

OPTIMIZATION OF ROUTES AND MODES OF NUCLEAR
MATERIAL TRANSPORTATION CONSTRAINED BY
SAFETY CONSIDERATIONS

by

JAY PAUL ODOM

B.S., Oklahoma University, 1971

42-6074

A MASTER'S THESIS

submitted in partial fulfillment of the
requirements for this degree

MASTER OF SCIENCE

Department of Nuclear Engineering

KANSAS STATE UNIVERSITY

Manhattan, Kansas

1972

Approved by:

Walter Meyer
N. Dean Schubert
Major Professor

LO
2668
TH
1972
036
c.2
Docu-
ment

CONTENTS

| | | |
|-----|--|----|
| 1.0 | INTRODUCTION | 1 |
| 2.0 | SHIPPING CONSTRAINTS | 6 |
| 2.1 | Accessibility | 6 |
| 2.2 | Cost of Shipment | 7 |
| 2.3 | Safety | 11 |
| 3.0 | MODEL DESCRIPTION | 19 |
| 3.1 | Linear Programming | 19 |
| 3.2 | Mathematical Formulation | 26 |
| 3.3 | Results and Conclusions | 32 |
| 4.0 | POST OPTIMAL ANALYSIS | 41 |
| 4.1 | Solution Range Analysis | 41 |
| 4.2 | Cost Coefficient Analysis | 44 |
| 4.3 | Risk Coefficient Analysis | 48 |
| 4.4 | Conclusions | 49 |
| 5.0 | SUGGESTIONS FOR FURTHER STUDY | 51 |
| 6.0 | ACKNOWLEDGEMENTS | 52 |
| 7.0 | LITERATURE CITED | 53 |
| | APPENDICES | 54 |
| | APPENDIX A: MPS/360 computer listing and output for optimization and range analysis | 54 |
| | APPENDIX B: MPS/360 PARAOBJ computer listing and output for analysis of overweight truck cost | 66 |

LIST OF TABLES

| | | |
|-----------|---|----|
| TABLE I | INCIDENT EXPERIENCE BY MODE OR LOCATION | 14 |
| TABLE II | MODE, MILES TRAVELED AND ACCIDENT CHARACTERISTICS | 15 |
| TABLE III | VARIABLE DESCRIPTION | 27 |
| TABLE IV | ROUTE 1 HAZARD QUANTIFICATION DATA | 31 |
| TABLE V | PREDICTED SHIPPING ROUTES AND QUANTITIES FOR THE MODEL | 38 |
| TABLE VI | EFFECT OF VARYING OVERWEIGHT TRUCK COST | 46 |
| TABLE VII | EFFECT OF VARYING VSTOL AND LARGE AIRCRAFT COST | 47 |

LIST OF FIGURES

| | | |
|---------|---|----|
| FIG. 1 | URANIUM-PLUTONIUM REACTOR FUEL CYCLE | 2 |
| FIG. 2 | NUCLEAR POWER GROWTH | 4 |
| FIG. 3 | REQUIRED SPENT FUEL CASK MOVEMENTS ASSUMING SINGLE MODE SHIPMENT | 5 |
| FIG. 4 | TRUCK FUEL SHIPMENT STANDARD TRIP | 8 |
| FIG. 5 | CASK USE CHARGE APPROXIMATION | 9 |
| FIG. 6 | SPENT FUEL TRANSPORT COST | 10 |
| FIG. 7 | RELATION OF HAZARD QUANTIFICATION FACTORS | 13 |
| FIG. 8 | MAJOR TRUCK ROUTES FOR SPENT FUEL SHIPMENTS | 17 |
| FIG. 9 | MAJOR RAILROADS FOR SPENT FUEL SHIPMENTS | 18 |
| FIG. 10 | LINEAR PROGRAMMING GRAPHICAL SOLUTION TO EXAMPLE PROBLEM | 22 |
| FIG. 11 | LINEAR PROGRAMMING CONSTRAINT MATRIX | 33 |

1.0 INTRODUCTION

The transportation of nuclear materials involved in the nuclear power industry can be understood by examining the nuclear fuel cycle which is illustrated in Fig. 1. The cycle begins with mining and preparation of fuels and ends with recovery from "spent" fuel elements of unused and newly-generated fuel materials. The central steps of the cycle concerns the fission process employed by the reactor plant to generate electricity. These plants are fueled by one or more of the fissionable materials uranium-235, uranium-233, or plutonium-239.

After sustained operation of the reactor, the fuel elements must be reprocessed since the fissionable material has been used to the extent that a chain reaction can no longer be maintained. During the fission process, the fissionable atoms are split releasing energy, and many fission fragments are often of unstable configuration and decay radioactively by emission of beta, gamma, or alpha rays. Since they are highly radioactive, the fuel elements are left to "cool" as the radioactivity decays exponentially with time.

After a sufficient cooling period, the spent fuel elements are packed in a shipping cask. The cask shielding generally is made of a dense material such as lead to attenuate the radiation. Shielding, heat transfer, impact fire damage and other design criteria demand a heavy and expensive shipping cask. Generally these casks are leased for costly rates.

Fissionable material is recovered from the depleted fuel elements at fuel-reprocessing plants. In this process, highly radioactive liquid and

**THIS BOOK
CONTAINS
NUMEROUS PAGES
WITH DIAGRAMS
THAT ARE CROOKED
COMPARED TO THE
REST OF THE
INFORMATION ON
THE PAGE.**

**THIS IS AS
RECEIVED FROM
CUSTOMER.**

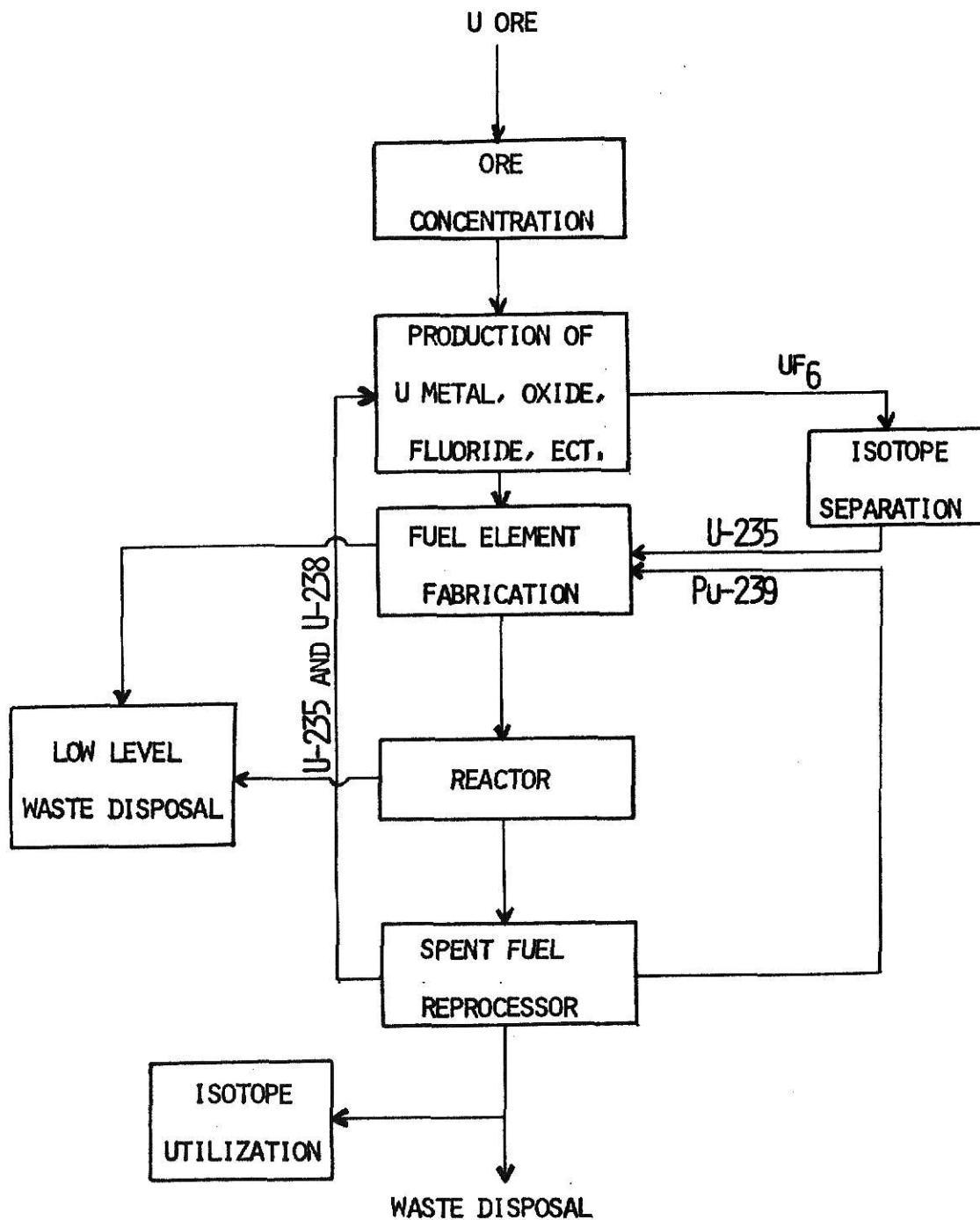


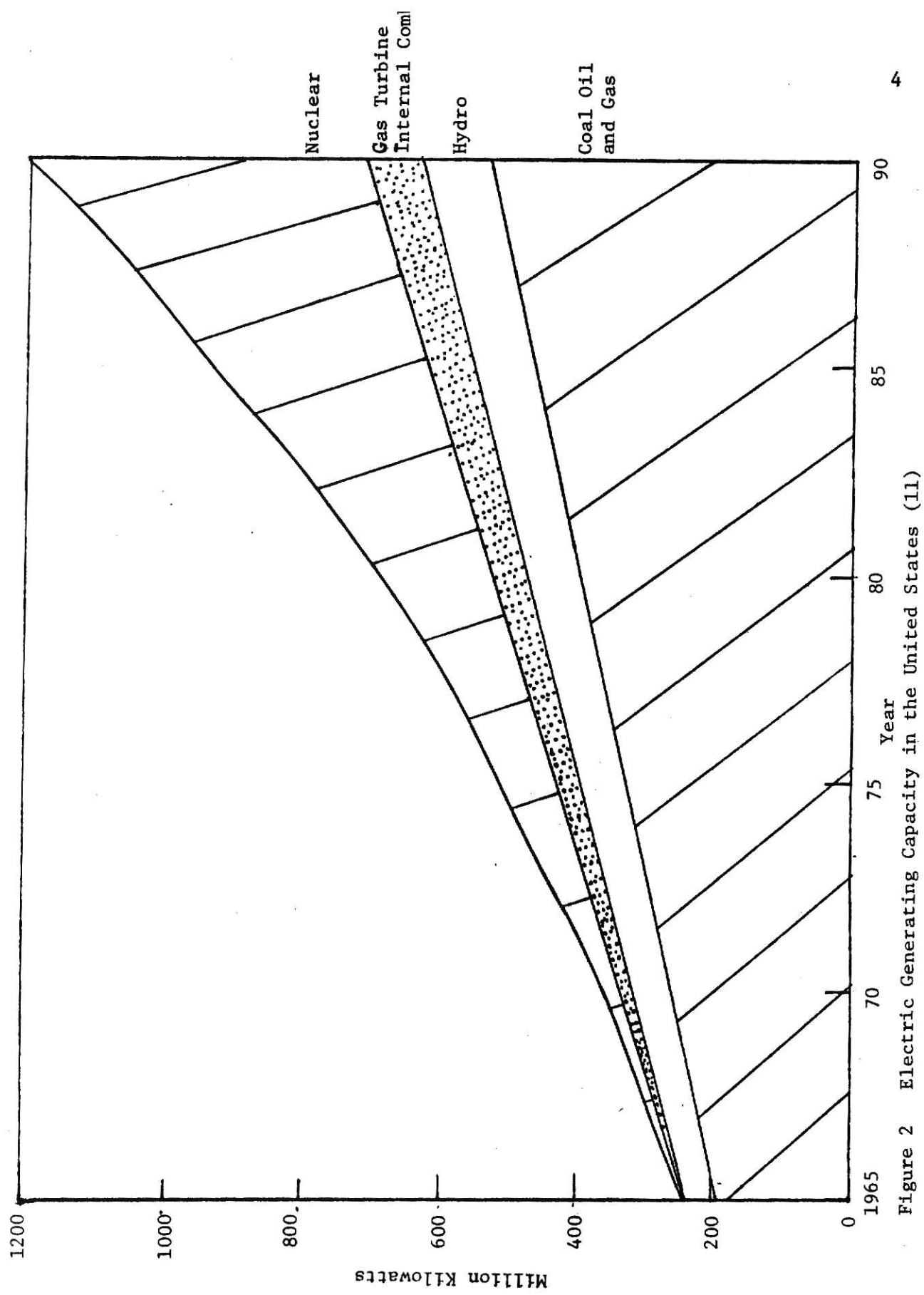
FIGURE 1 URANIUM-PLUTONIUM REACTOR FUEL CYCLE

solid wastes are produced. Currently, these wastes are stored in large underground tanks. Much consideration has been directed towards shipment of these wastes to nuclear waste burial grounds in salt or other geologic formation repositories.

In general, shipping casks are of standardized sizes at a weight allowing conventional modes of transportation shipment. A truck container may weigh between 12 to 15 tons, while a railroad container may range up to 120 tons or more. The heaviness of the casks is due almost completely to the shielding requirements. Considerable effort has been made to optimize shielding while minimizing handling costs.

It is speculated by Tremmel (1) that spent fuel transportation from the reactor to the reprocessing plant for the recovery of valuable uranium and plutonium fuels may reach such a magnitude as to hinder nuclear power industry progress. To understand this growing need for transportation, it is enlightening to examine the nuclear power industry growth. Figure 2 has become a familiar and accepted curve depicting the projected growth of the nuclear power industry (1). Not so familiar is the associated spent fuel discharge which clearly indicates an increasing need for spent fuel transportation within this decade. Figure 2 has been combined with the carrying capacity of different transportation modes to arrive at required cask movements in order to handle the anticipated transportation load, as shown in Figure 3.

Many different sizes of shipping casks may be used for different transportation modes. Presently, four transport modes seem a possibility (truck, rail, air, barge) to handle this projected load.



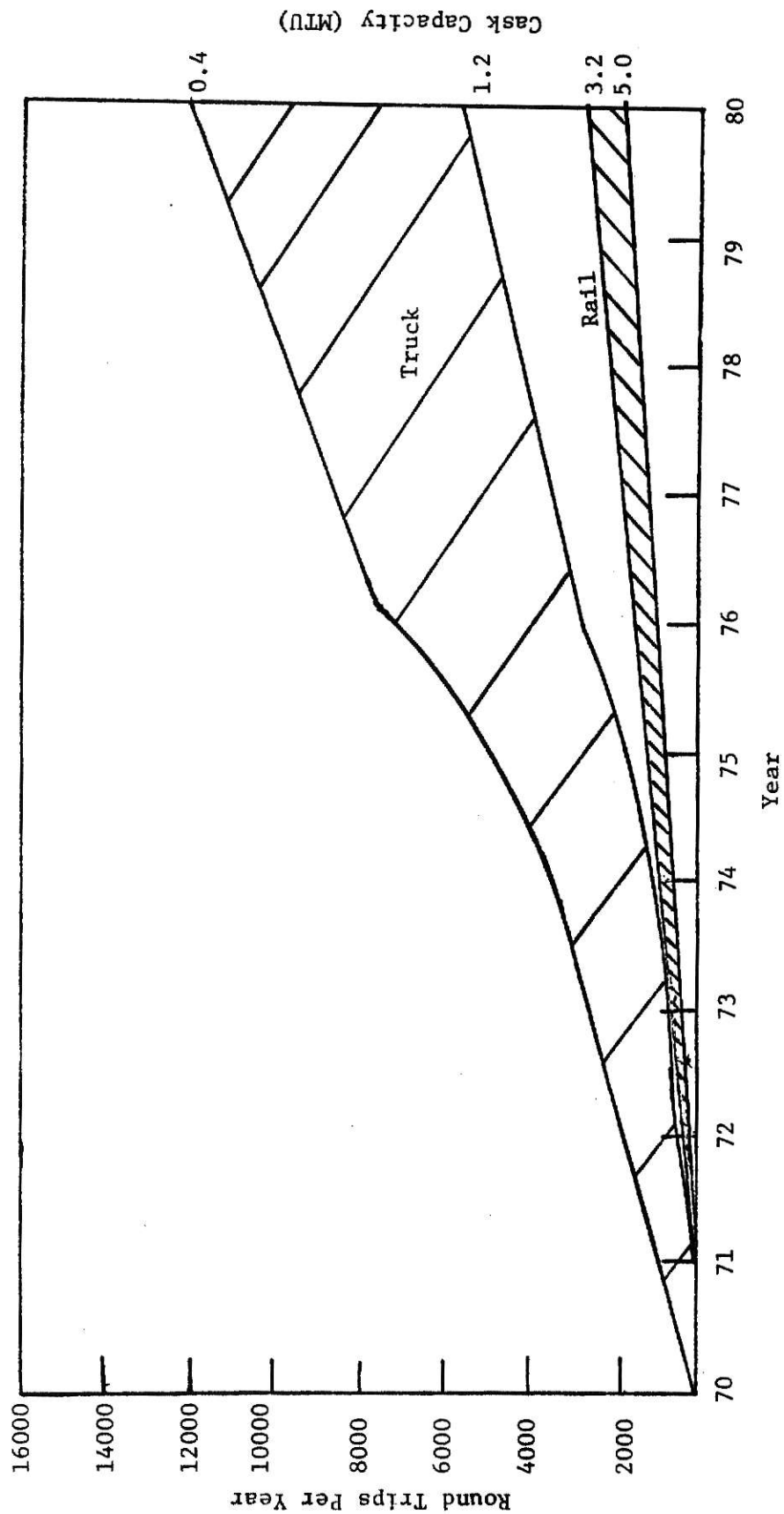


Figure 3 Required Spent Fuel Cask Movements Assuming Single Mode Shipment (1)

2.0 SHIPPING CONSTRAINTS

Associated with each mode of transportation and each reactor site are obvious factors such as accessibility of transportation, cost, weight restrictions and legal restrictions. Other not so obvious factors include safety considerations, transportation safeguards, insurance and indemnity. All these factors represent constraints on the shipment of the spent fuel. In order to understand more completely the effect that each of these constraints may have, they are examined in the following sections.

2.1 Accessibility

Accessibility may be limited at a reactor site due to geographical location of shipping and receiving facilities or mechanical capabilities of the particular reactor. For instance, some reactors do not have rail sidings necessary to ship the casks by rail. Although sidings could be constructed, often the cost of building a bridge or tunnel is prohibitive when compared with truck shipment. In addition, the cooling pond cranes are sometimes not capable of handling the heavier rail shipping casks (10).

Obviously the expense of building a canal would sometimes prohibit immediate access of barge transportation. Air runways can be built at a reasonable cost if VSTOL (Vertical and Short Take-Off and Landing) air craft ever become feasible; however, geographical terrain may eliminate the possibility of a landing strip. Also, closeness to populated districts may cause adverse public and government reaction.

2.2 Cost of Shipment

Of prime importance to the transportation considerations is cost. The cost of transportation depends not only on the mode used, but also on legal restrictions which apply along the transportation route. This problem is described by Dufrane and North (2). Taken from that paper are Figs. 4, 5, and 6 which develop a relative cost comparison for two overweight cask configurations under various highway restrictions. Freight costs have been excluded since the relative results are not affected.

Figure 4 represents the number of trips per week that could be anticipated for a cask traveling a 1000 mile trip between a power utility's reactor and the fuel reprocessor. A cask turnaround of 24 hours was assumed at both the reactor and reprocessor sites along with a 24 hour day, 7 day week operation at each end of the transportation link. Three sets of driving restrictions were considered -- 1) none 2) weekend restrictions, i.e., no travel for 48 hours over the weekend but loading and unloading operations scheduled for any time 3) night and weekend restrictions, i.e., travel 5 days at an average of 12 hours per day, but loading and unloading at any time. It can be seen from the results that at a speed of 25 miles per hour the number of trips completed per week varies between 1 and 1.9; at 36 miles per hour, the number of trips varies between 1.25 and 2.2. In both cases, the number of trips (equivalent to the amount of fuel transported) could vary by almost a factor of two.

To evaluate this effect on transportation, the anticipated cask use charges must be determined first. Figure 5 presents typical data on two casks of interest. A three PWR (pressurized water reactor) fuel assembly

500 MILE ONEWAY DISTANCE
 24 HR TURNAROUND AT UTILITY
 24 HR TURNAROUND AT REPROCESSOR
 24 HR/DAY OPERATION AT UTILITY & REPROCESSOR

| <u>Average Travel Speed</u> | <u>Driving Restrictions</u> | <u>Trips/Week</u> |
|-----------------------------|------------------------------|-------------------|
| 25 MPH | NONE | 1.91 |
| | WEEKEND RESTRICTIONS | 1.5 |
| | NIGHT & WEEKEND RESTRICTIONS | 1.0 |
| 36 MPH | NONE | 2.21 |
| | WEEKEND RESTRICTIONS | 1.66 |
| | NIGHT & WEEKEND RESTRICTIONS | 1.25 |

FIGURE 4
 TRUCK FUEL SHIPMENT STANDARD TRIP (2)

| <u>Cask Capacity</u> | <u>Weight (lbs)</u> | <u>Cask Cost</u> | <u>Cask Use Charge</u> |
|----------------------|------------------------------|------------------|--|
| (tonnes) | Loaded vehicle cask (GVW) | (dollars) | (dollars/week) Probable Range Selected for Study |
| 1.35 (3 PWR) | 105,000 | 75,000 | 500,000 3000-5000 4000 |
| 0.90 | 90,000 | 65,000 | 430,000 2500-4500 3500 |

FIGURE 5
CASK USE CHARGE APPROXIMATION (2)

STANDARD TRIP OF 500 MILES
CASK COST APPROXIMATION
EXCLUDES FREIGHT COSTS

| <u>Average Transport Speed</u> (MPH) | <u>Cask Capacity</u> (MTU) | <u>Transportation Costs</u> (dollars/MTU) |
|---|-------------------------------|--|
| | | Driving Restrictions |
| | | None Weekends Nights & Weekends |
| 25 | 1.35 | 1550 1980 2960 |
| | 0.90 | 2040 2600 3900 |
| 36 | 1.35 | 1340 1780 2370 |
| | 0.90 | 1760 2340 3110 |

FIGURE 6
SPENT FUEL TRANSPORT COST (2)

cask could carry about 1.35 tons of uranium in a 75,000 lb. cask at a gross vehicle weight of 105,000 lbs. The cask, constructed with depleted uranium to save weight, would cost approximately one-half million dollars. A smaller cask, carrying 2 PWR fuel assemblies, would weigh about 65,000 lbs providing a gross vehicle weight of 90,000 lbs. Factors such as cask capital cost, desired return on investment, estimated cask life, cask utilization factor, insurance cost, cask maintenance cost, and fleet management costs make it difficult to estimate the cask use cost. A crude estimate has been made by Dufrane and North of \$3,000 per week to \$5,000 per week for the 2 PWR fuel assembly cask. By using an average cask usage cost of \$4,000 per week and \$3,500 per week with the number of trips per week from Fig. 4, the cost per ton of spent fuel shipped can be calculated. As detailed in Fig. 6, for an average transport speed of 25 MPH, driving restrictions placed upon the 3 or 2 PWR assembly cask would cause a variation on cask transportation costs of \$1,410 and \$1,860 per ton respectively. A combination of both weight and driving restrictions would provide a total differential cost of approximately \$2,350 per ton. It is therefore, evident that, in general, shipping cost is far from fixed for a particular transportation mode.

2.3 Safety

The cost of transportation is related directly to safety. In general, the effect on cost, which would result from a transportation accident involving spent fuel, is recognized by personnel of the nuclear power industry. Aside from direct costs, indirect costs due to unfavorable public reaction are almost certain. Clearly, safety considerations have a major role in the selection of routes and modes of spent fuel transportation.

The risk involved in the shipment of radioactive materials is of growing concern. As yet this risk has not been quantified. To do so, one must recognize the many factors involved. This can be illustrated best by a simplified picture as shown in Fig. 7.

From Fig. 7 it can be seen that the risk is a function of several variables. Data for analysis of many of these variables is difficult to obtain, e.g., accident probability. Certainly one of the major parameters in risk quantification, the probability of a transportation accident may be estimated on an average basis. A detailed study of accident analysis on a cost basis was performed by Limekohler (3). Limekohler's analysis gives evidences that the probability of accident is indeed a function of the parameters indicated in Fig. 7. Table I is from the Atomic Energy Commission accident analysis report showing the number of accidents occurring by mode over a 15 year period (5). The probability of accident may be approximated by the number of accidents per mile if the number of miles traveled in those 15 years can be estimated. A rough estimate of these milages has been obtained from Dufrane and North (2). The mileages and the calculated average probability per mile appear in Table II.

The seriousness of the accident depends on the fuel material, amount of fuel, and the mode of transport. For instance, plutonium, a highly toxic and dispersable low level alpha emitter, would present a much greater potential hazard than liquid U-235 during transport. A barge accident, for example, could cause a very difficult cleanup operation, but the probability of a barge accident is quite low as shown in Table II. A table of relative seriousness of different accidents is also shown in Table II.

ILLEGIBLE DOCUMENT

**THE FOLLOWING
DOCUMENT(S) IS OF
POOR LEGIBILITY IN
THE ORIGINAL**

**THIS IS THE BEST
COPY AVAILABLE**

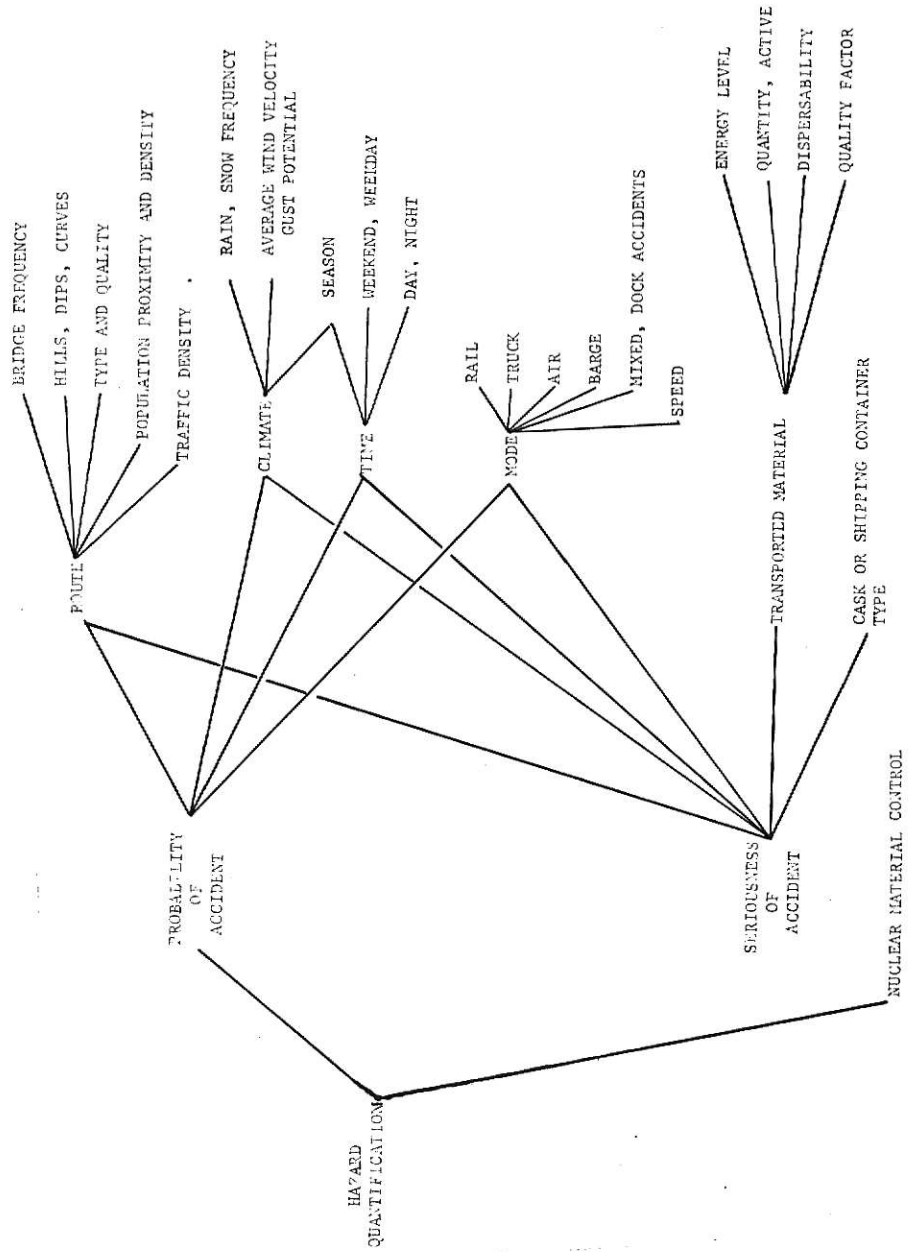


FIGURE 7 FACTORS PERTAINING TO HAZARD QUANTIFICATION

TABLE I

INCIDENT EXPERIENCE INVOLVING NUCLEAR MATERIALS BY MODE OR LOCATION (5)

| Mode | No. of Incidents | | | |
|--------------------|------------------|----------|-----------|-----------|
| | 1963-1964 | 1962 | 1957-1961 | 1949-1956 |
| Truck Incidents | 17 | 8 | 21 | 9 |
| Rail Incidents | 5 | 5 | 11 | 2 |
| Air Incidents | 0 | 0 | 0 | 1 |
| Terminal Incidents | <u>2</u> | <u>1</u> | <u>15</u> | <u>1</u> |
| Total | 24 | 14 | 47 | 13 |

TABLE II
MODE, MILES TRAVELED AND ACCIDENT CHARACTERISTICS

| | TOTAL MILES* TRAVELED 1949-1964 | PROBABILITY OF** ACCIDENT, MILE ⁻¹ | RELATIVE SERIOUSNESS OF ACCIDENT, TON ⁻¹ | |
|-------|---------------------------------------|--|--|-------------|
| TRUCK | 1,400,000 | 4.6×10^{-6} | 1000 (LWT) | 2000 (OWT) |
| RAIL | 880,000 | 7.2×10^{-6} | 1000 | |
| AIR | 64,000 | 5.1×10^{-7} | 3000 (VSTOL) | 2000 (L.A.) |
| BARGE | 11,000 | 1.0×10^{-9} | 4000 | |

*Dufrane and North (2).

**TID-16764 (5).

For the purpose of this study the relative seriousness of an accident is estimated on the basis of mode only. A more sophisticated analysis would demand data concerning the seriousness of accidents as a function of the several parameters indicated in Fig. 7.

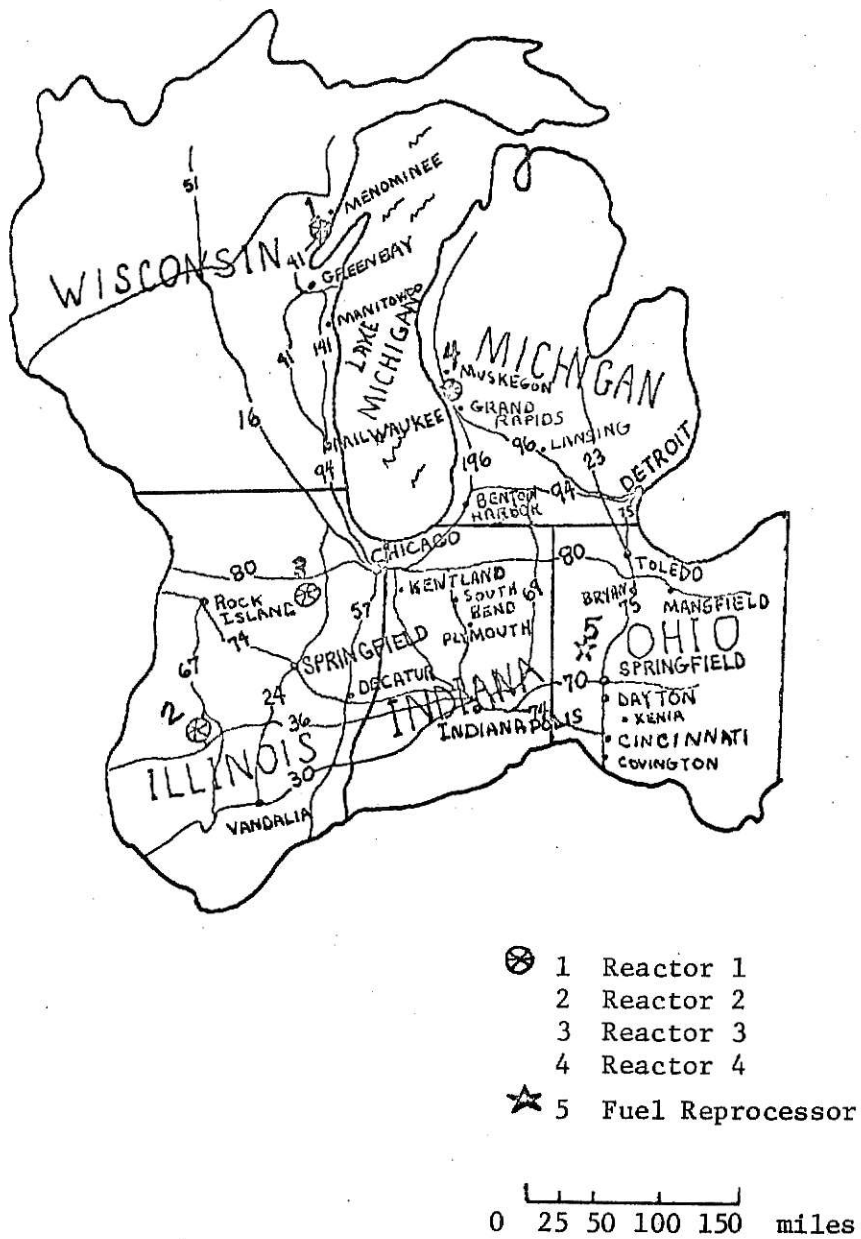


Figure 8 Major truck routes for spent fuel shipment selected by the author

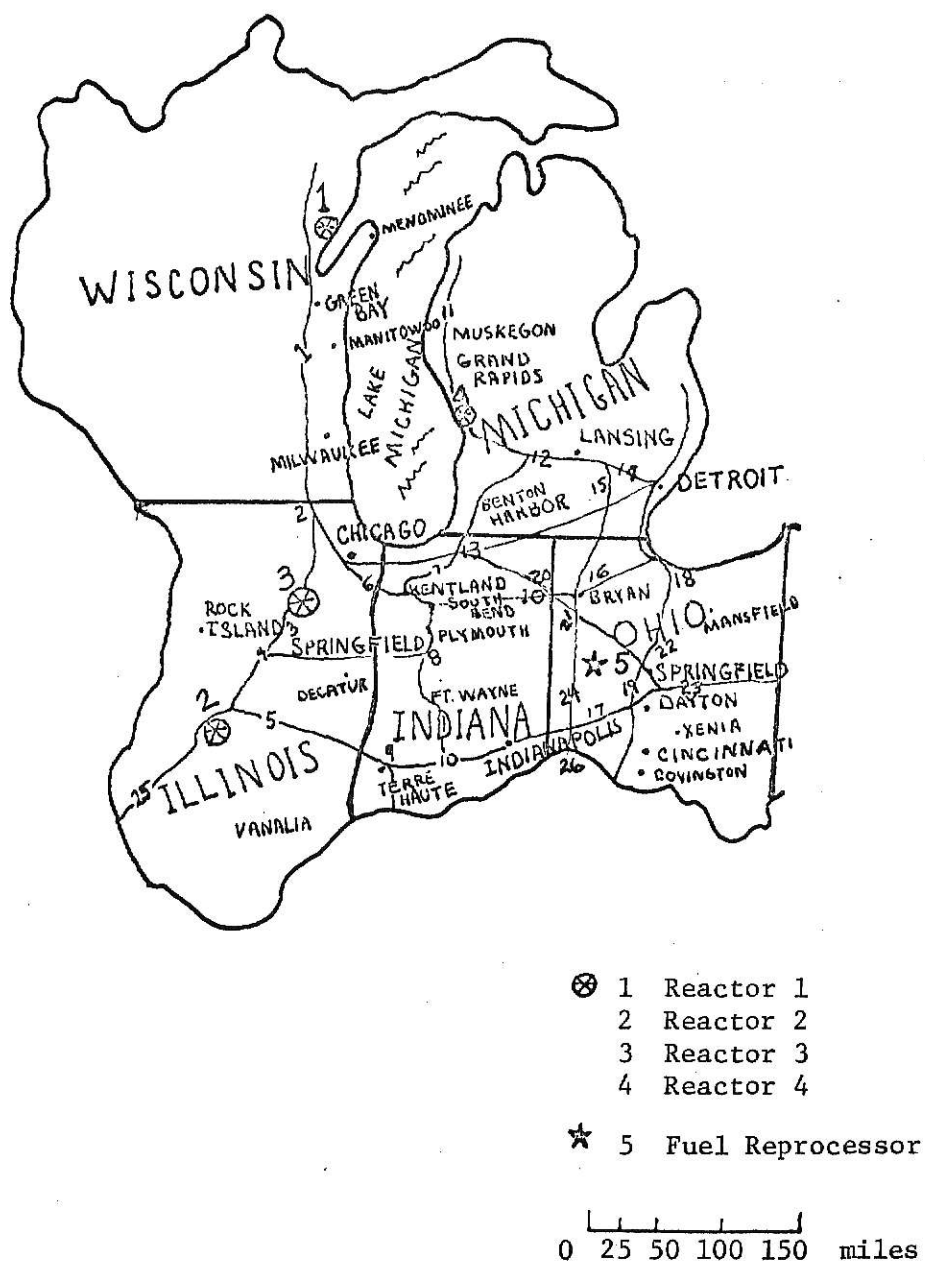


Figure 9 Major railroads for spent fuel shipment selected by the author

3.0 MODEL DESCRIPTION

The model developed in this work considers 4 different reactor locations and one spent fuel reprocessor. These plants and the reprocessor are shown along with the major highways and railroads in Figs. 8 and 9, respectively. Four modes are considered -- truck, rail, air, and barge. The possibility of mixed mode is also considered in the route candidates. The objective of the problem was to minimize the cost of transporting a representative amount of spent fuel from hypothetical reactor plants, Reactor 1, Reactor 2, Reactor 3, and Reactor 4 to the fuel reprocessor at a risk below a specified hazard level. The amount of spent fuel shipment for Point Beach 2, Dresden 2, Zion and Palisades reactors, for 1973, was estimated by Tremmel and Berte (1):

| | |
|---------------|-----------------------|
| Point Beach 2 | 16 Tons of spent fuel |
| Dresden 2 | 42 Tons |
| Zion | 28 Tons |
| Palisades | 28 Tons |

These amounts are used as representative for hypothetical reactors 1, 2, 3, and 4 respectively since their geographical locations are similar. The optimization of this model can be handled by linear programming methods as shown in the following sections.

3.1 Linear Programming

In general, a linear programming (LP) problem can be defined as a system of linear equations which represents constraints on an objective function. This objective function is to be maximized or minimized (7). In mathematical terms the LP problem may be stated as follows:

Find values of the variables x_1, x_2, \dots, x_n which satisfy the inequalities

$$\begin{array}{l} a_{11}x_1 + a_{12}x_2 + \dots + a_{1n}x_n \quad [\geq \text{ or } \leq] \quad b_1 \\ \vdots \\ a_{p1}x_1 + a_{p2}x_2 + \dots + a_{pn}x_n \quad [\geq \text{ or } \leq] \quad b_N \end{array}$$

where x_1, x_2, \dots, x_N all are greater than or equal to zero, such that

$$z = c_1x_1 + c_2x_2 + \dots + c_Nx_N$$

is a maximum or minimum. The a_{ij} 's, b 's, and c 's are known.

An example of a simple linear programming problem will help to clarify the technique. Consider a nuclear reactor which must ship its spent fuel to a reprocessor. There are two modes of transportation available for the shipment under consideration ... truck and rail. Necessary information is:

1. 12 tons of spent fuel to be shipped
2. Costs of shipment are \$38 and \$45 per ton for truck and rail respectively
3. Relative risk indices are 0.2 and 0.4 per ton for truck and rail respectively
4. An upper limit of relative risk index is set at 0.3 per ton

The problem is to minimize the cost of shipment of 12 tons of spent fuel while keeping the relative risk index below 0.3 per ton.

This model may be formulated as follows.

Let x_1 denote the number of tons of spent fuel shipped by truck
 x_2 denote the number of tons of spent fuel shipped by rail

Then the objective is to minimize the cost

$$z = 38x_1 + 45x_2$$

subject to

$$x_1 + x_2 \geq 12 \quad \text{Demand shipment constraint} \quad (1)$$

$$\frac{0.2x_1 + 0.4x_2}{x_1 + x_2} \leq 0.3 \quad \text{Risk index constraint} \quad (2)$$

It was assumed that a "mixed" risk index may be represented as a weighted average of risk indices for x_1 and x_2 . If Eq. (2) is multiplied by (x_1+x_2) and the x 's are collected on the left hand side, Eq. (2) can be rewritten as

$$-0.1 x_1 + 0.1 x_2 \leq 0 \quad (2.1)$$

Graphical representation of the problem leads to a simple solution as illustrated in Fig. 10. The shaded regions represent the feasible regions allowed by constraints (1) and (2.1). Line 2.1 and Line 1 correspond to Eq. (2.1) and Eq. (1). Thus the doubly shaded region is the feasibility region for the solution. Suppose $z=17$, then a line may be constructed which contains all points x_1 and x_2 which yield this cost value. Notice that all cost lines are parallel to this line since only z will change, not the variable coefficients. Then by moving this "equi-cost" line outward toward the feasibility region, the minimum value of z which will satisfy both constraints exists at the intersection of lines (1) and the x_1 -axis. This point is

$$x_1 = 12, x_2 = 0$$

and the total cost is

$$z = 38(12) + 45(0) \text{ or } \$456 .$$

More complex LP problems can be solved by using computer programs such as IBM's Mathematical Programming System (MPS)/360 (8).

MPS/360 is composed of a set of procedures, a subset of which deals with LP. These LP procedures use the bounded variable/product form of the inverse revised simplex method (8). The simplex method is based on the fact that if there are m constraints (or rows) in the constraint matrix which are linearly dependent, then there is a set of m columns (variables or

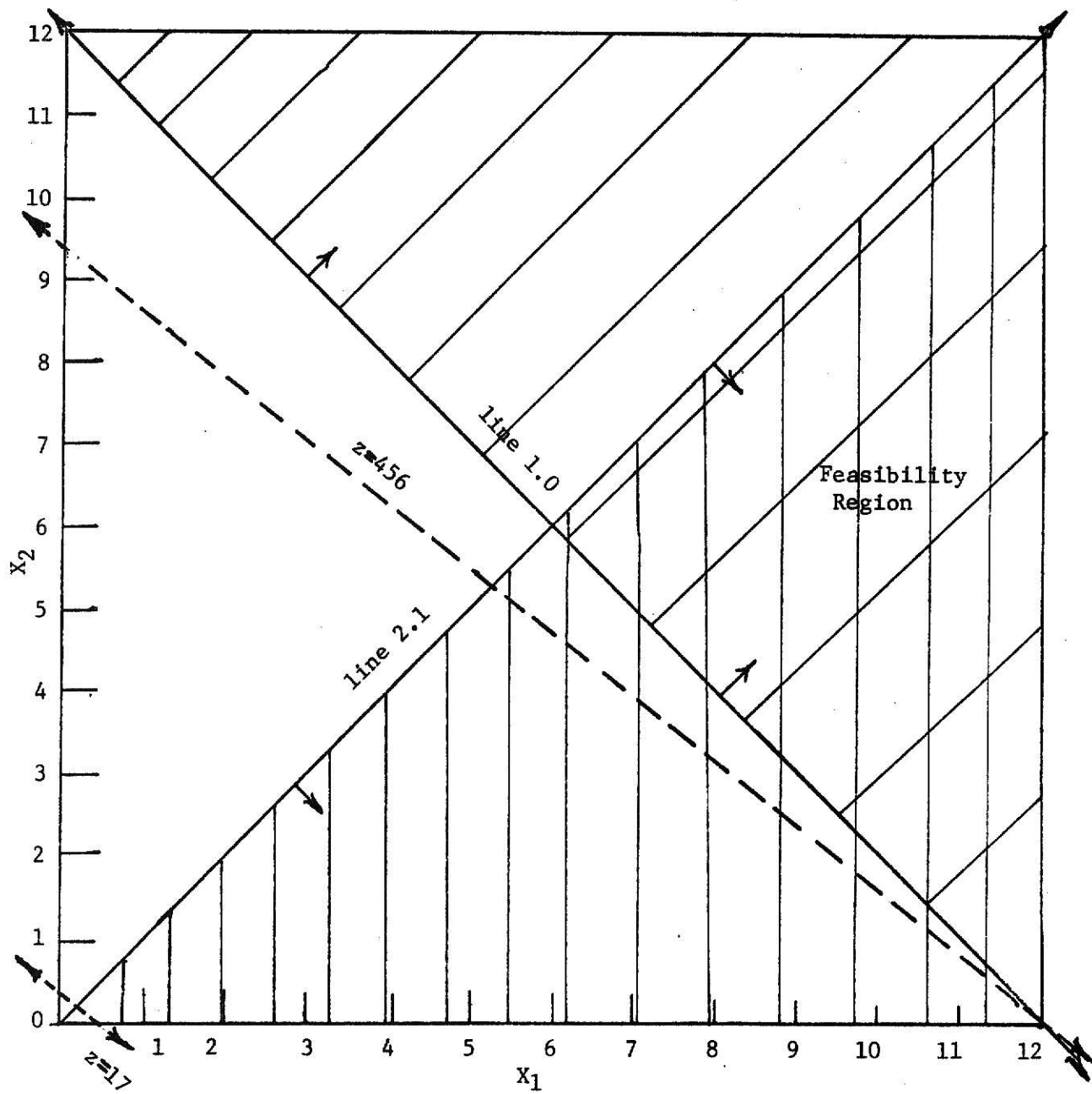


Figure 10 Linear Programming Solution to Example Problem

vectors) which are linearly independent and form a so called basic solution. That is, the right hand side (RHS) of the problem formation can be expressed as a linear combination of the m columns in the basis. The MPS/360 program systematically exchanges the column vectors according to the revised simplex method until an optimal solution is reached (8). Short notes which explain the control cards needed follow (9).

SHORT NOTES ON MPS COMPUTER PROGRAM

PROGRAM. PROGRAM is a mandatory statement at the beginning of each program.

INITIALIZE. INITIALIZE is used to establish initial settings for tolerance, frequencies and demands. This is a system macro instruction.

TITLE ('EXAMPLE'). This statement is used to suitably name the problem.

MOVE (XDATA, 'EXAMPLE') and MOVE (XPBNAME, 'PBFILE'). The first statement moves input data set name EXAMPLE into the cell XDATA. The second moves the problem file name, PBFILE, into the cell XPBNAME.

CONVERT. This routine is the master control card of the convert procedure, which is used to convert external input data into a binary form and transfers these data to PBFILE.

SETUP ('MAX'). This routine is the master control card of the setup procedure, which is used to set up the problem name in XPBNAME by

1. searching for the problem,
2. opening the matrix, eta, and scratch files,
3. making the storage allocation,
4. building the work matrix,
5. setting the logical basis and structural bounded variables at the upper bound, and
6. building the inverse of the logical basis.

For minimization 'MAX' should be changed to 'MIN'.

BCDOUT. This converts the specified binary problem into the external input data format. The output may be listed and/or punched out and is in the order of the input data sections, ROWS, COLUMNS, RHS, RANGES, and BOUNDS. The NAME and ENDATA cards may also be produced.

MOVE (XOBJ, 'PROFIT') and MOVE (XRHS, 'LIMITS'). These statements are for identifying the objective function and the right hand side limits. For minimizing, 'PROFIT' becomes 'COST'. Objective function and right hand side have to be named because a program can work with many objective functions and limits.

PICTURE. The PICTURE procedure produces a "picture" of the current work matrix in condensed format. Up to 45 rows and 55 columns for an output page are given. The pages are numbered using matrix notation for ease of identification. The output of PICTURE gives a quick visual check to see if the structure of the matrix is correct and if any coefficients are missing.

The range on the problem right hand side, and bounds on the variables are indicated if they exist.

PRIMAL. Primal optimizes the current problem using a composite primal algorithm. It can work with a composite objective function and/or a composite right hand side. It can work with a composite restraint row if neither the objective function nor the right hand side is composite.

SOLUTION. Solution is the output of a summary of the solution corresponding to the current basis. This output may be either printed or filed depending on a parameter in the procedure card.

EXIT. Exit is a procedure linked by the executor before return to the operating system. It is mainly used to close data sets and print the time of the executor job step.

PEND. This is equivalent to the END statement in FORTRAN.

3.2 Mathematical Formulation

To formulate the model in mathematical terms, it is necessary to define the following quantities:

- x_{ij} the number of ton-miles of spent fuel sent by mode i on route j
- c_i the relative cost per ton-mile of shipment by mode i
- d_k the demand of tons of spent fuel needed to be shipped from reactor k
- P_{ij} the associated hazard of transportation of spent fuel by mode i along route j per ton-mile

The objective is to minimize the cost of transport which may be written as

$$z = \sum_{ij} c_i x_{ij} \quad i = 1, \dots, 6 \quad j = 1, \dots, 32$$

where c_i is speculated to correspond to the following values for $i = 1$ through 6:

| | | |
|-------|--------------------|----------------------------|
| c_1 | Legal Weight Truck | 1.0 unit cost per ton-mile |
| c_2 | Over Weight Truck | 1.9 unit cost per ton-mile |
| c_3 | Barge | 2.7 unit cost per ton-mile |
| c_4 | VSTOL Aircraft | 2.5 unit cost per ton-mile |
| c_5 | Large Aircraft | 2.2 unit cost per ton-mile |
| c_6 | Railroad | 1.2 unit cost per ton-mile |

Table III lists the routes and modes.

TABLE III. VARIABLE DESCRIPTION

| x_{ij} | Plant | Mode | Route | Total Miles |
|------------|-----------|-------|-------------------------------|-------------|
| $x_{1,1}$ | Reactor 1 | LWT | 41-141-94-80-75-70 | 620 |
| $x_{2,1}$ | | OWT | 41-141-94-80-75-70 | 620 |
| $x_{4,2}$ | | VSTOL | ----- | 410 |
| $x_{5,2}$ | | L.A. | ----- | 410 |
| $x_{3,3}$ | | BARGE | To Grand Rapids - Truck | 250 |
| $x_{1,3}$ | | LWT | Grand Rapids -96-75-70 | 390 |
| $x_{2,3}$ | | OWT | Grand Rapids -96-75-70 | 390 |
| $x_{3,4}$ | | BARGE | Grand Rapids - Truck | 250 |
| $x_{1,4}$ | | LWT | Grand Rapids -196-94-23-75-70 | 420 |
| $x_{2,4}$ | | OWT | Grand Rapids -196-94-23-75-70 | 420 |
| $x_{3,5}$ | | BARGE | Grand Rapids - Truck | 250 |
| $x_{1,5}$ | | LWT | Grand Rapids -96-33-75-70 | 350 |
| $x_{2,5}$ | | OWT | Grand Rapids -96-33-75-70 | 350 |
| $x_{1,6}$ | | LWT | Grand Rapids -196-94-23-70 | 330 |
| $x_{2,6}$ | | OWT | Grand Rapids -196-94-23-70 | 330 |
| $x_{3,6}$ | | BARGE | Grand Rapids - Truck | 250 |
| $x_{6,22}$ | | RAIL | 1-2-6-13-20-21-24 | 500 |
| $x_{6,23}$ | | RAIL | 1-2-6-7-8-20-21-24 | 520 |
| $x_{6,24}$ | | RAIL | Barge -11-14-24 | 480 |
| $x_{3,24}$ | | BARGE | Rail | 120 |
| $x_{6,25}$ | | RAIL | 1-2-3-7-8-20-21-24 | 500 |
| $x_{1,7}$ | Reactor 2 | LWT | 36-94-70 | 400 |
| $x_{2,7}$ | | OWT | 36-94-70 | 400 |
| $x_{1,8}$ | | LWT | 36-Barge-75-70 | 400 |
| $x_{2,8}$ | | OWT | 36-Barge-75-70 | 400 |
| $x_{3,8}$ | | BARGE | Truck-Barge-Truck | 440 |
| $x_{4,9}$ | | VSTOL | ----- | 300 |
| $x_{5,9}$ | | L.A. | ----- | 300 |
| $x_{6,26}$ | | RAIL | 5-9-10-17-24 | 400 |
| $x_{6,27}$ | | RAIL | 5-4-8-20-21-24 | 400 |
| $x_{6,28}$ | | RAIL | 5-24-Barge-26-34 | 230 |
| $x_{3,28}$ | | BARGE | Rail-Barge-Rail | 300 |

| x_{ij} | Plant | Mode | Route | Total Miles |
|------------|-----------|-------|----------------------|-------------|
| $x_{1,10}$ | Reactor 3 | LWT | 80-75-70 | 420 |
| $x_{2,10}$ | | OWT | 80-75-70 | 420 |
| $x_{1,11}$ | | LWT | 8-57-74-70 | 400 |
| $x_{2,11}$ | | OWT | 8-57-74-70 | 400 |
| $x_{1,12}$ | | LWT | 80-69-70 | 450 |
| $x_{2,12}$ | | LWT | 80-69-70 | 450 |
| $x_{1,13}$ | | LWT | 80-24-74-70 | 360 |
| $x_{2,13}$ | | OWT | 80-24-74-70 | 360 |
| $x_{1,14}$ | | LWT | 24-70-57-Barge-75-70 | 350 |
| $x_{2,14}$ | | OWT | Truck-Barge-Truck | 350 |
| $x_{3,14}$ | | BARGE | Truck-Barge-Truck | 250 |
| $x_{1,15}$ | | LWT | 80-57-Barge-75-70 | 300 |
| $x_{2,15}$ | | OWT | 80-57-Barge-75-70 | 300 |
| $x_{3,15}$ | | BARGE | Truck-Barge-Truck | 250 |
| $x_{4,40}$ | | VSTOL | ----- | 210 |
| $x_{5,40}$ | | L.A. | ----- | 210 |
| $x_{6,29}$ | | RAIL | 3-7-8-20-21-24 | 410 |
| $x_{6,30}$ | | RAIL | 3-5-9-10-17-24 | 450 |
| $x_{1,16}$ | Reactor 4 | LWT | 96-23-75-70 | 390 |
| $x_{2,16}$ | | OWT | 96-23-75-70 | 390 |
| $x_{1,17}$ | | LWT | 196-23-15-70 | 420 |
| $x_{2,17}$ | | OWT | 196-23-75-70 | 420 |
| $x_{1,18}$ | | LWT | 96-23-75-70 | 350 |
| $x_{2,18}$ | | OWT | 96-23-75-70 | 350 |
| $x_{1,19}$ | | LWT | 196-94-23-70 | 330 |
| $x_{2,19}$ | | OWT | 196-94-23-70 | 330 |
| $x_{1,20}$ | | LWT | Barge-80-75-70 | 290 |
| $x_{2,20}$ | | OWT | Barge-80-75-70 | 290 |
| $x_{3,20}$ | | BARGE | Barge-Truck | 150 |
| $x_{6,31}$ | | RAIL | 12-14-15-24 | 250 |
| $x_{6,32}$ | | RAIL | 12-13-20-21-24 | 380 |

The amount of spent fuel transported from each reactor must be at least as large as the previously mentioned representative demand. This may be formulated as follows:

$$\sum_{j(k)} x_{ij} / (\text{total miles})_j \geq d_k$$

where corresponds to

| | | |
|-------|-----------|-------------|
| k = 1 | Reactor 1 | j = 1 to 10 |
| 2 | Reactor 2 | 11 to 16 |
| 3 | Reactor 3 | 17 to 25 |
| 4 | Reactor 4 | 26 to 32 |

When a mixed transport mode situation exists for a given route j, the quantity of spent fuel which is shipped on both modes is constant. For instance, route 4 involves shipment by barge for 250 miles and then truck for 420 miles. Therefore, in this case, the amount shipped by OWT and LWT must equal the amount shipped by barge, or

$$x_{1,4}/420 + x_{2,4}/420 = x_{3,4}/250 \quad .$$

Similar cases exist for other bi-modal routes.

In order to formulate restrictions on transportation due to risk consideration, it is necessary to discuss the parameters involved in quantification of risk. As shown in Fig. 7 risk depends on many factors. Of major importance among all these factors are probability of accident, severity of accident, and the population density near an accident. The major risk involved is that of overexposing a person to radioactive material. Although such variables as type of radioactive material, climate, time of day, etc. are important, for the purposes of this work the risk evaluation was limited to consideration only of the three factors: probability of accident, severity of accident, and potential population near an accident. For the purposes of this work, risk was assumed to be modeled by the following equation:

$$P_{ij} = (\text{Risk})_{ij} = \sum_{\text{All Cities}} \left\{ \frac{(\text{Population of City})}{(\text{Total Distance})(\text{Distance from Route to City})^2} \right. \\ \left. (\text{SA})(\text{PA}) + (0.001)(\text{SA}) \right\} \quad \text{for each route and mode}$$

where

SA is the severity of accident per ton of fuel, and

PA is probability of accident per mile for mode i.

Again, the probability of accident shown in Table II has been calculated from accident reports taken from (5) and are obtained by averaging the number of accidents per mile calculated from Table I. The relative severity of accident is an estimate of the characteristics of each mode arrived at using general considerations such as average speed traveled, damage upon typical accident, and amount of cargo transported. Clearly, a more detailed analysis of seriousness of accident would be required for a more sophisticated model.

An example of the calculation of risk of route 1, legal weight truck from Reactor 1 to the fuel reprocessor along route 41-141-94-80-75-70, appears below. A list of the cities exposed to this route, their population, and the closest distance of that city to route 1 is tabulated in Table IV. This information was used as input to the risk formula along with the seriousness of accident and probability of accident by truck from Table II. The result is a risk index of 0.736 per ton mile. Similarly, the risks of all routes concerned with Reactor 1 were calculated. Thus the risk associated with each route was multiplied by the number of ton-miles (x_{ij}) attributed to this route and the weighted average was restricted to be less than some predetermined upper limit of risk. The upper limit criterion can be set arbitrarily or by the best available information. For the purposes of this work, it was arrived at by assuming the following allowable values of the parameters:

Table IV
Route 1 HAZARD QUANTIFICATION DATA

| CITY | POPULATION | (CLOSEST DISTANCE) ² |
|-------------------|------------|---------------------------------|
| MENOMINEE, WISC. | 8,600 | 1 |
| GREENBAY, WISC. | 82,500 | 1.25 |
| MANITOWOC, WISC. | 32,200 | 4 |
| MILWAUKEE, WISC. | 765,000 | 1 |
| CHICAGO, ILL. | 3,520,000 | 2.25 |
| KENTLAND, IND. | 1,780 | 625 |
| SOUTH BEND, INC. | 135,000 | 25 |
| PLYMOUTH, IND. | 7,300 | 900 |
| BRYAN, OHIO | 7,800 | 4 |
| TOLEDO, OHIO | 354,000 | 625 |
| MANSFIELD, OHIO | 49,000 | 400 |
| SPRINGFIELD, OHIO | 82,500 | 2 |
| DAYTON, OHIO | 260,000 | 400 |

| | |
|-----------------------------|-----------|
| 1 city exposed to the route | |
| population | 1,000,000 |
| closest distance | 1 mile |
| total distance | 400 miles |
| seriousness of accident | 2000 |
| probability of accident | 0.0000001 |

Therefore;

upper limit = UL

$$= \frac{1,000,000}{400} (2000(10^{-7}) + 2(10^{-5}))$$

$$= 0.5 \text{ ton}^{-1} \text{ mile}^{-1}$$

Then the risk constraint for a particular reactor can be written as:

$$\frac{\sum_{i=1}^6 \sum_{j=k_1}^{k_2} P_{ij} X_{ij}}{\sum_{i=1}^6 \sum_{j=k_1}^{k_2} X_{ij}} \leq \text{UL}$$

where k_1 is the first numbered route servicing reactor k

k_2 is the last numbered route servicing reactor k

The four risk constraints, the four demand constraints, and the mixed mode constraints are summarized in Fig. 11. This matrix serves as the input matrix to be optimized by the revised simplex LP method. The MPS/360 was used to find the optimal solution and the printout is displayed in appendix A.

3.3 Results and Conclusions

The optimal solution is displayed on page 11 of the computer output, Appendix A. As indicated, the lowest cost possible incurred in shipping the demanded fuel and satisfying the risk criterion is 48152.00720 cost units. The unit cost corresponds to that of a legal weight truck. It is estimated that the cost per ton-mile for a legal weight truck is \$0.38.

| ROW | COLUMN | COST | | | | | | | | | | | | | | |
|-----|---------------------|------|---|------|------|------|------|------|------|------|------|------|------|------|------|------|
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| 1 | REACTOR 2 | 1 | 1 | 1.51 | 1.51 | 1.59 | 1.59 | 1.59 | 1.59 | 1.48 | 1.48 | 1.48 | 1.77 | 1.77 | 1.87 | 1.87 |
| 2 | MIXED MODE ROUTE 3 | | | | | | | | | | | | | | | |
| 3 | MIXED MODE ROUTE 4 | | | | | | | | | | | | | | | |
| 4 | MIXED MODE ROUTE 5 | | | | | | | | | | | | | | | |
| 5 | MIXED MODE ROUTE 6 | | | | | | | | | | | | | | | |
| 6 | MIXED MODE ROUTE 24 | | | | | | | | | | | | | | | |
| 7 | REACTOR 2 | | | | | | | | | | | | | | | |
| 8 | MIXED MODE ROUTE 8 | | | | | | | | | | | | | | | |
| 9 | MIXED MODE ROUTE 28 | | | | | | | | | | | | | | | |
| 10 | REACTOR 3 | | | | | | | | | | | | | | | |
| 11 | MIXED MODE ROUTE 14 | | | | | | | | | | | | | | | |
| 12 | MIXED MODE ROUTE 15 | | | | | | | | | | | | | | | |
| 13 | REACTOR 4 | | | | | | | | | | | | | | | |
| 14 | MIXED MODE ROUTE 20 | | | | | | | | | | | | | | | |
| 15 | RISK REACTOR 1 | | | | | | | | | | | | | | | |
| 16 | RISK REACTOR 2 | | | | | | | | | | | | | | | |
| 17 | RISK REACTOR 3 | | | | | | | | | | | | | | | |
| 18 | RISK REACTOR 4 | | | | | | | | | | | | | | | |

FIGURE 11 LINEAR PROGRAMMING CONSTRAINT MATRIX

| ROW | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 |
|-----|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 1 | X _{3,6} | X _{6,22} | X _{6,23} | X _{6,24} | X _{6,25} | X _{3,24} | X _{1,7} | X _{1,7} | X _{1,8} | X _{2,8} | X _{3,8} | X _{5,9} | X _{4,9} | X _{6,26} | X _{6,27} | X _{6,28} | X _{3,28} | X _{1,10} |
| 2 | 2.7 | 1.2 | 1.2 | 1.2 | 1.2 | 2.7 | 1.0 | 1.9 | 1.0 | 1.9 | 2.7 | 2.2 | 2.5 | 1.2 | 1.2 | 1.2 | 2.7 | 1.0 |
| 3 | | | | | | | | | | | | | | | | | | |
| 4 | | | | | | | | | | | | | | | | | | |
| 5 | -2.48 | | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | | | | | | | | | | | |
| 7 | | | | | | | 1.0 | 1.0 | 2.22 | 2.22 | | 1.33 | 1.33 | 1.0 | 1.0 | 1.79 | | |
| 8 | | | | | | | | | 2.22 | 2.22 | -91 | | | | | | | |
| 9 | | | | | | | | | | | | | | | | -1.74 | 1.35 | |
| 10 | | | | | | | | | | | | | | | | | | 1.0 |
| 11 | | | | | | | | | | | | | | | | | | |
| 12 | | | | | | | | | | | | | | | | | | |
| 13 | | | | | | | | | | | | | | | | | | |
| 14 | | | | | | | | | | | | | | | | | | |
| 15 | -462 | .87 | .92 | -.45 | -.282 | -.324 | | | | | | | | | | | | |
| 16 | | | | | | | -.288 | -.08 | .116 | .834 | -.49 | -.47 | -.48 | .305 | -.37 | -.45 | -.49 | |
| 17 | | | | | | | | | | | | | | | | | | .89 |
| 18 | | | | | | | | | | | | | | | | | | |

FIGURE 11 (CONT'D)

| ROW | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 |
|-----|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | X _{2,10} | X _{1,11} | X _{2,12} | X _{2,12} | X _{1,12} | X _{2,13} | X _{1,13} | X _{1,14} | X _{2,14} | X _{3,14} | X _{1,15} | X _{2,15} | X _{3,15} | X _{4,40} | X _{5,40} | X _{6,29} | X _{6,30} | X _{1,16} |
| 1 | 1.9 | 1.0 | 1.9 | 1.9 | 1.0 | 1.9 | 1.0 | 1.0 | 1.9 | 2.7 | 1.0 | 1.9 | 2.7 | 2.5 | 2.2 | 1.2 | 1.2 | 1.0 |
| 2 | | | | | | | | | | | | | | | | | | |
| 3 | | | | | | | | | | | | | | | | | | |
| 4 | | | | | | | | | | | | | | | | | | |
| 5 | | | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | | | | | | | | | | | |
| 8 | | | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | | | | | | | | | | | |
| 10 | 1.0 | 1.25 | 1.05 | .935 | .935 | 1.17 | 1.17 | 1.2 | 1.2 | 1.2 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.02 | .935 | |
| 11 | | | | | | | | 1.2 | 1.2 | -1.3 | | | | | | | | |
| 12 | | | | | | | | | | | 1.4 | 1.4 | -1.68 | | | | | 1.0 |
| 13 | | | | | | | | | | | | | | | | | | |
| 14 | | | | | | | | | | | | | | | | | | |
| 15 | | | | | | | | | | | | | | | | | | |
| 16 | | | | | | | | | | | | | | | | | | |
| 17 | 2.2 | .15 | 2.8 | .94 | 2.5 | .16 | .82 | -.16 | .19 | -.49 | 1.5 | 3.5 | -.49 | -.43 | -.43 | -.37 | -.33 | |
| 18 | | | | | | | | | | | | | | | | | | -.46 |

FIGURE 11 (CONT'D)

| ROW | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | |
|-----|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|---------------|
| | $X_{2,16}$ | $X_{1,17}$ | $X_{2,17}$ | $X_{2,18}$ | $X_{1,18}$ | $X_{1,19}$ | $X_{1,10}$ | $X_{1,20}$ | $X_{2,20}$ | $X_{3,20}$ | $X_{6,31}$ | $X_{6,32}$ | |
| 1 | 1.9 | 1.0 | 1.9 | 1.0 | 1.9 | 1.0 | 1.9 | 1.0 | 1.9 | 2.7 | 1.2 | 1.2 | $\geq 9,900$ |
| 2 | | | | | | | | | | | | | = 0 |
| 3 | | | | | | | | | | | | | = 0 |
| 4 | | | | | | | | | | | | | = 0 |
| 5 | | | | | | | | | | | | | = 0 |
| 6 | | | | | | | | | | | | | = 0 |
| 7 | | | | | | | | | | | | | $\geq 16,800$ |
| 8 | | | | | | | | | | | | | = 0 |
| 9 | | | | | | | | | | | | | = 0 |
| 10 | | | | | | | | | | | | | $\geq 11,750$ |
| 11 | | | | | | | | | | | | | = 0 |
| 12 | | | | | | | | | | | | | = 0 |
| 13 | 1.0 | .93 | .93 | 1.1 | 1.1 | 1.18 | 1.18 | 1.34 | 1.34 | 1.34 | 1.21 | 1.11 | $\geq 10,900$ |
| 14 | | | | | | | | 1.34 | 1.34 | -.28 | | | = 0 |
| 15 | | | | | | | | | | | | | ≤ 0 |
| 16 | | | | | | | | | | | | | ≤ 0 |
| 17 | | | | | | | | | | | | | ≤ 0 |
| 18 | -.43 | -.47 | -.45 | -.46 | -.43 | -.46 | -.42 | 1.8 | 4.1 | -.49 | -.48 | -.47 | ≤ 0 |

FIGURE 11 (CONT'D)

The cost in dollars is calculated as $(48152.00720)(.38)$ and is approximately equal to \$18,297.00. This cost does not include the cost of shipping cask indemnity or insurance. It was assumed that consideration of these additional costs would simply add on additional cost in the final analysis and would not affect the choice of optimal routes. For a more detailed examination of the problem, these additional costs could be included.

The amount that should be shipped on a particular route is obtained from pages 13 and 14 of the computer output, appendix A. The values listed are the number of ton-miles attributed to shipment on a given route by a given mode. The amount of spent fuel shipped along a route is calculated by dividing the ton-miles by the distance that the spent fuel is shipped on the route by a given mode. For instance, Column 20 corresponds to $x_{6,25}$. The computer output indicates 1983.87 ton-miles associated with shipment on route 25 by train. The total distance traveled by the train on route 25 is 500 miles; therefore, the amount of spent fuel shipped is $1983.87/500 = 3.97$ tons. A summary of all the amounts shipped by various routes and modes appears in Table V.

As mentioned previously, many of the quantities used in the calculations of risk, seriousness of accident, and cost require more detailed study. In addition, some of these quantities are not fixed. For instance, cost of transport is regionally and seasonally dependent. Cost is also subject to negotiation and is by no means fixed. It was, however, hypothesized that a given reactor facility will be able to arrive at many of these quantities accurately and then may apply this procedure realistically. In addition to economic aspects of nuclear transport, the personnel of the nuclear

Table V
Shipping Routes and Quantities for the Model

| REACTOR | VARIABLE | AMOUNT TON-MILES | ROUTE TOTAL MILES | AMOUNT TONS | MODE | ROUTE |
|-----------|------------|---------------------|----------------------|----------------|------|--------------------|
| Reactor 1 | $X_{6,25}$ | 7,983 | 500 | 16 | RAIL | 1-2-3-7-8-20-21-24 |
| Reactor 2 | $X_{1,7}$ | 16,800 | 400 | 42 | LWT | 36-94-70 |
| Reactor 3 | $X_{1,13}$ | 3,425 | 360 | 9.5 | LWT | 80-24-74-70 |
| Reactor 3 | $X_{6,29}$ | 7,590 | 410 | 18.5 | RAIL | 3-7-8-20-21-24 |
| Reactor 4 | $X_{1,18}$ | 4,681 | 350 | 13.5 | LWT | 96-23-75-70 |
| Reactor 4 | $X_{1,19}$ | 4,793 | 330 | 14.5 | LWT | 196-94-23-70 |

industry are beginning to feel the ever-growing pressure of the Environmental Protection Agency to choose a safe method of transportation of nuclear material. From consideration of the magnitude of the predicted spent fuel shipments, it seems imperative that some criterion of hazard limitation be implemented at a realistic expense.

Comparison of the LP method to a common current method of route and mode selection suggests the potential value of the LP method. As an example, the shipment of spent fuel from Reactor 3 was examined employing a selection process as follows:

```

SINGLE MODE CHOICE
  ↓
LEAST EXPENSIVE?
  ↓
SATISFY HAZARD LIMITATION?
  ↓
CHOICE OF ROUTE AND MODE

```

Following the above outlined logic, $x_{6,29}$ is the resulting choice (see Fig. 11); that is, shipment by rail over route 3-7-8-20-21-24. To satisfy the demand for spent fuel shipped,

$$\frac{x_{6,29} \text{ ton-miles}}{410 \text{ miles}} = 28 \text{ tons} \quad \text{or} \quad x_{6,29} = 10,490 \text{ ton-miles}$$

which corresponds to a cost of

$$(10,490 \text{ ton-miles}) (1.2 \text{ unit cost/ton-miles}) = 12,600 \text{ unit cost}$$

As shown in Table V, the LP solution is

$$x_{1,13} = 3,425 \text{ ton-miles}$$

$$x_{6,29} = 7,590 \text{ ton-miles}$$

which corresponds to a cost of

$$(3,425 \text{ ton-miles})(1.0 \text{ unit cost/ton-mile})$$

$$+ (7,590 \text{ ton-miles})(1.2 \text{ unit cost/ton-mile}) = 12,525 \text{ unit cost}$$

A saving of 75 cost units is realized by the LP method even in this simplified model. The full value of the LP method clearly becomes more obvious as the model becomes more complicated. One could imagine the use of this method by a shipping agency which is constrained by such factors as the following:

1. Limited number of each type of vehicle and cask,
2. Limited maintenance available depending on the vehicle,
3. Legal restrictions imposed by state or government agencies, and
4. Others,

while having many options available such as

1. Several existing modes,
2. Possible new modes, and
3. Mixed modes.

LP also offers the capacity for ready updating of information. This seems imperative considering the variable nature of route characteristics, cost, etc. This aspect is discussed in detail in Sections 4.0 - 4.4.

4.0 POSTOPTIMAL ANALYSIS

After an optimal solution has been attained, there is information to be gained from the MPS/360 output concerning the optimal solution. As mentioned previously, the cost of transportation by various modes is by no means fixed. MPS/360 allows the user to examine the range for which a cost coefficient may be varied while maintaining the same basic solution (although the total cost may change). Similarly, the range of the RHS (demands) and risk coefficients may be examined without changing the basis.

An extension of this analysis would allow the cost coefficients, RHS, row coefficients, or column coefficients to be varied to determine their effect on the solution. For instance, the cost coefficient of over weight truck shipment may be varied over any range, say 1.9 through 0.5, thus generating a series of related LP problems. Clearly, the basis most likely would change in this instance introducing a new solution. This procedure is referred to as parameteric programming.

4.1 Range Analysis

Range analysis is used postoptimally to generate an output analysis of the current basis. This analysis includes:

1. The effects of cost changes on optimum activities,
2. The cost of changing an activity from the optimum level and the activity range for which this cost is valid,
3. The value of changing the row activity (RHS) and the interval for which this change is valid.

Although the parameters may be changed from their optimum value, a better total optimum is possible. In general, a cost increase forces an activity decrease, and conversely a cost decrease promotes an activity increase.

The computer output of the RANGE analysis for the model problem is displayed in Appendix A. Sections 1 and 3 are row sections in which section 1 contains economic information for rows at their lower or upper limit; section 3 contains such information at an intermediate level. Parameters which may appear are defined as follows:

| | | | | | | | | | |
|--------|---|----|------------------------------------|----|-----------------------------|----|-----------------------------|----|-----------------------------|
| Number | The internal serial number of this row | | | | | | | | |
| Row | User's name for row | | | | | | | | |
| AT | A two-character code denoting the status that the row activity has in the solution. Codes and their meanings are: <table> <tr> <td>BS</td><td>Row activity at intermediate level</td></tr> <tr> <td>EQ</td><td>Row activity at fixed level</td></tr> <tr> <td>UL</td><td>Row activity at upper limit</td></tr> <tr> <td>LL</td><td>Row activity at lower limit</td></tr> </table> | BS | Row activity at intermediate level | EQ | Row activity at fixed level | UL | Row activity at upper limit | LL | Row activity at lower limit |
| BS | Row activity at intermediate level | | | | | | | | |
| EQ | Row activity at fixed level | | | | | | | | |
| UL | Row activity at upper limit | | | | | | | | |
| LL | Row activity at lower limit | | | | | | | | |

| | |
|----------|---|
| Activity | The value of the row activity in the solution |
|----------|---|

| | |
|----------------|--|
| Slack Activity | The value of the associated slack variable |
|----------------|--|

The upper line for each row shows the activity-cost relationship for activity decrease/cost increase and employs the following parameters:

| | | | | | |
|------------------|--|----|---------------------------------------|----|---------------------------------------|
| Lower Limit | The input lower limit for this row | | | | |
| Lower Activity | The level to which the row activity may be decreased at a cost per unit of decrease given by Unit Cost | | | | |
| Unit Cost | The change of the objective function per unit of decrease of activity. The problem can be modified to decrease the row activity as far as Lower Activity. | | | | |
| Limiting Process | The name of the row or column that would change its status if the activity level of the row were decreased below Lower Activity. In section 1, Limiting Process will leave the basis; in section 3, Limiting will enter the basis. | | | | |
| AT | The status associated with Limiting Process <table> <tr> <td>LL</td><td>leaves or enters basis at lower limit</td></tr> <tr> <td>UL</td><td>leaves or enters basis at upper limit</td></tr> </table> | LL | leaves or enters basis at lower limit | UL | leaves or enters basis at upper limit |
| LL | leaves or enters basis at lower limit | | | | |
| UL | leaves or enters basis at upper limit | | | | |

The lower line for each row shows the activity-cost relationship for activity increase/cost decrease.

| | |
|------------------|--|
| Upper Limit | The upper limit for the row |
| Upper Activity | The level to which the row activity may be increased at a cost per unit increase of Unit Cost |
| Unit Cost | The change in the objective function per unit increase in row activity. The problem can be modified to increase the row activity level as far as Upper Activity, at this cost per unit increase. |
| Limiting Process | The name of the row or column which would change its status if the activity level of the row were increased above Upper Activity. In section 1, Limiting Process will leave the basis; in section 2, Limiting Process will enter the basis |
| AT | The status associated with Limiting Process LL Leaves or enters the basis at lower limit UL Leaves or enters the basis at upper limit |

Sections 2 and 4 are column sections. Section 2 contains the economic information for the variables at their lower limit; section 4, for those at intermediate level. The following parameters may appear:

| | |
|----------|---|
| Number | The internal serial number of the column |
| Column | User's name for the column |
| AT | Column activity status BS In the basis FR Non basic or free EQ Non basic, artificial UL Non basic at upper level LL Non basic at lower level |
| Activity | The value of column activity in the solution |

Similar to sections 1 and 3, the upper line displays the activity-cost relationship for activity decrease/cost increase and the lower line displays the activity-cost relationships for activity increase/cost decrease.

Input Cost refers to the unit cost of the variable as specified by the user. In sections 2 and 4 Input Cost is varied to Upper Cost and Lower Cost, respectively. The other parameters are Lower Limit, Lower Activity, Unit Cost, Limiting Process, AT, Upper Activity, Upper Limit, and Lower Cost. Their meanings are analogous to those in sections 1 and 3.

An example will more clearly illustrate the use of Range. Referring to page 19 of the Range output in the Appendix A, consider Number 64. The output indicates this is Column 45 at its lower limit (LL) with a solution value (activity) of 0. The Input cost is listed as 1.9, and the lower limit is 0. The upper limit is listed as infinity; that is, no upper limit exists. Reading the top line, Lower Activity reveals the activity level of -4117.51953 would result if Input Cost were increased to an Upper Cost of infinity. The change in the objective function per unit decrease in Column 45 down to -4117.51953 is shown as 1.50506. Limiting Process indicates that Column 49 would leave the basis if the activity level of this column (Column 45) were decreased below Lower Activity. AT demonstrates that Column 49 will leave the basis at its Lower Limit (LL). For more detailed information on Range see Mathematical Programming Systems Handbook (8).

4.2 Cost Coefficient Analysis

Due to the variable nature of transportation mode cost coefficients, it may be informative to examine the effect of varying certain cost coefficients. This procedure can be performed by a MPS/360 subroutine PARAOBJ.

PARAOBJ is used postoptimally to perform parametric programming on the objective function. The original LP problem is modified by replacing the original objective function by the sum of the original objective function and a multiple of a "change row". This multiple is called Param. In other words the cost coefficients may be altered to examine their effect on the solution.

PARAOBJ was used to examine the effect of changing the cost coefficient of 1) over weight truck and 2) Large and VSTOL aircraft. These are realistic goals since the cost of OWT may be considerably decreased once the Interstate system is completed and appropriate legal legislation is enacted. Much research is being done concerning VSTOL aircraft. Their tremendous lift coefficients and short runway requirements are making these aircraft potentially exciting. The computer results of analysis of situation 1) appears in Appendix B and are summarized below.

As Param is gradually varied, the OWT cost is decreased by an amount equal to $(0.1)(\text{Param})$. The table on page 1 of the computer output in Appendix B displays an iteration table showing the vector leaving the basis and the vector entering the basis for the corresponding value of Param as it is gradually changed. The associated objective function value is indicated as Function Value. These results are summarized in Table VI as the cost coefficient of OWT is varied from 1.9 to 0.4. It is seen that no change in the basic solution occurs until the cost of OWT shipment is decreased to 1.1 unit cost per ton-mile. At this point shipment by $x_{1,13}$ left the basis and was replaced by $x_{2,13}$ at 7293.23939 ton-miles, while $x_{6,29}$ decreased from 7590.79808 to 3153.83325 ton-miles, i.e., OWT shipment along route 13 (36-94-70) has replaced LWT shipment and a part of the rail shipment along route 29. This appears on pages 36-39 of the PARAOBJ computer output, Appendix B.

Similarly, Table VII represents the effect of varying the cost coefficient of VSTOL and Large Aircraft (LA). Notice that air transport enters into use in all reactors except Reactor 4 where it has been hypothesized to be geographically prohibitive to construct an airstrip.

Table VI

EFFECT OF VARYING OVER WEIGHT TRUCK COST

| PARAM | ONT COST | VARIABLE | TON-MILES | OBJECTIVE FUNCTION |
|-------|----------|------------|------------|--------------------|
| 0 | 1.9 | $x_{6,25}$ | 7983.87097 | 48152.00720 |
| | | $x_{1,7}$ | 16800.0 | |
| | | $x_{1,13}$ | 3425.11621 | |
| | | $x_{6,29}$ | 7590.79808 | |
| | | $x_{1,19}$ | 9237.28814 | |
| 1 | 1.8 | no change | | |
| 2 | 1.7 | no change | | |
| 3 | 1.6 | no change | | |
| 4 | 1.5 | no change | | |
| 5 | 1.4 | no change | | |
| 6 | 1.3 | no change | | |
| 7 | 1.2 | no change | | |
| 8 | 1.1 | $x_{6,25}$ | 7983.87097 | 47425.09652 |
| | | $x_{1,7}$ | 16800.0 | |
| | | $x_{2,13}$ | 7293.23939 | |
| | | $x_{6,29}$ | 3153.83325 | |
| | | $x_{1,19}$ | 9237.28814 | |
| 9 | 1.0 | $x_{6,25}$ | 7983.87097 | 46695.77259 |
| | | $x_{1,7}$ | 16800.0 | |
| | | $x_{2,13}$ | 7293.23939 | |
| | | $x_{6,29}$ | 3153.83325 | |
| | | $x_{1,19}$ | 9237.28814 | |
| 10 | 0.9 | $x_{6,25}$ | 7983.87097 | 43576.97806 |
| | | $x_{2,7}$ | 16800.0 | |
| | | $x_{2,13}$ | 7293.23939 | |
| | | $x_{6,29}$ | 3153.83325 | |
| | | $x_{2,18}$ | 4681.93405 | |
| | | $x_{2,19}$ | 4793.41379 | |
| 11 | 0.8 | no change | | 40220.11884 |
| 12 | 0.7 | no change | | 36863.25962 |
| 13 | 0.6 | no change | | 33506.40039 |
| 14 | 0.5 | no change | | 30149.54117 |
| 15 | 0.4 | no change | | 26792.68195 |

Table VII
EFFECT OF VARYING VSTOL AND LARGE AIRCRAFT COST

| PARAM | VSTOL COST | LA COST | VARIABLE | TON-MILES | TOTAL COST |
|-------|------------|---------|-----------------|-------------|-------------|
| 0 | 2.5 | 2.2 | $x_{6,25}$ | 7983.87097 | 48152.0072 |
| | | | $x_{1,7}$ | 16800.0 | |
| | | | $x_{1,13}$ | 3425.1162 | |
| | | | $x_{6,29}$ | 7590.79808 | |
| | | | $x_{1,19}$ | 9237.28814 | |
| 2 | 2.1 | 1.8 | -- NO CHANGE -- | | |
| 4 | 1.7 | 1.4 | $x_{5,2}$ | 6556.29139 | 46445.88229 |
| | | | $x_{1,7}$ | 16800.0 | |
| | | | $x_{1,13}$ | 3060.08116 | |
| | | | $x_{5,40}$ | 5835.5036 | |
| | | | $x_{1,19}$ | 9237.28814 | |
| 6 | 1.3 | 1.0 | $x_{5,2}$ | 6556.29139 | 36818.01562 |
| | | | $x_{5,9}$ | 12631.57895 | |
| | | | $x_{5,40}$ | 8392.85714 | |
| | | | $x_{1,19}$ | 9237.28814 | |
| 8 | 0.9 | 0.6 | -- NO CHANGE -- | | |
| 10 | 0.5 | 0.2 | -- NO CHANGE -- | | |

4.3 Risk Coefficient Analysis

The risk coefficient derived in section 2.3 is based on parameters which may be subject to change. For example, the seriousness of accident index (SA) may be greatly affected by improved construction of vehicle, careful route choices or better maintenance. It is then of interest to examine the effect that a change in the risk coefficient of a particular mode has on the model. This objective is attained by the use of the MPS/360 subroutine PARAROW.

PARAROW is used postoptimally to perform parametric programming on a constraint row. For any LP problem, a series of related problems may be generated by replacing the coefficients of a chosen row by new coefficients that are obtained by adding the original coefficients to Param times corresponding coefficients of a change row. Param is gradually changed thus changing the coefficients of the original constraint row.

PARAROW was applied to the risk coefficients of LWT for Reactor 2. As the Param value gradually changed the solution remained at the optimal activity until Param equalled 2.82. At this point the solution changed. Originally all the spent fuel from Reactor 2 was shipped by LWT over route 36-94-70. The current risk coefficient equals $0.218 + (0.1)(2.82)$ or 0.5. This forces some of the spent fuel to be shipped by rail to satisfy the risk constraint. A further increase in risk coefficient does not change the basis, but it does affect the amount shipped by truck or rail. It is noted that the higher the LWT risk coefficient becomes, the more ton-miles are attributed to rail shipment by route 5-48-20-21-24. For instance when Param equals 10, the risk coefficient LWT by route 36-94-70 equals $0.218 + 10(0.10)$ or 1.218. At this point, 5713.23529 ton-miles are attributed to LWT and 11086.76471 are attributed to rail.

A further example of the effect of changing the risk was performed by decreasing the risk coefficient of OWT for all reactors. This had no effect on the solution which is to be expected since there is no shipment by OWT in the original solution.

4.4 Conclusions

The shipping model formulated for this work determines the most economical mode and route of transportation of spent fuel. Even in the simplified model used here it is evident that the complexity of the problem makes an optimal solution far from intuitively obvious. MPS/360 appears to be an inexpensive and speedy method of determining an optimal shipping campaign. The computer solution (Primal) for this model costs \$1.55 and had an execution time of 0.24 minutes.

It has been noted that much of the data used is subject to change, but this is readily accomplished with the computer procedures described. The shipping model described is quite flexible with regard to sensitivity of the optimal results to changes in input data. The model can easily be modified to accept any corrections or updating. It is easy to imagine an agency responsible for shipping spent fuel utilizing a model of this nature and continually updating the matrix to accompany changes such as:

- 1) Cost rise or fall due to economic trends or negotiations
- 2) Route characteristic variance, e.g., by season
- 3) Changes in existing transportation modes
- 4) Introduction of new modes
- 5) Risk Limits become more or less restrictive
- 6) Any other model fluctuations

Reviewing the results of the present model, it is predicted that the four reactors in question will ship approximately two thirds of their spent fuel by LWT and the rest by rail. Presently, it is expected that in the near future about one half of the spent fuel will be shipped by truck and slightly less than that will be shipped by rail (10). However, the future result may be quite different depending upon the updating of existing cost or risk coefficients. For instance, air shipment could become economically competitive if its cost could be decreased to 1.4 as shown in Table VII. Further, air transport would completely dominate Reactors 1, 2, and 3 if the cost could be decreased to 1.0. Reactor 4 is hypothesized to be geographically prohibited from building an air strip, but certainly a mixed mode transportation campaign could be considered. It is evident that this type of model may find use as a predictive aid in anticipating future transport mode possibilities or routes of shipment as well as analyzing existing modes and routes.

5.0 SUGGESTIONS FOR FURTHER STUDY

It is suggested that to make the model more accurate a more detailed analysis of quantification of hazard be performed. This analysis would involve a detailed study of accident probability, seriousness of accident, and the relative importance of these factors to hazard quantification. In addition, a realistic evaluation of the risk upper limit and the risk coefficient demands that an absolute rather than relative evaluation of risk be performed. That is, an actual population dose for a given set of circumstances should be calculated. The maximum permissible dose would then determine the upper limit of risk. This would require a study of the radionuclides released upon accident and their dispersal characteristics. This implies a study of the relation between severity of accident and the consequential release of radionuclides.

Further parametric programming seems warranted. In particular, postoptimal analysis is possible on the RHS of the matrix (the risk upper limit) through a MPS/360 subroutine called PARARHS. It may also be of interest to change values in the objective function and RHS simultaneously. This can be done through a MPS/360 subroutine called PARARIM. These procedures enable the existing model to be readily analyzed concerning the effect of changing the risk upper limit or the effect of simultaneously varying the cost coefficients and the risk upper limit.

6.0 Acknowledgement

The author expresses his gratitude to Dr. Walter Meyer and Dr. N. D. Eckhoff for their guidance and encouragement throughout this work. Financial support from the National Defense and Education Act Fellowship is gratefully acknowledged. A note of thanks is extended to Janet Gaines for her perceptive typing and to the entire Nuclear Engineering faculty and staff for successfully integrating the author into a new university and curriculum.

7.0 Literature Cited

1. Ernest B. Tremmel and Robert J. Berts, "Trends in Nuclear Transportation," Proceedings of the Third International Symposium on Packaging and Transportation of Radioactive Materials, August, 1971, CONF 710801 pp. 75-96.
2. K. H. Dufrane and E. D. North, "The Effect of Highway Weight Restrictions on the Cost of Spent Fuel Shipments," Proceedings of the Third International Symposium on Packaging and Transportation of Radioactive Materials, August, 1971, CONF 710801 pp. 160-171.
3. Ferdinand Limekohler, Trucking of Radioactive Materials Safety vs Economy in Highway Material Transportation, John Hopkins Press, Library of Congress No. 63-16454 (1963).
4. K. B. Stewart, Rail Accident Statistics Pertinent to the Shipment of Radioactive Materials, January 21, 1963.
5. TID-16764 (Suppl. 2), A Summary of Incidents Involving USAEC Shipments of Radioactive Material, United States Atomic Energy Commission, April 1966.
6. W. C. McCluggage, "The AEC Accident Record and Recent Changes in AEC Manual Chapter 0529," Proceedings of the Third International Symposium on Packaging and Transportation of Radioactive Materials, August, 1971, CONF 71801 pp. 108-129.
7. W. A. Spinney and R. M. Thrall, Linear Optimization, Holt, Rinehart, and Winston, Inc., 1970.
8. _____, "Mathematical Programming Systems/360 Version 2, Linear and Separable Programming, H20-0476-2."
9. S. Ashour, Class Lecture Notes on Linear Programming, Industrial Engineering, Kansas State University, (Spring 1972).
10. Walter Meyer, R. E. Faw, et. al., "Hazard Evaluation of Nuclear Facility Related Transportation Accidents" (Research Proposal submitted to Environmental Protection Agency, 1972) p. 22.
11. _____, "The Nuclear Industry 1970, U. S. Atomic Energy Commission, Washington, D.C., November, 1970.

APPENDICES

APPENDIX A

MPS/360 Computer Listing and Output for Optimization
and Range Analysis

This computer program arrives at an optimal primal solution and performs RANGE analysis on the solution. MPS programming is explained in Section 3.1; Range analysis is explained in Section 4.1. Execution times for PRIMAL and RANGE were 0.45 minutes and 0.17 minutes, respectively.

PAGE 1 - 72/194

CONTRCL PROGRAM COMPILER - MPS/360 V2-M10

```
0001 PROGRAM
0002 INITIALZ
0003 MOVE(XDATA,'TRANS')
0004 MOVE(XPNAME,'PBFILE')
0005 CONVERT('SUMMARY')
0006 SETUP('MIN')
0007 PICTURE
0008 BCODEUT
0009 MOVE(XOBJ,'COST')
0010 MOVE(XRHS,'LIMITS')
0011 PRIMAL
0012 SOLUTION
0013 RANGE
0014 EXIT
0015 PEND
0016
0017
```

**THIS BOOK
CONTAINS
NUMEROUS PAGES
WITH THE ORIGINAL
PRINTING BEING
SKEWED
DIFFERENTLY FROM
THE TOP OF THE
PAGE TO THE
BOTTOM.**

**THIS IS AS RECEIVED
FROM THE
CUSTOMER.**

EXECUTOR. MPS/360 V2-M10

PAGE 1 - 72/194

CONVERT TRANS TO PROFILE

TIME = 0.03

SUMMARY

1- ROWS SECTION.

0 MINOR ERRORS - 0 MAJOR ERRORS.

2- COLUMNS SECTION.

0 MINOR ERRORS - 0 MAJOR ERRORS.

3- RHS'S SECTION.

LIMITS

0 MINOR ERRORS - 0 MAJOR ERRORS.

THE FOLLOWING ROWS ARE NOT USED.

19

EXECUTOR. MPS/360 V2-M10

PAGE 2 - 72/194

NUMBER OF ELEMENTS BY COLUMN ORDER

| | | | | | | | | | | | | | | |
|----|-------|--------|-------|--------|-------|--------|-------|--------|-------|--------|-------|--------|-------|--------|
| 25 | COL1 |3 | COL2 |3 | COL3 |3 | COL4 |3 | COL5 |3 | COL6 |4 | COL7 |4 |
| 27 | COL8 |3 | COL9 |4 | COL10 |4 | COL11 |3 | COL12 |4 | COL13 |4 | COL14 |4 |
| 30 | COL15 |4 | COL16 |3 | COL17 |3 | COL18 |3 | COL19 |4 | COL20 |2 | COL21 |3 |
| 41 | COL22 |3 | COL23 |3 | COL24 |4 | COL25 |4 | COL26 |3 | COL27 |3 | COL28 |3 |
| 48 | COL29 |3 | COL30 |3 | COL31 |4 | COL32 |1 | COL33 |3 | COL34 |3 | COL35 |3 |
| 55 | COL36 |3 | COL37 |3 | COL38 |3 | COL39 |3 | COL40 |3 | COL41 |4 | COL42 |4 |
| 62 | COL43 |3 | COL44 |4 | COL45 |4 | COL46 |3 | COL47 |3 | COL48 |3 | COL49 |3 |
| 69 | COL50 |3 | COL51 |3 | COL52 |3 | COL53 |3 | COL54 |3 | COL55 |3 | COL56 |3 |
| 76 | COL57 |3 | COL58 |3 | COL59 |4 | COL60 |4 | COL61 |3 | COL62 |3 | COL63 |3 |

EXECUTOR. MPS/360 V2-M10

PAGE 3 - 72/194

NUMBER OF ELEMENTS BY ROW ORDER, EXCLUDING RHS'S, INCLUDING SLACK ELEMENT

| | | | | | | | | | | | | | | | | | | | | | |
|----|---|-------|---------|---|-------|---------|---|-------|---------|---|-------|---------|---|-------|--------|---|-------|--------|---|-------|---------|
| 1 | N | CS1 |64 | G | ROW1 |17 | E | ROW2 |4 | E | ROW3 |4 | E | ROW4 |4 | E | ROW5 |4 | E | ROW6 |3 |
| 8 | G | ROW7 |10 | E | ROW8 |3 | E | ROW9 |4 | G | ROW10 |17 | E | ROW11 |4 | E | ROW12 |4 | G | ROW13 |13 |
| 15 | E | ROW14 |4 | L | ROW15 |21 | L | ROW16 |12 | L | ROW17 |19 | L | ROW18 |4 | | | | | | |

PROBLEM STATISTICS - 19 ROWS, 42 VARIABLES, 225 ELEMENTS, DENSITY = 14.44

THESE STATISTICS INCLUDE ONE SLACK VARIABLE FOR EACH ROW.

0 MINOR ERRORS, 0 MAJOR ERRORS.

EXECUTOR. MPS/360 V2-M10

PAGE 4 - 72/194

SETUP PROFILE

TIME = 0.14

MIN

MATRIX1 ASSIGNED TO MATRIX1

ETAL ASSIGNED TO ETAL

SCRATCH1 ASSIGNED TO SCRATCH1

SCRATCH2 ASSIGNED TO SCRATCH2

MAXIMUM PRICING NOT REQUIRED - MAXIMUM POSSIBLE 7

NO CYCLING

| POOLS | NUMBER | SIZE | CORE |
|----------------|--------|------|------|
| N-REG-BITS MAP | | | 80 |
| WORK REGIONS | 4 | 176 | 1584 |
| MATRIX BUFFERS | 3 | 1600 | 5040 |
| ETA BUFFERS | 4 | 2700 | 4152 |

| ROWS (LOG-VAR.) | TOTAL | NORMAL | FREE | MIXED | UNBOUND |
|--------------------|-------|--------|------|-------|---------|
| | 19 | 8 | 1 | 10 | 0 |
| COLUMNS (STR-VAR.) | 63 | 63 | 0 | 0 | 0 |

225 ELEMENTS - (DENSITY = 14.44 - 2 MATRIX RECORDS (WITHOUT RHS'S))

PICTURE - USING PROFILE

TIME = 0.17

EXECUTCR. HPS/360 V2-M10

PAGE 5 - 72/194

SUMMARY OF MATRIX

| SYMBOL | RANGE | COUNT (INCL. RHS) |
|--------|---------------------------------|-------------------|
| I | LESS THAN .000001 | |
| T | .000001 THRU .000009 | |
| X | .000010 .000099 | |
| W | .000100 .000999 | |
| V | .001000 .009999 | |
| U | .010000 .099999 | 2 |
| T | .100000 .999999 | 57 |
| I | 1.000000 1.000000 | 28 |
| A | 1.000001 10.000000 | 119 |
| B | 10.000001 100.000000 | |
| C | 100.000001 1,000.000000 | |
| D | 1,000.000001 10,000.000000 | 1 |
| E | 10,000.000001 100,000.000000 | 3 |
| F | 100,000.000001 1,000,000.000000 | |
| G | GREATER THAN 1,000,000.000000 | |

EXECUTCR. HPS/360 V2-M10

PAGE 6 - 72/194

ACCOMPT - USING PROFILE

TIME = 0.19

| EXECUTOR. | | RPS/360 V2-M10 | | PAGE 7 - 72/194 | |
|-----------|-------|----------------|-------|-----------------|--|
| NAME | TRANS | | | | |
| ROWS | | | | | |
| N COST | | | | | |
| G ROW1 | | | | | |
| E ROW2 | | | | | |
| E ROW3 | | | | | |
| E ROW4 | | | | | |
| E ROW5 | | | | | |
| E ROW6 | | | | | |
| G ROW7 | | | | | |
| E ROW8 | | | | | |
| E ROW9 | | | | | |
| G ROW10 | | | | | |
| E ROW11 | | | | | |
| E ROW12 | | | | | |
| G ROW13 | | | | | |
| E ROW14 | | | | | |
| L ROW15 | | | | | |
| L ROW16 | | | | | |
| L ROW17 | | | | | |
| L ROW18 | | | | | |
| COLUMNS | | | | | |
| COL1 | COST | 1.00000 | ROW1 | 1.00000 | |
| COL1 | ROW15 | -.23600 | | | |
| COL2 | COST | 1.90000 | ROW1 | 1.00000 | |
| COL2 | ROW15 | -.97200 | | | |
| COL3 | COST | 2.50000 | ROW1 | 1.51000 | |
| COL3 | ROW15 | -.47600 | | | |
| COL4 | COST | 2.20000 | ROW1 | 1.51000 | |
| COL4 | ROW15 | -.46600 | | | |
| COL5 | COST | 2.70000 | ROW2 | 2.48000 | |
| COL5 | ROW15 | -.46700 | | | |
| COL6 | COST | 1.00000 | ROW1 | 1.44000 | |
| COL6 | ROW2 | 1.59000 | ROW15 | -.70800 | |
| COL7 | COST | 1.90000 | ROW1 | 1.44000 | |
| COL7 | ROW2 | 1.59000 | ROW15 | -.40010 | |
| COL8 | COST | 2.70000 | ROW3 | 2.48000 | |
| COL8 | ROW15 | -.46200 | | | |
| COL9 | COST | 1.00000 | ROW1 | 1.48000 | |
| COL9 | ROW3 | 1.48000 | ROW15 | -.20900 | |
| COL10 | COST | 1.90000 | ROW1 | 1.48000 | |
| COL10 | ROW3 | 1.48000 | ROW15 | -.10000 | |
| COL11 | COST | 2.70000 | ROW4 | 2.48000 | |
| COL11 | ROW15 | -.46200 | | | |
| COL12 | COST | 1.90000 | ROW1 | 1.70000 | |
| COL12 | ROW4 | 1.77000 | ROW15 | -.19600 | |
| COL13 | COST | 1.00000 | ROW1 | 1.77000 | |
| COL13 | ROW4 | 1.77000 | ROW15 | -.15200 | |
| COL14 | COST | 1.00000 | ROW1 | 1.87000 | |
| COL14 | ROW5 | 1.87000 | ROW15 | -.18200 | |
| COL15 | COST | 1.90000 | ROW1 | 1.87000 | |
| COL15 | ROW5 | 1.87000 | ROW15 | -.13600 | |
| COL16 | COST | 2.70000 | ROW5 | 2.48000 | |
| COL16 | ROW15 | -.46200 | | | |

| EXECUTOR. | | RPS/360 V2-M10 | | PAGE 8 - 72/194 | |
|-----------|-------|----------------|-------|-----------------|--|
| COL17 | COST | 1.20000 | ROW1 | 1.24000 | |
| COL17 | ROW15 | -.87000 | | | |
| COL18 | COST | 1.20000 | ROW1 | 1.19000 | |
| COL18 | ROW15 | -.92000 | | | |
| COL19 | COST | 1.70000 | ROW1 | 1.29000 | |
| COL19 | ROW6 | 1.29000 | ROW15 | -.31500 | |
| COL20 | COST | 1.20000 | ROW1 | 1.24000 | |
| COL21 | COST | 2.70000 | ROW6 | 2.70000 | |
| COL21 | ROW15 | -.52400 | | | |
| COL22 | COST | 1.00000 | ROW7 | 1.00000 | |
| COL22 | ROW16 | -.28200 | | | |
| COL23 | COST | 1.90000 | ROW7 | 1.00000 | |
| COL23 | ROW16 | -.08000 | | | |
| COL24 | COST | 1.00000 | ROW7 | 2.22000 | |
| COL24 | ROW7 | 2.20000 | ROW16 | -.11600 | |
| COL25 | COST | 1.90000 | ROW7 | 2.22000 | |
| COL25 | ROW9 | 2.20000 | ROW16 | -.83400 | |
| COL26 | COST | 2.70000 | ROW9 | 2.70000 | |
| COL26 | ROW16 | -.49000 | | | |
| COL27 | COST | 2.20000 | ROW7 | 1.33000 | |
| COL27 | ROW16 | -.47000 | | | |
| COL28 | COST | 2.50000 | ROW7 | 1.33000 | |
| COL28 | ROW16 | -.48000 | | | |
| COL29 | COST | 1.20000 | ROW7 | 1.60000 | |
| COL29 | ROW16 | -.30500 | | | |
| COL30 | COST | 1.20000 | ROW7 | 1.00000 | |
| COL30 | ROW16 | -.37000 | | | |
| COL31 | COST | 1.20000 | ROW7 | 1.74000 | |
| COL31 | ROW8 | 1.74000 | ROW16 | -.42000 | |
| COL32 | COST | 2.70000 | ROW8 | 1.35000 | |
| COL32 | ROW16 | -.44000 | | | |
| COL33 | COST | 1.00000 | ROW10 | 1.00000 | |
| COL33 | ROW17 | -.89000 | | | |
| COL34 | COST | 1.90000 | ROW10 | 1.00000 | |
| COL34 | ROW17 | 2.20000 | | | |
| COL35 | COST | 1.00000 | ROW10 | 1.05000 | |
| COL35 | ROW17 | 1.15000 | | | |
| COL36 | COST | 1.90000 | ROW10 | 1.05000 | |
| COL36 | ROW17 | 2.80000 | | | |
| COL37 | COST | 1.90000 | ROW10 | 1.05000 | |
| COL37 | ROW17 | 1.90000 | | | |
| COL38 | COST | 1.00000 | ROW10 | 1.05000 | |
| COL38 | ROW17 | 1.90000 | | | |
| COL39 | COST | 1.90000 | ROW10 | 1.17000 | |
| COL39 | ROW17 | 1.00000 | | | |
| COL40 | COST | 1.00000 | ROW10 | 1.17000 | |
| COL40 | ROW17 | 1.00000 | | | |
| COL41 | COST | 1.00000 | ROW10 | 1.27000 | |
| COL41 | ROW17 | 1.00000 | | | |
| COL42 | COST | 1.90000 | ROW10 | 1.27000 | |
| COL42 | ROW11 | 1.20000 | ROW17 | 1.93000 | |
| COL43 | COST | 2.70000 | ROW11 | 1.10000 | |
| COL43 | ROW17 | 1.90000 | | | |
| COL44 | COST | 1.00000 | ROW10 | 1.40000 | |

EXECUTOR. MPS/360 V2-M10

| | | | | | |
|--------|--------|-------------|------------|-------------|-------------|
| COL44 | ROW12 | 1.40000 | ROW17 | 1.50000 | |
| COL45 | COST | 1.90000 | ROW10 | 1.40000 | |
| COL45 | ROW12 | 1.40000 | ROW17 | 1.50000 | |
| COL46 | COST | 2.70000 | ROW12 | 1.68000 | |
| COL46 | ROW17 | 1.40000 | | | |
| COL47 | COST | 2.50000 | ROW10 | 1.40000 | |
| COL47 | ROW17 | 1.40000 | | | |
| COL48 | COST | 2.20000 | ROW10 | 1.40000 | |
| COL48 | ROW17 | 1.40000 | | | |
| COL49 | COST | 1.20000 | ROW10 | 1.02000 | |
| COL49 | ROW17 | 1.37000 | | | |
| COL50 | COST | 1.20000 | ROW10 | .93500 | |
| COL50 | ROW17 | 1.33000 | | | |
| COL51 | COST | 1.00000 | ROW13 | 1.00000 | |
| COL51 | ROW18 | 1.40000 | | | |
| COL52 | COST | 1.90000 | ROW13 | 1.00000 | |
| COL52 | ROW18 | 1.40000 | | | |
| COL53 | COST | 1.00000 | ROW13 | .93000 | |
| COL53 | ROW18 | 1.47000 | | | |
| COL54 | COST | 1.90000 | ROW13 | .93000 | |
| COL54 | ROW18 | 1.45000 | | | |
| COL55 | COST | 1.00000 | ROW13 | 1.12000 | |
| COL55 | ROW18 | 1.40000 | | | |
| COL56 | COST | 1.90000 | ROW13 | 1.12000 | |
| COL56 | ROW18 | 1.40000 | | | |
| COL57 | COST | 1.00000 | ROW13 | 1.18000 | |
| COL57 | ROW18 | 1.40000 | | | |
| COL58 | COST | 1.90000 | ROW13 | 1.18000 | |
| COL58 | ROW18 | 1.42000 | | | |
| COL59 | COST | 1.00000 | ROW13 | 1.34000 | |
| COL59 | ROW14 | 1.34000 | ROW18 | 1.80000 | |
| COL60 | COST | 1.90000 | ROW13 | 1.34000 | |
| COL60 | ROW14 | 1.34000 | ROW18 | 1.10000 | |
| COL61 | COST | 2.70000 | ROW14 | 2.80000 | |
| COL61 | ROW18 | 1.40000 | | | |
| COL62 | COST | 1.20000 | ROW13 | 1.20000 | |
| COL62 | ROW18 | 1.40000 | | | |
| COL63 | COST | 1.20000 | ROW13 | 1.11000 | |
| COL63 | ROW18 | 1.47000 | | | |
| RMS | LIMITS | ROW1 | 9900.00000 | ROW7 | 16800.00000 |
| LIMITS | ROW10 | 11750.00000 | ROW13 | 10900.00000 | |
| ENDATA | | | | | |

PAGE 9 - 72/194

EXECUTOR. MPS/360 V2-M10

PRIMAL OBJ = COST RMS = LIMITS

TIME = 0.24 PINS. PRICING 7

INVERT CALLED TIME 0.24 CURRENT INVERSE --- ETA-VECTORS4 ELEMENTS4 RECORDS1 ITERATION3

BASIS --- NO.CP ROWS19 LOGICALS19 STRUCTURALS0

INVERSE --- NUCLEUS0 TRANSFORMED0 ETA-VECTORS4 ELEMENTS4 RECORDS1 TIME TAKEN 0.00

PRIMAL OBJ = COST RMS = LIMITS

TIME = 0.25 PINS. PRICING 7

SCALE =

| ITER | NUMBER | VECTOR | VECTOR | REDUCED | SUM |
|--------|--------|--------|--------|----------|---------|
| NUMBER | INFEAS | CLT | IN | COST | INFEAS |
| M | 1 | 3 | 2 | 1.51000- | 39650.7 |
| M | 2 | 2 | 11 | 1.40000- | 27700.0 |
| M | 3 | 1 | 14 | 1.18000- | 16800.0 |
| M | 4 | 0 | 8 | 1.31000- | |

FEASIBLE SOLUTION

PRIMAL OBJ = COST RMS = LIMITS

TIME = 0.27 PINS. PRICING 7

SCALE =

SCALE RESET TO 1.00000

| ITER | NUMBER | VECTOR | VECTOR | REDUCED | FUNCTION | |
|--------|--------|--------|--------|----------|----------|---------|
| NUMBER | NONOPT | CLT | IN | COST | VALUE | |
| M | 5 | 32 | 17 | 4.3 | 2.07218- | 72432.7 |
| | 6 | | 31 | 1.72450- | 72432.7 | |
| | 7 | | 50 | 1.07819- | 72432.7 | |
| | 8 | | 32 | 1.57881- | 72432.7 | |
| | 9 | | 61 | 1.50000- | 72432.7 | |
| | 10 | | 25 | 1.31656- | 72432.7 | |
| M | 11 | 21 | 18 | 1.08928- | 69099.4 | |
| | 12 | | 28 | 1.15629- | 69099.4 | |
| | 13 | | 60 | .95021- | 69099.4 | |
| | 14 | | 38 | .67947- | 69099.4 | |
| M | 15 | 11 | 46 | .65414- | 58110.0 | |
| | 16 | | 68 | .67381- | 52995.2 | |
| | 17 | | 39 | .60662- | 48152.0 | |
| M | 18 | 1 | 78 | .13559- | 48152.0 | |

OPTIMAL SOLUTION

PAGE 10 - 72/194

EXECUTOR. RPS/360 V2-M10
 SOLUTION (OPTIMAL)
 TIME = 0.29 MINS. ITERATION NUMBER = 18

PAGE 11 - 72/194

...NAME... ...ACTIVITY... DEFINED AS
 FUNCTIONAL 48152.00720 COST
 RESTRAINTS LIMITS

EXECUTOR. RPS/360 V2-M10
 SECTION 1 - ROWS

PAGE 12 - 72/194

| NUMBER | ...ROW... | AT | ...ACTIVITY... | SLACK ACTIVITY | ..LOWER LIMIT. | ..UPPER LIMIT. | ..DUAL ACTIVITY |
|--------|-----------|----|----------------|----------------|----------------|----------------|-----------------|
| 1 | COST | BS | 48152.00720 | 48152.00720- | NONE | NONE | 1.00000 |
| 2 | ROW1 | LL | 9900.00000 | | 9900.00000 | NONE | .96774- |
| 3 | ROW2 | EC | | | | | .33881 |
| 4 | ROW3 | EC | | | | | .29207 |
| 5 | ROW4 | EC | | | | | .43277 |
| 6 | ROW5 | EC | | | | | .43298 |
| 7 | ROW6 | EC | | | | | .03751 |
| 8 | ROW7 | LL | 16800.00000 | | 16800.00000 | NONE | 1.00000- |
| 9 | ROW8 | EC | | | | | .31034- |
| 10 | ROW9 | EC | | | | | .55455 |
| 11 | ROW10 | LL | 11750.00000 | | 11750.00000 | NONE | 1.06673- |
| 12 | ROW11 | EC | | | | | .27373 |
| 13 | ROW12 | EC | | | | | .02831 |
| 14 | ROW13 | LL | 10900.00000 | | 10900.00000 | NONE | .84746- |
| 15 | ROW14 | EC | | | | | .10119 |
| 16 | ROW15 | BS | | | NONE | | |
| 17 | ROW16 | BS | 4737.60000- | 4737.60000 | NONE | | |
| 18 | ROW17 | UL | | | | | .30253 |
| 19 | ROW18 | BS | 4249.15254- | 4249.15254 | NONE | | |

EXECUTOR. RPS/360 V2-M10
 SECTION 2 - COLUMNS

PAGE 13 - 72/194

| NUMBER | ..COLUMN. | AT | ...ACTIVITY... | ..INPUT COST.. | ..LOWER LIMIT. | ..UPPER LIMIT. | ..REDUCED COST. |
|--------|-----------|----|----------------|----------------|----------------|----------------|-----------------|
| 20 | COL1 | LL | | 1.00000 | | NONE | .03226 |
| 21 | COL2 | LL | | 1.90000 | | NONE | .93226 |
| 22 | COL3 | LL | | 2.50000 | | NONE | 1.03871 |
| 23 | COL4 | LL | | 2.20000 | | NONE | .73871 |
| 24 | COL5 | LL | | 2.70000 | | NONE | 1.85975 |
| 25 | COL6 | BS | | 1.00000 | | NONE | |
| 26 | COL7 | LL | | 1.90000 | | NONE | .90000 |
| 27 | COL8 | LL | | 2.70000 | | NONE | 1.97568 |
| 28 | COL9 | BS | | 1.00000 | | NONE | |
| 29 | COL10 | LL | | 1.90000 | | NONE | .90000 |
| 30 | COL11 | LL | | 2.70000 | | NONE | 1.70113 |
| 31 | COL12 | LL | | 1.90000 | | NONE | .96774 |
| 32 | COL13 | BS | | 1.00000 | | NONE | |
| 33 | COL14 | BS | | 1.00000 | | NONE | |
| 34 | COL15 | LL | | 1.90000 | | NONE | .90000 |
| 35 | COL16 | LL | | 2.70000 | | NONE | 1.62620 |
| 36 | COL17 | LL | | 1.20000 | | NONE | |
| 37 | COL18 | LL | | 1.20000 | | NONE | .64839 |
| 38 | COL19 | BS | | 1.20000 | | NONE | |
| 39 | COL20 | BS | 7983.87097 | 1.20000 | | NONE | |
| 40 | COL21 | LL | | 2.70000 | | NONE | |
| 41 | COL22 | BS | 16800.00000 | 1.00000 | | NONE | 2.59872 |
| 42 | COL23 | LL | | 1.90000 | | NONE | |
| 43 | COL24 | BS | | 1.00000 | | NONE | .90000 |
| 44 | COL25 | LL | | 1.90000 | | NONE | .90000 |
| 45 | COL26 | LL | | 2.70000 | | NONE | 2.19536 |
| 46 | COL27 | LL | | 2.20000 | | NONE | .87000 |
| 47 | COL28 | LL | | 2.50000 | | NONE | 1.17000 |
| 48 | COL29 | LL | | 1.20000 | | NONE | .20000 |
| 49 | COL30 | LL | | 1.20000 | | NONE | .20000 |
| 50 | COL31 | BS | | 1.20000 | | NONE | |
| 51 | COL32 | LL | | 2.70000 | | NONE | 2.28103 |
| 52 | COL33 | LL | | 1.00000 | | NONE | .22252 |
| 53 | COL34 | LL | | 1.90000 | | NONE | 1.49883 |
| 54 | COL35 | LL | | 1.00000 | | NONE | .22784 |
| 55 | COL36 | LL | | 1.90000 | | NONE | 1.62701 |
| 56 | COL37 | LL | | 1.90000 | | NONE | 1.70211 |
| 57 | COL38 | LL | | 1.00000 | | NONE | .75693 |
| 58 | COL39 | LL | | 1.90000 | | NONE | .70033 |
| 59 | COL40 | BS | 3625.11621 | 1.00000 | | NONE | |
| 60 | COL41 | BS | | 1.00000 | | NONE | |
| 61 | COL42 | LL | | 1.90000 | | NONE | 1.00589 |
| 62 | COL43 | LL | | 2.70000 | | NONE | 2.19591 |
| 63 | COL44 | BS | | 1.00000 | | NONE | |
| 64 | COL45 | LL | | 1.90000 | | NONE | 1.59306 |
| 65 | COL46 | LL | | 2.70000 | | NONE | 2.50421 |
| 66 | COL47 | LL | | 2.50000 | | NONE | .87649 |
| 67 | COL48 | LL | | 2.20000 | | NONE | .57649 |
| 68 | COL49 | BS | 1590.79808 | 1.20000 | | NONE | |

EXECUTOR. MPS/360 V2-H10 PAGE 14 - 72/194

| NUMBER | COLUMN | AT | ...ACTIVITY... | ...INPUT COST... | ...LOWER LIMIT... | ...UPPER LIMIT... | ...REDUCED COST... |
|--------|--------|----|----------------|------------------|-------------------|-------------------|--------------------|
| 69 | COL50 | LL | . | 1.20000 | . | NONE | .10277 |
| 70 | COL51 | LL | . | 1.00000 | . | NONE | .15254 |
| 71 | COL52 | LL | . | 1.90000 | . | NONE | 1.05254 |
| 72 | COL53 | LL | . | 1.00000 | . | NONE | .21184 |
| 73 | COL54 | LL | . | 1.90000 | . | NONE | 1.11184 |
| 74 | COL55 | LL | . | 1.00000 | . | NONE | .05005 |
| 75 | COL56 | LL | . | 1.90000 | . | NONE | .95005 |
| 76 | COL57 | BS | 9237.28014 | 1.00000 | . | NONE | . |
| 77 | COL58 | LL | . | 1.90000 | . | NONE | .90000 |
| 78 | COL59 | BS | . | 1.00000 | . | NONE | . |
| 79 | COL60 | LL | . | 1.90000 | . | NONE | .90000 |
| 80 | COL61 | LL | . | 2.70000 | . | NONE | 2.41667 |
| 81 | COL62 | LL | . | 1.20000 | . | NONE | .18305 |
| 82 | COL63 | LL | . | 1.20000 | . | NONE | .25932 |

EXECUTOR. MPS/360 V2-H10 PAGE 15 - 72/194

RANGE

TIME = 0.33 MINS. ITERATION NUMBER = 10

| INVERT CALLED | TIME | 0.33 | CURRENT INVERSE | ETA-VECTORS | ELEMENTS | RECORDS | ITERATION |
|---------------|-------------|------|-----------------|-------------|----------|---------|-----------|
| BASIS | NO. OF REVS | 19 | LOGICALS | 22 | 88 | 1 | 10 |
| INVERSE | NUCLEUS | 2 | TRANSFORMED | 15 | 50 | 1 | 0.03 |
| | | | | 17 | 96 | | |

EXECUTOR. MPS/360 V2-H10 PAGE 16 - 72/194

RANGE

TIME = 0.34 MINS. ITERATION NUMBER = 10

| ...NAME... | ...ACTIVITY... | DEFINED AS |
|------------|----------------|------------|
| FUNCTIONAL | 40152.00391 | COST |
| RESTRAINTS | | LIMITS |

| EXECUTOR. MPS/360 V2-M10 | | | | PAGE 19 - 72/194 | | | | | | |
|--------------------------|--------|----|-------------|------------------|---------------|----------------|-------------|--------------|----------|----|
| NUMBER | COLUMN | AT | ACTIVITY... | INPUT COST.. | LOWER LIMIT.. | LOWER ACTIVITY | UNIT COST.. | UPPER COST.. | LIMITING | AT |
| | | | | | UPPER LIMIT. | UPPER ACTIVITY | UNIT COST.. | UPPER COST.. | PROCESS. | |
| 44 | COL25 | LL | * | 1.90000 | NONE | INFINITY- | .90000- | INFINITY | NONE | LL |
| | | | | | | | .90000 | 1.00000 | COL24 | LL |
| 45 | COL26 | LL | * | 2.70000 | NONE | 18295.21094 | 2.19536- | INFINITY | COL24 | LL |
| | | | | | | | 2.19536 | .50464 | COL22 | LL |
| 46 | COL27 | LL | * | 2.20000 | NONE | 49900.98484- | .87000- | INFINITY | ROW16 | UL |
| | | | | | | 12631.57422 | .87000 | 1.33000 | COL22 | LL |
| 47 | COL28 | LL | * | 2.50000 | NONE | 49145.77344- | 1.17000- | INFINITY | ROW16 | UL |
| | | | | | | 12631.57422 | 1.17000 | 1.33000 | COL22 | LL |
| 48 | COL29 | LL | * | 1.20000 | NONE | INFINITY- | .28000- | INFINITY | NONE | UL |
| | | | | | | 4070.86328 | .28000 | 1.00000 | ROW16 | UL |
| 49 | COL30 | LL | * | 1.20000 | NONE | 55836.33904- | .28000- | INFINITY | ROW16 | UL |
| | | | | | | 16799.99659 | .28000 | 1.00000 | COL22 | LL |
| 51 | COL32 | LL | * | 2.70000 | NONE | 12444.44141 | 2.28103- | INFINITY | COL31 | LL |
| | | | | | | | 2.28103 | .41897 | COL22 | LL |
| 52 | COL33 | LL | * | 1.00000 | NONE | 43538.18750- | .20252- | INFINITY | COL49 | LL |
| | | | | | | 3402.33179 | .20252 | .79748 | COL40 | LL |
| 53 | COL34 | LL | * | 1.90000 | NONE | 5493.15625- | 1.49883- | INFINITY | COL49 | LL |
| | | | | | | 1663.15967 | 1.49883 | .40117 | COL40 | LL |
| 54 | COL35 | LL | * | 1.00000 | NONE | 19886.48047- | .22784- | INFINITY | COL49 | LL |
| | | | | | | 2784.18164 | .22784 | .77216 | COL40 | LL |
| 55 | COL36 | LL | * | 1.90000 | NONE | 3989.64819- | 1.62701- | INFINITY | COL49 | LL |
| | | | | | | 1339.95972 | 1.62701 | .27299 | COL40 | LL |
| 56 | COL37 | LL | * | 1.90000 | NONE | 24604.18750- | 1.20211- | INFINITY | COL49 | LL |
| | | | | | | 3206.71191 | 1.20211 | .69789 | COL40 | LL |
| 57 | COL38 | LL | * | 1.00000 | NONE | 4464.16016- | .75693- | INFINITY | COL49 | LL |
| | | | | | | 1501.23438 | .75693 | .24307 | COL40 | LL |
| 58 | COL39 | LL | * | 1.90000 | NONE | INFINITY- | .70033- | INFINITY | NONE | LL |
| | | | | | | 7293.23828 | .70033 | 1.19967 | COL40 | LL |
| 61 | COL42 | LL | * | 1.90000 | NONE | 23528.68750- | 1.00589- | INFINITY | COL49 | LL |
| | | | | | | | 1.00589 | .89411 | COL41 | LL |
| 62 | COL43 | LL | * | 2.70000 | NONE | 5230.44141 | 2.19591- | INFINITY | COL41 | LL |
| | | | | | | | 2.19591 | .50409 | COL49 | LL |
| 64 | COL45 | LL | * | 1.90000 | NONE | 4117.91953- | 1.50506- | INFINITY | COL49 | LL |
| | | | | | | | 1.50506 | .39494 | COL44 | LL |

| EXECUTOR. MPS/360 V2-M10 | | | | PAGE 20 - 72/194 | | | | | | |
|--------------------------|--------|----|-------------|------------------|---------------|------------------------------|---------------------|---------------------|----------------|----|
| NUMBER | COLUMN | AT | ACTIVITY... | INPUT COST.. | LOWER LIMIT.. | LOWER ACTIVITY | UNIT COST.. | UPPER COST.. | LIMITING | AT |
| | | | | | UPPER LIMIT. | UPPER ACTIVITY | UNIT COST.. | UPPER COST.. | PROCESS. | |
| 65 | COL46 | LL | * | 2.70000 | NONE | 2220.60449 | .50421- 2.50421 | INFINITY .19579 | COL44 COL40 | LL |
| 66 | COL47 | LL | * | 2.50000 | NONE | INFINITY- 5835.50000 | .87649- .87649 | INFINITY 1.62351 | NONE COL49 | LL |
| 67 | COL48 | LL | * | 2.20000 | NONE | INFINITY- 5835.50000 | .57649- .57649 | INFINITY 1.62351 | NONE COL49 | LL |
| 69 | COL50 | LL | * | 1.20000 | NONE | INFINITY- 8357.90625 | .13277- 1.0277 | INFINITY 1.09723 | NONE COL49 | LL |
| 70 | COL51 | LL | * | 1.00000 | NONE | 60555.57813- 10899.99609 | .15254- 15254 | INFINITY .84746 | ROW18 COL57 | UL |
| 71 | COL52 | LL | * | 1.90000 | NONE | 105780.62500- 10899.99609 | 1.05254- 1.05254 | INFINITY .84746 | ROW18 COL57 | UL |
| 72 | COL53 | LL | * | 1.00000 | NONE | 39562.60156- 11720.42578 | .21186- .21186 | INFINITY .78814 | ROW18 COL57 | UL |
| 73 | COL54 | LL | * | 1.90000 | NONE | 40585.28906- 11720.42578 | 1.11186- 1.11186 | INFINITY .78814 | ROW18 COL57 | UL |
| 74 | COL55 | LL | * | 1.00000 | NONE | 181666.68750- 9732.13672 | .05085- .05085 | INFINITY .94915 | ROW18 COL57 | UL |
| 75 | COL56 | LL | * | 1.90000 | NONE | INFINITY- 9732.13672 | .95085- .95085 | INFINITY .94915 | NONE COL57 | LL |
| 77 | COL58 | LL | * | 1.90000 | NONE | INFINITY- 4828.58281 | .90000- .90000 | INFINITY 1.00000 | NONE ROW18 | UL |
| 79 | COL60 | LL | * | 1.90000 | NONE | INFINITY- | .90000- .90000 | INFINITY 1.00000 | NONE COL59 | LL |
| 80 | COL61 | LL | * | 2.70000 | NONE | 973.96851 | 2.41667- 2.41667 | INFINITY .28333 | COL59 ROW18 | LL |
| 1 | COL62 | LL | * | 1.20000 | NONE | 348194.97500- 9881.32813 | .18305- .18305 | INFINITY 1.01695 | ROW18 COL57 | UL |
| 82 | COL63 | LL | * | 1.20000 | NONE | 113956.90000- 9819.81641 | .25932- .25932 | INFINITY .94068 | ROW18 COL57 | UL |

EXECUTOR. MPS/360 V2-M10

PAGE 21 - 72/194

SECTION 3 - ROWS AT INTERMEDIATE LEVEL

| NUMBER | ...ROW... | AT | ...ACTIVITY... | SLACK ACTIVITY | ..LOWER LIMIT.. ..UPPER LIMIT.. | LOWER ACTIVITY UPPER ACTIVITY | ...UNIT COST.. ...UNIT COST.. | ..UPPER COST.. ..LOWER COST.. | LIMITING PROCESS. | AT |
|--------|-----------|----|----------------|----------------|------------------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------|----------|
| 16 | ROW15 | BS | . | . | NONE | 3642.11621- 8945.96096 | 1.59205 | | COL 4 COL 17 | LL LL |
| 17 | ROW16 | BS | 4737.99766- | 4737.99766 | NONE | 6215.99707- 5123.99639 | 2.27273 .34072 | | COL 30 COL 29 | LL LL |
| 19 | ROW18 | BS | 4249.15234- | 4249.15234 | NONE | 5508.60083- 4249.15234- | 1.97161 .39130 | | COL 53 COL 60 | LL LL |

EXECUTOR. MPS/360 V2-M10

PAGE 22 - 72/194

SECTION 4 - COLUMNS AT INTERMEDIATE LEVEL

| NUMBER | ..COLUMN.. | AT | ...ACTIVITY... | ..INPUT COST.. | ..LOWER LIMIT.. ..UPPER LIMIT.. | LOWER ACTIVITY UPPER ACTIVITY | ...UNIT COST.. ...UNIT COST.. | ..UPPER COST.. ..LOWER COST.. | LIMITING PROCESS. | AT |
|--------|------------|----|----------------|----------------|------------------------------------|----------------------------------|----------------------------------|----------------------------------|----------------------|----------|
| 25 | COL 6 | BS | . | 1.00000 | NONE | . | .90030 1.19234 | 1.90000 .19234- | COL 7 COL 5 | LL LL |
| 28 | COL 9 | BS | . | 1.00000 | NONE | 6689.18359 | .90030 1.17903 | 1.90000 .17903- | COL 10 COL 8 | LL LL |
| 32 | COL 13 | BS | . | 1.00000 | NONE | 5593.21484 | .96774 1.21411 | 1.96774 .71411- | COL 12 COL 11 | LL LL |
| 33 | COL 14 | BS | . | 1.00000 | NONE | 5294.10938 | .90030 1.22621 | 1.90000 .22621- | COL 15 COL 16 | LL LL |
| 38 | COL 19 | BS | . | 1.20000 | NONE | 7674.41016 | INFINITY 1.24161 | INFINITY .04161- | NONE COL 21 | LL |
| 39 | COL 20 | BS | 7983.86719 | 1.20000 | NONE | 7983.86719 INFINITY | . 1.20000 | 1.20000 . | COL 17 ROW 1 | LL LL |
| 41 | COL 22 | BS | 16799.99609 | 1.00000 | NONE | 8729.13672 INFINITY | .20030 1.00000 | 1.20000 . | COL 29 ROW 7 | LL LL |
| 43 | COL 24 | BS | . | 1.00000 | NONE | 6598.32031- 7567.56250 | .90000 5.33747 | 1.90000 4.30747- | COL 25 COL 26 | LL LL |
| 50 | COL 31 | BS | . | 1.20000 | NONE | 9655.16797 | INFINITY 2.94000 | INFINITY 1.74000- | NONE COL 32 | LL |
| 59 | COL 40 | BS | 3425.11597 | 1.00000 | NONE | INFINITY- INFINITY | .18521 3.65946 | 1.18521 2.65946- | COL 35 ROW 10 | LL LL |
| 60 | COL 41 | BS | . | 1.00000 | NONE | 12177.86328- 5666.30859 | 1.00589 2.02699 | 2.00589 1.02699- | COL 42 COL 43 | LL LL |
| 63 | COL 44 | BS | . | 1.00000 | NONE | 2131.12695- 2664.72405 | 1.53506 2.08684 | 2.50506 1.08684- | COL 45 COL 46 | LL LL |
| 68 | COL 49 | BS | 7590.79688 | 1.20000 | NONE | 414705.76563- 11519.60547 | .11316 .32821 | 1.31316 .87179 | COL 50 ROW 17 | LL UL |
| 76 | COL 57 | BS | 9237.28516 | 1.00000 | NONE | INFINITY- INFINITY | .05357 1.00000 | 1.05357 . | COL 55 ROW 13 | LL LL |
| 78 | COL 59 | BS | . | 1.00000 | NONE | 1847.45726- 2035.15771 | .90000 1.15655 | 1.90000 .15655- | COL 60 COL 61 | LL LL |

APPENDIX B

MPS/360 PARAOBJ Computer Listing and Output for
Analysis of Overweight Truck Cost

As detailed in Section 4.2, the cost of over weight truck shipment was varied in order to examine the effect this cost variation would have on the solution. The computer results are summarized in Table VI. Only the PARAOBJ output corresponding to basis changes is contained in the following output. Pages 1 through 9 are also deleted as they are identical to pages 1 through 9 of Appendix A.

CONTROL PROGRAM COMPILER - PPS/360 V2-M10

PAGE 1 - 72/194

```

0001          PROGRAM
0002          INITIALJ
0003          MOVE(XDATA,'TRANS')
0004          MOVE(XPMAPL,'PROFILE')
0005          CONVERT('SUPMARY')
0006          SETUP('PLN')
0007          PICTURE
0008          BCTOUT
0009          MOVE(XOBJ,'COST')
0010          MOVE(XRMS,'LIMITS')
0011          PRIMAL
0012          * PARAOBJ
0013          * TESTOBJ TITLE('PARAOBJ')
0014          * MOVE (XCHMOD,'VARY')
0015          * PARAP=0.0
0016          * KPARAX=15.0
0017          * XPAROBL=1.0
0018          * PARAOBJ
0019          SOLUTION
0020          EXIT
0021          PEND

```

EXECUTOR. PPS/360 V2-M10

PAGE 10 - 72/194

PRIPAL OBJ = CCST RHS = LIMITS

TIME = 0.80 MINS. PRICING 7

| INVERT CALLED | TIME | 0.81 | CURRENT INVERSE | ETIA-VECTORS | ELEMENTS | RECORDS | ITERATION |
|---------------|-------------|------|-----------------|--------------|-------------|---------|-----------|
| BASIS | NO. OF REHS | 20 | LOGICALS | 20 | STRUCTURALS | 0 | 0 |
| INVERSE | NUCLEUS | 0 | TRANSFORMED | 0 | ELEMENTS | 20 | 0.00 |

PRIPAL OBJ = CCST RHS = LIMITS

TIME = 0.83 MINS. PRICING 7

| ITER | NUMBER | VECTOR | VECTOR | REDUCED | SUP |
|--------|--------|--------|--------|----------|---------|
| NUMBER | INFEAS | CLT | IN | COST | INFEAS |
| M 1 | 1 | 2 | 24 | 1.51000- | 39490.0 |
| M 2 | 2 | 11 | 67 | 1.40000- | 27700.0 |
| M 3 | 1 | 14 | 77 | 1.10000- | 16800.0 |
| M 4 | 0 | 8 | 47 | 1.10000- | . |

* FEASIBLE SOLUTION

PRIPAL OBJ = COST RHS = LIMITS

TIME = 0.86 MINS. PRICING 7

SCALE = 1.00000

| ITER | NUMBER | VECTOR | VECTOR | REDUCED | FUNCTION |
|--------|--------|--------|--------|----------|----------|
| NUMBER | INOPT | CLT | IN | COST | VALUE |
| M 5 | 32 | 10 | 44 | 2.67218- | 72432.7 |
| M 6 | | 6 | 34 | 1.72490- | 72432.7 |
| M 7 | | 9 | 51 | 1.67819- | 72432.7 |
| M 8 | | 5 | 33 | 1.57801- | 72432.7 |
| M 9 | | 13 | 64 | 1.50000- | 72432.7 |
| M 10 | | 3 | 26 | 1.31656- | 72432.7 |
| M 11 | 21 | 18 | 60 | 1.08428- | 69099.4 |
| M 12 | | 4 | 29 | 1.15629- | 69099.4 |
| M 13 | | 12 | 61 | .95021- | 65059.4 |
| M 14 | | 7 | 39 | .67947- | 69099.4 |
| M 15 | 11 | 47 | 42 | .65414- | 58110.0 |
| M 16 | | 67 | 69 | .67381- | 52995.2 |
| M 17 | | 24 | 40 | .60662- | 48152.0 |
| M 18 | 1 | 15 | 79 | .13559- | 48152.0 |

OPTIMAL SOLUTION

PARACBJ PAGE 1 - 72/194

PARACBJ OBJ = CCST RMS = LIPITS CMROW = VARY PARAP =

TIME = 0.96 MINS.

PARACBJ PAGE 2 - 72/194

SOLUTION (OPTIMAL)

TIME = 0.97 MINS. ITERATION NUMBER = 10

...NAME... ...ACTIVITY... DEFINED AS.....

FUNCTIONAL 48152.C0720 COST + 1.00000 VARY

RESTRAINTS LIMITS

PARACBJ PAGE 3 - 72/194

SECTION 1 - ROWS

| NUMBER | ...ROW... | A1 | ...ACTIVITY... | SLACK ACTIVITY | ..LOWER LIMIT.. | ..UPPER LIMIT.. | ..DUAL ACTIVITY |
|--------|-----------|----|----------------|----------------|-----------------|-----------------|-----------------|
| 1 | COST | BS | 48152.C0720 | 48152.C0720- | NONE | NONE | 1.00000 |
| 2 | ROW1 | LL | 9900.C0C00 | - | 9900.C0C00 | NONE | .96774- |
| 3 | ROW2 | EC | - | - | - | - | .33881 |
| 4 | ROW3 | EC | - | - | - | - | .29207 |
| 5 | ROW4 | EC | - | - | - | - | .40277 |
| 6 | ROW5 | EC | - | - | - | - | .43298 |
| 7 | ROW6 | EC | - | - | - | - | .03791 |
| 8 | ROW7 | LL | 16800.C0C00 | - | 16800.C0C00 | NONE | 1.00000- |
| 9 | ROW8 | EC | - | - | - | - | .31034- |
| 10 | ROW9 | EC | - | - | - | - | .55455 |
| 11 | ROW10 | LL | 11750.C0C00 | - | 11750.C0C00 | NONE | 1.06673- |
| 12 | ROW11 | EC | - | - | - | - | .27373 |
| 13 | ROW12 | EC | - | - | - | - | .02631 |
| 14 | ROW13 | LL | 10900.C0C00 | - | 10900.C0C00 | NONE | .84746- |
| 15 | ROW14 | EC | - | - | - | - | .10119 |
| 16 | ROW15 | BS | - | - | NONE | - | - |
| 17 | ROW16 | BS | 4737.6C070- | 4737.6C070- | NONE | - | .30253 |
| 18 | ROW17 | LL | - | - | NONE | - | - |
| 19 | ROW18 | BS | 4249.15254- | 4249.15254- | NONE | - | 1.00000 |
| 20 | VARY | BS | - | - | NONE | NONE | - |

PARACBJ

PAGE 4 - 72/194

SECTION 2 - COLUMNS

| NUMBER | COLUMN | AT | ...ACTIVITY... | ..INPUT COST.. | ..LOWER LIMIT. | ..UPPER LIMIT. | ..REDUCED COST. |
|--------|--------|----|----------------|----------------|----------------|----------------|-----------------|
| 21 | COL1 | LL | . | 1.00000 | . | NONE | .03226 |
| 22 | COL2 | LL | . | 1.80000 | . | NONE | .83226 |
| 23 | COL3 | LL | . | 2.90000 | . | NONE | 1.05871 |
| 24 | COL4 | LL | . | 2.70000 | . | NONE | .75871 |
| 25 | COL5 | LL | . | 2.70000 | . | NONE | 1.05975 |
| 26 | COL6 | BS | . | 1.00000 | . | NONE | . |
| 27 | COL7 | LL | . | 1.80000 | . | NONE | .80000 |
| 28 | COL8 | LL | . | 2.70000 | . | NONE | 1.07568 |
| 29 | COL9 | BS | . | 1.00000 | . | NONE | . |
| 30 | COL10 | LL | . | 1.80000 | . | NONE | .80000 |
| 31 | COL11 | LL | . | 2.70000 | . | NONE | 1.70113 |
| 32 | COL12 | LL | . | 1.80000 | . | NONE | .86774 |
| 33 | COL13 | BS | . | 1.00000 | . | NONE | . |
| 34 | COL14 | BS | . | 1.00000 | . | NONE | . |
| 35 | COL15 | LL | . | 1.80000 | . | NONE | .80000 |
| 36 | COL16 | LL | . | 2.70000 | . | NONE | 1.62620 |
| 37 | COL17 | LL | . | 1.20000 | . | NONE | . |
| 38 | COL18 | LL | . | 1.20000 | . | NONE | .04839 |
| 39 | COL19 | BS | . | 1.20000 | . | NONE | . |
| 40 | COL20 | BS | 7983.87087 | 1.20000 | . | NONE | . |
| 41 | COL21 | LL | . | 2.70000 | . | NONE | 2.59872 |
| 42 | COL22 | BS | 16800.00000 | 1.00000 | . | NONE | . |
| 43 | COL23 | LL | . | 1.80000 | . | NONE | .80000 |
| 44 | COL24 | BS | . | 1.00000 | . | NONE | . |
| 45 | COL25 | LL | . | 1.80000 | . | NONE | .80000 |
| 46 | COL26 | LL | . | 2.70000 | . | NONE | 2.19536 |
| 47 | COL27 | LL | . | 2.20000 | . | NONE | .87000 |
| 48 | COL28 | LL | . | 2.90000 | . | NONE | 1.17000 |
| 49 | COL29 | LL | . | 1.20000 | . | NONE | .20000 |
| 50 | COL30 | LL | . | 1.20000 | . | NONE | .20000 |
| 51 | COL31 | BS | . | 1.20000 | . | NONE | . |
| 52 | COL32 | LL | . | 2.70000 | . | NONE | 2.28103 |
| 53 | COL33 | LL | . | 1.00000 | . | NONE | .20252 |
| 54 | COL34 | LL | . | 1.80000 | . | NONE | 1.39883 |
| 55 | COL35 | LL | . | 1.00000 | . | NONE | .22784 |
| 56 | COL36 | LL | . | 1.80000 | . | NONE | 1.52701 |
| 57 | COL37 | LL | . | 1.80000 | . | NONE | 1.10211 |
| 58 | COL38 | LL | . | 1.00000 | . | NONE | .75893 |
| 59 | COL39 | LL | . | 1.80000 | . | NONE | .60033 |
| 60 | COL40 | BS | 3425.11671 | 1.00000 | . | NONE | . |
| 61 | COL41 | BS | . | 1.00000 | . | NONE | . |
| 62 | COL42 | LL | . | 1.80000 | . | NONE | .90589 |
| 63 | COL43 | LL | . | 2.70000 | . | NONE | 2.19991 |
| 64 | COL44 | BS | . | 1.00000 | . | NONE | . |
| 65 | COL45 | LL | . | 1.80000 | . | NONE | 1.40506 |
| 66 | COL46 | LL | . | 2.70000 | . | NONE | 2.50421 |
| 67 | COL47 | LL | . | 2.90000 | . | NONE | .87649 |
| 68 | COL48 | LL | . | 2.20000 | . | NONE | .97649 |
| 69 | COL49 | BS | 7590.79808 | 1.20000 | . | NONE | . |

PARACBJ

PAGE 5 - 72/194

| NUMBER | COLUMN | AT | ...ACTIVITY... | ..INPUT COST.. | ..LOWER LIMIT. | ..UPPER LIMIT. | ..REDUCED COST. |
|--------|--------|----|----------------|----------------|----------------|----------------|-----------------|
| 70 | COL50 | LL | . | 1.20000 | . | NONE | .10277 |
| 71 | COL51 | LL | . | 1.60000 | . | NONE | .19254 |
| 72 | COL52 | LL | . | 1.60000 | . | NONE | .95254 |
| 73 | COL53 | LL | . | 1.00000 | . | NONE | .21186 |
| 74 | COL54 | LL | . | 1.80000 | . | NONE | 1.01186 |
| 75 | COL55 | LL | . | 1.00000 | . | NONE | .05085 |
| 76 | COL56 | LL | . | 1.80000 | . | NONE | .85085 |
| 77 | COL57 | BS | 9237.28814 | 1.00000 | . | NONE | .80000 |
| 78 | COL58 | LL | . | 1.80000 | . | NONE | . |
| 79 | COL59 | BS | . | 1.00000 | . | NONE | .80000 |
| 80 | COL60 | LL | . | 1.80000 | . | NONE | 2.41667 |
| 81 | COL61 | LL | . | 2.70000 | . | NONE | .18305 |
| 82 | COL62 | LL | . | 1.20000 | . | NONE | .25932 |
| 83 | COL63 | LL | . | 1.20000 | . | NONE | . |

PARACEJ PAGE 36 - 72/194

PARAOBJ OBJ = COST RHS = LIMITS C-ROW = VARY PARAR = 7.00000

TIME = 1.49 MINS.

| ITER | NUMBER | VECTOR | VECTOR | REDUCED | FUNCTION | PARAM |
|--------|--------|--------|--------|---------|----------|---------|
| NUMBER | NONOPT | CLT | IN | COST | VALUE | VALUE |
| 19 | 0 | EO | 59 | .00013 | 40152-C | 7.00331 |

INVERT DEPENDANT AFTER 17 MAJOR/ 19 MINOR ITERATIONS - CLOCK CONTROL

INVERT CALLED TIME 1.50 CURRENT INVERSE ---- ETA-VECTORS23 ELEMENTS72 RECORDS1 ITERATION19

BASIS ---- NO.OF RCVS20 LOGICALS5 STRUCTURALS15 ELEMENTS60

INVERSE -- NUCLEUS2 TRANSFORMED1 ETA-VECTORS17 ELEMENTS37 RECORDS1 TIME TAKEN 0.00

PARAOBJ OBJ = COST RHS = LIMITS C-ROW = VARY PARAR = 7.00331

TIME = 1.50 MINS.

PARACEJ PAGE 37 - 72/194

SOLUTION (OPTIMAL)

TIME = 1.52 MINS. ITERATION NUMBER = 19

| NAME | ACTIVITY | DEFINED AS |
|------------|-------------|------------|
| FUNCTIONAL | 47429.09692 | COST |
| RESTRAINTS | | LIMITS |

PARACBJ PAGE 38 - 72/194

SECTION 1 - ROWS

| NUMBER | ROW | AI | ACTIVITY | SLACK ACTIVITY | LOWER LIMIT | UPPER LIMIT | DUAL ACTIVITY |
|--------|-------|----|-------------|----------------|-------------|-------------|---------------|
| 1 | COST | BS | 53259.68804 | 53259.68804- | NONE | NONE | 1.00000 |
| 2 | ROW1 | LL | 9900.CC000 | " | 9900.CC000 | NONE | .96774- |
| 3 | ROW2 | EC | " | " | " | " | .33881 |
| 4 | ROW3 | EC | " | " | " | " | .29207 |
| 5 | ROW4 | EC | " | " | " | " | .40277 |
| 6 | ROW5 | EC | " | " | " | " | .43298 |
| 7 | ROW6 | EC | " | " | " | " | .03751 |
| 8 | ROW7 | LL | 16800.CC000 | " | 16800.CC000 | NONE | 1.00000- |
| 9 | ROW8 | EC | " | " | " | " | .31034- |
| 10 | ROW9 | EC | " | " | " | " | .39455 |
| 11 | ROW10 | LL | 11750.CC000 | " | 11750.CC000 | NONE | 1.00486- |
| 12 | ROW11 | EC | " | " | " | " | .23461 |
| 13 | ROW12 | EC | " | " | " | " | .21629- |
| 14 | ROW13 | LL | 10900.CC000 | " | 10900.CC000 | NONE | .84746- |
| 15 | ROW14 | EC | " | " | " | " | .10119 |
| 16 | ROW15 | BS | " | " | NONE | " | " |
| 17 | ROW16 | BS | 4717.6CC00- | 4737.6CC00 | NONE | " | " |
| 18 | ROW17 | LL | " | " | NONE | " | .47307 |
| 19 | ROW18 | BS | 4249.19294- | 4249.15254 | NONE | " | " |
| 20 | VARY | BS | 729.32194- | 729.32154 | NONE | NONE | 0.00000 |

PARACEJ

PAGE 39 - 72/194

SECTION 2 - COLUMNS

| NUMBER | COLUMN | AT | ...ACTIVITY... | ..INPUT COST.. | ..LOWER LIMIT. | ..UPPER LIMIT. | ..REDUCED COST. |
|--------|--------|----|----------------|----------------|----------------|----------------|-----------------|
| 21 | COL1 | LL | . | 1.00000 | . | NONE | .03226 |
| 22 | COL2 | LL | . | 1.10000 | . | NONE | .13226 |
| 23 | COL3 | LL | . | 2.50000 | . | NONE | 1.03871 |
| 24 | COL4 | LL | . | 2.20000 | . | NONE | .73871 |
| 25 | COL5 | LL | . | 2.70000 | . | NONE | 1.05975 |
| 26 | COL6 | BS | . | 1.00000 | . | NONE | . |
| 27 | COL7 | LL | . | 1.10000 | . | NONE | .10000 |
| 28 | COL8 | LL | . | 2.70000 | . | NONE | 1.97568 |
| 29 | COL9 | BS | . | 1.00000 | . | NONE | . |
| 30 | COL10 | LL | . | 1.10000 | . | NONE | .10000 |
| 31 | COL11 | LL | . | 2.70000 | . | NONE | 1.70113 |
| 32 | COL12 | LL | . | 1.10000 | . | NONE | .16774 |
| 33 | COL13 | BS | . | 1.00000 | . | NONE | . |
| 34 | COL14 | BS | . | 1.00000 | . | NONE | . |
| 35 | COL15 | LL | . | 1.10000 | . | NONE | .10000 |
| 36 | COL16 | LL | . | 2.70000 | . | NONE | 1.62676 |
| 37 | COL17 | LL | . | 1.20000 | . | NONE | . |
| 38 | COL18 | LL | . | 1.20000 | . | NONE | .04439 |
| 39 | COL19 | BS | . | 1.20000 | . | NONE | . |
| 40 | COL20 | BS | 7983.87007 | 1.20000 | . | NONE | . |
| 41 | COL21 | LL | . | 2.70000 | . | NONE | 2.59872 |
| 42 | COL22 | BS | 16800.00000 | 1.00000 | . | NONE | . |
| 43 | COL23 | LL | . | 1.10000 | . | NONE | .10000 |
| 44 | COL24 | BS | . | 1.00000 | . | NONE | . |
| 45 | COL25 | LL | . | 1.10000 | . | NONE | .10000 |
| 46 | COL26 | LL | . | 2.70000 | . | NONE | 2.19536 |
| 47 | COL27 | LL | . | 2.20000 | . | NONE | .07000 |
| 48 | COL28 | LL | . | 2.50000 | . | NONE | 1.17000 |
| 49 | COL29 | LL | . | 1.20000 | . | NONE | .20000 |
| 50 | COL30 | LL | . | 1.20000 | . | NONE | .20000 |
| 51 | COL31 | BS | . | 1.20000 | . | NONE | . |
| 52 | COL32 | LL | . | 2.70000 | . | NONE | 2.28103 |
| 53 | COL33 | LL | . | 1.00000 | . | NONE | .41617 |
| 54 | COL34 | LL | . | 1.10000 | . | NONE | 1.13590 |
| 55 | COL35 | LL | . | 1.00000 | . | NONE | .48893 |
| 56 | COL36 | LL | . | 1.10000 | . | NONE | 1.36950 |
| 57 | COL37 | LL | . | 1.10000 | . | NONE | .62880 |
| 58 | COL38 | LL | . | 1.00000 | . | NONE | 1.24314 |
| 59 | COL39 | BS | 7293.23439 | 1.10000 | . | NONE | . |
| 60 | COL40 | LL | . | 1.00000 | . | NONE | .21223 |
| 61 | COL41 | BS | . | 1.00000 | . | NONE | . |
| 62 | COL42 | LL | . | 1.10000 | . | NONE | .26558 |
| 63 | COL43 | LL | . | 2.70000 | . | NONE | 2.16320 |
| 64 | COL44 | BS | . | 1.00000 | . | NONE | . |
| 65 | COL45 | LL | . | 1.10000 | . | NONE | 1.04615 |
| 66 | COL46 | LL | . | 2.70000 | . | NONE | 2.83156 |
| 67 | COL47 | LL | . | 2.90000 | . | NONE | .88977 |
| 68 | COL48 | LL | . | 2.20000 | . | NONE | .58977 |
| 69 | COL49 | BS | 3155.83375 | 1.20000 | . | NONE | . |

PARACEJ

PAGE 40 - 72/194

| NUMBER | COLUMN | AT | ...ACTIVITY... | ..INPUT COST.. | ..LOWER LIMIT. | ..UPPER LIMIT. | ..REDUCED COST. |
|--------|--------|----|----------------|----------------|----------------|----------------|-----------------|
| 70 | COL50 | LL | . | 1.20000 | . | NONE | .10434 |
| 71 | COL51 | LL | . | 1.00000 | . | NONE | .15254 |
| 72 | COL52 | LL | . | 1.10000 | . | NONE | .25254 |
| 73 | COL53 | LL | . | 1.60000 | . | NONE | .21186 |
| 74 | COL54 | LL | . | 1.10000 | . | NONE | .31186 |
| 75 | COL55 | LL | . | 1.00000 | . | NONE | .05085 |
| 76 | COL56 | LL | . | 1.10000 | . | NONE | .15085 |
| 77 | COL57 | BS | 9237.20814 | 1.00000 | . | NONE | . |
| 78 | COL58 | LL | . | 1.10000 | . | NONE | .10000 |
| 79 | COL59 | BS | . | 1.00000 | . | NONE | . |
| 80 | COL60 | LL | . | 1.10000 | . | NONE | .10000 |
| 81 | COL61 | LL | . | 2.70000 | . | NONE | 2.41667 |
| 82 | COL62 | LL | . | 1.20000 | . | NONE | .18305 |
| 83 | COL63 | LL | . | 1.20000 | . | NONE | .25932 |

PARACBJ
 PAKOBJ OBJ = CCST RMS = LIMITS CHROM = VARY PARAM = 9.C0000
 TIME = 1.62 MINS.

| ITER NUMBER | NUMBER NCHOPT | VECTOR CLT | VECTOR IN | PRODUCED COST | FUNCTION VALUE | PARAP VALUE |
|----------------|------------------|---------------|--------------|------------------|-------------------|----------------|
| M 20 | 0 | 16 | 27 | - | 46695.0 | 9.00000 |
| M 21 | 0 | 42 | 43 | - | 46695.0 | 9.00000 |
| M 22 | 0 | 44 | 45 | - | 46695.0 | 9.00000 |
| M 23 | 0 | 19 | 78 | - | 46695.0 | 9.00000 |
| M 24 | 0 | 29 | 30 | - | 46695.0 | 9.00000 |
| M 25 | 0 | 14 | 33 | - | 46695.0 | 9.00000 |
| M 26 | 0 | 77 | 76 | -.05089 | 45214.0 | 9.51232 |
| M 27 | 0 | 33 | 32 | -.03117 | 43731.0 | 9.95411 |

PAGE 46 - 72/194

PARACBJ
 SOLUTION (OPTIMAL)
 TIME = 1.64 MINS. ITERATION NUMBER = 27

| NAME | ACTIVITY | DEFINIC AS |
|------------|-------------|----------------------|
| FUNCTIONAL | 43576.97806 | CCST + 10.00000 VARY |
| RESTRAINTS | | LIMITS |

PAGE 47 - 72/194

PARACBJ
 SECTION 1 - ROWS

| NUMBER | ROW | AT | ACTIVITY | SLACK ACTIVITY | LOWER LIMIT | UPPER LIMIT | DUAL ACTIVITY |
|--------|-------|----|-------------|----------------|-------------|-------------|---------------|
| 1 | COST | BS | 77145.57028 | 77145.57028- | NONE | NONE | 1.00000 |
| 2 | ROW1 | LL | 9900.00000 | - | 5900.00000 | NONE | -.96774- |
| 3 | ROW2 | EC | - | - | - | - | -.30212 |
| 4 | ROW3 | EC | - | - | - | - | -.35400 |
| 5 | ROW4 | EC | - | - | - | - | -.41177 |
| 6 | ROW5 | EC | - | - | - | - | -.48040 |
| 7 | ROW6 | EC | - | - | - | - | -.05786 |
| 8 | ROW7 | LL | 16800.00000 | - | 16800.00000 | NONE | -.90000- |
| 9 | ROW8 | EC | - | - | - | - | -.21034- |
| 10 | ROW9 | EC | - | - | - | - | -.49909 |
| 11 | ROW10 | LL | 11750.00000 | - | 11750.00000 | NONE | -.00072- |
| 12 | ROW11 | EC | - | - | - | - | -.15610 |
| 13 | ROW12 | EC | - | - | - | - | -.70710- |
| 14 | ROW13 | LL | 10900.00000 | - | 10900.00000 | NONE | -.78237- |
| 15 | ROW14 | EC | - | - | - | - | -.03808- |
| 16 | ROW15 | UL | - | - | NONE | - | -.00333 |
| 17 | ROW16 | RS | 1344.00000- | 1344.00000 | NONE | - | - |
| 18 | ROW17 | UL | - | - | NONE | - | -.01530 |
| 19 | ROW18 | UL | - | - | NONE | - | -.05523 |
| 20 | VARY | BS | 3356.85922- | 3356.85922 | NONE | NONE | 10.00000 |

PAGE 48 - 72/194

PARADIS
SECTION 2 - COLUMNS

PAGE 40 - 72/194

| NUMBER | COLUMN | AT | ACTIVITY... | INPUT COST.. | LOWER LIMIT. | UPPER LIMIT. | REDUCED COST. |
|--------|--------|----|-------------|--------------|--------------|--------------|---------------|
| 21 | COL1 | LL | . | 1.00000 | . | NONE | .09192 |
| 22 | COL2 | LL | . | .90000 | . | NONE | .01926 |
| 23 | COL3 | LL | . | 2.90000 | . | NONE | .99904 |
| 24 | COL4 | LL | . | 2.20000 | . | NONE | .70004 |
| 25 | COL5 | LL | . | 2.70000 | . | ACNE | 1.91223 |
| 26 | COL6 | BS | . | 1.00000 | . | NONE | . |
| 27 | COL7 | BS | . | .90000 | . | NONE | . |
| 28 | COL8 | LL | . | 2.70000 | . | NONE | 1.70357 |
| 29 | COL9 | LL | . | 1.00000 | . | NONE | .07500 |
| 30 | COL10 | BS | . | .90000 | . | NONE | . |
| 31 | COL11 | LL | . | 2.70000 | . | NONE | 1.64032 |
| 32 | COL12 | BS | . | .90000 | . | NONE | . |
| 33 | COL13 | LL | . | 1.00000 | . | NONE | .00326 |
| 34 | COL14 | LL | . | 1.00000 | . | NONE | .07350 |
| 35 | COL15 | BS | . | .90000 | . | ACNE | . |
| 36 | COL16 | LL | . | 2.70000 | . | NONE | 1.47011 |
| 37 | COL17 | LL | . | 1.20000 | . | NONE | .07250 |
| 38 | COL18 | LL | . | 1.20000 | . | NONE | .12505 |
| 39 | COL19 | BS | . | 1.20000 | . | NONE | . |
| 40 | COL20 | PS | 7983.87097 | 1.20000 | . | NONE | . |
| 41 | COL21 | LL | . | 2.70000 | . | NONE | 2.51678 |
| 42 | COL22 | LL | . | 1.00000 | . | NONE | .10000 |
| 43 | COL23 | BS | 16800.00000 | .90000 | . | NONE | . |
| 44 | COL24 | LL | . | 1.00000 | . | NONE | .10000 |
| 45 | COL25 | BS | . | .90000 | . | NONE | . |
| 46 | COL26 | LL | . | 2.70000 | . | NONE | 2.24583 |
| 47 | COL27 | LL | . | 2.20000 | . | NONE | 1.00300 |
| 48 | COL28 | LL | . | 2.90000 | . | NONE | 1.30300 |
| 49 | COL29 | LL | . | 1.20000 | . | NONE | .10000 |
| 50 | COL30 | LL | . | 1.20000 | . | NONE | .30000 |
| 51 | COL31 | BS | . | 1.20000 | . | NONE | . |
| 52 | COL32 | LL | . | 2.70000 | . | NONE | 2.41603 |
| 53 | COL33 | LL | . | 1.00000 | . | NONE | .84489 |
| 54 | COL34 | LL | . | .90000 | . | NONE | 1.81293 |
| 55 | COL35 | LL | . | 1.00000 | . | NONE | 1.01283 |
| 56 | COL36 | LL | . | .90000 | . | NONE | 2.29808 |
| 57 | COL37 | LL | . | .90000 | . | NONE | .68367 |
| 58 | COL38 | LL | . | 1.00000 | . | NONE | 2.21477 |
| 59 | COL39 | BS | 7293.23939 | .90000 | . | NONE | . |
| 60 | COL40 | LL | . | 1.00000 | . | NONE | .63810 |
| 61 | COL41 | BS | . | 1.00000 | . | NONE | . |
| 62 | COL42 | LL | . | .90000 | . | NONE | .18535 |
| 63 | COL43 | LL | . | 2.70000 | . | NONE | 2.09750 |
| 64 | COL44 | BS | . | 1.00000 | . | NONE | . |
| 65 | COL45 | LL | . | .90000 | . | NONE | 1.53060 |
| 66 | COL46 | LL | . | 2.70000 | . | NONE | 3.48842 |
| 67 | COL47 | LL | . | 2.50000 | . | NONE | .91641 |
| 68 | COL48 | LL | . | 2.20000 | . | NONE | .61641 |
| 69 | COL49 | BS | 3153.89325 | 1.20000 | . | NONE | . |

PARADIS
SECTION 2 - COLUMNS

PAGE 50 - 72/194

| NUMBER | COLUMN | AT | ACTIVITY... | INPUT COST.. | LOWER LIMIT. | UPPER LIMIT. | REDUCED COST. |
|--------|--------|----|-------------|--------------|--------------|--------------|---------------|
| 70 | COL50 | LL | . | 1.20000 | . | NONE | .10747 |
| 71 | COL51 | LL | . | 1.00000 | . | NONE | .19223 |
| 72 | COL52 | LL | . | .90000 | . | NONE | .09380 |
| 73 | COL53 | LL | . | 1.00000 | . | NONE | .24644 |
| 74 | COL54 | LL | . | .90000 | . | NONE | .18755 |
| 75 | COL55 | LL | . | 1.00000 | . | NONE | .09834 |
| 76 | COL56 | BS | 4681.93905 | .90000 | . | NONE | . |
| 77 | COL57 | LL | . | 1.00000 | . | NONE | .05140 |
| 78 | COL58 | BS | 4793.41379 | .90000 | . | NONE | . |
| 79 | COL59 | BS | . | 1.00000 | . | NONE | . |
| 80 | COL60 | LL | . | .90000 | . | NONE | .02702 |
| 81 | COL61 | LL | . | 2.70000 | . | NONE | 2.77950 |
| 82 | COL62 | LL | . | 1.20000 | . | NONE | .23463 |
| 83 | COL63 | LL | . | 1.20000 | . | NONE | .30561 |

PARABJ
 PARABJ OBJ = CCST RMS = LIMITS CHROW = VARY PARAR = 10.0000
 TIME = 1.68 MINS.

| ITER | NUMBER | VECTOR | VECTOR | REDUCED | FUNCTION | PARAM |
|------|--------|--------|--------|---------|----------|---------|
| N | NUMBER | NOOPT | OLT | IN | COST | VALUE |
| 28 | 0 | 79 | 80 | .02702 | 42782.1 | 10.2368 |
| 29 | 0 | 27 | 22 | .00876 | 41234.6 | 10.6978 |

PAGE 91 - 72/194

PARABJ
 SOLUTION (OPTIMAL)
 TIME = 1.69 MINS. ITERATION NUMBER = 29

| NAME | ACTIVITY | DEFINED AS |
|------------|-------------|---------------------|
| FUNCTIONAL | 4C220.11AP4 | COST + 11.0000 VARY |
| RESTRAINTS | | LIMITS |

PAGE 92 - 72/194

PARABJ
 SECTION 1 - ROWS

| NUMBER | ROW | ST | ACTIVITY | SLACK | ACTIVITY | LOWER LIMIT | UPPER LIMIT | DUAL ACTIVITY |
|--------|-------|----|-------------|-------------|-------------|-------------|-------------|---------------|
| 1 | COST | ES | 77149.57028 | 77149.57028 | NONE | NONE | 1.00000 | |
| 2 | ROW1 | LL | 9900.00000 | | 9900.00000 | NONE | .96774 | |
| 3 | ROW2 | EC | | | | | .26284 | |
| 4 | ROW3 | EC | | | | | .41554 | |
| 5 | ROW4 | EC | | | | | .45838 | |
| 6 | ROW5 | EC | | | | | .52138 | |
| 7 | ROW6 | EC | | | | | .07965 | |
| 8 | ROW7 | LL | 16800.00000 | | 16800.00000 | NONE | .00000 | |
| 9 | ROW8 | EC | | | | | .11034 | |
| 10 | ROW9 | EC | | | | | .44364 | |
| 11 | ROW10 | LL | 11750.00000 | | 11750.00000 | NONE | .01865 | |
| 12 | ROW11 | EC | | | | | .11684 | |
| 13 | ROW12 | EC | | | | | .95250 | |
| 14 | ROW13 | LL | 10900.00000 | | 10900.00000 | NONE | .69544 | |
| 15 | ROW14 | EC | | | | | .05176 | |
| 16 | ROW15 | LL | | | | | .17257 | |
| 17 | ROW16 | ES | 1344.00000 | 1344.00000 | NONE | | .98641 | |
| 18 | ROW17 | UL | | | | | .04909 | |
| 19 | ROW18 | LL | | | | | .04909 | |
| 20 | VARY | ES | 1356.89422 | 1356.89422 | NONE | NONE | 11.00000 | |

PAGE 93 - 72/194

PARACPJ
SECTION 2 - COLUMNS

PAGE 54 - 72/194

| NUMBER | COLUMN | AT | ...ACTIVITY... | ..INPUT COST.. | ..LOWER LIMIT. | ..UPPER LIMIT. | ..REDUCED COST. |
|--------|--------|----|----------------|----------------|----------------|----------------|-----------------|
| 21 | COL1 | LL | . | 1.CCCCN | . | NONE | .07299 |
| 22 | COL2 | PS | . | .8CCCO | . | NONE | . |
| 23 | COL3 | LL | . | 2.9CCCO | . | NONE | .99656 |
| 24 | COL4 | LL | . | 2.7CCCO | . | NONE | .49864 |
| 25 | COL5 | LL | . | 2.7CCCO | . | NONE | 1.96844 |
| 26 | COL6 | PS | . | 1.CCCCO | . | NONE | . |
| 27 | COL7 | LL | . | .8CCCO | . | NONE | .00709 |
| 28 | COL8 | LL | . | 2.7CCCO | . | NONE | 1.58973 |
| 29 | COL9 | LL | . | 1.CCCCO | . | NONE | .14823 |
| 30 | COL10 | PS | . | .8CCCO | . | NONE | . |
| 31 | COL11 | LL | . | 2.7CCCO | . | NONE | 1.40348 |
| 32 | COL12 | PS | . | .8CCCO | . | NONE | . |
| 33 | COL13 | LL | . | 1.CCCCO | . | NONE | .07220 |
| 34 | COL14 | LL | . | 1.CCCCO | . | NONE | .14912 |
| 35 | COL15 | PS | . | .8CCCO | . | NONE | . |
| 36 | COL16 | LL | . | 2.7CCCO | . | NONE | 1.31236 |
| 37 | COL17 | LL | . | 1.2CCCO | . | NONE | .15014 |
| 38 | COL18 | LL | . | 1.2CCCO | . | NONE | .20716 |
| 39 | COL19 | PS | . | 1.2CCCO | . | NONE | . |
| 40 | COL20 | PS | 7985.87997 | 1.2CCCO | . | NONE | . |
| 41 | COL21 | LL | . | 2.7CCCO | . | NONE | 2.42903 |
| 42 | COL22 | LL | . | 1.CCCCO | . | NONE | .20000 |
| 43 | COL23 | PS | 16807.CCCNO | .8CCCO | . | NONE | . |
| 44 | COL24 | LL | . | 1.CCCCO | . | NONE | .20000 |
| 45 | COL25 | PS | . | .8CCCO | . | NONE | . |
| 46 | COL26 | LL | . | 2.9CCCO | . | NONE | 2.29629 |
| 47 | COL27 | LL | . | 2.9CCCO | . | NONE | 1.116C0 |
| 48 | COL28 | LL | . | 2.5CCCO | . | NONE | 1.41600 |
| 49 | COL29 | LL | . | 1.2CCCO | . | NONE | .400C0 |
| 50 | COL30 | LL | . | 1.2CCCO | . | NONE | .400C0 |
| 51 | COL31 | PS | . | 1.2CCCO | . | NONE | . |
| 52 | COL32 | LL | . | 2.7CCCO | . | NONE | 2.55103 |
| 53 | COL33 | LL | . | 1.CCCCO | . | NONE | 1.05923 |
| 54 | COL34 | LL | . | .8CCCO | . | NONE | 2.15145 |
| 55 | COL35 | LL | . | 1.CCCCO | . | NONE | 1.27479 |
| 56 | COL36 | LL | . | .8CCCO | . | NONE | 2.70237 |
| 57 | COL37 | LL | . | .8CCCO | . | NONE | 1.01111 |
| 58 | COL38 | LL | . | 1.CCCCO | . | NONE | 2.70059 |
| 59 | COL39 | PS | 7293.23939 | .8CCCO | . | NONE | . |
| 60 | COL40 | LL | . | 1.CCCCO | . | NONE | .85103 |
| 61 | COL41 | PS | . | 1.CCCCO | . | NONE | . |
| 62 | COL42 | LL | . | .8CCCO | . | NONE | .14524 |
| 63 | COL43 | LL | . | 2.7CCCO | . | NONE | 2.06476 |
| 64 | COL44 | PS | . | 1.CCCCO | . | NONE | . |
| 65 | COL45 | LL | . | .8CCCO | . | NONE | 1.77262 |
| 66 | COL46 | LL | . | 2.7CCCO | . | NONE | 3.81686 |
| 67 | COL47 | LL | . | 2.9CCCO | . | NONE | .92973 |
| 68 | COL48 | LL | . | 2.2CCCO | . | NONE | .62973 |
| 69 | COL49 | PS | 3153.83325 | 1.2CCCO | . | NONE | . |

PARACPJ

PAGE 55 - 72/194

| NUMBER | COLUMN | AT | ...ACTIVITY... | ..INPUT COST.. | ..LOWER LIMIT. | ..UPPER LIMIT. | ..REDUCED COST. |
|--------|--------|----|----------------|----------------|----------------|----------------|-----------------|
| 70 | COL50 | LL | . | 1.2CCCO | . | NONE | .10904 |
| 71 | COL51 | LL | . | 1.CCCCO | . | NONE | .28198 |
| 72 | COL52 | LL | . | .8CCCO | . | NONE | .08345 |
| 73 | COL53 | LL | . | 1.CCCCO | . | NONE | .33017 |
| 74 | COL54 | LL | . | .8CCCO | . | NONE | .13115 |
| 75 | COL55 | LL | . | 1.CCCCO | . | NONE | .19853 |
| 76 | COL56 | PS | 4681.93905 | .8CCCO | . | NONE | . |
| 77 | COL57 | LL | . | 1.CCCCO | . | NONE | .15680 |
| 78 | COL58 | PS | 4793.41779 | .8CCCO | . | NONE | . |
| 79 | COL59 | LL | . | 1.CCCCO | . | NONE | .08709 |
| 80 | COL60 | PS | . | .8CCCO | . | NONE | . |
| 81 | COL61 | LL | . | 2.7CCCO | . | NONE | 2.82092 |
| 82 | COL62 | LL | . | 1.2CCCO | . | NONE | .34191 |
| 83 | COL63 | LL | . | 1.2CCCO | . | NONE | .40499 |

OPTIMIZATION OF ROUTES AND MODES OF
NUCLEAR MATERIAL TRANSPORTATION CONSTRAINED
BY SAFETY CONSIDERATIONS

by

JAY PAUL ODOM

B.S., Kansas State University

AN ABSTRACT OF A MASTER'S THESIS
submitted in partial fulfillment of the
requirements for the degree
MASTER OF SCIENCE

Department of Nuclear Engineering

KANSAS STATE UNIVERSITY

Manhattan, Kansas

1972

ABSTRACT

The amount of spent fuel from reactors which is to be shipped in the near future may grow to a level sufficient enough to limit the development of the nuclear power industry. Specifically, the complexity of determining the most economic route and mode while satisfying safety restrictions will most likely lead to increasingly non-optimal or unsafe shipments as the amount of spent fuel to be shipped increases.

The purpose of this work was to develop and analyze a model which characterizes the choice of route and mode for spent fuel shipment from one of several reactors constrained by safety considerations. A model was established which represents the choice of route and mode constrained by a safety factor. The safety factor employed is a function of probability of accident and severity of accident.

The complexity of analyzing such a model implies a computer approach. This model is analyzed with linear programming through a computer package, Mathematical Programming System (MPS). MPS efficiently handles the model formulated in this work and can evidently handle more complex situations. That is the least expensive route and mode was found for the model, while satisfying the safety requirements. In addition, the flexibility of MPS is demonstrated through the use of parametric programming which modifies specified parameters of the model.