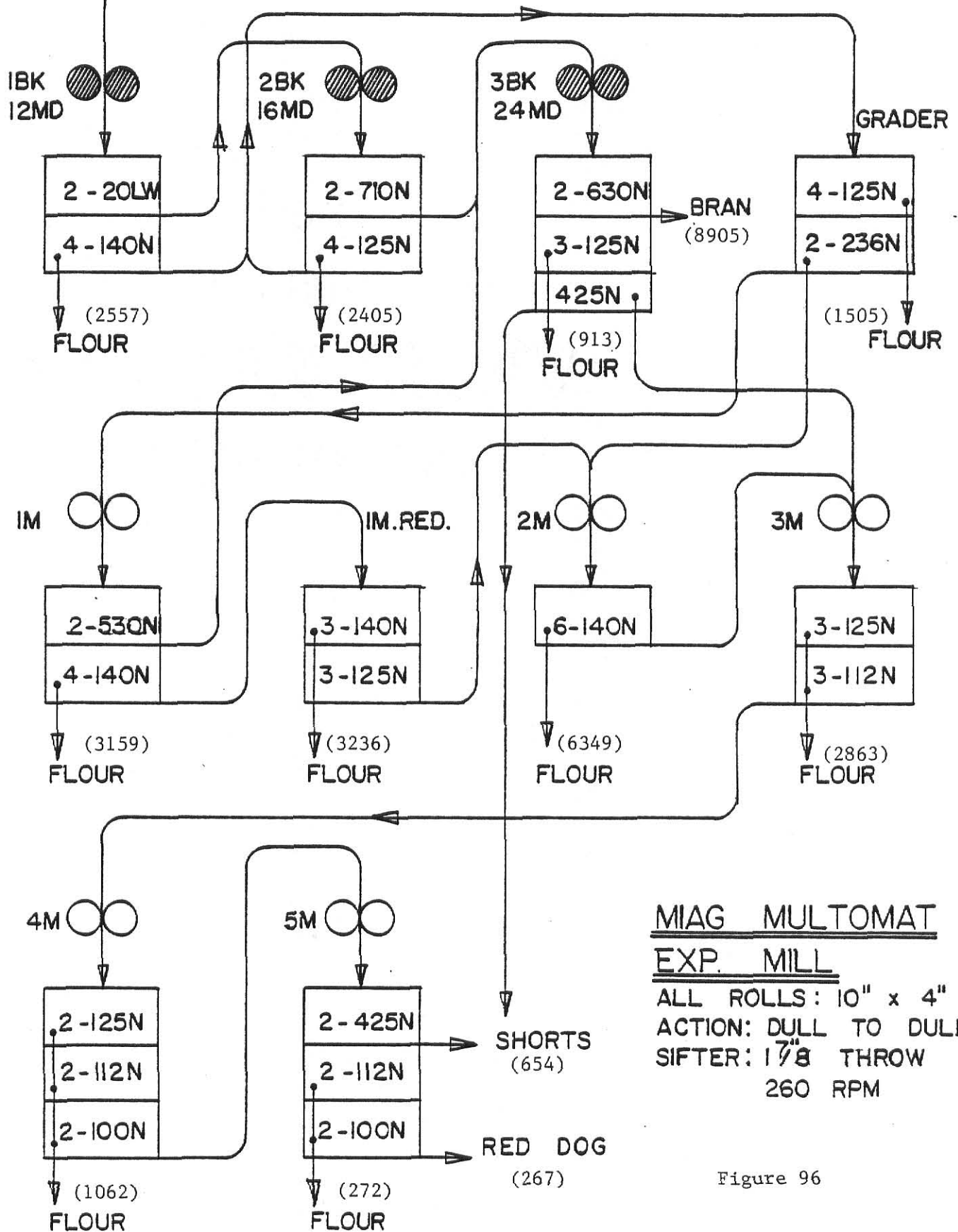


Figure 96















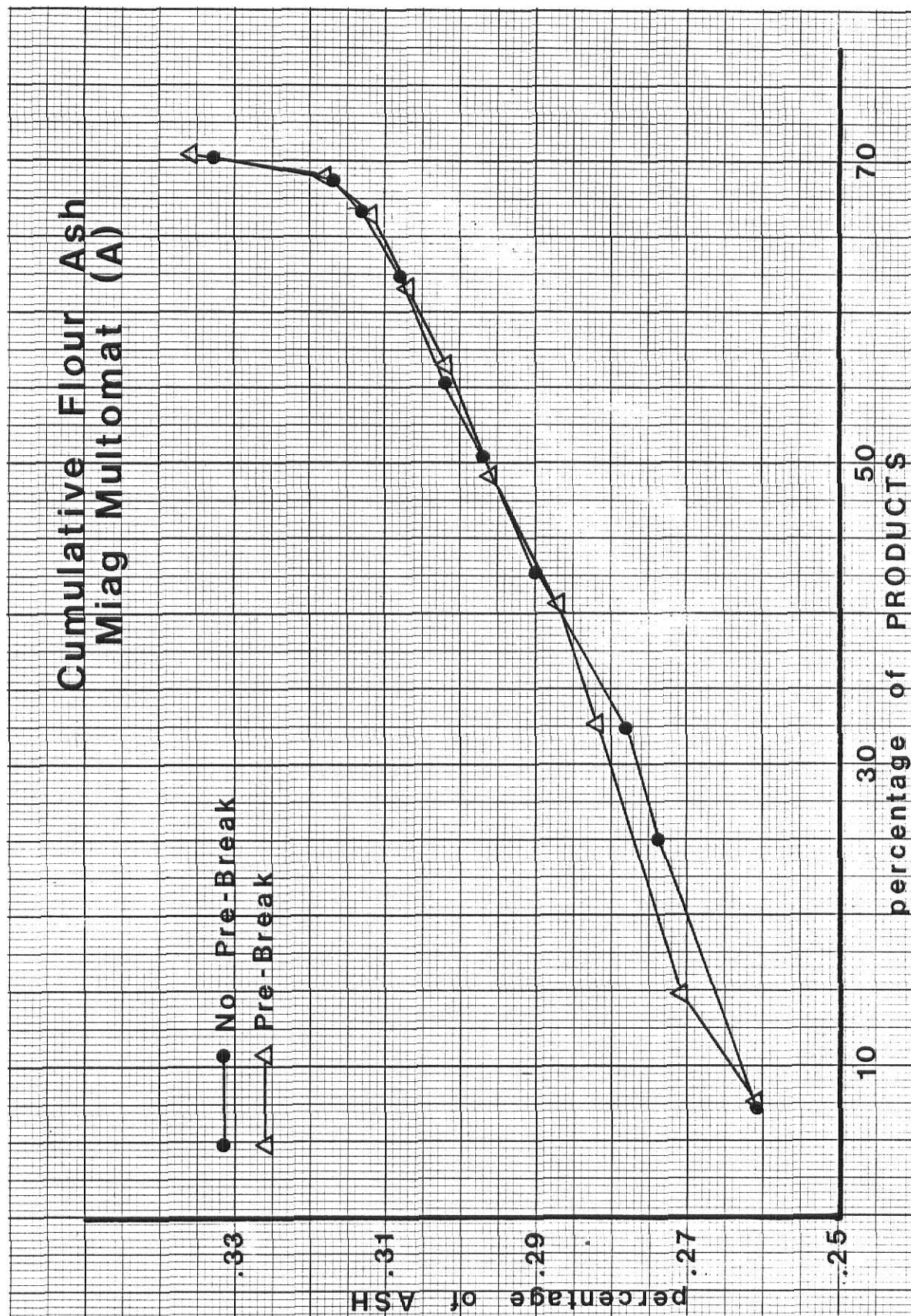


Figure 97

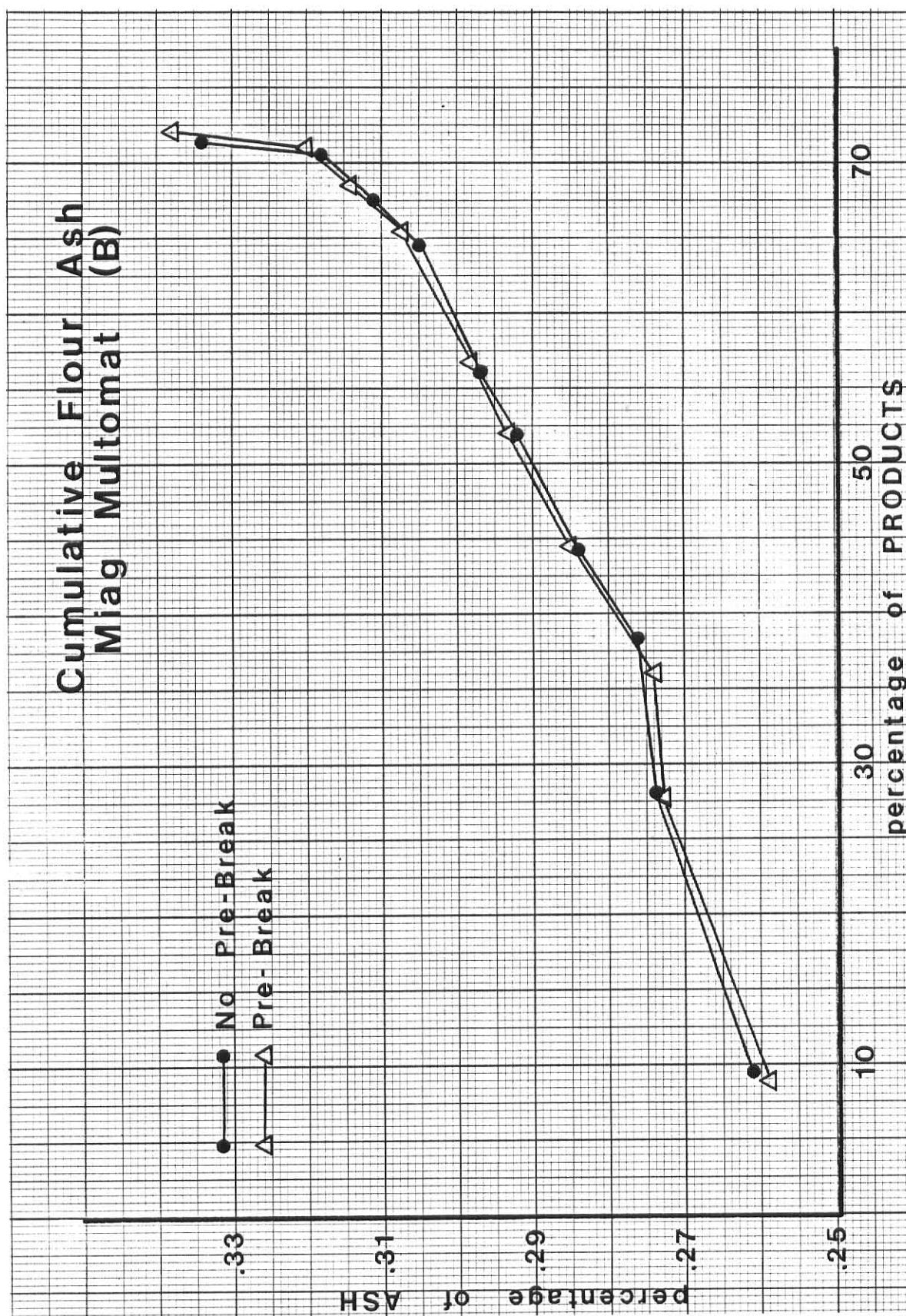


Figure 98

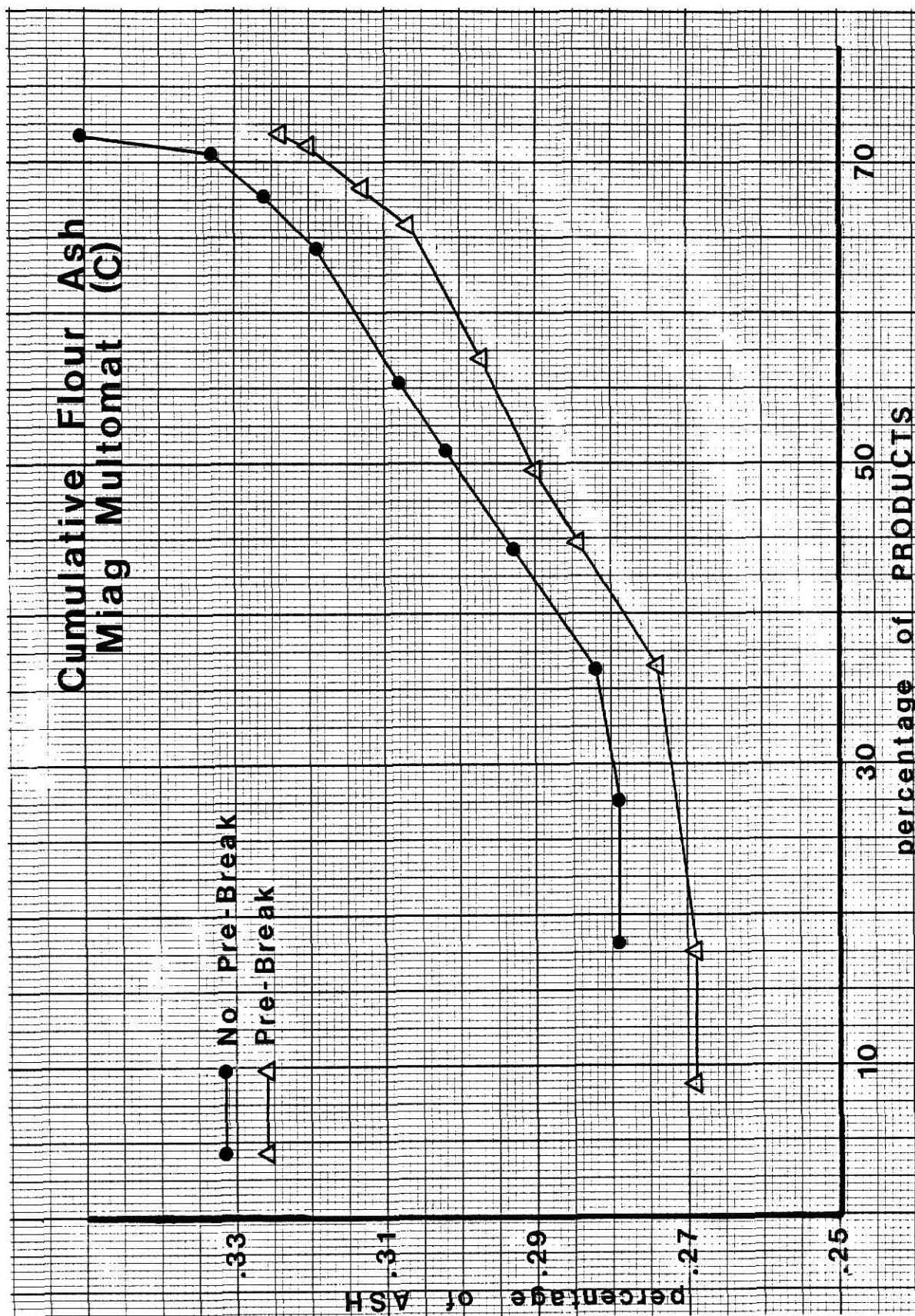


Figure 99



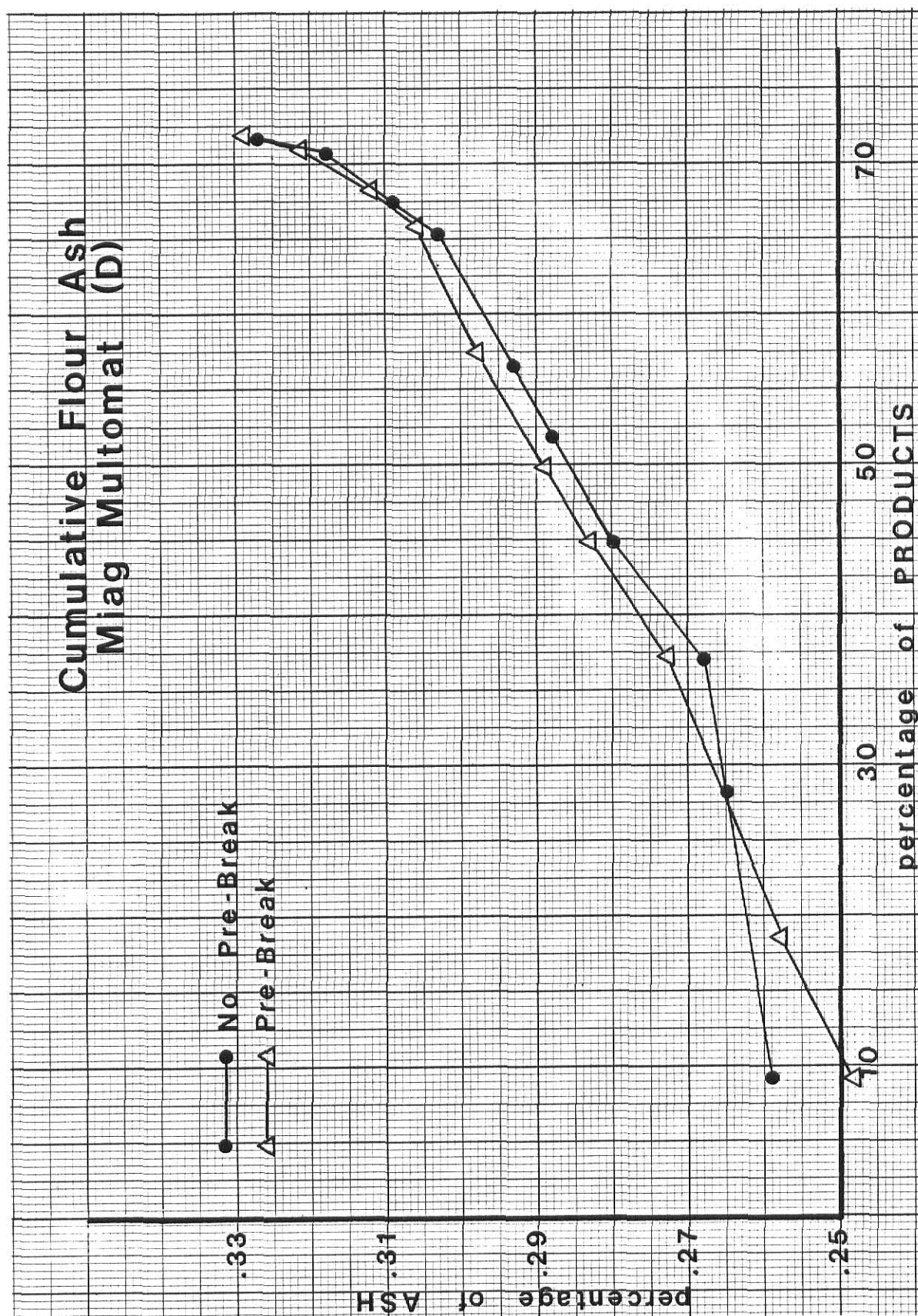


Figure 100

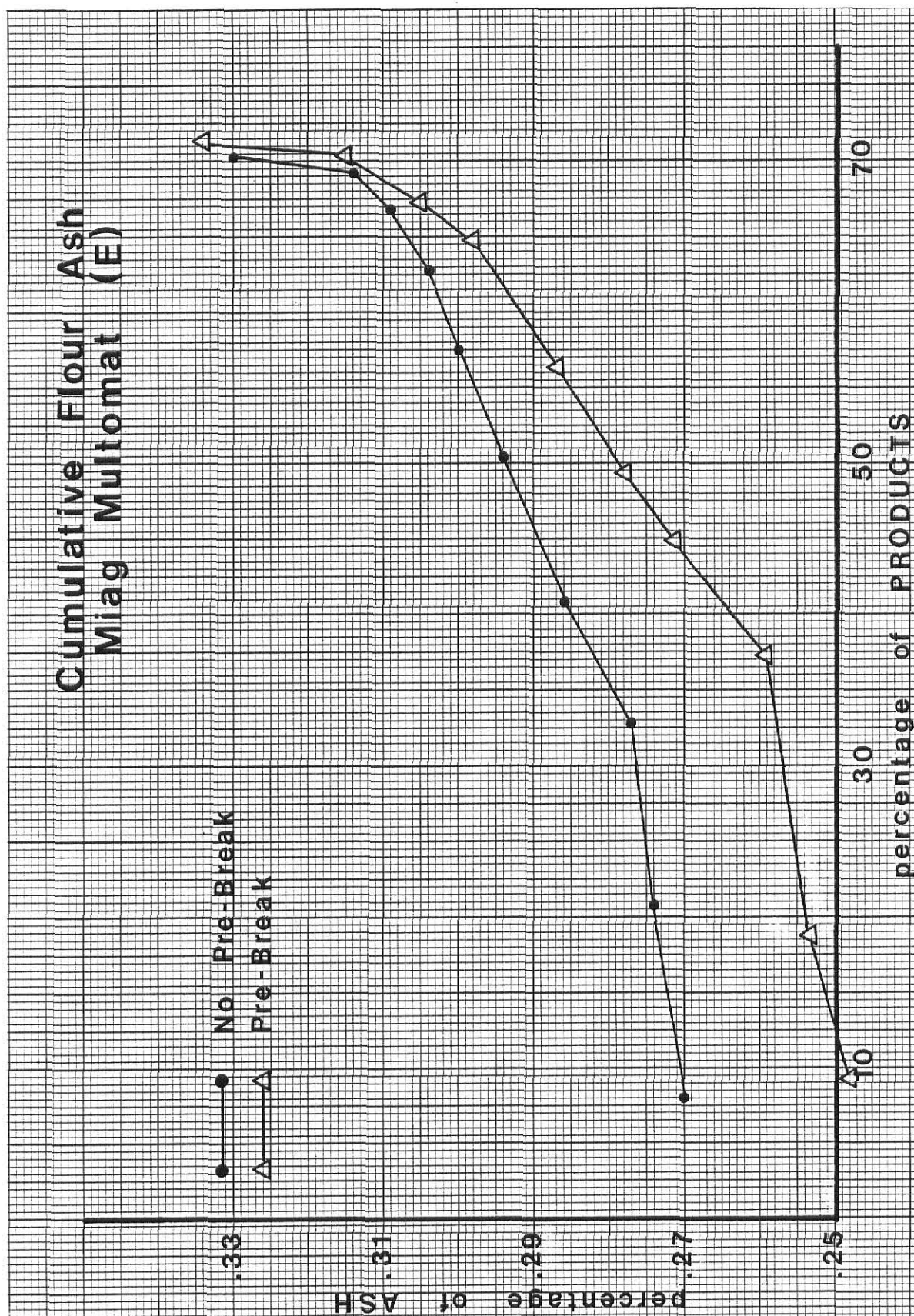


Figure 101

## APPENDIX B

## APPENDIX B

Preliminary Tests of Pre-Break on the Kansas  
State University Pilot Flour Mill

Preliminary testing of the use of Pre-Break on a large scale was initiated using the Kansas State University Pilot Flour Mill.

The KSU Pilot Mill has a capacity of approximately 200 hundredweights of flour in 24 hours. Although this is small in comparison to commercial mills, the equipment is scaled down to give comparable performance.

The Pilot Mill Flow (Figure 102) consists of 5 pairs of corrugated Breaks rolls, 10 pairs of smooth reduction rolls, 5 two-section free-swinging sifters and 5 purifiers (4 double, 1 single). Twenty-three separate flour streams are produced simultaneously with the capability of sampling each stream during mill operation. By obtaining 5-minute stream weights of each flour stream and sampling each for laboratory analysis of moisture and ash, milling performance for each mill run can be measured.

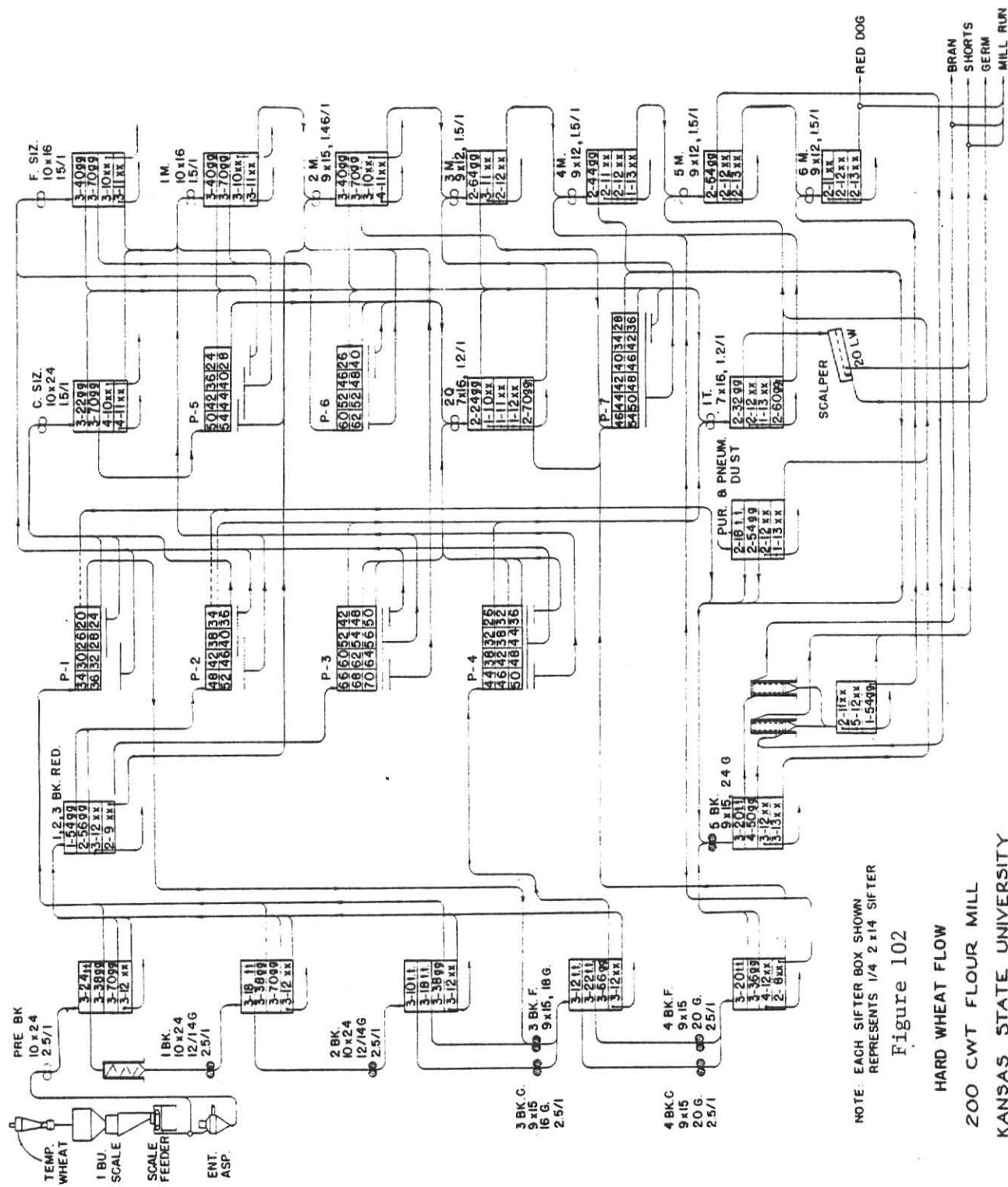
The Pre-Break System incorporated into the Pilot Mill Flow is shown in Figure 103. Tempered wheat from a belt scale feeder, to set the feed rate to the mill, can pass through an Entoleter-Scourer-Aspirator or directly to Pre-Break or First Break rolls. If Pre-Break is used, the Pre-Broken stock is sifted and the overs of a 24 light wire sieve are sent to an aspirator and then to First Break. Other separators from the sifter include sizings stock to purifier one, middlings stock to a Break Redust section and a small amount of flour.

Pre-Breaking itself is accomplished with a pair of smooth, 10 inch diameter by 24 inch length, Buhler rolls. Differential is created by a chain and sprocket drive. Initially, the roll was set up for a 2.5 to 1 differential, therefore the first two tests were run using this



differential. The chain was then removed for the remaining tests to give approximately a one to one differential with the flow of the wheat turning the free roll.

Data from these preliminary tests along with the resulting cumulative flour ash curves for each test are given in the following tables and figures.



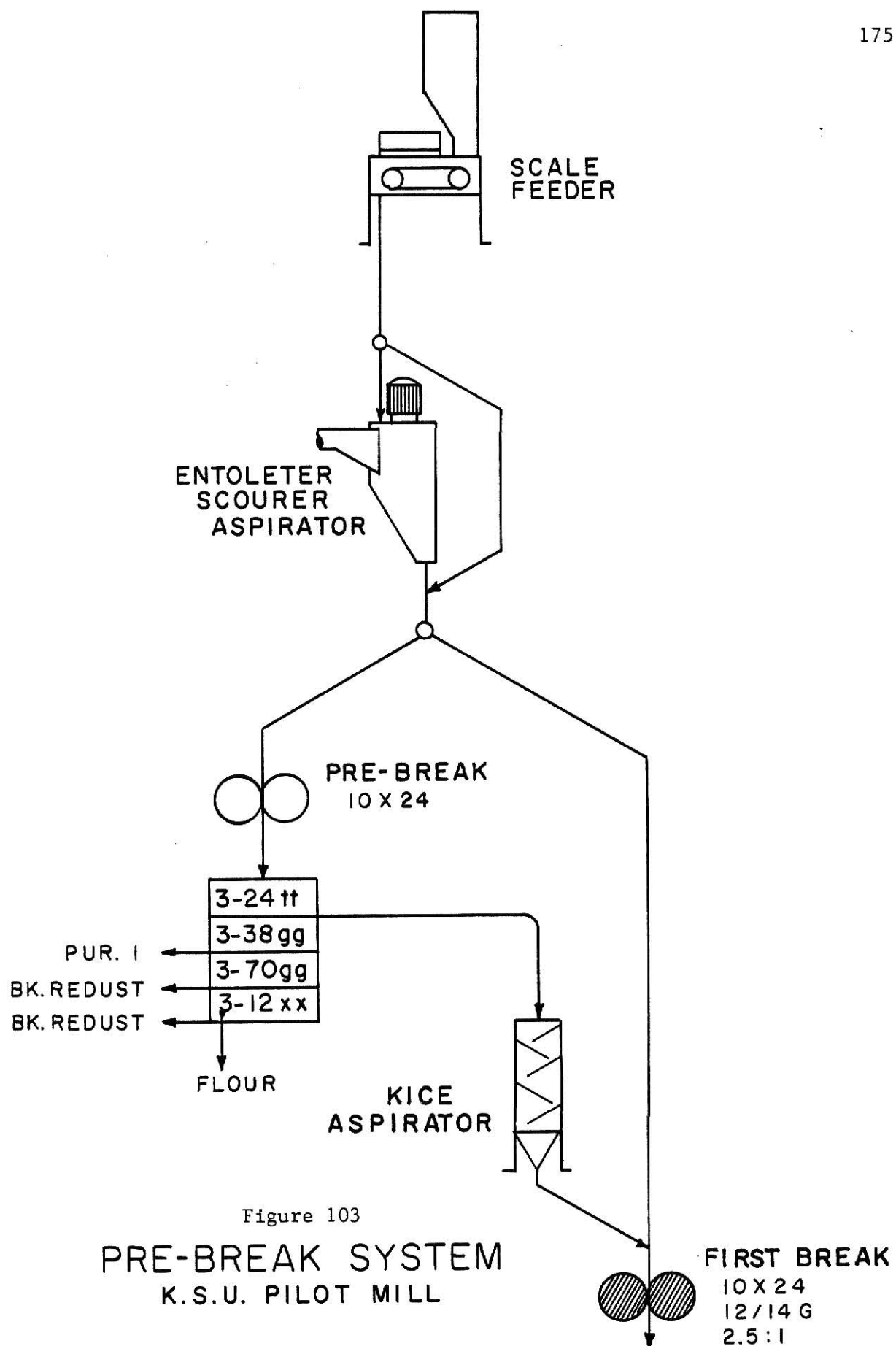


Figure 103

PRE-BREAK SYSTEM  
K.S.U. PILOT MILL





MILL	K.S.U. PILOT MILL
TEST	NO. 3A 2.5:1 DIFF
WHEAT	HARD RED WINTER

[illegible]







MILL	K.S.U. PILOT MILL
TEST	NO. 2B 2.5:1 DIFF
WHEAT	HARD RED WINTER

[illegible]

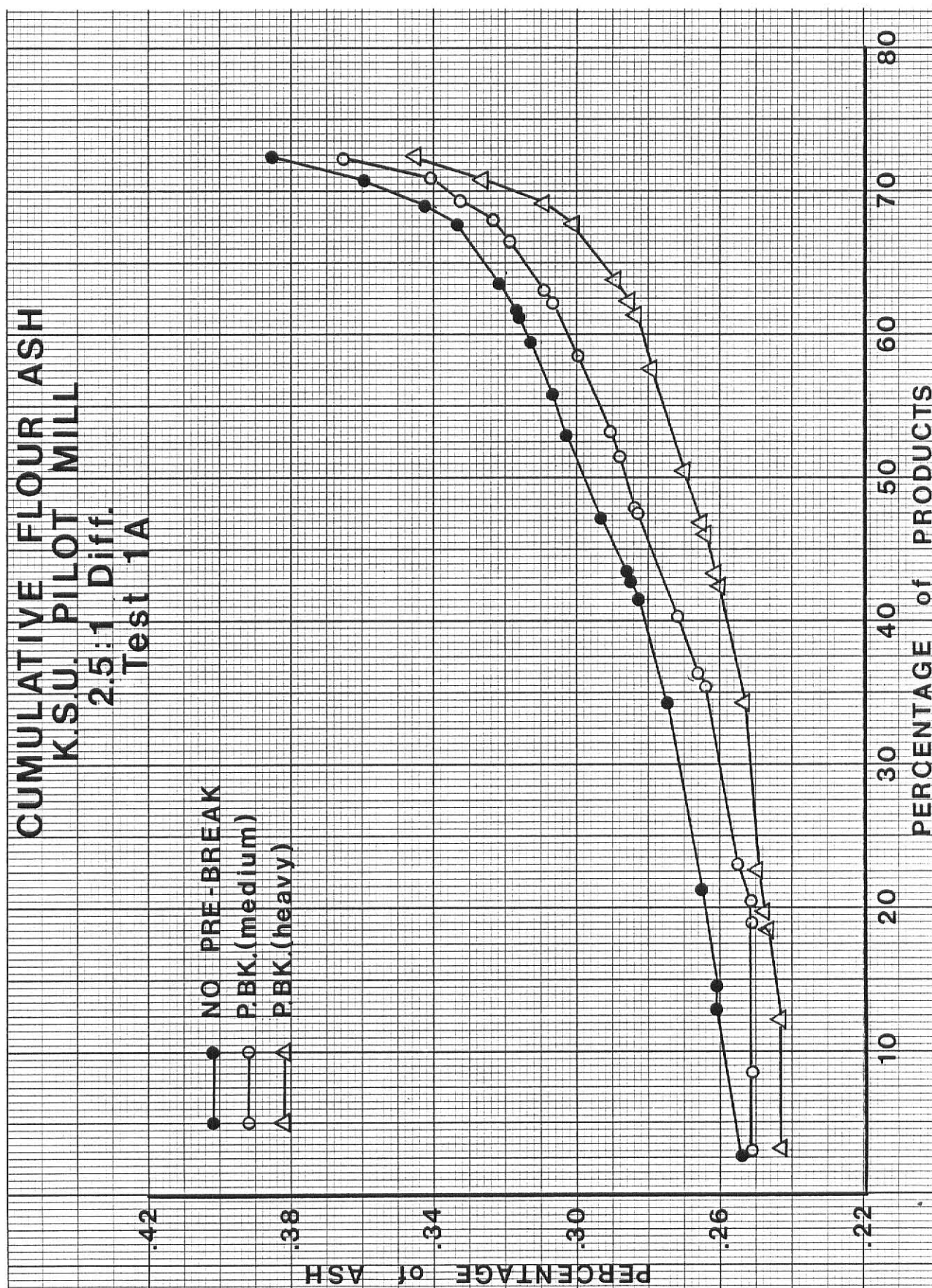


Figure 104



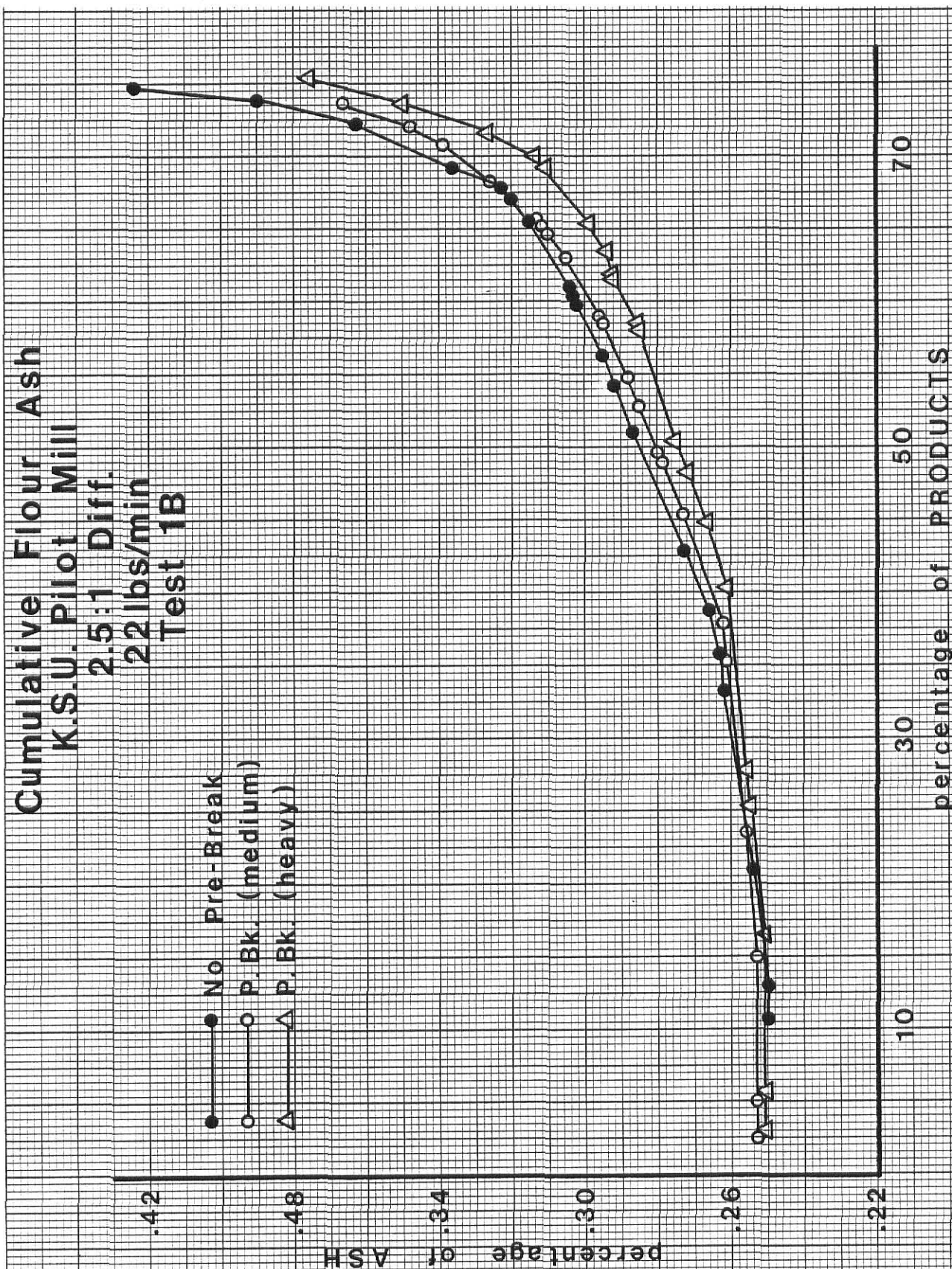


Figure 105



A=ASH (14% Moisture Basis)  
Q= QUANTITY (% of Total Products)  
S= SUMMATION

MILL	K.S.U. PILOT MILL
TEST	NO. 3A 1:1 DIFF
WHEAT	HARD RED WINTER

[illegible]





A=ASH (14% Moisture Basis)  
Q= QUANTITY (% of Total Products)  
S= SUMMATION

MILL	K.S.U. PILOT MILL
TEST	NO. 5A 1:1 DIFF
WHEAT	HARD RED WINTER

[illegible]



A=ASH (14% Moisture Basis)  
Q= QUANTITY (% of Total Products)  
S= SUMMATION

MILL	K.S.U. PILOT MILL
TEST	NO. 2B 1:1 DIFF
WHEAT	HARD RED WINTER

[illegible]

MILL	K.S.U. PILOT MILL
TEST	NO. 3B 1:1 DIFF
WHEAT	HARD RED WINTER

[illegible]

MILL TEST WHEAT	K.S.U. PILOT MILL	
	NO. 1C	1:1 DIFF
	HARD RED WINTER	

[illegible]









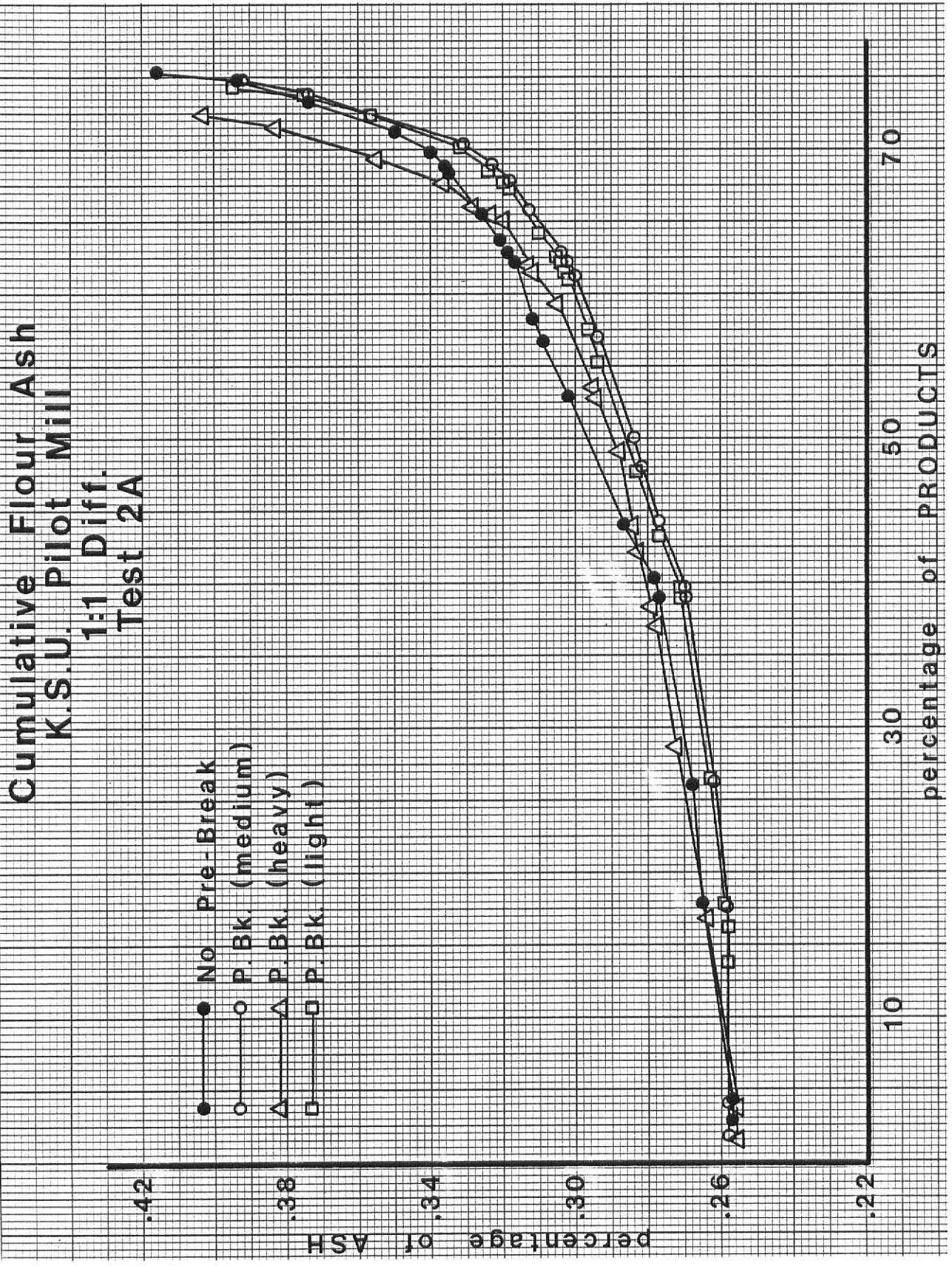


Figure 106

# CUMULATIVE FLOUR ASH K.S.U. PILOT MILL

1:1 Diff.

Test 2B

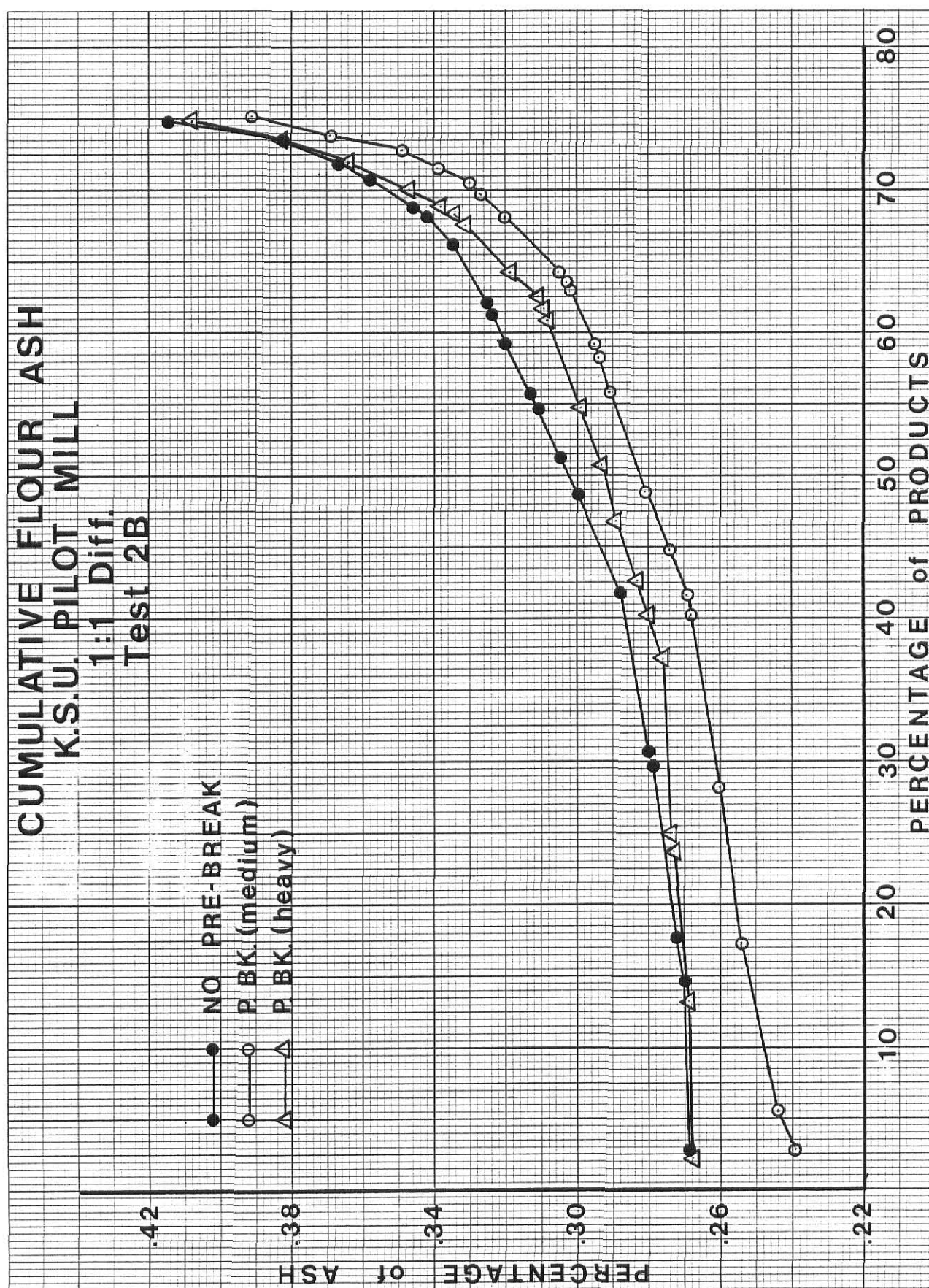


Figure 107



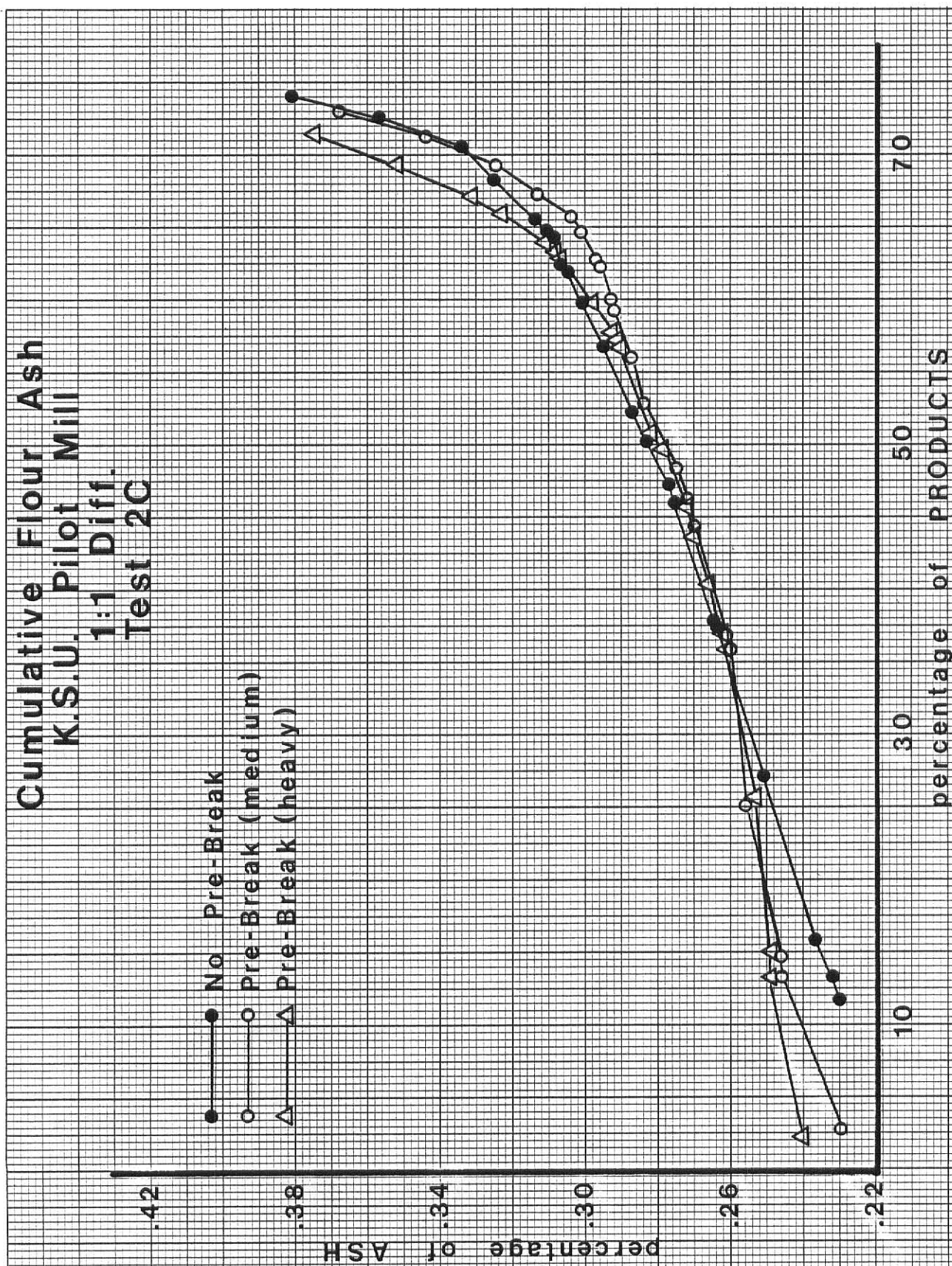


Figure 108

PRE-BREAKING: DOCUMENTING ITS EFFECTS

by

STEVEN P. CURRAN

B.S., Kansas State University, 1974

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AN ABSTRACT OF A MASTER'S THESIS

submitted in partial fulfillment of the

requirements for the degree

MASTER OF SCIENCE

Department of Grain Science and Industry

KANSAS STATE UNIVERSITY  
Manhattan, Kansas

1982

The purpose of this research was to document the effect of Pre-Breaking wheat kernels prior to the actual milling process. Five different types of experimental mills were used for the testing. A Hard Red Winter Wheat was used for all of the milling.

The five experimental mills which were utilized for the testing are as follows:

1. Brabender Quadrumat Junior
2. Brabender Quadrumat Senior
3. Buhler Experimental Mill
4. Ross Mill Walking Flow
5. Miag Multomat

Testing on each mill involved milling with the whole wheat kernels going directly to the First Breaking operation, as in a normal milling operation, and milling with the whole kernels being slightly broken, or opened at the crease of the kernel, before proceeding to the First Break. This Pre-Breaking was accomplished using, in most cases, smooth 9" x 6" rolls operating at a one to one differential. Where possible the Pre-Broken stock was also sifted prior to milling; this being done to determine if sifting of the Pre-Broken wheat had any effects other than just simple Pre-Breaking.

Flours from each milling were weighed and analyzed for both moisture and ash content. Cumulative flour ash was then calculated for each milling. To analyze the effect Pre-Breaking had on milling quality for each test, cumulative flour ash was plotted against the cumulative percentage of total products.

The analysis of the test results showed that, in all cases, milling performance of the same wheat mix was improved by Pre-Breaking the wheat prior to milling. Flour ash content was significantly lowered and a slight improvement in total extraction was realized for the samples that



were Pre-Broken. Where sifting of the Pre-Broken wheat was done prior to milling, improvement was noticed over the samples that were Pre-Broken and not sifted.